# Adapting the Chumbley Score to Bullet Striations

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# Objective and Motivation

- Same Source Matching of Bullet lands
- Evaluate performance of Chumbley Score method when used for Bullet Striations
- Bullet striations have curvature, not present in toolmarks
- ▶ Identify Error rates and effect of different parameters on them (In short finding the best error rates possible )

#### Structure

- Error rates in toolmarks
- Data being used
- What is the Chumbley Score Method?
- Identifying Best parameter Settings for Bullets
- ► Modifications to the Algorithm
- Results using Hadler and Morris [2017] method and results using Modified method

# Variations of Chumbley score method and Error Rates for toolmarks

Research paper	Method	Data Source	False Positives	False Negatives
Faden et al. [2007]	Maximized	Screwdrivers		
	Correlation		-	-
Chumbley et al. [2010]	Randomized	Screwdrivers		
(Same-Surface Same-Angle)	Chumbley Score		2.3%	8.9%
Grieve et al. [2014]	Randomized	Slip-joint		
	Chumbley Score		-	-
Hadler and Morris [2017]	Deterministic	Screwdrivers		
(Same-Surface Same-Angle)	Chumbley Score		0%	6%

Table 1: Error Rates for Toolmarks using variations of the chumbley score method

# Digitized Striation Marks

- Data
  - ▶ Ruger P85s Bullet Lands, or Hamby scans (Hamby et al. [2009]) provided by NIST (85,491 comparisons)
  - ▶ Bullet striation marks ≈ 2mm
  - lacktriangle Screwdriver marks pprox 7mm (all chumbley score papers)
- Let  $x(t_1)$ ,  $t_1 = 1, 2, ... T_1$  and  $y(t_2)$ ,  $t_2 = 1, 2... T_2$  be two digitized marks (where  $T_1$  and  $T_2$  are not necessarily equal).
- T<sub>1</sub> and T<sub>2</sub> are the final pixel indexes of each marking. Therefore give the respective lengths of the markings.
- ▶ Signatures/ Profiles (NIST- Hamby)  $\approx$  1200 pixels (2 mm) Screwdriver toolmarks (Chumbley Papers)  $\approx$  9000 pixels (7 mm)

# Chumbley Score

## Step 0 : Defining a coarseness parameter

- Used to remove drift and (sub)class characteristics from individual markings
- ► Lowess or Loess fit residuals = Signatures
- Removes topographic structure (curvature)
- ► Improve the signal to noise Ratio

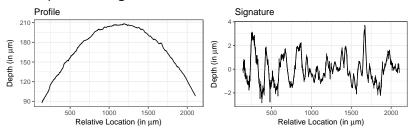


Figure 1: Bullet land profile (left) and the corresponding signature (right).

## Algorithm

- ▶ Two steps: Optimization  $(1^{st})$  and Validation  $(2^{nd})$ .
- ▶ Windows ⇒ short segments of the markings
  - ▶ Have predefined sizes.  $(T_1 \text{ or } T_2 >>> w_o \& w_v\$)$ 
    - 1. w<sub>o</sub> used in the Optimization step
    - 2.  $w_v$  used in the Validation step

## Optimization step

- ► **Goal** :Align markings horizontally as best as possible
- Correlation Matrix of all possible windows of size  $w_o$  between  $x(t_1)$  and  $y(t_2)$  computed
- ▶ Identify lag for horizontal alignment
  Window Pair with maximized correlation  $\Longrightarrow$ Optimal vertical (in-phase) shift of  $t_1^o t_2^o$ 
  - For aligning the two markings.  $(t^0, t^0) = \arg\max_{x \in \mathcal{X}} \operatorname{cor}(x^{w_0}(t_1))$

$$(t_1^o, t_2^o) = \underset{1 \le t_1 \le T_1, 1 \le t_2 \le T_2}{\operatorname{arg \, max}} \operatorname{cor}(x^{w_o}(t_1), y^{w_o}(t_2))$$

where  $t_1^o, t_2^0$  are the respective starting points of  $w_o$  in  $x(t_1)$  and  $y(t_2)$ 

- Let  $t_1^*$  and  $t_2^*$  be relative optimal locations, where  $t_i^* = t_i^o/(T_i w_o)$  for i = 1, 2, such that  $t_1^*, t_2^* \in [0, 1]$ .
- ➤ Once (sub-)class characteristics are removed, these locations have uniform distribution in [0,1]

## Validation Step

- Two sets of windows of size  $w_v$  chosen from both markings (see Figure 2)
- First set or Same Shift
  - **p** pairs of windows are extracted from the two markings using the optimal vertical shift.  $t_1^o t_2^o$
- Second set or Different Shift
  - the windows are extracted using a different (out-of-phase) shift.

# In-phase and Out-of-phase

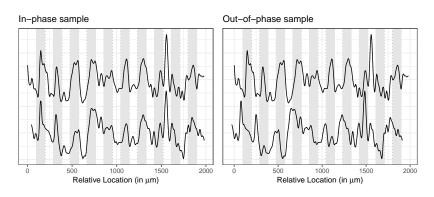


Figure 2: Two markings made by the same source. For convenience, the markings are moved into phase on the left and out-of phase on the right. In-phase (left) and out-of-phase (right) samples are shown by the light grey background. The Chumbley-score is based on a Mann-Whitney U test of the correlations derived from these two sets of samples.

- Both same- and different-shift pairs correlations between the markings are calculated.
- ► For Same-Source markings, correlations
  - ▶ for the in-phase shift should be high
  - for out-of-phase shift should be low.
    - Provide a measure for the base-level correlation to which in-phase shift correlations can be compared.
- The Chumbley score is the Mann Whitney U statistic computed by comparing between in-phase sample and out-of-phase sample.

# Block Diagram

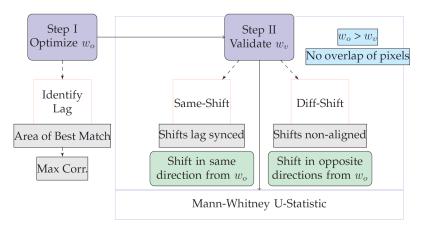


Figure 3: An overview of the adjusted chumbley score method as given by Hadler and Morris [2017]

# Starting Points

More precisely, let us define starting points of the windows of validation  $s_i^{(k)}$  for each marking k=1,2 as

$$s_i^{(k)} = \begin{cases} t_k^o + iw_v & \text{for } i < 0\\ t_k^o + w_o + iw_v & \text{for } i \ge 0, \end{cases}$$
 (1)

for integer values of i with  $0 < s_i^{(k)} \le T_k - w_v$  where  $s \in \mathbb{Z}$ 

# The Hadler and Morris [2017] method (CS1)

 $\triangleright$  Same-shift pairs of length  $w_V$  are all pairs that start in:

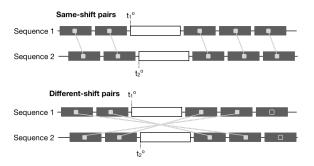
$$(s_i^{(1)}, s_i^{(2)}) \quad \forall i \in \mathbb{Z}$$

for which both  $s_i^{(1)}$  and  $s_i^{(2)}$  are defined.

▶ Different-shift pairs are defined as

$$(s_i^{(1)}, s_{-i-1}^{(2)}) \quad \forall i \in \mathbb{Z}$$

where both  $s_i^{(1)}$  and  $s_{-i-1}^{(2)}$  are defined (see fig. 4).



## Failed Tests

- By definition (equation 1), some number of tests fail to produce a result
- ► Either because the number of eligible same-shift pairs is 0, or the number of different-shift pairs is 0.
- $ightharpoonup t_1^o, t_2^o$  not necessarily independent
  - **> same-source:** Assume high dependence,  $corr(t_1^o, t_2^o) \approx 1$ 
    - Example:  $w_o = 120$ , coarseness (c) = 0.3,  $corr(t_1^o, t_2^o) = 0.85$
  - **diff-source:** Assume independence of  $t_1^o, t_2^o$ 
    - Example:  $w_o = 120$ , coarseness (c) = 0.3,  $corr(t_1^o, t_2^o) = 0.12$

#### Failure Rate

$$\begin{split} P\left(t_{1}^{o} < w_{v} \ \bigcap \ t_{2}^{o} > T_{2} - w_{o} - w_{v}\right) + \\ P\left(t_{1}^{o} < T_{1} - w_{o} - w_{v} \ \bigcap \ t_{2}^{o} < w_{v}\right). \end{split}$$

## Same-shift failure

- ► Same-source  $\approx 0$
- ▶ Different-source  $\approx 2 \ P(t_i < w_o)^2 = \frac{2w_v^2}{(T_1 w_o)(T_2 w_o)}$

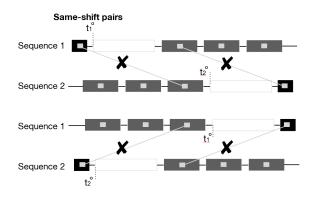


Figure 5: Sketch of same-shift pairings (top) when the lag is too large to accommodate a a vaildation window in either of the two signatures

## Different-Shift Failure

▶ Same-source (Assuming  $t_1^o \approx t_2^o$ )  $\approx 2w_v/(T_i - w_o)$ 

$$P(t_1^o < w_v \cap t_2^o < w_v) + P(t_1^o < w_v \cap t_2^o < w_v) = 2P(t_0^1 < w_v)$$

▶ Different-source  $\approx 2P(t_i < w_o)^2 = \frac{2w_v^2}{(T_1 - w_o)(T_2 - w_o)}$ 

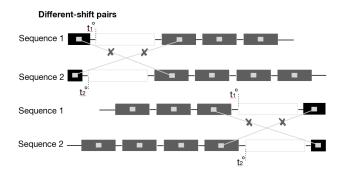


Figure 6: Sketch of diff-shift pairings (top) when the number of diff-shift computations is likely to 0

# **Proposed Modification**

- ▶ Failures due to missing Same-shift pairs unavoidable
- Failures due to missing different-shift pairs preventable

Define same-shift pairs identical to Hadler and Morris [2017] as pairs

$$(s_i^{(1)}, s_i^{(2)}) \quad \forall i \in \mathbb{Z}$$

where the boundary conditions of both sequences are met simultaneously.

- Let us assume that this results in *I* pairs.
- Let  $s_{(j)}^{(k)}$  to be the *j*th starting location in sequence k = 1, 2, i.e.  $s_{(1)}^{(k)} < s_{(2)}^{(k)} < ... < s_{(l)}^{(k)}$ .

We then define the pairs for different-shifts as

$$\left(s_{(j)}^{(1)},s_{(I-j+1)}^{(1)}\right) \text{ for } j = \begin{cases} 1,...,I & \text{for even } I \\ 1,...,(I-1)/2,(I-1)/2+2,...,I & \text{for odd } I \end{cases}$$
(2)

- ► For an odd number of same-shift correlations
  - ▶ We skip the middle pair for the different-shift correlations (see fig. 7).
- ► This pairing ensures that the number of different-shift pairings is the same or at most one less than the number of same-shift pairings in all tests.

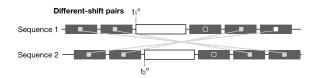


Figure 7: Sketch of adjusted different-shift pairings. At most one of the same-shift pairings can not be matched with a different-shift pair.

## Case where CS1 fails but CS2 does not fail

**CS1** Hadler and Morris [2017] algorithm **CS2** the suggested modified algorithm

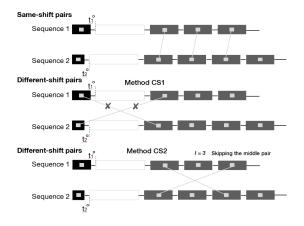


Figure 8: Sketch of a case where CS1 fails but CS2 does not fail

## Results Failed Tests

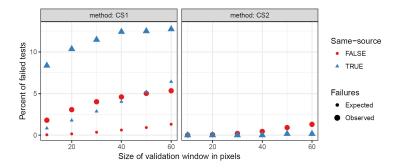


Figure 9: Percent of failed land-to-land comparisons for  $\it w_o=120$  and coarseness  $\it c=0.25$ 

## Conclusions Failed Tests

- ▶ With an increase in the  $w_v$  higher percent of tests fail under both CS1 and CS2
- Number is highly dependent on the comparison window sizes
- Correlated to the ground truth,
- Higher for known same-sourced lands (CS1) than for known different sourced lands.
- ► CS1 fails to conduct a test about 8 to 13 % of the time for known same-source lands, and 2 to 6% of the time for known different source lands.
- Number for CS1 always higher than the corresponding theoretical number of failed tests.
- Using CS2, the case with largest # of failed tests is still lower than the case where CS1 gives the lowest # of failed tests
- ► Even for high coarseness, CS2 will have lower number of failed tests than CS1, Making it more robust.
- CS2 performs better for both same and different-sources
- Solves a critical issue of CS1 known same-source matching, by having a negligible number of Known same-source failed tests

## Coarseness

- Remove (sub-)class characteristics from profiles before comparisons for matching.
- ► Hadler and Morris [2017] suggest a coarseness parameter of 0.25 for toolmark comparisons.
- ► For bullet lands, coarseness might need to be adjusted because of the strong effect bullet curvature has on profiles.
- Optimal locations are distributed uniformly once (sub-)class characteristics are removed.
- ▶ Distinct boundary effects: c > 0.20 optimal locations  $t^*$  are found at the very extreme ends of a profile more often than one would expect based on a uniform distribution. -smaller coarseness value of c = 0.15 to be suitable

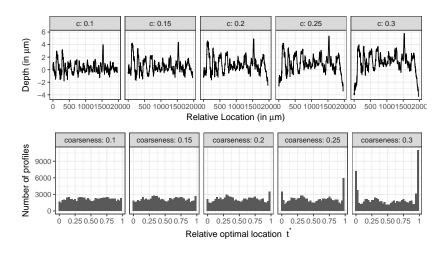


Figure 10: Overview of the effect of different coarseness parameters c on the profile shown in Figure 1 (top). The bottom row shows histograms of the (relative) optimal locations  $t^o$  identified in the optimization step for different values of the coarseness parameter c.

# Type II error rates

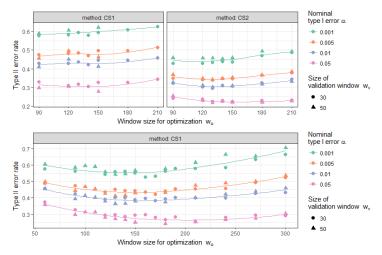


Figure 11: Type 2 error of methods CS1 and CS2 across a range of different optimization windows  $w_o$ . Top two figures are for a **coarseness**  $\approx 0.15$  and the bottom one is for 0.3

# Conclusions for Type II Error

#### CS1

- ▶ Best works best for  $w_o$  of  $\approx$  130 to 160 and  $w_v$  50 when the smoothing is  $c \approx 0.3$ .
- ▶ The Type II rate is lowest for a nominal  $\alpha$  of 5%, with type I error rate of 6.2% and the Type II error rate of 24%.
- For lower nominal alpha levels of 1%, 0.5% and 0.1% the lowest type II error rate increases to about 36.4%, 41% and 52.5% respectively.
- Gets worse for coarseness 0.15

## CS<sub>2</sub>

- Significantly reduced over CS1
- For a window size of  $w_o=130$  we see a minimum in type II error rate across all type I rates considered. Smaller validation sizes  $w_v$  are typically associated with a smaller type II error.
- ► CS2 shows an increase in the power of the test.
- ▶ Type II CS2, still much higher for bullet lands than for toolmarks.
- ► Fix in CS2 will also improve power for matching toolmarks thans CS1
- $\blacktriangleright$  Bullet-to-bullet comparison using CS2  $\approx$  more power out of the test.

## **ROC Curves**

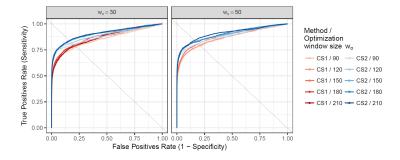


Figure 12: ROC curves of methods CS1 and CS2 for different sizes of optimization window  $w_o$ .

- Superior performance of CS2 over CS1
- ▶ Best performances wrt ROC curves are reached for  $w_0$  150 and higher.
- Points of equal error rates (EERs): intersection of the dotted line and the ROC curves.

# **THANK YOU. Questions?**

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