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April 12, 2016



## objectives.

- Review the handling of complex coupled equations sets in foam-extend using block-coupled solution algorithms.
- Show the interface and implementation examples of coupled equation sets.

## Topics:

- Introduction on implicit coupling models.
- 2 Block-coupled solution for multiple variables on a single mesh.
- **3** Examples of coupled systems:
  - Simple multi-equation coupling: blockCoupledScalarTransportFoam.
  - Block-coupled (vector) finite volume operators fvm.
  - Block-coupled  $p \mathbf{u}$  algorithm: pUCoupledFoam.
  - Block-coupled by a algorithm. pocoupled roam.
     Block-coupled eddy viscosity turbulence models.





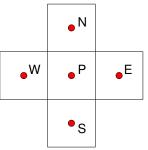
- For cases of strong coupling between the components of a vector, the components can be solved as a **block variable**:  $(u_x, u_y, u_z)$  will appear as variables in the same linear system.
- In spite of the fact that the system is much larger, the coupling pattern still exists: components of **u** in cell P may be coupled to other components in the same point or to vector components in the neighbouring cell.
- With this in mind, we can still keep the sparse addressing defined by the mesh: if a variable is a vector, a tensorial diagonal coefficients couples the vector components in the same cell. A tensorial off-diagonal coefficient couples the components of  $\mathbf{u}_P$  to all components of  $\mathbf{u}_N$ , which covers all possibilities.

**Block-Coupled Operators** 

- For multi-variable block solution like the compressible Navier-Stokes system above, the same trick is used: the cell variable consists of  $(\rho, \rho \mathbf{u}, \rho E)$  and the coupling can be coupled by a  $5 \times 5$  matrix coefficient.
- Important disadvantages of a block coupled system are:
  - Large linear system: several variables are handled together,
    - Different kinds of physics can be present, *e.g.* the transport-dominated (parabolic/hyperbolic) momentum equation and elliptic pressure equation. At matrix level, it is impossible to separate them, which makes the system more difficult to solve.



Irrespective of the level of coupling, the FVM dictates that a cell value will depend only on the values in surrounding cells.



• We still have freedom to organise the matrix by ordering entries for various components of  $\phi$ . Also, the matrix connectivity pattern may be changed by reordering the computational points.

- **Example:** block-coupled vector equation  $(u_x, u_y, u_z)$ .
  - Per-variable organisation: first  $u_x$  for all cells, followed by  $u_y$  and  $u_z$ . Ordering of each sub-list matches the cell ordering.

$$\mathbf{A}_{P} = \begin{bmatrix} [u_{x} \leftrightarrow u_{x}] & [u_{x} \leftrightarrow u_{y}] & [u_{x} \leftrightarrow u_{z}] \\ [u_{y} \leftrightarrow u_{x}] & [u_{y} \leftrightarrow u_{y}] & [u_{y} \leftrightarrow u_{z}] \\ [u_{z} \leftrightarrow u_{x}] & [u_{z} \leftrightarrow u_{y}] & [u_{z} \leftrightarrow u_{z}] \end{bmatrix}$$

Diagonal blocks, e.g.  $[u_x \leftrightarrow u_x]$  have the size equal to the number of computational points and contain the coupling within the single component. All matrix coefficients are scalars. Off-diagonal block represent variable-to-variable coupling.

- Per-cell organisation:  $(u_x, u_y, u_z)$  for each cell. A single numbering space for all cells, but each individual coefficient is more complex: contains complete coupling.
- Both choices have advantages and choice depends on software infrastructure and matrix assembly methods. In order to illustrate the nature of coupling, we shall choose per-cell organisation.

- Steady-state conjugate heat transfer between a porous medium and a fluid flowing through it. Assuming frozen flow field.
- (This corresponds to modelling of radiators in automotive under-hood simulations).
- Fluid and solid domains are overlapping: same physical volume
- Heat transfer in fluid with heat exchange to solid:

Simple Equation Coupling

$$\nabla_{\bullet}(\mathbf{u}T) - \nabla_{\bullet}K(\nabla T) = \alpha(T_s - T)$$

■ Heat transfer in solid with heat exchange to fluid:

$$-\nabla_{\bullet} K_s(\nabla T_s) = \alpha (T - T_s)$$





- All cells share all field variables and allow coupling to.
  - Other variables in the same cells: "source term coupling"
  - Other variables in a neighbour cell: "transport coupling"
- ... but neighbourhood is still implied by the mesh: global sparseness pattern!

$T_1$ $T_{s1}$	T <sub>2</sub> T <sub>s2</sub>	



Trivial implementation: This is what FOAM was designed for!

```
fvScalarMatrix TEqn
    fvm::div(phi, T)
  - fvm::laplacian(DT, T)
    alpha*Ts - fvm::Sp(alpha, T)
);
TEqn.relax();
TEqn.solve();
fvScalarMatrix TsEqn
  - fvm::laplacian(DTs, Ts)
    alpha*T - fvm::Sp(alpha, Ts)
);
TsEqn.relax();
TsEqn.solve();
```



- The most important coupling is lagged: temperature fields T and  $T_s$  see each other in the source terms.
- Transport in each variable is handled implicitly.
- $\blacksquare$  ... but the dominant term of T to  $T_s$  is lagged, delaying convergence!

## Equation Coupling Idea: Solve T and $T_s$ in a Single Matrix

- How to couple the variables implicitly: source term with temperature difference must be updated implicitly.
- A variable solved for is a pair of temperatures in each cell  $\mathbf{x} = \begin{bmatrix} T \\ T_s \end{bmatrix}$ .
- Matrix coefficients become tensors ... What does this look like?

#### Generalisation of Matrix Operations

Global sparseness pattern is dependent on the mesh: matrix row contains an off-diagonal entry if two cells share a face.

$$\begin{bmatrix} \begin{bmatrix} a_{ff} & a_{fs} \\ a_{sf} & a_{ss} \end{bmatrix}_{P} & \vdots & \begin{bmatrix} a_{ff} & a_{fs} \\ a_{sf} & a_{ss} \end{bmatrix}_{U} & \vdots \\ \begin{bmatrix} a_{ff} & a_{fs} \\ a_{sf} & a_{ss} \end{bmatrix}_{P} & \vdots & \vdots & \vdots \end{bmatrix}_{U} & \vdots & \vdots & \vdots & \vdots \end{bmatrix} \begin{bmatrix} \begin{bmatrix} T_1 \\ T_{s1} \end{bmatrix} \\ \begin{bmatrix} T_2 \\ T_{s2} \end{bmatrix} \\ \begin{bmatrix} T_3 \\ T_{s3} \end{bmatrix} \\ \vdots & \vdots & \vdots & \vdots & \vdots \end{bmatrix} \begin{bmatrix} b_1 \\ b_{s1} \end{bmatrix}$$

- Analysis: which equations are zero or non-zero?
- Diagonal coefficient, off-diagonal entry: source coupling.
- Off-diagonal coefficient, off-diagonal entry: cross-transport



```
fvBlockMatrix<vector2> blockM(blockT);
// Insert equations into block Matrix
blockM.insertEquation(0, TEqn);
blockM.insertEquation(1, TsEqn);
// Add off-diagonal coupling terms
scalarField coupling (mesh. n Cells (), -alpha. value ());
blockM.insertEquationCoupling(0, 1, coupling);
blockM.insertEquationCoupling(1, 0, coupling);
// Update source coupling: coupling terms eliminated from
blockM.updateSourceCoupling();
blockM.solve(); // Block coupled solver call
// Retrieve solution
blockM.retrieveSolution(0, T.internalField());
blockM.retrieveSolution(1, Ts.internalField());
T. correctBoundaryConditions();
```

Ts. correctBoundaryConditions();

**Couple Gauss gradient** (of a scalar), eg.  $\nabla p$ 

$$\int_{V_P} \nabla \phi \, dV = \oint_{\partial V_P} d\mathbf{s} \, \phi$$
$$= \sum_f \mathbf{s}_f \phi_f$$
$$\phi_f = f_x \phi_P + (1 - f_x) \phi_N$$

- $\mathbf{a}_N = f_X \, \mathbf{s}_f$  and  $\mathbf{a}_P = -\sum_N \mathbf{a}_N$  are vector coefficient multiplying a scalar field
- Coupled Gauss divergence (of a vector), eg.  $\nabla_{\bullet} \mathbf{u} =$  transpose of a gradient operator
- Other block-coupled terms: work-in-progress
  - $\nabla_{\bullet} [\gamma (\nabla_{\mathbf{u}})^T]$  for structural analysis solvers
  - $\mathbf{v}_{\bullet}(\nabla \mathbf{u})^T$  for adjoint convection



Turbulent Steady Incompressible Flows: SIMPLE or Coupled.

**Equation** set contains linear  $p - \mathbf{u}$  and non-linear  $\mathbf{u} - \mathbf{u}$ coupling.

$$\frac{\partial \mathbf{u}}{\partial t} + \nabla_{\bullet}(\mathbf{u}\mathbf{u}) - \nabla_{\bullet}(\nu\nabla\mathbf{u}) = -\nabla\rho$$
$$\nabla_{\bullet}\mathbf{u} = 0$$

- Traditionally, this equation set is solved using the segregated SIMPLE algorithm.
  - Low memory peak: solution + single scalar matrix in peak storage.
  - p-U coupling is handled explicitly: loss of convergence (under-relaxation).
  - Number of iterations is substantial; not only due to non-linearity.
    - Convergence dependent on mesh size: SIMPLE slows down on large meshes. ◆□ > ◆圖 > ◆臺 > ◆臺 >



#### ■ Block-implicit p - u coupled solution

- Coupled solution significantly increases matrix size: 4 blocks instead of 1
- ... but the linear  $p \mathbf{u}$  coupling is fully implicit!
- Iteration sequence only needed to handle the non-linearity in the u-equation and the turbulence.
- Net result: significant convergence improvement (steady or transient) at a cost of increase in memory usage: reasonable performance compromise!



#### SIMPLE-Based Segregated p-U Solver

```
// Momentum equation assembly and solution
fvVectorMatrix UEqn
    fvm::div(phi, U)
  + turbulence -> div Dev Reff (U)
UEqn. relax();
solve(UEgn = -fvc :: grad(p));
// Pressure equation assembly and solution
U = UEqn().H()/UEqn.A();
phi = fvc::interpolate(U) & mesh.Sf();
fvScalarMatrix pEqn
    fvm::laplacian(1/UEqn.A(), p) = fvc::div(phi)
pEqn. solve();
phi -= pEqn.flux();
p.relax();
```



<b>u</b> <sub>1</sub>	<b>u</b> <sub>2</sub>	

$$\begin{bmatrix} \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \begin{pmatrix} a_{N}(\mathbf{u}\,\mathbf{u}) & a_{N}(\mathbf{u}\,\rho) \\ a_{N}(\rho\,\mathbf{u}) & a_{N}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\mathbf{u}\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\mathbf{u}) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\mathbf{u}) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho) & a_{P}(\rho\,\rho) \\ a_{P}(\rho\,\rho) & a_{P}(\rho\,\rho) \end{pmatrix} & \dots \\ \begin{pmatrix} a_{P}(\mathbf{u}\,\rho)$$

Block Coupled Matrix

Coupled Implicit p-U Solver: pUCoupledFoam

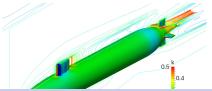
```
fvVectorMatrix UEqn
    fvm::div(phi, U)
  + turbulence -> div Dev Reff (U)
);
fvScalarMatrix pEqn
   - fvm::laplacian(rUAf, p) == -fvc::div(fvc::grad(p))
BlockLduSystem<vector, vector> plnU(fvm::grad(p));
BlockLduSystem<vector, scalar> Ulnp(fvm::UDiv(U));
fvBlockMatrix<vector4> UpEqn(Up);
UpEqn.insertEquation(0, UEqn);
UpEqn.insertEquation(3, pEqn);
UpEqn.insertBlockCoupling(0, 3, plnU, true);
UpEqn.insertBlockCoupling(3, 0, Ulnp, false);
UpEqn. solve();
UpEqn.retrieveSolution(0, U.internalField());
UpEqn.retrieveSolution(3, p.internalField());
```

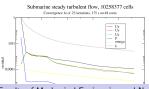
#### Open Source Implementation of the Coupled Implicit $p - \mathbf{u}$ Solver.

- Coupled solver reproduces the results of the segregated algorithm.
- Full integration with the finiteVolume library: re-use the existing and validated discretisation operators and boundary conditions without re-coding.

#### Coupled Solver Performance:

- Example: steady turbulent flow around a submarine, 10.2 million cells
- Turbulent  $k \omega$  SST model converges to 1e-4 in 23 iterations, 175 s on 48 cores



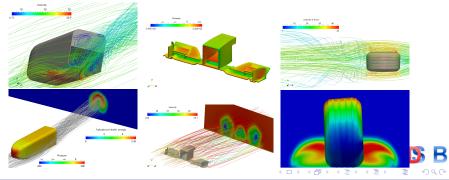




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### Who Needs a Coupled Solver?

- Improved speed-to-solution and reliability on difficult meshes.
- Robust discretisation: fewer settings.
- Improved parallel scaling: fewer processor communication calls.
- Already done: coupled turbulence model equations.



## Block-Coupled Turbulence

Block-Coupled Turbulence Models: coupledKEpsilon and coupledKOmegaSST:

Turbulence kinetic energy equation:

$$\frac{\partial k}{\partial t} + \nabla_{\bullet}(\overline{\mathbf{u}}k) - \nabla_{\bullet}(\nu_{eff}\nabla k) = G - \epsilon$$
$$G = \nu_{t} \left[ \frac{1}{2} (\nabla \overline{\mathbf{u}} + \nabla \overline{\mathbf{u}}^{T}) \right]^{2} = \mathbf{R} : \nabla U$$

Dissipation of turbulence kinetic energy equation:

$$\frac{\partial \epsilon}{\partial t} + \nabla_{\bullet}(\overline{\mathbf{u}}\epsilon) - \nabla_{\bullet}((\nu_{eff})\nabla \epsilon] = C_1 G \frac{\epsilon}{k} - C_2 \frac{\epsilon^2}{k}$$

Acknowledgment: Mr. Robert Keser (diploma thesis).



 Multiple equations with strong coupling: sparse-on-dense matrix class. Discretisation for "obvious" block-coupling; segregated discretisation is re-packed into block coefficients.

#### Block Matrix Tools in foam-extend:

- Dynamic coefficient expansion for general NxN coupling (used up to N=128),
- Support for coupled boundaries and parallelisation,
- Automated block matrix assembly and solution retrieval tools.

### Coupled Solution for the $p - \mathbf{u}$ Equation Set:

- Implicit block-coupled fvm::div(.) and fvm::grad(.) operators, re-using existing FVM discretisation
- Efficient coupled  $p \mathbf{u}$  solver for steady-state simulations, excellent results!



# Thanks for your attention. Questions, please?



**Block-Coupled Operators**