

STEPSS

Static and Transient Electric Power Systems Simulation

Documentation of models and user guide

April 2023

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6. Limited version of the Software

This free-of-charge version of the software is limited to power system models up to 1000 buses (or nodes) and can be executed with parallelization using no more than two cores. For extensions to larger models or execution using more than two cores, you have to contact the Authors.

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Part I

Information pertaining to all three modules

Chapter 1

A quick overview of STEPSS

1.1 The three modules of STEPSS

STEPSS includes three modules:

- **PFC** (for Power Flow Computation) performs a power flow computation in order to determine the initial operating point of a dynamic simulation;
- **RAMSES** (for RApid Multiprocessor Simulation of Electric power Systems) simulates the dynamic evolution of the power system in response to disturbances/actions specified by the user;
- **CODEGEN** (for CODE GENerator) translates a model described by the user in a text file into its equivalent in FORTRAN 2003 language. The latter has to be compiled and linked to a user-defined executable version RAMSES.

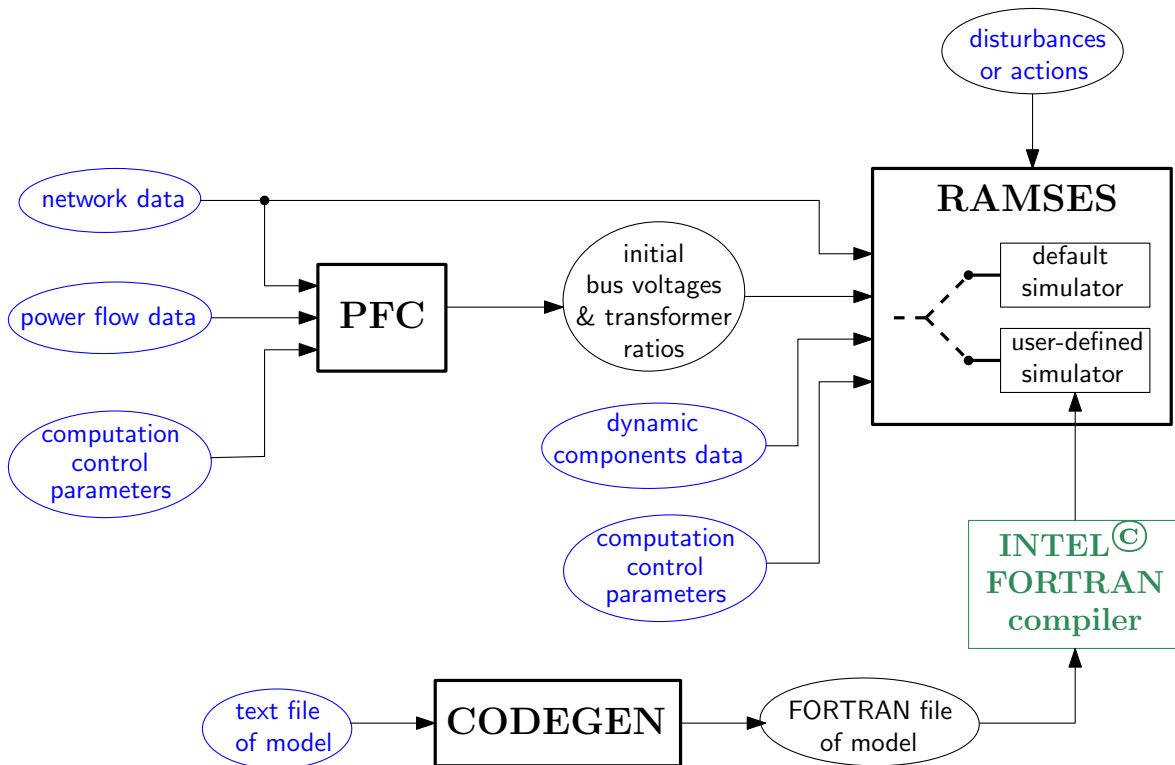


Figure 1.1: STEPSS: Overview of modules and data files. The files shown in blue are provided by the user, those in black are produced internally. The Intel[®] FORTRAN compiler is not part of STEPSS

The three modules, their relationships and their input/output data files are shown graphically in Fig. 1.1.

Note that each of the three modules can be used separately. Here are examples of such uses:

- PFC alone: a power flow computation is run to inspect the power system state and/or save the corresponding power flow solution for use by RAMSES;

- PFC alone: a sequence of power flow computations is performed until obtaining the desired power system state. The corresponding power flow solution is saved for use by RAMSES;
- RAMSES alone: with the initial power flow solution produced by PFC, several dynamic simulations are run starting from that initial state, i.e. without invoking PFC each time;
- CODEGEN alone: a model is built and saved for future incorporation in a user-defined version of RAMSES.

1.2 PFC module

The power flow computation resorts to the well-known Newton(-Raphson) method. Polar coordinates are used.

As shown in Fig. 1.1, the input information consists of:

- network data relative to buses, lines, transformers, etc.
- power flow data specified at PV, PQ and slack buses, respectively
- PFC control parameters. These are settings such as: tolerances on final power mismatches, thresholds to enforce reactive power limits of generators, etc. These are optional data; if they are not provided, default values (listed in this documentation) are used.

Optionally PFC also adjusts the ratios of some transformers, with the objective:

- for an in-phase transformer: to bring the voltage magnitude at a bus inside a specified dead-band
- for a phase-shifting transformer: to bring the active power flow in a network branch inside a specified deadband.

PFC produces an output file including:

- the voltage magnitudes and phase angles at all buses of the network
- the adjustable transformer data with updated values of their ratios.

1.3 RAMSES module

RAMSES is aimed at simulating the dynamic response of power system models derived under the phasor approximation (also known as RMS approximation).

It takes as input (see Fig. 1.1):

- the network data, which are shared with PFC¹
- the data pertaining to the dynamics of the components connected to the network
- RAMSES control parameters. These are settings such as: tolerances for solving the equations, variation of state variables to identify the Jacobians, time steps of plots, reference angular speed, etc.
- the sequence of actions and/or disturbances imposed during the simulation.

The mathematical model involves both differential and algebraic equations.

Three algebraization methods are available to integrate the differential equations:

- Backward Euler:

$$x_{k+1} = x_k + h \dot{x}_{k+1}$$

- Trapezoidal method:

$$x_{k+1} = x_k + \frac{h}{2} (\dot{x}_{k+1} + \dot{x}_k)$$

- Second-order Backward Differentiation Formula (BDF2):

$$x_{k+1} = \frac{4}{3}x_k - \frac{1}{3}x_{k-1} + \frac{2h}{3}\dot{x}_{k+1}$$

where h is the time step size. The three methods are implicit, which contributes to numerical robustness. BDF2 is a stiff-decay (or L_1 -stable) integration scheme allowing to somewhat increase the time step size when fast transients are not of interest.

The resulting algebraized and the original algebraic equations are solved all together using a Newton method. Some more information follows.

1.3.1 About the solver

The solver was developed in response to the growing demand for simulations that last longer (e.g. long-term stability studies) or involve larger models (e.g. to account for the impact of active distribution networks). A high computational efficiency is made possible by two acceleration techniques: parallel processing and localization.

Parallel processing is based, first, on the decomposition of the power system model into respectively the network, the “injectors” and the “two-ports”. Injectors and two-ports are solved independently of each other. However, by resorting to the Schur-complement for the network equations, RAMSES yields the exact same solution as a non-decomposed scheme².

Next, the tasks pertaining to injectors and two-ports are assigned to a number of *threads*. Examples of tasks are:

¹with a few exceptions (detailed in this document)

²The solution scheme is thus of the simultaneous type while offering some advantages of a partitioned scheme

- the update and factorization of injector Jacobians
- the computation of the whole mismatch vector of Newton method
- the computation of injector contributions to the Schur-complement matrix
- the solution of local linear systems.

The threads can be executed each on a separate processor, the computational load being balanced among the available processors. The freeware version of STEPSS allows exploiting two processors.

The solver in RAMSES has been developed using a shared-memory parallel programming model with the help of the OpenMP Application Programming Interface. The implementation is general: there is no “hand-crafted” optimization particular to the computer system, the power system or the disturbance.

Localization is based on the fact that, after a disturbance, the various components of a (large enough) system exhibit different levels of dynamic activity.

This property is exploited at each time step:

- to accelerate the Newton scheme: thanks to the decomposed solution scheme, Newton iterations are skipped on injectors and two-ports that have already converged
- to exploit component “latency”: injectors with high dynamic activity are classified as active, the others as latent. Active injectors have their original model simulated, while latent injectors are replaced by automatically calculated, sensitivity-based models to accelerate the simulation. A fast to compute metrics is used to classify the injectors, which seamlessly switch between categories according to their activity.

More information on the solver can be found in the following references:

- D. Fabozzi, A. Chieh, B. Haut, and T. Van Cutsem, “Accelerated and localized newton schemes for faster dynamic simulation of large power systems,” IEEE Trans. on Power Systems, Vol. 28, No 4, pp. 4936-4947, Dec. 2013
doi: 10.1109/TPWRS.2013.2251915
- P. Aristidou, D. Fabozzi, and T. Van Cutsem, “Dynamic simulation of large-scale power systems using a parallel Schur-complement-based decomposition method,” IEEE Trans. on Parallel and Distributed Systems, Vol. 25, No 10, pp. 2561-2570, Sept. 2014,
doi:10.1109/TPDS.2013.252

1.4 CODEGEN module

CODEGEN allows incorporating user-defined models in RAMSES. Different versions of the RAMSES executable can be loaded and executed. This involves a translation of the user model speci-

fied in a text file into FORTRAN 2003 code to be compiled and linked to the rest of the executable. The FORTRAN 2003 language can produce very efficient number crunching code.

Don't panic: in the vast majority of cases, the user does not need to even open the FORTRAN file. The user concentrates on the text file describing his/her model, which is rather easy to read.

Thus, the user model is not interpreted but executed.

There are four types of user-defined models:

- excitation controller of synchronous machine: typically the excitation system and the automatic voltage regulator
- torque controller of synchronous machine: typically the turbine and the speed governor
- injector: a component connected to a single AC bus
- two-port: a component connecting two buses.

While the code of the solver is not made public, the models are expected to be freely shared by users.

The above features make STEPSS a true **open-source simulation software**.

Chapter 2

Installing STEPSS

The material of this chapter is specific to the Windows 64-bit version of STEPSS, to its Java-based Graphic User Interface (GUI) and the Intel oneAPI Fortran Compiler.

Before going any further, you have to read and accept the legal terms detailed at the beginning of this document.

2.1 Graphical User Interface

STEPSS comes with a Java-based Graphical User Interface (GUI). This is a Java archive containing a (legal) copy of all executables and libraries required to run the simulations and display the results.

Using that GUI requires to have a Java machine installed on your computer. This is very often the case in the Windows environment. It can be checked as follows:

- open a Windows Command prompt
- in the latter, enter the command:

```
java -version
```

It should display a message similar to the one shown in Fig. 2.1. If so, close the command prompt.

- Otherwise download and install a Java machine as explained on the Web page:

```
www.java.com/en/download/.
```

Apart from the Java machine, STEPSS does not require any installation in the usual meaning of the term. Just download the `STEPSS.jar` file in any convenient place of the computer. The Windows desktop is a very convenient location.

Leave the archive intact; in particular do not uncompress it !

STEPSS is launched by merely double-clicking on `STEPSS.jar` or a shortcut to the latter.

When STEPSS is launched it creates a temporary working folder and copies all needed executables and libraries into that folder.

To remove STEPSS from your computer, just delete the archive file. STEPSS does not leave anything in your computer !



```
C:\Users\tvanc\onedrive\Travail>java -version
java version "17.0.4.1" 2022-08-18 LTS
Java(TM) SE Runtime Environment (build 17.0.4.1+1-LTS-2)
Java HotSpot(TM) 64-Bit Server VM (build 17.0.4.1+1-LTS-2, mixed mode, sharing)

C:\Users\tvanc\onedrive\Travail>
```

Figure 2.1: Checking the presence of a Java machine

2.2 Intel oneAPI Fortran Compiler

The Intel oneAPI Fortran Compiler is needed if (and only if) you develop new models with the help of the CODEGEN module.

There are four packages to download from Microsoft and Intel Web sites. All are freely available. Wait until all packages are downloaded before installing.

2.2.1 Downloading Microsoft developer studio

This is a (monster) development environment hosting the Intel software. Here is the link to the 2019 version of Visual Studio Community:

<https://visualstudio.microsoft.com/en/thank-you-downloading-visual-studio/?sku=Community&rel=16>

Select "Windows operating system".

2.2.2 Downloading Intel oneAPI Base Toolkit

This is required for full functionality of the compiler. Here is the link:

<https://software.intel.com/content/www/us/en/develop/tools/oneapi/base-toolkit/download.html>

Select “Windows operating system”.

2.2.3 Downloading Intel oneAPI HPC toolkit

This includes the Fortran Classic compiler (among various programming languages). Here is the link:

<https://software.intel.com/content/www/us/en/develop/tools/oneapi/hpc-toolkit/download.html>

Select “Windows operating system”.

2.2.4 Downloading Intel Fortran Compiler Classic Runtime for Windows

These are libraries specific to a given compiler. They must be downloaded and installed separately from the oneAPI HPC toolkit. Here is the link:

<https://software.intel.com/content/www/us/en/develop/articles/oneapi-standalone-components.html>

Select “Runtime Versions - Microsoft Windows” and “Intel Fortran Compiler Runtime for Windows”.

2.2.5 Installing

Simply run (double-click) the .exe packages, **in the following order**:

1. Microsoft visual studio. Select the workload “Desktop development with C++”
2. oneAPI Base Toolkit
3. oneAPI HPC toolkit
4. Fortran runtime libraries for oneAPI.

Chapter 3

Organisation of the data files

Data files are organised into *records* and *comments*, whose syntax is detailed next.

3.1 Records

Each record includes:

- a leading *keyword*, which identifies the information provided in the record
- a number of *fields*. A field is either a real number (numeric field) or a string of characters (character field). There is at least one field
- a *terminating semicolon* (;), which indicates the end of the record.

✚ The following record, with keyword `LINE`, specifies a transmission line:

```
LINE A-B BUS_A BUS_B 3.0 30.0 150.0 1400.0 1 ;
```

Inside the record, the keyword, the fields and the terminating semicolon are separated by (at least one) space(s). Anything after the semicolon is ignored. The next record (or comment) starts with the next line.

✚ Two incorrect versions of the above sample record, owing to missing spaces:

```
LINE A-B BUS_ABUS_B 3.0 30.0 150.0 1400.0 1 ;
LINE A-B BUS_A BUS_B 3.030.0 150.0 1400.0 1 ;
```

Inside a data file, a record may span over multiple lines; the semicolon indicates the end of the record. Spanning over several lines is highly recommended for records that include many fields. Note that, depending upon the text editor and its settings, a long record could appear truncated when displayed.

✚ An example of long record spanning over two lines:

```
INJEC GFOL VSC1 A 1.0 1.0 0.0 0.0 0.005 0.15 1.00 1044.0 0.005 0.15 33.3
10.0 0.002 -999.0 10.0 0.1667 50.0 0.10 0.4 0.5 1.0 0.95 0.5 99.0 1 ;
```

The nature of each field, and the total number of fields are specified in this documentation. Some records have optional fields, which are always located at the end of the record.

3.1.1 Constraints on numeric fields

There is almost no constraint on numeric fields. They are written in free format. The notation is that of floating-point numbers in MATLAB: with or without a dot, with or without an exponent, exponent denoted by E or D.

☛ Different valid formats of the same number: 30 30. 30.0 3E01 3.E01 3.0E01 3.E1 3.e1

3.1.2 Constraints on character fields

Character fields are limited to 20 characters. Only the first 20 characters are read; the remaining of the string is just ignored, without warning. It is thus discouraged to have more than 20 characters in a field.

Furthermore, some character fields are limited to eight characters; the remaining of the string is just ignored.

Uppercase letters are significant within a character field. Thus, two fields that differ by the upper-case/lowercase spelling are different.

If a character field includes a space or a slash (/), it must be enclosed with quotes (' or "). In between the two quotes, the leading spaces are significant while the trailing ones are ignored. Keywords do not include spaces; hence, the use of quotes is useless.

Because the semi-column (;) is a special character (used to indicate the end of a record), **it must not be included in any character field**, even within quotes.

3.2 Comments

There are three ways to insert comments in the data files:

1. a line in which the first non blank character is an exclamation mark (!). At most the first 130 characters after the ! are memorised and reproduced on output files
2. a line in which the first non blank character is the sharp character (#): this line is simply ignored by the program
3. anything written after the semicolon that terminates a record is also ignored. This is convenient to store (short) comments next to a record, without interfering with the latter.

☛ Comments starting with # can be used to identify the fields of a record:

```

#           name bus FP  FQ  P  Q SNOM RS   LLS LSR  RR    LLR
INJEC INDMACH1 SM   2  0.2 0.2 0. 0. 0. 0.031 0.1 3.2 0.018 0.180
#
                                     H   A   B   LF
                                     0.7 0.5 0.0 0.6 ;

```

Comments do not span over several lines. If several lines are needed, each of them must start with a ! or a #.

Empty lines are just ignored.

3.3 Sharing data between files

Records may be distributed over an arbitrary number of data files, which will be read sequentially. The order in which the records are placed inside the data files does not matter. The order in which the files are read does not matter either.

For instance, a first data file may be devoted to network data, a second one to data for the initial power flow computation, a third one to the dynamic data of the components connected to the network and a last one to simulation control parameters. The second and third files, for instance, may be swapped in the list without any effect.

Chapter 4

Modelling of network components

The network model includes buses, lines, cables, transformers and shunts. Their models and data are described in the present chapter.

4.1 Buses

In dynamic simulations with RAMSES the only parameter associated with a bus is its nominal voltage (more precisely, the RMS value of the nominal line-to-line voltage). This is used as base voltage to convert parameters from physical to per unit values.

If two buses have different nominal voltages they cannot be connected through a path made up of lines or switches (see next sections). This causes the software to issue an error message and stop.

4.1.1 Data format

The record, with keyword BUS, includes the following fields:

```
BUS NAME VNOM ;
```

where:

- NAME is the name of the bus. This is a string of at most 8 characters
- VNOM is the nominal voltage, in kV.

Only one BUS record per bus is allowed.

All buses must be declared through BUS records. If the software finds (in other than BUS records) a bus name not defined through a BUS record, it issues an error message and stops.

Caveat. The above record is used in the RAMSES module. For the initial power flow computation with PFC, an extended version of the BUS record is used with six fields instead of two. Please refer to Section 5.1. Thus, when RAMSES is initialized, if a BUS record has six fields, only the first two are read, the others are ignored.

4.2 Lines and cables

4.2.1 Modelling

Lines and cables both have the same pi-equivalent model, which is shown in Fig. 4.1. Note that shunt conductances are neglected.

Under the phasor approximation, series capacitors can also be modelled with this pi-equivalent, by setting R and C to zero and X to a negative value.

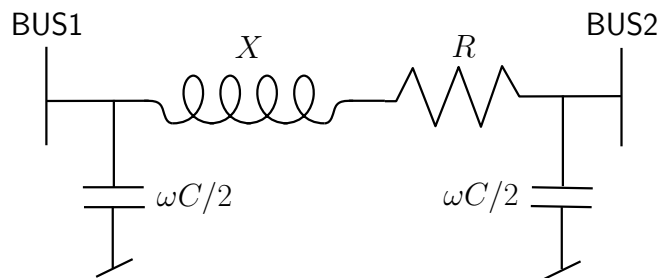


Figure 4.1: Pi-equivalent of lines and cables

4.2.2 Data format

The record, with keyword LINE, includes the following fields:

```
LINE NAME BUS1 BUS2 R X WC2 SNOM BR ;
```

where:

- **NAME** is the name of the line or cable. This is a string of at most 20 characters
- **BUS1** is the name of the first bus. This is a string of at most 8 characters defined in a BUS record
- **BUS2** is the name of the second bus. This is a string of at most 8 characters defined in a BUS record
- **R** is the series resistance R , in Ω
- **X** is the series reactance X , in Ω
- **WC2** is the half shunt susceptance $\omega C/2$, in μS (microSiemens)
- **SNOM** is the nominal apparent power, in MVA. This value is used to display the line loading, or possibly in user-defined models. If not used, it may be set to zero; this will be interpreted as an infinite power
- **BR** is the on/off status of the line breakers. A zero value indicates that the breakers are open at both ends (line out of service); any other value (e.g. 1) means that both breakers are closed (line in service).

The orientation of the line is arbitrary: BUS1 and BUS2 may be swapped.

Only one LINE record per line is allowed.

All lines are memorized, even those that are out of service. A line out of service is not involved (it appears in the output results with a zero power flow) but it can be put into service in the dynamic simulation.

As mentioned in Section 4.1, a line must not connect two buses with different nominal voltages.

To have a line connected through a single end, add a bus at the open end and set BR to a nonzero value.

4.3 Switches

4.3.1 Modelling

A switch is a connection without impedance between two buses. It is treated as a very short line, more precisely a line with $R = 0$, $\omega C/2 = 0$ and X set to a very low value. Thus it has no active power losses and negligible reactive power losses.

4.3.2 Data format

The record, with keyword SWITCH, includes the following fields:

```
SWITCH NAME BUS1 BUS2 BR ;
```

where:

- **NAME** is the name of the switch. This is a string of at most 20 characters
- **BUS1** is the name of the first bus. This is a string of at most 8 characters defined in a BUS record
- **BUS2** is the name of the second bus. This is a string of at most 8 characters defined in a BUS record
- **BR** is the on/off status of the switch. A zero value indicates that the switch is open; any other value means that it is closed.

The orientation of the switch is arbitrary: BUS1 and BUS2 may be swapped.

Only one SWITCH record per switch is allowed.

All switches are memorized, even those which are open. An open switch is not involved (it appears in the output results with a zero power flow) but it can put into service in the dynamic simulation.

As mentioned in Section 4.1, it is not allowed to have a switch connecting two buses with different nominal voltages.

4.4 Transformers

4.4.1 Modelling

Transformers are represented by the two-port shown in Fig. 4.2. Note that R , X , B_1 and B_2 are specified on the “from” side of the transformer.

R corresponds to the copper losses. The iron losses are neglected (no shunt resistance). X is the leakage reactance. B_1 or B_2 are the magnetizing susceptances, which have negative values. Usually one of them is zero. n (resp. ϕ) is the magnitude (resp. the phase angle) of the transformer ratio. A phase-shifting transformer is characterized by a nonzero value of ϕ .

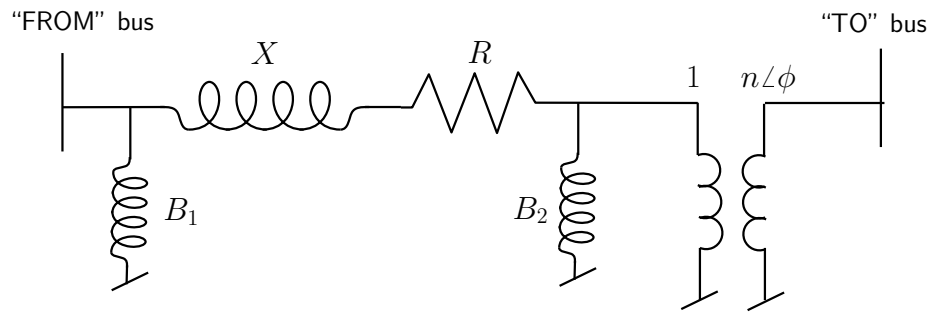


Figure 4.2: Two-port model of transformers

It may be of interest to recall how the values of R , X , B_1 and B_2 relate to the following characteristics, easily obtained from manufacturer data:

- S_{nom} the nominal apparent power
- V_{N1} (resp. V_{N2}) the nominal voltage on the “from” (resp. “to”) side (see Fig. 4.2)
- $R_{baseV_{N1}}$ (resp. $X_{baseV_{N1}}$) the series resistance (resp. leakage reactance) in per unit on the (S_{nom}, V_{N1}) base
- $B_{1baseV_{N1}}$ and $B_{2baseV_{N1}}$ the shunt susceptances in per unit on the (S_{nom}, V_{N1}) base
- V_{o1} and V_{o2} the open-circuit voltages corresponding to the transformer ratio¹.

¹Very often the open-circuit voltages coincide with the nominal voltages, i.e. $V_{o1} = V_{N1}$ and $V_{o2} = V_{N2}$

Let V_{B1} and V_{B2} be the nominal voltages of respectively the “from” and the “to” buses, as specified in their BUS records (see Section 4.1).

In STEPSS R , X , B_1 and B_2 are in percent on the (S_{nom}, V_{B1}) base. The following changes of base have to be used:

$$\begin{aligned} R &= 100 R_{baseV_{N1}} \left(\frac{V_{N1}}{V_{B1}} \right)^2 & X &= 100 X_{baseV_{N1}} \left(\frac{V_{N1}}{V_{B1}} \right)^2 \\ B_1 &= 100 B_{1baseV_{N1}} \left(\frac{V_{B1}}{V_{N1}} \right)^2 & B_2 &= 100 B_{2baseV_{N1}} \left(\frac{V_{B1}}{V_{N1}} \right)^2 \end{aligned}$$

n is in percent on the (V_{B1}, V_{B2}) base. Its value is given by:

$$n = 100 \frac{V_{o2} V_{B1}}{V_{o1} V_{B2}}$$

A second transformer model is available. It is a simplified version with $B_2 = 0$ and $\phi = 0$ in Fig. 4.2 and includes data for PFC to adjust the transformer ratio (see Section 5.5). This model cannot be used for phase-shifting transformers.

4.4.2 Data format

The record, with keyword TRANSFO, includes the following fields:

```
TRANSFO NAME FROMBUS TOBUS R X B1 B2 N PHI SNOM BR ;
```

where:

- NAME is the name of the transformer. This is a string of at most 20 characters
- FROMBUS is the name of the “from” bus (see Fig. 4.2). This is a string of at most 8 characters defined in a BUS record
- TOBUS is the name of the “to” bus (see Fig. 4.2). This is a string of at most 8 characters defined in a BUS record
- R is the series resistance, in % on the base detailed above
- X is the leakage reactance, in % on the base detailed above
- B1 is the shunt suceptance, in % on the base detailed above
- B2 is the shunt suceptance, in % on the base detailed above
- N is the magnitude of the transformer ratio in % (dimensionless)
- PHI is the phase angle of the transformer ratio, in degree
- SNOM is the nominal apparent power of the transformer, in MVA. This value must not be zero
- BR is the on/off status of the transformer breakers. A zero value indicates that the breakers are open at both ends (transformer out of service); any other value means that both breakers are closed (transformer in service).

The second transformer model is described by the record with keyword TRFO:

```
TRFO NAME FROMBUS TOBUS CONBUS R X B N SNOM NFIRST NLAST NBPOS TOLV VDES BR ;
```

where:

- NAME is the name of the transformer. This is a string of at most 20 characters
- FROMBUS is the name of the “from” bus (see Fig. 4.2). This is a string of at most 8 characters defined in a BUS record
- TOBUS is the name of the “to” bus (see Fig. 4.2). This is a string of at most 8 characters defined in a BUS record
- CONBUS is used by PFC for adjusting n : see Section 5.5. It is not used by RAMSES, but a (dummy) name must be provided
- R is the series resistance, in % on the base detailed above
- X is the leakage reactance, in % on the base detailed above
- B is the shunt susceptance, in % on the base detailed above
- N is the magnitude of the transformer ratio in % (dimensionless)
- SNOM is the nominal apparent power of the transformer, in MVA. This value must not be zero
- NFIRST is used by PFC for adjusting n : see Section 5.5.
- NLAST: same as for NFIRST
- NBPOS: same as for NFIRST
- TOLV: same as for NFIRST
- VDES: same as for NFIRST
- BR is the on/off status of the transformer breakers. A zero value indicates that the breakers are open at both ends (transformer out of service); any other value means that both breakers are closed (transformer in service).

The following remarks apply to both TRANSFO and TRFO records.

The orientation of the transformer is not arbitrary: FROMBUS and TOBUS cannot be swapped.

Only one TRANSFO or TRFO record per transformer is allowed.

All transformers are memorized, even those that are out of service. A transformer out of service is not involved (it appears in the output results with a zero power flow) but it can be put into service in the dynamic simulation.

To have a transformer connected through a single end, add a bus at the open end and set BR to a nonzero value.

4.5 Non-reciprocal two-ports

4.5.1 Modelling

A non-reciprocal two-port is a two-port with a non-symmetric nodal admittance matrix of the form:

$$\mathbf{Y} = \begin{bmatrix} (G_{si} + jB_{si}) + (G_{ij} + jB_{ij}) & -(G_{ij} + jB_{ij}) \\ -(G_{ji} + jB_{ji}) & (G_{ji} + jB_{ji}) + (G_{sj} + jB_{sj}) \end{bmatrix}$$

with:

$$G_{ij} \neq G_{ji} \quad \text{and} \quad B_{ij} \neq B_{ji}$$

where i and j relate to the terminal nodes of the two-port, as shown in Fig. 4.3.

Typically, two-ports are produced when reducing a network that includes phase-shifting transformers, the purpose being to obtain an equivalent.



Figure 4.3: A two-port connecting buses i and j

4.5.2 Data format

The record, with keyword NRTP, includes the following fields:

```
NRTP NAME FROMBUS TOBUS GIJ BIJ GJI BJI GSI BSI GSJ BSJ BR ;
```

where:

- NAME is the name of the two-port. This is a string of at most 20 characters
- FROMBUS is the name of bus i in Fig. 4.3. This is a string of at most 8 characters defined in a BUS record
- TOBUS is the name of bus j in Fig. 4.3. This is a string of at most 8 characters defined in a BUS record
- GIJ is the G_{ij} conductance, in pu
- BIJ is the B_{ij} susceptance, in pu
- GJI is the G_{ji} conductance, in pu
- BJI is the B_{ji} susceptance, in pu
- GSI is the G_{si} conductance, in pu
- BSI is the B_{si} susceptance, in pu
- GSJ is the G_{sj} conductance, in pu
- BSJ is the B_{sj} susceptance, in pu

- `BR` is the on/off status of the two-port breakers. A zero value indicates that the breakers are open at both ends (two-port out of service); any other value means that both breakers are closed (two-port in service).

The parameters of the two-port are given in per unit on the following base: nominal bus voltages, system base power. By default a value of 100 MVA is used² but it can be changed: see Section 5.9.

It is allowed for a non-reciprocal two-port to connect two buses with different nominal voltages.

The orientation of the two-port is not arbitrary: FROMBUS and TOBUS cannot be swapped.

Only one NRTP record per two-port is allowed.

A non-reciprocal two-port is treated as a piece of equipment; hence, the presence of the `BR` field. All non-reciprocal two-ports are memorized, even those which are out of service. A non-reciprocal two-port out of service is not involved (it appears in the output results with a zero power flow) but it can be put into service in the dynamic simulation.

4.6 Shunts

4.6.1 Modelling

The shunt element is treated as a purely reactive, constant shunt admittance. Hence, the reactive power Q it produces varies with the square of the voltage V according to:

$$Q = B V^2$$

where B is the susceptance. The element may correspond to either a capacitor ($B > 0$) or a reactor ($B < 0$).

4.6.2 Data format

The record, with keyword SHUNT, includes the following fields:

```
SHUNT NAME BUS_NAME QNOM BR ;
```

where:

- `NAME` is the name of the shunt. This is a string of at most 20 characters

²a typical value for transmission systems

- `BUS_NAME` is the name of the bus to which the shunt is connected. This is a string of at most 8 characters defined in a BUS record
- `QNOM` is the nominal reactive power of the shunt, in Mvar. This is the reactive power produced by the shunt under the nominal voltage of the bus, specified in its BUS record. `QNOM` is positive (resp. negative) for a shunt capacitor (resp. inductor)
- `BR` is the on/off status of the shunt. A zero value indicates that the shunt is not connected; any other value means that it is in service.

Only one SHUNT record per named shunt is allowed. Multiple shunts at the same bus are allowed, but each with its own name. In this case, the susceptances are added (taking signs into account).

All shunts are memorized, even those which are disconnected. A disconnected shunt is not involved (it appears in the output results with a zero power flow) but it can be put into service in the dynamic simulation.

Caveat. The above record is used in the RAMSES module. However, for the initial power flow computation with PFC, the shunt data are attached to a bus and are specified in an extended version of the BUS record. Please refer to Section 5.1.

Part II

Power Flow Computation with PFC

Chapter 5

PFC data

The following records, documented in Chapter 4 are used by PFC:

BUS
 LINE
 SWITCH
 TRANSFO
 TRFO
 NRTP.

The additional (mandatory or optional) records only used in power flow computations are documented in this chapter.

5.1 Load and shunt data

Load and shunt data are attached to buses. They are specified in an extended version of the BUS record, as follows:

```
BUS NAME VNOM PLOAD QLOAD BSHUNT QSHUNT ;
```

where:

- **NAME** is the name of the bus. This is a string of at most 8 characters
- **VNOM** is the nominal voltage, in kV
- **PLOAD** is the total active power load at the bus, in MW. A positive value corresponds to power drawn from the network
- **QLOAD** is the total reactive power load at the bus, in Mvar. A positive value corresponds to power drawn from the network
- **BSHUNT** is the nominal reactive power of the shunt modelled as constant susceptance, in Mvar. This is the reactive power produced by the shunt under the nominal voltage of the bus, specified in its BUS record. BSHUNT is positive (resp. negative) for a shunt capacitor (resp. inductor)
- **QSHUNT** is the reactive power produced by the shunt modelled as constant power, in Mvar. QSHUNT is positive (resp. negative) for a shunt capacitor (resp. inductor).

The total reactive power Q produced by the two shunt components is given, in Mvar, by:

$$Q = BSHUNT \left(\frac{V}{V_{nom}} \right)^2 + QSHUNT$$

where V is the bus voltage and V_{nom} the corresponding nominal voltage.

If no shunt is connected to the bus, BSHUNT and QSHUNT are set to zero.

If no load is connected to the bus, PLOAD and QLOAD are set to zero.

Let us recall that the PLOAD, QLOAD, BSHUNT and QSHUNT fields are ignored by RAMSES.

5.2 Generator data

Generators are specified by GENER records, as follows:

```
GENER NAME BUS P Q VIMP SNOM QMIN QMAX BR ;
```

where:

- **NAME** is the name of the generator. This is a string of at most 20 characters
- **BUS** is the name of the bus which the generator is connected to. This is a string of at most 8 characters
- **P** is the active power produced by the generator, in MW
- **Q** is the reactive power produced by the generator, in Mvar. This value is ignored if the **VIMP** field is nonzero
- **VIMP** is the voltage imposed by the generator, in pu. If **VIMP** is zero, the bus is treated as a PQ bus with the reactive power production set to **Q**; if **VIMP** is nonzero, the bus is treated as a PV bus and the **Q** field is ignored
- **SNOM** is the nominal apparent power of the generator, in MVA
- **QMIN** is the lower reactive power limit, in Mvar. It is used only if **V** is nonzero
- **QMAX** is the upper reactive power limit, in Mvar. It is used only if **V** is nonzero
- **BR** is the on/off status of the generator breaker. A zero value indicates that the breaker is open; any other value means that the breaker is closed.

For all generators with a nonzero value of **VIMP**, the connection bus is initially assumed of the PV type.

If this entails exceeding the generator upper reactive power limit **QMAX**, the bus switches to PQ type, the **QMAX** limit is enforced, and Newton iterations continue. If subsequently the bus voltage gets larger than **VIMP**, the bus switches back to PV type with the voltage imposed at the **VIMP** value.

Similarly, if the generator lower reactive power limit **QMIN** is exceeded, the bus switches to PQ type, the **QMIN** limit is enforced, and Newton iterations continue. If subsequently the bus voltage gets smaller than **VIMP**, the bus switches back to PV type with the voltage imposed at the **VIMP** value.

Only one generator is allowed per bus.

All generators are memorized, even those which are disconnected. A disconnected generator is not involved (it appears in the output results with a zero power output) but it can be put into service in the dynamic simulation.

Remark 1. For simplicity, a generator producing constant active and reactive powers can be modelled as a negative load using the BUS and no GENER record.

Remark 2. There exists a variant of the GENER record with the following syntax:

```
GENER NAME BUS P Q V SNOM QMIN QMAX PMIN PMAX BR ;
```

where `PMIN` (resp. `PMAX`) is the minimum (resp. maximum) active power that the generator can produce, in MW. If this record is present in the data, the `PMIN` and `PMAX` fields are ignored by STEPSS.

5.3 Slack-bus specification

The presence of a slack-bus is mandatory in power flow computations: indeed, not all buses can be of the PV or PQ type, since this would entail specifying the active power losses in the network, which are not known before performing the power flow calculation.

A generator of the PV type must be connected to the slack-bus. Its voltage magnitude, specified in its GENER record, is imposed at the bus, while the voltage phase angle is set to zero.

PFC can handle only one connected network. If the network graph is not connected, *only the connected sub-network including the slack-bus is treated*; the rest of the network is ignored with a warning message.

The SLACK record allows specifying which bus is the slack-bus. The syntax is as follows:

```
SLACK NAME ;
```

where `NAME` is the name of the bus. This is a string of at most 8 characters.

There must be exactly one SLACK record in the whole set of data.

5.4 Static Var Compensators

5.4.1 Modelling

The Static Var Compensator (SVC) is modelled as shown in Fig. 5.1. j is the *monitored* bus, whose voltage is regulated, while i is the *controlled* bus, where the shunt susceptance B is varied. i and j can be any two buses but usually j is the transmission bus on the high-voltage side of the SVC step-up transformer, while the SVC is connected to bus i .

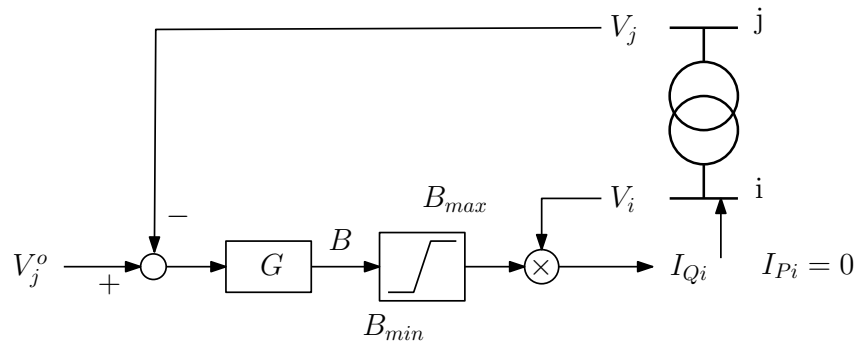


Figure 5.1: Block-diagram of the static var compensator

The SVC being assumed lossless, the active current injected at bus i is zero ($I_{Pi} = 0$), while the reactive current takes on one of the following forms:

$$I_{Qi} = BV_i = G(V_j^o - V_j)V_i \quad \text{under voltage control} \quad (5.1)$$

$$I_{Qi} = B_{max}V_i \quad \text{under upper susceptance limit} \quad (5.2)$$

$$I_{Qi} = B_{min}V_i \quad \text{under lower susceptance limit.} \quad (5.3)$$

Although reference is made to an SVC, the model can be used in general for a component controlling voltage with a droop.

5.4.2 Data format

The record, with keyword SVC, includes the following fields:

```
SVC NAME CON_BUS MON_BUS V0 Q0 SNOM BMAX BMIN G BR ;
```

where:

- NAME is the name of the compensator. This is a string of a most 20 characters
- CON_BUS is the name of the controlled bus. This is a string of a most 8 characters

- `MON_BUS` is the name of the monitored bus. This is a string of a most 8 characters
- `V0` is the voltage setpoint V_j^o , in pu (see Fig. 5.1)
- `Q0` is the reactive power setpoint, in Mvar. If `V0` is set to zero, the SVC is treated under constant power, with $P = 0$ and $Q = Q0$, and no limit is tested. If `V0` is nonzero, the `Q0` field is ignored
- `SNOM` is the nominal reactive power of the SVC, in Mvar
- `BMAX` is the maximal nominal reactive power, in Mvar. This is the reactive power produced by the compensator under $V_i = 1$ pu, when B is at the maximal value B_{max} .
- `BMIN` is the minimal nominal reactive power, in Mvar. This is the reactive produced by the compensator under $V_i = 1$ pu, when B is at the minimal value B_{min} .
- `G` is the gain G , in pu on the (V_B, SNOM) base, where V_B is the nominal voltage at the controlled bus, as given by its BUS record
- `BR` is the on/off status of the SVC breaker. A zero value indicates that the breaker is open, any other value means that it is closed.

It is common for `BMAX` to be positive and `BMIN` negative but other combinations are allowed.

For all SVCs with a nonzero value of `V0`, Eq. (5.1) is solved initially.

If this entails exceeding the susceptance upper reactive power limit `BMAX`, Eq. (5.2) is substituted, the `BMAX` limit is enforced, and Newton iterations continue. If subsequently $G(V_j^o - V_j) < B_{max}$, the program reverts to Eq. 5.1 and keeps on iterating.

Similarly, if the SVC lower susceptance limit `BMIN` is exceeded, Eq. (5.3) is substituted, the `BMIN` limit is enforced, and Newton iterations continue. If subsequently $G(V_j^o - V_j) > B_{min}$, the program reverts to Eq. (5.1) and keeps on iterating.

Only one SVC is allowed per bus.

It is not allowed to connect both a generator and an SVC to the same bus.

All SVCs are memorized, even those which are disconnected. A disconnected SVC is not involved (it appears in the output results with a zero power output) but it can be put into service in the dynamic simulation.

5.5 Transformer ratio adjustment for voltage control

5.5.1 Modelling

PFC can adjust the ratio of a designated transformer with the objective of bringing a controlled voltage inside a deadband $[V_{des} - \epsilon, V_{des} + \epsilon]$, where V_{des} is the desired voltage and ϵ is a tolerance.

The ratio is changed in discrete steps (as in the real life), between a minimum and a maximum value. During the computation, the ratio is changed by one step at a time, after which Newton iterations are performed until convergence is achieved. The process is repeated until the controlled voltage falls in the deadband. When multiple transformers are adjusted, some may reach their deadbands before others.

5.5.2 First data format

The first way to specify ratio adjustment is through the TRFO record. The following refers to the material presented in Section 4.4.2.

The controlled bus is `CONBUS`. This must be one of the two ending buses of the transformer. An empty or blank string *enclosed within quotes* indicates that the transformer ratio is not to be adjusted. In this case, however, dummy values must be provided for each of the fields listed below.

The fields of concern are:

- `NFIRST`: the ratio in % corresponding to the first tap position. This is the lower bound on the transformer ratio
- `NLAST`: the ratio in % corresponding to the last tap position. This is the upper bound on the transformer ratio
- `NBPOS`: the total number of tap positions including the first and the last
- `TOLV`: the voltage tolerance ϵ , in pu
- `VDES`: the desired voltage V_{des} , in pu.

The transformer ratio n corresponding to position p ($1 \leq p \leq \text{NBPOS}$) of the tap changer is given by:

$$n = \frac{\text{NFIRST}}{100} + \frac{p - 1}{\text{NBPOS} - 1} \frac{\text{NLAST} - \text{NFIRST}}{100} \quad (5.4)$$

The value of p is increased or decreased by one at each adjustment iteration.

An initial value of the transformer ratio is given by the `N` field of the TRFO record. If the transformer is to be adjusted, before starting the power flow computation that value is adjusted to coincide with the nearest tap position, in accordance with Eq. (5.4).

5.5.3 Second data format

The second way to specify ratio adjustment is through a separate record with keyword LTC-V. The syntax is as follows:

```
LTC-V NAME CON_BUS NFIRST NLAST NBPOS TOLV VDES ;
```

where `NAME` is the name of the controlled transformer (a string of at most 20 characters) and all the other fields have the same meaning as for the TRFO record.

A transformer can be controlled by a single tap changer only. It is more natural to use the LTC-V record in association with a TRANSFO record. However, the LTC-V record can be associated with a TRFO record, provided that no adjustment is specified in the latter.

5.6 Phase-shifting transformer ratio adjustment for power control

5.6.1 Modelling

PFC can also adjust the phase angle of a transformer with the objective of bringing the active power flow in a branch inside a deadband $[P_{des} - \epsilon, P_{des} + \epsilon]$, where P_{des} is the desired power flow and ϵ is a tolerance.

The adjustment is very similar to that of in-phase transformers for voltage control detailed in Section 5.5.

5.6.2 Data format

The record, with keyword `PSHIFT-P`, includes the following fields:

```
PSHIFT-P CONTRFO MONBRANCH PHAFIRST PHALAST NBPOS SIGN PDES TOLP ;
```

where:

- `CONTRFO` is the name for the transformer whose phase angle is to be adjusted. This is a string of at most 20 characters, defined in either a TRFO or a TRANSFO record. If the transformer does not exist, the whole record is ignored with a warning message
- `MONBRANCH` is the name of the branch in which the active power flow P is monitored. This is a string of at most 20 characters, defined in either a LINE, a TRFO or a TRANSFO record. The sign convention is the following: P is the active power flow leaving the first bus specified in the LINE, TRFO or TRANSFO record and entering the branch of concern
- `PHAFIRST` is the phase angle ϕ , in degrees, corresponding to the first tap position. This is the lower bound on ϕ
- `PHALAST` is the phase angle ϕ , in degrees, corresponding to the last tap position. This is the upper bound on ϕ
- `NBPOS` is the number of tap positions
- `SIGN` is an indication of the direction in which the phase angle ϕ must be adjusted to reach

the objective. A value of 1 indicates that ϕ must be increased to increase the active power flow in the monitored branch. A value of -1 indicates that it must be decreased. Any other value is invalid and causes the program to stop

- PDES is the desired active power flow, in MW
- TOLP is the tolerance ϵ , in MW.

The phase angle ϕ corresponding to position p ($1 \leq p \leq \text{NBPOS}$) of the tap changer is given by:

$$\phi = \text{PHAFIRST} + \frac{p - 1}{\text{NBPOS} - 1} (\text{NLAST} - \text{NFIRST}) \quad (5.5)$$

The value of p is increased or decreased by one at each adjustment iteration.

PFC performs a sensitivity analysis to determine whether the phase angle should be increased or decreased. If this analysis indicates a direction opposite to what is specified in `SIGN`, a warning is issued and the value of `SIGN` is ignored. On output, when it produces a file with the records updated, PFC sets `SIGN` to the value corresponding to its sensitivity analysis.

An initial value of the phase angle is given by the `PHI` field of the `TRANSFO` record. If the transformer is to be adjusted, before starting the power flow computation, that value is adjusted to coincide with the nearest tap position, in accordance with Eq. (5.5).

A transformer cannot be controlled by both an `LTC-V` and a `PSHIFT-P` record.

Only one `PSHIFT-P` record per transformer is allowed. The `PSHIFT-P` record is intended to be used in association with a `TRANSFO` record. However, it is allowed to associate it with a `TRFO` record in spite of the fact that the latter assumes a zero phase angle. In this case, the angle will be initialized to zero and will be controlled as specified in the `PSHIFT-P` record.

5.7 Bus voltages: initial values and results

On output, PFC produces a file with the computed bus voltage magnitudes and phase angles. The latter are specified in records with keyword `LFRESV`. The syntax is as follows:

```
LFRESV BUS MODV PHASV ;
```

where:

- `BUS` is the name of the bus. This is a string of a most 8 characters defined in a `BUS` record
- `MODV` is the bus voltage magnitude, in pu
- `PHAV` is the bus voltage phase angle, in radian, the slack bus being the reference.

If `LFRESV` records are provided on input, they are used as initial voltages of the Newton iterations, at the specified buses.

If no LFRESV record is specified at a bus:

- the voltage magnitude is initialized to 1 pu if the bus is of the PQ type or to the value imposed by the generator in case of a PV bus
- the phase angle is initialized to 0 degree.

Thus, if the LFRESV records obtained from a first run of PFC are added to the data files, the other data being unchanged, no Newton iteration is going to be performed since we are already at the solution. This is an easy way to check that system data come with their corresponding voltages.

5.8 Share of records between PFC and RAMSES

A summary of the records used by respectively PFC and RAMSES is given in Table 5.1.

Table 5.1: records used by PFC and RAMSES, respectively

record	in PFC	in RAMSES
BUS	all 6 fields used	only first two fields used
LINE	used	used
SWITCH	used	used
NRTP	used	used
TRANSFO	used	used
TRFO	used	only fields 1 to 9 and 15 used
SHUNT	ignored	used
GENER	used	ignored
SVC	used	ignored
SLACK	used	used
LFRESV	used	used
LTC-V	used	ignored
PHSHIFT-P	used	ignored

5.9 Computation control parameters

5.9.1 Parameters

PFC performs Newton(-Raphson) iterations to solve the power flow equations. At the k -th iteration, the following indices are computed:

$$\epsilon_P = \max_i |f_i(\mathbf{v}^{(k)}, \boldsymbol{\theta}^{(k)}) - P_i^o| \text{ the largest absolute mismatch of the active power equations}$$

$\epsilon_Q = \max_i |g_i(\mathbf{v}^{(k)}, \boldsymbol{\theta}^{(k)}) - Q_i^o|$ the largest absolute mismatch of the reactive power equations
 $\epsilon_S = \max_i \sqrt{(f_i(\mathbf{v}^{(k)}, \boldsymbol{\theta}^{(k)}) - P_i^o)^2 + (g_i(\mathbf{v}^{(k)}, \boldsymbol{\theta}^{(k)}) - Q_i^o)^2}$ the largest apparent power mismatch.

Convergence is achieved once :

- both ϵ_P and ϵ_Q are below specified thresholds
- all controls on transformer ratios and phase shifts are satisfied, and
- all generators and SVCs are within their reactive limits.

ϵ_S is used to check that the solution is accurate enough to :

- “freeze” the Jacobian matrix (in order to save some computing time)
- check the generator and SVC reactive power limits and enforce the latter if needed
- adjust the transformer ratios and phase shifts to control voltage magnitudes and active power flows, if specified in the data.

Finally, the iterations stop as soon as divergence is detected. To this purpose the quadratic index:

$$\varphi(k) = \sum_i \sqrt{(f_i(\mathbf{v}^{(k)}, \boldsymbol{\theta}^{(k)}) - P_i^o)^2 + (g_i(\mathbf{v}^{(k)}, \boldsymbol{\theta}^{(k)}) - Q_i^o)^2}$$

is monitored. Under normal convergence conditions, φ decreases from one iteration to the next. Therefore, the increase in φ is used to detect divergence. The algorithm stops at the iteration k such that :

$$\varphi(k) > 1.1 \varphi(k-1)$$

However, this test is skipped at any iteration k that follows the switching of generators or SVCs under limit, or the adjustment of transformer ratios and phase shifts¹.

5.9.2 Records

The records detailed hereafter are used to control the computation. They all start with a \$ to distinguish them from the other records. They all have a single field, as detailed in Table 5.2. The default value assigned in the absence of the record is given in the fourth column.

¹indeed, these adjustments cause increases in φ that have nothing to do with divergence

Table 5.2: Computation control parameters

record	meaning of field	unit	default value
\$SBASE	base power (on which pu values are expressed)	MVA	100
\$TOLAC	ϵ_P	MW	0.1
\$TOLREAC	ϵ_Q	Mvar	0.1
\$NBITMA	max number of iterations	-	20
\$MISQLIM	value of ϵ_S below which the reactive power limits are checked and enforced. Set to 0 to skip the limit check	MVA	20
\$MISBLOC	value of ϵ_S below which the Jacobian is kept constant.	MVA	10
\$MISADJ	value of ϵ_S below which transformers are adjusted. Set to 0 to skip adjustment	MVA	10
\$DIVDET	set to 1 to activate divergence test during iterations. Set to 0 to skip test	-	0

Part III

Dynamic Simulation with RAMSES

Part IV

Adding user-defined models with CODEGEN

Chapter 6

User models: mathematical formulation and syntax of description

6.1 States and equations

6.1.1 States

The four categories of user-defined models and their acronyms are as follows:

EXC excitation controller of synchronous machine: typically the excitation system and the Automatic Voltage Regulator (AVR), including the Power System Stabilizer (PSS)

TOR torque controller of synchronous machine: typically the turbine and the speed governor

INJ injector: a component connected to a single AC bus

TWOP two-port: a component connecting two buses.

Whichever its type, any model has input states (grouped in \mathbf{x}_{IN}), internal states (in \mathbf{x}_{ITL}) and output states (in \mathbf{x}_{OUT}) as sketched in Fig. 6.1. Note that states can be indifferently differential or algebraic states.

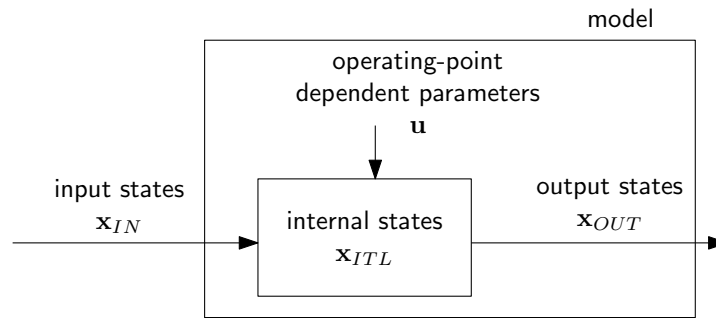


Figure 6.1: Outline of a model

The input and output states pertaining to each category of model are detailed in Table 6.1. The notation is as follows:

For an excitation controller:

V terminal voltage of the machine, in pu

P active power produced, in pu on the machine rated apparent power (MVA)

Q reactive power produced, in pu on the machine rated apparent power (MVA)

ω rotor speed, in pu

i_f field current, in pu on the exciter base current

v_f field voltage, in pu on the exciter base voltage.

For a torque controller:

ω rotor speed, in pu

P active power produced, in pu on the turbine rated power (MW)

T_m mechanical torque applied to rotor, in pu on the turbine rated torque.

Table 6.1: Input and output states

type of model	input states	output states
excitation controller of synchronous machine	V, P, Q, ω, i_f of machine	v_f of machine
torque controller of synchronous machine	P, ω of machine	T_m of machine
injector	v_x, v_y at bus ω_{coi}	i_x, i_y into bus
two-port	$v_{x1}, v_{y1}, v_{x2}, v_{y2}$ at buses ω_{coi}	$i_{x1}, i_{y1}, i_{x2}, i_{y2}$ into buses

For an injector:

- v_x, v_y rectangular components of phasor of voltage at the connection bus (the (x, y) reference axes have been defined in Chapter ???)
- i_x, i_y rectangular components of phasor of current injected into the connection bus
- ω_{coi} angular frequency of center of inertia, in pu¹.

For a two-port:

- v_{x1}, v_{y1} rectangular components of phasor of voltage at bus 1
- v_{x2}, v_{y2} rectangular components of phasor of voltage at bus 2
- i_{x1}, i_{y1} rectangular components of phasor of current injected into bus 1
- i_{x2}, i_{y2} rectangular components of phasor of current injected into bus 2
- ω_{coi} angular frequency of center of inertia, in pu.

The models also include operating-point dependent parameters (grouped in **u**).

The three categories of states are treated as follows:

- **at the initialization** of the model:
 - the input states are given. They are obtained from the synchronous machine states (see Section ???) or the initial power injected into buses (see Section ???)
 - the output states are also given, using the same information²
 - the internal states are initialized either explicitly by the user or automatically by RAM-SES
 - the operating-point dependent parameters are initialized by the user, in agreement with the initial values of the states

¹This can be used as an average system frequency. One of the modelling blocks (see next Chapter) offers the possibility to estimate the “local” frequency at the connection bus

²at first glance, specifying both the input and the output states would lead to an overdetermined system with more equations than states; this is not the case since the excess equations are used to initialize the operating-point dependent parameters **u**. The number of the latter is equal to the number of output states

- **during the simulation:**

- the input, the internal and the output states are computed together with the other system states
- the operating-point dependent parameters remain constant, unless they are modified by a user action (see Section ???).

Note that the model must have a number of equations at least equal to the number of output states, otherwise it is not correctly formulated.

Note also that not all input states need be used.

✚ Consider the very simple excitation system shown in Fig. 6.2. The following equations are easily derived:

$$0 = V^o - V - dV \quad (6.1)$$

$$T \frac{dv_f}{dt} = -v_f + G dV \quad (6.2)$$

The model has a single input (V), a single internal state (dV) and the requested output state (v_f). dV is an algebraic state, while v_f is a differential one. V^o is the single component of the \mathbf{u} vector.

At initialization, the system is assumed in steady state: $\frac{dv_f}{dt} = 0$. Hence, $dV(0) = \frac{v_f(0)}{G}$, where (0) denotes values at $t = 0$. V^o is obtained from Eq. (6.1) as: $V^o = V(0) + dV(0)$.

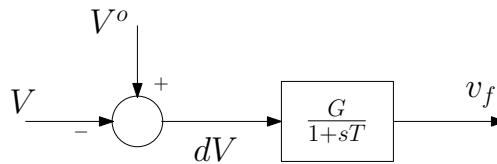


Figure 6.2: A very simple model of excitation system

6.1.2 Equations

As they are determined from the machine and the network equations, the input states are not part of the user model state vector, which thus takes on the form:

$$\mathbf{x} = \begin{bmatrix} \mathbf{x}_{ITL} \\ \mathbf{x}_{OUT} \end{bmatrix} \quad (6.3)$$

The differential-algebraic equations can be written in compact form as:

$$\mathbf{T}\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{x}_{IN}, \mathbf{u}, \mathbf{z}) \quad (6.4)$$

where \mathbf{x} and \mathbf{f} have the same dimension. The i -th row of matrix \mathbf{T} includes:

- only zeros if the i -th equation is algebraic
- a single nonzero term T_{ij} if the i -th equation is differential with:

$$T_{ij}\dot{x}_j = f_i(\mathbf{x}, \mathbf{x}_{IN}, \mathbf{u}, \mathbf{z})$$

where i and j may be different.

The nonzero components of \mathbf{T} are time constants, typically.

\mathbf{z} is a vector of discrete variables whose role is detailed in the next section.

6.2 Discrete transitions

The material of this section is provided for information in so far as the corresponding treatment is performed automatically by STEPSS. Nevertheless, it may help interpreting the output curves and/or some execution messages.

6.2.1 Formulation

✚ Consider now a little more detailed version of the model in Fig. 6.2, including non-windup limits on the integrator embedded in the first-order transfer function, as shown in Fig. 6.3.

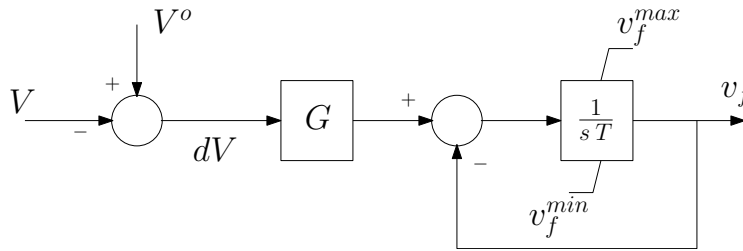


Figure 6.3: A little more detailed version of the system in Fig 6.2

The system is modelled by one of the following three sets of equations:

- if the integrator is not at any of its limits ($z = 0$):

$$0 = V^o - V - dV \quad (6.5)$$

$$T \frac{dv_f}{dt} = -v_f + G dV \quad (6.6)$$

- if the integrator is at its upper limit ($z = 1$):

$$0 = V^o - V - dV \quad (6.7)$$

$$0 = v_f^{max} - v_f \quad (6.8)$$

- if the integrator is at its lower limit ($z = -1$):

$$0 = V^o - V - dV \quad (6.9)$$

$$0 = v_f^{min} - v_f \quad (6.10)$$

As shown in the above example, a discrete variable z is used to identify which set of equations must be solved at any given time of the simulation. The values assigned to z are completely arbitrary. Changing z from one value to another corresponds to substituting one set of equations to another. Such “discrete transitions” take place when some inequality constraints are violated. A typical example is when a state exceeds its prescribed limit.

Note incidentally that differential equations can be changed into algebraic ones, and conversely. This is a feature offered by RAMSES.

✚ In the example of Eqs. (6.5-6.10), here is the pseudo-code performing the discrete transitions relative to the non-windup integrator:

```

if  $z = 0$  then
  if  $v_f > v_f^{max}$  then
     $z \leftarrow 1$ 
  else if  $v_f < v_f^{min}$  then
     $z \leftarrow -1$ 
  end if
else if  $z = 1$  then
  if  $(-v_f + G dV)/T < 0$  then
     $z \leftarrow 0$ 
  end if
else if  $z = -1$  then
  if  $(-v_f + G dV)/T > 0$  then
     $z \leftarrow 0$ 
  end if
end if

```

The z variables are initialized at the beginning of the simulation, as for the states.

✚ In the example of Eqs. (6.5-6.10), here is the pseudo-code initializing the z variable relative to the non-windup integrator:

```

if  $v_f > v_f^{max}$  then
   $z \leftarrow 1$ 
else if  $v_f < v_f^{min}$  then
   $z \leftarrow -1$ 

```

```

else
   $z \leftarrow 0$ 
end if

```

In the above example, at $t = 0$, if v_f violates one of its limits, it is brought back to that limit. This means that a discrete transition will take place right away at $t = 0$.

6.2.2 Solution scheme

This section deals with the handling of discrete transitions when passing from time t to time $t + h$, where h is the time step size. It is assumed that the system equations have been irrevocably solved until time t .

When the solver detects that the condition for a discrete transition has been satisfied in the time interval $[t, t + h]$, it does not attempt to identify the exact time t' ($t < t' \leq t + h$) when the condition became satisfied. Instead, the following *ex post* solution scheme is used:

1. for the value of the discrete variables z prevailing at time t , Eqs. (6.4) are integrated from t to $t + h$ with full accuracy³
2. at the resulting point, the inequality constraints associated with discrete transitions are checked. If needed, z is changed, i.e. Eqs. (6.4) are changed
3. the integration step from t to $t + h$ is canceled, all states are reset to their values at time t , and the new equations (6.4) are integrated from t to $t + h$ with full accuracy
4. if needed, steps 2 and 3 are repeated until no change in z takes place. As the solver could be trapped in a limit cycle of discrete transitions, a maximum number of z changes at the same time is allowed. If that number is reached, the integration time step size is temporarily decreased from h to its minimum value h_{min} (see Section ???). If the limit cycle problem persists with the minimum step size, the simulation stops; the model should be adjusted with respect to the sequence of discrete transitions.

The solution scheme is presented in greater detail in:

D. Fabozzi, A. S. Chieh, P. Panciatici and T. Van Cutsem “On simplified handling of state events in time-domain simulation”, Proc. of the 17th Power System Computation Conference (PSCC), 2011

It is illustrated graphically in Fig. 6.4, for a single state x and a single discrete variable z . The numbers refer to the above steps and times are shown in parentheses.

³solving them with less accuracy, to the purpose of gaining time, might lead to wrong identification of the discrete transitions

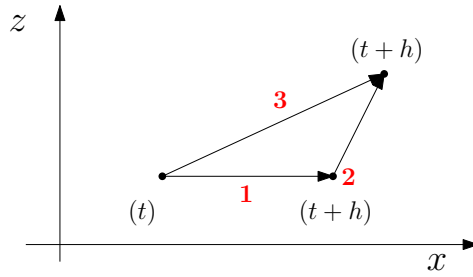


Figure 6.4: Graphical representation of the solution scheme to handle discrete transitions

6.3 Model assembly

In order for CODEGEN to generate the differential-algebraic equations of an arbitrarily complex user model, the latter is decomposed into a set of simple, interconnected *modelling blocks*. The latter correspond to time constants, integrators, PID controllers, non-linearities, etc. The library of available modelling blocks is documented in Chapter 7.

The EXC, TOR, INJ or TWOP model is thus handled as a set of interconnected modelling blocks, as illustrated in Fig. 6.5.

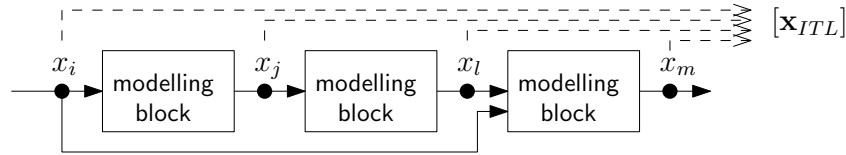


Figure 6.5: A user model made up of interconnected modelling blocks

Each block contributes with its algebraic and/or differential equations. Equations (6.4) are obtained by gathering the equations of all the blocks.

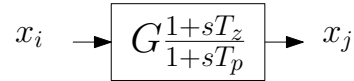
The blocks are interconnected through links. A distinct internal state (contributing to \mathbf{x}_{ITL}) is associated with each link. It can be differential or algebraic. Each of these states must be given by the user a unique name as well as an initial value.

Most of the modelling blocks also involve internal states (contributing to \mathbf{x}_{ITL}). Unlike the states associated with links between the blocks, the user does not need to name them, nor to initialize them; this is done automatically by the code generated by CODEGEN.

Finally, some modelling blocks involve discrete variables \mathbf{z} .

☛ **Example.** The modelling block `tflpz` is an example of block with one internal state. It implements the transfer function with one pole and one zero shown in Fig. 6.6.

x_i is either an input or an internal state, while x_j is either an internal or an output state. The model requires three data: G , T_z and T_p .

Figure 6.6: The `tf1p1z` modelling block

CODEGEN generates the following equations:

$$\dot{x}_1 = G x_i - x_j \quad (6.11)$$

$$0 = T_p x_j - G T_z x_i - x_1 \quad (6.12)$$

where x_1 is an internal state. The latter is automatically initialized to :

$$x_1(0) = G (T_p - T_z) x_i(0)$$

which is obtained by setting the derivative of x_1 to zero in the above equations.

6.4 Syntax of the model description

A model is specified in a text file with the contents and structure shown in Fig. 6.7. The name of the file can be freely chosen.

The file is made up of six sections, which are detailed hereafter. All sections must be present and in the order shown in Fig. 6.7.

All keywords must be written exactly as specified in this documentation. In particular the upper/lowercase must be the same and no blank must be inserted or skipped.

6.4.1 Header

The header includes two lines in which:

<type of model> specifies the type of model. It can be `exc`, `tor`, `inj` or `twop`, as explained in Section 6.1.1

<name of model> specifies the name of the model. This is a string of at most 16 characters

If a model type `abc` and a model name `xyz` are specified, the complete name of the model will be `abc_xyz.f90`. This name has to be used in the data files (see Section ???). CODEGEN will correspondingly produce a file named `abc_xyz.f90` with the FORTRAN code of the model.

```

<type of model>
<name of model>
%data
<name of data 1>
<name of data 2>
:
%parameters
<name of parameter 1>=<mathematical expression 1>
<name of parameter 2>=<mathematical expression 2>
:
%states
<name of internal state 1>=<mathematical expression of initial value 1>
<name of internal state 2>=<mathematical expression of initial value 2>
:
%observables
<name of state, data or parameter 1>
<name of state, data or parameter 2>
:
%models
& <name of modelling block 1>
<name of state 1>
<name of state 2>
:
<name of data 1, name of parameter 1 or mathematical expression 1>
<name of data 2, name of parameter 2 or mathematical expression 2>
:
& <name of modelling block 2>
<name of state 1>
<name of state 2>
:
<name of data 1, name of parameter 1 or mathematical expression 1>
<name of data 2, name of parameter 2 or mathematical expression 2>
:

```

Figure 6.7: Syntax of model files

6.4.2 Data section

The data section starts with the keyword `%data`.

Each data must be given a unique name. That name, enclosed with braces {}, is used in the rest of the model description.

Each name can be followed by a comment, on the same line, starting with an exclamation mark !.

At the initialization of a simulation, RAMSES maps the data present in the input file with those declared in the data section of the model. The data are read from the data file in the order specified in the data section.

As explained in Chapter ???, the data of the EXC and TOR models are embedded in the synchronous machine record. Those of the INJ model are provided in an INJEC record and those of the TWOP model in a TWOP record.

6.4.3 Parameter section

The parameter section starts with the keyword `%parameters`.

Each parameter must be given a unique name. That name, enclosed with braces {}, is used in the rest of the model description. The braces are not needed when a parameter is first defined, i.e. before the = symbol⁴.

Each name can be followed by a comment, on the same line, starting with an exclamation mark !.

A data and a parameter cannot be given the same name.

At initialization of the simulation, each parameter is given the value specified by the mathematical expression after the = symbol. This expression usually involves data but it can also involve parameters which have been previously defined⁵. It may involve standard mathematical functions such as *cos*, ****, *sqrt*, etc. The syntax is that of the FORTRAN language. It can be found for instance at:

<https://www.intel.com/content/www/us/en/docs/fortran-compiler/developer-guide-reference/2023-0/categories-of-intrinsic-functions.html>

6.4.4 State section

The state section starts with the keyword `%states`.

Each internal state must be given a unique name. That name, enclosed with brackets [], is used in the rest of the model description. As for parameters, the brackets are not needed when a state

⁴since CODEGEN expects to find a parameter, there is no ambiguity

⁵the names of those parameters must be enclosed in braces

Table 6.2: Reserved names that must be used for internal states

model type	reserved names	meaning of state
exc	v	terminal voltage of machine
	p	active power produced by machine
	q	reactive power produced by machine
	omega	rotor speed of machine
	if	field current of machine
	vf	field voltage of machine
tor	p	mechanical power produced by turbine
	omega	rotor speed of machine
	tm	mechanical torque of turbine
inj	vx	x component of bus voltage
	vy	y component of bus voltage
	omega	angular speed of center of inertia
	ix	x component of current injected into network
	iy	y component of current injected into network
twop	vx1	x component of voltage at bus 1
	vy1	y component of voltage at bus 1
	vx2	x component of voltage at bus 2
	vy2	y component of voltage at bus 2
	omega	angular speed of center of inertia
	ix1	x component of current injected into network at bus 1
	iy1	y component of current injected into network at bus 1
	ix2	x component of current injected into network at bus 2
	iy2	y component of current injected into network at bus 2

is first defined, i.e. before the = symbol.

Each state declaration can be followed by a comment, on the same line, starting with an exclamation mark !.

A state cannot have the same name as a data or a parameter.

Input and output states have their own, reserved names that cannot be used for internal states. They are listed in Table 6.2. All values are in pu on the bases detailed in Section 6.1.1.

Each internal state is initialized at the value specified by the mathematical expression after the = symbol. This expression may involve data, parameters or states⁶ that have been previously defined or are listed in Table 6.2. The mathematical expression may involve standard mathematical functions: see previous section.

Only internal states are declared, input and output states are not. Let us recall that their initial

⁶the initial values of those states, to be precise

values are known.

6.4.5 Observable section

The observable section starts with the keyword `%observables`.

Observables are quantities candidate to be plotted as functions of time at the end of the simulation. They are usually (input, output or internal) states but data or parameters are also allowed⁷.

There is no need to enclose the names with braces or brackets.

6.4.6 Model section

The model section starts with the keyword `%models`.

The modelling blocks and their data are enumerated sequentially. The order does not matter. Each modelling block is identified by the `&` symbol, **followed by a space**, followed by the name of the block. The information required by each block is detailed in the next chapter.

Each name can be followed by a comment, on the same line, starting with an exclamation mark `!`.

The end of the section coincides with the end of the file.

6.4.7 An example

Here is the code of the simple excitation system shown in Fig. 6.3. The name of the model is “simple_avr”. There are three observables: one parameter, one internal state and one output state

```
exc
simple_avr
%data
G          ! gain of exciter
T          ! time constant of the exciter
vfmin      ! lower field voltage
vfmax      ! upper field voltage
%parameters
Vo = [v]+ [vf]/{G}  ! voltage setpoint of AVR
```

⁷this allows displaying the time evolution of a controller setpoint, for instance

```

%states
dv = [vf]/{G}          ! voltage error
%observables
Vo
dv
vf
%models
& algeq                ! calculation of voltage error
{Vo}-[v]-[dv]
& tf1plim              ! exciter transfer function
dv
vf
{G}
{T}
{vfmin}
{vfmax}

```

Here is the trace of execution, showing the counts of equations and states, respectively, as the modelling blocks are assembled.

```

                WELCOME TO CODEGEN      v5
            the model generator of STEPSS

Input file with model description: simple_avr.txt

MODEL NAME : exc_simple_avr

Processing data...
    prm( 1)=  G                ! gain of exciter
    prm( 2)=  T                ! time constant of the exciter
    prm( 3)=  vfmin            ! lower fielf voltage
    prm( 4)=  vfmax            ! upper field voltage

Processing parameters...
    prm( 5)=  Vo    voltage setpoint of AVR

Processing states...

    Output states
        x( 1)=  vf                field voltage
    Internal states defined by user
        x( 2)=  dv                voltage error

Processing observables...
    Vo
    dv

```

```

vf

Number of user-defined and output d/a states :    2

Processing models...
    & algeq                ! calculation of voltage error
                           1 d/a eqs      2 d/a states    0 disc states
    & tf1plim              ! exciter transfer function
                           2 d/a eqs      2 d/a states    1 disc states

Merging temporary files...
com.tmp
head.tmp
obs.tmp
init.tmp
evalf.tmp
updz.tmp

```

6.5 Mistake detection

CODEGEN performs some “sanity checks” to detect mistakes such as:

- unbalanced braces or brackets
- missing keyword %data, %parameters, %states, %observables or %models
- multiply defined data, states or parameters
- usage of a reserved name for an internal state
- typo leading to an unknown name of state or modelling block
- output variable not appearing in any equation of the model
- number of states different from number of equations (differential or algebraic).

However, not all mistakes are flagged by CODEGEN. Typos or syntax errors may not be detected, leading to error messages by the compiler when the .f90 file is compiled. Some examples are:

- typos in the name of a mathematical function. For instance, “cus([delta])” instead of “cos([delta])”, exponent denoted by ^ instead of **
- forgotten braces { } enclosing the name of a data or a parameter
- forgotten brackets [] enclosing the name of a state.

Chapter 7

Library of modelling blocks

7.1 List of modelling blocks

The list of modelling blocks is given in the table below, together with a brief description.

Table 7.1: List of modelling blocks

abs	Absolute value of input
algeq	Algebraic equation
db	Deadband
f_inj	Estimate of frequency at bus of injector
ftwop_bus1	Estimate of frequency at first bus of two-port
ftwop_bus2	Estimate of frequency at second bus of two-port
fsa	Finite State Automaton
hyst	Hysteresis
int	Integrator with time constant
inlim	Integrator with time constant and non-windup limits on output
invlim	Integrator with time constant and non-windup variable limits on output
lim	Limiter with constant bounds
limvb	Limiter with variable bounds
max1v1c	Maximum between a state and a constant
max2v	Maximum between two states
min1v1c	Minimum between a state and a constant
min2v	Minimum between two states
nint	Integer nearest to the input shifted by a constant
pictl	Proportional-Integral (PI) controller
pictlim	Proportional-Integral (PI) controller with non-windup limit on integral term
pictl2lim	PI controller with non-windup limit on integral term and limit on proportional term
pictlieee	PI controller with non-windup limit on integral term, compliant with IEEE standards
pwlin	Piece-wise linear function of input
switch	Set output to one among n inputs, based on value of a controlling state
swwsign	Switch between two input states, based on sign of a third input state
tf1p	Transfer function between input and output: one time constant
tf1plim	same as tf1p with non-windup limits on output
tf1pvlm	same as tf1p with variable non-windup limits on output
tf1p2lim	same as tf1p with limits on rate of change of output and non-windup limits on output
tfder1p	Transfer function: derivative with one time constant
tf1p1z	Transfer function between input and output: one zero and one pole
tf2p2z	Transfer function between input and output: two real zeros and two real poles
timer	Timer with delay varying piecewise linearly with monitored variable
timersc	Timer with delay varying as a staircase function of monitored variable
tsta	Two-state automaton with transitions based on signs of two inputs

7.2 Information provided for each block

All blocks have input and output states. Their names do not need to be enclosed with brackets¹.

Most (but not all) blocks require parameters. Each of them is either a data (enclosed with braces) or a parameter in the sense defined in the previous chapter (also enclosed with braces) or a mathematical expression involving data and/or parameters.

☛ Here are three examples of information that can be specified for a time constant:

2.

{T}

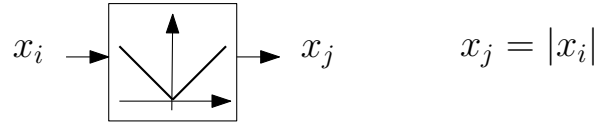
1/{omegac}

7.3 Library

¹since CODEGEN expects to find a state name. Using brackets does not harm though

abs

Absolute value of input.



Syntax : & abs
 name of state x_i
 name of state x_j

Internal states : none

Discrete variable : $z \in \{-1, 1\}$

Equations :

$$0 = \begin{cases} x_j - x_i & \text{if } z = 1 \\ x_j + x_i & \text{if } z = -1 \end{cases}$$

Discrete transitions :

```

if  $z = 1$  then
  if  $x_i < 0$  then
     $z \leftarrow -1$ 
  end if
else
  if  $x_i > 0$  then
     $z \leftarrow 1$ 
  end if
end if

```

Initialization of discrete variables:

```

if  $x_i > 0$  then
   $z \leftarrow 1$ 
else
   $z \leftarrow 0$ 
end if

```


The model having a discontinuous derivative at $x_i = 0$, it is implemented internally with a small hysteresis; see model **hyst** with $x_I = \epsilon, y_{IB} = -\epsilon, y_{IA} = \epsilon, x_D = -\epsilon, y_{DB} = -\epsilon, y_{DA} = \epsilon$, where ϵ is the absolute accuracy used to solve the algebraic equations in RAMSES.

algeq*algebraic equation*

Syntax : & algeq
 math expression

Internal states : none

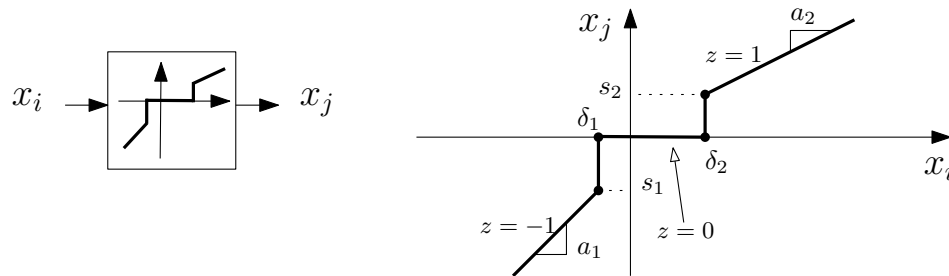
Discrete variables : none

This block forces an algebraic constraint (or equation) involving one of several states :

$$f(x_1, x_2, \dots, x_n) = 0$$

where n is the number of states ($n \geq 1$)

Note that this blocks does not really have “inputs” and “outputs”. The latter stem from the rest of the model involving the algebraic constraint.

db*Deadband.*

Syntax :

& db

name of variable x_i name of variable x_j data name, parameter name or math expression for δ_1 data name, parameter name or math expression for s_1 data name, parameter name or math expression for a_1 data name, parameter name or math expression for δ_2 data name, parameter name or math expression for s_2 data name, parameter name or math expression for a_2

Internal states : none

Discrete variables : $z \in \{0, 1, -1\}$

Equations :

$$x_j = \begin{cases} x_i & \text{if } z = 0 \\ x_i - s_2 - a_2(x_i - \delta_2) & \text{if } z = 1 \\ x_i - s_1 - a_1(x_i - \delta_1) & \text{if } z = -1 \end{cases}$$

Discrete transitions :

```

if  $z \in \{0, 1\}$  then
  if  $x_i < \delta_1$  then
     $z \leftarrow -1$ 
  end if
else if  $z \in \{-1, 0\}$  then
  if  $x_i > \delta_2$  then
     $z \leftarrow 1$ 
  end if
else if  $z \in \{-1, 1\}$  then
  if  $\delta_1 < x_i < \delta_2$  then
     $z \leftarrow 0$ 
  end if
end if

```

Initialization of discrete variables :

```

if  $x_i > \delta_2$  then
   $z \leftarrow 1$ 
else if  $x_i < \delta_1$  then
   $z \leftarrow -1$ 
else
   $z \leftarrow 0$ 
end if

```

The data must obey $\delta_1 < \delta_2$, $a_1 \geq 0$ and $a_2 \geq 0$ (see for instance the diagram above).

A particular case is $s_1 = s_2 = 0$ and $a_1 = a_2 = 1$ (but all values are allowed for these four parameters).

The pwlin4, pwlin5 or pwlin6 block can be used as an alternative to this block.

f_inj

Computes f , an estimate of the frequency (in per unit) at a given bus, from the evolution of the rectangular components v_x and v_y of the bus voltage. A measurement time constant T is involved. Can be used in the model of an injector only.

Syntax : & f_inj
 name of variable f
 data name, parameter name or math expression for T

Internal states : v_{xm} and v_{ym} .

Discrete variables : none

Equations :

$$\dot{v}_{xm} = \frac{v_x - v_{xm}}{T} \quad (7.1)$$

$$\dot{v}_{ym} = \frac{v_y - v_{ym}}{T} \quad (7.2)$$

$$0 = \omega_{ref,pu} + \frac{(v_y - v_{ym})v_{xm} - (v_x - v_{xm})v_{ym}}{2\pi f_N T (v_{xm}^2 + v_{ym}^2)} - f \quad (7.3)$$

Initialization of internal states : $v_{xm} = v_x$ and $v_{ym} = v_y$.

Explanation of model

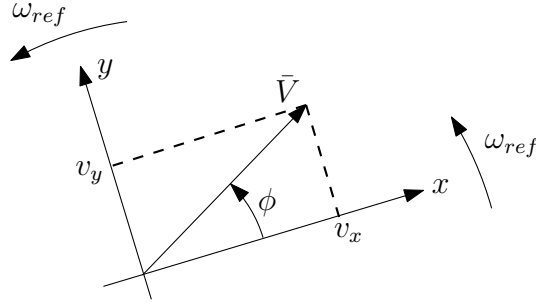
The model uses v_x and v_y as inputs but these variables are automatically inherited and must not be declared. Only the name given to the estimated frequency and the time constant T must be provided.

As shown in the figure below, v_x and v_y are the projections of the bus voltage phasor on the references axes x and y rotating at the angular speed ω_{ref} (rad/s). The latter is known from the settings of the simulation. The angular frequency of the corresponding rotating vector is given by :

$$\omega = \omega_{ref} + \frac{d\phi}{dt}$$

with:

$$\phi = \arctan \frac{v_y}{v_x}$$



The frequency in per unit is given by :

$$f = \frac{\omega}{2\pi f_N} = \frac{\omega_{ref}}{2\pi f_N} + \frac{1}{2\pi f_N} \frac{d\phi}{dt} = \omega_{ref,pu} + \frac{1}{2\pi f_N} \frac{d}{dt} \left(\arctan \frac{v_y}{v_x} \right)$$

where f_N is the nominal frequency (known from the system data).

By developing the last term, it is easily found that:

$$f = \omega_{ref,pu} + \frac{1}{2\pi f_N} \frac{\dot{v}_y v_x - v_x \dot{v}_y}{v_x^2 + v_y^2} \quad (7.4)$$

To filter the transients affecting v_x and v_y , a measurement device with a time constant T is simulated. The “measured” values, denoted v_{xm} and v_{ym} , evolve according to (7.1, 7.2). These measured values and their derivatives are then used in (7.4), which becomes:

$$f = \omega_{ref,pu} + \frac{1}{2\pi f_N} \frac{\dot{v}_{ym} v_{xm} - v_{xm} \dot{v}_{ym}}{v_{xm}^2 + v_{ym}^2}$$

Replacing \dot{v}_{xm} and \dot{v}_{ym} by their expressions (7.1,7.2) yields Eq. (7.3).

A recommended value for T is in the order to 0.05 – 0.10 s. A zero value for T is not allowed. If too small a value is specified for T , the solver may encounter a singularity and the simulation may not proceed.

f_twop_bus1

Similar to f_inj, computes f , an estimate of the frequency (in per unit) at the first bus of a given two-port. Can be used in the model of a two-port only.

Syntax : & f_twop_bus1
 name of variable f
 data name, parameter name or math expression for T

Please refer to f_inj.

f_twop_bus2

Similar to f_inj, computes f , an estimate of the frequency (in per unit) at the second bus of a given two-port. Can be used in the model of a two-port only.

Syntax : & f_twop_bus2
 name of variable f
 data name, parameter name or math expression for T

Please refer to f_inj.

fsa*Finite State Automaton*

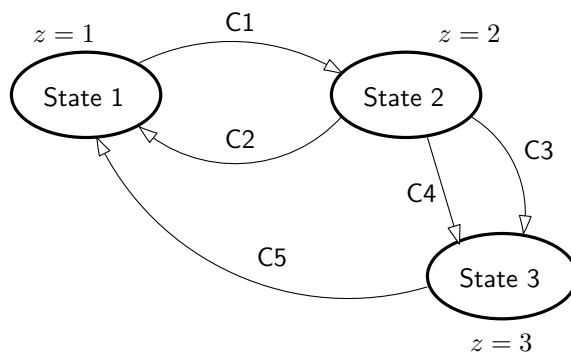
This block forces a set of n algebraic equations. There are s possible sets, each of them corresponding to a value of the discrete state z . The change from one set to another takes place when boolean expressions are true.

Syntax : see example below

Internal states : none

Discrete variables: z , the number of the state currently active

Example. Consider the example below with three states ($s = 3$). $n = 2$ is assumed.



```

& fsa
initial state of the system
# 1
algebraic constraint No. 1
algebraic constraint No. 2
-> 2
boolean expression C1
# 2
algebraic constraint No. 3
algebraic constraint No. 4
-> 1
boolean expression C2
-> 3
boolean expression C3
-> 3
boolean expression C4
# 3
algebraic constraint No. 5
algebraic constraint No. 6
-> 1
boolean expression C5
##
  
```

The # symbol indicates the start of the section relative to a state. It is followed by the number of the state. The states must be numbered consecutively from 1 to s , and they must be listed by

increasing order. The ## symbol indicates the end of the list of states.

The initial state is specified as an integer in the second line.

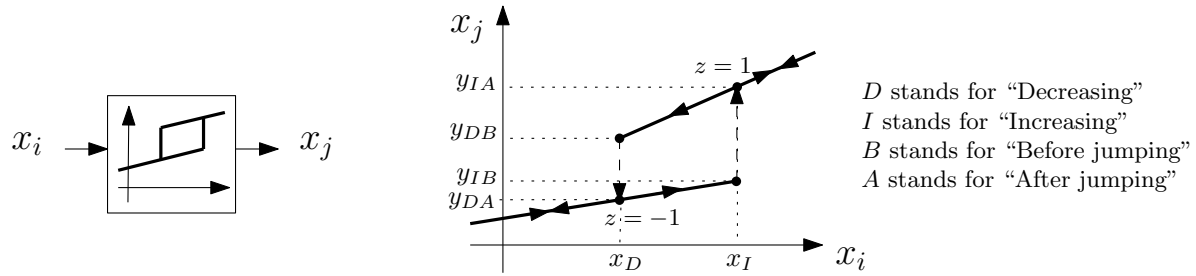
The number n of algebraic constraints must be the same in all states.

The \rightarrow symbol indicates a transition. It is followed by the number of the state reached after the transition has taken place. The next line is the corresponding boolean expression, involving states and possibly parameters.

In the example above, there are two possible transitions from State 2 to State 3. Alternatively a single transition can be specified with the combined condition "C3 or C4".

hyst

Hysteresis



Syntax :

& hyst

name of variable x_i

name of variable x_j

data name, parameter name or math expression for x_I

data name, parameter name or math expression for y_{IB}

data name, parameter name or math expression for y_{IA}

data name, parameter name or math expression for x_D

data name, parameter name or math expression for y_{DB}

data name, parameter name or math expression for y_{DA}

data name, parameter name or math expression for z_0

Internal states : none

Discrete variables : $z \in \{-1, 1\}$

Equations :

$$0 = \begin{cases} x_j - y_{IA} - \frac{y_{IA} - y_{DB}}{x_I - x_D}(x_i - x_I) & \text{if } z = 1 \\ x_j - y_{DA} - \frac{y_{IB} - y_{DA}}{x_I - x_D}(x_i - x_D) & \text{if } z = -1 \end{cases}$$

Discrete transitions :

```

if  $z = -1$  then
  if  $x_i > x_I$  then
     $z \leftarrow 1$ 
  end if
else
  if  $x_i < x_D$  then
     $z \leftarrow -1$ 
  end if
end if

```

Initialization of discrete variables :

```

if  $x_i > x_I$  then
   $z \leftarrow 1$ 
else if  $x_i < x_D$  then
   $z \leftarrow -1$ 
else
  if  $z_0 \geq 0$  then
     $z \leftarrow 1$ 
  else
     $z \leftarrow 0$ 
  end if
end if

```

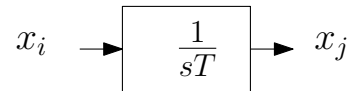
At $t = 0$, if $x_D < x_i(0) < x_I$ the initial state of the system is indeterminate, since it could operate on the (y_{IA}, y_{DB}) line (i.e. with an initial value of z equal to 1) as well as on the (y_{DA}, y_{IB}) line (i.e. with an initial value of z equal to -1). Hence, the user must specify z_0 , the initial value of z .

If $x_i(0) < x_D$ (resp. $x_i(0) > x_I$) the initial value is $z = -1$ (resp. $z = 1$) and z_0 is not used.

The data must obey $x_D < x_I$, otherwise the model would not correspond to hysteresis. The case $x_D = x_I$ is not allowed either, but it can be handled with the **pwlin4** model.

int

Integrator with (positive) time constant T



Syntax : & int
 name of variable x_i
 name of variable x_j
 data name, parameter name or math expression for T

Internal states : none

Discrete variables : none

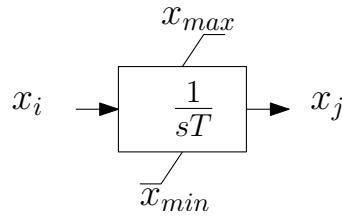
Equations :

$$T\dot{x}_j = x_i \tag{7.5}$$

A zero value for T is not allowed. If too small a value is specified for T , the solver may encounter a singularity and the simulation may not proceed.

inlim

Integrator with (positive) time constant T and non-windup limits on output



Syntax : & inlim
 name of variable x_i
 name of variable x_j
 data name, parameter name or math expression for T
 data name, parameter name or math expression for x_{min}
 data name, parameter name or math expression for x_{max}

Internal states : none

Discrete variables : $z \in \{0, 1, -1\}$

Equations :

$$\begin{aligned}
 T\dot{x}_j &= x_i && \text{if } z = 0 \\
 0 &= x_j - x_{min} && \text{if } z = -1 \\
 0 &= x_j - x_{max} && \text{if } z = 1
 \end{aligned} \tag{7.6}$$

Discrete transitions :

```

if  $z = 0$  then
  if  $x_j > x_{max}$  then
     $z \leftarrow 1$ 
  else if  $x_j < x_{min}$  then
     $z \leftarrow -1$ 
  end if
else if  $z = 1$  then
  if  $x_i < 0$  then
     $z \leftarrow 0$ 
  end if
else if  $z = -1$  then
  if  $x_i > 0$  then
     $z \leftarrow 0$ 
  end if
end if

```

Initialization of discrete variables :

```

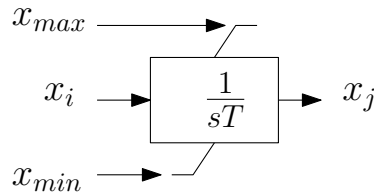
if  $x_j > x_{max}$  then
   $z \leftarrow 1$ 
else if  $x_j < x_{min}$  then
   $z \leftarrow -1$ 
else
   $z \leftarrow 0$ 
end if

```

A zero value for T is not allowed. If too small a value is specified for T , the solver may encounter a singularity and the simulation may not proceed.

invlim

Integrator with (positive) time constant T and non-windup limits on output. The lower and upper limits are variables.



Syntax : & invlim
 name of variable x_i
 name of variable x_{min}
 name of variable x_{max}
 name of variable x_j
 data name, parameter name or math expression for T

Internal states : none

Discrete variables : $z \in \{0, 1, -1\}$

Equations :

$$\begin{aligned}
 T\dot{x}_j &= x_i && \text{if } z = 0 \\
 0 &= x_j - x_{min} && \text{if } z = -1 \\
 0 &= x_j - x_{max} && \text{if } z = 1
 \end{aligned}
 \tag{7.7}$$

Discrete transitions :

```

if  $z = 0$  then
  if  $x_j > x_{max}$  then
     $z \leftarrow 1$ 
  else if  $x_j < x_{min}$  then
     $z \leftarrow -1$ 
  end if
else if  $z = 1$  then
  if  $x_i < 0$  then
     $z \leftarrow 0$ 
  end if
else if  $z = -1$  then
  if  $x_i > 0$  then
     $z \leftarrow 0$ 
  end if
end if

```

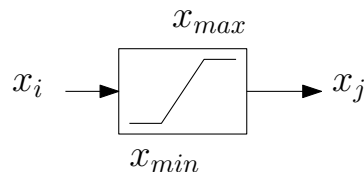
Initialization of discrete variables :

```

if  $x_j > x_{max}$  then
   $z \leftarrow 1$ 
else if  $x_j < x_{min}$  then
   $z \leftarrow -1$ 
else
   $z \leftarrow 0$ 
end if

```

A zero value for T is not allowed. If too small a value is specified for T , the solver may encounter a singularity and the simulation may not proceed.

lim*Limiter with constant bounds*

Syntax :

- & lim
- name of variable x_i
- name of variable x_j
- data name, parameter name or math expression for x_{min}
- data name, parameter name or math expression for x_{max}

Internal states : none

Discrete variables : $z \in \{-1, 0, 1\}$

Equations :

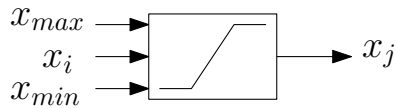
$$0 = \begin{cases} x_j - x_i & \text{if } z = 0 \\ x_j - x_{max} & \text{if } z = 1 \\ x_j - x_{min} & \text{if } z = -1 \end{cases}$$

Discrete transitions :

```
if  $z = 0$  then  
  if  $x_i > x_{max}$  then  
     $z \leftarrow 1$   
  else if  $x_i < x_{min}$  then  
     $z \leftarrow -1$   
  end if  
else if  $z = 1$  then  
  if  $x_i < x_{max}$  then  
     $z \leftarrow 0$   
  end if  
else if  $z = -1$  then  
  if  $x_i > x_{min}$  then  
     $z \leftarrow 0$   
  end if  
end if
```

Initialization of discrete variables :

```
if  $x_j > x_{max}$  then  
   $z \leftarrow 1$   
else if  $x_j < x_{min}$  then  
   $z \leftarrow -1$   
else  
   $z \leftarrow 0$   
end if
```

limvb*Limiter with variable bounds*

Syntax :

- & limvb
- name of variable x_i
- name of variable x_{min}
- name of variable x_{max}
- name of variable x_j

Internal states : none

Discrete variables : $z \in \{-1, 0, 1\}$

Equations :

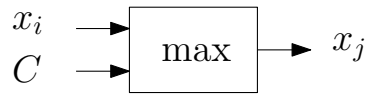
$$0 = \begin{cases} x_j - x_i & \text{if } z = 0 \\ x_j - x_{max} & \text{if } z = 1 \\ x_j - x_{min} & \text{if } z = -1 \end{cases}$$

Discrete transitions :

```
if  $z = 0$  then  
  if  $x_i > x_{max}$  then  
     $z \leftarrow 1$   
  else if  $x_i < x_{min}$  then  
     $z \leftarrow -1$   
  end if  
else if  $z = 1$  then  
  if  $x_i < x_{max}$  then  
     $z \leftarrow 0$   
  end if  
else if  $z = -1$  then  
  if  $x_i > x_{min}$  then  
     $z \leftarrow 0$   
  end if  
end if
```

Initialization of discrete variables :

```
if  $x_i > x_{max}$  then  
   $z \leftarrow 1$   
else if  $x_i < x_{min}$  then  
   $z \leftarrow -1$   
else  
   $z \leftarrow 0$   
end if
```

max1v1c*Maximum between a state and a constant*

Syntax : & max1v1c
 name of variable x_i
 name of variable x_j
 data name, parameter name or math expression for C

Internal states : none

Discrete variables : $z \in \{1, 2\}$

Equations :

$$0 = \begin{cases} x_j - C & \text{if } z = 1 \\ x_j - x_i & \text{if } z = 2 \end{cases}$$

Discrete transitions :

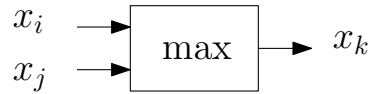
```

if  $z = 1$  then
  if  $x_i > C$  then
     $z \leftarrow 2$ 
  end if
else if  $z = 2$  then
  if  $x_i \leq C$  then
     $z \leftarrow 1$ 
  end if
end if

```

Initialization of discrete variables :

```
if  $x_i < C$  then  
   $z \leftarrow 1$   
else  
   $z \leftarrow 2$   
end if
```

max2v*Maximum between two states*

Syntax : & max2v
 name of variable x_i
 name of variable x_j
 name of variable x_k

Internal states : none

Discrete variables : $z \in \{1, 2\}$

Equations :

$$0 = \begin{cases} x_i - x_k & \text{if } z = 1 \\ x_j - x_k & \text{if } z = 2 \end{cases}$$

Discrete transitions :

```

if  $z = 1$  then
  if  $x_i < x_j$  then
     $z \leftarrow 2$ 
  end if
else if  $z = 2$  then
  if  $x_j \leq x_i$  then
     $z \leftarrow 1$ 
  end if
end if

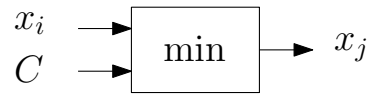
```

Initialization of discrete variables :

```

if  $x_i > x_j$  then
   $z \leftarrow 1$ 
else
   $z \leftarrow 2$ 
end if

```


min1v1c*Minimum between a state and a constant*

Syntax : & min1v1c
 name of variable x_i
 name of variable x_j
 data name, parameter name or math expression for C

Internal states : none

Discrete variables : $z \in \{1, 2\}$

Equations :

$$0 = \begin{cases} x_j - x_i & \text{if } z = 1 \\ x_j - C & \text{if } z = 2 \end{cases}$$

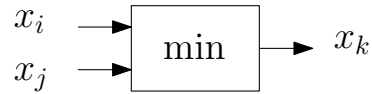
Discrete transitions :

```

if  $z = 1$  then
  if  $x_i > C$  then
     $z \leftarrow 2$ 
  end if
else if  $z = 2$  then
  if  $x_i \leq C$  then
     $z \leftarrow 1$ 
  end if
end if
  
```

Initialization of discrete variables :

```
if  $x_i < C$  then  
   $z \leftarrow 1$   
else  
   $z \leftarrow 2$   
end if
```

min2v*Minimum between two states*

Syntax : & min2v
 name of variable x_i
 name of variable x_j
 name of variable x_k

Internal states : none

Discrete variables : $z \in \{1, 2\}$

Equations :

$$0 = \begin{cases} x_i - x_k & \text{if } z = 1 \\ x_j - x_k & \text{if } z = 2 \end{cases}$$

Discrete transitions :

```

if  $z = 1$  then
  if  $x_i > x_j$  then
     $z \leftarrow 2$ 
  end if
else if  $z = 2$  then
  if  $x_j \geq x_i$  then
     $z \leftarrow 1$ 
  end if
end if
  
```

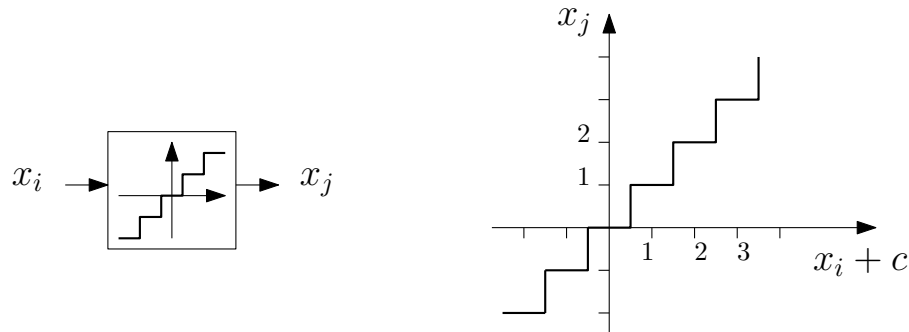
Initialization of discrete variables :

```

if  $x_i < x_j$  then
   $z \leftarrow 1$ 
else
   $z \leftarrow 2$ 
end if
  
```

nint

Integer nearest to the input shifted by a constant c .



Syntax : & nint
 name of variable x_i
 name of variable x_j
 data name, parameter name or math expression for c

Internal states : none

Discrete variables : $z \in \mathcal{I}$

Equations :

$$0 = x_j - z$$

Discrete transitions :

```

if nint( $x_i + c$ )  $\neq z$  then
   $z \leftarrow$  nint( $x_i + c$ )
end if

```

where the nint function returns the nearest integer.

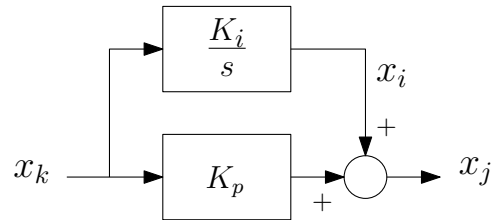
Particular cases:

- with $c = 0$, the output is the integer nearest to x_i ;
- with $c = -0.5$, the output is the “floor” integer of x_i , i.e. the largest integer smaller or equal to x_i ;

- with $c = 0.5$, the output is the “ceiling” integer of x_i , i.e. the smallest integer larger or equal to x_i .

Initialization of discrete variables :

$$z \leftarrow \text{nint}(x_i + c)$$

pictl*Proportional-Integral (PI) controller*

Syntax : & pictl
 name of variable x_k
 name of variable x_j
 data name, parameter name or math expression for K_i
 data name, parameter name or math expression for K_p

Internal states : x_i

Discrete variables: none

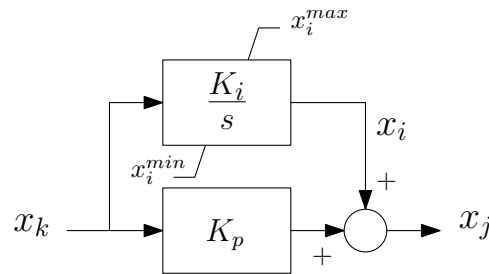
Equations :

$$\begin{aligned} \dot{x}_i &= K_i x_k \\ 0 &= K_p x_k + x_i - x_j \end{aligned}$$

Initialization of internal states: $x_i = x_j$

pictllim

Proportional-Integral (PI) controller with non-windup limit on the integral term.



Syntax :

- & pictllim
- name of variable x_k
- name of variable x_j
- data name, parameter name or math expression for K_i
- data name, parameter name or math expression for K_p
- data name, parameter name or math expression for x_i^{min}
- data name, parameter name or math expression for x_i^{max}

Internal states: x_i

Discrete variables : $z \in \{-1, 0, 1\}$

Equations :

$$\begin{cases} \dot{x}_i &= K_i x_k & \text{if } z = 0 \\ 0 &= x_i - x_i^{min} & \text{if } z = -1 \\ 0 &= x_i - x_i^{max} & \text{if } z = 1 \end{cases}$$

$$0 = K_p x_k + x_i - x_j$$

Discrete transitions :

```

if  $z = 0$  then
  if  $x_i > x_i^{max}$  then
     $z \leftarrow 1$ 
  else if  $x_i < x_i^{min}$  then
     $z \leftarrow -1$ 
  end if
else if  $z = 1$  then
  if  $K_i x_k < 0$  then
     $z \leftarrow 0$ 
  end if
else if  $z = -1$  then
  if  $K_i x_k > 0$  then
     $z \leftarrow 0$ 
  end if
end if

```

Initialization of the internal state and the discrete variable:

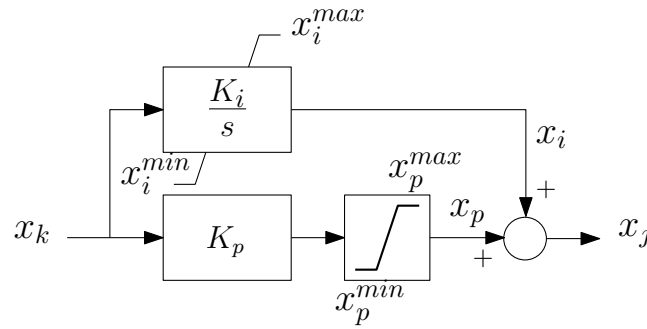
```

if  $K_i x_k > 0$  then
   $z \leftarrow 1$ 
   $x_i \leftarrow x_i^{max}$ 
else if  $K_i x_k < 0$  then
   $z \leftarrow -1$ 
   $x_i \leftarrow x_i^{min}$ 
else
   $z \leftarrow 0$ 
   $x_i \leftarrow x_j$ 
end if

```


pictl2lim

Proportional-Integral (PI) controller with non-windup limit on the integral term and limit on the proportional term.



Syntax :

- & pictl2lim
- name of variable x_k
- name of variable x_j
- data name, parameter name or math expression for K_i
- data name, parameter name or math expression for K_p
- data name, parameter name or math expression for x_i^{min}
- data name, parameter name or math expression for x_i^{max}
- data name, parameter name or math expression for x_p^{min}
- data name, parameter name or math expression for x_p^{max}

Internal states : x_i and x_p

Discrete variables : $z_1 \in \{-1, 0, 1\}$ and $z_2 \in \{-1, 0, 1\}$

Equations :

$$\begin{cases} 0 &= K_p x_k - x_p & \text{if } z_1 = 0 \\ 0 &= x_p - x_p^{min} & \text{if } z_1 = -1 \\ 0 &= x_p - x_p^{max} & \text{if } z_1 = 1 \end{cases}$$

$$\begin{cases} \dot{x}_i &= K_i x_k & \text{if } z_2 = 0 \\ 0 &= x_i - x_i^{min} & \text{if } z_2 = -1 \\ 0 &= x_i - x_i^{max} & \text{if } z_2 = 1 \end{cases}$$

$$0 = x_p + x_i - x_j$$

```

if  $z_1 = 0$  then
  if  $x_p > x_p^{max}$  then
     $z_1 \leftarrow 1$ 
  else if  $x_p < x_p^{min}$  then
     $z_1 \leftarrow -1$ 
  end if
else if  $z_1 = 1$  then
  if  $K_p x_k < x_p^{max}$  then
     $z_1 \leftarrow 0$ 
  end if
else if  $z_1 = -1$  then
  if  $K_p x_k > x_p^{min}$  then
     $z_1 \leftarrow 0$ 
  end if
end if
if  $z_2 = 0$  then
  if  $x_i > x_i^{max}$  then
     $z_2 \leftarrow 1$ 
  else if  $x_i < x_i^{min}$  then
     $z_2 \leftarrow -1$ 
  end if
else if  $z_2 = 1$  then
  if  $K_i x_k < 0$  then
     $z_2 \leftarrow 0$ 
  end if
else if  $z_2 = -1$  then
  if  $K_i x_k > 0$  then
     $z_2 \leftarrow 0$ 
  end if
end if

```

Initialization of the internal state x_p : $x_p = \min(x_p^{max}, \max(x_p^{min}, K_p x_k))$

Initialization of internal state x_i and the discrete variables:

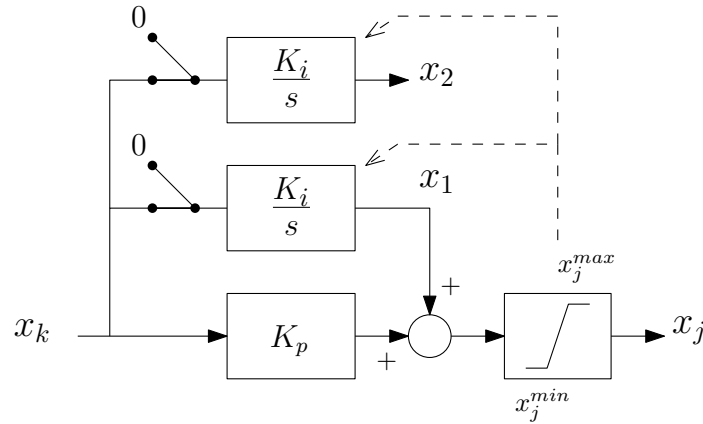
```

if  $K_p x_k > x_p^{max}$  then
   $z_1 \leftarrow 1$ 
else if  $K_p x_k < x_p^{min}$  then
   $z_1 \leftarrow -1$ 
else
   $z_1 \leftarrow 0$ 
end if
if  $K_i x_k > 0$  then
   $z_2 \leftarrow 1$ 
   $x_i \leftarrow x_i^{max}$ 
else if  $K_i x_k < 0$  then
   $z_2 \leftarrow -1$ 
   $x_i \leftarrow x_i^{min}$ 
else
   $z_2 \leftarrow 0$ 
   $x_i \leftarrow x_j - x_p$ 
end if

```

pictlieee

Proportional-Integral (PI) controller with non-windup limit on the integral term, compliant with IEEE standards.



This PI controller involves a limiter and a non-windup integrator compliant with the IEEE specifications in:

- IEEE recommended practice for excitation system models for power system stability studies, IEEE Std 421.5-1992
- IEEE recommended practice for excitation system models for power system stability studies, IEEE Std 421.5-2005 (Revision of IEEE Std 421.5-1992)
- IEEE recommended practice for excitation system models for power system stability studies, IEEE Std 421.5-2016 (Revision of IEEE Std 421.5-2005)

The IEEE standard specifies that the x_1 variable is frozen as soon as x_j reaches its (lower or upper) limit. This is done by merely setting the input of the integrator to zero.

However, the standard does not specify the condition under which x_1 is let to vary again, i.e. when the integrator is put back into service. A simple way would be to re-activate the integrator as soon as x_j gets back within its limits. However, at that time instant, the x_k variable may have a value such that $x_j = K_p x_k + x_1$ is pushed again to its (lower or upper) limit. The system would then be trapped into a limit cycle (which would not match the behaviour of the system to model !).

With the implementation shown in the above block diagram, the limit cycle is avoided by relying on the upper integrator to decide when the lower integrator can be released. The upper integrator is used to observe what the evolution of the system would be with x_1 free to vary: the lower integrator is re-activated only when $K_p x_k + x_2$ is in $[x_j^{\min}, x_j^{\max}]$. As it is in “open loop”, the additional integrator does not interact with the rest of the system.

Syntax : & pictlieee
 name of variable x_k
 name of variable x_j
 data name, parameter name or math expression for K_i
 data name, parameter name or math expression for K_p
 data name, parameter name or math expression for x_j^{min}
 data name, parameter name or math expression for x_j^{max}

Internal states: x_1 and x_2

Discrete variables : $z \in \{-2, -1, 0, 1, 2\}$

Equations :

$$\text{if } z = 0 : \begin{cases} 0 &= K_p x_k + x_1 - x_j \\ \dot{x}_1 &= K_i x_k \\ 0 &= x_2 - x_1 \end{cases}$$

$$\text{if } z = 2 : \begin{cases} 0 &= x_j^{max} - x_j \\ \dot{x}_1 &= 0 \\ 0 &= x_2 - x_1 \end{cases} \quad \text{if } z = 1 : \begin{cases} 0 &= x_j^{max} - x_j \\ \dot{x}_1 &= 0 \\ \dot{x}_2 &= K_i x_k \end{cases}$$

$$\text{if } z = -2 : \begin{cases} 0 &= x_j^{min} - x_j \\ \dot{x}_1 &= 0 \\ 0 &= x_2 - x_1 \end{cases} \quad \text{if } z = -1 : \begin{cases} 0 &= x_j^{min} - x_j \\ \dot{x}_1 &= 0 \\ \dot{x}_2 &= K_i x_k \end{cases}$$

Discrete transitions (note the use of x_2 in the tests marked with (*)):

```

if  $z = 0$  then
  if  $x_j > x_j^{max}$  then
     $z \leftarrow 2$ 
  else if  $x_j < x_j^{min}$  then
     $z \leftarrow -2$ 
  end if
else if  $z = 2$  then
  if  $K_p x_k + x_1 < x_j^{max}$  then
     $z \leftarrow 1$ 
  end if
else if  $z = 1$  then
  if  $K_p x_k + x_1 > x_j^{max}$  then
     $z \leftarrow 2$ 
  else if  $K_p x_k + x_2 < x_j^{max}$  (*) then
     $z \leftarrow 0$ 
  end if
else if  $z = -2$  then
  if  $K_p x_k + x_1 > x_j^{min}$  then
     $z \leftarrow -1$ 
  end if
else if  $z = -1$  then
  if  $K_p x_k + x_1 < x_j^{min}$  then
     $z \leftarrow -2$ 
  else if  $K_p x_k + x_2 > x_j^{min}$  (*) then
     $z \leftarrow 0$ 
  end if
end if

```

Initialization of the internal state and the discrete variable:

```

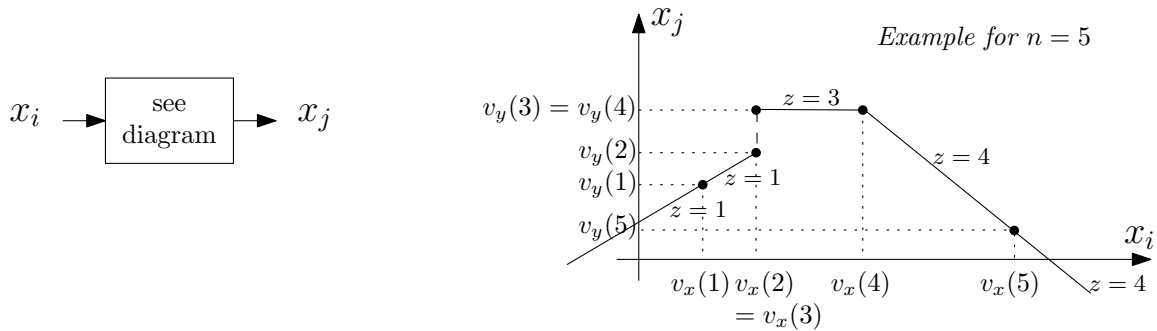
if  $x_j \geq x_j^{max}$  then
   $z \leftarrow 2$ 
   $x_1 \leftarrow x_j^{max} - K_p x_k$ 
   $x_2 \leftarrow x_1$ 
else if  $x_j \leq x_j^{min}$  then
   $z \leftarrow -2$ 
   $x_1 \leftarrow x_j^{min} - K_p x_k$ 
   $x_2 \leftarrow x_1$ 
else
   $z \leftarrow 0$ 
   $x_1 \leftarrow x_j$ 
   $x_2 \leftarrow x_1$ 
end if

```

pwlin*

Piece-wise linear function of input, defined by n points.

Separate blocks exist for $n = 3, 4, 5$ and 6.



Syntax :

& pwlin3

name of variable x_i

name of variable x_j

data name, parameter name or math expression for $v_x(1)$

data name, parameter name or math expression for $v_y(1)$

data name, parameter name or math expression for $v_x(2)$

data name, parameter name or math expression for $v_y(2)$

data name, parameter name or math expression for $v_x(3)$

data name, parameter name or math expression for $v_y(3)$

& pwlin4

name of variable x_i

name of variable x_j

data name, parameter name or math expression for $v_x(1)$

data name, parameter name or math expression for $v_y(1)$

data name, parameter name or math expression for $v_x(2)$

data name, parameter name or math expression for $v_y(2)$

data name, parameter name or math expression for $v_x(3)$

data name, parameter name or math expression for $v_y(3)$

data name, parameter name or math expression for $v_x(4)$

data name, parameter name or math expression for $v_y(4)$

& pwlin5

name of variable x_i

name of variable x_j

data name, parameter name or math expression for $v_x(1)$

data name, parameter name or math expression for $v_y(1)$

data name, parameter name or math expression for $v_x(2)$

data name, parameter name or math expression for $v_y(2)$

data name, parameter name or math expression for $v_x(3)$

data name, parameter name or math expression for $v_y(3)$

data name, parameter name or math expression for $v_x(4)$

data name, parameter name or math expression for $v_y(4)$

data name, parameter name or math expression for $v_x(5)$

data name, parameter name or math expression for $v_y(5)$

& pwlin6

name of variable x_i

name of variable x_j

data name, parameter name or math expression for $v_x(1)$

data name, parameter name or math expression for $v_y(1)$

data name, parameter name or math expression for $v_x(2)$

data name, parameter name or math expression for $v_y(2)$

data name, parameter name or math expression for $v_x(3)$

data name, parameter name or math expression for $v_y(3)$

data name, parameter name or math expression for $v_x(4)$

data name, parameter name or math expression for $v_y(4)$

data name, parameter name or math expression for $v_x(5)$

data name, parameter name or math expression for $v_y(5)$

data name, parameter name or math expression for $v_x(6)$

data name, parameter name or math expression for $v_y(6)$

Internal states : none

Discrete variables : $z \in \{1, \dots, n-1\}$

Equations :

$$0 = v_y(z) + \frac{v_y(z+1) - v_y(z)}{v_x(z+1) - v_x(z)} (x_i - v_x(z)) - x_j$$

Discrete transitions :

```

if  $x_i < v_x(1)$  then
   $z \leftarrow 1$ 
else if  $x_i \geq v_x(n)$  then
   $z \leftarrow n - 1$ 
else
  for  $k = 1$  to  $n - 1$  do
    if  $v_x(k) \leq x_i$  and  $x_i < v_x(k + 1)$  then
       $z \leftarrow k$ 
    end if
  end for
end if

```

Initialization of discrete variables : same code as for the discrete transitions

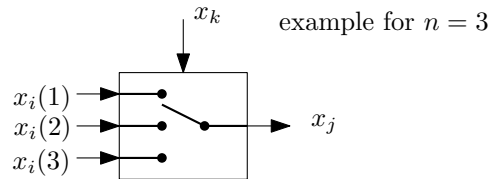
The v_x values must be increasing, i.e. $v_x(1) < v_x(2) \leq v_x(3) \leq \dots \leq v_x(n-1) < v_x(n)$.

For x_i values smaller than $v_x(1)$ (resp. larger than $v_x(n)$), x_j is obtained by linear extrapolation based on the first two (resp. the last two) points. Hence, the data must be such that $v_x(1) \neq v_x(2)$ and $v_x(n-1) \neq v_x(n)$.

switch*

Set the output state to one among n input states, based on the value of a controlling state.

Separate blocks exist for $n = 2, 3, 4$ and 5 .



Syntax :

& switch2

name of variable $x_i(1)$
 name of variable $x_i(2)$
 name of variable x_k
 name of variable x_j

& switch3

name of variable $x_i(1)$
 name of variable $x_i(2)$
 name of variable $x_i(3)$
 name of variable x_k
 name of variable x_j

& switch4

name of variable $x_i(1)$
 name of variable $x_i(2)$
 name of variable $x_i(3)$
 name of variable $x_i(4)$
 name of variable x_k
 name of variable x_j

& switch5

name of variable $x_i(1)$
 name of variable $x_i(2)$
 name of variable $x_i(3)$
 name of variable $x_i(4)$
 name of variable $x_i(5)$
 name of variable x_k
 name of variable x_j

Internal states : none

Discrete variables : $z \in \{1, 2, \dots, n\}$

Equations :

$$0 = x_j - x_i(z)$$

Discrete transitions :

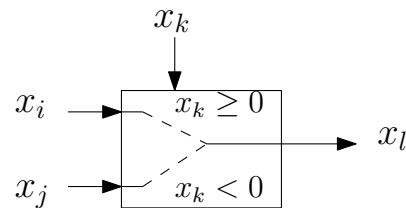
$$z \leftarrow \max(1, \min(n, \text{nint}(x_k)))$$

where the `nint` function returns the nearest integer.

Initialization of discrete variables : same code as for the discrete transitions

swsign

Switch between two input states, based on the sign of a third input state



Syntax : & swsign
 name of variable x_i
 name of variable x_j
 name of variable x_k
 name of variable x_l

Internal states : none

Discrete variables : $z \in \{1, 2\}$

Equations :

$$0 = \begin{cases} x_l - x_i & \text{if } z = 1 \\ x_l - x_j & \text{if } z = 2 \end{cases}$$

Discrete transitions :

```

if  $z = 1$  then
  if  $x_k < 0$  then
     $z \leftarrow 2$ 
  end if
else if  $z = 2$  then
  if  $x_k \geq 0$  then
     $z \leftarrow 1$ 
  end if
end if

```

Initialization of discrete variables :

if $x_k < 0$ **then**

$z \leftarrow 2$

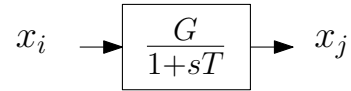
else

$z \leftarrow 1$

end if

tf1p

Transfer function between input and output: one time constant



Syntax : & tf1p
 name of variable x_i
 name of variable x_j
 data name, parameter name or math expression for G
 data name, parameter name or math expression for T

Internal states : none

Discrete variables : none

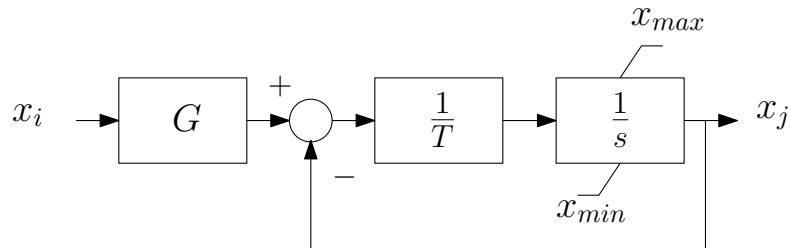
Equations :

$$T \dot{x}_j = -x_j + G x_i$$

The time constant T can be zero.

tf1plim

Transfer function between input and output: one time constant with non-windup limits on output.



Syntax :

& tf1plim

name of variable x_i

name of variable x_j

data name, parameter name or math expression for G

data name, parameter name or math expression for T

data name, parameter name or math expression for x_{min}

data name, parameter name or math expression for x_{max}

Internal states : none

Discrete variables : $z \in \{-1, 0, 1\}$

Equations :

$$\begin{cases} T \dot{x}_j = G x_i - x_j & \text{if } z = 0 \\ 0 = x_j - x_{max} & \text{if } z = 1 \\ 0 = x_j - x_{min} & \text{if } z = -1 \end{cases}$$

Discrete transitions :

```

if  $z = 0$  then
  if  $x_j > x_{max}$  then
     $z \leftarrow 1$ 
  else if  $x_j < x_{min}$  then
     $z \leftarrow -1$ 
  end if
else if  $z = 1$  then
  if  $G x_i - x_j < 0$  then
     $z \leftarrow 0$ 
  end if
else if  $z = -1$  then
  if  $G x_i - x_j > 0$  then
     $z \leftarrow 0$ 
  end if
end if

```

The time constant T can be zero. In this case:

- the block behaves like a gain: $x_j = Gx_i$
- the limits x_{min} and x_{max} remain in effect.

Initialization of discrete variables :

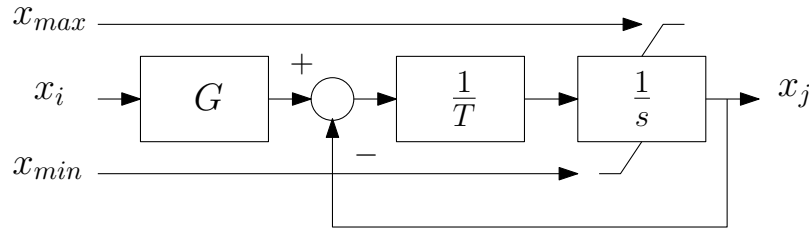
```

if  $x_j \geq x_{max}$  then
   $z \leftarrow 1$ 
else if  $x_j \leq x_{min}$  then
   $z \leftarrow -1$ 
else
   $z \leftarrow 0$ 
end if

```

tf1pvlm

Transfer function between input and output: one time constant with non-windup limits on output. The limits are variables.



Syntax : & tf1plim
 name of variable x_i
 name of variable x_j
 name of variable x_{min}
 name of variable x_{max}
 data name, parameter name or math expression for G
 data name, parameter name or math expression for T

Internal states : none

Discrete variables : $z \in \{-1, 0, 1\}$

Equations :

$$\begin{cases} T \dot{x}_j = G x_i - x_j & \text{if } z = 0 \\ 0 = x_j - x_{max} & \text{if } z = 1 \\ 0 = x_j - x_{min} & \text{if } z = -1 \end{cases}$$

Discrete transitions :

```

if  $z = 0$  then
  if  $x_j > x_{max}$  then
     $z \leftarrow 1$ 
  else if  $x_j < x_{min}$  then
     $z \leftarrow -1$ 
  end if
else if  $z = 1$  then
  if  $G x_i - x_j < 0$  then
     $z \leftarrow 0$ 
  end if
else if  $z = -1$  then
  if  $G x_i - x_j > 0$  then
     $z \leftarrow 0$ 
  end if
end if

```

The time constant T can be zero. In this case:

- the block behaves like a gain: $x_j = Gx_i$
- the limits x_{min} and x_{max} remain in effect.

Initialization of discrete variables :

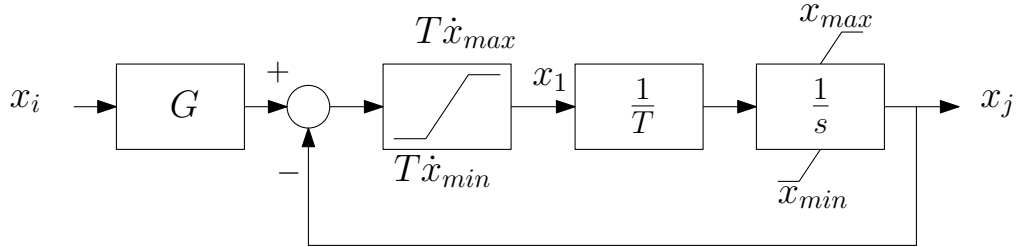
```

if  $x_j \geq x_{max}$  then
   $z \leftarrow 1$ 
else if  $x_j \leq x_{min}$  then
   $z \leftarrow -1$ 
else
   $z \leftarrow 0$ 
end if

```

tf1p2lim

Transfer function between input and output: one time constant, with limits on rate of change of output and non-windup limits on output



Syntax :

& tf1p2lim

name of variable x_i

name of variable x_j

data name, parameter name or math expression for G

data name, parameter name or math expression for T

data name, parameter name or math expression for x_{min}

data name, parameter name or math expression for x_{max}

data name, parameter name or math expression for \dot{x}_{min}

data name, parameter name or math expression for \dot{x}_{max}

One internal state : x_1 initialized at $\min[\max(0, T \dot{x}_{min}), T \dot{x}_{max}]$

Two discrete variables : $z_1 \in \{-1, 0, 1\}$ and $z_2 \in \{-1, 0, 1\}$

Two equations :

$$\begin{cases} 0 = x_1 - G x_i + x_j & \text{if } z_1 = 0 \\ 0 = x_1 - T \dot{x}_{max} & \text{if } z_1 = 1 \\ 0 = x_1 - T \dot{x}_{min} & \text{if } z_1 = -1 \end{cases}$$

$$\begin{cases} T \dot{x}_j = x_1 & \text{if } z_2 = 0 \\ 0 = x_j - x_{max} & \text{if } z_2 = 1 \\ 0 = x_j - x_{min} & \text{if } z_2 = -1 \end{cases}$$

\dot{x}_{max} (resp. \dot{x}_{min}) is the maximum (resp. minimum) rate of change of x with time.

The time constant T can be zero. In this case:

- $x_1 = 0$ throughout the whole simulation
- the block behaves like a gain: $x_j = Gx_i$
- both limiters are ignored: $x_{max} \rightarrow \infty$, $x_{min} \rightarrow -\infty$, $T\dot{x}_{max} \rightarrow \infty$, $T\dot{x}_{min} \rightarrow -\infty$.

Discrete transitions :

```

if  $z_1 = 0$  then
  if  $x_1 > T \dot{x}_{max}$  then
     $z_1 \leftarrow 1$ 
  else if  $x_1 < T \dot{x}_{min}$  then
     $z_1 \leftarrow -1$ 
  end if
else if  $z_1 = 1$  then
  if  $Gx_i - x_j < T \dot{x}_{max}$  then
     $z_1 \leftarrow 0$ 
  end if
else if  $z_1 = -1$  then
  if  $Gx_i - x_j > T \dot{x}_{min}$  then
     $z_1 \leftarrow 0$ 
  end if
end if
if  $z_2 = 0$  then
  if  $x_j > x_{max}$  then
     $z_2 \leftarrow 1$ 
  else if  $x_j < x_{min}$  then
     $z_2 \leftarrow -1$ 
  end if
else if  $z_2 = 1$  then
  if  $x_1 < 0$  then
     $z_2 \leftarrow 0$ 
  end if
else if  $z_2 = -1$  then
  if  $x_1 > 0$  then
     $z_2 \leftarrow 0$ 
  end if
end if

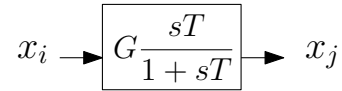
```

Initialization of discrete variables :

```
if  $Gx_i - x_j > T \dot{x}_{max}$  then  
   $z_1 \leftarrow 1$   
else if  $Gx_i - x_j < T \dot{x}_{min}$  then  
   $z_1 \leftarrow -1$   
else  
   $z_1 \leftarrow 0$   
end if  
if  $x_j > x_{max}$  then  
   $z_2 \leftarrow 1$   
else if  $x_j < x_{min}$  then  
   $z_2 \leftarrow -1$   
else  
   $z_2 \leftarrow 0$   
end if
```

tfder1p

Transfer function: derivative with one time constant



Syntax : & tfder1p
 name of variable x_i
 name of variable x_j
 data name, parameter name or math expression for G
 data name, parameter name or math expression for T

Internal states : x_1

Discrete variables : none

Equations :

$$T \dot{x}_1 = x_j \tag{7.1}$$

$$0 = G x_i - x_1 - x_j \tag{7.2}$$

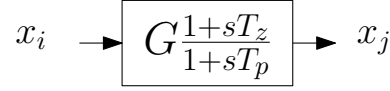
Initialization of internal states: $x_1 = G x_i$

The model allows $T = 0$. In this case:

- $x_j = 0$ as expected;
- Eq. (7.2) is useless but is integrated with the rest of the model.

tf1p1z

Transfer function between input and output: one zero and one pole



Syntax : & tf1p1z
 name of variable x_i
 name of variable x_j
 data name, parameter name or math expression for G
 data name, parameter name or math expression for T_z
 data name, parameter name or math expression for T_p

Internal states : x_1

Discrete variables : none

Equations :

$$\dot{x}_1 = G x_i - x_j \quad (7.3)$$

$$0 = T_p x_j - G T_z x_i - x_1 \quad (7.4)$$

Initialization of internal states : $x_1 = G (T_p - T_z) x_i$

The model allows $T_z = 0$. In this case, simplifying Eq. (7.4) and combining it with Eq. (7.3) yields $T_p \dot{x}_j = -x_j + G x_i$, which corresponds to $x_j = \frac{G}{1 + sT_p} x_i$ as expected.

Formally, the model also allows $T_p = 0$. However, in this case, the transfer function between x_i and x_j becomes $G (1 + sT_z)$. **This involves a pure derivator. Hence, the solver may produce undesired transients when x_i or \dot{x}_i undergoes a discontinuity.**

The model allows $T_p = T_z = T$. In this case, Equation (7.4) becomes $x_j - G x_i = \frac{x_1}{T}$, and replacing this result in Eq. (7.3) yields $\dot{x}_1 = -\frac{x_1}{T}$, showing that x_1 evolves independently of x_i and x_j . Furthermore, when $T_z = T_p$, x_1 is initialized to zero; hence, it remains equal to zero for the whole simulation. Replacing $x_1 = 0$ yields $x_j = G x_i$ as expected.

tf2p2z

Transfer function between input and output: two real zeros and two real poles

$$x_i \rightarrow \boxed{G \frac{1+n_1s+n_2s^2}{1+d_1s+d_2s^2}} \rightarrow x_j$$

Syntax : & tf2p2z
 name of variable x_i
 name of variable x_j
 data name, parameter name or math expression for G
 data name, parameter name or math expression for n_1
 data name, parameter name or math expression for n_2
 data name, parameter name or math expression for d_1
 data name, parameter name or math expression for d_2

Internal states : x_1 and x_2

Discrete variables : none

Equations : correspond to a second-order state space model with controllable canonical form:

$$\dot{x}_1 = x_2 \tag{7.1}$$

$$d_2 \dot{x}_2 = -x_1 - d_1 x_2 + d_2 x_i \tag{7.2}$$

$$0 = G(d_2 - n_2)x_1 + G(n_1 d_2 - d_1 n_2)x_2 + G n_2 d_2 x_i - d_2^2 x_j \tag{7.3}$$

Initialization of internal states : $x_2 = 0$ and $x_1 = d_2 x_i$

Exception. If a small value is specified for d_2 , namely if $d_2 < 0.005$, both d_2 and n_2 are set to zero and the transfer function becomes:

$$G \frac{1 + n_1 s}{1 + d_1 s}$$

as considered in the `tf1p1z` block.

If, in addition, a small value is specified for d_1 , namely if $d_1 < 0.005$, both d_1 and n_1 are set to zero and the block behaves as a simple gain:

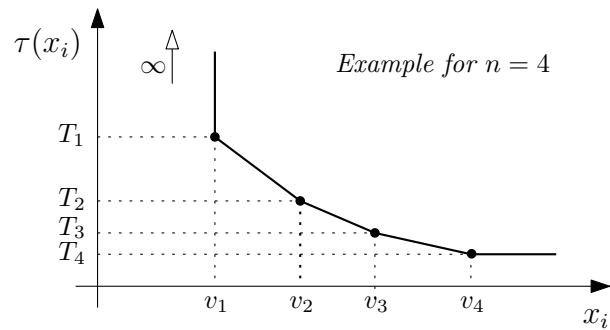
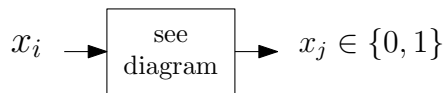
$$x_j = G x_i$$

timer*

Timer with varying delay. The latter is a piecewise linear function of the monitored variable

If x_i is smaller than a threshold v_1 , the output x_j is equal to zero. Otherwise, x_j changes from zero to one at time $t^ + \tau(x_i)$ where t^* is the time at which the input x_i became larger than v_1 and the delay $\tau(x_i)$ varies with x_i according to a piecewise linear characteristic involving n points (see diagram below).*

Separate blocks exist for $n = 1, 2, 3, 4$ and 5.



Syntax :

& timer1

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

& timer2

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

data name, parameter name or math expression for v_2

data name, parameter name or math expression for T_2

& timer3

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

data name, parameter name or math expression for v_2

data name, parameter name or math expression for T_2

data name, parameter name or math expression for v_3

data name, parameter name or math expression for T_3

& timer4

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

data name, parameter name or math expression for v_2

data name, parameter name or math expression for T_2

data name, parameter name or math expression for v_3

data name, parameter name or math expression for T_3

data name, parameter name or math expression for v_4

data name, parameter name or math expression for T_4

& timer5

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

data name, parameter name or math expression for v_2

data name, parameter name or math expression for T_2

data name, parameter name or math expression for v_3

data name, parameter name or math expression for T_3

data name, parameter name or math expression for v_4

data name, parameter name or math expression for T_4

data name, parameter name or math expression for v_5

data name, parameter name or math expression for T_5

Internal states : x_1

Discrete variables : $z \in \{-1, 0, 1\}$

Equations :

$$0 = \begin{cases} x_j & \text{if } z \in \{-1, 0\} \\ x_j - 1 & \text{if } z = 1 \end{cases}$$

$$\begin{cases} 0 & = x_1 & \text{if } z = -1 \\ \dot{x}_1 & = 1 & \text{if } z = 0 \\ \dot{x}_1 & = 0 & \text{if } z = 1 \end{cases}$$

Discrete transitions :

```

if  $z = -1$  then
  if  $x_i \geq v_1$  then
     $z \leftarrow 0$ 
  end if
else
  if  $x_i < v_1$  then
     $z \leftarrow -1$ 
  end if
end if
if  $z = 0$  then
  if  $x_1 \geq \tau(x_i)$  then
     $z \leftarrow 1$ 
  end if
end if

```

Initialization of internal states : $x_1 \leftarrow 0$

Initialization of discrete variables : $z \leftarrow -1$

The v_i values must be increasing, but two consecutive values may be equal, i.e. $v_1 \leq v_2 \leq v_3 \leq \dots \leq v_{n-1} \leq v_n$.

The piecewise linear characteristic is typically used to approximate an inverse-time characteristic, in which case the T values are decreasing, i.e. $T_1 \geq T_2 \geq T_3 \geq \dots \geq T_{n-1} \geq T_n$. Nevertheless, non decreasing values are also allowed.

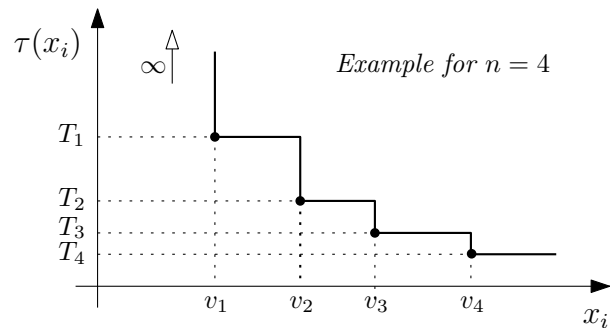
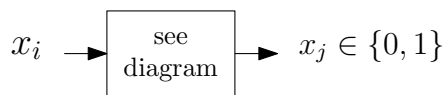
If the initial value of x_i is larger than v_1 , x_j will change to one after the time $\tau(x_i)$, unless x_i decreases below v_1 before the delay τ is elapsed.

timersc*

Timer with varying delay. The latter is a staircase function of the monitored variable

If x_i is smaller than a threshold v_1 , the output x_j is equal to zero. Otherwise, x_j changes from zero to one at time $t^ + \tau(x_i)$ where t^* is the time at which the input x_i became larger than v_1 and the delay $\tau(x_i)$ varies with x_i according to a staircase characteristic involving n points (see diagram below).*

Separate blocks exist for $n = 1, 2, 3, 4, 5$ and 6 .



Syntax :

& timersc1

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

& timersc2

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

data name, parameter name or math expression for v_2

data name, parameter name or math expression for T_2

& timersc3

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

data name, parameter name or math expression for v_2

data name, parameter name or math expression for T_2

data name, parameter name or math expression for v_3

data name, parameter name or math expression for T_3

& timersc4

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

data name, parameter name or math expression for v_2

data name, parameter name or math expression for T_2

data name, parameter name or math expression for v_3

data name, parameter name or math expression for T_3

data name, parameter name or math expression for v_4

data name, parameter name or math expression for T_4

& timersc5

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

data name, parameter name or math expression for v_2

data name, parameter name or math expression for T_2

data name, parameter name or math expression for v_3

data name, parameter name or math expression for T_3

data name, parameter name or math expression for v_4

data name, parameter name or math expression for T_4

data name, parameter name or math expression for v_5

data name, parameter name or math expression for T_5

& timersc6

name of variable x_i

name of variable x_j

data name, parameter name or math expression for v_1

data name, parameter name or math expression for T_1

data name, parameter name or math expression for v_2

data name, parameter name or math expression for T_2

data name, parameter name or math expression for v_3

data name, parameter name or math expression for T_3

data name, parameter name or math expression for v_4

data name, parameter name or math expression for T_4

data name, parameter name or math expression for v_5

data name, parameter name or math expression for T_5

data name, parameter name or math expression for v_6

data name, parameter name or math expression for T_6

Internal states : x_1

Discrete variables : $z \in \{-1, 0, 1\}$

Equations :

$$0 = \begin{cases} x_j & \text{if } z \in \{-1, 0\} \\ x_j - 1 & \text{if } z = 1 \end{cases}$$

$$\begin{cases} 0 & = x_1 & \text{if } z = -1 \\ \dot{x}_1 & = 1 & \text{if } z = 0 \\ \dot{x}_1 & = 0 & \text{if } z = 1 \end{cases}$$

Discrete transitions :

```

if  $z = -1$  then
  if  $x_i \geq v_1$  then
     $z \leftarrow 0$ 
  end if
else
  if  $x_i < v_1$  then
     $z \leftarrow -1$ 
  end if
end if
if  $z = 0$  then
  if  $x_1 \geq \tau(x_i)$  then
     $z \leftarrow 1$ 
  end if
end if

```

Initialization of internal states : $x_1 \leftarrow 0$

Initialization of discrete variables : $z \leftarrow -1$

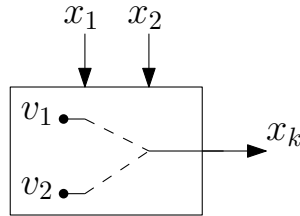
The v_i values must be increasing, but two consecutive values may be equal, i.e. $v_1 \leq v_2 \leq v_3 \leq \dots \leq v_{n-1} \leq v_n$.

The staircase characteristic is typically used to approximate an inverse-time characteristic, in which case the T values are decreasing, i.e. $T_1 \geq T_2 \geq T_3 \geq \dots \geq T_{n-1} \geq T_n$. Nevertheless, non decreasing values are also allowed.

If the initial value of x_i is larger than v_1 , x_j will change to one after the time $\tau(x_i)$, unless x_i decreases below v_1 before the delay τ is elapsed.

tsa

Two-state automaton with transitions based on signs of two inputs



The output state x_k can take two values: v_1 or v_2 . When $x_k = v_1$ the change to v_2 depends on the sign of x_1 ; when $x_k = v_2$ the change to v_1 depends on the sign of x_2 .

Syntax : & 2sa
 name of variable x_1
 name of variable x_2
 name of variable x_k
 data name, parameter name or math expression for v_1
 data name, parameter name or math expression for v_2

Internal states : none

Discrete variable : $z \in \{1, 2\}$ represents the state of the automaton

Equations :

$$0 = \begin{cases} x_k - v_1 & \text{if } z = 1 \\ x_k - v_2 & \text{if } z = 2 \end{cases}$$

Discrete transitions :

```

if  $z = 1$  and  $x_1 > 0$  then
   $z \leftarrow 2$ 
else if  $z = 2$  and  $x_2 > 0$  then
   $z \leftarrow 1$ 
end if

```

Initialization of discrete variable : the initial value is $z = 1$, i.e. $x_k = v_1$ is assumed initially.

7.4 Functions available in models

The functions documented in this section can be used in all mathematical expressions mentioned in Fig. 6.7.

The first two are general. The others are power system-oriented. Among them, some functions are restricted to some types of models.

```
double precision function equal(var1,var2)
```

```
double precision:: var1, var2
```

This function returns 1.d0 if var1 differs from var2 by less than 10^{-6} , and 0.d0 otherwise.

```
double precision function equalstr(var1,var2)
```

```
character:: var1, var2
```

This function returns 1.d0 if the non-blank parts of str1 and str2 are the same, and 0.d0 otherwise.

```
double precision ppower([vx],[vy],[ix],[iy])
```

Returns the active power injected into network

Can be used in models of type: inj

Computation :

$$P = v_x i_x + v_y i_y$$

```
double precision qpower([vx],[vy],[ix],[iy])
```

Returns the reactive power injected into network

Can be used in models of type: inj

Computation :

$$Q = v_y i_x - v_x i_y$$

```
double precision function vrectif([if],[vin],{kc})
```

```
double precision:: kc
```

This function is used to model the voltage drop in rectifiers. It gives the output voltage v_{rectif} as a function of the output current i_f and the input voltage v_{in} . It appears in some IEEE standard excitation models with $v_{rectif} = f_{ex} E_{FD}$

Can be used in models of type: exc

Computation :

```
in = kc if / max(vin, 10-3)
if in ≤ 0 then
    vrectif = vin
else if in ≤ 0.433 then
    vrectif = vin - 0.577 kc if
else if in ≤ 0.75 then
    vrectif = √(0.75 vin2 - (kc if)2)
else if in ≤ 1.00 then
    vrectif = 1.732(vin - kc if)
else
    vrectif = 0
end if
```

```
double precision function vinrectif([if],[vrectif],{kc})
```

```
double precision:: kc
```

This function is the inverse of v_{rectif} . It is aimed at being called at initialization. For given values the field current i_f and rectifier output voltage v_{rectif} it returns the value of the rectifier input voltage $v_{inrectif}$. This determination is iterative because the portion of the nonlinear input-output characteristic on which the rectifier is operating is not known beforehand. The function does not work with a zero rectifier output v_{rectif} since, in this case, the input voltage is indeterminate.

Can be used in models of type: exc

Computation :

```

nbtries = 1
vinest = vrectif + 0.577 kc if
loop
  in = kc if / max(vinest, 1d - 03)
  if in ≤ 0 then
    vinrectif = vrectif
  else if in ≤ 0.433 then
    vinrectif = vrectif + 0.577 kc if
  else if in ≤ 0.75 then
    vinrectif =  $\sqrt{vrectif^2 + (kc\ if)^2} / 0.75$ 
  else
    vinrectif = (vrectif / 1.732) + kc if
  end if
  if vinrectif = vinest or nbtries > 5 then
    exit loop
  end if
  nbtries = nbtries + 1
  vinest = vinrectif
end loop

```

```
double precision function vcomp([v],[p],[q],[Kv},{Rc},{Xc})
```

```
double precision:: Kv, Rc, Xc
```

This function returns the magnitude of a combination of the terminal voltage and the current of a synchronous machine. It appears in some IEEE standard excitation models

Can be used in models of type: exc

Computation :

$$\begin{aligned}
 V_{comp} &= |K_v \bar{V} + (R_c + jX_c) \bar{I}| = |K_v V + (R_c + jX_c)(i_P - ji_Q)| \\
 &= |K_v V + (R_c + jX_c)(\frac{P}{V} - j\frac{Q}{V})| \\
 &= \frac{1}{V} \sqrt{(K_v V^2 + R_c P + X_c Q)^2 + (X_c P - R_c Q)^2}
 \end{aligned}$$

```
double precision function satur([ve],[ve1},{se1},{ve2},{se2})
```

```
double precision:: ve1, se2, ve2, se2
```

This function returns the increment of field current needed to obtain a given output voltage, taking saturation into account. It appears in the model of some excitation systems.

Can be used in models of type: `exc`

Computation :

$$satur = m \, ve^n$$

where:

$$n = \frac{\log_{10}(se1/se2)}{\log_{10}(ve1/ve2)}$$

$$m = \frac{se1}{ve1^n}$$

Exception. *The function returns $satur = 0$ if any of the following conditions holds true:*

$$ve \leq 0 \quad or \quad ve1 \leq 0 \quad or \quad ve2 \leq 0 \quad or \quad ve1 = ve2 \quad or \quad se1 = 0 \quad or \quad se2 = 0$$