DESIGN OF PIER CAP :-						
D.L./ M Width along bridge						
DL. Of Slab =	0.75 x	8.40 x.	2.4 =	15.12 T		
D.L. of Wearing coat =	0.08 x	8.40 x.	2.4 =	1.51 T		
· · · · · · · · · · · · · · · · ·			TOTAL	16.63 T		
D.L. of Slab & Wearing coat on half of the pier	=	=	<u> </u>	<u>'</u>		
		16.63 /	2 =	8.32 T		
L.L. on Pier cap including impact along bridge						
	=	82.50 x	1.1375 =	93.84 T		
(Refer Live Load Computation)						
Dispersion width across the span for						
70 T TRACKED VEHTCLE	=	6.695 M				
(Refer Solid slab design page SS-16)						
Live Load u.d.l. on Pier	=	93.84 /	6.695 =	14.02 T		
Per M width						
Total Load on Half =	8.32 -	+ 14	.02 =	22.33 T		
of pier along bridge				Per M width		
Effective depth of slab =90-2.5-2.5/2 =	71.25 cm					
Placement of the live load at effective depth from the support (taking support width 750 mm)						
Eccentricity = 71.25 -75/2	=	33.75 cm	= 0	.34 M		
Bending Moment along the bridge =						
	22.33 x	0.34	7	.54 T - M/M width		
=	22.00 X	0.01	•	.011 W/W WIGHT		
	7.54 x	10.00 =	75.4 kN-M/N	ما دار ا		
This mamont is too small benes it will not the deverging D.M.	7.54 X	10.00 =	/ 3.4 KIN-IVI/IV	i wiath		
This moment is too small hence it will not/be the governing B.M.		75.40 kN-m				
Moment in pier cap CONCRETE GRADE						
	M30					
FOR THIS GRADE σcbc		10 N/mm2 9.33				
m 		9.33 200				
σst factor k		0.318				
factor k		0.894				
J D		1.422				
R Effective Denth Required		1.422 230 mm				
Effective Depth Required						
Adopt Total Depth		1200 mm 50 mm				
Cover Assume Bar Dia		25 mm				
Keeping A Cover Of 50 mm Effective Depth		1138 mm				
		1137.5 mm				
Adopt Effective Depth						
Steel Required Ast		371 mm ²				
Area Of One Bar		491 mm ²				
Spacing S		1323 mm	A local Control	400		
Provide Bars Of Dia And Spacing	25 mm	100 mm	Adopt spacing as	100 mm		
Provide Bars Of Dia And Spacing for Top Main Steel	25 mm	100 mm				
Provide Bars Of Dia And Spacing for Bottom Steel	16 mm	100 mm				
PIER SECTION ACROSS BRIDGE						
DEAD LOAD MOMENT PER METRE Width across bridge :-	0.075	4=	2.4	05.40.		
Slab D.L.	0.975 x	15 x.	2.4 =	35.10 T		
D.L. of Wearing coat =	0.075 x	12 x.	2.4 =	2.16 T		
			TOTAL	37.26 ⊤		
D.L. of Slab & Wearing coat on half of the pier	=	= 07.00./	^	40.00 T/14 : 1		
		37.26 /	2 =	18.63 T/ M widt		

L.L on pier		=			64.69 T		
Dispersion width along the span for							
70 T Tracked vehical	=	5.3 N	Л				
L.L per M width on pier =			64.69 /	5.3	5.3 = 12.21 T/ M width		
Total D.L. + L.L. on half of Pier across		18.63 +	- 12	2.21	= 30.84 T		
bridge per M width					Per M width	h	
The Live Load is with clearance from the Footpath and kerb. The cantilever portion of pier	cap and width of footpath is 1	1500 mm					
Hence There is no eccentricity.							
Bending Moment across the bridge =							
		30.84 x	0		0.00 T - M/M width	n	
Provide Minimum steel							
Minimum Reinforcement calculation for Pier cap :-							
As per clause 710.8.2, IRC- 78 - 2000, the thickness of pier							
cap shall be at least 200 mm. However the thickness							
of Pier cap here is 1200 MM.							
Grade of Concrete M 30	4 2000						
Minimum Shrinkage and Temperature reinforcement required as per Clause 305.10 IRC 2 in any RC structure is 250 Sq mm per m in each direction. Allowable maximum spacing is 3							
	300 mm.			250 x	1.2 =	300 mm ²	
Shrinkage and Temperature reinforcement required = Provide 25 mm tor reiforcement @ 100 mm c/c (14 Nos.) in top along the pier cap			•	250 X	1.2 =	300 11111	
Provide 25 min for reiforcement @ 100 min c/c (14 Nos.) in top along the pier cap Provide 16 mm tor reiforcement @ 100 mm c/c (14 Nos.) in bottom along the pier cap	n						
Area of Steel Provided at top	P						
= (14x 491)	=	6874 n	nm² > 300	mm ²	OK		
- (TIX 10 1)	_	007 1					
Area of Steel Provided at bottom			_				
= (14x 201)	=	2814 n	$nm^2 > 300$	mm ²	OK		
CHECK FOR SHEAR ALONG BRIDGE DIRECTION							
V =		30.84 T					
Shear Force	/ - ->		308.40 kN				
V=V' + M/d tanB	(B=0) Hence V =V'						
Actual Shear Stress	4004 # 1	0.27 N/mm ²					
Percentage Steel	100As/bd	0.25					
Tc			0.23 N/mm ²				
k=1			2 22 2				
Permissble Shear Stress = k Tc		Λ -4	0.23 N/mm² al Shear Stress h				
			orcement should b				
Dia Of two Legged Stirrups		Keinik	16 mm	e provided			
Dia Oi two Legged Stirrups			10 111111				
Area Of One Bar In Distribution Reinforcement			201 mm ²				
Using The Bars Spacing Required s= Asw ts d/V			296 mm				
Provide Bars Of Dia And Spacing		16 mm	100 mm	Adopt space	cing as 100 mm		
HOWEVER							
Provide 16 mm tor 2 legged vertical stirrups @ 100 mm centre to centre along the pier Provide 16 mm tor 2 legged horizontal stirrups @ 100 mm centre to centre along the	_						
SHEAR CHECK ACROSS BRIDGE DIRECTION							
V =		20.3 T					
Shear Force		20.0 1	203.00 kN				
V VI - M/d to D	(B. 0) Hansa \/ \/'						

(B=0) Hence V =V'

V=V' + M/d tanB

Actual Shear Stress
Percentage Steel
Tc
k=1
Permissble Shear Stress = k Tc

0.18 **N/mm²** 100As/bd 0.25 0.23 **N/mm²**

0.23 N/mm² > Actual Shear Stress hence No Shear Reinforcement is required.

HOWEVER

Provide 16 mm tor 2 legged vertical stirrups @ 100 mm centre to centre along the pier cap Provide 16 mm tor 2 legged horizontal stirrups @ 100 mm centre to centre along the pier cap

3/{3} cross section Pier Cap