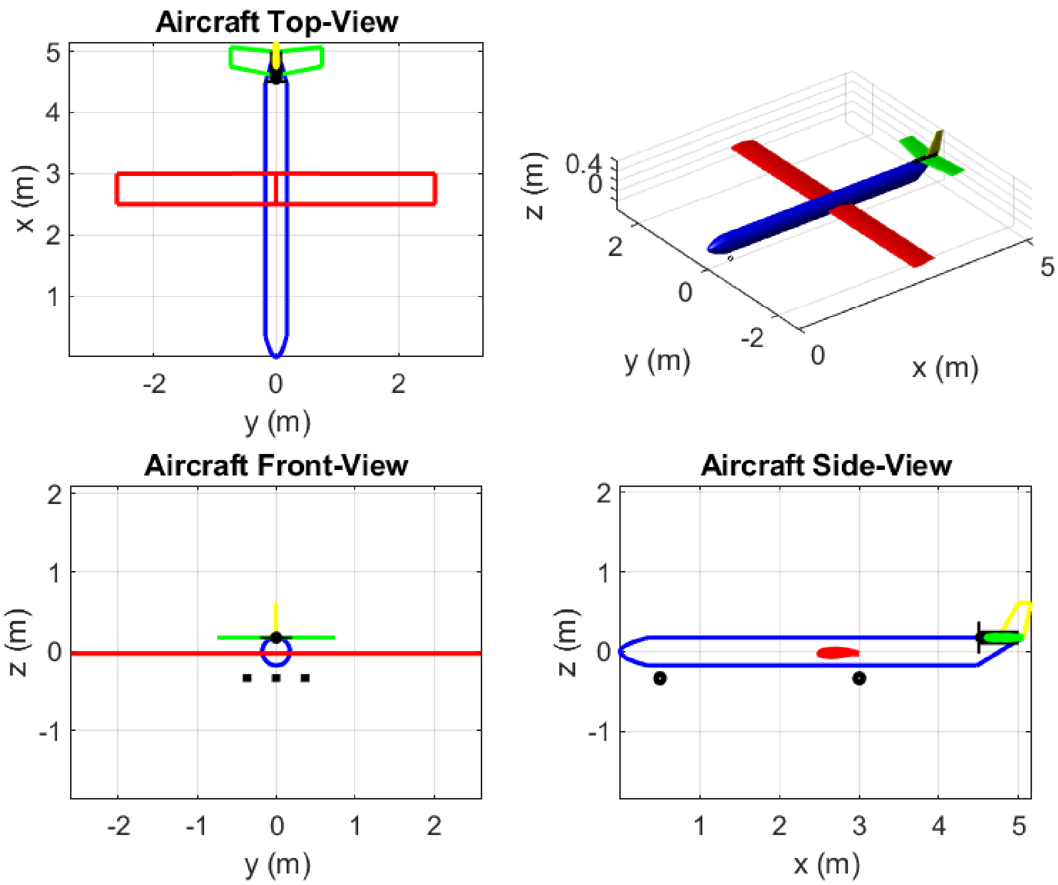
Flight Loads: DroneVLA aircraft



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Design of Aircraft and Flight Technologies, DAF

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Chapter 1. Introduction

This document defines the SUBPART C - Structure - Flight Loads of the:DroneVLA.The boundaries of the flight envelope will be defined within this document. All speeds are calibrated airspeeds (CAS) (requirement 4.4 [1])and given in knots if not stated otherwise.All other units used are metric (SI units).The weights are given in mass units (kg) but the formulas require force units as input,therefore these are calculated in place wherever they are used.Note: The speeds defined within this document should be used for the placards,speed markings, aeroplane flight manual (limitations), load calculations and need to be verified by flight test.

Chapter 2. References

1. ASTM F2245-12d," ASTM."ASTM F2245-12d, ASTM.
2. ABCD-FL-57-00 Wing Load Calculation, EASA.
3. ISO 2533:1975, International Standardization Organization, 1975.
4. CS-LSA Certification Specifications and Acceptable Means of Compliance, Amnd.1 29.Jul.2013, EASA, 2013.
5. "ABCD-FTR-01-00 Flight Test Report," EASA.
6. L. Smith, "NACA technical note 1945, 'Aerodynamic characteristics of 15 NACA airfoil sections at seven Reynolds numbers from 0.7x10E6 to 9x10E6," 1949.
7. ABCD-WB-08-00 Weight and Balance Report, EASA.

HERE BELOW AN EXAMPLE OF REFERENCES TO BE EDITED

Chapter 3. List of Abbreviations

- CL = lift coefficient
- CD....
- ...
- ...
- ...
- ...
- ...

ADD HERE list of abbreviations as a formatted table....to be created

Chapter 4. Aircraft data

The aircraft geometrical, masses, inertial and aerodynamic data, useful for flight loads estimation are summarized in this chapter.

4.1. Geometry

The aircraft reference geometrical characteristics are summarized in the following tables.Wing parameters

Table 4.1. Wing parameters

Wing parameters	Value	Measure unit
b	5.2	m
S	2.589	m^2
AR	10.446	-
taper	NaN	-
sweep	0	deg
sweep_location	0	percentage
secondary_sweep_location	0	percentage
croot	0.498	m
ctip	0.498	m
xle	1.638	m
yle	0	m
zle	0.165	m
xtip_le	NaN	% fuselage length
dihedral	0	deg
mac	0.498	m
xmac	NaN	% fuselage length
ymac	NaN	% semispan
ypos	NaN	% semispan
zpos	NaN	% fuselage diameter
camberloc	0.15	Percentage
thickchord	0.18	Percentage
type	Rectangular	flag
twist_angle	3	deg
chord_kink_one	0.498	m
chord_kink_two	0.498	m
panel_span1	0.33	Semispan percentage
panel_span2	0.33	Semispan percentage

Wing parameters	Value	Measure unit
panel_span3	0.33	Semispan percentage
mgc	0.49788	m
taper_ratio	1	Non dimensional

Table 4.2. Horizontal Tail parameters

Horizontal parameters	Value	Measure unit
S	0.529	m^2
l	1.492	m
camber	0	percentage
camberloc	NaN	percentage
thickchord	0.12	percentage
twist	0	deg
twistloc	0.25	percentage
xloc0	1.49	m
xloc	3.128	m
yloc	0	m
zloc	0.15	m
xrot	0	m
yrot	0	m
zrot	0	m
b	1.496	m
ctip	0.3136	m
croot	0.3929	m
sweep	15	deg
sweeploc	0	percentage
secsweeploc	1	percentage
dihedral	0	deg
location_of_camber	0.2	percentage
secondary_sweep_location	1	percentage
ce_c_root	0.34	Non dimensional
ce_c_tip	0.36	Non dimensional

Table 4.3. Vertical Tail parameters

Vertical parameters	Value	Measure unit
xle	0.95	% of fuselage length
croot	0.3136	m
ctip	0.15347	m

Vertical parameters	Value	Measure unit
xtip_le	1	% of fuselage length
b	0.4375	m
zpos	1	% of df
S	0.1022	m^2
chord	0.3136	m
MAC	0.23354	m
l_vt	1.65	m
empennage_flag	Double fin	NaN

Table 4.4. Fuselage parameters

Fuselage parameters	Value	Measure unit
length	3.64	Non dimensional
diameter	0.42	Non dimensional
Non_dim_radius_of_gyration	0.34	Non dimensional
Radius_of_gyration	NaN	m

Table 4.5. Elevator parameters

Elevator parameters	Value	Measure unit
S	0.14749	m^2
chord	0.12324	m
chord_ratio_ce_c	0.35	Non dimensional
overhang	0.12	Non dimensional
span_ratio	0.8	Non dimensional
S_hinge	0.126	m^2
eta_inner	0.1	percentage
eta_outer	0.9	percentage
cf_c_inner	0.3	percentage
cf_c_outer	0.3	percentage
y_inner	0.0748	m
y_outer	0.6732	m
cf	0.10845	m
moment_arm	0.016021	m

Table 4.6. Rudder parameters

Rudder parameters	Value	Measure unit
S	0.019062	m^2
chord	0.10893	m

Rudder parameters	Value	Measure unit
chord_ratio_cf_c	0.35	Non dimensional
overhang	0.12	Non dimensional
span_ratio	0.8	Non dimensional
cr_c_root	0.45	Non dimensional
cr_c_tip	0.5	Non dimensional
eta_inner	0.1	Non dimensional
eta_outer	0.9	Non dimensional
croot	0.14112	m
ctip	0.076735	m
y_inner	0.021875	m
y_outer	0.19688	m
moment_arm	0.014161	m

Table 4.7. Aileron parameters

Aileron parameters	Value	Measure unit
S	0.14018	m^2
b	0.908	m
ca	0.15438	m
cb	0.019	m
y_inner	1.63	m
y_outer	2.538	m
eta_inner	0.627	Non dimensional
eta_outer	0.976	Non dimensional
ca_c_inner	0.31	Non dimensional
ca_c_outer	0.31	Non dimensional
croot	0.15438	m
ctip	0.15438	m
cf	0.13538	m
moment_arm	0.016928	m

4.2. Masses and inertia

The aircraft reference masses and inertia are summarized in this subsection

The Aircraft masses and inertia are summarized in Table: Weight parameters

Table 4.8. Weight parameters

Weight	Value	Measure unit
W_maxTakeOff	100	kg

Weight	Value	Measure unit
W_OperativeEmpty	NaN	kg
W_Payload	NaN	kg
W_Fuel	NaN	kg
W_Crew	NaN	kg
IY	100	kg * m^2

4.3. Aerodynamic

The aircraft reference aerodynamic is in figure: Wing-Body reference Aerodynamics

Chapter 5. Design Airspeeds

This chapter defines the operating and design airspeeds as required for certification-CSVLA

5.1. Maximum speed in level flight VH

Data not yet available...to be added Available and Required Power.

5.2. Stall speeds VS, VS0, VS1

These speeds will be verified by flight test according to certification requirements.In order to calculate the stall speed, the maximum lift coefficient of the aeroplane as a whole is determined first. The maximum lift coefficient of the aeroplane has been calculated from high fidelity CFD. In landing configuration computed with full flap, CLMAX landing =2.1 in take-off configuration leading to CLMAX takeoff =1.9, and in clean configuration, leading to CLMAX clean =1.58 , also considering the horizontal tail balancing force.

Flaps retracted(clean configuration):

$$V_S \ = \sqrt{\frac{2\ W_{MTOM}}{\rho_0 C_{L_{MAX_{Clean}}} S}} \ = \sqrt{\frac{2 * 981}{1.225 * 1.58 * 2.589}} \ = 19.7839 m/s$$

Flaps extended(Landing configuration):

$$V_{S_0} \ = \sqrt{\frac{2\ W_{MTOM}}{\rho_0 C_{L_{MAX_{Landing}}} S}} \ = \sqrt{\frac{2 * 981}{1.225 * 2.1 * 2.589}} \ = 17.1606 m/s$$

Flaps extended(Take-off configuration):

$$V_{S_1} \ = \sqrt{\frac{2\ W_{MTOM}}{\rho_0 C_{L_{MAX_{Takeoff}}} S}} \ = \sqrt{\frac{2 * 981}{1.225 * 1.9 * 2.589}} \ = 18.0412 m/s$$

Add here comments if necessary

Note: These speeds are estimates. The methods for the estimation can be various.It is important that these estimations are as precise as possible. Flight tests will be used to validatethe stall speeds. In case the flight tests show different values, this might have an impact on the speedsused for design and ultimately might impair the compliance to the-CSVLA

5.3. Design manoeuvring speed VA

According to requirement-CSVLA-335,

the maneuvering speed VA cannot be less then:

$V_A \geq V_S\sqrt{n_{max}} = 19.7839 * \sqrt{3.8} = 38.566 m/s$

Add here comments if necessary

5.4. Flaps maximum operating speed VF

According to requirement-CSVLA -345,

such speed shall be not less than the greater of 1.4VS and 1.8VS0

The speed has been selected as the greater between 1.4VS =27.6975m/s and 1.8 VSF =24.0248m/s, where VSF is the computed stalling speed with flaps fully extended at the design weight.

The flaps operating speeds is:

$V_F = 27.6975 m/s$

5.5. Flaps maximum extension speed VFE

On this aeroplane the maximum flap extension speed is identical to the flap operating speed VF. This speed is the maximum speed for flaps in take-off and landing configuration.

$V_{FE} = 27.6975 m/s$

5.6. Design cruising speed VC

According to requirement-CSVLA-335.

- VC (in m/s) may not be less than -

$$2.4\sqrt{\frac{Mg}{S}}\left(V_C(kt) = 4.7\sqrt{\frac{Mg}{S}}\right) \to 2.4 * \sqrt{\frac{100 * 9.8066}{2.589}} = 46.7095 m/s$$

where M/S is the wing loading in kg/m2 and g is the acceleration due to gravity in m/s2.

- VC need not be more than 0·9 VH at sea level.

VH must be available. Otherwise previous value is considered!!!

$V_C = 46.7095 m/s$

5.7. Design dive speed VD

According to requirement-CSVLA-335.

(1) VD may not be less than 1·25 VC; and (2) with VCmin, the required minimum design cruising speed, VD may not be less than 1·40 VCmin.

(1) 1.25VC =58.3869m/s

(2) 1.4VCmin =40m/s

$V_C = 1.25 * 46.7095 = 58.3869 m/s$

5.8. Demonstrated dive speed VDF

VDF is not a design airspeeds for this category.

5.9. Never exceed speed VNE

VNE is not a design airspeeds. It must be checked into sec. CS-VLA 1505 Airspeed limitations.

5.10. Design Airspeeds summary

Design airspeeds summary is resumed in Table:Design airspeeds

Table 5.1. Design airspeeds

Design airspeeds	Value	Measure unit
VS	19.78	m/s
VS0	17.16	m/s
VS1	18.04	m/s
VA	38.57	m/s
VC	46.71	m/s
VD	58.39	m/s
VE	58.39	m/s
VG	30.46	m/s
VS_inv	24.87	m/s
VF	30.89	m/s

Chapter 6. Altitude

The maximum permissible operational altitude for the aircrat is 1300m. Despite the-CSVLA requirements do not require to accounts for the effects of altitude,such effects have been considered up to 1300m. In fact the gust load factor have been calculated at such altitude. This is considered acceptable since it covers the operational range within which the aeroplane will fly most of the time.

(Note: the-CSVLA requirement does not require to account for the effects of altitude.Calculating the loads at sea level would be acceptable. In this case, the choice to consider such effect up to 1300m is a decision of a designer, which would be accepted by the team.)

Chapter 7. Manoeuvring and Gust load factors n

According to CSVLA 337(a) , the positive limit moeuvring load factor n may not be less than 3.8, while according to CSVLA 337(b) , the negative limit manoeuvring load factor may not be less than -1.5.

The following value will be considered:

1. nmax =3.8
2. nmin =-1.5

7.1. Gust envelope

Gust load factors need to be considered because they can exceed the prescribed maximum load factors at different weights and altitudes. Since gust loads depend on air density and aircraft mass they will be calculated for Compliance with the flight load requirements of this subpart to show:

(1) At each critical altitude within the range in which the aeroplane may be expected to operate from sea level up to maximum operative altitude equal to: 1300 m

(2) At each practicable combination of weight and disposable load within the operating limitations specified in the Flight Manual according to requirement CSVLA 321 and fully extended (requirement CSVLA 345(b) at VF).

The calculation is based on CSVLA 341 . To calculate the gust loads at altitudes other than at sea level the following equation is altered to include the density at any altitude.

$$n = 1 + \frac{1/2\, \rho_0\, V\, a\, K_g\, U_{de}}{Mg/S}$$

where:

- $K_g = \dfrac{0.88\mu_g}{5.3 + \mu_g}$
- $\mu_g = \dfrac{2(M/S)}{\rho \bar{C} a}$
- $U_{de} =$ derived gust velocities referred to in CSVLA 333(c) (m/s)
- $\rho_0 =$ density of air at sea level (kg/m3)
- $\rho =$ density of air (kg/m3)
- $M/S =$ wing loading (kg/m2)
- $\bar{c} =$ mean geometric chord (m); $g =$ acceleration due to gravity (m/s2);
- $a =$ slope of the aeroplane normal force coefficient curve CNA per radian

Since the gust loads on the wing and tail have been chosen to be treated together, a is the slope of the lift-curve of the aeroplane is equal to a =5.2341/rad and0.09131/deg.

The gust speed at VC is equal to: 15.24m/s

The gust speed at VD is equal to: 7.62m/s

TABLE TO BE CHECKED!!!

Table 7.1. Gust load factor, different Speeds and Altitude

ID	V(m/s)	M(kg)	M/S(kg/m^2)	Altitude(m)	rho(kg/m^3)	mug	Kg	Ude(m/s)	n
1	46.71	100	38.62	1300	1.079	27.47	0.7377	15.24	5.444

(Note: the applicant should provide the method for the calculation of the slope of the lift-curve of the aeroplane)

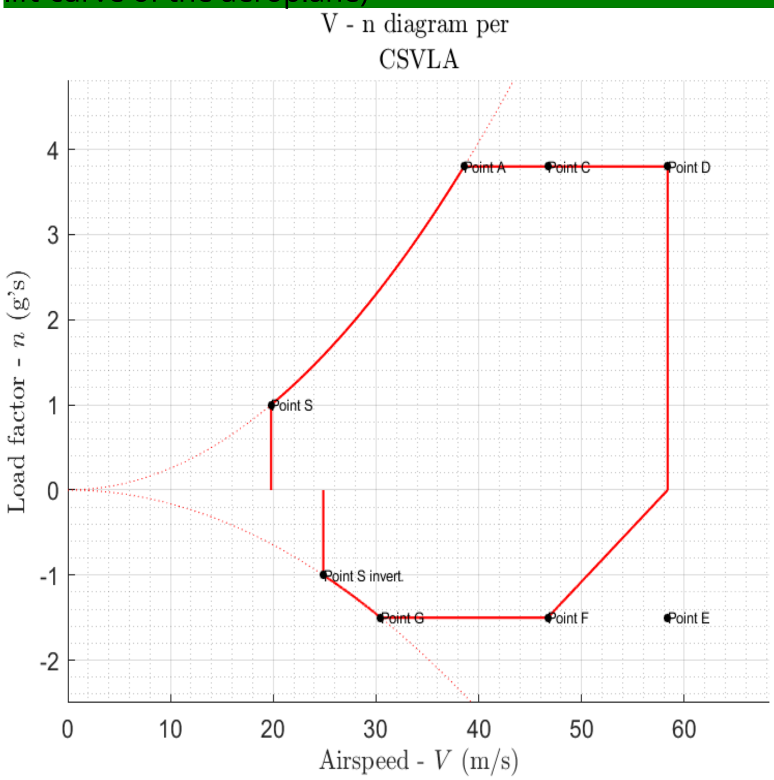

Figure 7.1. V-n diagram

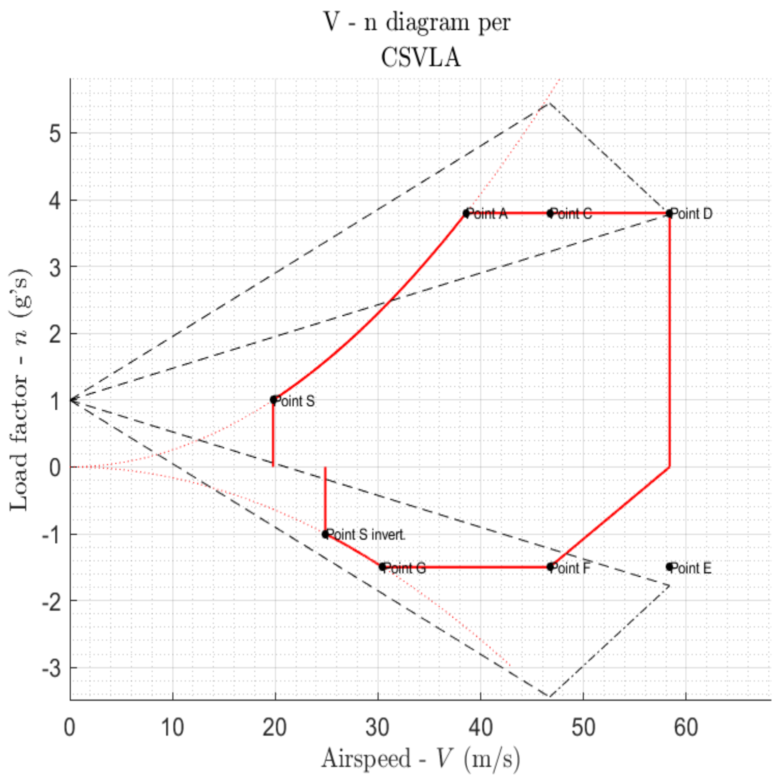

Figure 7.2. Gust diagram

Chapter 8. V-n Envelope

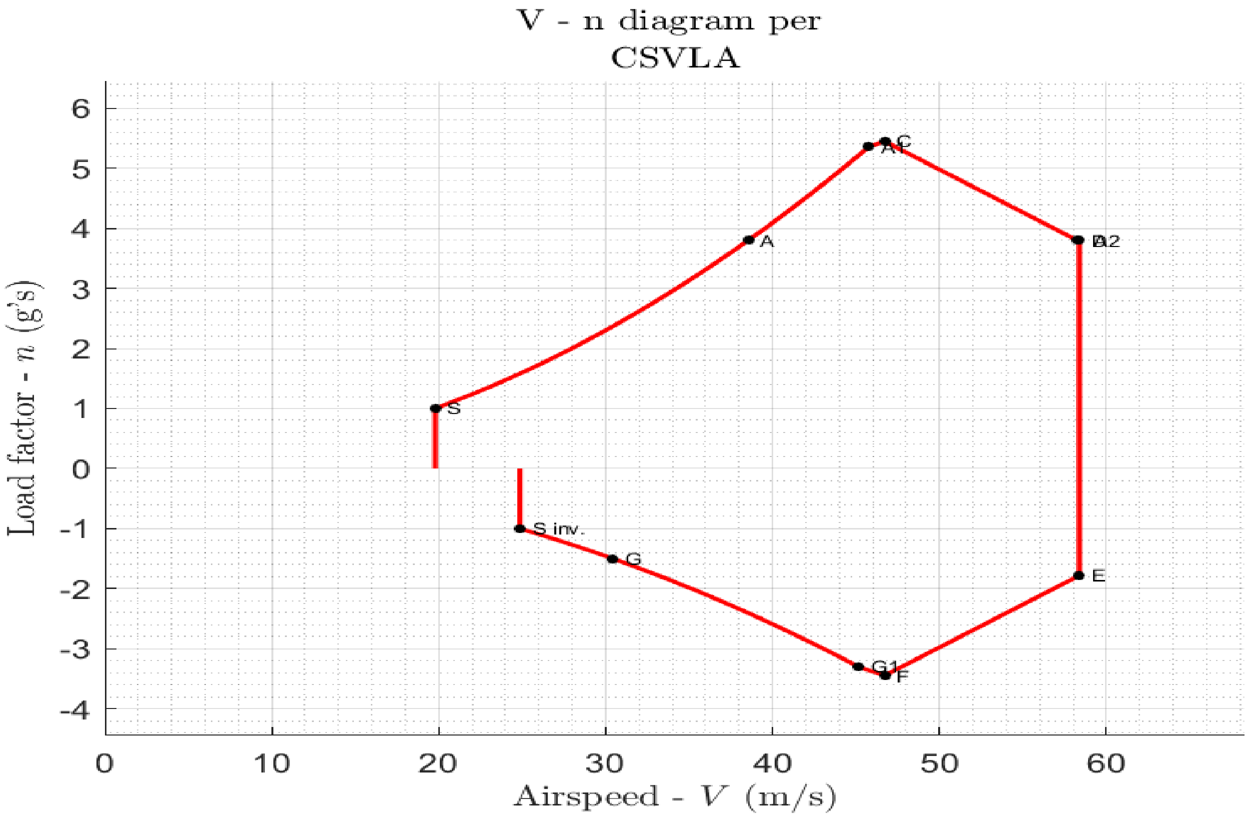

Figure 8.1. Maneuver and Gust load factors and diagram

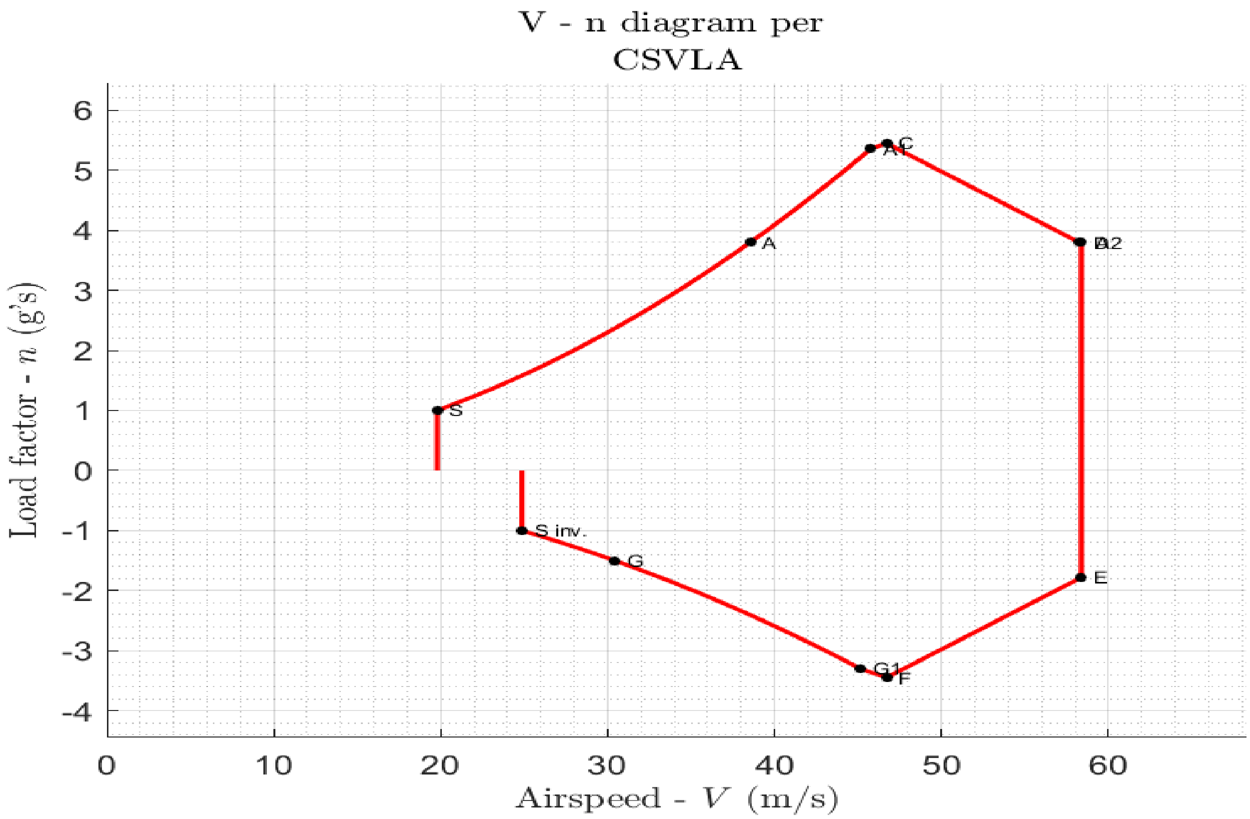

Figure 8.2. Maneuver and Gust load factors and diagram

ADD HERE V-n Envelope

Chapter 9. Loads on the aeroplane

ADD HERE details for balancing Equation

ADD HERE details for balancing Equation

9.1. Reference axes and sign convention

9.1.1. aaaaa

ADD HERE details for balancing Equation

9.2. Symmetrical flight conditions

ADD HERE details for balancing Equation

9.3. Aerodynamic centre

ADD HERE details for balancing Equation

9.4. Pitching moment of the wing

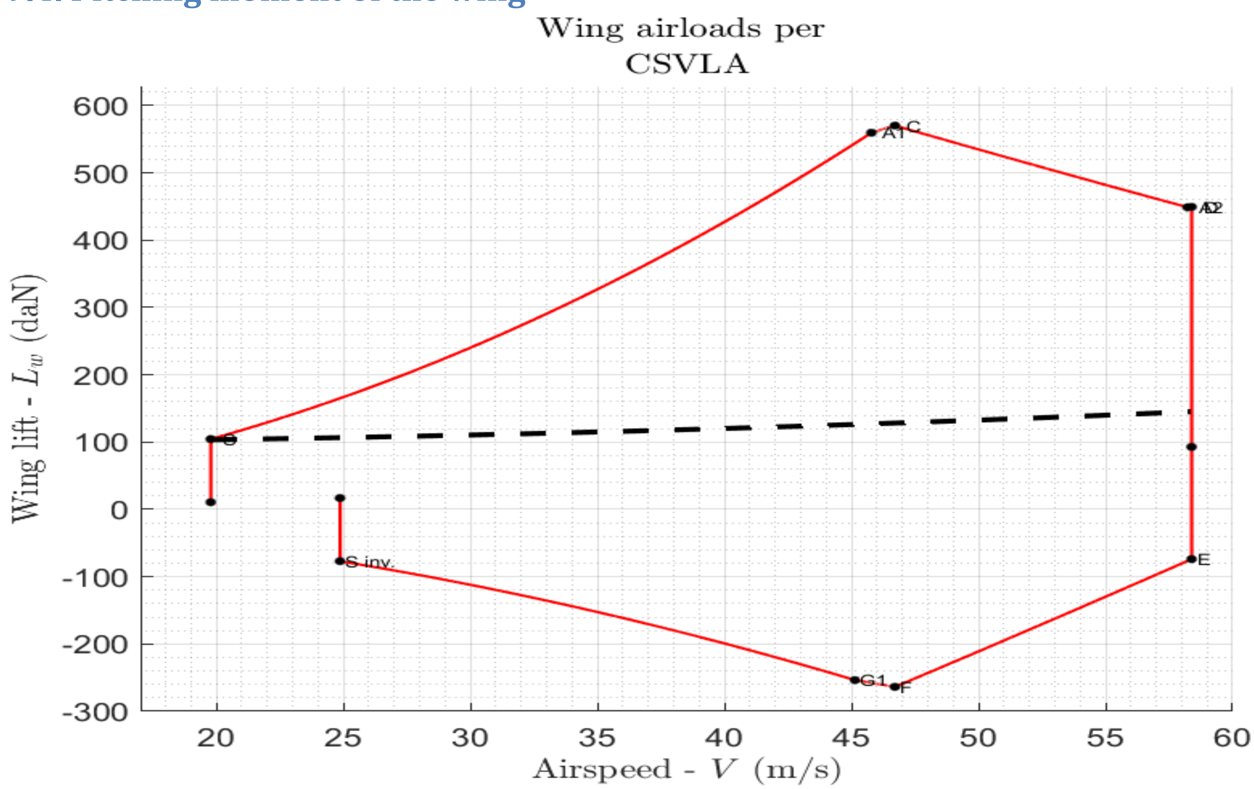

Figure 9.1. Wing airloads

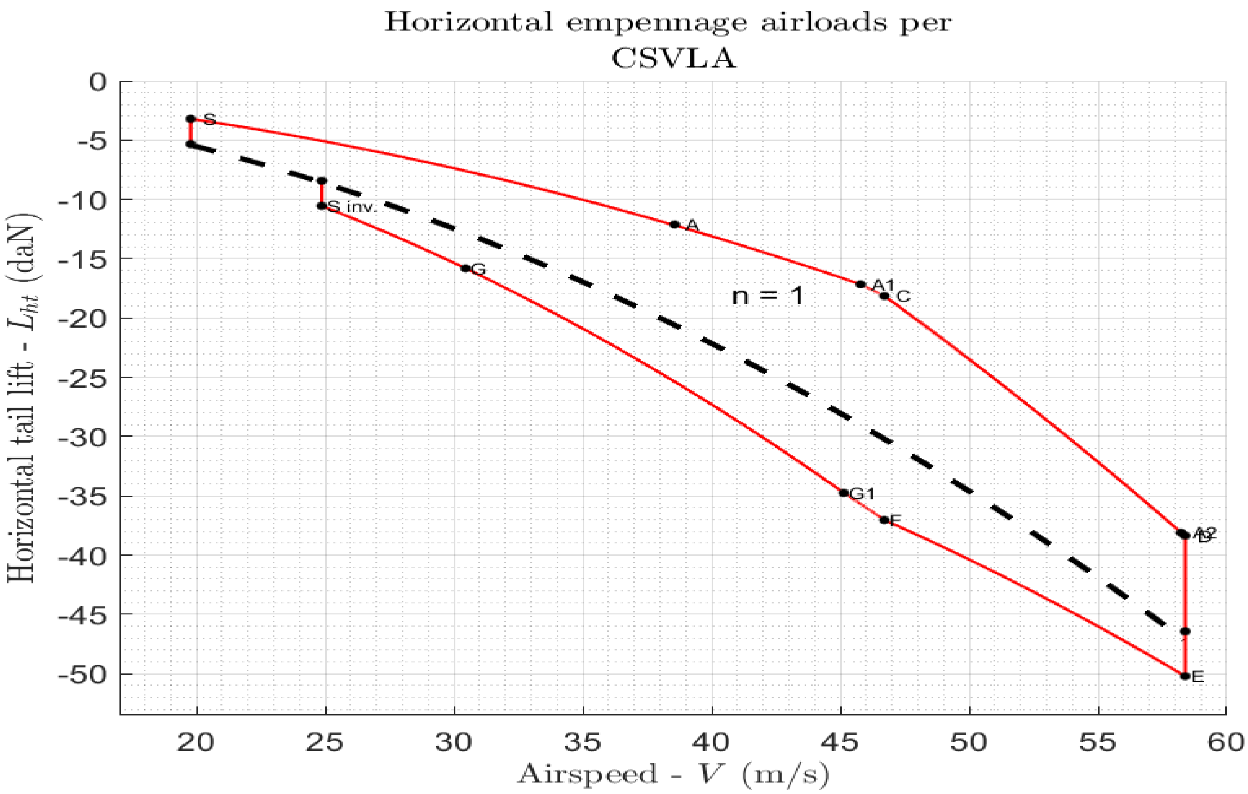

Figure 9.2. Balancing loads

Chapter 10. Loads on the wing

ADD HERE details for balancing Equation

ADD HERE details for fuselage effect how are they accounted?

10.1. Influence of the fuselage

ADD HERE details for balancing Equation

10.2. Forces and moments acting on the wings

10.2.1. SpanWise Airloads Distribution

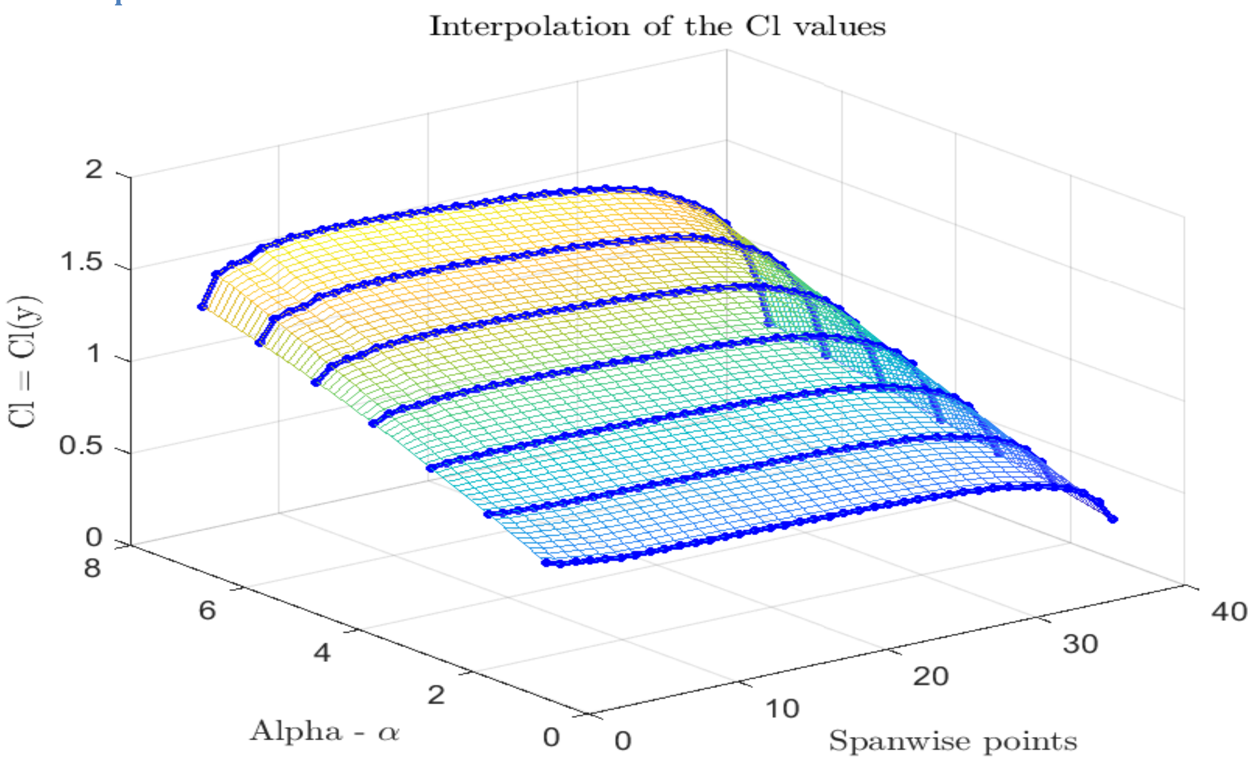

Figure 10.1. Wing lift coefficient spanwise distribution

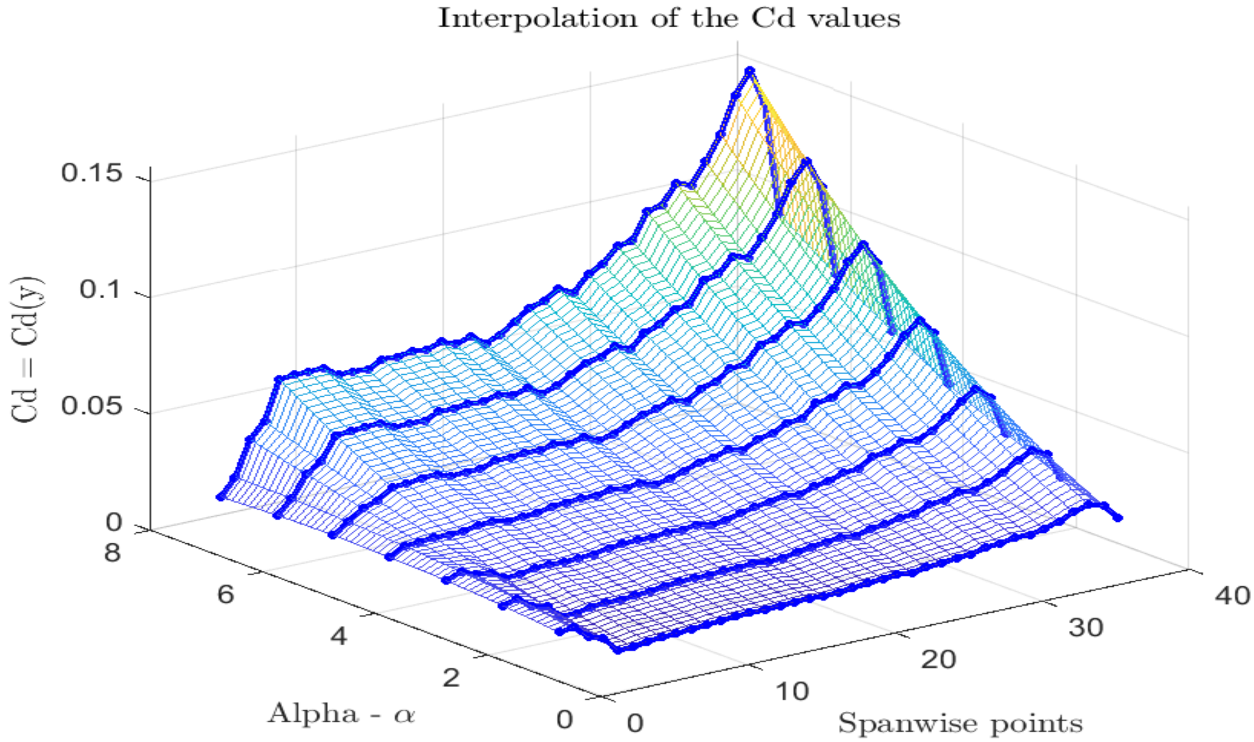

Figure 10.2. Wing drag coefficient spanwise distribution

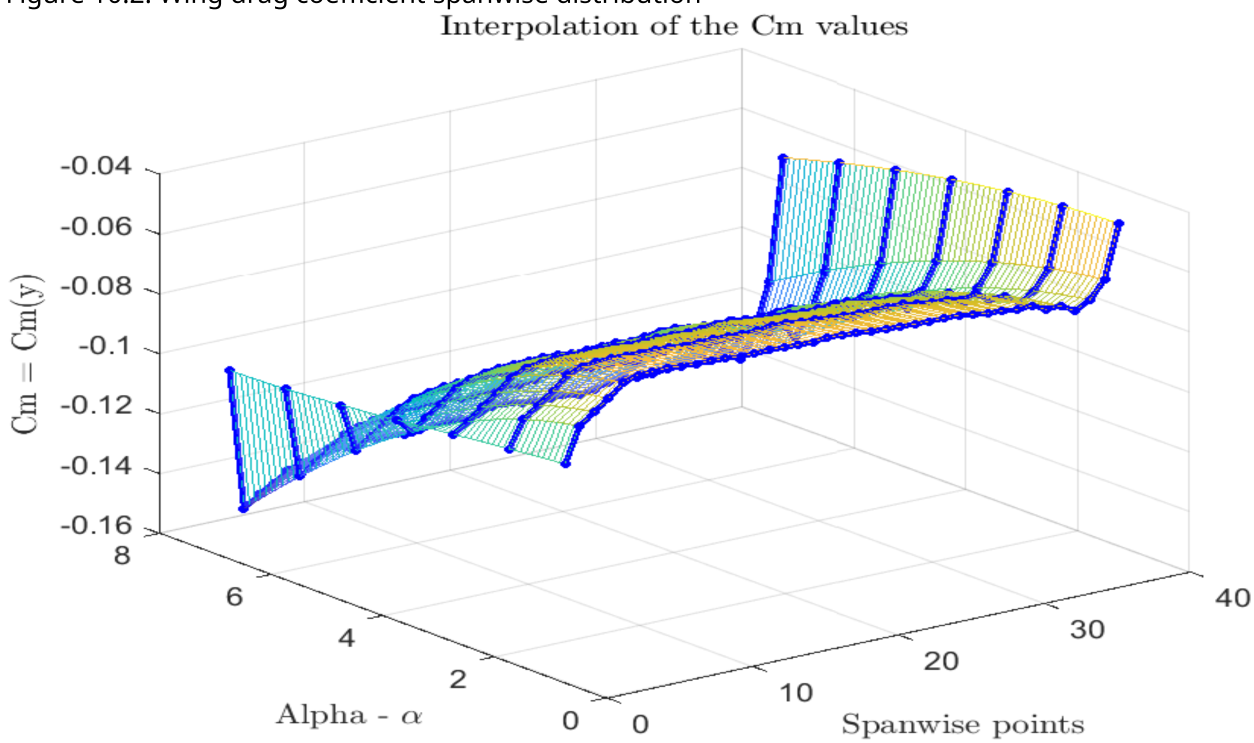

Figure 10.3. Wing pitching moment coefficient (0.25mac) spanwise distribution

10.2.2. Normal and parallel component

10.2.3. Shear, Bending and Torsion

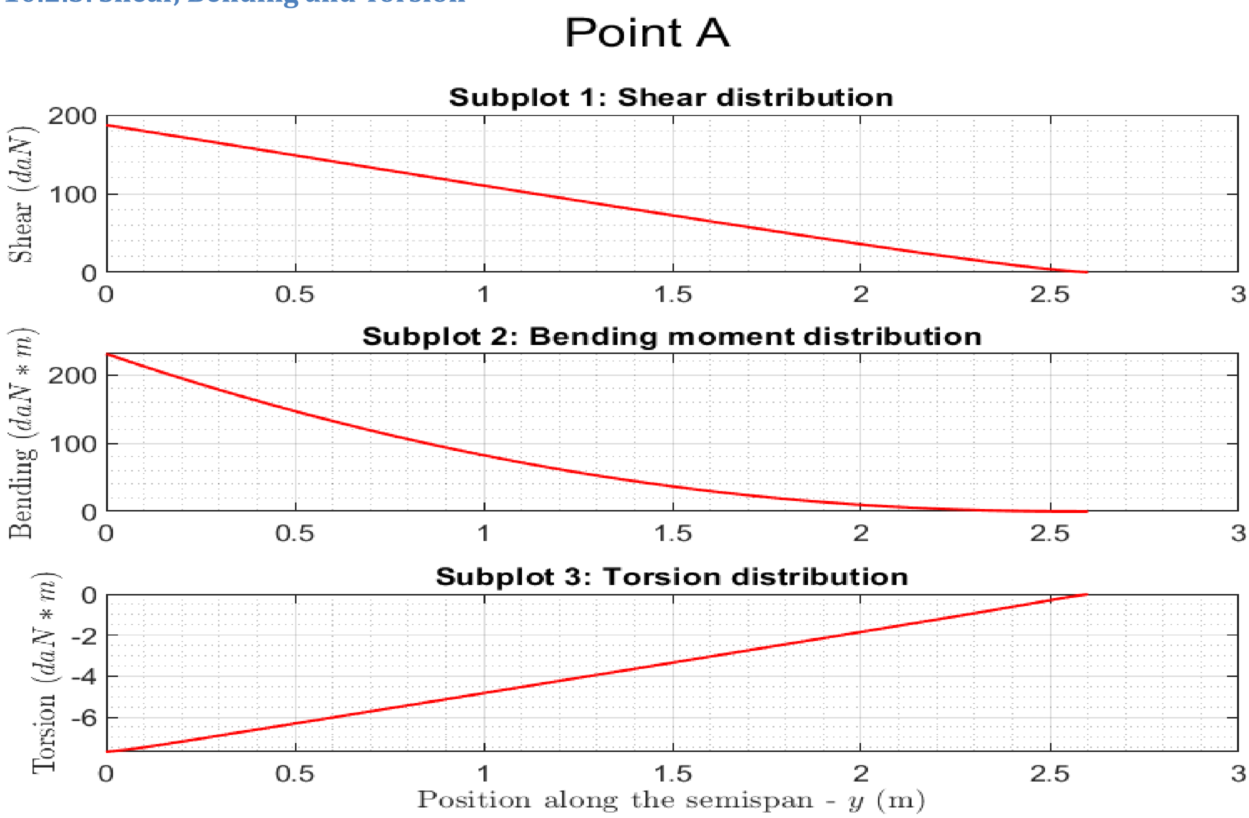

Figure 10.4. Shear, Bending and Torsion due to airloads - POINT A

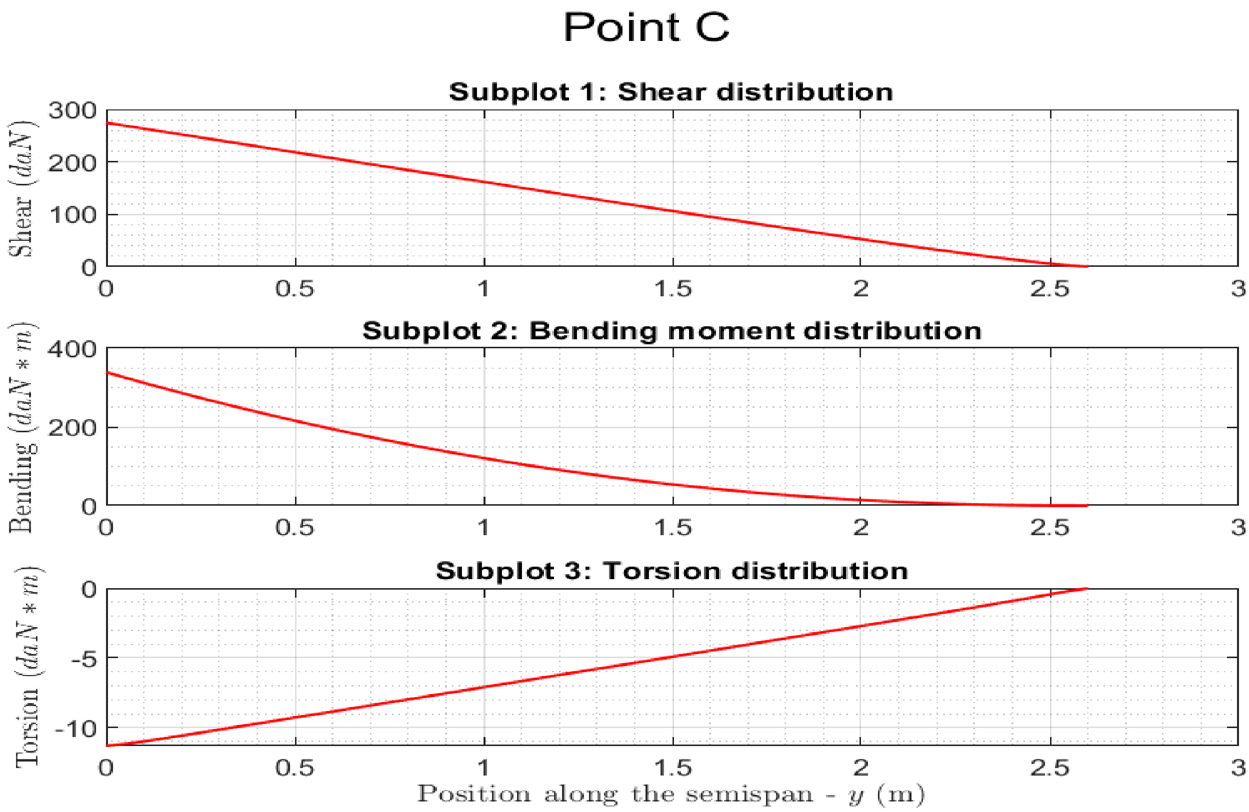

Figure 10.5. Shear, Bending and Torsion due to airloads - POINT C

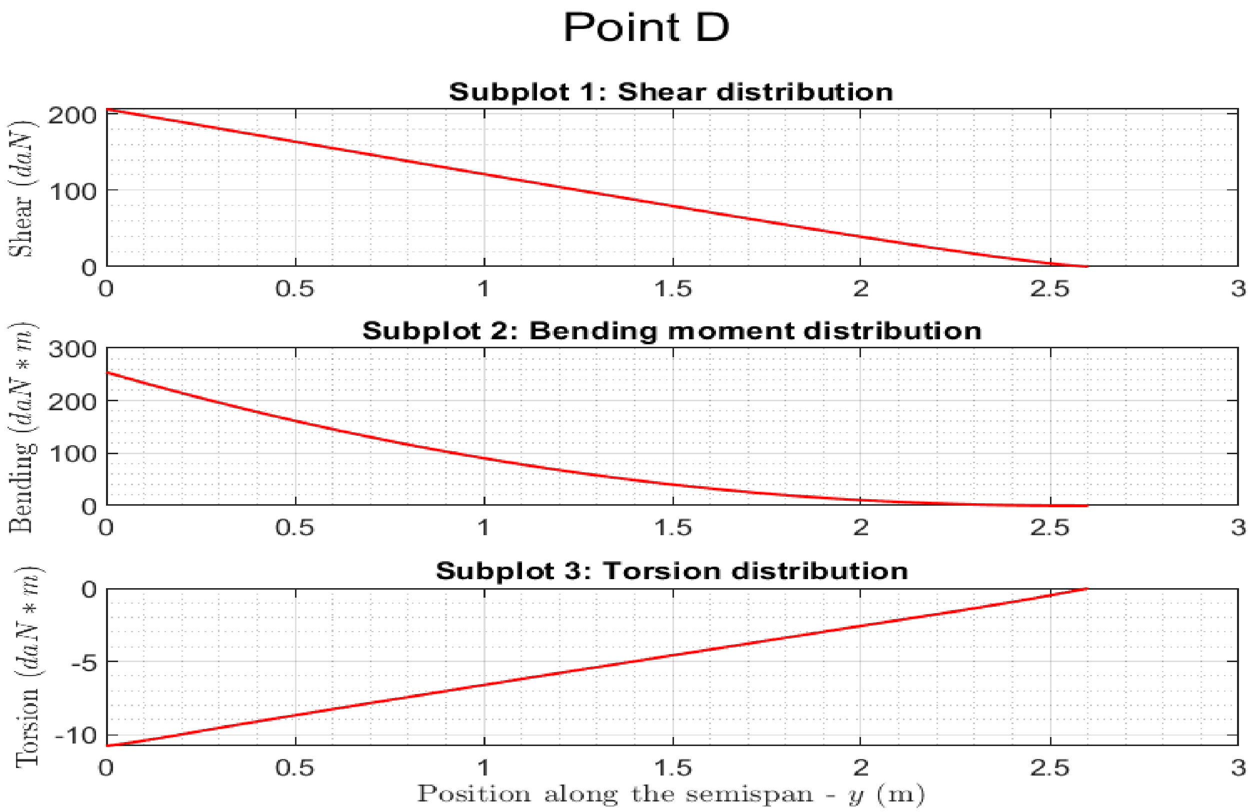

Figure 10.6. Shear, Bending and Torsion due to airloads - POINT D

10.2.4. Critical load condition

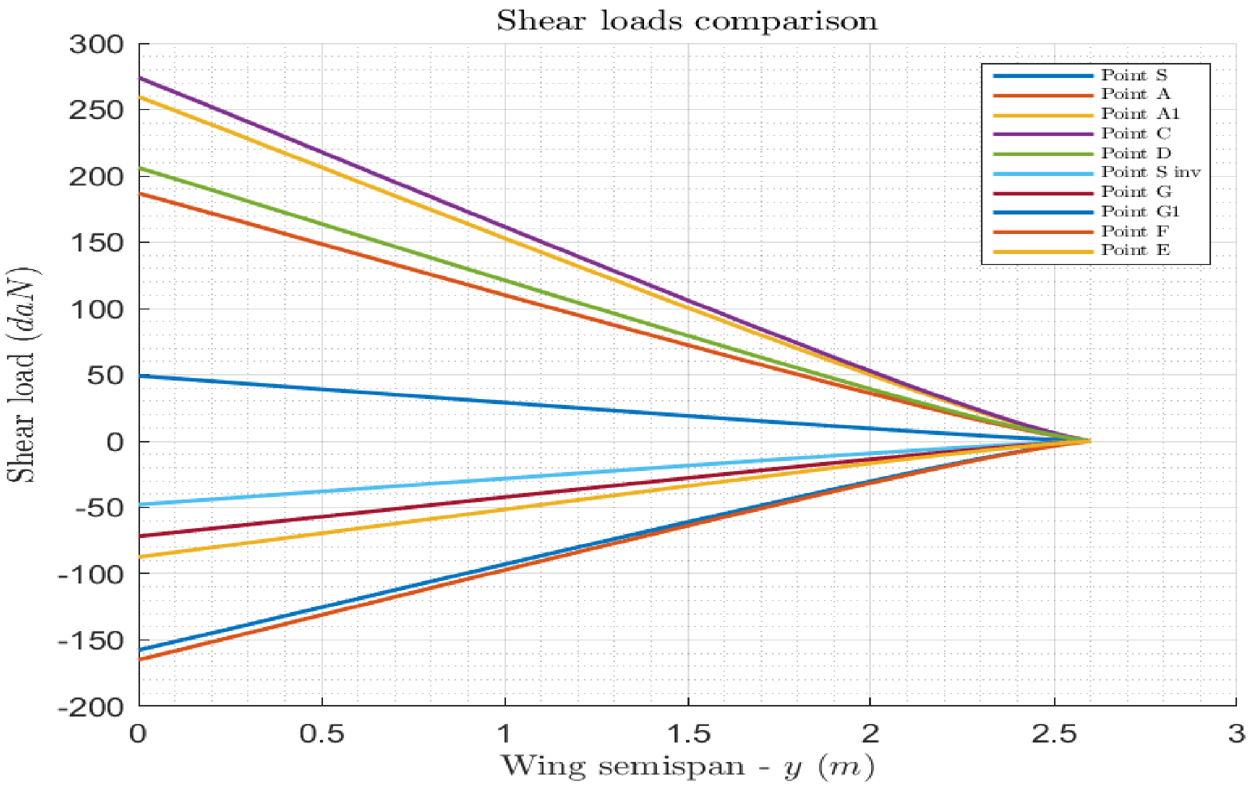

Figure 10.7. Shear comparison

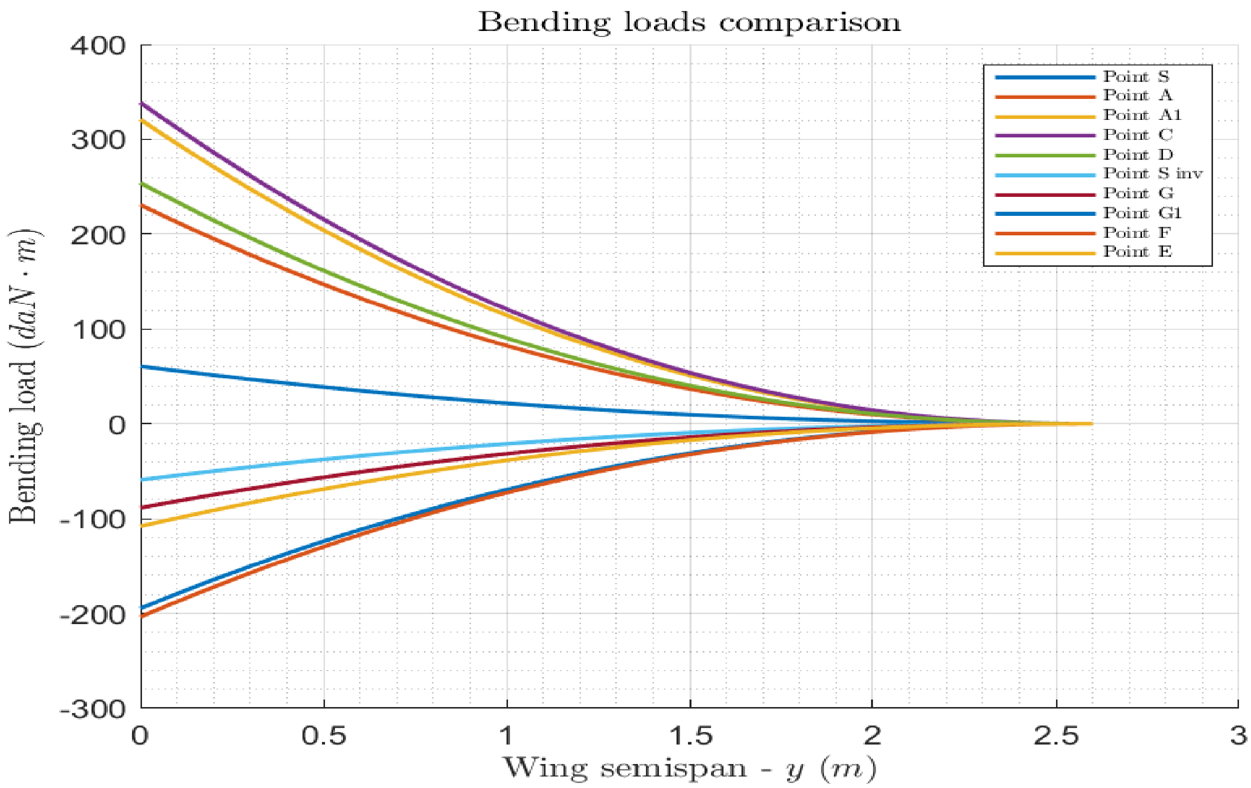

Figure 10.8. Bending comparison

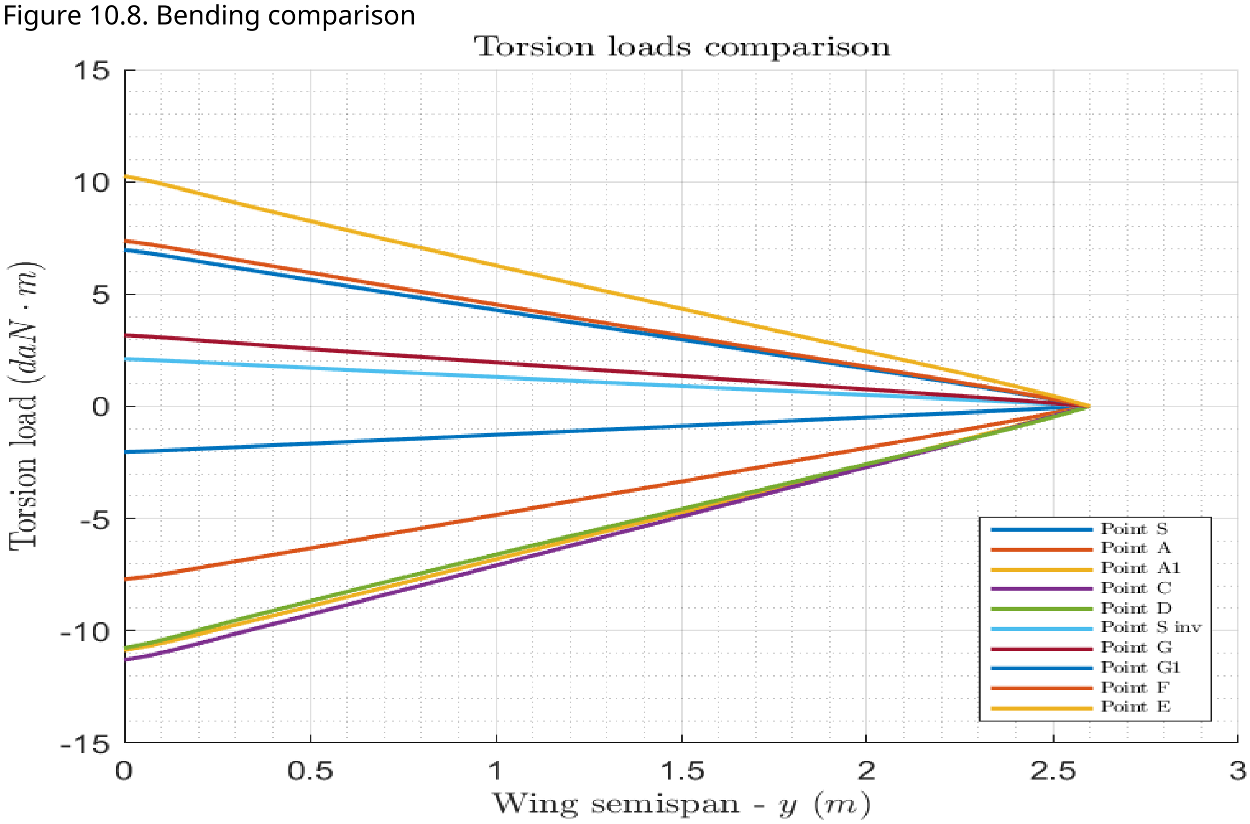

Figure 10.9. Torsion comparison

ADD HERE details for uns loads

10.3. Unsymmetrical loads

10.3.1. Rolling condition

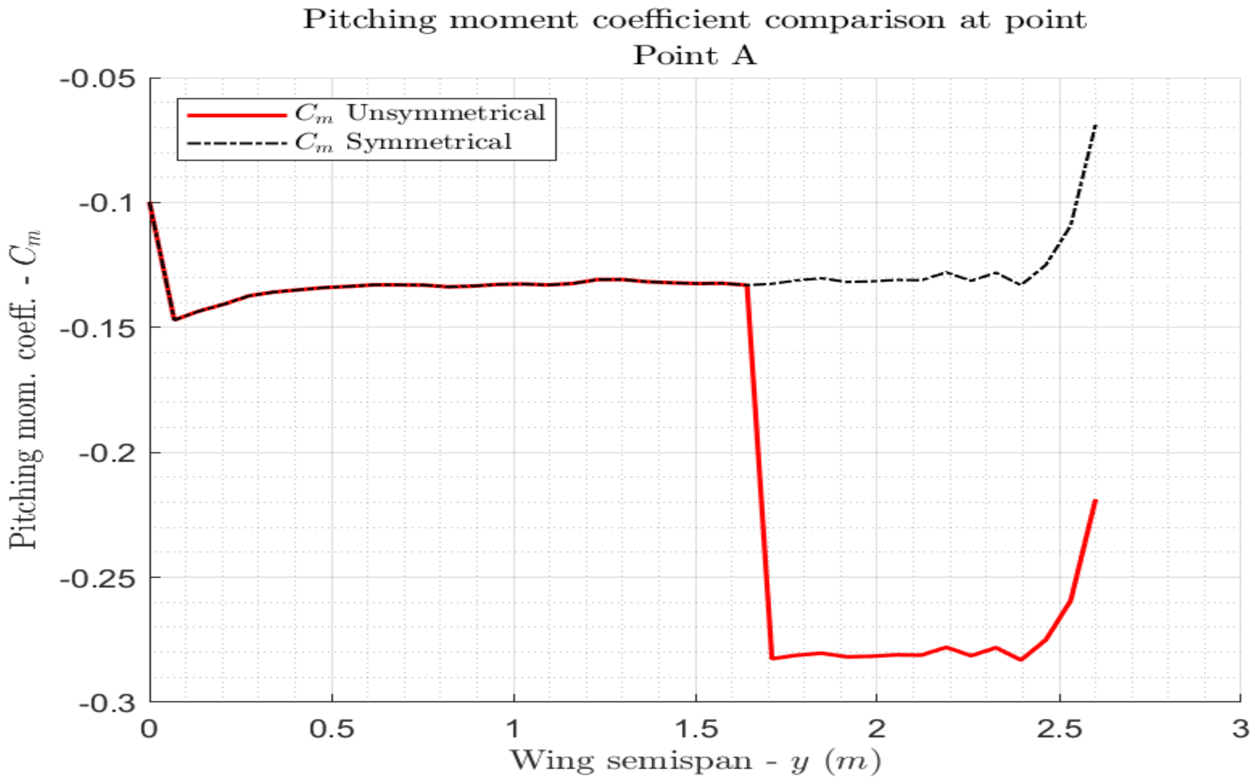

Figure 10.10. Pithcing moment coefficient - POINT A

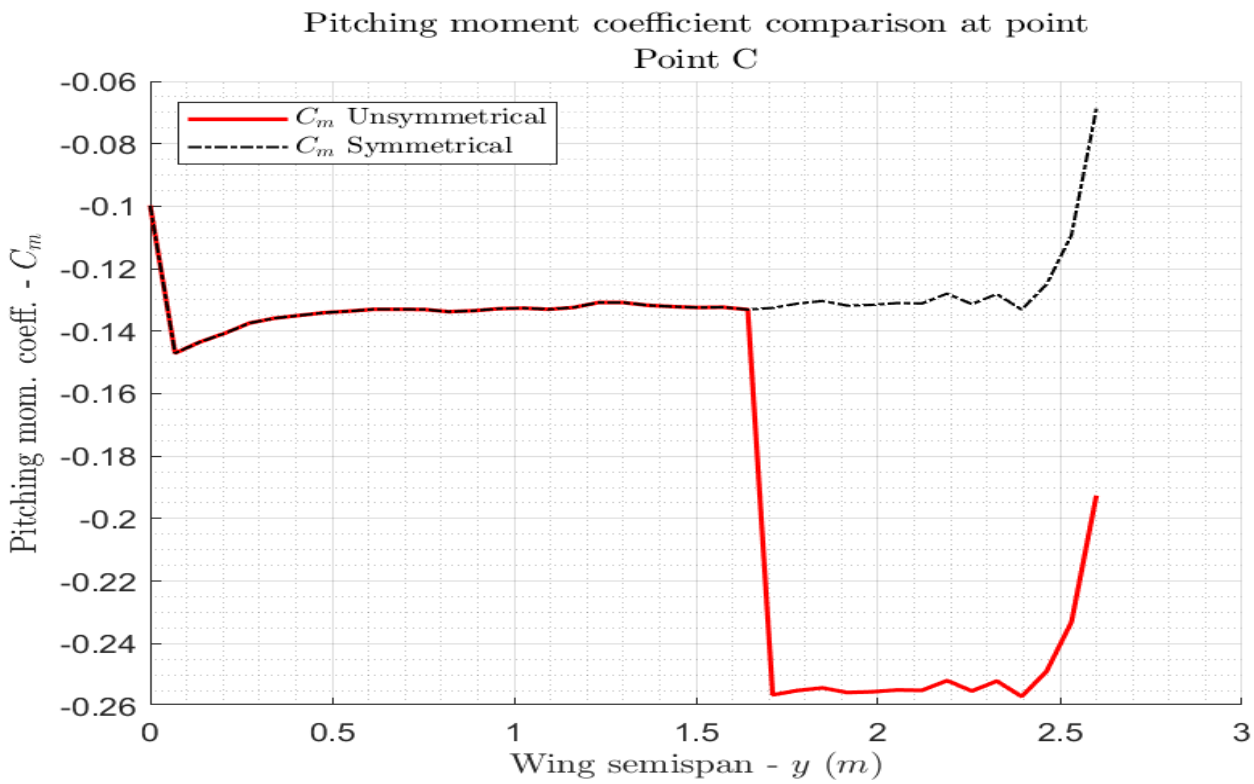

Figure 10.11. Pithcing moment coefficient - POINT C

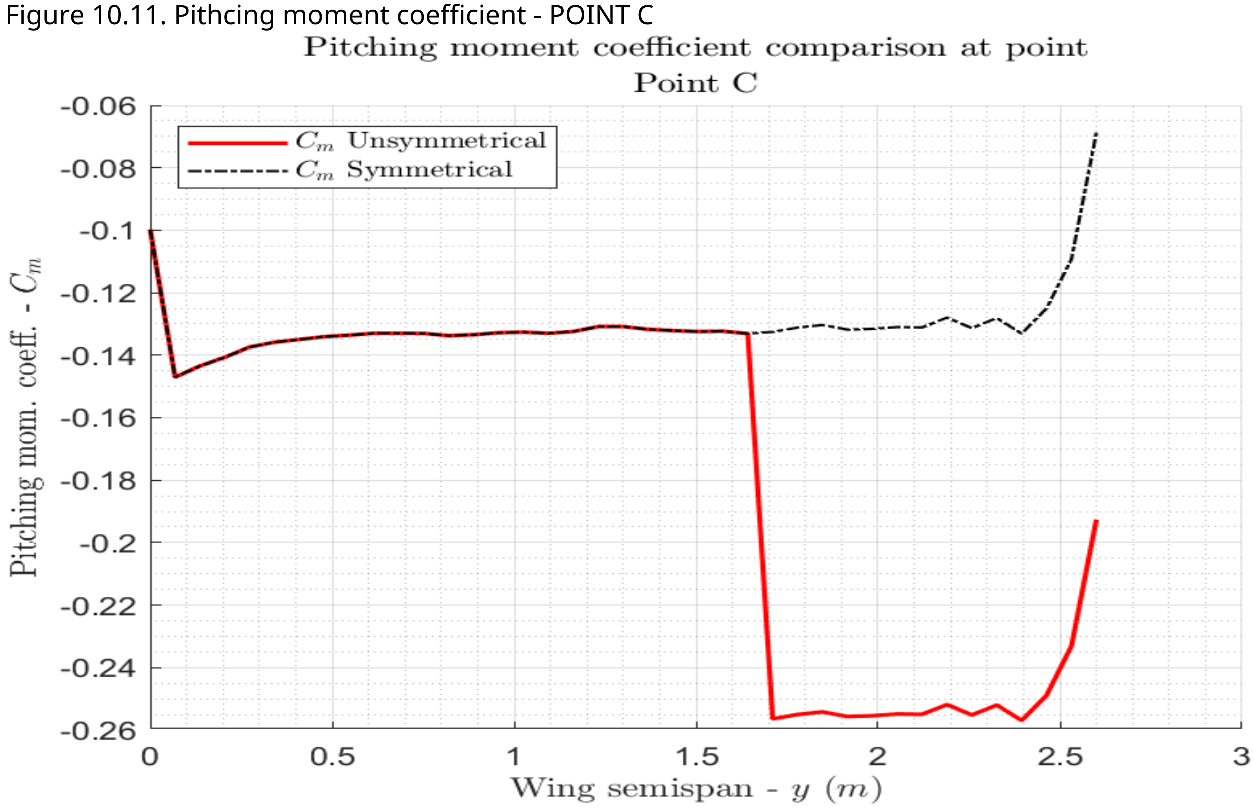

Figure 10.12. Pithcing moment coefficient - POINT D

10.3.2. Effect of aileron displacement on the wing torsion

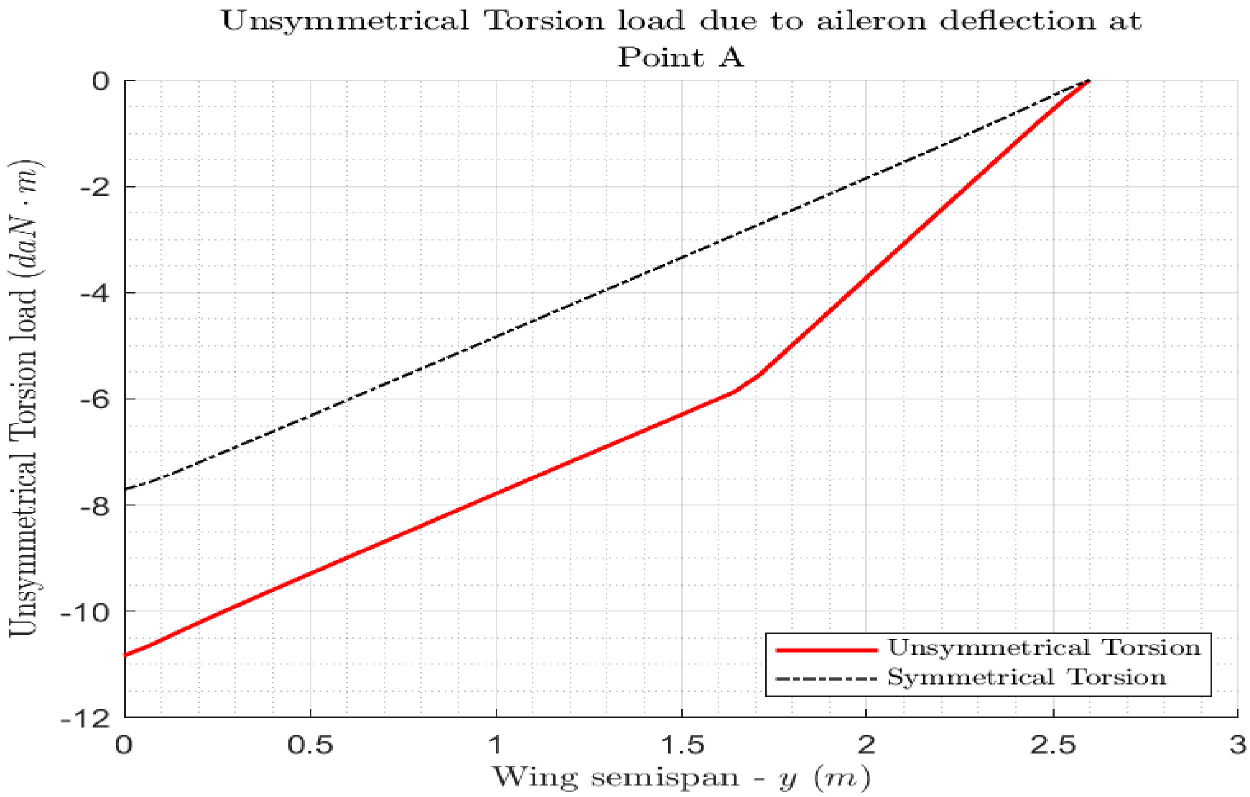

Figure 10.13. Torsion distribution full loads - POINT A

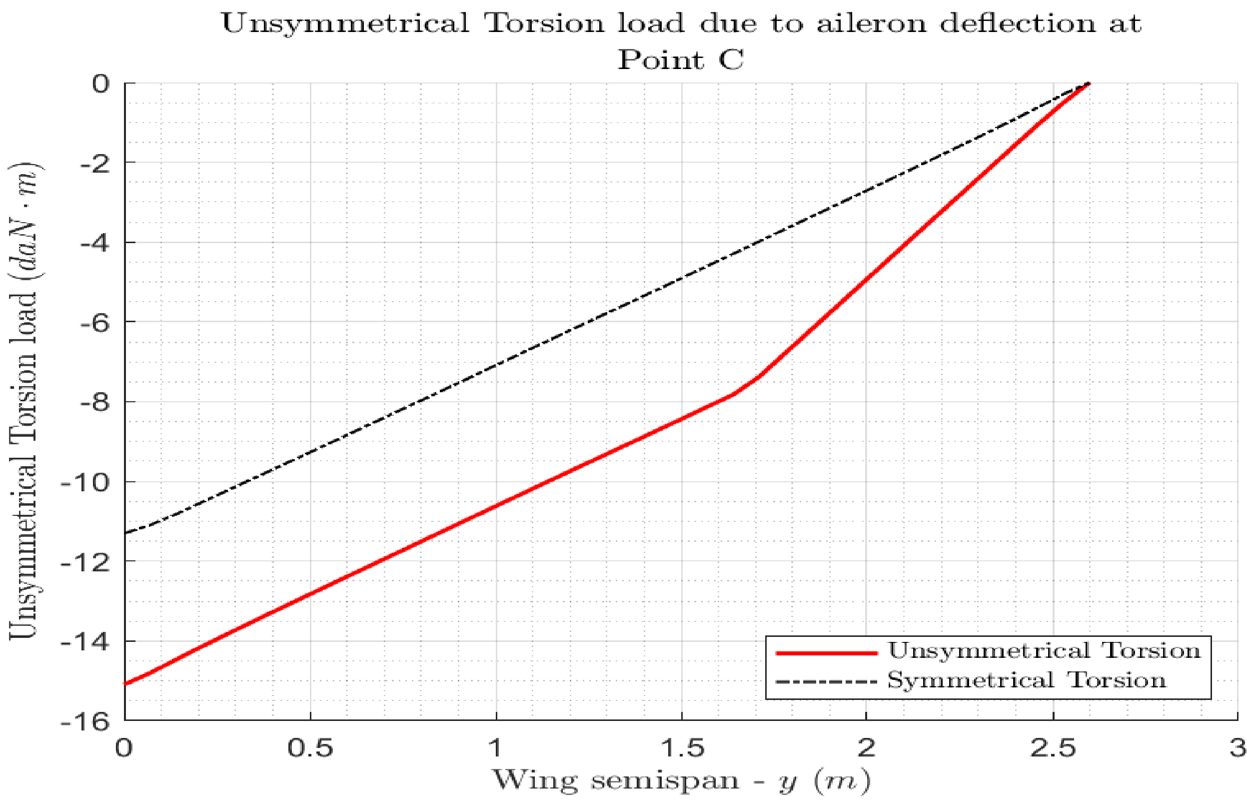

Figure 10.14. Torsion distribution full loads - POINT C

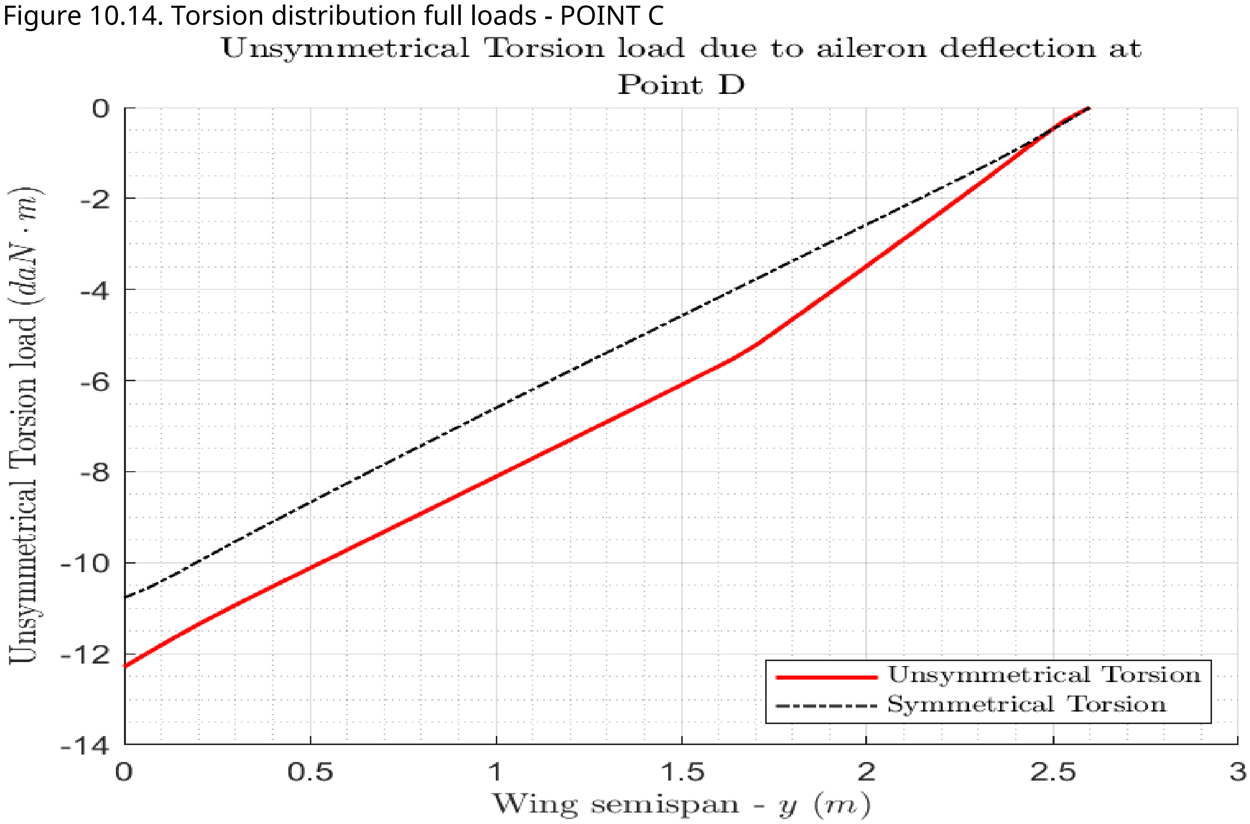

Figure 10.15. Torsion distribution full loads - POINT D

Chapter 11. Loads on the horizontal tail

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ADD HERE details

11.1. Balancing loads

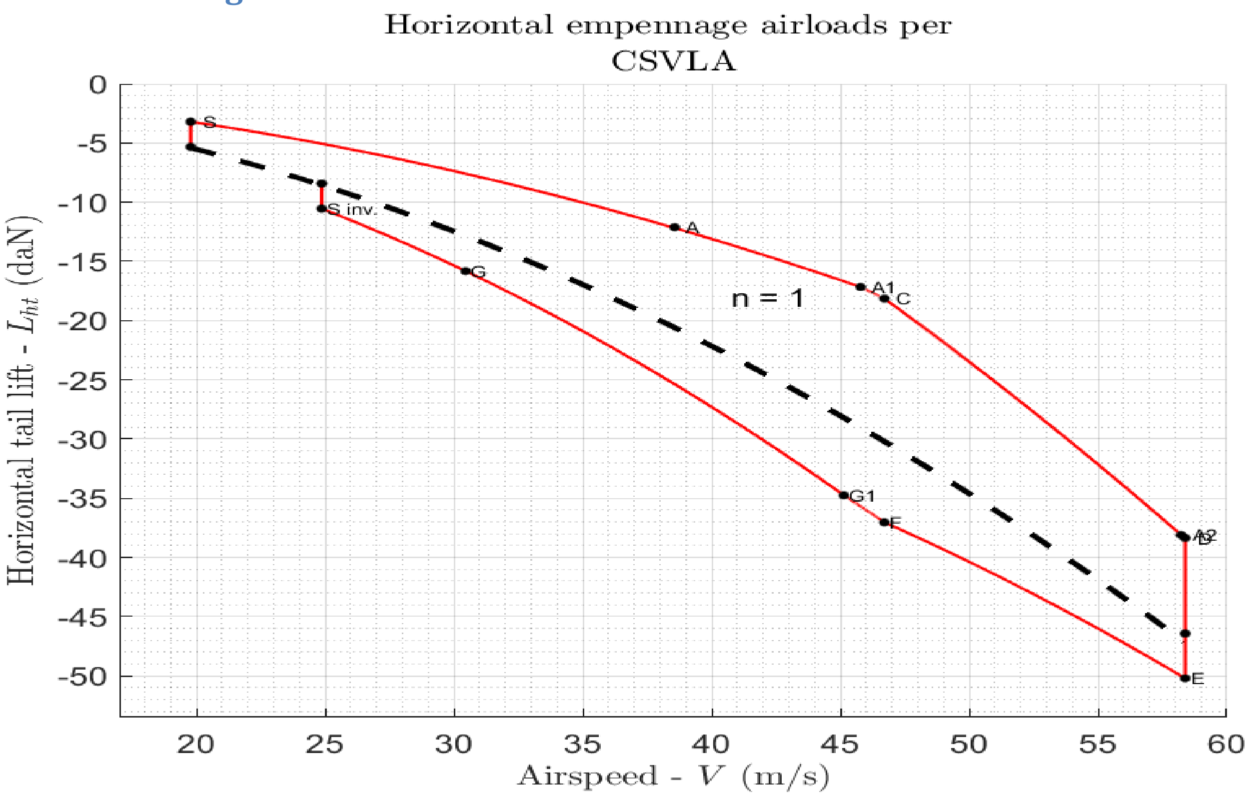

Figure 11.1. Balancing loads

ADD HERE details

11.2. Manouevring loads

11.2.1. Unchecked manoeuvre

11.2.2. Checked manoeuvre

11.2.3. Gust loads

ADD HERE details

11.3. Horizontal tail loads summary

ADD HERE details

11.4. Unsysmmetrical loads

Chapter 12. Loads on the vertical tail

According to CSVLA the vertical tail must withstand several manoeuvring loads. In this chapter, all these load case will be illustrated.

12.1. Manouevring load

At speeds up to VA, the vertical tail surfaces must be designed to withstand the following condition. In computing the tail loads, the yawing velocity may be assumed to be zero.

12.1.1. CSVLA 441(a)(1)

With the aeroplane in unaccelerated flight at zero yaw, it is assumed that the rudder control is suddenly displaced to the maximum deflection, as limited by the control stops or by limit pilot forces.The control stops are +/- 30 deg. The lateral force coefficient acting on the rudder when at maximum deflection angle is given by the following simple equation:

$$C_Y = C_{Y,0} + \frac{d\,C_Y}{d\,\delta_r} * \delta_{r,max}$$

where:

- C_Y = lateral force coefficient;
- $C_{Y,\,0}$ = lateral force coefficient at $\beta = \delta = 0$, equal to zero for symmetrical airfoil;
- $\frac{d\,C_Y}{d\,\delta_r}$ = lateral force curve slope per deg of rudder deflection;
- $\delta_{r,\,max}$ = rudder control stop.

Assuming no deflection of the control cable, the maximum value of the lateral force coefficient is:

$$(C_Y)_{\delta_r\,=\,30} = 0.000644 * 30 = 0.019356$$

The lateral force is calculated as follow:

$$Y = \frac{1}{10} * q_A * S_{vertical} * \frac{(C_Y)_{\delta_r\,=\,30}}{S_{ratio}} = (1/10) * 911 * 0.2044 * 0.01936/0.03947 = 9.131\ daN$$

The lateral force acting on a single fin of the vertical tail plain is 9.131/2 = 4.565 daN.

12.1.2. CSVLA 441(a)(2)

With the rudder deflected as specified in sub-paragraph CSVLA 441(a)(1) of this paragraph, it is assumed that the aeroplane yaws to the resulting sideslip angle. In lieu of a rational analysis, an overswing angle equal to 1.3 times the static sideslip angle of sub-paragraph CSVLA 441(a)(3) of this paragraph may be assumed. The overswing sideslip angle is 1.3 * 15 = 19.5 deg. The total lateral force acting on the vertical tail in this case is:

$$Y = \frac{1}{10} * q_A * S_{vertical} * \frac{C_Y}{S_{ratio}} = (1/10) * 911 * 0.2044 * 0.0245/0.03947 = 5.778 \ daN$$

The lateral force acting on a single fin of the vertical tail plain is 5.778/2 = 2.889 daN.

12.1.3. CSVLA 441(a)(3)

A yaw angle of 15 degrees with the rudder control maintained in the neutral position (except as limited by pilot strength). The total lateral force in this case is:

$$Y = \frac{1}{10} * q_A * S_{vertical} * \frac{C_Y}{S_{ratio}} = (1/10) * 911 * 0.2044 * 0.0233/0.03947 = 5.495 \ daN$$

The lateral force acting on a single fin of the vertical tail plain is 5.495/2 = 2.748 daN.

12.2. Manouevring and gust envelope

According to CSVLA 443 in the absence of a more rational analysis, the gust load must be computed as follows:

$$L_{vt} = \frac{K_{gt} * U_{de} * V * a_{vt} * S_{vt}}{16.3}$$

where:

- $U_{de} = \text{derived gust velocity (m/s)};$
- $L_{vt} = \text{vertical tail load (daN)}$
- $K_{gt} = \frac{0.88 * \mu_{gt}}{5.3 + \mu_{gt}} = \text{gust alleviation factor};$
- $\mu_{gt} = \frac{2 * M}{\rho * \bar{c}_t * g * a_{vt} * S_{vt}} * \frac{K^2}{l_t^2} = \text{lateral mass ratio};$
- $M = \text{aeroplane mass (kg)};$
- $rho = \text{air density } (kg/m^3);$
- $l_t = \text{aeroplane c.g.} - \text{to} - \text{lift} - \text{centre of vertical surface distance } (m);$
- $S_{vt} = \text{area of vertical tail } (m^2);$
- $a_{vt} = \text{lift curve slope of vertical tail } (1/rad);$
- $V = \text{aeroplane equivalent speed } (m/s);$
- $K = \text{radius of gyration in yaw } (m);$
- $g = \text{acceleration due to gravity } (m/s^2);$

These calculations must be performed at VC and VD; the results are the following:

1. Gust load at VC: 8.8395 daN
2. Gust load at VD: 5.5247 daN

The critical gust load is 8.8395 daN at VC.

12.3. Vertical tail loads summary

12.4. Combined loads

According to CSVLA 447 the following two additional condition must be verified:

1. With the aeroplane in a loading condition correspondint to point A or point D in the V - n diagram (whichever condition leads to the higher balance load) the loads on the horizontal tail must be combined with those on the vertical tail as specified in CSVLA 441 ; this prescription results in a combined load equal to 20.02 daN;
2. 75 % of the loads according to CSVLA 423 for the horizontal tail and CSVLA 441 for the vertical tail must be assumed acting simultaneously; this prescription results in a combined load equal to 69.39 daN.

The critical combined load is 69.3881 daN.

Chapter 13. Loads on the wing flaps

According to CSVLA the vertical tail must withstand several manoeuvring loads. In this chapter, all these load case will be illustrated.

13.1. Manouevring load

At speeds up to VA, the vertical tail surfaces must be designed to withstand the following condition. In computing the tail loads, the yawing velocity may be assumed to be zero.

13.1.1. CSVLA 441(a)(1)

With the aeroplane in unaccelerated flight at zero yaw, it is assumed that the rudder control is suddenly displaced to the maximum deflection, as limited by the control stops or by limit pilot forces.The control stops are +/- 30 deg. The lateral force coefficient acting on the rudder when at maximum deflection angle is given by the following simple equation:

$$C_Y \;=\; C_{Y,0} \;+\; \frac{d\,C_Y}{d\,\delta_r} \;*\; \delta_{r,max}$$

where:

- $C_Y \;=\;$ lateral force coefficient;
- $C_{Y,\,0} \;=\;$ lateral force coefficient at $\beta = \delta = 0$, equal to zero for symmetrical airfoil;
- $\dfrac{d\,C_Y}{d\,\delta_r} \;=\;$ lateral force curve slope per deg of rudder deflection;
- $\delta_{r,\,max} \;=\;$ rudder control stop.

Assuming no deflection of the control cable, the maximum value of the lateral force coefficient is:

$$(C_Y)_{\delta_r\,=\,30} \;= 0.000644 \;*30 \;= 0.019356$$

The lateral force is calculated as follow:

$$Y \;=\; \frac{1}{10} * q_A * S_{vertical} * \frac{(C_Y)_{\delta_r\,=\,30}}{S_{ratio}} \;=\; (1/10) * 911 * 0.2044 * 0.01936/0.03947 \;= 9.131\; daN$$

The lateral force acting on a single fin of the vertical tail plain is 9.131/2 = 4.565 daN.

13.1.2. CSVLA 441(a)(2)

With the rudder deflected as specified in sub-paragraph CSVLA 441(a)(1) of this paragraph, it is assumed that the aeroplane yaws to the resulting sideslip angle. In lieu of a rational analysis, an overswing angle equal to 1.3 times the static sideslip angle of sub-paragraph CSVLA 441(a)(3) of this paragraph may be assumed. The overswing sideslip angle is 1.3 * 15 = 19.5 deg. The total lateral force acting on the vertical tail in this case is:

$$Y = \frac{1}{10} * q_A * S_{vertical} * \frac{C_Y}{S_{ratio}} = (1/10) * 911 * 0.2044 * 0.0245/0.03947 = 5.778\ daN$$

The lateral force acting on a single fin of the vertical tail plain is 5.778/2 = 2.889 daN.

13.1.3. CSVLA 441(a)(3)

A yaw angle of 15 degrees with the rudder control maintained in the neutral position (except as limited by pilot strength). The total lateral force in this case is:

$$Y = \frac{1}{10} * q_A * S_{vertical} * \frac{C_Y}{S_{ratio}} = (1/10) * 911 * 0.2044 * 0.0233/0.03947 = 5.495\ daN$$

The lateral force acting on a single fin of the vertical tail plain is 5.495/2 = 2.748 daN.

13.2. Manouevring and gust envelope

According to CSVLA 443 in the abscence of a more rational analysis, the gust load must be computed as follows:

$$L_{vt} = \frac{K_{gt} * U_{de} * V * a_{vt} * S_{vt}}{16.3}$$

where:

- $U_{de} = \text{derived gust velocity (m/s)};$
- $L_{vt} = \text{vertical tail load (daN)}$
- $K_{gt} = \dfrac{0.88 * \mu_{gt}}{5.3 + \mu_{gt}} = \text{gust alleviation factor};$
- $\mu_{gt} = \dfrac{2 * M}{\rho * \overline{c}_t * g * a_{vt} * S_{vt}} * \dfrac{K^2}{l_t^2} = \text{lateral mass ratio};$
- $M = \text{aeroplane mass (kg)};$
- $rho = \text{air density } (kg/m^3);$
- $l_t = \text{aeroplane c.g.} - \text{to} - \text{lift} - \text{centre of vertical surface distance } (m);$
- $S_{vt} = \text{area of vertical tail } (m^2);$
- $a_{vt} = \text{lift curve slope of vertical tail } (1/rad);$
- $V = \text{aeroplane equivalent speed } (m/s);$
- $K = \text{radius of gyration in yaw } (m);$
- $g = \text{acceleration due to gravity } (m/s^2);$

These calculations must be performed at VC and VD; the results are the following:

1. Gust load at VC: 8.8395 daN
2. Gust load at VD: 5.5247 daN

The critical gust load is 8.8395 daN at VC.

Chapter 14. Loads on the control surfaces

According to CSVLA 395 , the flight control system and its supporting structure must be designed for loads corresponding to 125 % of the computed hinge moments of the movable control surface.

14.1. Ailerons

According to CSVLA 395 , the total aileron load is equal to -991.5 N . The hinge moment is calculated by the following equation

$$H_{aileron} = q * S_{aileron} * c_f * C_{h_{total}} = -0.3883 * 911 * 0.1402 * 0.1354 = -6.714\ N * m$$

where:

- $H_{aileron}$ = aileron hinge moment $(N * m)$;
- q = dynamic pressure at point A (Pa) ;
- $S_{aileron}$ = aileron surface (m^2) ;
- c_f = reference chord (m) ;
- $C_{h_{total}}$ = total hinge moment coefficient.

This is the formula used in all the following calculations. The total hinge moment that must be considered in structural calculations is the following:

$$H_{aileron_{total}} = 2 * 1.25 * H_{aileron} = 2 * 1.25 * (-6.714) = -16.78\ N * m$$

14.2. Elevator

According to CSVLA 395 , the total elevator load is equal to -531.9 N. The hinge moment is

$$H_{elevator} = q * S_{elevator} * c_f * C_{h_{total}} = -0.2339 * 911 * 0.1475 * 0.1085 = -3.409\ N * m$$

The total hinge moment that must be considered in structural calculations is the following:

$$H_{elevator_{total}} = 2 * 1.25 * H_{elevator} = 2 * 1.25 * (-3.409) = -8.522\ N * m$$

14.3. Rudder

According to CSVLA 395 , the total rudder load is equal to -66.13 N. The hinge moment is

$$H_{rudder} = q * (2 * S_{rudder}) * c_f * C_{h_{total}} = -0.00792 * 911 * (2 * 0.01906) * 0.1085 = -0.7491\ N * m$$

where the surface is related to the double fin geometrical arrangement. The total hinge moment that must be considered in structural calculations is the following:

$$H_{rudder_{total}} = 1.25 * H_{rudder} = 1.25 * (-0.7491) = -0.9364\ N * m$$

Chapter 15. Power plant

15.1. Engine torque

The engine takeoff power is 11.19 kW at 5800 RPM. The rotational speed of the propeller is 5800/2.429 = 2388 RPM. The maximum continuous power is 9.321 kW. The mean engine torque is 44.73 N * m. Using a factor of 2 for a four cylinder engine, the limit torque will be 89.45 N * m. This limit torque acts simultaneously with the 75 % of the inertia limit load. The mean engine torque at max continuous power is 39.3 N * m. Using a factor of 2 for a four cylinder engine, the limit torque will be 78.61 N * m which acts simultaneously with the 100 % of the inertia limit load.

$$MT_{continuous} = P_{continuous} * \frac{1000}{\frac{2\pi * RPM_{prop}}{60}} = 9.321 * \frac{1000}{\frac{2 * 3.14 * 2388}{60}} = 39.3042\ N * m$$

$$LT_{continuous} = RR_{prop} * MT_{continuous} = 2.429 * 39.3 = 78.6084 N * m$$

$$MT_{takeoff} = P_{takeoff} * \frac{1000}{\frac{2\pi * RPM_{prop}}{60}} = 11.19 * \frac{1000}{\frac{2 * 3.14 * 2388}{60}} = 44.7255\ N * m$$

$$LT_{takeoff} = RR_{prop} * MT_{takeoff} = 2.429 * 44.73 = 89.4509 N * m$$

- $MT_{takeoff} = \text{mean torque at takeoff power (N * m); and}$
- $LT_{takeoff} = \text{limit torque at takeoff power (N * m); and}$
- $MT_{continuous} = \text{mean torque at max continuous power (N * m); and}$
- $LT_{continuous} = \text{limit torque at max continuous power (N * m).}$

15.2. Side load on engine mount

The limit load factor in a lateral direction is 1.33. The mass of the engine group is 24.4 kg. The side load results is 1.33*24.4*9.807*(1/10) = 31.82 daN

15.3. Intertia load on engine mount

The inertia load is equal to the maximum limit load factor times the engine group weight: 5.357*24.4*9.807*(1/10) = 170.5 daN

15.4. Gyroscopic loads

According to AMC 23.371(a) , for a two blade propeller, the maximum gyroscopic couple is given by:

$$2 * I_p * \omega_1 * \omega_2$$

Where:

- I_p = polar moment of inertia of the propeller (kg $*$ m^2); and
- ω_1 = propeller rotation speed (rad / sec); and
- ω_2 = rate of pitch or yaw (rad / sec).

The asymmetric flow through the propeller disc is discounted because the propeller diameter is less than 2.74 m as established by AMC 23.371(a) . The polar moment of inertia of the propeller is 0.37 kg*m^2. The rate of pitch or yaw is established as 1.0 rad/sec and 2.5 rad/sec respectively , the load factor is 2.5 and the power condition is max continuous power as prescribed in AMC 23.371(a) . Therefore, the inertial load is equal to 2.5*24.4 = 61 daN. The rotation of the propeller at maximum continuous power is 5500/2.4286 = 2264.6792. The gyroscopic couple is:

1. Yaw case: 2*0.37*2.5*(2*3.14/60)*2264.6792 = 69.8276 daN * m
2. Pitch case: 2*0.37*1.0*(2*3.14/60)*2264.6792 = 27.931 daN * m