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MASTER OF SCIENCE IN APPLIED GEOPHYSICS  
RESEARCH THESIS

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## **Seismic deblending of simultaneous crossline sources**

**Christian Reinicke Urruticoechea**

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July 27, 2015



# **Seismic deblending of simultaneous crossline sources**

MASTER OF SCIENCE THESIS

for the degree of Master of Science in Applied Geophysics at  
Delft University of Technology  
ETH Zürich  
RWTH Aachen University  
by

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July 27, 2015

Department of Geoscience & Engineering	.	Delft University of Technology
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**Delft University of Technology**

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## Abstract

Blending is a recent seismic acquisition design which allows seismic shots to interfere. Blending is beneficial in terms of data quality and acquisition costs. Current processing techniques are not capable to deal with blended data. Consequently, the blended data must be separated as if they were acquired in a conventional way. The separation technique is referred to as deblending.

This thesis reviews the 2D deblending method of [Mahdad et al. \(2011\)](#), which is a noise prediction and subtraction method. Thus, this thesis points out how deblending benefits from incoherent shot interference, or "blending noise". For this purpose, a new measure of incoherency is introduced and 3 incoherent blending patterns are proposed. The deblending performance is measured with a quality factor which is similar to the signal to noise ratio.

A new blended acquisition design, 3D crossline blending, is presented. Based on the 2D method of [Mahdad et al. \(2011\)](#) a 3D deblending method is derived. The presented method is tested on a field data set. The field data results demonstrate that the method successfully deblends strong interfering events. The deblending of weak late events is not optimal yet.



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First of all I want to thank all the people who have participated in this project .. Remember, often more people have contributed to your final thesis than you initially would think of.

Delft, University of Technology  
July 27, 2015

Christian Reinicke Urruticoechea



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## **Acronyms**

**DUT** Delft University of Technology



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# Chapter 1

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## Introduction

### 1-1 Marine Seismic Acquisition

Today, our society strongly depends on oil and gas. For example, the magazine Forbes stated that "modern civilization would collapse in a matter of months if oil stopped flowing" ([Carlyle, 2013](#)).

In order to explore oil and gas the subsurface is "imaged" with acoustic waves. Seismic acquisition has a significant impact on the data quality, and thus, on the success of exploration. As a consequence optimizing seismic acquisition is beneficial for the modern society.

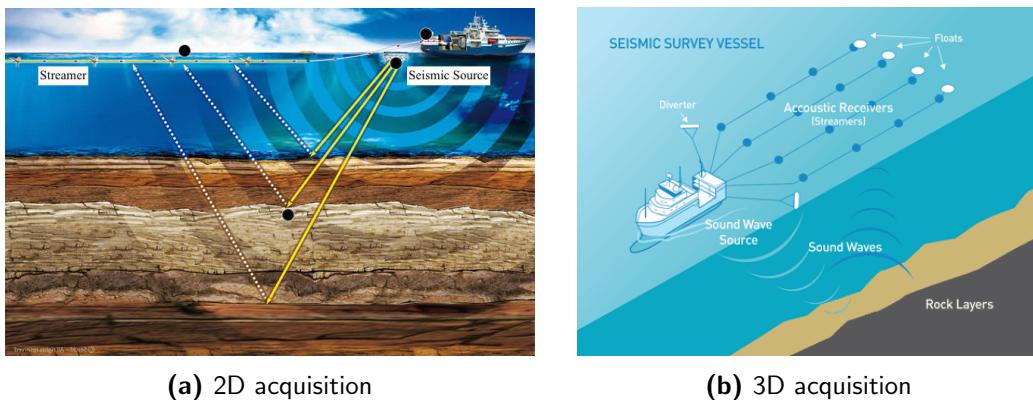
#### Conventional Acquisition

In marine acquisition the subsurface is "imaged" by emitting an acoustic wavefield, which is reflected in the subsurface and detected by the receivers. In a conventional marine acquisition set up a vessel tows a single seismic source (airgun) and multiple receivers (hydrophones). The receivers are assembled on, either a single streamer (2D acquisition), or on several streamers (3D acquisition). Figure 1-1 illustrates the conventional 2D and 3D acquisition set up.

During acquisition successive shots are separated by sufficient time, so called recording time, to avoid shot interference. As the vessel continuously moves while recording the spatial distance between successive shot positions is large, i.e. the spatial source sampling is coarse. Consequently, the subsurface is illuminated from few angles. In addition, the recording time between successive shots limits the minimum survey time. As the fuel consumption of the vessel is a major cost factor of a seismic survey it is desired to keep the survey time as short as possible.

#### Blended Acquisition

**The graduate problem.** Blended acquisition can be illustrated with the graduate problem. Imagine a Norwegian seismic service company wants to hire a new graduate student.



**Figure 1-1:** Illustration of (a) 2D and (b) 3D marine seismic acquisition. Both pictures are taken from the website [wikigrewal.com](http://wikigrewal.com) (Jul, 2015).

Unfortunately, the manager Mr Gert-Jan is too busy to interview each of them individually. Therefore, he invites all candidates at the same time and asks them to answer to his questions simultaneously. Mr Gert-Jan records their answers with his phone. Obviously, the recording is not understandable at all because all answers are interfered or "blended". Luckily, Mr Gert-Jan has a smart deblending algorithm, which is capable to separate or "deblend" the recording, such that he has individual recordings of all candidates. These recordings are clearly understandable and Mr Gert-Jan can pick the ideal candidate.

In blended acquisition, or simultaneous source acquisition, seismic shots may interfere. This allows to reduce the time between successive shots, and therefore, to improve the spatial source sampling. The two major advantages are; (1) illumination of the subsurface from multiple angles, and (2) reduction of the survey time. When designing a blended acquisition one can decide to put more weight on enhancing the data quality, or on reducing the survey time.

Existing blended acquisition designs blend sources along the inline direction (2D blending). During processing the data are deblended, i.e. the interfering shots are separated as if they were recorded in a conventional fashion.

## 1-2 Literature Review

The success of seismic deblending is strongly dependent on the acquisition design. In case of land data blended sources can be encoded, such that the deblending problem can be controlled (Womack et al., 1990). However, in marine acquisition impulsive sources are applied, i.e. a new approach to deblending has been needed.

Beasley et al. (1998) first proposed to apply simultaneous sources without source encoding. His method relies separating the blended sources in space. This allows to blend impulsive sources, and thus, to apply blending in marine acquisition.

Vaage (2005) suggested a blended acquisition design with random firing-time delays. The set-up consists of two seismic sources, which are towed at a fixed distance. In each experiment the two sources are fired with a time delay, which differs for each experiment. Consequently,

the second source becomes incoherent in any domain but the common shot domain. The sources can be separated with a coherency constraint.

Another way of overcoming the underdeterminacy of the deblending problem was proposed by [Ikelle et al. \(2007\)](#). His approach exploits the sparsity of seismic data as a constraint. This thesis builds on the 2D deblending method of [Mahdad et al. \(2011\)](#), which uses both a coherency and a sparsity constraint as presented in Chapter 2.

link to my method?

## 1-3 New Survey Design: Crossline Blending (3D)

Existing blended acquisition designs blend sources in inline direction, i.e. in 2D. This thesis suggests a new survey design, crossline blending. In crossline blending multiple sources are spread along the crossline direction and fired with a defined time delay. If the time delay is sufficiently short the acquisition is blended. Considering the movement of the vessel the blending is 3D process.

Crossline blending opens the possibility to design completely new acquisition set-ups. In this thesis a set-up with dense crossline source sampling will be presented and its suitability for blended acquisition will be tested. The suggested acquisition design is illustrated in Figure .

Insert sketch!

This thesis will demonstrate how deblending benefits from an incoherent blending pattern, and how deblending can be achieved for 3D blended data. The advantage of 3D blending is that (1) the subsurface is illuminated from several angles, in particular, from the side, and that (2) the dense source sampling allows to reduce the survey time.

## 1-4 Thesis Outline

This thesis aims to develop a 3D crossline deblending method. The content of the thesis is outlined below.

### Chapter 2: Theory

In this chapter the forward model of conventional and blended seismic data by [Berkhout \(1982\)](#) is explained. Next, the deblending method of [Mahdad et al. \(2011\)](#) is discussed in detail.

### Chapter 3: Incoherency

This chapter demonstrates the effect of an incoherent blending pattern, in terms of time and space, on the deblending quality. For this purpose a new measure of incoherency is introduced.

### Chapter 4: Crossline Deblending (3D)

A 3D deblending method derived. In particular, the data sorting and the design of a 3D  $f-k_x-k_y$  filter are discussed.

### Chapter 5: Results Field Data

In this chapter a 3D blended acquisition design is proposed and the presented 3D deblending method is tested on a complex data set.

**Chapter 6:** *Discussion and Conclusions*

The conclusions of the thesis are presented and discussed.

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# Chapter 2

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## Theory

This chapter describes the theory behind blending and deblending. First the detail hiding operator notation is explained. This notation is used to describe the forward model of seismic data. By introducing the blending operator the forward model is extended to the blended case. Next, the deblending method presented in [Mahdad et al. \(2011\)](#) is discussed to illustrate some of the concepts used in this thesis.

### 2-1 The Forward Model of Blending

#### 2-1-1 Conventional Seismic Data

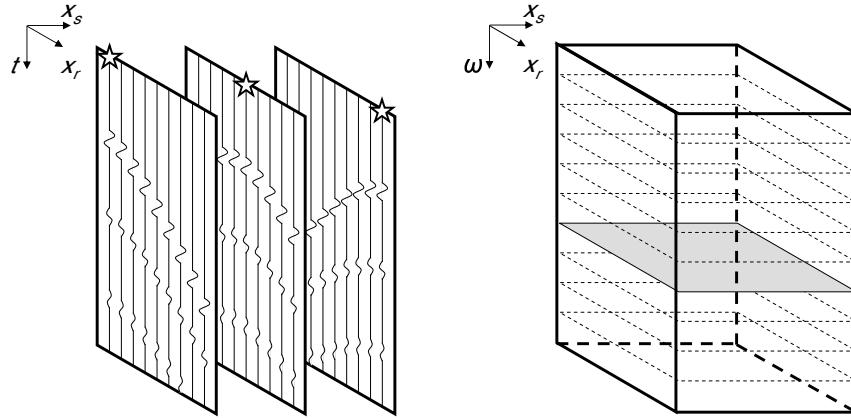
In the detail hiding operator notation ([Berkhout, 1982](#)) the recorded signal is considered discrete in terms of time  $t$ , receiver position  $x_r$ , and source position  $x_s$ . Thus, the measurements can be organized in a cube,  $\mathbf{p}(t, x_r, x_s)$ , (see Figure 2-1). Each frequency slice of this new cube represents the data matrix,  $\mathbf{P}$ .

In the data matrix,  $\mathbf{P}$ , each column corresponds to a monochromatic common shot gather (see Figure 2-2), each row to a monochromatic common receiver gather, each diagonal to a monochromatic common offset gather, and each anti-diagonal to a monochromatic common midpoint gather.

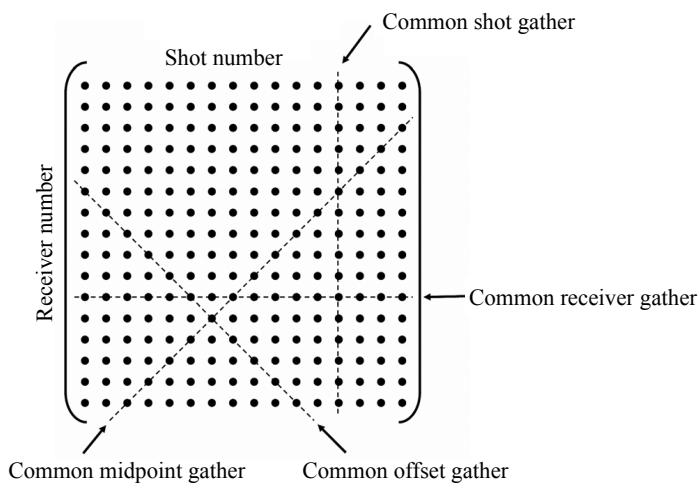
According to the seismic forward model of [Berkhout \(1982\)](#) the data matrix,  $\mathbf{P}$ , can be represented by a matrix multiplication of the source matrix,  $\mathbf{S}$ , the impulse response of the earth,  $\mathbf{X}$ , and the receiver matrix,  $\mathbf{D}$ :

$$\mathbf{P} = \mathbf{D} \mathbf{X} \mathbf{S}. \quad (2-1)$$

In the source matrix,  $\mathbf{S}$ , both rows and columns represent shot positions (see Figure 2-3). Thus,  $\mathbf{S}$  is a diagonal matrix. Each diagonal element  $s_{ii}$  captures one frequency component of the source signature injected in the earth at the position  $x_s = x_i$ . By applying a Fourier



**Figure 2-1:** Illustration of the data matrix,  $P$ , by van Groenestijn (2010). *Left:* The signal generated at the source position,  $x_s$ , is measured at receiver position,  $x_r$ , as a function of time,  $t$ . Thus, the discretized data is saved in a cube,  $p(t, x_r, x_s)$ . *Right:* The cube on the right equals the left cube after a Fourier transform with respect to time. Each frequency slice of the right cube represents the data matrix,  $P$ .



**Figure 2-2:** Illustration of the data matrix,  $P$ , by Mahdad et al. (2011). The dotted lines indicate directions of common gathers.

$$\begin{array}{|c|c|c|c|} \hline
 \star & 0 & 0 & 0 \\ \hline
 0 & \star & 0 & 0 \\ \hline
 0 & 0 & \star & 0 \\ \hline
 0 & 0 & 0 & \star \\ \hline
 \end{array}
 \cdot
 \begin{array}{|c|c|} \hline
 1 & 0 \\ \hline
 0 & 1 \\ \hline
 e^{-j\omega\Delta t_1} & 0 \\ \hline
 0 & e^{-j\omega\Delta t_2} \\ \hline
 \end{array}
 =
 \begin{array}{|c|c|} \hline
 \star & 0 \\ \hline
 0 & \star \\ \hline
 \star & 0 \\ \hline
 0 & \star \\ \hline
 \end{array}$$

**S**                     **$\Gamma$**                      **$S_{bl}$**

**Figure 2-3:** A conventional source matrix,  $\mathbf{S}$ , is transformed to a blended source matrix,  $\mathbf{S}_{bl}$ , by applying the blending matrix,  $\mathbf{\Gamma}$ . Each star represents one shot, and the gray scale of the stars represents the relative firing time.

transform to all frequency components of the element  $s_{ii}$  the source signature as a function of time is obtained.

The impulse response of the earth,  $\mathbf{X}$ , describes how an impulse at the source location,  $x_s$ , is transformed in the earth into the signal at the receiver location,  $x_r$ .

The receiver matrix,  $\mathbf{D}$ , converts the seismic wavefield at the receiver location,  $x_r$ , to the recorded signal. This includes adding the receiver ghost.

In practice, one tries to retrieve the unknown earth response,  $\mathbf{X}$ , from the data,  $\mathbf{P}$ , by removing  $\mathbf{S}$  (designation) and  $\mathbf{D}$  (receiver deghosting).

### 2-1-2 Blended Seismic Data

In blended acquisition the recorded events belonging to different shots overlap, as shown in the shot gather in Figure 2-4.

Blending can be captured in the forward model by introducing a blending matrix,  $\mathbf{\Gamma}$ , which transforms the source matrix,  $\mathbf{S}$ , into a blended source matrix,  $\mathbf{S}_{bl}$ ,

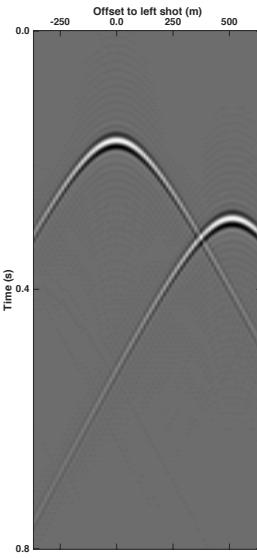
$$\mathbf{S}_{bl} = \mathbf{S} \mathbf{\Gamma}. \quad (2-2)$$

Figure 2-3 shows the structure of  $\mathbf{\Gamma}$ ; each row of  $\mathbf{\Gamma}$  represents one source, and each column of  $\mathbf{\Gamma}$  represents one experiment.

The blending matrix captures the physics of a blended acquisition as follows: An element  $\gamma_{ij}$  of the blending matrix includes a source  $i$  and an experiment  $j$ . If the source  $i$  is not fired in the  $j^{th}$  experiment  $\gamma_{ij}$  is zero. If it is fired, source  $i$  has a relative amplitude  $A_{ij}$  and a relative time delay  $\Delta t_{ij}$  with respect to the first source fired in the  $j^{th}$  experiment;

$$\gamma_{ij} = A_{ij} e^{-j\omega\Delta t_{ij}}. \quad (2-3)$$

Thus, the blending matrix selects specific sources from the source matrix and superimposes them as visualized in Figure 2-3. From Figure 2-3 it also becomes clear that both the blending



**Figure 2-4:** Blended shot gather of two shots. The right shot is fired 120 ms after the left shot.

matrix,  $\Gamma$ , and the blended source matrix,  $\mathbf{S}_{bl}$ , have more rows than columns, i.e. there are more sources than experiments. Thus, the acquisition is done in less time.

In the case of source blending the receiver matrix,  $\mathbf{D}$ , is not influenced. Of course, the earth impulse response,  $\mathbf{X}$ , is independent of the acquisition design. Hence, the blended data can be written as;

$$\mathbf{P}_{bl} = \mathbf{D} \mathbf{X} \mathbf{S}_{bl} = \mathbf{D} \mathbf{X} \mathbf{S} \Gamma = \mathbf{P} \Gamma. \quad (2-4)$$

Note that, the blended data matrix,  $\mathbf{P}_{bl}$ , also has less columns, i.e. less experiments, than the unblended data matrix,  $\mathbf{P}$ .

## 2-2 Deblending

Before removing the receiver matrix,  $\mathbf{D}$ , and the source matrix,  $\mathbf{S}$ , one must remove the blending matrix,  $\Gamma$ , from the blended data,  $\mathbf{P}_{bl}$ . This process is called deblending.

The deblending method presented in this thesis builds on the method of [Mahdad et al. \(2011\)](#). Therefore, the this method is described in great detail.

The basic workflow of the Mahdad method is summarized in Figure 2-5 and will be explained step by step in the following subsections.

### 2-2-1 Pseudo-Deblending

Unfortunately, the inverse problem of equation 2-4 is underdetermined, which means that there is not a unique solution for the unblended data,  $\mathbf{P}$ . Thus, additional constraints are



**Figure 2-5:** Flowchart belonging to the deblending method of Mahdad et al. (2011).

required to deblend the data, which are; (1) sparsity of the signal in the  $x$ - $t$ -domain and (2) coherency of the signal in the  $f$ - $k$ -domain.

The first estimate of the unblended data matrix,  $\mathbf{P}$ , is obtained by pseudo-deblending;

$$\mathbf{P}_{ps} = \mathbf{P}_{bl} \boldsymbol{\Gamma}^H, \quad (2-5)$$

where  $\boldsymbol{\Gamma}^H$  is the conjugate transpose of the blending matrix,  $\boldsymbol{\Gamma}$ . Pseudo-deblending copies the blended data to the locations of all shots present in the blended shot and shifts them upward in time to compensate for the time delay. For example, Figure 2-6a and 2-6b shows the two pseudo-deblended shot gathers of the blended data in Figure 2-4. Note that the pseudo-deblended data,  $\mathbf{P}_{ps}$ , have the same size as  $\mathbf{P}$ .

## 2-2-2 Common Receiver Gather

In Figure 2-6a and 2-6b the interfering shot is coherent. By transforming the data to another domain, e.g. to the common receiver domain, the interfering shot becomes incoherent and is visible as spiky noise (see Figure 2-6c). Therefore, the interfering shot can be attenuated with a noise filter.

definition  
of inco-  
herency?

## 2-2-3 Iterative Estimation of Blending Noise

In an ideal case the noise generated by the interfering shots present in the pseudo-deblended data, the so called blending noise, is calculated with the unblended data,

$$\mathbf{N} = \mathbf{P}_{bl} \boldsymbol{\Gamma}^H - \mathbf{P} = \mathbf{P}_{ps} - \mathbf{P}. \quad (2-6)$$



**Figure 2-6:** Pseudo-deblended data,  $\mathbf{P}_{ps}$ , sorted in common shot gathers (a,b) and in a common receiver gather (c). The pseudo-deblended data of the right shot (a) and the left shot (b,c) were shifted by different time delays. The overlapping sources map in the pseudo-deblended shot gathers as coherent events, while they map as incoherent spikes in the pseudo-deblended receiver gather.

Obviously, in practice the unblended data are unknown and are estimated by adding extra constraints. The loop shown in Figure 2-5 applies the constraints to reduce the blending noise iteratively until the solution is obtained.

In the following all the quantities which are estimated are indicated with a hat. The steps of the iterative blending noise estimation are illustrated in Figure 2-7.

### f-k-Filtering

One of the constraints is coherency, i.e. by assuming the blending noise in Figure 2-7a is incoherent it can be removed. For this purpose the data are transformed from the space time to the wavenumber frequency domain where the spiky noise spreads over all wavenumber and frequency components (see Figure 2-7b, top).

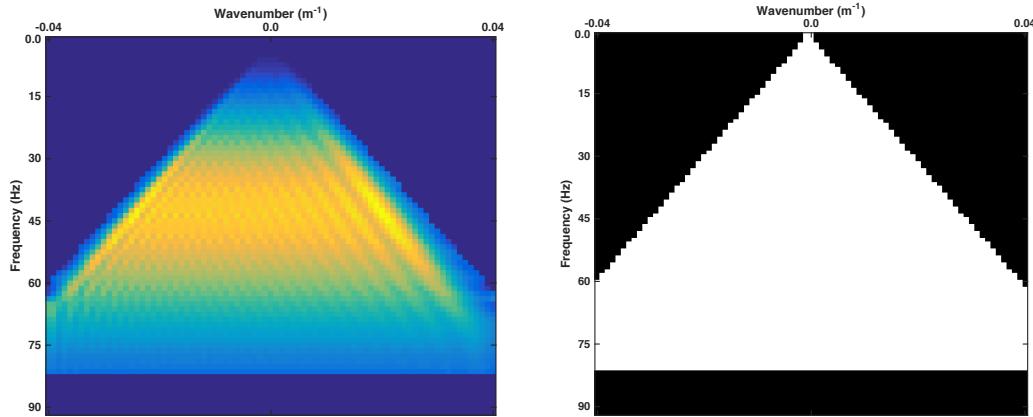
The unblended data would map in the *f-k*-domain in a cone (see Figure 2-8a). The minimum wavefield velocity present in the subsurface,  $v_{min}$ , determines the slope of the cone. This means that for a given frequency,  $f$ , the maximum wavenumber inside the cone,  $k_{max}$ , is defined as;

$$k_{max} = \frac{f}{v_{min}}. \quad (2-7)$$

In the marine case the minimum velocity is usually the water velocity,  $v_w = 1500 \text{ m s}^{-1}$ .



**Figure 2-7:** (a) Pseudo-deblended receiver gather. The subfigures (b)-(f) illustrate each step of the deblending algorithm. For better visibility examples from the 5<sup>th</sup> iteration are chosen. (b)  $f\text{-}k$ -spectrum before (top) and after (bottom)  $f\text{-}k$ -filtering, (c)  $f\text{-}k$ -filtered common receiver gather, (d) after thresholding, (e) estimated blending noise, (f) estimated data.



(a)  $f\text{-}k$ -spectrum of an unblended common shot gather.

(b) The  $f\text{-}k$ -mask is determined by the minimum signal velocity in the subsurface. The white area of the filter equals one, the black area equals zero. Thus, the filter removes data which are mapped outside of the white signal cone.

**Figure 2-8**

A 2D  $f\text{-}k$ -filter can be designed that removes all elements outside the cone (see Figure 2-8b). The  $f\text{-}k$ -filter removes the part of the blending noise, which maps outside of the signal cone (see Figure 2-7b). Thus, after transforming the data back to the space time domain the amplitudes of the spiky noise are attenuated (see Figure 2-7c).

Note that  $f\text{-}k$ -filtering can only reduce spatially unaliased blending noise. In Figure 2-8b the highest spatially unaliased frequency is defined by the point where the white cone intersects with the frequency axis, i.e. at 60 Hz. The spatially aliased blending noise will pass the  $f\text{-}k$ -filter and will be reduced afterwards by thresholding.

The high cut frequency of the  $f\text{-}k$ -mask,  $f_{cut} = 80$  Hz, is set according to the highest frequency components in the data.

### Thresholding

The second constraint for the estimation of the unblended data is sparsity of the signal in the space time domain.

After  $f\text{-}k$ -filtering the spiky noise is attenuated (see Figure 2-7c). Consequently, the signal amplitudes are now stronger than the noise amplitudes. This allows to define a threshold in the  $x\text{-}t$  domain, which is larger than the attenuated noise amplitudes and smaller than the highest signal amplitudes. Only amplitudes above the threshold are picked (see Figure 2-7d).

### Interference Estimation

The resulting thresholded data,  $\bar{\mathbf{P}}$ , is used to predict the blending noise;

$$\hat{\mathbf{N}}_i = \bar{\mathbf{P}} (\mathbf{\Gamma} \mathbf{\Gamma}^H - \mathbf{I}), \quad (2-8)$$

which is illustrated in Figure 2-7e.

### Blending Noise Subtraction

The estimate of the unblended data matrix  $\hat{\mathbf{P}}_i$  is updated by subtracting the estimated blending noise from the pseudo-deblended data,

$$\hat{\mathbf{P}}_{i+1} = \mathbf{P}_{ps} - \hat{\mathbf{N}}_i, \quad (2-9)$$

which is shown in Figure 2-7f.

This process is repeated iteratively till convergence is reached. In this context convergence can be defined as the point where the difference  $| \hat{\mathbf{P}}_{i+1} - \hat{\mathbf{P}}_i |$  drops below a predefined limit. Alternatively, one can set a maximum number of iterations.

Figure 2-9 shows the estimate of the unblended data for increasing iterations. At each iteration the blending noise is attenuated further, such that the threshold can be lowered. Hence, the predicted blending noise increases and approaches the true blending noise. The two blended shots are successively deblended.

Note that,  $f$ - $k$ -filtering lowers the noise level by removing spatially unaliased blending noise. Next, the lowered noise level enables thresholding to reduce spatially aliased blending noise. Thus, the combination of  $f$ - $k$ -filtering and thresholding is very powerful.



**Figure 2-9:** Common receiver gather of the estimated data after 1, 5, 10, 15, 20 and 25 iterations.

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# Chapter 3

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## Incoherency

In this chapter the blending operator is analyzed in greater detail. Then a measure for incoherency will be introduced. Finally, it will be discussed how deblending is influenced by incoherency and the so called maximum firing time delay.

### 3-1 Analysis of the Blending Matrix

In order to optimize the blended acquisition design, one must understand the properties of the blending matrix,  $\Gamma$ , and its influence on the deblending performance.

The blending matrix,  $\Gamma$ , determines the pseudo-deblended data,

$$\mathbf{P}_{ps} = \mathbf{P}\Gamma\Gamma^H, \quad (3-1)$$

which are a superposition of the unblended data,  $\mathbf{P}$ , and the blending noise,  $\mathbf{N}$ ,

$$\mathbf{P}_{ps} = \mathbf{P} + \mathbf{N} = \mathbf{P}\mathbf{I} + \mathbf{P}(\mathbf{\Gamma}\mathbf{\Gamma}^H - \mathbf{I}). \quad (3-2)$$

The more incoherent the blending noise,  $\mathbf{N}$ , the better it can be removed by noise filters.

In the following the effect of the blending matrix,  $\Gamma$ , on the pseudo-deblended data,  $\mathbf{P}_{ps}$ , is analyzed. For simplicity, it is assumed that all shots are equal in strength and fire the same signature into the earth. It is also assumed that each shot is fired only once, unlike e.g. the shot repetition case (Wu, 2014). This means that the blending matrix,  $\Gamma$ , only contains phase shift terms,  $e^{-j\omega\Delta t}$ , or zeros.

Each row of  $\Gamma$  represents a shot  $k$ , and each column of  $\Gamma^H$  represents a shot  $l$  with a complex conjugated phase term (see Figure 3-1). Hence, each element  $g_{kl}$  of the matrix  $\mathbf{\Gamma}\mathbf{\Gamma}^H$  is the dot product between the  $k^{th}$  shot and the complex conjugate of the  $l^{th}$  shot.

Consequently, an element  $g_{kl}$  of the matrix product,  $\mathbf{\Gamma}\mathbf{\Gamma}^H$ , represents the overlap of the shots  $k$  and  $l$  for all experiments. The main diagonal of  $\mathbf{\Gamma}\mathbf{\Gamma}^H$  refers to the overlap of each shot with

$$\begin{array}{c}
 \text{shot } k \\
 \left( \begin{array}{cc} e^{-j\omega\Delta t_i} & 0 \\ 0 & e^{-j\omega\Delta t_k} \\ e^{-j\omega\Delta t_j} & 0 \\ 0 & e^{-j\omega\Delta t_l} \end{array} \right) \cdot \left( \begin{array}{cccc} & & & \text{(shot)} \\ e^{+j\omega\Delta t_i} & 0 & e^{+j\omega\Delta t_j} & 0 \\ 0 & e^{+j\omega\Delta t_k} & 0 & e^{+j\omega\Delta t_l} \end{array} \right)_* = \left( \begin{array}{cccc} 1 & 0 & e^{-j\omega\Delta t_{ij}} & 0 \\ 0 & 1 & 0 & e^{-j\omega\Delta t_{kl}} \\ e^{-j\omega\Delta t_{ji}} & 0 & 1 & 0 \\ 0 & e^{-j\omega\Delta t_{lk}} & 0 & 1 \end{array} \right) \\
 \Gamma \qquad \qquad \qquad \Gamma^H \qquad \qquad \qquad \Gamma\Gamma^H
 \end{array}$$

**Figure 3-1:** Illustration of the matrix product,  $\Gamma\Gamma^H$ . In this notation  $\Delta t_k$  refers to the phase shift of the shot  $k$ , and  $\Delta t_{kl}$  refers to the phase shift between the shots  $k$  and  $l$ ,  $\Delta t_{kl} = \Delta t_k - \Delta t_l$ .

itself, which of course is perfect and therefore equal to 1. The off diagonal elements of  $\Gamma\Gamma^H$  are either 0 if the associated shots do not overlap, or contain a phase shift,  $e^{-j\omega\Delta t_{kl}}$ .

### Temporal incoherency

In the following the term "sub-diagonal" will be used to refer to an arbitrary diagonal of the matrix  $\Gamma\Gamma^H$ . For example, the  $d^{th}$  sub-diagonal includes all the matrix elements  $g_{ij}$ , which fulfill the condition;  $j - i = d$ .

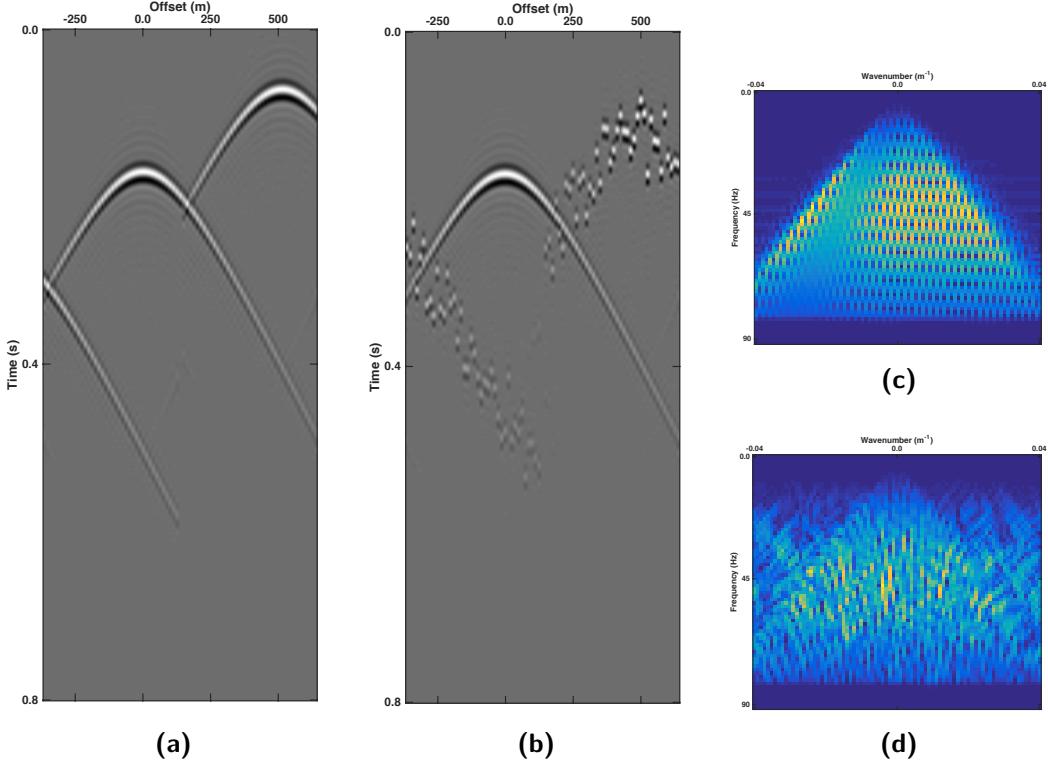
In equation 3-2 the main diagonal elements of  $\Gamma\Gamma^H$  copy the data matrix,  $\mathbf{P}$ , while the off-diagonal elements create the blending noise,  $\mathbf{N}$ . In case of constant firing time delays the elements along a sub-diagonal  $d$  all have the same phase. This means that the sub-diagonal elements will shift the columns of the data matrix and apply a constant phase shift to each of them resulting in the pseudo-deblended receiver gather shown in Figure 3-2a. Instead if firing times are not constant but random the elements  $g_{ij}$  along a sub-diagonal  $d$  will have different phases. Consequently, they will shift the columns of the data matrix and distort the phase of each column (see Figure 3-2b).

Figure 3-2c and 3-2d display the  $f$ - $k$ -spectra of the pseudo-blended data for constant firing time delays and random firing time delays respectively. In the case of constant firing time delays all of the energy maps in the signal cone. In the case of random firing time delays a significant part of the energy maps outside of the signal cone. From Figure 3-2c and 3-2d it is clear that the coherency constraint presented in section 2-2-3 cannot work with constant firing time delays, but needs the random firing time delays.

In this thesis the random firing time delays along a sub-diagonal are referred to as temporal incoherency.

### Spatial incoherency

Of course, the degree of incoherency of the blending noise,  $\mathbf{N}$ , also depends on whether the shot positions of shots blended in an experiment are selected randomly, or in a spatially coherent pattern. For example, one expects the blending noise to be more incoherent if in



**Figure 3-2:** Comparison of the pseudo-deblended receiver gather for (a) constant firing time delays of 100 ms, and (b) random firing time delays between 0 ms and 100 ms. (c) and (d) show the  $f$ - $k$ -spectra of (a) and (b) respectively.

$$\begin{array}{c}
 \begin{array}{|c|c|} \hline
 e^{-j\omega\Delta t_i} & 0 \\ \hline
 0 & e^{-j\omega\Delta t_k} \\ \hline
 0 & e^{-j\omega\Delta t_l} \\ \hline
 e^{-j\omega\Delta t_j} & 0 \\ \hline
 \end{array} \cdot \begin{array}{|c|c|c|c|} \hline
 & \text{shot } k & & \\ \hline
 & * & & \\ \hline
 e^{+j\omega\Delta t_i} & 0 & 0 & e^{+j\omega\Delta t_j} \\ \hline
 0 & e^{+j\omega\Delta t_k} & e^{+j\omega\Delta t_l} & 0 \\ \hline
 \end{array} = \begin{array}{|c|c|c|c|} \hline
 1 & 0 & 0 & e^{-j\omega\Delta t_{ij}} \\ \hline
 0 & 1 & e^{-j\omega\Delta t_{kl}} & 0 \\ \hline
 0 & e^{-j\omega\Delta t_{lk}} & 1 & 0 \\ \hline
 e^{-j\omega\Delta t_{ji}} & 0 & 0 & 1 \\ \hline
 \end{array} \\
 \Gamma \qquad \qquad \qquad \Gamma^H \qquad \qquad \qquad \Gamma \Gamma^H
 \end{array}$$

**Figure 3-3:** The blending matrix,  $\Gamma$ , is obtained by interchanging the 3<sup>rd</sup> and 4<sup>th</sup> row of the blending matrix in Figure 3-1. In acquisition this is equivalent to moving shot 3 to experiment 2, and shot 4 to experiment 1. A random permutation of the rows of the blending matrix spreads the off-diagonal elements of the matrix product,  $\Gamma \Gamma^H$ . The elements are not assembled on the sub-diagonals anymore.

each experiment randomly selected shot positions are blended as in Figure 3-3, than if in each experiment adjacent shot positions are blended as in Figure 3-1, because the interfering shots are spread over the sub-diagonals in Figure 3-3.

In this thesis selecting random shots for an experiment is referred to as spatial incoherency.

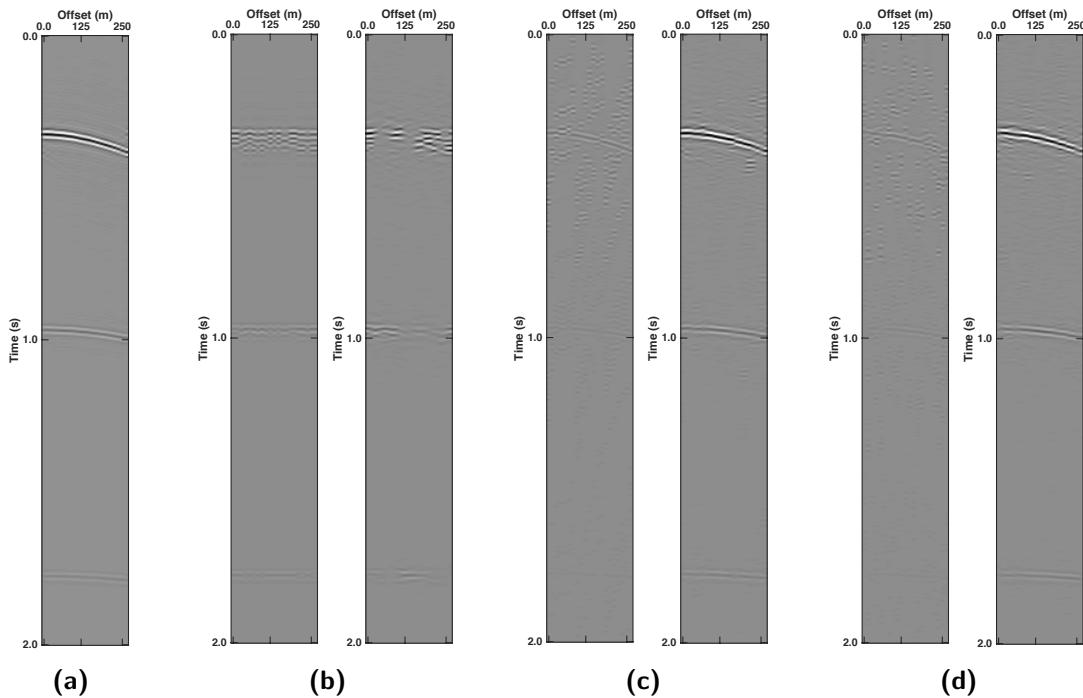
Although examples of spatial incoherency are shown in this chapter, it has to be noted that to blend shots in a spatially incoherent fashion is not very practical in 2D acquisition. However, in chapter 4 it will be shown that for 3D blending spatial incoherency becomes feasible.

## 3-2 Results Spatial and Temporal Incoherency

Based on the blending matrices in Figure 3-1 and 3-3 there are three possibilities to blend the shots incoherently. First, the phase terms along the sub-diagonals can be randomly varied, i.e. the shots are blended with random firing time delays (temporal incoherency). Second, the rows of the blending matrix can be randomly permuted, i.e. one randomly selects shots for each experiment (spatial incoherency). Third, temporal and spatial incoherency can be combined (mixed incoherency), i.e. randomly selected shots are blended with random firing time delays.

These 3 blending patterns are applied to a synthetic data set. The data are a common receiver gather with 21 shots (see Figure 3-4a), which are blended in 3 experiments with 7 shots per experiment. Next, the data are deblended with the deblending algorithm of section 2-2.

The deblended receiver gathers are shown in Figure 3-4. The results suggest that only spatial incoherency is not sufficient to deblend the data (see Figure 3-4b). By introducing random firing time delays the deblended data improve significantly as shown in Figure 3-4c. A combination of both spatial and temporal incoherency enhances the deblended data further (see Figure 3-4d).



**Figure 3-4:** (a) shows a synthetic unblended common receiver gather. The data are blended with a (b) spatially incoherent, (c) temporally incoherent, and (d) mixed incoherent blending pattern. The respective pseudo-deblended data (left) and deblended data (right) are shown in (b) to (d).

### 3-3 Effect of Incoherency

This section aims to analyze how strongly the deblending result depends on the incoherency of the blended acquisition. For this purpose a measure of incoherency and deblending quality will be introduced.

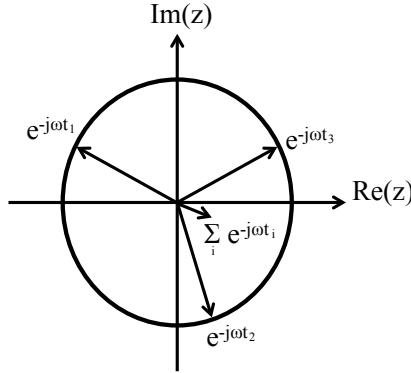
## Incoherency Measure

Move this sentence to the introduction (literature). You might also want to mention the work of the Greek guy Apostolos.

In this thesis only the incoherency of the acquisition design is considered. Thus, the blending matrix,  $\Gamma$ , or more precisely the product  $\boldsymbol{\Gamma}\boldsymbol{\Gamma}^H$  determines the incoherency.

In section 3-1 it was shown that for an incoherent blending pattern the elements,  $e^{-j\omega\Delta t_{kl}}$ , along a sub-diagonal of the matrix product,  $\mathbf{\Gamma}\mathbf{\Gamma}^H$ , should be out of phase. Therefore, the phase variability of the sub-diagonal elements will be used to quantify incoherency.

The sub-diagonal elements,  $e^{-j\omega\Delta t_{kl}}$ , map in the complex plane on a circle with radius 1 (see Figure 3-5). Thus, the sum of the elements along the  $d^{th}$  sub-diagonal can be constructive or destructive, depending on the phase variability. The absolute value of this sum,  $M(d, \omega)$ , measures the incoherency of the  $d^{th}$  sub-diagonal for the frequency component,  $\omega$ :



**Figure 3-5:** Illustration of the sub-diagonal elements in the complex number plane. The elements have unit length and variable phase. The absolute value of their sum depends on the phase coherency of the elements.

$$M(d, \omega) = \left| \sum_{j-i=d} \boldsymbol{\Gamma} \boldsymbol{\Gamma}_{ij}^H(\omega) \right|. \quad (3-3)$$

If all sub-diagonal elements are in phase the absolute value of their sum,  $M(d, \omega)$ , is maximized. Instead, in case of an incoherent blending pattern  $M(d, \omega)$  is small for all sub-diagonals  $d$ , except for the main diagonal ( $d = 0$ ).

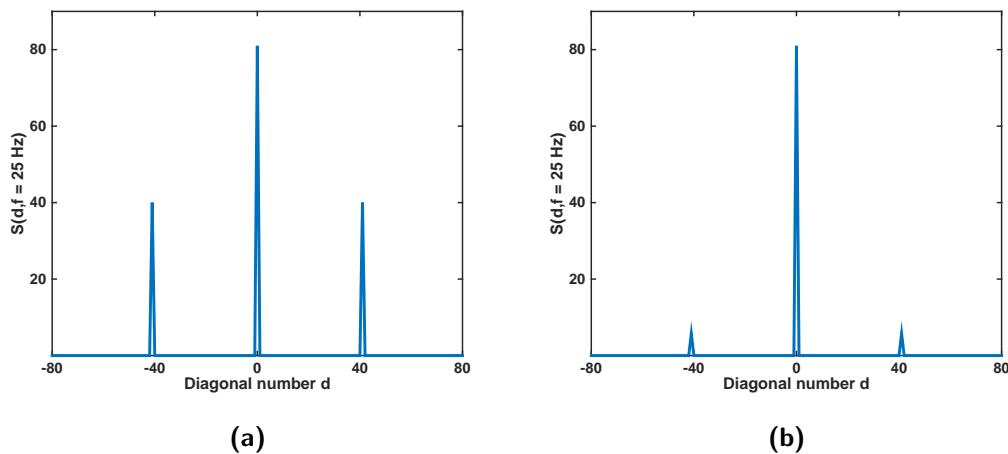
The incoherency measure,  $\mu$ , is introduced as;

$$\mu = \frac{(\sum_{\omega} M(d=0, \omega))^2}{\sum_{d=1-N_s}^{N_s-1} ((\sum_{\omega} M(d, \omega))^2)}, \quad (3-4)$$

where  $N_s$  is the number of sources, i.e. the matrix  $\boldsymbol{\Gamma} \boldsymbol{\Gamma}^H$  has  $N_s$  rows and columns. Note that in this ratio, the numerator relates to the main diagonal only, and the denominator to all sub-diagonals.

Equation 3-4 implies that the incoherency value can vary between 0 (perfectly coherent) and 1 (perfectly incoherent).

For example, consider the two blending matrices,  $\boldsymbol{\Gamma}_{coh}$  and  $\boldsymbol{\Gamma}_{ran}$ , which produce the pseudo-deblended receiver gathers in Figure 3-2a and 3-2b respectively. The blending matrix,  $\boldsymbol{\Gamma}_{coh}$ , uses constant firing time delays, while the blending matrix,  $\boldsymbol{\Gamma}_{ran}$ , uses random firing time delays. Figure 3-6 shows  $M(d, \omega)$  for both blending matrices for the frequency slice  $f = 25$  Hz. One can observe that for the incoherent blending matrix,  $\boldsymbol{\Gamma}_{ran}$ ,  $M(d, \omega)$  resembles a simple spike more than for the coherent blending matrix,  $\boldsymbol{\Gamma}_{coh}$ . The coherent blending matrix,  $\boldsymbol{\Gamma}_{coh}$ , yields an incoherency value of  $\mu_{coh} = 67\%$ , whereas the incoherent blending matrix,  $\boldsymbol{\Gamma}_{ran}$ , yields an incoherency value of  $\mu_{ran} = 98\%$ .



**Figure 3-6:** Illustration of the absolute sub-diagonal sums,  $M(d, \omega)$ , for the frequency slice  $f = 25$  Hz. (a) refers to the blending matrix  $\Gamma_{coh}$  with constant firing time delays. (b) refers to the blending matrix  $\Gamma_{ran}$  with random firing time delays.

## Deblending Performance Measure

The following data examples are synthetic data, i.e. the unblended data are known. Therefore, the deblending performance can be measured with the quality factor,  $Q$ , which is defined by Ibrahim and Sacchi (2015) as;

$$Q = 10 \cdot \log_{10} \left( \frac{\| \mathbf{P} \|_2^2}{\left\| \mathbf{P} - \hat{\mathbf{P}} \right\|_2^2} \right), \quad (3-5)$$

where  $\mathbf{P}$  are the unblended data, and  $\hat{\mathbf{P}}$  the deblended data. This is similar to the definition of signal to noise ratio.

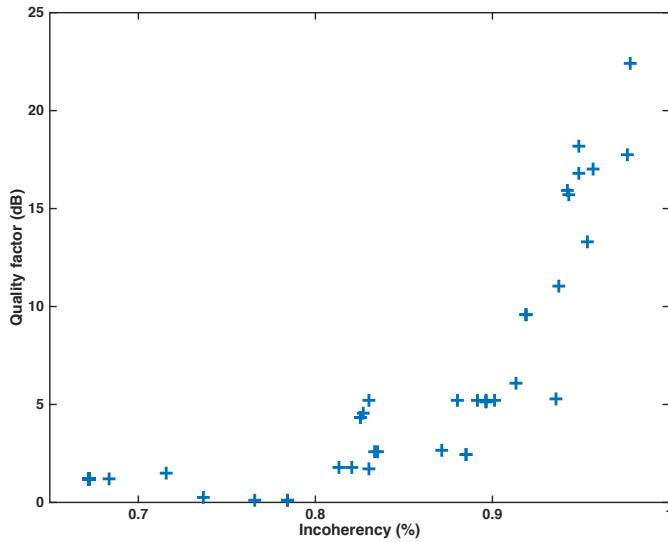
### 3-4 Results Incoherency

Consider again the two blending matrices,  $\boldsymbol{\Gamma}_{coh}$  and  $\boldsymbol{\Gamma}_{ran}$ , which produced the pseudo-deblended receiver gathers in Figure 3-2a and 3-2b respectively. Both blending matrices use the same maximum firing time delay, while their incoherency values differ ( $\mu_{coh} = 67\%$ ,  $\mu_{ran} = 98\%$ ).

An effective blending matrix,  $\boldsymbol{\Gamma}_{eff}$ , is created by superimposing the time delays  $e^{-j\omega\Delta t_{ij}}$  of the blending matrices  $\boldsymbol{\Gamma}_{coh}$  and  $\boldsymbol{\Gamma}_{ran}$ ;

$$\Delta t_{eff} = a \cdot \Delta t_{ij,ran} + (1 - a) \cdot \Delta t_{ij,coh}, \quad a \in [0, 1]. \quad (3-6)$$

The maximum firing time delay of the effective blending matrix,  $\mathbf{\Gamma}_{eff}$ , is constant while the incoherency varies with changing  $a$ . The resulting quality factors are shown as a function of the incoherency in Figure 3-7.



**Figure 3-7:** Deblending quality as a function of incoherency for a constant maximum firing time delay.

One can observe that the deblending quality increases with increasing incoherency.

### 3-5 Effect of Maximum Firing Time Delay

Another control factor of the deblending quality is the maximum firing time delay. In an extreme case of infinitely long maximum firing time delay the acquisition is not blended any more, and the deblending result is perfect. Hence, increasing maximum firing time delays are expected to enhance the deblending quality. Of course, they require more acquisition time.

### 3-6 Results Maximum Firing Time Delay

The three suggested blending patterns namely temporal, spatial and mixed incoherency are applied to synthetic data with varying maximum firing time delays.

Figure 3-8 shows the quality factors for the three blending patterns as a function of maximum firing time delay. Note that for a fixed maximum firing time delay and a specific blending pattern the firing time delays are generated with a random number generator. Consequently, the resulting quality factor varies depending on the variation of the random number series. For this reason several blending matrices are generated for each maximum firing time delay and each blending pattern. The resulting quality factors are averaged.

According to Figure 3-8 the spatially incoherent blending pattern yields a constant deblending quality independent of the maximum firing time delay. This is expected because it blends the sources without time delay. The deblending quality provided by the other two blending patterns continuously enhances with increasing maximum firing time delay. The difference in deblending quality between temporal and mixed blending patterns seems to be independent of the maximum firing time delay.



**Figure 3-8:** The 3 suggested blending patterns are simulated with maximum firing time delays between 40 ms and 400 ms. The quality factors are computed with respect to the unblended data and illustrated as a function of the maximum firing time delay.

For the conclusion/discussion of these results:

Say that a high degree of incoherency is required for successful deblending, but it is not useful as a control factor of the deblending performance. Instead the maximum firing time delay allows to fine tune the quality factor and might be suitable to fine tune a trade off between deblending quality and acquisition time.

One can also say that the spatial incoherency performs poorly because its degree of incoherency is simply too low.

## 3-7 Conclusions

In practice, the maximum firing time delay is given by the available acquisition time. Figure 3-7 demonstrates that for a fixed maximum firing time delay the deblending quality can be optimized by choosing a blending pattern with maximum incoherency. The maximum achievable deblending quality for a fixed maximum firing time delay can be estimated from Figure 3-8.



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## Chapter 4

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# Crossline Deblending (3D)

This thesis suggests to blend crossline sources. By combining several cross-lines one effectively blends sources in 3D.

The deblending method of [Mahdad et al. \(2011\)](#) described in section [2-2](#) is designed for 2D blended data. In this chapter I will explain how each step of the Mahdad method can be applied to 3D data as well, and I will demonstrate its performance.

First, the data sorting will be modified such that the blended 3D data can be described using the same forward model as in section [2-1](#). The presented data sorting will allow to maintain all other steps of the deblending algorithm of [Mahdad et al. \(2011\)](#) unchanged. Second, the  $f\text{-}k$ -filter will be extended to an  $f\text{-}k_x\text{-}k_y$ -filter to remove noise in both crossline and inline direction.

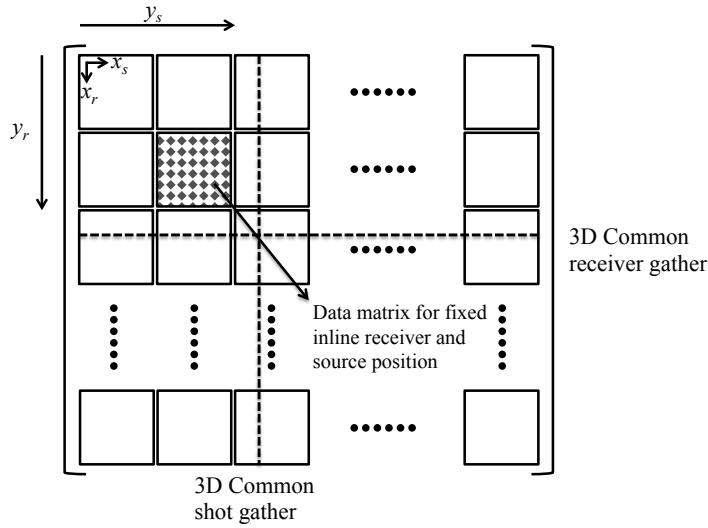
### 4-1 Data Sorting

#### Data Matrix

In 3D acquisition the sources and receivers are distributed on a 2D surface. Thus, their locations are defined by their crossline and inline positions,  $(x, y)$ . Each data point which is measured by a source receiver pair at a specific time is therefore described by 5 coordinates, time  $t$ , receiver crossline and inline position  $(x_r, y_r)$ , and source crossline and inline position  $(x_s, y_s)$ .

Similar as in section [2-1](#) the 5D data "cube" will be again reorganized in a 2D data matrix according to [van Dedem \(2002\)](#) (see Figure [4-1](#)). For this data sorting a 1D Fourier transform with respect to time is performed and a 4D frequency "slice" is selected.

The 4D "slice" is sorted in a 2D data matrix,  $\mathbf{P}$ , with as many rows as receivers and as many columns as shots. The total number of shots is obtained by multiplying the number of shots fired in each crossline and the number of shots fired in each inline. The total number of receivers is obtained likewise. Assume there are  $Ns_x$  shots per crossline. The shots of



**Figure 4-1:** Illustration of the data matrix  $\mathbf{P}$  for 3D data (van Dedem, 2002).  $y_r$  and  $y_s$  represent the inline receiver and shot positions.  $x_r$  and  $x_s$  represent the crossline receiver and shot positions. Each row refers to a 3D common receiver gather and each column to a 3D common shot gather. A sub-matrix with fixed receiver and source inline positions ( $y_r, y_s$ ) is equivalent to a data matrix for 2D acquisition.

the first crossline are assigned to the first  $Ns_x$  columns of the data matrix, the shots of the second crossline are assigned to the next  $Ns_x$  columns of the data matrix, etc. The receivers are sorted in the rows of the data matrix in analogy.

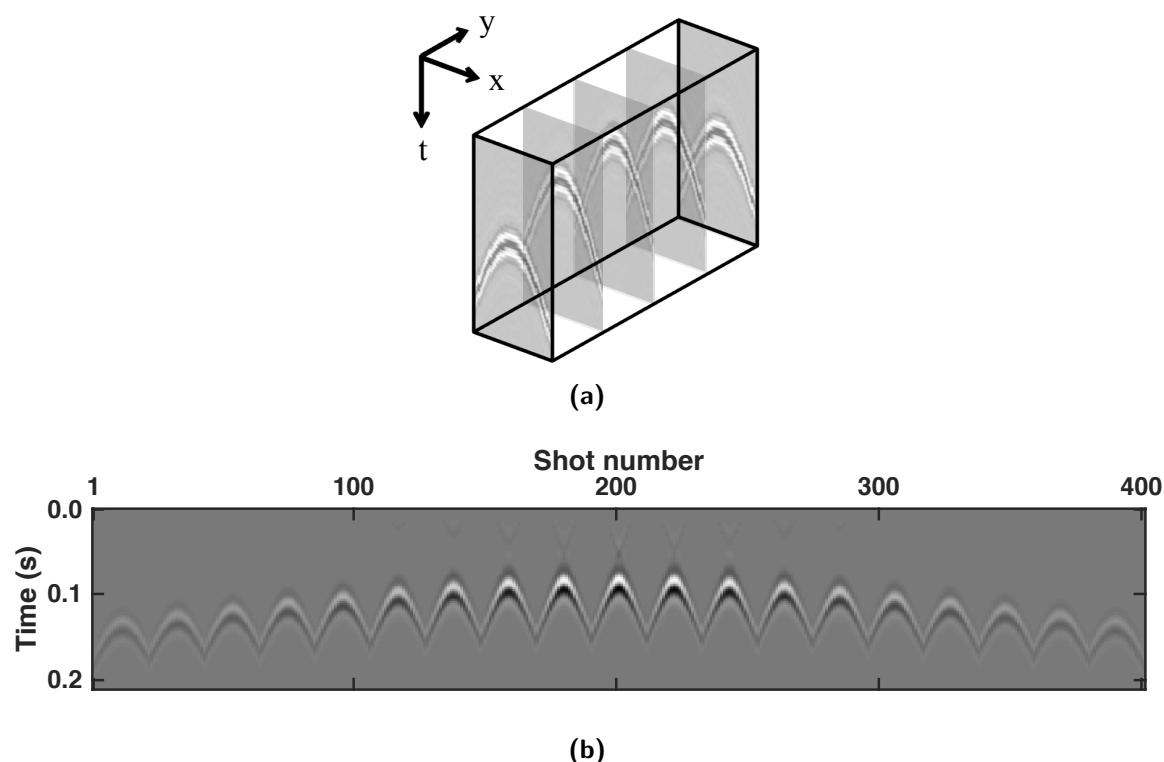
One row in the data matrix,  $\mathbf{P}$ , in Figure 4-1 represents a 3D common receiver gather. The data of this 3D common receiver gather are shown in Figure 4-2a in a 3D view, where the coordinates,  $x$  and  $y$ , indicate the crossline and inline shot position respectively. For the described data sorting individual crossline slices are extracted from this data cube and assembled next to each other in a data matrix as shown in Figure 4-2b. This view will be referred to as 3D CRG 2D view. Each hyperbolic event refers to the response of the shots of one crossline.

### Blending matrix

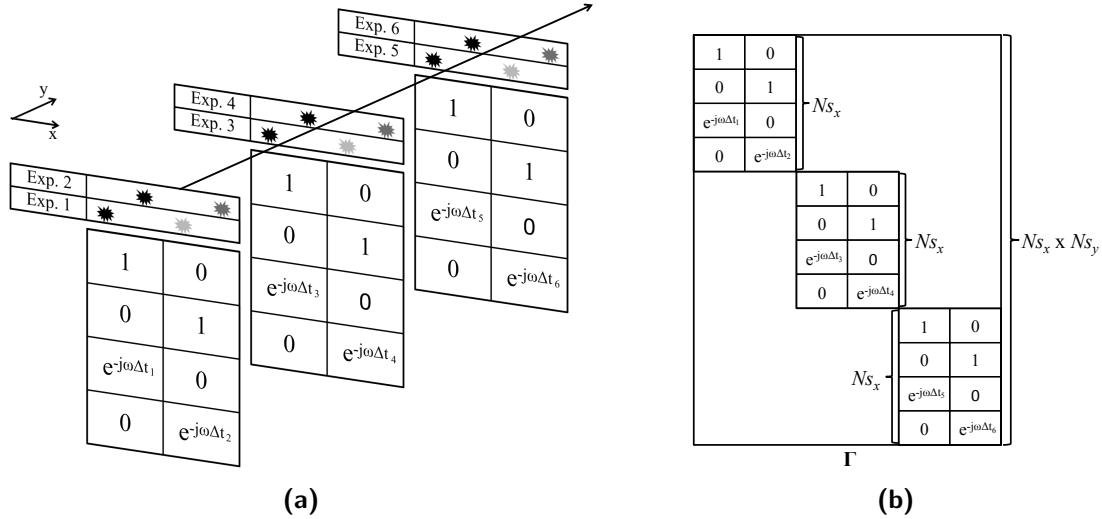
The blending matrix for 3D is build in a similar fashion as the data matrix in 3D. As described in section 3-1 each row of the blending matrix,  $\Gamma$ , captures one shot. For extension to 3D the shots of the first crossline are placed in the top  $Ns_x$  rows of the blending matrix, followed by the shots of the second crossline etc. (see Figure 4-3). The elements in the  $j^{th}$  column of the blending matrix,  $\Gamma$ , select the shots which are blended in the  $j^{th}$  experiment. For example, the first column of the blending matrix in Figure 4-3b describes that in the first experiment shots (rows) 1 and 3 are blended with a time delay of  $\Delta t_1$ .

Keep this sentence for later: This framework allows to blend any source combination independent of the cross- and inline positions of the involved sources.

With the new data and blending matrix sorting one can apply deblending to 3D data in



**Figure 4-2:** (a) 3D common receiver gather with crossline ( $x$ ) and inline ( $y$ ) sources (3D view).  
(b) Resorted data set. Individual crossline sections are plotted next to each other in 2D. For visibility both subfigures only show a reduced part of the data. This view is called 3D CRG 2D view.



**Figure 4-3:** Illustration of the blending matrix,  $\Gamma$ , for 3D acquisition. (a) At each of the  $N_{s_y}$  inline position the crossline sources ( $x$  direction) are blended. Each of these 2D blending processes is described by a 2D blending matrix, which has as many rows as there are crossline sources,  $N_{s_x}$ . (b) The 2D blending matrices are assembled in a single 3D blending matrix,  $\Gamma$ , which has  $N_{s_x}$  by  $N_{s_y}$  rows.

the same way as presented in section 2-1 and section 2-2. Note that unlike for 2D blending spatially incoherent blending patterns are practical for 3D blended acquisition.

## 4-2 3D f-k-k Filter

In section 2-2-3 the 2D  $f$ - $k$  filter was introduced. In 3D there are two spatial directions ( $x, y$ ), i.e. the filter can be extended to a 3D  $f$ - $k_x$ - $k_y$  filter.

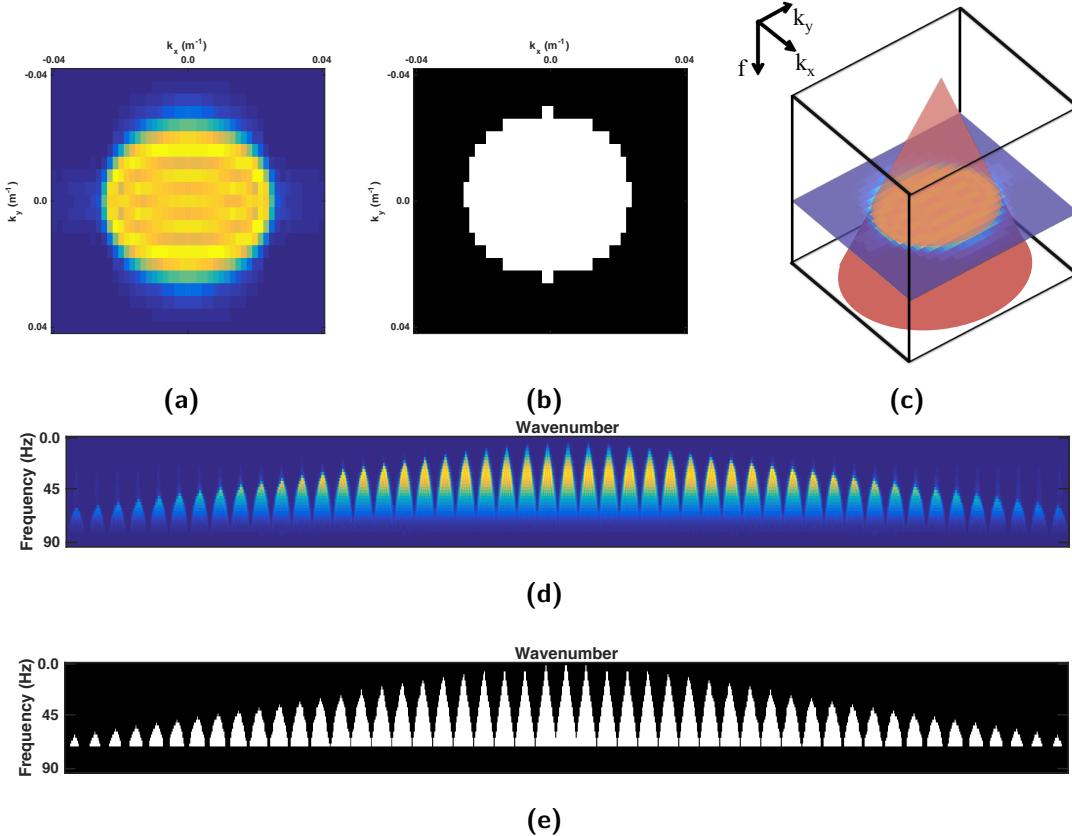
For this purpose one considers a 3D common receiver gather,  $\mathbf{p}(t, x_s, y_s)$ , and brings it to the  $f$ - $k_x$ - $k_y$  domain by applying a 3-dimensional Fourier transform. Next, a constant frequency slice is selected. This leaves a 2D matrix, which captures the crossline and inline wavenumbers ( $k_x, k_y$ ) as shown in Figure 4-4a. The minimum wavefield velocity,  $v_{min}$ , and the frequency,  $f$ , determine the maximum wavenumber,  $k_{max}$ , according to equation 2-7;

$$k_{max} = \frac{f}{v_{min}}. \quad (4-1)$$

The total wavenumber,  $k_T$ , must be smaller than the maximum wavenumber,  $k_{max}$ ,

$$k_T = \sqrt{k_x^2 + k_y^2} < k_{max}. \quad (4-2)$$

Hence the signal "cone" is defined by a circle (see Figure 4-4b). This is repeated for each frequency component, such that the overall  $f$ - $k_x$ - $k_y$  mask is a 3D cone (see Figure 4-4c). The cone can be sorted in a 2D view according to section 4-1 as illustrated in Figure 4-4d and Figure 4-4e. Finally, this mask is computed for each receiver gather.



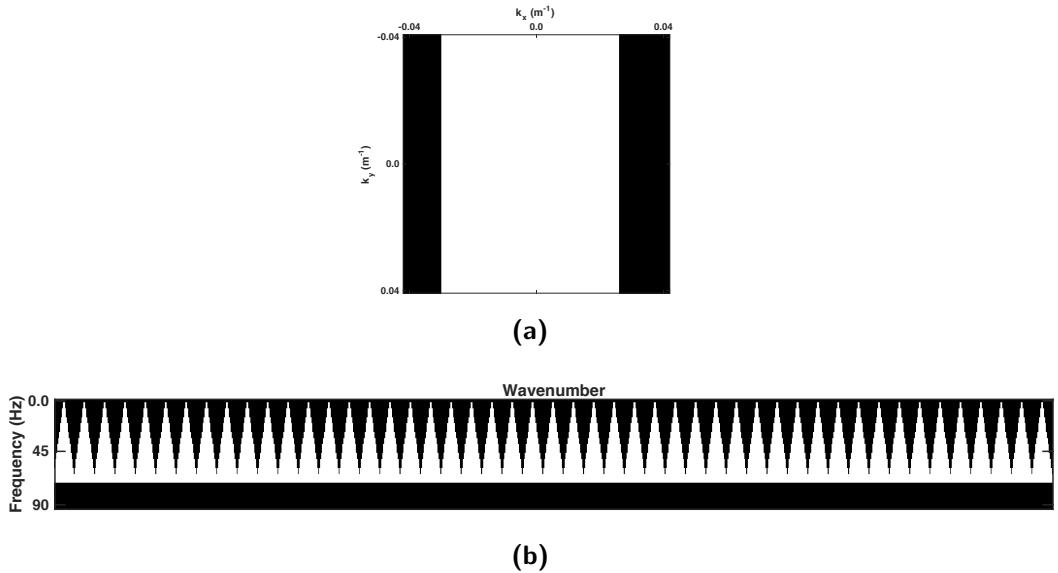
**Figure 4-4:** Illustration of the 3D  $f$ - $k_x$ - $k_y$ -filter. (a) is a 40 Hz frequency slice of the  $f$ - $k_x$ - $k_y$  spectrum of the data in Figure 4-2.  $k_x$  and  $k_y$  refer to the crossline and inline wavenumber respectively. (b) is a 40 Hz frequency slice of the  $f$ - $k_x$ - $k_y$  mask, where the white area equals 1 and the black area is 0. (c) shows the 40 Hz frequency slice of (a) sorted in a 3D cube. The red cone represents the edge of the 3D  $f$ - $k_x$ - $k_y$  filter mask. (d) and (e) display the  $f$ - $k_x$ - $k_y$  data spectrum and mask sorted according to section 4-1, i.e. each sub-cone refers to one inline wavenumber. Note that due to the sorting the wavenumber axis is a mix of crossline and inline wavenumbers. For this reason the wavenumber axis has no labels.

For comparison, a 2D  $f$ - $k$  filter is designed for 3D data and plotted in a 2D view in Figure 4-5. Note that the 3D  $f$ - $k_x$ - $k_y$  filter (see Figure 4-4) removes significantly more incoherent energy than the 2D  $f$ - $k$  filter.

### 4-3 Results

The 3D  $f$ - $k_x$ - $k_y$  filter removes incoherent energy in the crossline and inline direction. The 3D blended acquisition design suggested in this thesis blends shots within the same crossline. Hence, the underlying question is whether an extension of the 2D  $f$ - $k_x$  filter to the inline direction provides significant deblending enhancements.

For this purpose the synthetic data of Figure 4-6a are blended: Within each crossline there are 21 sources, which are blended in 3 experiments. For each experiment 7 randomly selected

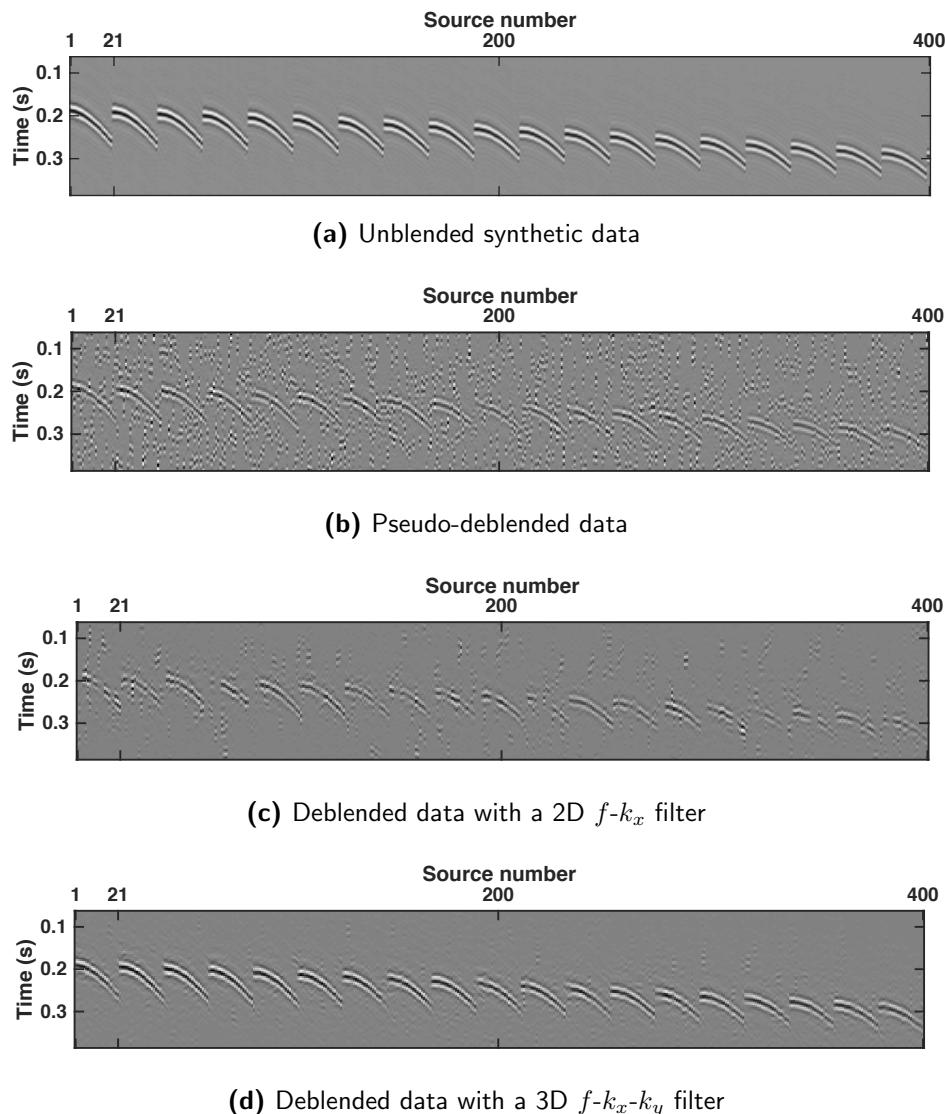


**Figure 4-5:** 2D  $f\text{-}k_x$ -filter for 3D data. (a) shows a 40 Hz frequency slice of the  $f\text{-}k_x\text{-}k_y$  spectrum, where the white area equals 1 and the black area is 0. Note that the filter is not affecting the inline wavenumbers  $k_y$ . (b) illustrates the 2D  $f\text{-}k_x$ -filter sorted according to section 4-1. Each cone represents a 2D  $f\text{-}k$ -filter for a single inline wavenumber.

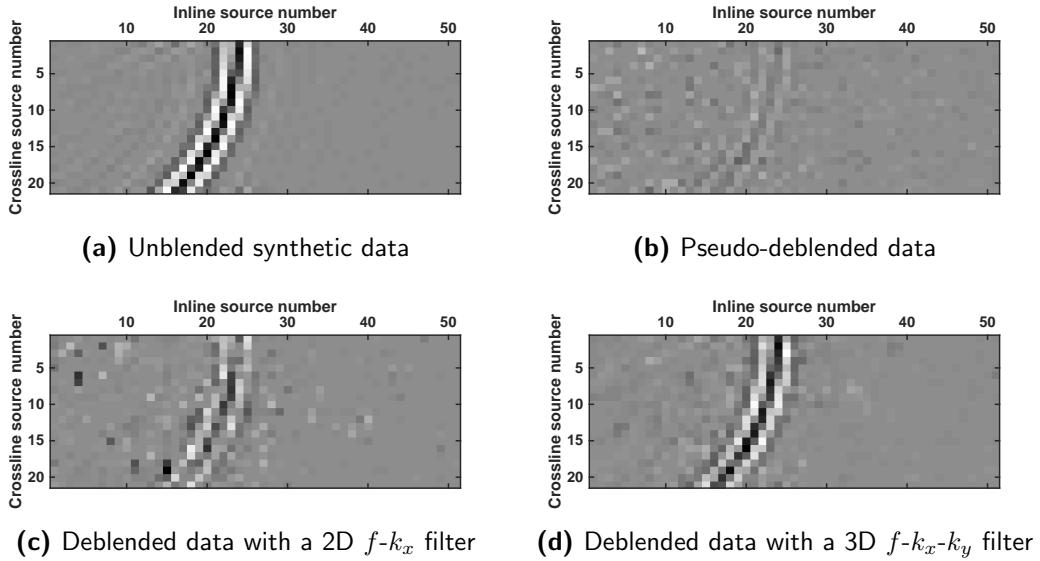
sources are blended with random time delays, i.e. the blending pattern with mixed incoherency is applied. The maximum allowed firing time delay is set to 400 ms. The incoherency measure of the used blending matrix,  $\Gamma$ , is  $\mu = 99\%$ .

The blended data are deblended with the 3D deblending algorithm. In one case a 2D  $f\text{-}k_x$  filter is applied (see Figure 4-6c). In the other case a 3D  $f\text{-}k_x\text{-}k_y$  filter is applied (see Figure 4-6d). It is clearly visible that the deblending quality increases significantly with the 3D  $f\text{-}k_x\text{-}k_y$  filter. Figure 4-7 displays a 420 ms time slice of each subplot in Figure 4-6.

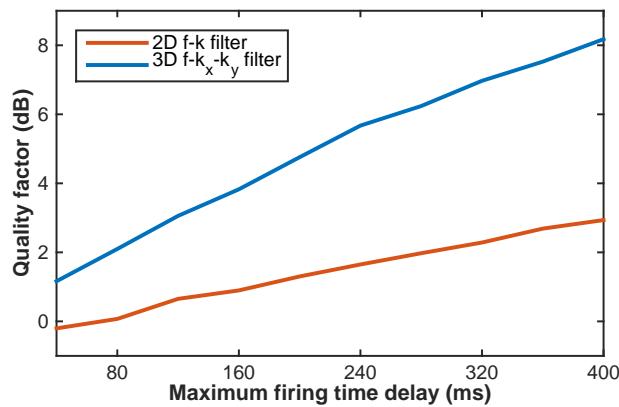
In order to quantify the quality gap between the results with 2D and 3D filters, the data of Figure 4-6a are blended with maximum firing time delays varying between 40 ms and 400 ms. The blended data are deblended in one case with a 2D  $f\text{-}k$  filter, and in the other case with a 3D  $f\text{-}k_x\text{-}k_y$  filter. The resulting quality factors are shown in Figure 4-8.



**Figure 4-6:** (a) is a synthetic 3D common receiver gather in 2D view. The data are generated by 21 crossline shots and 51 inline shots. The shown section is a zoom on the strongest events. Figure 3-4a shows one crossline of the data for all times. The data are blended with a mixed incoherency blending pattern. Then, the 3D deblending algorithm is applied. (b) shows the pseudo-deblended data. In case (c) the algorithm uses a 2D  $f-k_x$  filter. In case (d) it uses a 3D  $f-k_x-k_y$  filter.



**Figure 4-7:** (a) - (d) show 420 ms time slices of the data in Figure 4-6.



**Figure 4-8:** Comparison of the deblending quality with a 2D  $f\text{-}k_x$  filter and a 3D  $f\text{-}k_x\text{-}k_y$  filter. The data in Figure 4-6a are blended with varying maximum firing time delay. Then the blended data are deblended using a 2D  $f\text{-}k_x$  filter and a 3D  $f\text{-}k_x\text{-}k_y$  filter.

#### 4-4 Conclusions

The presented deblending method uses a coherency constraint. It has been demonstrated that for 3D deblending the quality of the deblended data can be enhanced significantly by extending the coherency constraint to crossline and inline direction.



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# Chapter 5

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## Results Field Data

The chapters 3 and 4 demonstrated the importance of an incoherent blending pattern and introduced 3D deblending. In the following, the presented deblending method is tested on a 3D complex data set. First, an incoherent blended acquisition set up is suggested. Second, the deblending results are presented and discussed.

### 5-1 Acquisition Set Up

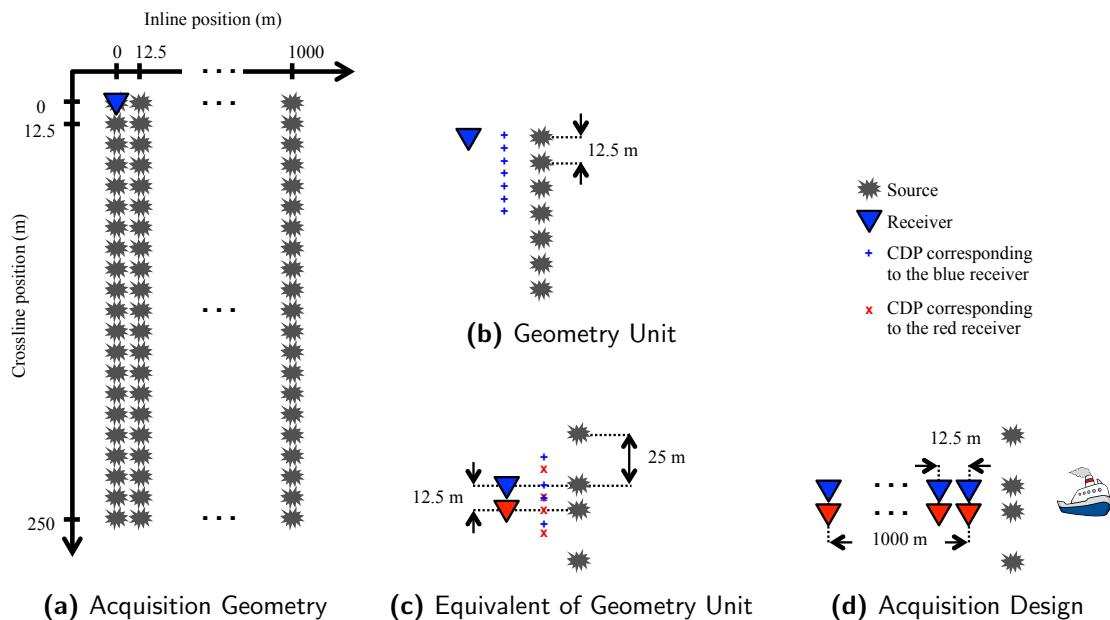
#### Geometry

The presented deblending method is applied to individual common receiver gathers. Thus, it is sufficient to test the method on a 3D CRG. In this example, the data are acquired with a source grid of 21 sources along crossline direction and 81 sources along inline direction as depicted in Figure 5-1a. The source spacing is 12.5 m in both directions and the receiver is placed in one corner of the source grid.

The sources in Figure 5-1a are fired crossline-wise, i.e. first all sources of crossline 1 are fired, next, all sources of crossline 2, etc. Hence, the acquisition set up can be build from a geometry unit as illustrated in Figure 5-1b.

In practice, densely-spaced crossline sources can be difficult to control, e.g. non linear effects start to occur. By introducing a second receiver, and by restructuring the geometry unit according to Figure 5-1c the crossline spacing can be doubled while the acquired common depth points (CDPs) remain unchanged. Thus, if the deblending method succeeds in deblending the geometry unit in Figure 5-1b it is also capable to deblend the equivalent geometry unit in Figure 5-1c.

Figure 5-1d illustrates how 3D blending can be realized. The crossline sources are blended at the first inline position and recorded by the first receiver pair from the right. Next, the crossline sources are blended at the second inline position and recorded by the second receiver pair from the right, etc. Note that in this thesis it is assumed that the crossline sources remain



**Figure 5-1:** The data example is acquired with the acquisition geometry (a). The sources are fired "crossline-wise", i.e. (a) can be built with a geometry unit (b). By adding a second receiver the geometry unit can be transformed to (c) without affecting the acquired common depth points. In practice the geometry unit (c) can be acquired as shown in (d).

at one inline position until all crossline sources are fired. Of course, this is not true in marine acquisition because the sources constantly move towards inline direction.

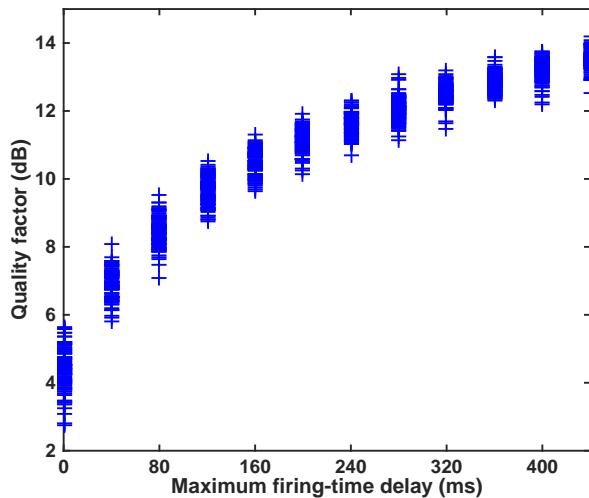
## Blending

An unblended common shot gather with the geometry of Figure 5-1a is extracted from an SEG seam data set. By applying reciprocity the common shot gather is converted to a common receiver gather. The crossline and inline spacing of the data is 50 m. This spacing is reduced to 12.5 m and the frequency components are increased accordingly. Figure 5-3a and 5-3d show an inline and crossline slice of the unblended data respectively. Note that the direct wave has been removed.

Each crossline of the unblended data is blended in 3 experiments with 7 sources per experiment. Assuming that the seismic vessel moves with a speed of  $1.2 \text{ m s}^{-1}$ , it moves from one inline position to the next within 10.4 s. Thus, given a recording time of 3 s per experiment the maximum firing-time delay can reach up 1.4 s for the 3 experiments, which is equivalent 467 ms per experiment.

## 5-2 Deblending Results

Chapter 3 demonstrated that among the 3 presented blending patterns the one with mixed incoherency yields the best deblending results. Thus, the data are blended in an mixed

**Figure 5-2**

incoherent fashion and the maximum firing-time delay is varied between 0 ms and 440 ms. The test is repeated 100 times with different random time delays and different random source permutations. Figure 5-2 shows the resulting quality factors as a function of maximum firing-time delays. Note that due to the repetition of the test the quality factors spread over about 3 dB.

In the following data example the maximum firing-time delay is set to 440 ms. From Figure 5-2 the random firing-time delays and random source permutations with maximum quality factor are chosen. The unblended, pseudo-deblended and deblended data are shown in Figure 5-3 and 5-4.

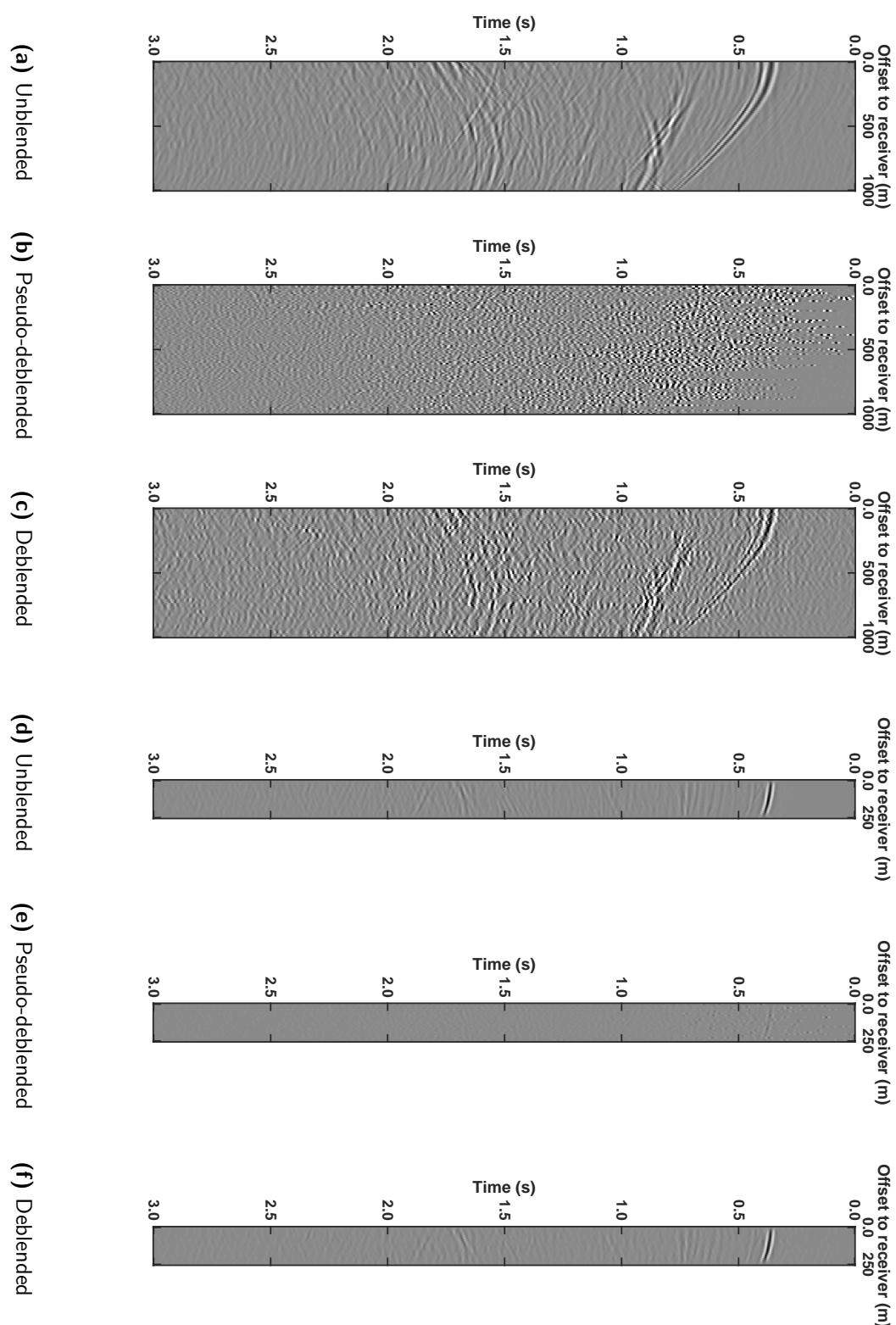
The shown deblended data have a quality factor of 14.2 dB and an incoherency value of 99.65 %. In case of the "worst" combination of random firing-time delays and random source permutation the quality factor is 12.5 dB and the incoherency value is 99.63 %.

### 5-3 Discussion

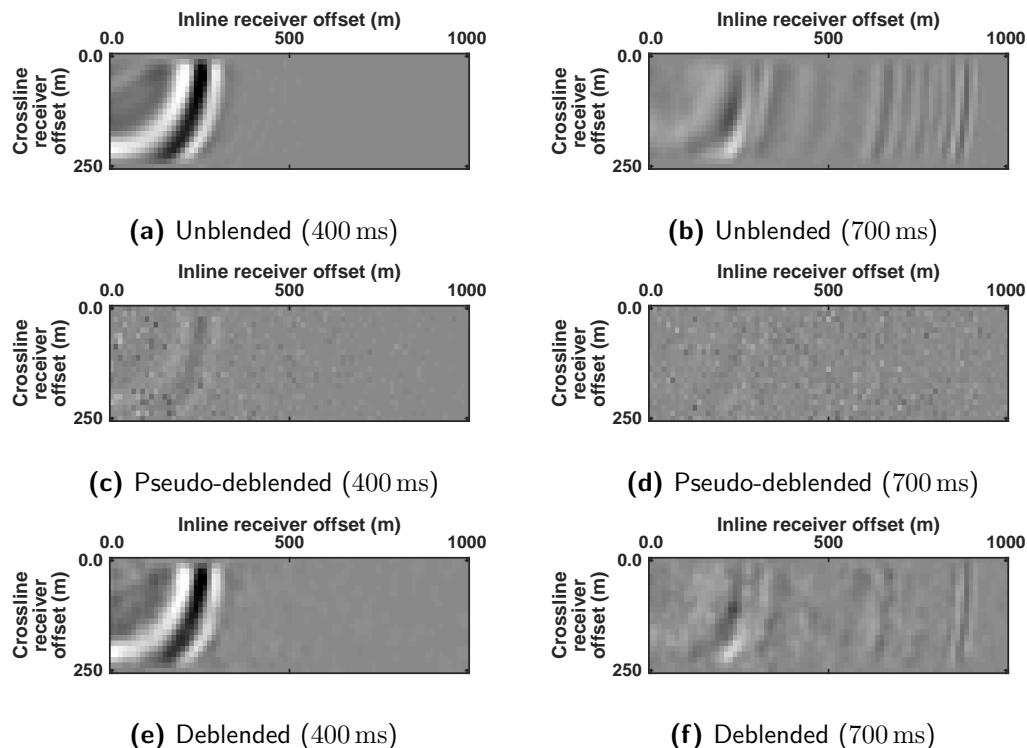
The deblending results in Figure 5-3 and 5-4 demonstrate that crossline deblending is feasible in a realistic set up. Comparing the unblended and deblended data one observes that the strong events are successfully deblended. However, the deblending result of the weak and late events is poor.

Figure 5-2 illustrates that for a given blending pattern and maximum firing-time delay the random firing-time delays and random source permutation should be designed to maximize the incoherency. Maximum incoherency will provide the maximum deblending quality.

As mentioned above the constant movement of the seismic vessel has not been taken into account. This correction can be implemented in future work. Due to the constant vessel movement a firing-time delay implies a change in the inline shot position. Thus, temporal and spatial incoherency will be linked to each other.



**Figure 5-3:** (a)-(c) show an inline slice of the unblended, pseudo-deblended and deblended data respectively. (d)-(f) show a crossline slice of the unblended, pseudo-deblended and deblended data respectively. The shown seismic sections are common receiver gathers.



**Figure 5-4:** Left column: 400 ms time slice of the (a) unblended, (c) pseudo-deblended and (e) deblended data. Right column: Equivalent of left column for a 700 ms time slice.

## 5-4 Conclusion

The complex data example demonstrates that 3D crossline deblending works. Before applying it in practice further work is required. In particular, the deblending of weak and late events must be improved. In addition, the movement of vessel must be included in the deblending method. As this movement adds an extra degree of incoherency to the blending pattern it is promising to enhance the deblending result.



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# Chapter 6

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## Conclusions and Discussion

### 6-1 Conclusions

The main conclusions of this thesis are:

- The deblending success is very sensitive to the blended acquisition design. The blending noise, or source interference, should be as incoherent as possible. This incoherency can be generated by random firing-time delays and by permuting the shot positions randomly. In addition, the maximum firing-time delay can be modified in order to adjust the deblending quality.
- This thesis presented a 3D deblending method, which takes advantage of; (1) a coherency constraint of the data in the  $f-k_x-k_y$  domain, and (2) a sparsity constraint of the data in the  $x-t$  domain. It was demonstrated that the coherency constraint in both crossline and inline direction performs significantly better in deblending than the coherency constraint in crossline direction only.
- The feasibility of the proposed 3D deblending method was validated with a field data example: 21 crossline sources were blended in 3 experiments. The maximum firing-time delay was set such that all shots are fired before they reach the next inline shot position. Only one blended acquisition design was tested, but in principle other designs are equally good as long as the blended shots are sufficiently incoherent.

### 6-2 Discussion

It was demonstrated that successful deblending depends on (1) the degree of incoherency, and (2) the maximum firing-time delay. These parameters are linked to each other because a longer maximum firing-time delay gives more freedom to generate incoherency. However, the two parameters affect the deblending quality very differently. The degree of incoherency influences

the deblending quality step-like (see Figure 3-7), i.e. either the incoherency is sufficiently high to deblend the data, or it is not and the deblending result is poor. The maximum firing-time delay shows an almost linear effect on the deblending quality (see Figure 3-8). Thus, the maximum firing-time delay allows to adjust the desired deblending quality.

In practice, the maximum firing-time delay will be defined by the schedule of the seismic survey. Hence, for a given maximum firing-time delay the blending pattern must be designed sufficiently incoherent to achieve the desired deblending quality. Of course, if the maximum firing-time delay is too short, it is not possible to achieve a sufficiently high degree of incoherency to deblend the data. In such a case the maximum-firing time delay must be increased.

In future work one could investigate further possibilities to generate incoherent blending noise. The degree of incoherency can be increased by introducing further degrees of freedom for the blending pattern. For example, the amplitudes of the blended shots can be varied randomly, several source vessel can be used in order to achieve more freedom for the random shot position permutation, or one can allow shot repetition as proposed by Wu (2014).

In this thesis it was assumed that the vessel stops at each inline shot position until all crossline sources are fired and recorded. For a practical realization the continuous vessel movement must be taken into account. This movement will increase the variation of the shot positions. Consequently, this correction is promising to increase the degree of incoherency further, which enhances the deblending quality.

The presented deblending method is performed in the common shot domain. Thus, a dense spatial source sampling is required. In future work one should try to overcome this restriction in order to build more incoherent blending patterns.

This thesis demonstrated that 3D crossline blending has potential to enhance seismic acquisition. From today's point of view 3D crossline blending is not sufficiently developed to be realized on an industry scale. However, in view of increasing challenges in seismic acquisition 3D crossline blending is promising to gain significant interest in the future.

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# Appendix A

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## The back of the thesis

### A-1 An appendix section

#### A-1-1 An appendix subsection with C++ Listing

```
//  
// C++ Listing Test  
//  
#include <stdio.h>  
for( int i=0;i<10;i++)  
{  
    cout << "Ok\n";  
}
```

1  
6

#### A-1-2 A Matlab Listing

```
%  
% Comment  
%  
n=10;  
for i=1:n  
    disp('Ok');  
end
```

5



---

## Appendix B

---

# Yet another appendix

### B-1 Another test section

Ok, all is well.



---

# Nomenclature

## Abbreviations

$\Delta t_{ij}$	Time delay of the $i^{th}$ source in the $j^{th}$ experiment
$\gamma_{ij}$	Element of the blending matrix $\Gamma$ corresponding to the $i^{th}$ source and the $j^{th}$ experiment
$\Gamma$	(Monochromatic) blending matrix as a function of source and experiment number
$\Gamma^H$	(Monochromatic) conjugate transpose of the blending matrix $\Gamma$ as a function of experiment and source number
$\Gamma_{coh}$	(Monochromatic) blending matrix with constant firing-time delays
$\Gamma_{eff}$	Linear superposition of the blending matrices $\Gamma_{coh}$ and $\Gamma_{ran}$
$\Gamma_{ran}$	(Monochromatic) blending matrix with random firing-time delays
$\mathbf{D}$	(Monochromatic) receiver matrix as a function of receiver number
$\mathbf{I}$	Identity matrix
$\mathbf{N}$	(Monochromatic) blending noise matrix as a function of receiver and source number
$\mathbf{P}$	(Monochromatic) data matrix as a function of receiver and source number
$\mathbf{p}$	3D data cube as a function of time, receiver coordinates, and source coordinates
$\mathbf{P}_{bl}$	(Monochromatic) blended data matrix as a function of receiver and experiment number
$\mathbf{P}_{ps}$	(Monochromatic) pseudo-deblended data matrix as a function of receiver and source number
$\mathbf{S}$	(Monochromatic) source matrix as a function of source number
$\mathbf{S}_{bl}$	(Monochromatic) blended source matrix as a function of source and experiment number
$\mathbf{X}$	(Monochromatic) earth impulse response matrix as a function of receiver and source number
$\mu$	Incoherency value of the blending matrix $\Gamma$
$\mu_{coh}$	Incoherency of the blending matrix $\Gamma_{coh}$
$\mu_{ran}$	Incoherency of the blending matrix $\Gamma_{ran}$

$\omega$	Circular frequency
$\bar{\mathbf{P}}$	(Monochromatic) data matrix after thresholding as a function of receiver and source number
$\hat{\mathbf{P}}_i$	(Monochromatic) data matrix prediction after $i$ iterations as a function of receiver and source number
$\hat{\mathbf{N}}_i$	(Monochromatic) blending noise prediction after $i$ iterations as a function of receiver and source number
$A_{ij}$	Amplitude of the element $\gamma_{ij}$ of the blending matrix $\mathbf{\Gamma}$
$f$	Frequency
$f_{cut}$	High cut frequency of the $f$ - $k$ mask
$g_{ij}$	Element of the matrix product $\mathbf{\Gamma}\mathbf{\Gamma}^H$ corresponding to the interference between the $i^{th}$ and $j^{th}$ source
$k$	Wavenumber in a 2D case
$k_T$	Total wavenumber
$k_x$	Crossline wavenumber in a 3D case
$k_y$	Inline wavenumber in a 3D case
$k_{max}$	Maximum wavenumber for a given frequency $f$
$M(d, \omega)$	(Monochromatic) absolute value of the sum along the $d^{th}$ sub-diagonal of the matrix product $\mathbf{\Gamma}\mathbf{\Gamma}^H(\omega)$
$N_s$	Total number of sources
$Ns_x$	Number of sources in crossline direction
$Ns_y$	Number of sources in inline direction
$Q$	Quality factor
$s_{ii}$	Diagonal element of the source matrix $\mathbf{S}$
$t$	Time
$v_w$	Seismic velocity in water
$v_{min}$	Minimum wavefield velocity present in the subsurface
$x$	Crossline space coordinate
$x_i$	Coordinates of the $i^{th}$ source
$x_r$	Receiver coordinates
$x_s$	Source coordinates
$y$	Inline space coordinate
CDP	Common depth point
CRG	Common receiver gather
CSG	Common shot gather