

# ECE 707: Control Systems Design (6)

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These viewgraphs are based on the text  
“Linear System: Theory and Design” by Chi-Tsong Chen  
Oxford University Press, 1999.

### Canonical Decomposition

Consider the state equation

$$\begin{aligned}\dot{\underline{x}} &= \underline{A}\underline{x} + \underline{B}\underline{u} \\ \underline{y} &= \underline{C}\underline{x} + \underline{D}\underline{u}\end{aligned}\tag{1}$$

Let  $\bar{\underline{x}} = \underline{P}\underline{x}$ , then an equivalent state equation is given by

$$\begin{aligned}\dot{\bar{\underline{x}}} &= \bar{\underline{A}}\bar{\underline{x}} + \bar{\underline{B}}\underline{u} \\ \bar{\underline{y}} &= \bar{\underline{C}}\bar{\underline{x}} + \bar{\underline{D}}\underline{u}\end{aligned}\tag{2}$$

where  $\bar{\underline{A}} = \underline{P}\underline{A}\underline{P}^{-1}$ ,  $\bar{\underline{B}} = \underline{P}\underline{B}$ ,  $\bar{\underline{C}} = \underline{C}\underline{P}^{-1}$ , and  $\bar{\underline{D}} = \underline{D}$ .

All properties of (1), such as controllability, observability are preserved in (2).

## Controllability

The new **controllability matrix** is given by

$$\begin{aligned}\bar{X} &= [\bar{B} \quad \bar{A}\bar{B} \quad \dots \quad \bar{A}^{n-1}\bar{B}] = [PB \quad PAP^{-1}PB \quad \dots \quad PA^{n-1}P^{-1}PB] \\ &= P[B \quad AB \quad \dots \quad A^{n-1}B] = PX\end{aligned}\quad (3)$$

The new **observability matrix** is given by

$$\bar{O} = \begin{bmatrix} \bar{C} \\ \bar{C}\bar{A} \\ \vdots \\ \bar{C}\bar{A}^{n-1} \end{bmatrix} = \begin{bmatrix} CP^{-1} \\ CP^{-1}PAP^{-1} \\ \vdots \\ CP^{-1}PA^{n-1}P^{-1} \end{bmatrix} = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix} P^{-1} = OP^{-1} \quad (4)$$

**Theorem:** Consider the  $n$  dimensional state equation in (1) with rank of controllability matrix

$$\rho(X) = \rho([B \ AB \ \cdots \ A^{n-1}B]) = n_1 < n \quad (5)$$

We form  $n \times n$  matrix (for **equivalence transform**)

$P^{-1} \triangleq [\underline{q}_1 \ \underline{q}_2 \ \cdots \ \underline{q}_{n_1} \ \cdots \ \underline{q}_n]$  where the first  $n_1$  columns are any  $n_1$  linearly independent columns of  $X$ , and the remaining columns are arbitrarily chosen to make  $P$  nonsingular.

Then the equivalence transform  $\underline{\bar{x}} = P\underline{x}$  gives

$$\begin{aligned} \begin{bmatrix} \dot{\underline{\bar{x}}}_c \\ \dot{\underline{\bar{x}}}_{\bar{c}} \end{bmatrix} &= \begin{bmatrix} \bar{A}_c & \bar{A}_{12} \\ 0 & \bar{A}_{\bar{c}} \end{bmatrix} \begin{bmatrix} \underline{\bar{x}}_c \\ \underline{\bar{x}}_{\bar{c}} \end{bmatrix} + \begin{bmatrix} \bar{B}_c \\ 0 \end{bmatrix} \underline{u} \\ \underline{y} &= [\bar{C}_c \ \bar{C}_{\bar{c}}] \begin{bmatrix} \underline{\bar{x}}_c \\ \underline{\bar{x}}_{\bar{c}} \end{bmatrix} + D\underline{u} \end{aligned} \quad (6)$$

where  $\bar{A}_c$  is  $n_1 \times n_1$  and the  $n_1$  dimensional subequation of (6)

$$\dot{\underline{\bar{x}}}_c = \bar{A}_c \underline{\bar{x}}_c + \bar{B}_c \underline{u} \quad \underline{y} = \bar{C}_c \underline{\bar{x}}_c + D\underline{u} \quad (7)$$

is observable and has the same transfer function as (6).

**Proof:** Since  $\bar{A} = PAP^{-1}$  and  $P^{-1} = [\underline{q}_1 \ \underline{q}_2 \ \cdots \ \underline{q}_{n_1} \ \cdots \ \underline{q}_n]$ , the  $i$ th column of  $\bar{A}$  is the representation of  $A\underline{q}_i$  w.r.t.  $\{\underline{q}_1 \ \underline{q}_2 \ \cdots \ \underline{q}_n\}$ .

To prove  $A\underline{q}_i$ , for  $i = 1, 2, \dots, n_1$ , are linearly dependent on the set  $\{\underline{q}_1 \ \underline{q}_2 \ \cdots \ \underline{q}_{n_1}\}$ , and independent of the set  $\{\underline{q}_{n_1+1} \ \underline{q}_{n_1+2} \ \cdots \ \underline{q}_n\}$ : For simplicity let  $B = \underline{b}$  (single column). The  $X = [\underline{b} \ A\underline{b} \ \cdots \ A^{n-1}\underline{b}]$ , or,  $X$  has  $n$  columns each of which is linear combination of  $\{\underline{q}_1 \ \underline{q}_2 \ \cdots \ \underline{q}_{n_1}\}$ .

Since  $A^n = c_0I + c_1A + \cdots + c_{n-1}A^{n-1}$  we have

$$\begin{aligned} AX &= [A\underline{b} \ A^2\underline{b} \ \cdots \ A^{n-1}\underline{b} \ A^n\underline{b}] \\ &= [A\underline{b} \ A^2\underline{b} \ \cdots \ A^{n-1}\underline{b} \ c_0\underline{b} + c_1A\underline{b} + \cdots + c_{n-1}A^{n-1}\underline{b}] \quad (8) \end{aligned}$$

This means any column of  $AX$  is linear combination of columns of  $X$ , i.e., linear combination of  $\{\underline{q}_1 \ \underline{q}_2 \ \cdots \ \underline{q}_{n_1}\}$ .

Since  $\{\underline{q}_1 \ \underline{q}_2 \ \cdots \ \underline{q}_{n_1}\}$  are columns of  $X$ , so  $A\underline{q}_i$ , for  $i = 1, 2, \dots, n_1$ , are linear combination of  $\{\underline{q}_1 \ \underline{q}_2 \ \cdots \ \underline{q}_{n_1}\}$  and independent of  $\{\underline{q}_{n_1+1} \ \underline{q}_{n_1+2} \ \cdots \ \underline{q}_n\}$ .

Same is true for any  $B$  (having multiple columns).

Thus  $i$  th column of  $\bar{A}$  for  $i = 1, 2, \dots, n_1$ , which is the representation of  $A\underline{q}_i$  w.r.t.  $\{\underline{q}_1 \ \underline{q}_2 \ \cdots \ \underline{q}_n\}$ , has  $n - n_1$  zero elements, or,

$$\bar{A} = \begin{bmatrix} \bar{A}_c & \bar{A}_{12} \\ 0 & \bar{A}_{\bar{c}} \end{bmatrix}$$

Now  $\bar{B} = PB$ , or the columns of  $\bar{B}$  are the representation of columns of  $B$  w.r.t.  $\{\underline{q}_1 \ \underline{q}_2 \ \cdots \ \underline{q}_n\}$ .

Now columns of  $B$  are independent of  $\{\underline{q}_{n_1+1} \ \underline{q}_{n_1+2} \ \cdots \ \underline{q}_n\}$ , hence  $\bar{B}$  has the following form

$$\bar{B} = \begin{bmatrix} \bar{B}_c \\ 0 \end{bmatrix}$$

The rank of controllability matrix of  $(\bar{A}, \bar{B})$  is given by

$$\begin{aligned} \rho(\bar{X}) &= \rho([\bar{B} \ \bar{A}\bar{B} \ \cdots \ \bar{A}^{n-1}\bar{B}]) \\ &= \rho\left(\begin{bmatrix} \bar{B}_c & \bar{A}_c\bar{B}_c & \cdots & \bar{A}_c^{n_1-1}\bar{B}_c & \vdots & \bar{A}_c^{n_1}\bar{B}_c & \cdots & \bar{A}_c^{n-1}\bar{B}_c \\ 0 & 0 & \cdots & 0 & \vdots & 0 & \cdots & 0 \end{bmatrix}\right) \\ &= \rho(X) = n_1 \end{aligned} \tag{9}$$

Since  $A_c$  is  $n_1 \times n_1$ , columns of  $A_c^k B_c$  for  $k \geq n_1$ , are linearly dependent on the columns of  $\bar{X}_c = [\bar{B}_c \ \bar{A}_c \bar{B}_c \ \cdots \ \bar{A}_c^{n_1-1} \bar{B}_c]$ , so

$$\rho(\bar{X}_c) = \rho(\bar{X}) = n_1 \quad (10)$$

Hence the pair  $(\bar{A}_c, \bar{B}_c)$  is controllable, or, the state equation (7) is controllable.

Next we show that state equations (6) and (7) have same transfer function.

We can show

$$\begin{bmatrix} sI - \bar{A}_c & -\bar{A}_{12} \\ 0 & sI - \bar{A}_{\bar{c}} \end{bmatrix}^{-1} = \begin{bmatrix} (sI - \bar{A}_c)^{-1} & M \\ 0 & (sI - \bar{A}_{\bar{c}})^{-1} \end{bmatrix} \quad (11)$$

where  $M = (sI - \bar{A}_c)^{-1} \bar{A}_{12} (sI - \bar{A}_{\bar{c}})^{-1}$ .

Thus the transfer matrix of (6) is

$$\begin{bmatrix} \bar{C}_c & \bar{C}_{\bar{c}} \end{bmatrix} \begin{bmatrix} sI - \bar{A}_c & -\bar{A}_{12} \\ 0 & sI - \bar{A}_{\bar{c}} \end{bmatrix}^{-1} \begin{bmatrix} \bar{B}_c \\ 0 \end{bmatrix} + D = \bar{C}_c (sI - \bar{A}_c)^{-1} \bar{B}_c + D$$

which is the transfer function of (7).

It can be seen from the equivalent state equation

$$\begin{bmatrix} \dot{\underline{\bar{x}}}_c \\ \dot{\underline{\bar{x}}}_{\bar{c}} \end{bmatrix} = \begin{bmatrix} \bar{A}_c & \bar{A}_{12} \\ 0 & \bar{A}_{\bar{c}} \end{bmatrix} \begin{bmatrix} \underline{\bar{x}}_c \\ \underline{\bar{x}}_{\bar{c}} \end{bmatrix} + \begin{bmatrix} \bar{B}_c \\ 0 \end{bmatrix} \underline{u}$$
$$\underline{y} = [\bar{C}_c \quad \bar{C}_{\bar{c}}] \begin{bmatrix} \underline{\bar{x}}_c \\ \underline{\bar{x}}_{\bar{c}} \end{bmatrix} + D\underline{u}$$

that the input  $\underline{u}$  can't control  $\underline{\bar{x}}_{\bar{c}}$ , since updated  $\underline{\bar{x}}_{\bar{c}}$  does not depend on  $\underline{u}$  directly or indirectly through  $\underline{\bar{x}}_c$ .

By dropping the uncontrollable states  $\underline{\bar{x}}_{\bar{c}}$ , we can obtain a controllable state equation

$$\begin{aligned} \dot{\underline{\bar{x}}}_c &= \bar{A}_c \underline{\bar{x}}_c + \bar{B}_c \underline{u} \\ \underline{y} &= \bar{C}_c \underline{\bar{x}}_c + D\underline{u} \end{aligned}$$

which has same transfer matrix.



**Example:** Consider the three dimensional state equation

$$\dot{\underline{x}} = \begin{bmatrix} 1 & 1 & 0 \\ 0 & 1 & 0 \\ 0 & 1 & 1 \end{bmatrix} \underline{x} + \begin{bmatrix} 0 & 1 \\ 1 & 0 \\ 0 & 1 \end{bmatrix} \underline{u} \quad y = [1 \ 1 \ 1] \underline{x}$$

Is the state equation controllable? If not find a controllable state equation that has same transfer function.

**Solution:** Since rank of  $B$  is 2; we can use  $X_2 = [B \ AB]$ , instead of  $X = [B \ AB \ A^2B]$  to check controllability. Here

$$\rho(X_2) = \rho([B \ AB]) = \rho\left(\begin{bmatrix} 0 & 1 & 1 & 1 \\ 1 & 0 & 1 & 0 \\ 0 & 1 & 1 & 1 \end{bmatrix}\right) = 2 < 3 \quad (12)$$

Hence the state equation is not controllable. We can choose

$$P^{-1} = \begin{bmatrix} 0 & 1 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}$$

Let  $\bar{x} = P\underline{x}$ . We compute

$$\begin{aligned}\bar{A} &= PAP^{-1} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & -1 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 \\ 0 & 1 & 0 \\ 0 & 1 & 1 \end{bmatrix} \begin{bmatrix} 0 & 1 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \\ &= \begin{bmatrix} 1 & 0 & \vdots & 0 \\ 1 & 1 & \vdots & 0 \\ \dots & \dots & \dots & \dots \\ 0 & 0 & \vdots & 1 \end{bmatrix} \\ \bar{B} &= PB = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & -1 \end{bmatrix} \begin{bmatrix} 0 & 1 \\ 1 & 0 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ \dots & \dots \\ 0 & 0 \end{bmatrix} \\ \bar{C} &= CP^{-1} = \begin{bmatrix} 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} 0 & 1 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} = \begin{bmatrix} 1 & 2 & \vdots & 1 \end{bmatrix}\end{aligned}$$

Hence the controllable state equation is given by

$$\dot{\underline{\bar{x}}}_c = \begin{bmatrix} 0 & 1 \\ 1 & 1 \end{bmatrix} \underline{\bar{x}}_c + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \underline{u} \quad y = \begin{bmatrix} 1 & 2 \end{bmatrix} \underline{\bar{x}}_c$$

**Theorem:** Consider the  $n$  dimensional state equation in (1) with rank of observability matrix

$$\rho(O) = \rho \left( \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix} \right) = n_2 < n \quad (13)$$

We form  $n \times n$  matrix (for equivalence transform)

$$P^{-1} \triangleq \begin{bmatrix} \underline{p}_1^T \\ \underline{p}_2^T \\ \vdots \\ \underline{p}_{n_2}^T \\ \vdots \\ \underline{p}_n^T \end{bmatrix} \quad (14)$$

where the first  $n_2$  rows are any  $n_2$  linearly independent rows of  $O$ , and the remaining rows are arbitrarily chosen to make  $P$  nonsingular. Then the equivalence transform  $\bar{x} = Px$  gives

$$\begin{aligned} \begin{bmatrix} \dot{\bar{x}}_o \\ \dot{\bar{x}}_{\bar{o}} \end{bmatrix} &= \begin{bmatrix} \bar{A}_o & 0 \\ \bar{A}_{21} & \bar{A}_{\bar{o}} \end{bmatrix} \begin{bmatrix} \bar{x}_c \\ \bar{x}_{\bar{c}} \end{bmatrix} + \begin{bmatrix} \bar{B}_o \\ \bar{B}_{\bar{o}} \end{bmatrix} \underline{u} \\ \underline{y} &= [\bar{C}_o \ 0] \begin{bmatrix} \bar{x}_o \\ \bar{x}_{\bar{o}} \end{bmatrix} + D\underline{u} \end{aligned} \quad (15)$$

where  $\bar{A}_o$  is  $n_2 \times n_2$  and the  $n_2$  dimensional subequation of (15)

$$\dot{\bar{x}}_o = \bar{A}_o \bar{x}_o + \bar{B}_o \underline{u} \quad \underline{y} = \bar{C}_o \bar{x}_o + D\underline{u} \quad (16)$$

is controllable and has the same transfer function as (15).

**Theorem:** Every state equation can be transformed, by an equivalence transform, into the following canonical form

$$\begin{bmatrix} \dot{\underline{x}}_{co} \\ \dot{\underline{x}}_{c\bar{o}} \\ \dot{\underline{x}}_{\bar{c}o} \\ \dot{\underline{x}}_{\bar{c}\bar{o}} \end{bmatrix} = \begin{bmatrix} A_{co} & 0 & A_{13} & 0 \\ A_{21} & A_{c\bar{o}} & A_{23} & A_{24} \\ 0 & 0 & A_{\bar{c}o} & 0 \\ 0 & 0 & A_{43} & A_{\bar{c}\bar{o}} \end{bmatrix} \begin{bmatrix} \underline{x}_{co} \\ \underline{x}_{c\bar{o}} \\ \underline{x}_{\bar{c}o} \\ \underline{x}_{\bar{c}\bar{o}} \end{bmatrix} + \begin{bmatrix} B_{co} \\ B_{c\bar{o}} \\ 0 \\ 0 \end{bmatrix} \underline{u}$$

$$\underline{y} = \begin{bmatrix} C_{co} & 0 & C_{\bar{c}o} & 0 \end{bmatrix} \underline{x} + D\underline{u} \quad (17)$$

where the vectors

- $\underline{x}_{co}$  is controllable and observable,
- $\underline{x}_{c\bar{o}}$  is controllable but not observable,
- $\underline{x}_{\bar{c}o}$  is observable but not controllable and
- $\underline{x}_{\bar{c}\bar{o}}$  is neither controllable nor observable.

Furthermore the state equation has same transfer matrix (or zero state equivalent) to the observable and controllable state equation

$$\begin{aligned} \dot{\underline{x}}_{co} &= A_{co}\underline{x}_{co} + B_{co}\underline{u} \\ \underline{y} &= C_{co}\underline{x}_{co} + D\underline{u} \end{aligned} \quad (18)$$

The corresponding transfer function is given by

$$G(s) = C_{co}(sI - A_{co})^{-1}B_{co} + D \quad (19)$$

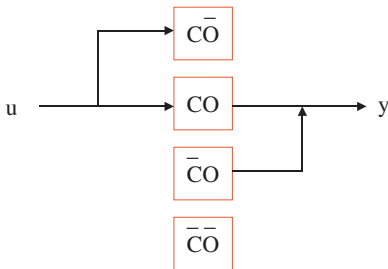


Fig. 8.1

Here we can see the reason why the transfer function description and the state-space description are not equivalent.

For example, if any portion of  $A$  matrix other than  $A_{co}$  has an eigenvalue with a positive real part, then the corresponding state variable will grow without bound and the system may burn out. This can't be detected from the transfer matrix.

**Example:** Consider circuit a shown in Fig. 8.2. Is it observable and controllable. If not find reduced state observable and controllable equation that has same transfer function.

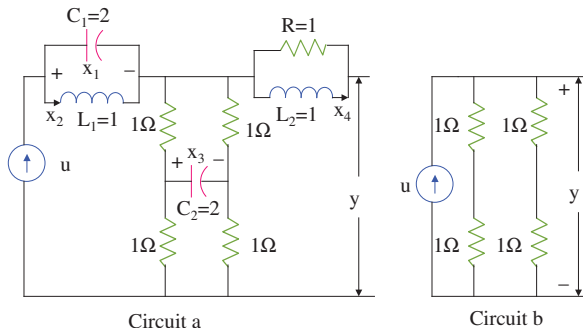


Fig. 8.2

**Solution:** By observation of the circuit we can say that initial state of  $L_1$  and  $C_1$  is not observable from the output. Also,  $L_2$  is not controllable by the input.

If we assign state variables as shown in circuit a of Fig. 8.2, the state equation is given by

$$\begin{aligned}\underline{\dot{x}} &= \begin{bmatrix} 0 & -0.5 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & -0.5 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix} \underline{x} + \begin{bmatrix} 0.5 \\ 0 \\ 0 \\ 0 \end{bmatrix} u \\ y &= [0 \ 0 \ 0 \ 1] \underline{x} + u\end{aligned}$$

Because the equation is already in the form of

$$\begin{aligned}\begin{bmatrix} \dot{x}_{co} \\ \dot{x}_{c\bar{o}} \\ \dot{\bar{x}}_{\bar{c}o} \\ \dot{\bar{x}}_{\bar{c}\bar{o}} \end{bmatrix} &= \begin{bmatrix} A_{co} & 0 & A_{13} & 0 \\ A_{21} & A_{c\bar{o}} & A_{23} & A_{24} \\ 0 & 0 & A_{\bar{c}o} & 0 \\ 0 & 0 & A_{43} & A_{\bar{c}\bar{o}} \end{bmatrix} \begin{bmatrix} x_{co} \\ x_{c\bar{o}} \\ \bar{x}_{\bar{c}o} \\ \bar{x}_{\bar{c}\bar{o}} \end{bmatrix} + \begin{bmatrix} B_{co} \\ B_{c\bar{o}} \\ 0 \\ 0 \end{bmatrix} \underline{u} \\ \underline{y} &= [C_{co} \ 0 \ C_{\bar{c}o} \ 0] \underline{x} + D \underline{u}\end{aligned}$$

it can be reduced to the following controllable state equation

$$\underline{\dot{x}}_c = \begin{bmatrix} 0 & -0.5 \\ 1 & 0 \end{bmatrix} \underline{x}_c + \begin{bmatrix} 0.5 \\ 0 \end{bmatrix} u \quad y = [0 \ 0] \underline{x}_c + u$$

The output is independent of  $\underline{x}_c$ , thus it can be further reduced to  $y = u$  (circuit b).



## Conditions in Jordan-Form Equations

We know controllability and observability are invariant under any equivalence transform.

The following discussion will show us that if a state equation is transformed to Jordan form, then the conditions for these properties become very simple.

Consider the state equation

$$\begin{aligned}\dot{\underline{x}} &= J\underline{x} + B\underline{u} \\ \underline{y} &= C\underline{x}\end{aligned}\tag{20}$$

where  $J$  is in Jordan form. We assume  $J$  to be having two distinct eigenvalues  $\lambda_1$  and  $\lambda_2$  and can be written as

$$J = \text{diag}(J_1, J_2)\tag{21}$$

where  $J_1$  and  $J_2$  consists of Jordan blocks associated with eigenvalue  $\lambda_1$  and  $\lambda_2$ , respectively.

Again let  $J_1$  and  $J_2$  can be decomposed in the following Jordan blocks

$$J_1 = \text{diag}(J_{11}, J_{12}, J_{13}) \quad J_2 = \text{diag}(J_{21}, J_{22}) \quad (22)$$

- The row of  $B$  corresponding to the last row of  $J_{ij}$  is denoted by  $\underline{b}_{lij}^T$ ,
- The column of  $C$  corresponding to the first column of  $J_{ij}$  is denoted by  $\underline{c}_{fij}$ .

**Theorem:** For the state equation discussed above

- The state equation is controllable if and only if the three row vectors  $\{\underline{b}_{l11}^T, \underline{b}_{l12}^T, \underline{b}_{l13}^T\}$  are linearly independent and the two row vectors  $\{\underline{b}_{l21}^T, \underline{b}_{l22}^T\}$  are linearly independent,
- The state equation is observable if and only if the three column vectors  $\{\underline{c}_{f11}, \underline{c}_{f12}, \underline{c}_{f13}\}$  are linearly independent and the two column vectors  $\{\underline{c}_{f21}, \underline{c}_{f22}\}$  are linearly independent.

**Proof:** For simplicity let us define

$$J = \begin{bmatrix} \lambda_1 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & \lambda_1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \lambda_1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \lambda_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \lambda_2 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & \lambda_2 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \lambda_2 \end{bmatrix} \quad (23)$$

Controllability condition can be obtained from the requirement that  $[sI - J \ B]$  must have full row rank for the state equation to be controllable. Here

$$[sI - J \ B] = \begin{bmatrix} s - \lambda_1 & -1 & 0 & 0 & 0 & 0 & 0 & \frac{b_{111}^T}{s - \lambda_1} \\ 0 & s - \lambda_1 & 0 & 0 & 0 & 0 & 0 & \frac{b_{112}^T}{s - \lambda_1} \\ 0 & 0 & s - \lambda_1 & 0 & 0 & 0 & 0 & \frac{b_{113}^T}{s - \lambda_1} \\ 0 & 0 & 0 & s - \lambda_1 & 0 & 0 & 0 & \frac{b_{121}^T}{s - \lambda_1} \\ 0 & 0 & 0 & 0 & s - \lambda_2 & -1 & 0 & \frac{b_{122}^T}{s - \lambda_2} \\ 0 & 0 & 0 & 0 & 0 & s - \lambda_2 & 0 & \frac{b_{123}^T}{s - \lambda_2} \\ 0 & 0 & 0 & 0 & 0 & 0 & s - \lambda_2 & \frac{b_{124}^T}{s - \lambda_2} \end{bmatrix} \quad (24)$$

For the eigenvalue  $\lambda_1$  we have

$$[\lambda_1 I - J B] = \begin{bmatrix} 0 & -1 & 0 & 0 & 0 & 0 & 0 & \underline{b}_{l11}^T \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \underline{b}_{l11}^T \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \underline{b}_{l12}^T \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \underline{b}_{l13}^T \\ 0 & 0 & 0 & 0 & \lambda_1 - \lambda_2 & -1 & 0 & \underline{b}_{l21}^T \\ 0 & 0 & 0 & 0 & 0 & \lambda_1 - \lambda_2 & 0 & \underline{b}_{l21}^T \\ 0 & 0 & 0 & 0 & 0 & 0 & \lambda_1 - \lambda_2 & \underline{b}_{l22}^T \end{bmatrix} \quad (25)$$

By elementary column operations we can show

$$\rho([\lambda_1 I - J B]) = \rho \left( \begin{bmatrix} 0 & -1 & 0 & 0 & 0 & 0 & 0 & \underline{0}^T \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \underline{b}_{l11}^T \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \underline{b}_{l12}^T \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \underline{b}_{l13}^T \\ 0 & 0 & 0 & 0 & \lambda_1 - \lambda_2 & 0 & 0 & \underline{0}^T \\ 0 & 0 & 0 & 0 & 0 & \lambda_1 - \lambda_2 & 0 & \underline{0}^T \\ 0 & 0 & 0 & 0 & 0 & 0 & \lambda_1 - \lambda_2 & \underline{0}^T \end{bmatrix} \right) \quad (26)$$

This shows us that the rows are independent iff  $\{\underline{b}_{l11}^T, \underline{b}_{l12}^T, \underline{b}_{l13}^T\}$  are linearly independent.

For the other eigenvalue  $\lambda_2$  we get

$$\rho([\lambda_2 I - J \quad B]) = \rho \left( \begin{bmatrix} \lambda_2 - \lambda_1 & 0 & 0 & 0 & 0 & 0 & 0 & \underline{0}^T \\ 0 & \lambda_2 - \lambda_1 & 0 & 0 & 0 & 0 & 0 & \underline{0}^T \\ 0 & 0 & \lambda_2 - \lambda_1 & 0 & 0 & 0 & 0 & \underline{0}^T \\ 0 & 0 & 0 & \lambda_2 - \lambda_1 & 0 & 0 & 0 & \underline{0}^T \\ 0 & 0 & 0 & 0 & -1 & 0 & 0 & \underline{0}^T \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \underline{b}_{l21}^T \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \underline{b}_{l22}^T \end{bmatrix} \right) \quad (27)$$

Hence for controllability we need  $\{\underline{b}_{l21}^T, \underline{b}_{l22}^T\}$  to be linearly independent.

Similarly for the state equation to be observable we need  $\begin{bmatrix} sI - J \\ C \end{bmatrix}$  to have full column rank for  $s = \lambda_1, \lambda_2$ . Here

$$\begin{bmatrix} sI - J \\ C \end{bmatrix} = \begin{bmatrix} s - \lambda_1 & -1 & 0 & 0 & 0 & 0 & 0 \\ 0 & s - \lambda_1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & s - \lambda_1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & s - \lambda_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & s - \lambda_2 & -1 & 0 \\ 0 & 0 & 0 & 0 & 0 & s - \lambda_2 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & s - \lambda_2 \\ c_{f11} & b_{211} & c_{f12} & c_{f13} & c_{f21} & c_{221} & c_{f22} \end{bmatrix} \quad (28)$$

For  $s = \lambda_1$  we have (after elementary row operations)

$$\rho \left( \begin{bmatrix} \lambda_1 I - J \\ C \end{bmatrix} \right) = \rho \left( \begin{bmatrix} 0 & -1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \lambda_1 - \lambda_2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & \lambda_1 - \lambda_2 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \lambda_1 - \lambda_2 \\ c_{f11} & \underline{0} & c_{f12} & c_{f13} & \underline{0} & \underline{0} & \underline{0} \end{bmatrix} \right) \quad (29)$$

For  $s = \lambda_2$  we have (after elementary row operations)

$$\rho \left( \begin{bmatrix} \lambda_2 I - J \\ C \end{bmatrix} \right) = \rho \left( \begin{bmatrix} \lambda_2 - \lambda_1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & \lambda_2 - \lambda_1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \lambda_2 - \lambda_1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \lambda_2 - \lambda_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \underline{0} & \underline{0} & \underline{0} & \underline{0} & \underline{c}_{f21} & \underline{0} & \underline{c}_{f22} \end{bmatrix} \right) \quad (3)$$

From last two equations it is clear that for  $\rho \left( \begin{bmatrix} sI - J \\ C \end{bmatrix} \right)$  to have full column rank we need the sets  $\{\underline{c}_{f11}, \underline{c}_{f12}, \underline{c}_{f13}\}$  and  $\{\underline{c}_{f21}, \underline{c}_{f22}\}$  to be linearly independent.

**Example:** Consider the Jordan form state equation

$$\begin{aligned}\dot{\underline{x}} &= \begin{bmatrix} \lambda_1 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & \lambda_1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \lambda_1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \lambda_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \lambda_2 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & \lambda_2 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & \lambda_2 \end{bmatrix} \underline{x} + \begin{bmatrix} 0 & 0 & 0 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \\ 1 & 1 & 1 \\ 1 & 2 & 3 \\ 0 & 1 & 0 \\ 1 & 1 & 1 \end{bmatrix} \underline{u} \\ \underline{y} &= \begin{bmatrix} 1 & 1 & 2 & 0 & 0 & 2 & 1 \\ 1 & 0 & 1 & 2 & 0 & 1 & 1 \\ 1 & 0 & 2 & 3 & 0 & 2 & 0 \end{bmatrix} \underline{x}\end{aligned}\quad (31)$$

Find if the state equation is controllable and observable.

**Solution:** The matrix  $J$  has two distinct eigenvalues  $\lambda_1$  and  $\lambda_2$ . There are three Jordan blocks, with order 2, 1, and 1 associated with  $\lambda_1$ . The rows of  $B$  corresponding to the last row of the Jordan blocks associated with  $\lambda_1$  are  $\{[1 \ 0 \ 0], [0 \ 1 \ 0], [1 \ 1 \ 1]\}$ . These three rows are linearly independent.



There is only one Jordan block of order 3 associated with  $\lambda_2$ . The row corresponding to the last row of Jordan block is  $[1 \ 1 \ 1]$ , which is nonzero, so linearly independent.

Hence the state equation is controllable.

The columns of  $C$  corresponding to first columns of Jordan blocks for  $\lambda_1$  are  $\{[1 \ 1 \ 1]', [2 \ 1 \ 2]', [0 \ 2 \ 3]'\}$  are linearly independent.

But the columns of  $C$  corresponding the first column of the Jordan block corresponding to  $\lambda_2$  is  $[0 \ 0 \ 0]$ , not linearly independent.

Hence the state equation is not observable.

Now consider the Jordan form state equation

$$\begin{aligned} \dot{\underline{x}} &= \begin{bmatrix} \lambda_1 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & \lambda_1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \lambda_1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \lambda_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \lambda_2 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & \lambda_2 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & \lambda_2 \end{bmatrix} \underline{x} + \begin{bmatrix} b_{111}^T \\ b_{l11}^T \\ b_{l12}^T \\ b_{l13}^T \\ b_{l21}^T \\ b_{221}^T \\ b_{l21}^T \end{bmatrix} \underline{u} \\ \underline{y} &= \begin{bmatrix} c_{f11} & c_{211} & c_{f12} & c_{f13} & c_{f21} & c_{221} & c_{321} \end{bmatrix} \underline{x} \end{aligned} \quad (32)$$

Since  $(sI - J)^{-1}$  is given by

$$(sI - J)^{-1} = \begin{bmatrix} \frac{1}{1-\lambda_1} & \frac{1}{(1-\lambda_1)^2} & 0 & 0 & 0 & 0 & 0 \\ 0 & \frac{1}{1-\lambda_1} & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \frac{1}{1-\lambda_1} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \frac{1}{1-\lambda_1} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{1}{1-\lambda_2} & \frac{1}{(1-\lambda_2)^2} & \frac{1}{(1-\lambda_2)^3} \\ 0 & 0 & 0 & 0 & 0 & \frac{1}{1-\lambda_2} & \frac{1}{(1-\lambda_2)^2} \\ 0 & 0 & 0 & 0 & 0 & 0 & \frac{1}{1-\lambda_2} \end{bmatrix} \quad (33)$$

From the relation between  $\underline{u}$  and  $\underline{y}$ , i.e.,  $\underline{y}(s) = C(sI - J)^{-1}B\underline{u}(s)$ .  
Now the output can be written as

$$\underline{y}(s) = \underline{y}_1(s) + \underline{y}_2(s) + \underline{y}_3(s) + \underline{y}_4(s) + \underline{y}_5(s) + \underline{y}_6(s) + \underline{y}_7(s) \quad (34)$$

$$\underline{y}_1(s) = \underline{c}_{f11} \left[ \frac{1}{(s - \lambda_1)^2} \underline{b}_{l11}^T \underline{u}(s) + \frac{1}{s - \lambda_1} \underline{b}_{l11}^T \underline{u}(s) \right] \quad (35)$$

$$\underline{y}_2(s) = \underline{c}_{211} \left[ \frac{1}{s - \lambda_1} \underline{b}_{l11}^T \underline{u}(s) \right] \quad (36)$$

$$\underline{y}_3(s) = \underline{c}_{f12} \left[ \frac{1}{s - \lambda_1} \underline{b}_{l12}^T \underline{u}(s) \right] \quad (37)$$

$$\underline{y}_4(s) = \underline{c}_{f13} \left[ \frac{1}{s - \lambda_1} \underline{b}_{l13}^T \underline{u}(s) \right] \quad (38)$$

$$\underline{y}_5(s) = \underline{c}_{f21} \left[ \frac{1}{(s - \lambda_2)^3} \underline{b}_{l21}^T \underline{u}(s) + \frac{1}{(s - \lambda_2)^2} \underline{b}_{l21}^T \underline{u}(s) + \frac{1}{s - \lambda_2} \underline{b}_{l21}^T \underline{u}(s) \right] \quad (39)$$

$$\underline{y}_6(s) = \underline{c}_{221} \left[ \frac{1}{(s - \lambda_2)^2} \underline{b}_{l21}^T \underline{u}(s) + \frac{1}{s - \lambda_2} \underline{b}_{l21}^T \underline{u}(s) \right] \quad (40)$$

$$\underline{y}_7(s) = \underline{c}_{321} \left[ \frac{1}{s - \lambda_2} \underline{b}_{l21}^T \underline{u}(s) \right] \quad (41)$$

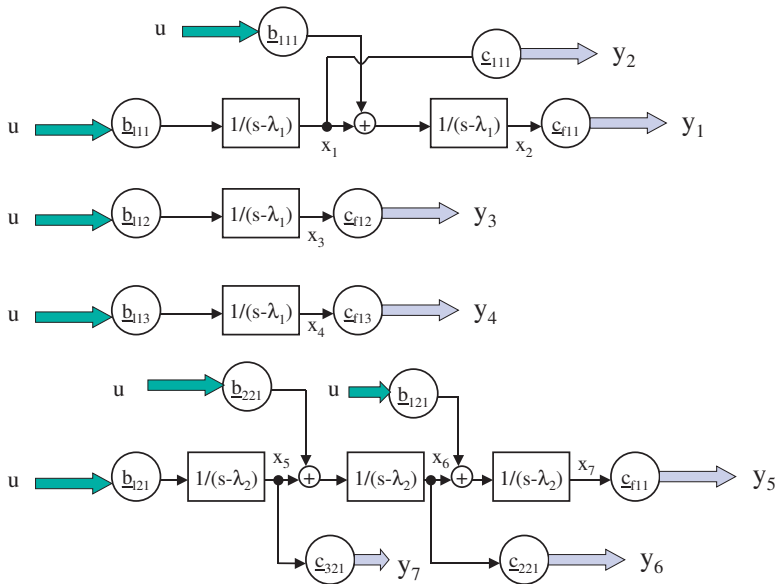


Fig. 8.3

**Corollary:** A single-input Jordan form state equation is controllable iff there is only one Jordan block associated with each distinct eigenvalue and every entry of  $B$  (which is a column) corresponding to the last row of each Jordan block is nonzero.

In this case  $B = [b_1 \ b_2 \ \cdots \ b_n]^T$ .

**Corollary:** A single-output Jordan form state equation is observable iff there is only one Jordan block associated with each distinct eigenvalue and every entry of  $C$  (which is a row) corresponding to the first column of each Jordan block is nonzero.

In this case  $C = [c_1 \ c_2 \ \cdots \ c_n]$ .

Consider the single-input single-output state equation

$$\begin{aligned}\dot{\underline{x}} &= \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -2 \end{bmatrix} \underline{x} + \begin{bmatrix} 10 \\ 9 \\ 0 \\ 1 \end{bmatrix} u \\ y &= [1 \ 0 \ 0 \ 2] \underline{x} + u\end{aligned}$$

Here we have two Jordan blocks, one with order 3 associated with eigenvalue 0, other one of order 1 and associated with eigenvalue -2. Hence one Jordan block for each distinct eigenvalue.

But the entry in  $B$  corresponding to the last row of the first Jordan block is zero. Hence not controllable.

The entries in  $C$  corresponding to the first column of both Jordan block is nonzero. Hence observable.

## Discrete-Time State Equations

Consider the discrete time state equation (time invariant)

$$\begin{aligned}\underline{x}[k+1] &= A\underline{x}[k] + B\underline{u}[k] \\ \underline{y}[k] &= C\underline{x}[k] + D\underline{u}[k]\end{aligned}\tag{42}$$

**Theorem:** The following statements are equivalent:

1. The state equation (42) or the pair  $(A, B)$  is controllable.
2. The matrix

$$W_{dc}[n-1] = \sum_{m=0}^{n-1} A^m B B' (A')^m \tag{43}$$

is nonsingular

3. The controllability matrix  $X_d = [B \ AB \ A^2B \ \dots \ A^{n-1}B]$  has full row rank.
4. The matrix  $[A - \lambda I \ B]$  has full row rank for every eigenvalue of  $A$ .

Solution of (42) at  $k = n$  is given by

$$\underline{x}[n] = A^n \underline{x}[0] + \sum_{m=0}^{n-1} A^{n-1-m} B \underline{u}[m] \quad (44)$$

which can be written as

$$\underline{x}[n] - A^n \underline{x}[0] = [B \ AB \ \cdots \ A^{n-1} B] \begin{bmatrix} \underline{u}[n-1] \\ \underline{u}[n-2] \\ \vdots \\ \underline{u}[0] \end{bmatrix} \quad (45)$$

It can be shown that for any  $\underline{x}[0]$  and  $\underline{x}[n]$  a solution of (45) exists iff  $X_d$  has full row rank. (equivalence of 1 and 3 proved)

Now the matrix  $W_{dc}[n-1]$  can be written as

$$W_{dc}[n-1] = [B \ AB \ A^2 B \ \cdots \ A^{n-1} B] \begin{bmatrix} B' \\ B' A' \\ \vdots \\ B' (A')^{n-1} \end{bmatrix} = X_d X_d' \quad (46)$$

Thus  $X_d$  is of full row rank iff  $W_{dc}[n-1]$  is nonsingular. (equivalence of 2 and 3 proved)



**Theorem:** The following statements are equivalent:

1. The state equation (42) or the pair  $(A, C)$  is observable.
2. The matrix

$$W_{do}[n-1] = \sum_{m=0}^{n-1} (A')^m C' C A^m \quad (47)$$

is nonsingular

3. The controllability matrix

$$O_d = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix} \quad (48)$$

has full column rank.

4. The matrix  $\begin{bmatrix} A - \lambda I \\ C \end{bmatrix}$  has full column rank for every eigenvalue of  $A$ .

## Controllability to the Origin and Reachability

We have three different type of controllability definition:

1. Transfer any state to any other state. (we have discussed this controllability)
2. Transfer any state to zero state, called controllability to origin.
3. Transfer zero state to any state, called reachability.

In continuous time case the three definitions are equivalent, as  $e^{At}$  is nonsingular.

In discrete-time case, if  $A$  is nonsingular, the three definitions are equivalent. If  $A$  is singular, still (1) and (3) are equivalent, not (2) and (3).

Let us consider the following state equation

$$\underline{x}[k+1] = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \end{bmatrix} \underline{x}[k] + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} u[k]$$

The controllability matrix is 0. Hence not controllable. But since  $A^k = 0$  for  $k \geq 3$ . Thus we have  $\underline{x}[3] = A^3 \underline{x}[0] = \underline{0}$  for any initial  $\underline{x}[0]$ . Thus the equation is controllable to the origin.

## Controllability After Sampling

Consider the state equation

$$\dot{\underline{x}}(t) = A\underline{x}(t) + B\underline{u}(t) \quad (49)$$

If the input is piecewise constant, or,

$$u[k] \triangleq u(kT) = u(t) \quad \text{for } kT \leq t < (k+1)T \quad (50)$$

Then the equation can be described by

$$\bar{\underline{x}}[n] = \bar{A}\bar{\underline{x}}[0] + \bar{B}u[k] \quad (51)$$

with

$$\bar{A} = e^{AT} \quad \bar{B} = \left( \int_0^T e^{At} dt \right) B \quad (52)$$

It can be shown that if (49) is uncontrollable then (51) also uncontrollable, but if (49) is controllable then (51) may not be controllable for all values of  $T$ .

## Linear Time Variant Equations

Consider the state equation

$$\begin{aligned}\dot{\underline{x}}(t) &= A(t)\underline{x}(t) + B(t)\underline{u}(t) \\ \underline{y}(t) &= C(t)\underline{x}(t)\end{aligned}\tag{53}$$

The state equation is said to be controllable at  $t_0$ , if there exists a finite  $t_1 > t_0$  such that for any initial state  $\underline{x}(t_0)$  and final state  $\underline{x}(t_1)$  there exists an input that can perform the transfer.

Difference with LTI: for LTI if the system is controllable it is controllable at each  $t_0$ , and the transfer can be performed in any interval  $\tau = t_1 - t_0$ .

**Theorem:** The state equation (53) or the pair  $(A(t), B(t))$  is controllable at time  $t_0$  iff there exists  $t_1 > t_0$  such that the matrix

$$W_c(t_0, t_1) = \int_{t_0}^{t_1} \Phi(t_1, \tau) B(\tau) B'(\tau) \Phi'(t_1, \tau) d\tau\tag{54}$$

is nonsingular, where  $\Phi(t, \tau)$  is the state transition matrix of  $\dot{\underline{x}}(t) = A(t)\underline{x}(t)$ .

**Proof:** The response of the system at  $t_1$  is given by

$$\underline{x}(t_1) = \Phi(t_1, t_0)\underline{x}(0) + \int_{t_0}^{t_1} \Phi(t_1, \tau)B(\tau)\underline{u}(\tau)d\tau \quad (55)$$

We claim that the input

$$\underline{u}(t) = -B'(t)\Phi'(t_1, t)W_c^{-1}(t_0, t_1)[\Phi(t_1, t_0)\underline{x}_0 - \underline{x}_1] \quad (56)$$

can transfer  $\underline{x}$  from  $\underline{x}_0$  to  $\underline{x}_1$ . Indeed substituting (56) in (55) we get

$$\begin{aligned} \underline{x}(t_1) &= \Phi(t_1, t_0)\underline{x}_0 \\ &\quad - \int_{t_0}^{t_1} \Phi(t_1, \tau)B(\tau)B'(\tau)\Phi'(t_1, \tau)W_c^{-1}(t_0, t_1)[\Phi(t_1, t_0)\underline{x}_0 - \underline{x}_1]d\tau \\ &= \Phi(t_1, t_0)\underline{x}_0 \\ &\quad - \left( \int_{t_0}^{t_1} \Phi(t_1, \tau)B(\tau)B'(\tau)\Phi'(t_1, \tau)d\tau \right) W_c^{-1}(t_0, t_1)[\Phi(t_1, t_0)\underline{x}_0 - \underline{x}_1] \\ &= \underline{x}_1 \end{aligned} \quad (57)$$

Thus the equation is controllable if  $W_c(t_0, t_1)$  is invertible, i.e., nonsingular.

Now let us consider that  $W_c(t_0, t_1)$  is singular but the equation is controllable. Then there exists one vector  $\underline{v}$  such that

$$\begin{aligned}\underline{v}' W_c(t_0, t_1) \underline{v} &= \int_{t_0}^{t_1} \underline{v}' \Phi(t_1, \tau) B(\tau) B'(\tau) \Phi'(t_1, \tau) \underline{v} d\tau \\ &= \int_{t_0}^{t_1} \|B'(\tau) \Phi'(t_1, \tau) \underline{v}\|^2 d\tau = 0\end{aligned}\quad (58)$$

which implies

$$B'(\tau) \Phi'(t_1, \tau) \underline{v} = \underline{0} \quad \text{or} \quad \underline{v}' \Phi(t_1, \tau) B(\tau) = \underline{0}' \quad (59)$$

for all  $\tau$  such that  $t_0 \leq \tau \leq t_1$ . Since the state equation is controllable there exists an input that can transfer the state  $\underline{x}_0 = \Phi(t_0, t_1) \underline{v}$  at  $t_0$  to  $\underline{x}(t_1) = \underline{0}$ .

Then (55) becomes

$$\underline{0} = \underbrace{\Phi(t_1, t_0) \Phi(t_0, t_1)}_{\text{I}} \underline{v} + \int_{t_0}^{t_1} \Phi(t_1, \tau) B(\tau) \underline{u}(\tau) d\tau \quad (60)$$

Its premultiplication with  $\underline{v}'$  gives

$$\begin{aligned} 0 &= \underline{v}'\underline{v} + \int_{t_0}^{t_1} \underline{v}'\Phi(t_1, \tau)B(\tau)\underline{u}(\tau)d\tau \\ &= \underline{v}'\underline{v} + 0 \end{aligned} \tag{61}$$

This means the construct is true only if  $\underline{v} = \underline{0}$ . That means if the state equation is controllable  $W_c(t_0, t_1)$  is nonsingular. (EOP)

Since the transition matrix may not be available we need controllability condition that does not involve it.

Let us define matrices

$$M_{m+1}(t) = -A(t)M_m(t) + \frac{d}{dt}M_m(t) \tag{62}$$

where  $M_0(t) = B(t)$ .

It can be shown that

$$\frac{\partial^m}{\partial t^m}\Phi(t_2, t)B(t) = \Phi(t_2, t)M_m(t) \tag{63}$$

for  $m = 0, 1, 2, \dots$

**Theorem:** Let  $A(t)_{n \times n}$  and  $B(t)_{n \times p}$  be  $n - 1$  times continuously differentiable. Then the  $n$  dimensional pair  $(A(t), B(t))$  is controllable at  $t_0$  if there exists a finite  $t_1 > t_0$  such that

$$\rho([M_0(t_1) \ M_1(t_1) \ \cdots \ M_{n-1}(t_1)]) = n \quad (64)$$

Note that this is a sufficient condition, not a necessary condition.

**Proof:** Let us consider that (64) holds, but  $W_c(t_0, t)$  is singular for some  $t_2 \geq t_1$ . Then there exists one vector  $\underline{v}$  such that

$$\begin{aligned} \underline{v}' W_c(t_0, t_2) \underline{v} &= \int_{t_0}^{t_2} \underline{v}' \Phi(t_1, \tau) B(\tau) B'(\tau) \Phi'(t_1, \tau) \underline{v} d\tau \\ &= \int_{t_0}^{t_1} ||B'(\tau) \Phi'(t_1, \tau) \underline{v}||^2 d\tau = 0 \end{aligned} \quad (65)$$

which implies

$$B'(\tau) \Phi'(t_1, \tau) \underline{v} = \underline{0} \quad \text{or} \quad \underline{v}' \Phi(t_1, \tau) B(\tau) = \underline{0}' \quad (66)$$



for all  $\tau$  such that  $t_0 \leq \tau \leq t_2$ . Differentiations w.r.t.  $\tau$  yields

$$\underline{v}'\Phi(t_1, \tau)M_m(\tau) = \underline{0}' \quad (67)$$

for  $m = 0, 1, 2, \dots, n-1$ , and all  $t_0 \leq \tau \leq t_2$ . Since  $t_2 \geq t_1$  we have

$$\underline{v}'\Phi(t_2, t_1)[M_0(t_1) \ M_1(t_1) \ \cdots \ M_{n-1}(t_1)] = \underline{0}' \quad (68)$$

Since  $\Phi(t_2, t_1)$  is nonsingular  $\underline{v}'\Phi(t_2, t_1) \neq \underline{0}'$ . Hence (64) is not valid. A contradiction. Hence (64) valid implies  $W_c(t_0, t_1)$  nonsingular, or, the state equation is controllable at  $t_0$ .

**Example:** Consider

$$\dot{\underline{x}} = \begin{bmatrix} t & -1 & 0 \\ 0 & -t & t \\ 0 & 0 & t \end{bmatrix} \underline{x} + \begin{bmatrix} 0 \\ 1 \\ 1 \end{bmatrix} u$$

Prove that the matrix is controllable for all  $t$ .

**Solution:** We have  $M_0 = B = [0 \ 1 \ 0]'$  and we can get

$$M_1 = -A(t)M_0 + \frac{d}{dt}M_0 = \begin{bmatrix} 1 \\ 0 \\ -t \end{bmatrix}$$

$$M_2 = -A(t)M_1 + \frac{d}{dt}M_1 = \begin{bmatrix} -t \\ t^2 \\ t^2 - 1 \end{bmatrix}$$

The determinant of the matrix

$$[M_0 \ M_1 \ M_2] = \begin{bmatrix} 0 & 1 & -t \\ 1 & 0 & t^2 \\ 1 & -t & t^2 - 1 \end{bmatrix}$$

is  $t^2 + 1$ , which is nonzero for all  $t$ . Thus the state equation is controllable for all  $t$ .

**Example:** Consider

$$\dot{\underline{x}} = \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \underline{x} + \begin{bmatrix} e^t \\ e^{2t} \end{bmatrix} u$$

Find if the matrix is controllable.

**Solution:** Here since  $A$  does not vary with time

$$\Phi(t, \tau) = \exp \left( \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} (t - \tau) \right) = \begin{bmatrix} e^{t-\tau} & 0 \\ 0 & e^{2(t-\tau)} \end{bmatrix} \quad (69)$$

and

$$\Phi(t, \tau) B(\tau) = \begin{bmatrix} e^{t-\tau} & 0 \\ 0 & e^{2(t-\tau)} \end{bmatrix} \begin{bmatrix} e^\tau \\ e^{2\tau} \end{bmatrix} = \begin{bmatrix} e^t \\ e^{2t} \end{bmatrix} \quad (70)$$

We can find

$$\begin{aligned}
 W_c(t_0, t) &= \int_{t_0}^t \Phi(t, \tau) B(\tau) B'(\tau) \Phi'(t, \tau) d\tau = \int_{t_0}^t \begin{bmatrix} e^t \\ e^{2t} \end{bmatrix} \begin{bmatrix} e^t & e^{2t} \end{bmatrix} d\tau \\
 &= \begin{bmatrix} \int_{t_0}^t e^{2t} d\tau & \int_{t_0}^t e^{3t} d\tau \\ \int_{t_0}^t e^{3t} d\tau & \int_{t_0}^t e^{4t} d\tau \end{bmatrix} = \begin{bmatrix} e^{2t}(t - t_0) & e^{3t}(t - t_0) \\ e^{3t}(t - t_0) & e^{4t}(t - t_0) \end{bmatrix} \quad (71)
 \end{aligned}$$

Its determinant is identically zero for all  $t_0$  and  $t$ . Thus the state equation is not controllable at any  $t_0$ .

**Theorem:** The state equation (53) or the pair  $(A(t), C(t))$  is observable at time  $t_0$  iff there exists  $t_1 > t_0$  such that the matrix

$$W_o(t_0, t_1) = \int_{t_0}^{t_1} \Phi'(\tau, t_0) C'(\tau) C(\tau) \Phi(\tau, t_0) d\tau \quad (72)$$

is nonsingular, where  $\Phi(t, \tau)$  is the state transition matrix of  $\dot{\underline{x}}(t) = A(t)\underline{x}(t)$ .

**Theorem:** Let  $A(t)_{n \times n}$  and  $C(t)_{q \times n}$  be  $n - 1$  times continuously differentiable. Then the  $n$  dimensional pair  $(A(t), C(t))$  is controllable at  $t_0$  if there exists a finite  $t_1 > t_0$  such that

$$\rho \left( \begin{bmatrix} N_0(t_1) \\ N_1(t_1) \\ \vdots \\ N_{n-1}(t_1) \end{bmatrix} \right) = n \quad (73)$$

where

$$N_{m+1}(t) = N_m(t)A(t) + \frac{d}{dt}N_m(t) \quad \text{for } m = 0, 1, 2, \dots, n - 1 \quad (74)$$

with  $N_0 = C(t)$ .