

REINFORCEMENT CALCULATION IN PIER

Name Of Work :- Construction of Submersible Bridge on ON KHERWARA - JAWAS - SUVERI ROAD IN KM 9/000, ACROSS RIVER SOM

R.L. 93.57 M TO 100.80 M

FOR SERVICE CONDITION

VERTICAL LOADS			
SUPER STRUCTURE	=	1463.62 kN	
SUB STRUCTURE	=	2821.21 kN	Without Buoyancy
SUB STRUCTURE	=	2271.84 kN	With Buoyancy
LIVE LOAD	=	788.27 kN	
Total Load without Buoyancy	=	5073.09 kN	
Total Load with Buoyancy	=	4523.72 kN	

Total LONGITUDINAL MOMENT			
Moment @ R. L.	93.57 M =	328.88 kN-m	

Total TRANSVERSE MOMENT			
Moment @ R. L.	93.57 M =	2332.51 kN-m	

CONCRETE MIX	M-25		
CHARACTERISTIC STRENGTH OF REINFORCEMENT		415 N/mm2	

PERMISSIBLE STRESSES			
IN STEEL	190		

IN CONCRETE			
CHARACTERISTIC STRENGTH OF			
Concrete	fck	=	30 N/mm2

Permissible Compressive Stress in			
Bending	σcbc	=	8 N/mm2

Permissible Compressive Stress in Direct			
Compression	σcc	=	8 N/mm2
	σct	=	3.6 N/mm2

Ultimate Axial Load P _U	=	1.5 X	5073.09 =	7609.631 kN
Ultimate Longitudinal Moment M _U	=	1.5 X	328.88 =	493.323 kN-m
Ultimate Transverse Moment M _U	=	1.5 X	2332.51 =	3498.765 kN-m

INCREASE WHEN WIND CONDITION IS CONSIDERED 33.33 %

Neglecting area of Cut and Ease water parts Rectangular Section considered is

12000 mm x 1200 mm

	Assume cover as	75				
d ¹ /d	=	87.5 /	1200 =	0.0729		
P _U /(f _{ck} b d)	=	7609.63 x	1000 / (30 x	12000 x	1200)
	=	0.0176				

FOR LONGITUDINAL MOMENT

Mu/(f _{ck} b d ²)	=	493.32 x	1000000 / (30 x	12000 x	1200 ²)
	=	0.0010				

Refer Chart 31 & 32 of Design Aids for Reinforced concrete SP-16 the point lies below the range of applicability. Hence provide minimum percentage of steel.

The point lies below the range of applicability. Hence provide minimum percentage of steel

CRITERIA 1 FOR MINIMUM STEEL P_t = 0.8 % OF CROSS SECTION AREA OF COLUMN REQUIRED FOR COMPRESSION

$$\begin{aligned} \text{Area Required due to Compression} &= \frac{4523.72 \times 1000}{8} \\ &= 565465 \text{ mm}^2 \\ \text{Area of steel @ 0.8\%} &= 0.8 \times \frac{565465}{100} \\ &= 4524 \text{ mm}^2 \end{aligned}$$

CRITERIA 2 FOR MINIMUM STEEL $P_t = 0.3\%$ OF GROSS SECTION AREA OF COLUMN

$$\begin{aligned} \text{Area of steel @ 0.3\%} &= 0.3 \times \frac{12000 \times 1200}{100} \\ &= 43200 \text{ mm}^2 \\ \text{PROVIDE STEEL AREA} &= 43200 \text{ mm}^2 \\ \text{NO. OF SPACING} &= 25 \text{ MM BARS} = 88 \text{ Nos.} \\ \text{FOR TRANSVERSE MOMENT} &= 290 \text{ MM} \end{aligned}$$

$$\begin{aligned} \frac{M_u}{(f_{ck} b d^2)} &= \frac{3498.76 \times 1000000}{12000 \times 1200^2} \times 30 \\ &= 0.0067 \end{aligned}$$

Refer Chart 31 & 32 of Design Aids for Reinforced concrete SP-16 the point lies below the range of applicability. Hence provide minimum percentage of steel.

TRANSVERSE REINFORCEMENT

Shear Force to be resisted by the pier In Accordance to IS 1893

$$\frac{2332.51}{11.87} = 196.46 \text{ kN}$$

Check for Shear

$$\begin{aligned} \text{Nominal Shear Stress} &= \frac{196.46 \times 1000}{12000 \times 1200} \\ &= 0.01 \text{ N/mm}^2 \\ P_t &= 0.30 \end{aligned}$$

$$\text{Permissible Shear Stress} = 0.40 \text{ N/mm}^2 \quad \text{Refer table 61}$$

Nominal Shear Reinforcement will suffice

According to IRC 21-1987 Clause 306.3

$$\begin{aligned} \text{Dia of Transverse Reinforcement} &= \frac{25}{4} = 6.25 \text{ mm} \\ \text{Provide} &= 12 \text{ mm dia rings} \end{aligned}$$

Pitch of the Transverse should be least of

$$\begin{aligned} \text{a) Least lateral Dimension} &= 1200 \text{ mm} \\ \text{b) } 12 d &= 12 \times 25 = 300 \text{ mm} \\ \text{c) } 300 \text{ mm} &= 300 \text{ mm} \\ \text{d) As per IS 13920:1993 Cl. 7.4.6} &< \text{ or } = 100 \text{ mm} \\ \text{Provide} &= 12 \text{ mm dia rings @ } 100 \text{ mm c/c.} \end{aligned}$$

This spacing is in accordance to IS 13920:1993 Cl. 7.4.6

CODE OF PRACTICE FOR DUCTILE DETAILING OF REINFORCED CONCRETE STRUCTURES SUBJECTED TO SEISMIC FORCES

Check for Size of Hoop Reinforcement

Refer IS 13920:1993 Cl. 7.4.8

$$A_{sh} = 0.18 S_h (F_{ck}/F_y) (A_g/A_k - 1)$$

$$\begin{aligned} S &= 100.00 \text{ mm} \\ h &= 300.00 \text{ N/mm}^2 \\ F_{ck} &= 30.00 \text{ N/mm}^2 \\ F_y &= 415.00 \text{ N/mm}^2 \end{aligned} \quad \begin{aligned} & \text{(Spacing of long. bars+ effective cover) or 300 mm whichever is less} \\ & \text{Cover 75 mm to main reinforcement} \end{aligned}$$

Ag	=	1200.00	mm ²	Considering 1 mm Wide Pier
Ak	=	1099.00	mm ²	Considering 1 mm Wide Pier Effective
Hence Ash	=	35.87	mm ²	
Ash ProvideD	=	113.04	mm ²	Which is OK

d) As per IS IS 13920:1993 Cl. 7.4.6 < or = 100 mm

Provide 12 mm dia rings @ 100 mm c/c.

This spacing is in accordance to IS 13920:1993 Cl. 7.4.6
CODE OF PRACTICE FOR DUCTILE DETAILING OF REINFORCED CONCRETE STRUCTURES SUBJECTED TO SEISMIC FORCES

ABSTRACT

LONGITUDINAL REINFORCEMENT	25	MM BARS	290	MM	However Adopt spacing as 250 mm
TRANSVERSE REINFORCEMENT	12mm dia rings @100mm c/c.				