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Westinghouse Hipersil® Core Design Engineer's Handbook







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INTRODUCTION

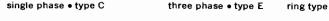
Hipersil tape-wound cut and uncut cores were introduced by Westinghouse in 1942. Hipersil steel is a grain oriented magnetic iron silicon alloy of very high permeability and low core loss. By continuously winding the steel into cores, the direction of magnetic flux always coincides with the best magnetic direction of the Hipersil material.

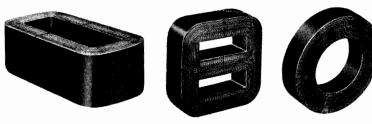
Through the years, Hipersil cores have become commonly used for many transformer and reactor components both commercial and military. Their use enables the designer to shrink the size of his component or obtain better performance characteristics.



GENERAL DESCRIPTION

Hipersil cores are made either cut or uncut in ring or C-core form for single phase applications or E-core form for three phase applications.





Hipersil cores are prepared by slitting the steel to width; then winding it on a form of the desired shape. They are then carefully annealed in a special atmosphere under exacting conditions to relieve stresses set up in slitting and winding. The C and E cores are next bonded in a special resin to hold the layers together. Uncut cores may be supplied as annealed or may be bonded to make the core more rigid. Bonding the core increases the exciting watts and core losses somewhat. To take full advantage of the material uncut cores are often supplied less bonding. They may also be supplied with edge-bonding or with Polyclad, a hard resin coating which completely surrounds the core and provides insulation which can be used as a base for most windings. The C or E cores are carefully cut after bonding to keep the air gap small when the halves are placed together.

Hipersil cores are available in several lamination thicknesses. They cover a wide field of application from power distribution frequencies to very high frequencies used in electronic components.

Single-phase 12-mil Hipersil C cores are commonly used at power distribution frequencies to make use of the excellent high density permeability, and low loss for conventional continuous duty designs. They can also be used to further reduce size or increase output of intermittent duty transformers—for example, those used for resistance welding or x-ray applications.

Single-phase 4-mil Hipersil cores offer the advantage of lower loss at higher frequencies and are therefore primarily advantageous in aircraft or shipboard circuits operating at 320 to 5000 cycles. Reduction in thickness has been obtained without sacrifice of permeability or saturation level, so that reductions in weight and space or improvements in operating characteristics are possible over this frequency range.

Single-phase 1 and 2-mil Hipersil C cores have found their chief application in pulse transformers and similar duty components. Here the thinness of laminations together with high space factor, permits the design of small high frequency components without sacrifice of permeability or saturation density. The excellent magnetic and loss characteristics have also proven advantageous in the design of transformers and reactors for alternating voltage applications up to 500 kc or higher. All C cores are manufactured to specifications that meet the requirements set forth in EIA standard RS 217 for wound cut cores.

Three-phase Hipersil E cores offer a solution to the problem of a small, light-weight, three-phase transformer utilizing the high permeability and low loss characteristics of Hipersil cores. Consisting of two-piece construction and three winding legs of equal cross-section, they are made in 12, 4 and 2-mil gauges to cover a wide range of frequencies.

Ring type 12, 4, 2 and 1-mil Hipersil cores offer the advantages of high permeability and low hysteresis loss without impairment caused by a magnetic joint. They offer a solution to many magnetic amplifier, reactor or current transformer problems where material quality is of prime importance.

GENERAL MAGNETIC DEFINITIONS

Terminology

- a. <u>Unit Pole—a convenient concept defined so that two unit poles (m) of like kind placed one centimeter apart in vacuum will repel each other with a force of one dyne.</u>
- b. Magnetic Field Strength or Magnetizing Force (H) one centimeter away from a unit pole in vacuum is one <u>Oersted</u>. Gauss showed experimentally that the field drops off as the inverse square of the distance.
- c. Intensity of Magnetization (I) is defined as the number of unit poles per unit area.
- d. Faraday introduced the concept that some magnetic properties may be likened to an endless flow along <u>lines of induction</u>. These "lines" would be the paths described by mobile unit poles moving in a magnetic field.

It is customary to draw these lines so that in a field of one oersted one line will pass through a perpendicular unit area.

Gauss's theorem states that 4π lines emanate from a unit pole. The proof of this is rather simple. The field on the surface of a sphere formed by rotating a one centimeter radius about a unit pole is, by definition, one oersted. We have seen that one line passes through each square centimeter at this field strength. Therefore, 4π lines cut the sphere, since the surface area equals $4\pi r^2$.

- e. Flux is the number of lines, or maxwells (ϕ) crossing a given area perpendicular to the lines.
- f. Magnetic Induction, or Flux Density is the flux per unit area. It is usually expressed in gauss. $(B=\phi/A)$.
- g. Thus far, consideration has been given to the behavior of magnetic forces acting within a vacuum. A demagnetized iron bar may be considered as containing a large number of free north- and south-seeking poles, so arranged that they neutralize one another. If this bar is placed in a longitudinal field, unit north and south poles will move to opposite ends of the bar.

The applied field will pass easily between these infinitesimal poles and will remain unchanged. Each unit pole has, as previously discussed, 4π lines radiating from it. Hence the total flux in the bar will be the vectorial sum of the applied and induced fields, or $B=H+4\pi I$ where I=m/A. The term $4\pi I$ is referred to as the intrinsic induction.

If the poles are considered to have a random distribution over the area A, one may write $B=\mu H$, where μ is a proportionality factor called the permeability.

h. <u>Magnetomotive Force</u> (mmf) is analogous to voltage and may be expressed (in gilberts) as:

$$mmf = \frac{4\pi Ni}{10}$$

where Ni represent the ampere-turns in a coil generating this mmf.

i. Flux may be likened to electrical current and mmf to voltage. It is natural, therefore, to reason that a parallel to Ohm's law may exist in magnetic circuits. If $\frac{\text{mmf}}{\phi} = R$, R will be found experimentally to equal $\frac{\ell}{\mu \Lambda}$.

The permeability, μ , corresponds to electrical conductivity. R, comparable to resistance, is called the reluctance.

Classification of Materials, Magnetically

Materials may be classified into various groups, depending upon their behavior in a magnetic field.

- a. <u>Diamagnetic</u> materials are those having permeabilities less than unity. They are repelled from the poles of a magnet. Examples are the halogens, the rare gases, and the noble metals.
- b. <u>Paramagnetic</u> materials are weakly attracted by a magnet. Their permeabilities range from 1 to about 1.1. Examples are: the alkali metals, the rare earths, and oxygen.
- c. <u>Ferromagnetic</u> materials have permeabilities ranging into the thousands. They include the alloys of iron, nickel, cobalt, and gadolinium. Their important attributes are:
 - 1. Permeabilities much greater than one.
 - 2. Dependence of permeability on field and previous history (hysteresis).
 - 3. Approach of the intrinsic magnetization to a finite limit as the field is increased (saturation).
 - 4. Spontaneous magnetization (presence of small, intensely magnetized regions).
 - Curie point (disappearance of the above characteristics when the temperature exceeds a critical value).

Magnetization Curve and Hysteresis Loop

If a piece of unmagnetized iron is subjected to a magnetic field, the magnetization induced in the iron may be described by a curve obtained by plotting magnetic induction B against field strength H. (figure 1.)

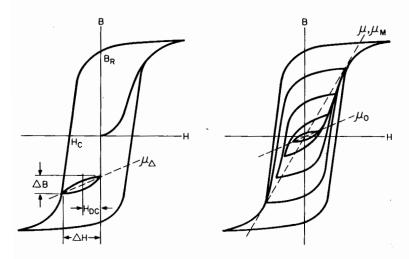


Figure 1

Figure 2

If the field is now decreased to zero and reversed cyclically, it is observed that the original curve is not retraced; the induction lags the field and forms a characteristic curve, called a <u>hysteresis</u> loop. If this alternating field is now reduced stepwise, a family of loops is obtained. (figure 2.)

The value of H for which B is zero is called the <u>coercive force</u> H_c . The value of induction for which H=0 is the <u>residual induction</u> B_r ; and these values vary as the applied field is varied. When the field is sufficient to drive the iron close to saturation, these points become the coercivity and retentivity.

Saturation induction, B_s , is the ceiling value of B-H (or $4\pi I$).

Permeability

As previously stated, the ratio B/H is called the permeability. The numerical value of this ratio will vary widely, depending upon the fields applied and the previous magnetic history. Refer to figures 1 and 2.

- a. Normal Permeability, μ , is the slope of a line drawn through the tips of a hysteresis loop formed at a specified value of H (or B). It is the ratio of the normal induction to the corresponding magnetizing force.
- b. Initial Permeability, μ_0 is the limit approached by the normal permeability as B and H decrease toward zero. It is customarily measured at 40 gauss.
- c. Maximum Permeability, μ_{m} is the largest value of normal permeability attained by varying H.
- d. Differential Permeability, μ_d , is simply dB/dH at a specified point. It is the absolute value of the slope of the hysteresis loop at any point.
- e. Incremental Permeability, $\mu\Delta$, is the permeability measured with superposed fields. It is of great interest in the design of reactors carrying direct current.

Magnetization Process

a. Ferromagnetic material has long been regarded as an assemblage of tiny permanent magnets. The nature of this tiny magnet has been the subject of much consideration and conjecture. Modern theory calls it a domain—a group of atoms acting in unison. This domain is said to be spontaneously magnetized—that is, a magnetic moment is associated with it.

In a demagnetized iron bar, the domains are so arranged that their fields cancel. If an external field is applied to the bar, the domains will rearrange themselves so that a net field is produced.

b. The magnetic moment of a given domain is governed by the magnitude and direction of its magnetization, and by its volume. Changes in magnitude depend upon temperature, and—to a slight degree—upon the applied field. Ordinarily, therefore, the moment is changed by (1) an alteration in the direction of magnetization (rotation); and (2) by a change in the volume of the domain (moving boundary).

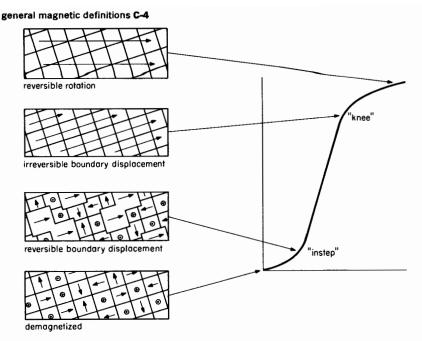


Figure 3

Figure 3 illustrates a highly idealized representation of possible domain orientation within an iron crystal. As an external field is applied gradually, the domains oriented in line with the field will grow at the expense to those opposed or perpendicular to it. This process is essentially reversible and corresponds to the "foot" of the magnetization curve.

As the applied field is increased still further, <u>irreversible</u> boundary displacement sets in, as the unfavorable domains are assimilated. The next figure illustrates the condition at the "knee" of the curve.

Still higher applied fields will effect reversible domain rotation. At this point the material becomes saturated. Stronger fields will produce no further change.

Losses

a. It can be shown mathematically that all the energy expended in magnetizing a piece of iron will not be recovered by de-magnetizing it. Some will be lost as heat. This loss is independent of the rate of change of magnetization and is known as hysteresis loss. It may be expressed as

$$W_h = \frac{\int HdB}{4\pi}$$

Typical values are in (ergs/cm²—cycle)

<u>Material</u>	Loss	Induction
Supermalloy	4	5,000
3% Silicon Steel	300	10,000
Alnico V	2.5 x 10 ⁶	14,000

Steinmetz developed the empirical expression $W_h=\eta B^{1.6}$, which holds rather accurately for iron through the range of 5 to 15 kilogauss.

b. If a conductive specimen is subjected to an alternating magnetic field, circulating Foucault or "eddy" currents will be set up. These currents act to oppose the applied field, and their net effect is to prevent the field from penetrating immediately to the interior of the material. The induction decreases, therefore, from the surface inward.

Eddy currents give rise to an energy loss equal to $\int \rho I^2$ over the volume of the material where ρ is the resistivity and I is the current density.

In sheets of thickness δ subject to a sinusoidal field parallel to the sheet the <u>eddy loss</u> is given by

$$W_e = \frac{\pi^2 \delta^2 B^2 f}{6a}$$

when flux penetration is essentially complete. ($2\pi\delta\sqrt{\mu f/\rho}$ < 1).

Other expressions have been developed for use if this is not the case.

Magnetic Anisotropy

Crystals of the magnetic metals are anisotropic—that is, their properties vary with direction.

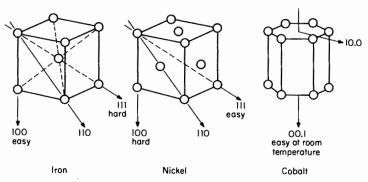
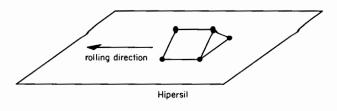


Figure 4

a. Iron is arranged in a body-centered cubic structure, as shown in figure 4. Experiments have indicated that magnetization proceeds most readily in a direction parallel to a cubic axis (100 direction), and least so parallel to the body diagonal (111). Magnetization along a face diagonal (110) is intermediate in responsiveness.

In many polycrystalline materials, the crystals are oriented more or less at random. The process of cold rolling metal sheets produces, however, some regularity in orientation; and the magnetic properties are markedly anisotropic.



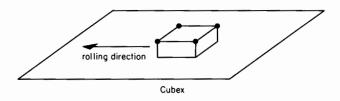


Figure 5

The crystalline structures of <u>Hipersil</u> and <u>Cubex</u> are shown in figure 5. They illustrate why Hipersil has a single preferred orientation; and Cubex, a double one.

- b. Nickel is arranged in a face centered cubic lattice. Its directions of progressively harder magnetization are opposite those of iron.
- c. Cobalt forms a hexagonal prismatic structure. At room temperature, the hexagonal axis is the direction of easy magnetization; but this becomes the most difficult direction avove 275°C.

Effect of an Air Gap

Gapping a core is, in effect, adding reluctances in series—the reluctance of the air gap to that already existing for the core.

$$R_{\text{total}} = R_{\text{c}} + R_{\text{g}} = \frac{\ell_{\text{C}}}{\mu_{\text{c}} A_{\text{c}}} + \frac{\ell_{\text{g}}}{\mu_{\text{g}} A_{\text{g}}}$$

As a practical example, consider an uncut ring core 2" ID x 4" OD x 1" thick. A reasonable value for μ in silicon steel is 10,000 at 10 kilogauss. The reluctance is $3\pi/10,000$ or .00094.

If a .005" gap is now cut in the core, the reluctance will increase to

$$\frac{3\pi}{10,000} + \frac{.005}{1} = .00594$$

—over six times its uncut value. This illustrates the importance of minimizing the gap when a low core exciting volt-ampere value is essential.

The increase in reluctance will, however, cause the magnetization curve to "shear" as illustrated in figure 6, producing a sharp increase in B_{max} — B_r . It will be shown that this is very desirable in certain applications.

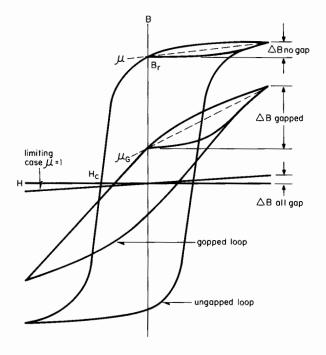


Figure 6

Hysteresis Loop Under Special Conditions

a. <u>Pulse</u>. For the purpose of this discussion, we will consider "pulse" applications as those in which a core is driven by unidirectional current surges and is not biased or "reset". Under these conditions, the core will cycle over a minor hysteresis loop from B_r to some higher value (figure 6).

In order to realize maximum flux swing and pulse permeability, it is often advantageous to introduce an air gap into the core; dropping B_r to the lowest value commensurate with high B_{max}.

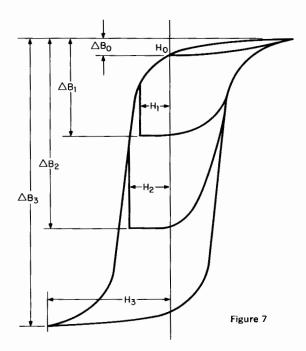
b. <u>Switching</u>. It was pointed out that low B_r/B_{max} is desirable in pulse transformer cores. Another application—the use of magnetic cores as "memory" devices—calls for the highest possible ratio of B_r/B_{max} .

Such a core may be driven by positive or negative pulses. Assume that a core has been driven to saturation by a positive pulse. It will then rest at $+B_r$. Successive positive pulses will drive the core from $+B_r$ to $+B_{max}$ and back; and the output developed will be very low.

If a negative pulse is now applied, the core will "switch" from $+B_{max}$ to $-B_{max}$; generating a high amplitude pulse in an output winding. The output is, therefore, dependent upon the <u>direction</u> of the applied pulses and the core's history.

The core constitutes a bistable "memory" device, ideally suited to binary digital computer applications.

c. <u>Magamp</u>. If a core is driven by positive pulses and "reset" or biased by an adjustable direct current, its output may be varied by changing the direct—or control—current. Under these conditions it will cycle as shown in figure 7. Since a small variation in control current usually effects a large change in output voltage—or power—the device is frequently called a "magnetic amplifier".



Desirable characteristics for such a core are:

- 1. High, narrow loop (high output with low control current).
- 2. Steep loop flanks (high gain).
- 3. High Br/Bmax (minimum output with zero bias).

Basic Equations

 a. If a conductor cuts one line per second, an electromotive force of one emu or 10⁻⁸ volts is developed.

$$e = \frac{Nd\phi}{dt \cdot 10^8} = \frac{NAdB}{dt \cdot 10^8} \tag{1}$$

Under step pulse conditions (1) becomes

$$e = \frac{6.45 \text{NA} \Delta B}{10^8 \cdot t} \text{ or } \Delta B = \frac{\text{et } 10^8}{6.45 \text{NA}}$$
 (2)

Where e=peak voltage; t=time in seconds; A=area in square inches; and \(\Delta B=flux \) swing in gauss. Equation (2) is the basic formula in pulse transformer design,

Under sinusoidal conditions, (1) may be solved as

$$E = \frac{6.45.2\pi f NAB}{1.4 \times 10^8} = \frac{f NAB}{3.49 \times 10^8} \text{ or } B = \frac{3.49 \times 10^6 E}{f NA}$$
 (3)

Where E=RMS voltage and f=cycles per second. Equation (3) is used for calculating basic operating conditions in power transformers.

b. We have seen that mmf= $\frac{4\pi \text{Ni}}{10}$

Field strength may be expressed as mmf/unit length, or (4)

$$H = \frac{4\pi Ni}{10\ell}$$

Equation (4) is used to calculate bias for reactors and transformers carrying direct current.

c. Pulse permeability may be calculated from $=\frac{\mu\Delta B}{\Delta H}$ or

$$\mu = \frac{\Delta B}{\frac{4\pi Ni}{2.54 \times 10\ell}} = \frac{2.02\Delta B\ell}{Ni}$$
(5)

Units are as above, except that ℓ has been converted to inches.

d. A circuit has one henry of inductance when 108 lines link the circuit for each am pere flowing.

$$L = \frac{\frac{N\phi}{10^8} - Li}{i}$$

$$L = \frac{\frac{N\phi \cdot 10^{\cdot 8}}{i} - \frac{NBA \cdot 10^{\cdot 8}}{i} - \frac{\mu NAH \cdot 10^{\cdot 8}}{i} - \frac{4\pi\mu N^2 A \cdot 10^{\cdot 9}}{\ell}$$

Converting to square inches and inches
$$L = \frac{3.2 \mu N^2 A \cdot 10^{-8}}{\ell}$$

If the core is cut or gapped

$$L = \frac{3.2N^{2}A \cdot 10^{-8}}{\frac{\ell c}{\ell_{g} + \frac{\ell c}{l'}}}$$
 (6)

This equation is widely used in the design of iron core reactors.

COMPONENT DESIGN

A. General

For any size parts, the number of turns determines the flux density in the iron. The fewer the turns the higher the flux density, i.e. the "harder" the core material is "worked". The wire size determines the loss in the winding while carrying current. The smaller the wire the "harder" the wire is "worked". How hard to work the iron and the copper is determined by such factors as

- a. Permissible temperature rise.
- b. Maximum regulation permitted.
- c. Specified limits, if any, on losses.

Temperature rise depends upon how hard the iron and copper are worked. It depends also upon configuration, type and size of case, potting material, encapsulation, etc. The temperature rise of the windings is usually of primary concern as it most directly affects the life of the insulation separating turns, section, and/or separate windings as well as the insulation to core, case, etc.

For some designs the iron (core) will cool the coil. In other cases the core may be hotter than the windings or be thermally blocked from dissipating heat so that heat dissipation will have to be from the winding itself. Thus the balance between how hard to work the core in relation to the winding depends also on configuration of core and coils, i.e. how the heat will be dissipated. While temperature rise often determines the size of the transformer, in some cases the voltage regulation (drop in output voltage from no load to full load) determines the size of parts. This latter is often true for the smaller ratings.

Since the area of the window is a measure of the amperes times turns, the product of the two areas is a measure of the kva rating at least for a reasonable range of ratings. It is assumed in this regard that the ratio of window to core cross section stays reasonably constant. The percent space used by insulation in the window will usually be less for a larger window since some of the insulation e.g. that from windings to case is a fixed thickness. On the other hand, as the windings get thicker, the heat has farther to travel to be dissipated, so that the hottest spot tends to increase in temperature as size increases. Putting in cooling ducts to reduce rise introduces factors that upset the size of parts required and hence affect the "relative power handling capacity" multiplier to be used to arrive at actual kva parts.

For C cores, the "relative power handling capacity" as given in the tables is the product of dimensions D, E, F, and G. For ring cores, it is the product of D, E, and $\frac{\pi F^2}{4}$. For E cores, it is the product of D, 2E, F and G.

B. Type C Cores—Performance Characteristics and Tests

Curves give the necessary data for calculating transformer designs using Hipersil cores. The curves represent maximum values for finished type C cores. These cores are tested prior to shipment for core loss (true watts, TW) and exciting voltamperes (apparent watts, AW). This exciting volt-ampere test limit includes the exciting volt amperes of the gap formed by the core butt joint.

SINGLE PHASE-12 MIL

Twelve-mil Hipersil cores are available in a wide variety of sizes and shapes for use in transformers and reactors operating in the frequency range of 50 to 400 cycles per second. The induction of transformer designs can be as high as 16,500 to 17,000 gauss, at reasonable exciting currents, thereby permitting savings in size, weight, regulation or combinations of these. Losses are comparatively low even at these high inductions, thus permitting full utilization of the high induction without creating temperature problems.

SINGLE PHASE-4 MIL

Loss becomes a predominant factor in core materials at frequencies higher than about 400 cycles per second.

Peak flux density could be lowered to keep losses at a reasonable value, loss being proportional to some power of B maximum. But this is a waste of material. Or, since losses increase with the thickness of material, they can be reduced by using thinner materials. However, the decreased material thickness must not be obtained at the expense of hysteresis losses or of d-c magnetic characteristics.

Four-mil thick Hipersil magnetic material in Westinghouse type C cores permits:

- 1. full advantage of decreased thickness in reduced losses.
- 2. reduced losses without sacrificing d-c magnetic characteristics.

Even in strips 0.004 inch thick, Hipersil maintains the grain-oriented characteristics so necessary to its excellent d-c magnetic properties and a grain structure which keeps hysteresis losses low.

Four-mil Hipersil in Westinghouse type C cores thus makes possible designs at high frequencies with (1) low losses, (2) low exciting current, with (3) no appreciable reduction in maximum flux density.

Its possibilities in high temperature, class H designs are outstanding, especially in the 320 to 1000 cycle range. The excellent magnetic properties of 4-mil Hipersil permit operation at flux densities as high as 17.6 kilogausses without excessive exciting current. Thus, full advantage can be taken of the ability to work at increased flux densities without the limitations of high losses and exciting currents imposed by poorer magnetic materials. Present type "C" cores can be safely used in designs having 200 C maximum temperature measured by rise in winding resistance.

The 4 mil, series Z, cores are made from very highly oriented silicon steel. Consequently, they will have lower excitation current requirements at high inductions (above 16,000 gauss). This property makes these cores particularly suitable for high temperature rise transformers and other applications where exciting current is the usual limiting design consideration. The core loss of 4-mil, series Z cores, is approximately the same as that of 4-mil, series H cores. Since the high degree of orientation provides a sharp knee to the magnetization curve, 4-mil, series Z cores also have a unique application to chokes and saturable reactors (magnetic amplifiers).

SINGLE PHASE-1 AND 2 MIL

Type C cores in 1 and 2-mil Hipersil are used primarily in pulse transformers. Hipersil C cores, made from highly oriented material give excellent results in pulse transformers. These cores have excellent d-c characteristics.

The familiar, two-piece type C construction makes it a relatively simple job to assemble the core with a coil compared to the tedious process of stacking tiny thin-gauge laminations. Another advantage of the two-piece construction is that a gap can be introduced in the magnetic path to reduce the remanent flux density. The length of the inherent gap in these cores is the same as discussed for the other gauges.

The flux density in a pulse transformer core rises somewhat uniformly during the pulse to a final value at the end of the pulse defined by the equation:

$$B = \frac{E \times t \times 10^8}{N \times A \times 6.45}$$
 gauss

where:

E=peak voltage

B=induction change in gauss (increment of average flux density above remanent value of B)

t=pulse length in seconds

N=number of primary turns

A=net area of the core in square inches

A large flux density change (B) during the pulse is necessary to good pulse transformer design. To accomplish this and still keep the number of turns and the area of the core small, the material used in the core should have low remanent magnetism and a high flux density saturating point. Because these features are inherent in Hipersil C cores, they are most desirable for pulse transformer work.

Pulse permeability is calculated from the formula

$$\mu = \frac{\Delta B \times L_c \times 2.54}{.4\pi N lm} = \frac{2.02 \times \Delta B \times L_c}{N \times lm}$$

where:

 $\mu = \text{effective pulse permeability}$

Im = peak exciting current in amperes

 $L_c = mean length of core in inches = (2F+2G+2.9E)$

 ΔB = induction change in gauss

N = number of turns

Two mil cores in the normal range of sizes when tested with a pulse of 2 micro-seconds, 400 pulses per second, and an induction of 10,000 gauss have a minimum pulse permeability of 600.

All cores are tested by effective methods and quality control measures to insure magnetic quality for different types of application. These include a-c excitation, inductance, and pulse permeability.

For high power pulse transformer applications where higher interlaminar resistance and high pulse permeability are required, Westinghouse offers a superior grade of 2-mil C cores designated by the letter "B" with a minimum of 800 pulse permeability under the conditions set forth above. These cores have several times the interlaminar resistance of regular 2 mil material. They are quoted specially at the factory and are available in all standard sizes.

One mil cores are available in the same sizes and shapes as those shown for the 2-mil cores. They are used for the shorter pulse length applications. When tested with a pulse of 0.25 microsecond, 2500 gauss flux density, and 1000 pulses per second,

the minimum pulse permeability is 300 for normal core sizes. This value may be lower for unusually small or large cores, or if the strip width exceeds one inch.

C CORE TEST GUARANTEES

Core	w/lb	VA/Ib	watts	volt-amperes	kg	cps		
A—12 mil	0.9	1.70	0.9 x lbs	1.70 x lbs+ *5.00 DE	15	60		
H- 4 mil	10.0	13.1	10 xlbs	13.1 x lb +29.9 DE	15	400		
Z— 4 mil	15	39.5	16.9 x lbs	45 x lbs+41.1 DE	17.6	400		
L— 2 mil	2 μ seconds 10 kg—min. perm—600							
B— 2 mil	2 μ s	econds 10	kg-min. pern	n—800				

^{* 5.00} DE is for cores having a maximum allowable joint gap length of .001. For larger cores having a maximum allowable joint gap length of .002 use twice the value.

C. Type E Cores—Performance Characteristics and Tests THREE PHASE—4 AND 12 MIL

Westinghouse has developed three phase Hipersil cores wound from the same highly grain oriented steels that are used in the manufacture of single phase "C" cores. Because of their configuration they are designated as "E" cores. They are available in 4 and 12-mil Hipersil.

The use of "E" cores results in a smaller and lighter weight three phase transformer than is obtained by the use of three single phase transformers. Although the nominal flux densities as used for single phase "C" cores apply, the losses will be somewhat greater because of third harmonics and certain unbalancing factors inherent in this type of construction. All "E" cores are tested to the following maximum limits:

material	nominal flux density	watts total	exciting va
12-mil TA	15,000 gauss	1.1 x lbs	(2.47 x lbs)+ 8.7*A
4-mil TH	15,000 gauss	12 x lbs	(17.8 x lbs)+51.7*A
4-mil TZ	17,600 gauss	18 x lbs	(68.4 x lbs)+71.0*A

A=D x 2E or gross area of leg cross-section in square inches.

^ If 2E exceeds one inch, D2E exceeds $2\frac{1}{4}$ square inches, or F is $1\frac{1}{6}$ or more, or G is $4\frac{1}{16}$ or more, use 17.4A for TA, 103.4A for TH, and 142.0A for TZ cores.

Note these values give the maximum total watts and va losses. Any unbalance in the volts per turn applied to one leg of a three-phase core affects the distribution of flux in the other legs and hence, the exciting va and/or watts. Even with exactly the same voltage per turn applied to each leg, there will be a variation in exciting current per leg. This is caused by variation in magnetic circuits including effective gaps at the joints. The maximum exciting va per leg will seldom be greater than one-third the total va multiplied by 1.2.

D. Ring Type Cores—Performance Characteristics and Tests 12, 4, 2 and 1 Mil

Tape wound Hipersil ring cores are available in numerous sizes for saturable core reactor, current transformer and magnetic amplifier applications. Actual sizes vary in weight over a range of much less than a pound to several thousand pounds. The ring type gapless configuration is characterized by a high saturation density, very high permeability and low hysteresis loss.

Ring type cores will be supplied with any one of the following treatments:

untreated (U)—Magnetic values closely approximate the epstein values of the material.

edgebond (E)—Is a specific Westinghouse Research developed process offering greater mechanical rigidity with a minimum of deleterious effect on electrical quality (usually not over 5%).

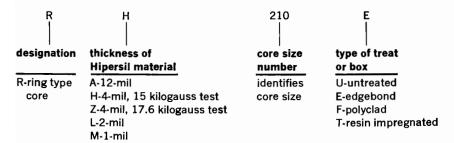
polyclad (F)—Also a Westinghouse developed and patented process providing a covering on the core which permits winding the coil directly on the core without further insulation. Magnetically this process results in slightly higher losses than experienced with edgebonded cores (10%). This is a fluidized epoxy coating capable of 1000 volt insulation test.

resin impregnated (T)—A treatment which is rapidly being superseded by either edgebonded or polyclad because of the relatively large increase in exciting current and losses due to strain effects of the resin impregnation (20-50%).

Cores are tested to assure quality. When specific guarantees are required on ring type cores, refer to Westinghouse.

CATALOG NUMBERING SYSTEM-RING CORES

Westinghouse Hipersil ring type cores are completely identified by catalog number. The following tabulation interprets this coding system for convenient ordering. For example, RH-210E covers a Hipersil ring type core using 4 mil series H material, 210 size, with edgebond treat.



Other uncut Hipersil cores can be furnished in round, oval, and rectangular shapes either untreated, edgebonded, or resin impregnated. For any special electrical or mechanical requirements, refer to Westinghouse.



TRANSFORMER DESIGN METHODS AND FORMULAS

Basically, a transformer is designed to meet some temperature rise limit, some specified maximum regulation and some maximum permissible exciting current value most economically. Actually, however, further limitations as to size, weight, and efficiency may make the final design quite different than it might be if it merely had to meet the requirements of temperature regulation and exciting current. These considerations will determine to a large extent the value of induction B, at which it is desirable to operate the core, and the number of turns and wire size which will go into the coil. Assuming that a value of B has been assigned and that a number of turns, T, has been assumed (giving volts/turn, V/T):

$$A = \frac{3.49 \times V \times 10^6}{B \times f \times T \times SF}$$

where:

V = rms volts

T = turns

B = induction in gauss

A = gross core area in square inches

f = frequency in cycles per second

SF = space factor=95% (for 12-mil Hipersil cores) 90% (for 4-mil Hipersil cores)

Solving this equation gives the gross core area necessary to satisfy the assigned conditions.

Checking the number of turns, wire size, amount of insulation needed and assembly clearances will give an approximation of the core window size required. From the list of standard cores, select one nearest to the calculated gross area (D \times E) and estimated window size (F \times G). This, then will be an approximate design.

To calculate losses and exciting current, proceed as follows:

core weight=KDE (2(F+G)+ π E-1.717R)=KDEL_c

where:

K=0.262 (for 12 mil)

D, E, F, G = core dimensions

L_C = mean length of core flux path

core loss (TW) = weight x TW/pound (see curve)

exciting volt-amperes (AW) = weight x AW/pound

(see curve + gap AW)

gap AW = $1.43 \text{ V/T} \times \text{B} \times \text{L} \times \text{SF}$

where:

V/T = volts per turn of coil

SF = space factor (=.95 for 12 mil cores)

B = induction in gauss

L = total core joint gap length in inches

L=.001 for cores with build-up (E) of 1 inch or less and cross-sectional area 2½ square inches or less and window width (F) less than 1½ inches and window length (G) less than 4½ inches

L=.002 for larger cores

These are the maximum total joint gap lengths of the completed cores.

scale A

If the loss and exciting current calculated above do not meet the desired values, a new trial may be made using other values of V/T and/or B.

When the desired values are obtained, check core dimensions on tolerance drawings and proceed with final transformer design.

Figure 8 Nomograph for transformer design Draw a line from scale A to scale F marking intersection on scale C. Draw line from this point to scale B. Intersection on scale D gives 1. (Wc) (Fc .06 .07 200 в scale B .03 .02 scale D scale C

scale F

WESTINGHOUSE DESIGN METHOD

The initial steps in design procedure are for the purpose of selecting the characteristic linear dimension (ℓ) from the nomograph. Subsequent steps then take this dimension (1) and substitute it in design equations containing dimensionless constants based on core proportions. The characteristic dimension (1) is selected from the nomograph by feeding in known quantities of a design. These known quantities are based on volt-ampere rating, ferquency, temperature rise, working voltage, number of windings and type of iron. Supporting curves assist in supplying such quantities as copper space factor, watts copper loss per unit of coil exposed surface area, and flux density in the core. See figure 8.

A. Selection of Characteristic Dimension (l)

- (1) calculate volt-ampere rating (Wr) For filament transformers Wr is the rated volt-ampere output. For transformers with plate windings the Wr is the average between the secondary voltampere output and the primary volt-amperes.
- (2) calculate copper space factor (F_c)
 - (a) Find the equivalent volt-ampere rating Wr'.

$$W_{r'} = \frac{W_{r}}{\left(\frac{f}{60}\right).76\left(\frac{\Delta T}{40}\right).63}$$

(b) Calculate copper space factor (F_c)

$$F_c = (.08) \log_{10} W_r' + F$$

F is taken from curve in figure 11.

(3) calculate the quantity $\left(\frac{K_0W_r}{f_{E_i}}\right)$

 K_0 for simple type \cong .796 K_0 for shell type \cong .846

 K_o for core type \cong .785

 F_i for wound core \cong .90

(4) calculate
$$\frac{F_cW_c}{\rho S_c}$$

 ρ = 1.15 ohm-cm (copper resistivity)

 $\left(\frac{W_c}{S_c}\right)$ is the watts copper loss per square inch of coil exposed surface from curve in figure 12.

- (5) select flux density (B)
 - (B) is selected from curve in figure 10.
- (6) Find the characteristic linear dimension (1) from nomograph figure 8.

note: Instructions are given on the nomograph.

B. Standard Cores

- (1) Refer to the lists of suggested cores in table A, depending on whether a simple, core, or shell type construction has been chosen. Select the characteristic dimension (l) nearest the value found in step (6). If this value falls between two values of (l) on the suggested core tables, the larger value should be selected. For the remainder of the calculations the (l) selected from the suggested core tables should be used.
- (2) calculate winding exposed surface Sc

$$S_c = K_3 \ell^2$$

K₃ is selected from suggested core table A

(3) calculate copper losses (Wc)

$$W_c = \left(\frac{W_c}{S_c}\right) S_c$$

 $\left(\frac{W_c}{S_c}\right)$ is taken from curve in figure 12.

(4) calculate percent regulation

% regulation=Wc/Wr x 100

(5) calculate copper weight (Mc)

$$M_c = (K_4 F_c \alpha_c) \ell^3$$

K4 is from suggested core table A

 α_c copper density is .321 lbs per cubic inch

(6) calculate turns per volt (N/V)

$$N/V = \frac{K_6}{f \text{ Fi B } \ell^2}$$

B is from curve in figure 10

K₆ is from suggested core table A

(7) determine primary turns (Np)

$$N_p = V_p \left(\frac{N}{V}\right)$$

Vp is the primary rms voltage

(8) calculate secondary turns (Ns)

$$N_s = \left(1 + \frac{\% \text{ Regulation}}{100}\right) (V_s) (N/V)$$

Vs is the secondary rms voltage under rated load conditions

(9) calculate core loss (Wi)

W = (watts/pound) (Mi) (1.25)

Watts/pound from core loss curve in figure 9

M_i is core weight from suggested core table A

(10) calculate exciting volt-amperes (Wex)

(a) W_{ex iron}=(apparent watts/pound) (Mi) (1.25)

Apparent watts/pound from core loss curve in figure 9

(b)
$$W_{ex}_{(butt-joint)} = \frac{(.221) (B) (V_p) (F_i)}{N_p}$$

(11) calculate circular mils per ampere (CM/A)

$$CM/A = \sqrt{\frac{\ell}{\frac{F_cW_c}{\rho S_c}}} (K_5) (F_c)$$

 K_5 is from the suggested core table A F_c was previously calculated in paragraph A.(2)

- (12) determine primary volt-amperes Pri volt-amperes=(Wr + Wc + Wi) + jWex
- (13) calculate primary current (Ip)

- (14) calculate primary wire size

 Circular mils of primary wire=CM/A x Ip

 Use wire size Awg of circular mils
- (15) calculate wire size for each secondary
 Circular mils of secondary=(CM/A) (I_S)
 Use wire size Awg of circular mils

Table A-Constant for Design Equations

	nalons in			weight in lbs	ť		for design			,	
	E	F	Q	IN IDE		Ko	K ₁	Ka	K4	Ks	Ke
IMPLE 1	YPE										
			,,,	.0455	.3515	.765	4.58	16.35	9,56	973	39,600
*	¥16	1/4	<i>y</i> e								
1/2	1/4	¥16	1	.1024	.444	.766	4.85	15.05	8.84	975	35,500
1/2	1/4	916	11/16	.1062	.452	.762	4,8	15.5	8.94	969	36,600
%	Y 16	₩	1	.176	.52	.781	5.19	13.35	8.15	994	31,180
%	7 /16	7/16	1 % is	,199	.56	.794	4.58	14.9	9.39	1010	36,600
3%	₹6	7/16	1%	.362	.669	.745	5.0	15,45	8,64	947	35,700
%	%	1/2	13/4	.388	.705	.765	4.58	16,35	9.56	973	39,600
%	7/16	%1s	111/16	.548	.776	.766	5.26	15.3	9.15	975	33,000
	۱		,						0.05	996	1
.76	7/16	%	119/16	.607 .816	.825 .881	.784 .771	4.43 4.85	15.75 14.7	9.95 8.74	980	44,100 35,100
1	1/2	%								969	
1	1/2	%	21/6	.851	.928	.762	4.8	15.5	8,94		36,600
11/6	Y 16	3/4	2∜≀6	1.205	1.026	.776	4.67	15.4	9.28	988	37,100
11/4	%	34	2¾	1.7	1.126	.751	4.9	15,63	8.83	955	36,600
11/4	1%	3/4	3	1.79	1,152	.743	4.86	16.4	9.02	945	38,100
1%	11/16	19/16	31/4	2.42	1.303	.766	4.51	16.55	9.76	961	40,400
11/2	3/4	13/16	31/2	3.1	1.388	.752	4.74	16.2	9.16	955	38,300
	<u> </u>		1					L			
ORE TY	PE									1	
%	9/82	7/16	9/16	.0274	.28	.68	5.27	14,08	6.46	865	30,100
%	%16	1/4	11/16	.041	.33	.707	4.78	14.3	7,08	900	35,000
1/2	1/32	l ű	*	.070	,378	.695	5,15	13.71	6.47	883	30,75
72 1/2	1/4	Yie.	74 %	.0946	,43	.696	4.96	14.1	6.84	886	33,00
	1		1		J		1				
%	9/32	*	1	.154	.507 .582	.706 .715	4.91 4.86	13,84	6.89 6.98	899 910	32,80
3/4	¥1e	7/16	11/6	.233							
3/4	1%	7/1e	11/4	.309	.627	.691	5.14	13.83	6.62	878	31,80
%	₩	1/2	1% is	.382	.681	.706	4.98	13.61	6.79	897	31,800
%	%	1/2	11/16	.402	.697	.698	4.9	14.28	6.97	889	33,30
1	7/18	9/16	11/2	.585	.778	.70	5.08	13.6	6.68	890	31,20
ī	1/2	56	1%	.74	.844	.702	5.04	13.6	6,72	895	32,000
11/6	1/2	1116	1%	.884	.906	.717	4.86	13.7	7.01	911	32,70
	l	١.,	2	1.25	1.014	.702	4.91	13.85	6.88	895	32,80
11/4	7/16	3/4			1.097	.682	5.2	14.21	6.62	867	31,44
1%	%	%	21/4	1.65							
11/2	1%	7€	21/2	1.975	1,19	.706	4.77	14.4	7.19	897	34,40
1%	**	1	21/2	2.76	1.322	.713	4.96	13.45	6,85	905	32,10
BHELL T	YPE										1,4
	1.	1,	Τ,	.0382	.286	.85	2.42	7.88	9.14	1080	36,70
76	7/32	1/4	3/4	,0382	.336	.85	2.42	7.42	9.14	1069	38,40
76	1/6	9 ∕16	7/8							1059	41,00
% % %	1/6	9/15	1	.0722	.348	.828	2.49	6.95	9,89		
₩	9 /32	1 %	11/4	.1312	.426	.834	2.39	7.64	9.07	1061	36,90
₩	%15	7/1e	11/4	.224	.504	.84	2.29	8.16	8.68	1069	34,30
%	¥⁄ie	1/2	11/2	.26	.545	.843	2,51	7.16	9.88	1071	40,00
*4	7/32	% 16	11/2	.382	.61	.854	2.42	7.96	9.16	1086	36,10
% % % %	7/32	9 ∕15	1%	.424	.634	,837	2.46	7.38	9.5	1064	38,90
%	1/4	%	1%	,528	,685	.834	2.482	7.18	9.7	1060	39,80
% %	1/4	11/16									
			2	.658	.741	.85	2.76	7.28	9.86	1080	39,80
1	7 32	*	2	.876	.806	.857	2.42	7.88	9.45	1090	36,70
1	9/16	19/16	21/4	1.068	.87	,849	2,475	7.46	9.66	1080	38,40
		1	1	1	.937	.852	2.536	7,35	9,94	1082	1
11/6	%/ie	%	21/2	1,308	.93/	,052	2.530		9.94	1082	39,65
11/6 11/4	%ie %a	1%	21/2	1,308	1.06	.852	2.48	7.5	9.94	1082	39,65 38,40
	% % %										

SYMBOLS USED

- Wr rating, volt-ampares

- wr reang, volt-amperes

 F_c copper space factor

 F_i iron space factor

 B flux density, kilolines per square inch

 f requency cycles per second
- Ac window area, square inches
- window area, square inches
 γ rms potential, volts
 Δ temperature rise, degrees centigrede
 ¢ characteristic linear dimension, inches
 ρ conductor resistivity, microhm-inches

- I rms current, amperes
 W_C winding loss, watts
 N turns of a winding
 W_I core loss, watts
 W_M exciting voltamperes
 M_C copper weight, ibs
 M_I fron weight, ibs
 K_D, K_I, K_N, K_A, K_S, K_C are constants used with design equations
 α_I density of Iron, pounds per cu. in,
 α_C density of conductor, pounds per cu. in.
 S_C exposed area of coil surface, square inches

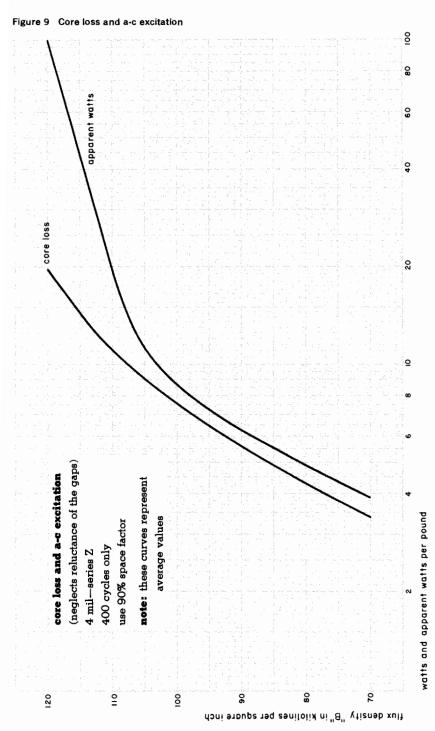
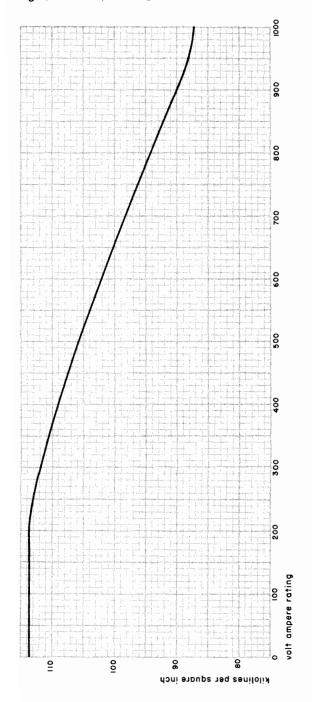
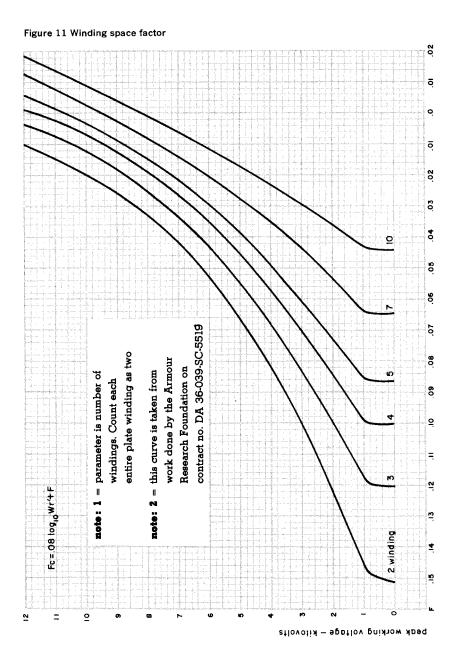


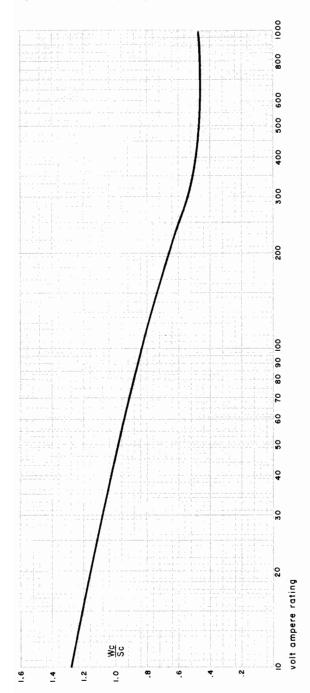
Figure 10 Volt ampere rating and flux density





April 15, 1965

Figure 12 Copper loss per square inch of exposed surface



FILTER REACTOR DESIGN METHODS AND FORMULAS

The design and choice of core for reactors depend upon three inter-related factors:

- 1. desired inductance
- 2. direct current
- 3. alternating volts

The type C Hipersil core lends itself very well to these applications because the air gap can be regulated or set to any desired value and because the incremental permeability is comparatively high even at high d-c inductions. The inductance of an iron-core reactor is dependent on the effective length of the magnetic path. This effective length is the sum of the air gap and the ratio of core mean length to incremental permeability.

$$L = \frac{3.2 \times T^2 \times A \times 10^{-8}}{Ig + \frac{Ic}{\Delta \mu}}$$

where:

L = inductance in henries

T == turns

A = gross core area in square inches

Ig = effective air gap length in inches

Ic = core mean length in inches

 $\Delta \mu = \text{incremental permeability}$

The value of $\Delta\mu$ depends on the values of alternating and direct flux densities in the core. The sum of these densities should not exceed saturation value. Incremental permeability is shown by curves (figures 16, 24, and 29) at various values of Hd-c (coersteds of direct mmf on the core) for different values of alternating flux densities.

A designer must select a combination of core area, air gap length and number of coil turns necessary to give the proper inductance, maintaining values for Bd-c and Ba-c which will not cause magnetic saturation and which will permit the highest inductance for a given volume of core material used. The core opening size will depend on the turns, wire size and insulation requirements.

For reactors carrying direct current and operating at very low alternating flux densities, a simple design method was originated by C. R. Hanna ("Design of Reactances and Transformers which Carry Direct Current," Jour. A. I. E. E., vol. 46, Feb. 1927, p. 128). A more detailed treatment of the design of reactors is presented in "Electronic Transformers and Circuits," by Reuben Lee, John Wiley & Sons, 1955.

BALANCING TRANSFORMERS USED WITH SILICON RECTIFIERS

Balancing transformers, as a means of forcing proper current balance, have been the subject of several technical papers and articles. Their effectiveness has been well established. These balancing transformers, or reactors as they are sometimes called, consist of laminated iron cores, usually with single turn primary and secondary windings. The currents from two cells in parallel pass through a core in opposite directions, and an unbalance between the two currents will induce a voltage which tends to correct the unbalance.

Varied designs and mechanical arrangements of cores have been used but will not be discussed here. Figure 13 is a pictorial view of an arrangement of hipersil iron "C" cores.

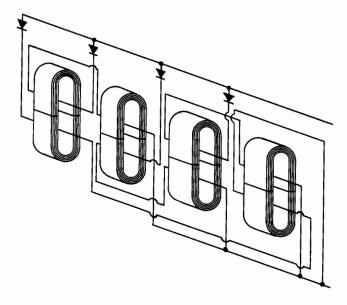


Figure 13 Hipersil iron "C" cores connected in a "chain" arrangement with four cells in parallel.

A core area of one to one and a half square inches has been found effective in reducing the unbalance between high power cells in parallel. An effective air gap of at least .001 inches should be retained in the core to reduce the possibility of saturation. The unbalance may be reduced to less than ten percent of the average current per cell with as many as six cells in parallel. With up to six cells in parallel, the cells should be operated at 90 per cent of their rating; with seven to ten cells in parallel, 85 per cent of their rating; and with 11 to 20 cells in parallel, 80 percent of their rating. In any design, current division among the cells should be measured to assure proper balancing. This may be done quite simply by inserting a shunt in place of the fuse. If the fuses are calibrated and checked for uniformity the voltage drop across the fuses will be an indication of the current division. It may not be desirable to place more than 20 cells in parallel, unless a separate transformer is used for each group of 20 cells.

Separate transformers or transformer windings may be used to supply a number of assemblies each with only one cell in parallel. Then the output of these assemblies may be connected in parallel. If separate transformer windings are used, care must be taken in the transformer design. Multiple windings on any one transformer core will not necessarily have the identical leakage reactances required to force division of current between assemblies.

If a series parallel arrangement of rectifying cells is necessary, no set rule exists which will determine whether the seriesing or the paralleling should be done first. Each has its advantages and disadvantages, depending upon the heat sink design, required fusing, necessary reliability, etc. Individual applications will determine which is most economical or practical.

CURVE DATA

Figure 14 Core loss curve • Single phase • 12 mil

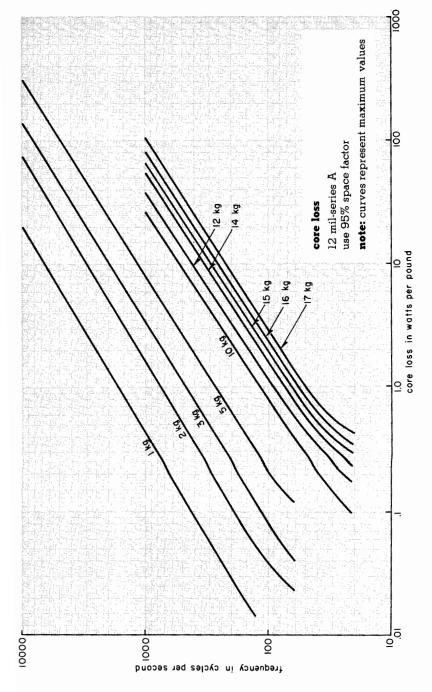


Figure 15 A-c excitation curve • Single phase • 12 mil

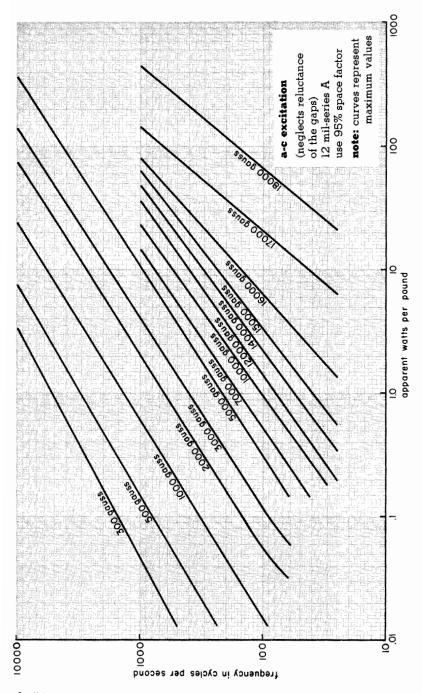


Figure 16 Incremental permeability . Single phase . 12 mil

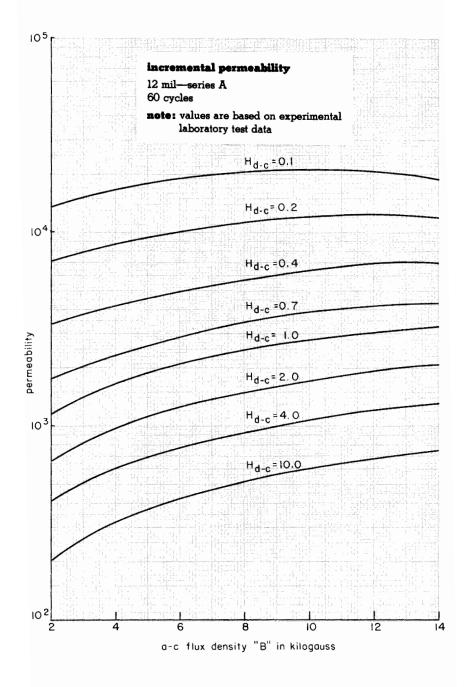


Figure 17 D-c magnetization curve • 12 mil • series A

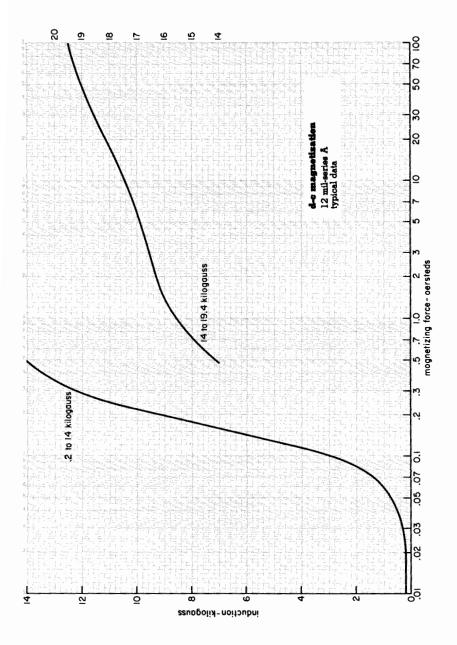


Figure 18 Core loss curve • 4 mil • series H

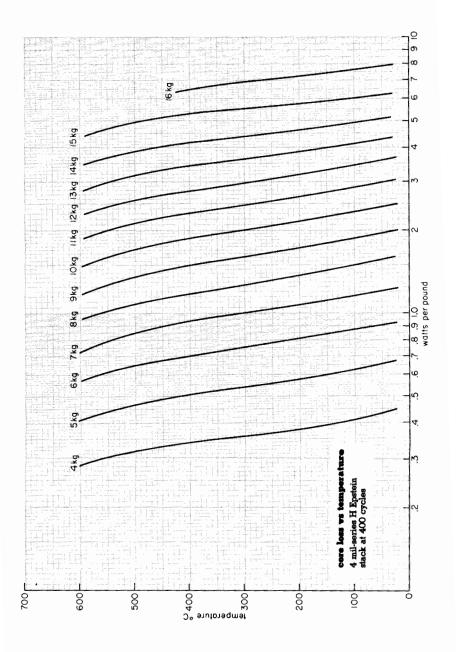


Figure 19 Watt per pound • series H

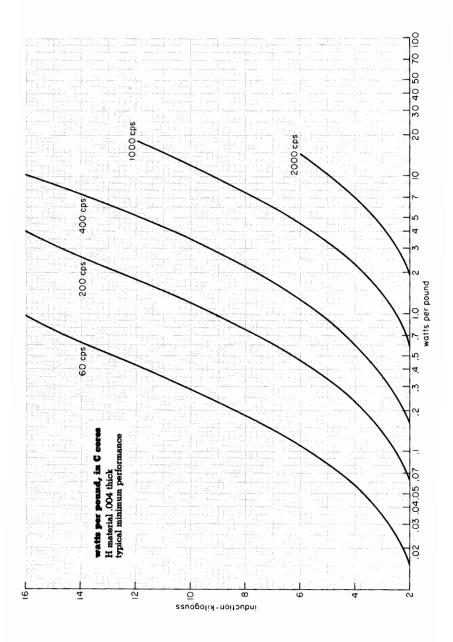


Figure 20 V-a per pound • series H

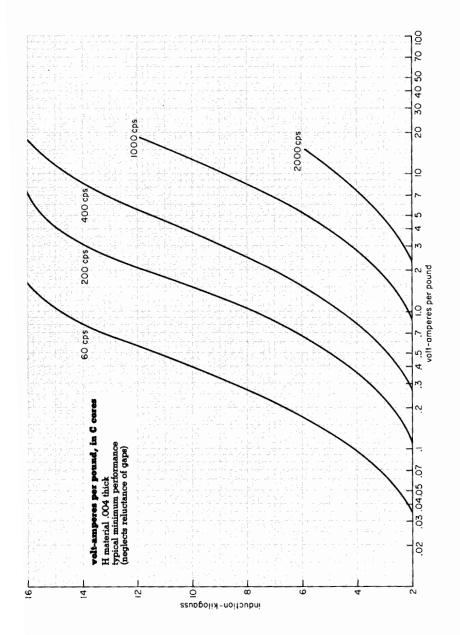


Figure 21 D-c magnetization • 4 mil • series H

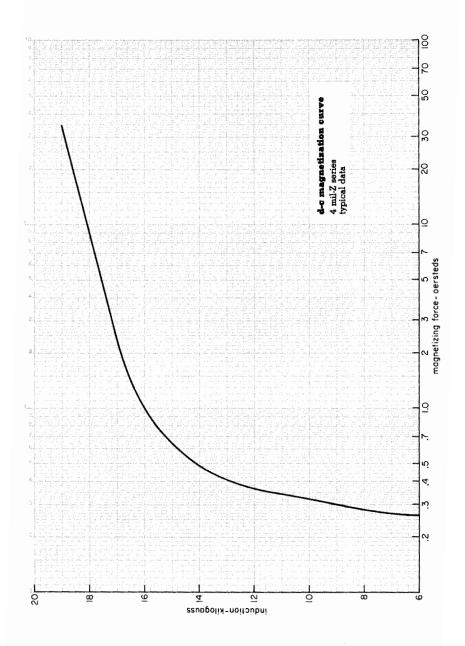


Figure 22 Core loss and excitation curve • single phase • 4 mil

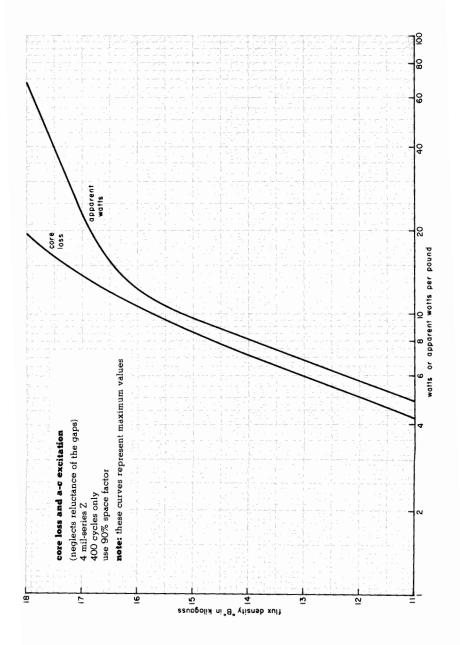


Figure 23 D-c magnetization • 4 mil • series Z

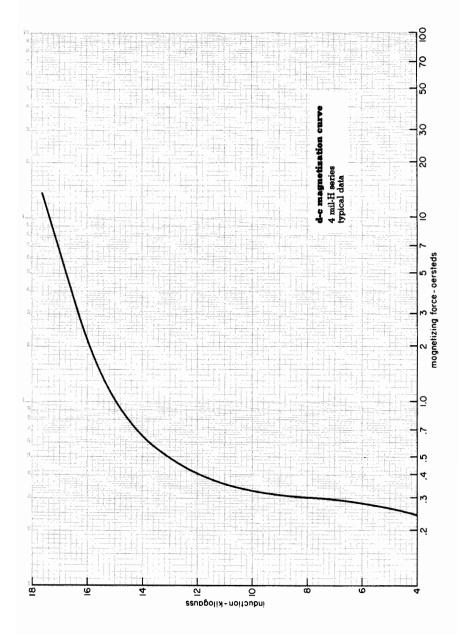


Figure 24 Incremental permeability • single phase • 4 mil

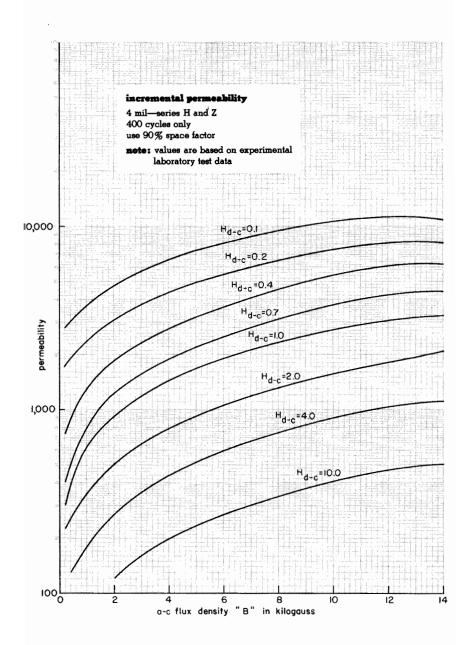


Figure 25 Core loss curve • single phase • 2 mil

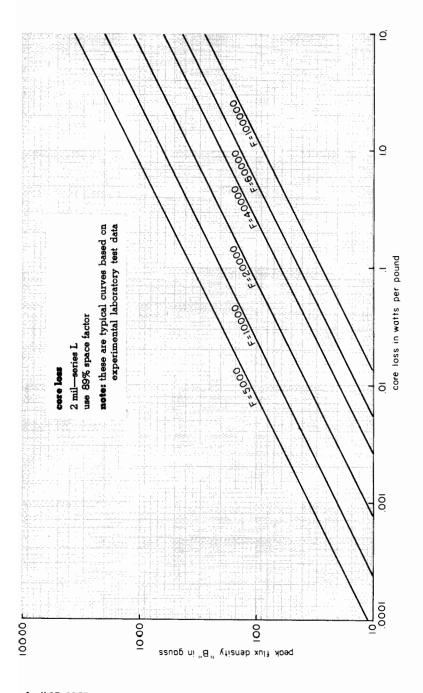


Figure 26 A-c excitation curve • single phase • 2 mil

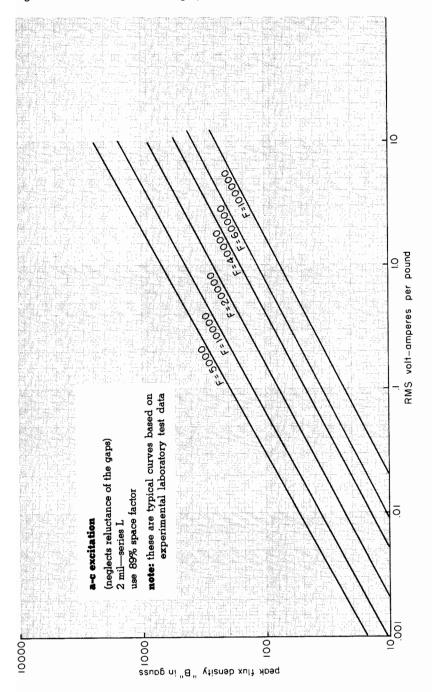


Figure 27 Pulsed excitation curve • single phase • 2 mil

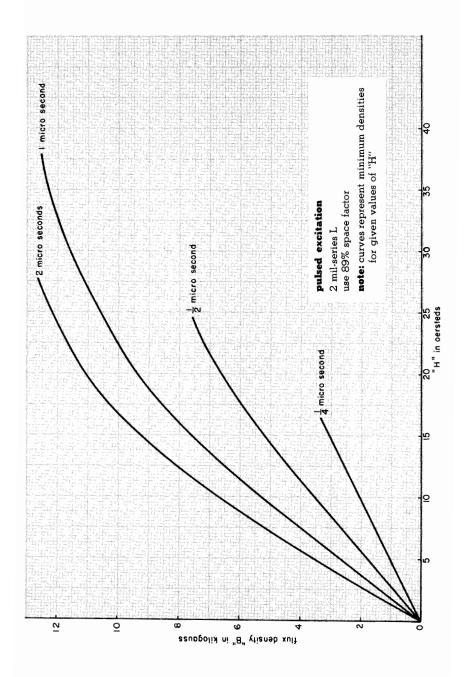


Figure 28 Pulsed core loss curve • single phase • 2 mil

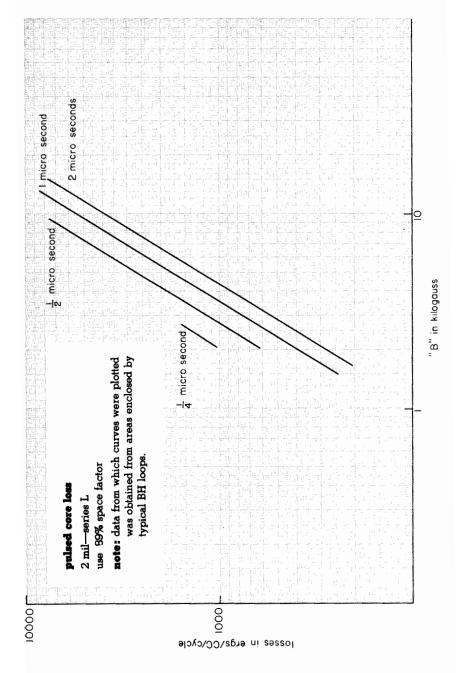


Figure 29 Incremental permeability • single phase • 1 and 2 mil

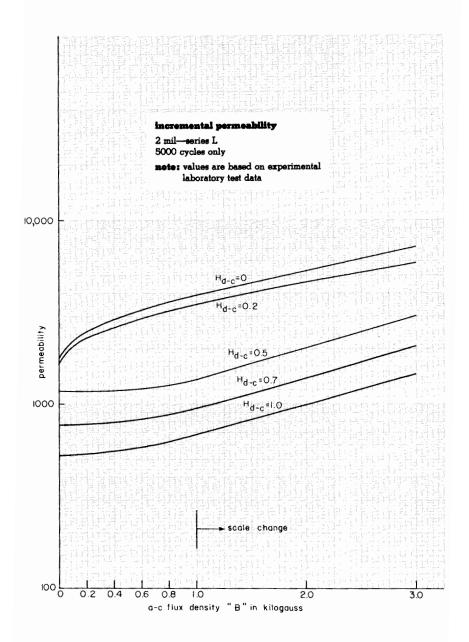
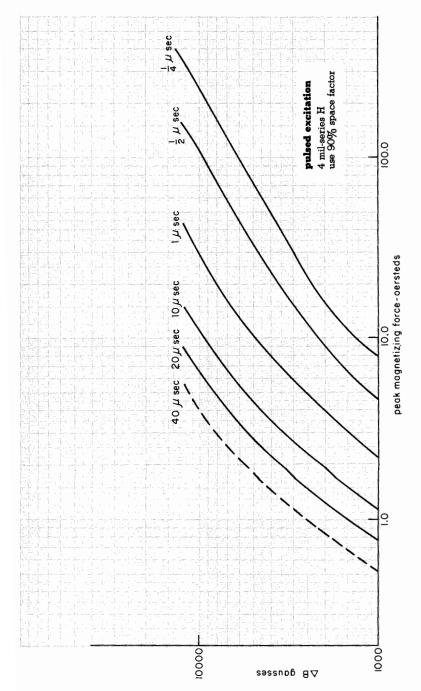


Figure 30 Pulsed excitation curve • 4 mil • Series H



MECHANICAL TOLERANCES

The mechanical tolerances of ring, C and E cores are shown in technical data 46-760. For type C cores, these are as adopted by the Electronic Industries Association and specified in Standard RS-217.



ASSEMBLY OF CORES WITH COILS

Assembly of Small Cores

Place the coil over the bottom section/sections of the core carefully to avoid gouging the insulation of the coil tube. Although small cores usually do not require a joint compound treatment, joint surfaces should be cleaned with a dry paintbrush or dry compressed air before assembly.

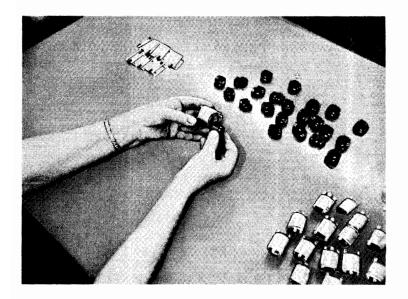


Figure 31 Core/coil assembly

POSITIONING THE BRACKET AND CORE

Next, the mounting bracket is placed in position. The band is pulled around the bracket and under the core.

ASSEMBLY OF UPPER CORE SECTION ON BOTTOM SECTION

The upper section is lined up with the catalog number marking on the core bottom section and is lowered into the coil with special care to insure that:

- -the coil is not gouged
- -no foreign material is carried into the joint.

For class F or H use, for 3 phase cores, or if noise is a problem, apply joint compound 1454 892 with an oil can (3-4 drops/sq. in.) to the bottom core half joint surfaces.

The upper section should be well-seated on the bottom section and in alignment with it.

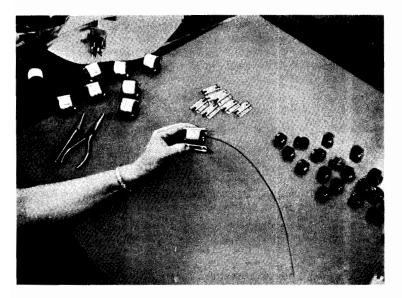


Figure 32 Bracket placed in position—band pulled around core and under bracket

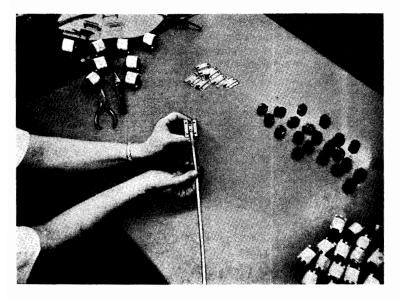


Figure 33 Seal on band-band pulled tight

BANDING OF SMALL CORES

Table B (Page I-1) should next be consulted to determine the size and number of bands to be utilized, and the seal style number for the particular core to be banded. The band(s) are placed around the core and the seal slipped over the end of the band and the band is bent inward under the seal. The starting end should be long enough to extend around the corner of the core.

The free end of the band is inserted into the jaws of stretching tool style number 1263 732 and the band is pulled up snugly to the core.

The core sections are than aligned, and the bands located parallel to the edge of the core at all points.

BAND SEAL AND CUTOFF

The band is now crimped, soldered or spot-welded to the seal with the banding tool in place. (In soldering operations, a minimum of rosin soldering fluid should be utilized. Solder consisting of 60% lead and 40% tin is recommended.)

After the seal is fastened, the banding tool is removed by pressing the release lever and excess banding is trimmed off by means of standard tin-snips.

WEDGES OR FILLERS

If coil wedges or fillers are used between the core and the inside of the coil to provide uniform spacing or centering, they should be designed for only a moderately tight fit so that there will be no danger of preventing the core joint from closing.

MOUNTING BRACKETS OR (FRAMES)

If the brackets are designed so that they extend around the edge of the core, insulation should be used so that laminations are not shorted together.

Also, the brackets should be so designed so that no force is transmitted to the core other than that developed by the band. High exciting current or high loss may be produced if these precautions are not observed.

note: Appendix A shows a series of mounting brackets that may be used for simple core-coil construction.

Lastly, the insulation between the core and the frame causes the core to "float" electrostatically. It is necessary, therefore, to ground the cores to the brackets through a metallic connection (usually a copper braid under the banding strap to the frame) to prevent static discharge.

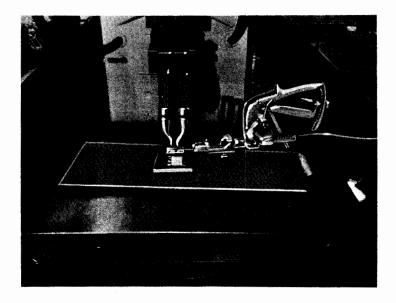


Figure 34 Band pulled tight with stretching tool—ready for spot welding

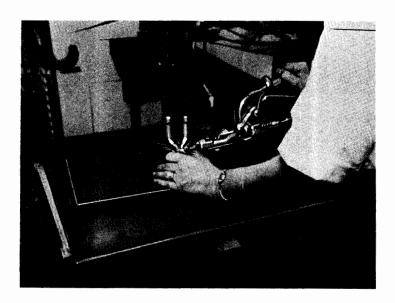


Figure 35 Spot welding—(note sparks)

ASSEMBLY OF LARGE CORES (11 LBS AND OVER)

When assembling large type C cores, the same general procedures are followed as for small cores except that a larger band is used with ¾ inch, crimp-type seals.

Strip all protective material from the cores and remove any traces of adhesive residue with a clean rag dampened with acetone. If necessary, buff the joint surfaces lightly with a motor driven soft steel wire brush. Maintain brush rotation in the plane of the laminations.

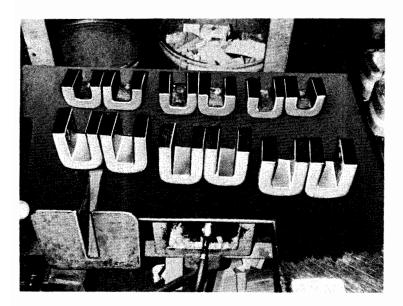


Figure 36 Cores laid out for assembly—bottom yoke insulation in place

Assemble the bottom core halves, coils, and any inter-core insulation. Check to be sure no foreign material is on the joint surfaces. Apply compound style number 1454 892 with an oil can (3-4 drops/sq. in.) to the bottom core half joint surfaces. Then lower the core caps into place, along with the top intercore spacers (when used). BE VERY CAREFUL NOT TO SCRAPE ANY FOREIGN MATERIAL INTO THE GAP DURING THIS OPERATION.



Figure 37 Coils lowered into place—top yoke insulation shown in position

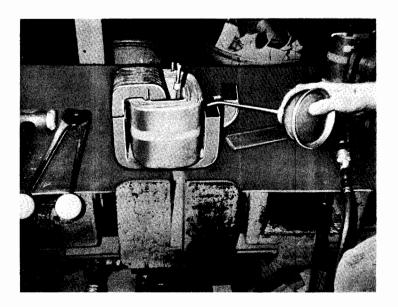


Figure 38 Applying joint compound

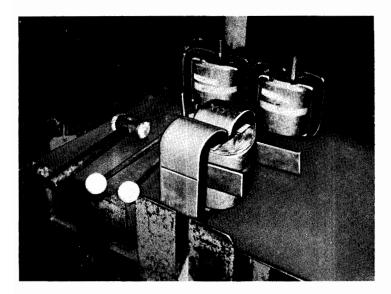


Figure 39 Core section in position—(wedges are to align core halves and will be withdrawn later)

Oscillate the halves to spread the compound and reduce joint thickness to a minimum; and band per next paragraph within five minutes after compound application. In most cases, this will necessitate assembling and banding one core at a time.

Place the required number of bands around each core, exercising care that they do not snag any laminations at the joint. Slide a seal on each band, with the pressed rib inside. Bend the lower end of the band back under the seal so this end reaches to at least 45° point of the core's corner radius when the seal is in position.

Set the air pressure for the Acme BID6 banding tool to the value marked on the calibration tag for the tension desired with the tool running idle. Slip the tool on the band and gradually pull up the latter by intermittently operating the air valve while tapping the core parts. Meanwhile, adjust the seal and band positions to secure proper register. Then pull the band to its rated tension by stalling the tool. The air valve must be left on while crimping the seal.

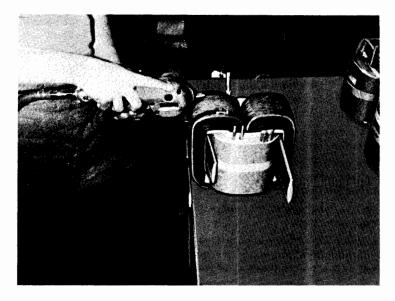


Figure 40 Application of bands—Acme B106 stretching tool in use

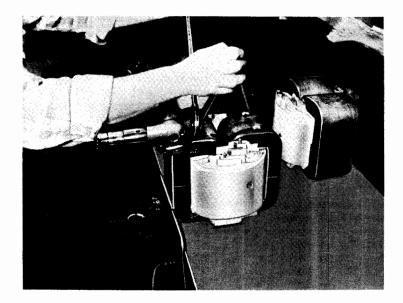


Figure 41 Seal being crimped

The loop end of the seal may be tapped with a mallet to flatten the band into good conformity with the seal. This arrests a tendency for the band to tear into the seal.

Keep the seals away from the core joint; and alternate them to prevent mutual interference. Adjacent bands should be at least 1/4" apart so the banding and crimping tools will not bear on any previously installed band.

Place the first band near the center of the core. Then tighten additional bands in order from this first band outward to the core edges.

Position the crimping tool squarely on the seal and operate it so minimum band lift occurs. Improper operation will result in a loose band.

Cut two crimps in each seal. The first should be nearer the nose of the banding tool. Tool wear and pressure will affect the depth of crimp; so periodic checks should be made to be sure the crimp marks cut through the seal and into the band.

Break off the band by elevating the rear of the banding tool while holding its nose firmly against the core.

The BID6 tool must be operated on clean, lubricated air. This may be provided by installing a filter, oiler, and regulator at each work station. Adjust the oiler so a slight deposit of oil is maintained around the tool vents. ASE-10 motor oil should be used.

Grease the rear bearing fitting once a week with #2 AGMA EP gear oil (Socony Gargoyle Compound AA or equivalent). Clean the rotary dog and pusher parts occasionally; and calibrate the tools on a regular basis ($\pm 10\%$).

The assembly should then be baked at 125-135°C and held at this temperature for three hours after reaching temperature.

If it becomes necessary to disassemble a core/coil assembly that contains baked joint compound, preferred technique is to heat the assembly to a temperature of 125°-135°C. Dismantle while the assembly is still hot, to minimize possible core damage.

If shop facilities are such that reheating is impractical, break the core joints by striking the core sides a sharp blow with a rawhide mallet. Clean all compound from the joint surfaces by wire brushing as in Section 1; and wipe these surfaces clean with an acetone dampened rag.

The following table may be used as a guide in determining the proper number of bands for a given core.

TABLE I

core dimensions (cross section in square inches—one leg)	band size	number	tension (pounds)
3.0 to 4.25	³4″ x .035″	1	900
4.25 to 6.0	3/4" x .023"	2	600
6.0 to 9.0	34" x .023"	3	600
9.0 to 13.5	¾″ x .035″	3	900
13.5 to 18.0	¾″ x .035″	4	900

This table is based upon a recommended core pressure of 200-300 psi. For larger cores, add bands as necessary to maintain this range.

Certain cores of relatively narrow strip width may not accommodate sufficient bands to develop 200 psi. In such cases, the minimum pressure may be shaded to 150 psi. This should be regarded as an absolute minimum.

Cores with an extremely low D/E ratio may require special clamping arrangements.

example:

A core of 71/2" strip width and 5" buildup is to be banded.

7½ x 5=37½ in² x 200 psi=7500 pounds 150 psi=5600 pounds

Normally, this core would require 9 bands ($\frac{3}{4}$ " x .035") pulled to 900 pounds each. 9 x 900=8100 pounds

Common practice is to allow at least $\frac{1}{4}$ " spacing between bands; and the application of 9 bands is not considered feasible.

Seven bands will permit the required spacing; and their cumulative tension (7 x 900= 6300 pounds) is above the absolute minimum. Hence, seven bands can be used with this core for all but the most critical applications.

CORE BANDING TECHNIQUE

Table II. Determining the Size and Number of Bands

(Select band, seal and tension according to core size in this table)

core dimensions (1 leg)		banding strap		seal		banding tool	
cross section area in sq. in. (D x E)	width of strip in core-inches	size in inches	no. used	style number	size in inches	style number	tension in pounds
.188 or less	any	3/6 x .006 ⊚	1	1304 065	3/16 x 1/4	1263 732	37.5
.188 to .375	% or larger	% x.006 ⊕	1	1294 363	% x %	1263 732	75
.375 to .75	% to 1½	% x .012 ⊕	1	1294 363	% x ⅓	1263 732	150
	1% or larger	% x.006 ⊕	2	1294 363	% x ⅓	1263 732	75
.75 to 1.5	½ to 1⅓	% x .012 ⊙	1	1294 363	%ax %a	1263 732	150
	11/4 or larger	% x .012 ⊙	2	1294 363	3⁄8 x 3∕8	1263 732	150
1.5 to 3.0	34 or larger	34 x .023 ①	1	1293 783	% x 1%	Acme ⊙	600
3.0 to 4.25	3/4 or larger	¾ x .035 ⊙	1	1293 783	% x 1%	Acme	900
4.25 to 6.0	2 or larger	¾ x .023 ①	2	1293 783	% x 1%	Acme	600
6.0 to 9.0	3¼ or larger	¾ x .023 ①	3	1293 783	% x 1%	Acme	600
9.0 to 13.5	3¼ or larger	3/4 x .035 ⊚	3	1293 783	% x 1%	Acme	900

joint compound-style number 1454 892 (1 quart)

- Style number 1629 485
- Style number 1629 486
- 3 Style number 1629 192
- Style number 1629 191
- Style number 1629 190
- Air operated banding tool model B1D6 for ¾" strap may be obtained from:

Acme Steel Products 2840 Archer Ave., Chicago 8, Illinois

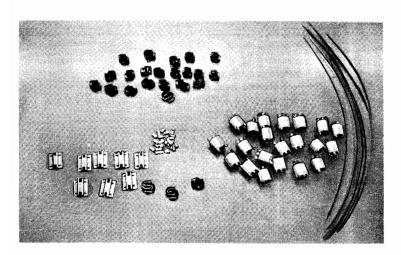


Figure 42 Cores, seals, mounting brackets, coils and bands laid out for assembly

Banding Tool (Style Number 1263 732)

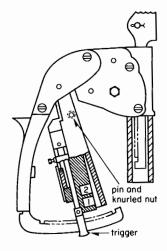


Figure 43 Banding tool, 150 pounds pressure used for smaller cores

The band stretching tool is shipped adjusted for 150 pounds of pressure. In operation, the nose of the tool is placed against the band seal, with the band running between the fixed and hinged portions of the nose and on back between the small platform and the dog on the side of the tool toward the reel. The handle is squeezed upward and allowed to drop. When the pre-set tool pressure is reached, the latch is tripped, preventing further tightening of the band. Specific pressures required for banding are as follows:

pressure	hole ∦1	hole #2	
37½ pounds	bright spring	black spring	
75 pounds	bright spring on foot	black spring on foot	
150 pounds	bright spring on foot	bright spring on foot	

To change tripping pressure, all that is necessary is to:

- -remove knurled nut from pin through the handle
- -withdraw pin
- -open handle and arrange the springs in accordance with the above outline.

Check calibration of banding tools frequently.

APPENDIX A

Mounting Brackets

Spot-Weld Cradle and Base Together (with E = number of spots)

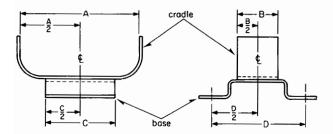


Figure 44

group	dimension	s in inches			E (no. of	core reference
	A	В	С	D	spots)	
1 2	1%6 1%	½ %	15/16 15/16	1¼ 1¼	2 2	Z-98 Z-99

Spot-Weld Cradle and Base Together (with E = number of spots)

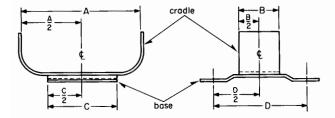


Figure 45

group	dimensions	in inches			E (no. of	core reference
	A	В	С	D	spots)	Telefalica
15 16	1% 1%	½ %	15/ ₁₆ 15/ ₁₆	1¼ 1%6	2 2	Z-98 Z-99

Spot-Weld Cradle and Base Together (with E = number of spots)

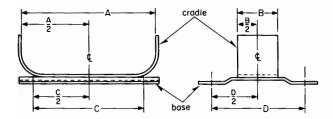


Figure 46

group	dimension	s in inches			E (no. of	core
	A	В	С	D	spots)	reference
3	113/16	5/8	111/16	17/16	2	Z-100
4	23/8	3/4	21/8	13/4	2	Z-101
5	21/2	3/4	21/8	1¾	2	Z-102
6	2%16	7∕8	21%4	255/64	2	Z-103
7	213/16	7∕8	25/8	21/8	4	Z-104
8	215/16	1	25/8	21/8	4	Z-105
9	35/8	1	3	21/16	5	Z-106
10	31/16	11/8	3	21/16	5	Z-107
11	41/16	11/4	35/16	211/16	5	Z-108
12	413/16	11/4	311/16	3	5	H-499
13	41/16	11/2	3	21/16	5	H-500
14	51/16	11/2	311/16	3	5	H-501

Spot-Weld Cradle and Base Together (with E = number of spots)

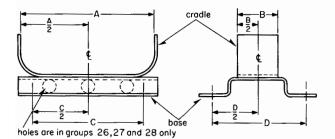


Figure 47

group	dimension	s in inches			E	core
	A	В	С	D	(no. of spots)	reference
17	113/16	5/8	111/16	17/16	2	Z-100
18	2%	3/4	21/8	13/4	2	Z-101
19	21/2	3/4	21/8	13/4	2	Z-102
20	2%16	7 ⁄8	21%4	155/64	2	Z-103
21	213/16	<i>7</i> ⁄8	25/8	21/8	4	Z-104
22	215/16	1	25/8	21/8	4	Z-105
23	3%	1	3	21/16	5	Z-106
24	37/16	11/8	3	27/16	5	Z-107
25	41/16	11/4	35/16	211/16	5	Z-108
26	413/16	11/4	311/16	3	5	H-499
27	41/16	11/2	3	21/16	5	H-500
28	51/16	1½	311/16	3	5	H-501

APPENDIX B

Core Listing

by relative power handling capacity



catalog number		sions in	inche		relative	weight:	catalog number	dimen		_	s	relative power	weigh
aumber	atrip width D	build up E	win- dow width F	win- dow length G	handl'g capac'y	pounds	димьег	strip width D	build up E	win- dow width F	win- dow length G	handl'g capac'y	pount
12 mil							12 mil						
	Γ												
A-52	3∕8	3/16	7∕8	11/4	.078	.086	A-399	11/4	1/2	1/2	13/4	.548	.97
A-424	5/8	1/4	3/8	13/8	.081	.171	A-205 A-416	11/2	3/8	5/8	19/16	.55	.80 .98
₽A-1 A-889	5% 7∕8	1/4	1/2 5/-	11/8	.088	.161 .224	+A-583	3/4 11/8	3/4 1/2	5% 5%	19/16 19/16	.55 .55	.89
A-210	/8 3/8	1/4	5/16 5/8	15/16 19/16	.092	.127	A-626	2	1/2	78 1/2	11/8	.563	1.24
-A-2	3/4	1/4	1/2	11/8	.106		+A-8	11/4	3/8	5%	115/16		.70
A-252	5/8	5/16	1/2	11/8	.11	.21	A-713	13%	7/16	5%	19/16	.587	.88
A-231	3/4	5/16	1/2	1	.117	.236	A-358	7/8	7/16	5%	21/2	.598	.74
A-373	3/4	9/32	7/16	13%	.127	.225	+ A-6	1	5/8	5/8	19/16	.611	1.03
A-335	3/4	9/32	9/16	11/8	.134	.229	A-375	1	1/2	1/2	21/2	.625	.90
A-584	1	5/16	1/2	1	.156	.317	A-227	1	5%	5/8	15%	.635	1.12
A-232	7∕8	3/8	1/2	1	.164	.35	+A-758	11/2	5%	7/16	19/16	.64	1.43
⊧A-4	3/4	3/8	7/16	13/8	.169	.324	A-80	1	17/32		115/16		.9:
A-325 A-479	, 5%	9/32	5/8	19/16	.172	.238 .266	A-374 A-168	1	3/8 5/	3/4 5/8	25/16	.65	.6 1.0
A-327	3/4	5/16	11/16	19/16	.172		+A-326	3/4	5% 5%	78 5%	21/2	.66 .66	.8
A-279	5/8	1/2	7/16	13/8	.188		A-354	1 74	11/16		19/16	.672	1.1
A-57	78 5/8	5/16	5/8	19/16	.191	.268	A-118	5%	5/8	3/4	25/16	.677	8.
A-669	78 7/8	7/16	1/2	11/8	.215	.452	A-114	11/2	3/8	5%	115/16		9.
A-463	3/4	5/16	5%	19/16	.228	.322	A-129	3/4	3/4	5/8	115/16		1.0
A-207	5%	5/16	5%	115/16	.236	.306	A-69	1	5%	5/8	13/4	.684	1.0
A-280	5∕8	1/2	5/8	11/4	.245	.427	A-406	5/8	5/8	15/16		.686	.7
A-250	11/4	1/4	3/8	21/4	.263	.477	A-260	.5%	1/2	1	21/4	.704	.6
A-853	1	7/16	1/2	11/4	.273	.543	A-60	1	13/32	3/4	25/16	.705	.7
A-141 A-605	1	9/32	5/8	19/16	.275	.382 .617	A-242 A-261	11/4	15/32	5% 5%	2 1 15/16	.709 .71	.9 1.1
A-005	l i	1/2 3/8	1/2	11/8	.281	.514	A-201 A-596	11/4	9/16 3/8	78 5/8	21/2	.733	.8
-A-434	3/4	1/2	1/2	19/16	.294	.547	A-726	7/8	5/8	3/4	113/16		1.0
A-128	11/8	7/16	7/16	13/8	.296	.59	A-148	11/2	3/8	11/16			ق. ا
₽ A -5	1	5/16	5/8	19/16	.305	.43	+A-9	11/4	1/2	5/8	115/16	.757	1.0
A-349	7/8	11/32	5%	111/16		.44	+A -161	1	7/16	3/4	25/16	.758	.8
A-776	11/8	7/16	1/2	15/16	.323	.63	A-494	11/4	5/8	5/8	19/16	.762	1.2
A-243	1	1/2	1/2	15/16	.328	.665	A-200	7/8 12/	3/8	15/16	21/2	.768	6.
A-87	1	7/16	1/2	19/16	.342	.62	A-458	13/8	7/32		2 214	.768	.8 .9
A-395 A-746	1 3/	1/2	7/16 5/	19/16	.342	.716 .583	A-312 A-85	1 1/8	7/16	5/8 13/16	2½ 1¾	.77	.9
A-415	1 3/4	1/2 5/	5/8 5/	19/16		.492	A-05 A-321	13%	3/8 15/ ₃₂		23/16	.792	1.1
A-24	l i	5/16 1/2	5/8 1/2	19/16	.376	.732	A-321 A-402	11/8	1/2	1/2	213/16		1.1
A-341	li	15/32	1/2	13/4	.411	.72	A-402 A-271	11/2	7/16	5/8	115/16	.794	1.1
A-432	3/4	7/16	3/4	113/16		.55	+A −10	11/4	3/8	3/4	25/16	.814	.8
₊∧ -7	1	3/8	5%	115/16	.453	.613	A-702	11/2	9/16	5%	19/16	.823	1.3
A-831	3/4	5/8	5%	19/16	.458	.754	A-470	1	11/16		115/16		1.2
A-774	11/8	1/2	5∕8	15/16	.462	.786	A-314	13/8	5∕8	5/8	19/16	.839	1.4
A-712	11/4	7/16	5∕8	13/8	.469	.748	A-45	11/8	5/8	5/8	115/16		1.2
A-376	1	7/16	5/8	13/4	.478	.693	A-50	1	17/32	1	15%	.863	.9
+A-81	1	1/2	5/8	19/16	.489	.765	A-195	1	1/2	3/4	25/16	.867	.9
+A-747	11/2	1/2	7/16	19/16	.512	1.07	A-256	1	1/2	3/4	25/16	.867	1.0
A-25 A-225	11/4	3/8	11/16		.525	.70	A-714	11/2	9/-	11/16	2 111/16	.871 .878	1.0
A-225 +A-163	1	1/2	5% 5/	111/16		.797	A-295 A-785	11/4	9/16	5/8 3/		.887	1.0
4-W-102	1	7/16	5/8	1 1 5/16	.529	.735	W-192	15/16	7/16	3/4	21/16	002	, 1.0

[•] preferred core sizes: These cores should be used wherever possible in designing new transformers. They are subject to maximum discount regardless of quantity ordered. See selling policy 46-700.



atalog	dimen	sions in	inche	. !	relative	weight:	catalog	dimen		inches		relative power	pounds
umber	strip width	build up	win- dow width F	win- dow length G	power handl'g capac'y	pounds	number	strip width D	build up E	win- dow width F	win- dow length G	handl'g capac'y	
2 mil	D	E A	<u> </u>	<u> </u>		'	12 mil	series	A				
2 mm								<u> </u>					
A-193	11/2	9/16	5%	111/16	.89	1.39	A-440	11/4	1/2	5%	31/2	1.369	1.57 1.593
A-328	1	9/16	7/8	113/16	.892	1.04	A-263	15%	1/2	3/4	25/16	1.41	1.34
₽ A -32	ı	3/4	5∕6	1 15/16	.908	1.453	A-1076	2	3/8	1 134	1% 3	1.419	.962
A-206	2	3/8	5/8	115/16	.908	1.22	A-61	1/2	11/16	13%s 5%s	21/4	1.429	1.99
A-654	11/8	3/4	5%	13/4	.924	1.55	A-320	15/8	5/8 1/8	11/16			2.26
A-342	11/2	7/16	11/16	21/16	.93	1.15	A-631 A-704	11/4	11/16	5/8	115/16	1	2.26
A-359	11/8	17/32		21/2	.933	1.21	A-104 A-322	11/8	34	3/4	25/16	1.463	1.83
A-770	11/2	1/2	1/2	21/2	.938	1.37	+A-138	11/4	1/2	15/16	21/2	1.465	1.35
A-126	11/4	5 ∕8	5/8	1 15/16	.945	1.43	A-769	2	3/4	5/6	19/16	1.465	1.57
A -59	11/8	1/2	3/4	21/4	.95	1.08	A-103	"	1		1		
A-64	11/4	1/2	3/4	25/16	.976		A -315	15/8	11/1	11/16	115/16	1.49 1.50	2.14
A-170	11/4	1/2	5/8	21/2	.978		A-191	1	1/2	11/2	25/16		1.72
+A-454	11/2	9/16	5%	115/16	1.021		A-336	13/4	1/2	3/4 5/8	31/2	1.537	1.80
A-703	15%	5/8	5√8	15%	1.032		A-277	11/4	9/16 9/16	78 5%	21/2	1.538	2.01
A-313	11/4	17/3:		21/2	1.038		A-644	13/4	3/4	13/16	13%	1.559	1.60
A-455	2	7/16	5 %	115/16			+A-17 A-180	2	3/8	13/16	13/4	1.559	1.36
A-493	11/4	5∕8	3/4	113/10			A-100 A-398	11/4	5%	1/2	4	1.564	2.19
A-194	11/4	9/16	5/8	27/16	1.07	1.41	A-352	3/4	11/8	11/2	11/4	1.583	2.85
A-310	1	5/8	3/4	25/16	1.084		+A-28	11/2	5%	3/4	25/16	1.628	1.94
A-701	11/4	1/2	3/4	25/16	1,084	1.23	T10 20	1 -/2	1			1	
A-112	11/4	1/2	1/2	31/2	1.09	1.55	A-125	11/4	3/4	3/4 5/8	25/16 25/8	1.628	
A-272	11/4	9/16		21/2	1.098		A-370	15/8	5% 1	1 78	11/2	1.688	
A-656	21/4	1/2	∫ 5/8	19/16			A-422 A-95	1 ½ 3/4	3/4	li	3	1.689	
A-379	1	17/3	2 13/16		1.10		A-886	13%	5%	5%	21/2	1.70	2.31
A-136	1/2	1/2	11/4	35/8	1.13	1	A-164	11/2	15/	ie 5%	115/	1.703	2.93
A-392	7/8	9/16	15/	6 21/2	1.15		A-291	11'2	123	Sol 2	1/2	1.719	4.63
A-42	11/4	25/	12 5/8	115/	1.18	_	A-716	13/4	54	13/	6 115/	16 1.72	2.09
A-90	13/8	17/	1 132 13/	15%	1.18		A-382	7/8	9/1	a 1	31/2	1.72	
A-121 A-286	1 1 1/2	9/16		16 4	1.19		A-278		9/1		6 3	1.74	1.97
75-200	1 -/2	1 "	' -/"		1			1,,,	1,,	15/	21/2	1.75	в 1.62
+A-257	2	1/2	5/8	115/			+A-12 A-174	11/2	1 ½ 548	3/4	3	1.75	
A-394			11/				A-728			16 1	29/1	1.76	3 1.60
A-175							A-483		أند ا	16 34	25/1		9 2.18
A-41	11/8		3/4	215/			W00 .				21/8	1.79	4 2.33
A-400	- / -				1.24		A-83	-/-	3/4		115		
A-715 A-727			5 3/4 7/8				A-176	11/4	1 1/2		3	1.87	
A-262		5/8 3/4	3/4	3	1.26		A-410	13/8	i 5∕6	3/4	215		
A-262	- /	1 1:	5%		1.28		A-29	13/4					· I
A-348			5%	, , -	1.28		A-30	1 13%	11	/16 7/8	25/1	6 1.91	4 2.0
		-		05/	1.30	02 1.63	A-35	1 13/2	ί 5 €	1	13/4	1.91	
+A-86	1	3/4	3/4	25/1			A-43			3/4	21/	1.93	
+A-11	11/		5/		1		A-42			16 3/4		1.94	1
A-80				16 21/2	-		88		5 3/4	1 3/4	25/	1.95	
A-12 A-14				16 2/2 16 2/2			A-36		á l	/16	/16 3	1.95	
A-14	- /		54	115			A-44	2 7	8 9	16 1	4	1.96	
+A-40		4 78	, "	/16 115			A-48	/-	6 9	16 15	/16 21/2		
+A-76		1 - 1 -	3/4	13/	1.3		A-63		8 1	5/16 3/4			
A-27		-	ie i	1/16 29/	~ 1	63 1.63	A-23	1 '	6 S	ś / 76			
A-43		4 7		2	1.3		■ A_11	24 13	6 3 _.	á 1 %	1 25/	16 2.0	5 I 2.3

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catalog	ı ldim	ension	s in inc	h			U						
numbe					relative	weight	catalog numb	dime	nsions	in inch	es	relative	weight:
	wid		dow	dow	handl'g capac'y		numb	strip width	build	dow	win- dow	power handl'g	pounds
	D	E	F	G		ı		D	E	width F	length	capac'y	1
12 mi	seri	es A					12 mi	serie		<u> </u>	G		
A-20	1,,,	1	, ,					T -	T			т	
+A-145	11/2	5/8	16 7/8 3/4	25/16	2.088	2.245	·	11/4	7/8	11/4	25%	3.591	2.92
A-94	11/4	78 7/8	7/8	25/16 25/16	2.169 2.213	2.58	+A-18	13/4	1/2	13%	3	3.609	2.322
+A-13	11/2	1/2	1	3	2.213	2.56	A-453	11/4	1	15/16	21/4	3.69	3.29
A-420	3/4	3/4	2	2	2.252	1.842 1.518	A-311	17/8	3/4	3/4	31/2	3.693	3.92
A-182	13%	3/4	15/	6 23/8	2.294	2.37	A-611 A-247	21/4	13/16	7/8	25/16	3.697	4.17
A-334	11/4	1	29/		2.301	2.88	A-247	13/8	29/32	2 1	3	3.738	3.46
A-318	15%	11/	11/	6 3	2.307	2.725	A-802	21/2	1/2	1	3	3.75	3.07
A-184	3/4	3/4	13%	3	2.322	1.61	A-854	2	25/32		3	3.81	3.99
A-640	1	3/4	11/4	21/2	2.345	1.90	A-369	15%	5% 34	13/16	23/4	3.85	3.15
A-317	17/	1 ~		1				1 - / 8	74	17/16	211/16	3.892	3.16
A-610	17/8	3/4	3/4	21/4	2,374	3.00	A-387 +A-185	11/8	11/16	15/16	31/2	3.92	3.76
A-292	134	11/1	6 3/4	25/16	2.386	2.91		13/8	5%	15/16	31/2	3.945	2.56
A-251	13%	3/4	3/4	215/16	2.411	2.61	A-718 A-139	21/4	3/4	15/16	21/2	3.955	4.00
A-495	2 28	3/4	15/1	6 21/2	2.415	2.435	A-139	15%	13/16	1	3 ~	3.96	3.58
A-281	11/2	5/8	3/4	15% 3½	2.438	2.95	A-706	21/4	7∕8	7/8	25/16	3.984	4.60
A-836	13/4	11/1		23/4	2.464 2.48	2.52	A-881	213/16	7∕8	5%	25%	4.04	5.83
A-661	11/2	3/4	15/1	23/8	2.503	2.82 2.584	A-269	11/8	13/8	3/4	31/2	4.06	1.045
A-127	2	3/4	3/4	21/4	2.531	3.20		13/8	29/32	15/16	31/2	4.088	3.75
A-4 75	3/4	3/4	11/2	31/16	2.587	1.66	A-300 A-592	2	7/8	15/16	21/2	4.10	4.31
		[.	1	"		1.00	A-332	2	5∕8	11/4	25%	4.103	3.111
A-705 A-329	2	13/10		21/8	2.588	3.44	A-391	1 1	1 [13%	3	4 100	2.000
A-329 A-729	2	3/4	3/4	25/16	2.601	3.25	+A-15	2	11/16	1 78	3	4.125 4.128	3.055
+A-49	11/8	3/4	11/8	23/4	2.613	2.185	A-258	21/4	5%	i	3	4.128	3.58 3.58
A-717	1½ 2	3/4	15/16	21/2	2.635	2.66	A-268	13/4	13/16	i l	3	4.263	3.86
A-751	11/2	11/16	7/8	21/4	2.709	2.96	A -181	21/2	3/4	15/16	21/2	4.393	4.44
A-443	11/2	23/32	34	31/2	2.709	2.70	A-439	11/2	25/32	11/4	3	4.395	3.60
+A-330	1	15/16	i	2 ⁹ / ₁₆	2.764	2.59	A-104	11/4	1/2	23/8	3	4.452	1.98
A-38	11/2	5%	Ιî	3	2.811	2.64	A-445	11/2	1	13/16	21/2	4.455	4.05
A-504	2	9/16	î	29/16	2.88	2.395	A-255	7/8	3/4	15%	43/16	4.464	2.37
		/.•		2716	2.00	2.56	+A-48	2	3/4	1	3	4.50	3.98
A-448 A-362	11/2	3/4	1	29/16	2.882	2.73	+A-111	11/2	1	1	3	4.50	4.30
A-362 A-14	1½ 2	3/4	3/4	31/2	2.954	3.14	A-212	13%		13%	31/2	4.554	2.89
A-117	21/2	1/2	1	3	3.00	2.48	A-419	21/2	23/32	15/16	23/4	4.634	4.44
A-270	11/4	13/ ₃₂	1 1	3	3.045	2.41	A-290	11/2	3/4	1%	3	4.641	3,205
A-384	11/2	11/16	15/16	21/4	3.045	2.75	A-347		1	15/16	21/2	4.685	5.14
A-773	213/16	5/8	3/4	25/16	3.047	2.48	A-171	21/2	, ,	1	3	4.689	3.99
-A-267	11/2	11/16	1 74	3	3.05	3.62	A-449	2	5/8	11/4	3	4.689	3.36
A-377	1	11/4	11/4	2	3.126	2.68 3.38	A-244 A-240	11/2		15/16	31/2	4.739	3.12
A-23	2	1/2	13/16	211/16	3.193	2.39	A-240 A-27	15/8 11/4		1	3	4.875	4.65
A-308	1			7.9		2.00		1/4	1/16	11/4	3	4.98	4.04
	11/2	%	1	31/2	3.283	2.64	A-58	13/4	9/16 1		E1/	5040	
	2	3/4	3/4	215/16	3.304	3.74		21/2			51/8 3	5.043	3.56
1	13/4	21/32	3/4	37/8	3.336	3.337		11/4 1		, -	3	5.157	3.31
1	11/2	1	15/16	23/8	3.339	3.75	A-130	2	% 1		3	5.157 5.25	3.79 4.84
'	2	3/4	1	3	3.375	2.99		13%			3		4.84 3.87
• • • · · ·	i l	2 1/32 15/16	11/16	33/4	3.386	3.69		13/4			3		3.74
	2	3/4	15/16	- 1	3.513	2.76		1/2	%s ∫ 1	3/8	3		3.87
• · · · · · ·		1 1	15/16	2½ 2½		3.55		21/2	15/16	15/16	21/2		5.88
	34	7/8	15/16			3.85 3.77		2/2	%	15/16	234		5,69
		, 0	/16	-/2	J.306 I	3.77	A-396	3/4	13/16 1	1 4	4		4.596

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	A:	nion- !-	inch		relative	weight.	catalog	dimen	ions in	inche	s I	relative	weight:
catalog number	strip	build	win-	win-	power	pounds	number	strip	build	win-	win-	power	pounds
	width	up	dow	dow	handl'g capac'y				up	dow width	dow length	handl'g capac'y	
	D	E	width F	length G				D	E	F	G		
12 mil :		<u> </u>	-	-	, ,		12 mil	series	A				
		, , l	15/	017	F 010	4.986	A-509	213/16	29/32	13/16	3	9,081	7.35
A-456 A-719	21/4	7/8 13/16	15/16 1	21/4 27/8	5.812 5.836	5.36	A-761	2 9 6	15/16	1	31/2	9.184	8,79
A-301	11/2	3/4	13%	37/8	5.995	3.74	A-622	33/8	11/2	3/4	27/16	9.253	14.42
+A-16	2	1 4	1	3	6.00	5.73	+A-54	21/2	1	13/16	31/8	9,281	7.56
A-429	1	7∕8	13/4	4	6.124	3.22	A-447	2	11/8	13/8	3	9.282	7.12
A-421	1	1	13/4	31/2	6,125	3,52	∔A -187	21/2	11/4	1	3	9.375	9,60
+A-19	2	3/4	13%	3	6.189	4.28	A-499	2	17/16	13/16	23/4	9.389	9.18
A-601	11/2	13/8	1	3	6.189	6.54	A-1103 A-63	2	1	13%	31/2	9.63 9.846	6.65 5.72
A-390	13/4	7/8	13/8	3	6.315	4.52 5,60	A-63 +A-393	13/4 21/2	3/4 7/8	1 1/4 15/16	31/2	10.049	6.96
A-508	213/16	3/4	1	3	6,327	3,60	₩ 7 -233			1716			
A-305 A-834	7/8	3/4	23/8	43/16	6,525 6,62	2.62 4.56	A-814 +A-119	213/16 21/2	7⁄8 1	7/8 13/8	411/16 3	10.08 10.314	8.79 7.64
A-834 A-1070	13/4 23/4	13/32	1 ½ 15%	41/2	7.54	4.10	A-981	2 / 2	11/4	13/8	3	10.314	8.16
A-309	21/2	1/2	15/16	41/16	6.662	3.96	+A-196	21/4	11/8	13%	3	10,44	8.00
A-437	2	15/16	13/16	3	6.678	5.45	A-586	21/2	11/8	13/16	31/8	10.444	8.804
A-83	11/4	9/16	15/16	73/8	6.80	3,48	A-655	21/4	11/4	13/16	31/8	10,444	9.09
A-253	11/4	11/4	11/4	31/2	6.839	5.41	A-284	21/2	11/16	1	4	10,62	9,15
A-414	21/4	1	15/16	31/4	6.851	6.66	A-51	2	1	13/8	37/8	10.656	7.04
A-441	1	1 7/	13/4	4	7,00	3.78	A-380 A-198	13/8	13/8	13/8	41/8	10.725	7.48 5.16
A-457	1	7/8	2	4	7.00	3.33	A-284 A-51 A-380 A-198 A-471	13/4	3/4	194	411/16	10,773	3.10
A-304	7/8	3/4	29/16	43/16	7.04	2.69	A-471	13%	1	13/4	41/2	10.827 10.953	5.56 8.27
+A-37 A-423	21/4	27/32	13/16 1	31/8	7.05 7.128	5.51 7.18	A-477 A-582	21/2	1 1/16	13/8	3	10.968	10.50
A-588	21/4	13/16	11/8	27/8	7.277	6.44	+A-355	21/4	11/8	11/4	31/2	11.074	8.50
A-82	11/4	9/16	111/16		7.419	3.21	A-709	3	1	13/16	31/8	11.138	9.07
A-40	2	1	13/16	31/8	7.425	6.05	A-216	21/4	7/8	15%	31/2	11.20	6.599
A-215	1	1	21/4	35/16	7.452	3.68	A-418	1 1/8	11/16	2	411/1		5.17
A-708	21/2	1	1	3	7,50	7.16	A-883	11/2	13/8	15/8	33/8	11.30	7.60 5.50
A-202 A-105	13/4	15/16		31/2	7.532	5.30	A-585 A-651	2 21/2	1 3/16	23/8 15/16	31/2	6 11.328 11.48	8.22
W-102	11/2	3/4	13%	47/8	7.542	4.32	A-031	4/2	-	19/16	372	11.40	0.22
A-407	21/4	29/32	13/16	31/8	7.569	6.025	A-733	13/4	11/8	13/4	33/8	11.63 11.738	4.34 9,40
A-413 A-428	11/2	29/32 3/4	13/16 15/4	31/8	7.569 7.656	6.02 4.06	A-754 A-608	33/8	17/16	6 13/16 13/8	31/8	11.756	
A-732	11/2	1	15%	33/16	7.772	4.92	+A-266	21/4	1	13%	37/8	11.989	
A-613	23/4	7/8	11/8	27/8	7.783	6,65	A-452	2	1	2	3	12,00	6.77
A-364	13%	13/8	13/8	3	7.80	6,36	A-614	3	1	11/4	31/4	12.188	
+A-102	11/2	15/16	13/8	3	8.118		A-188	21/2	15/8	1	3	12.189	
A-474	15%	1/2	2	5	8.13	3.27	A-98	2	1 1/16	17/16		12.208	7.80 9.52
A-461 +A-35	213/1		11/4	27/8 3	8.205		A-590 A-650	2 3	13%	17/16	31/8	12.35 12.375	
4V-32	2	1	13%	3	8.25	6.10		"	-	13/8			9.10
A-332	2	1	13/16	31/2	8.316		+A-254	21/4	13/1	6 15/8	43/16		
A-331 A-595	21/2	13/16		3 254	8,373 8,414		A-468 A-151	13/4	1114	13/4 15/8	41/16		
A-720	1 1/8 23/4	3/4 7/8	23/4 13/16	35%	8.414		A-151 A-462	213/1	11/8	11/2	3	12.443	
A-66	21/4	/8 7/8	11/4	31/2	8.614		+A-467	213/			3	12.69	9.64
A-476	13%	11/10		55%	8,646		A-865	21/2	11/8	11/4	35/8	12.70	9.50
A-134	1	1 "	113/1		8.84	4.27	A-600	23/4	15/1		31/2	12.961	
A-372	21/2	1	13/16	3	8.91	7.40	A-367 A-491 A-510	2	11/4	13/8	37/8	13.322	
A-132	2	11/2	1	3	9.00	9.80	A-491	21/4	7∕8	15%	43/16	13,402	
+A-53	21/4	1 1/8	15/16	31/2	9.041	6.26	A-510	1 213/	6 13/16	11/4	31/4	13.572	l 10.95

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:atalog :umber			n inche		relative		catalog	dimen	sions i	n inche		relative	weigh
	etrip width D	build up E	win- dow width F	win- dow length G	handl'g capac'y	pounds		strip width D	build up E	win- dow width F	win- dow length G	power handl'g capac'y	pound
2 mil	series	A					12 mil						<u> </u>
A-338	13/4	11/8	15%	41/4	13.60	7.78	A-283	21/	15/	17/		10.000	
A-189	2	l l	156	41/4	13.80	7.45	A-283 A-237	2½ 2½	15/16	17/16	4	18.852	12.70
A-1127	23/4	i	17/18	31/2	13.80	0.10		21/4	11/8	13%	47/8	18.857	11.65
A-378	11/4	15%	15%	43/18	13.82	8.79	A-771 A-435 A-1144 A-620 A-350		11/2	15%	35%	19.88	13.10
A-417	11/2	11/8	13/4	411/16		7.16	A-1144	21/4	13/16	11/4	6	20.046	12.6
A-84	15%	13/16	2	51/4	13.86	5.83	A-620		13/32	1%	43/16	20.40	11.60
A-203	21/4	11/8	15%	33%	13.881	8.85	A-350	31/8	11/4	11/2	31/2	20.507	14.0
A-29	21/2	1 /8	19/16	39/16	13.91	8.63	A-324	21/2	11/2	15%	3%	20.567	14.25
A-466	213/16	15/16	13/6	37/ ₈	14.00	9.14	A-606	11/2	17/16	23/16	43%	20.637	9.80
A-426	13%		, .	3 /B			624	31/8	3/4	113/16		20.704	9.5
75-120	1 778	13%	13/4	41/4	14.063	7.98	+A-459	213/16	13/32	15%	43/16	20.90	11.90
A-107	11/4	11/4	3	3	14.067	6.44	A-248	1%	15%	15%	4 1/8	20.924	12.3
A-323	21/4	111/16	13/16	31/8	14,10	13.65	A-750	21/4	13%	15%	43/16	21.057	12.6
A-623	33/6	11/2	1	213/16	14.237	16.08	A-750 A-624	33/6	11/2	15/16	33/16	21.178	17.9
A-505	13/4	11/8	1%	41/2	14.40	8.04	A-762 A-735	31/2	29/32		43/16	21.581	11.8
A-591	21/2	15/16	17/16	31/8	14.728			2	13/8	113/16	43%	21.801	11.7
A-306	2	1	13/4	41/4	14.875	7.82	A-749	213/16	15/32	15%	43/16	22.125	12.6
A-634	21/4	1	13%	47⁄8	15.083	9.08	A-658	31/4	11/8	13%	41/2	22.622	28.5
A-465	11/4	11/4	15/16	73%	15.126			21/2	15/16	15%	41/4	22.653	13.4
A-249	11/2	11/2	11/2	41/2	15.188	9.71	A-356	2	2	17/16	41/8	23.711	18.0
A-386	2	1 1/8	15%	43/18	15.311	8.80	A-446 A-356 A-427	21/2	11/4	13/4	41/2	24.611	13.2
L-1076	21/2	7∕8	11/2	4!1/16	15.40	8.50	A-598	11/2	3⁄4	21/8	75%	24.659	6.8
A-473	21/2	11/2	13%	3	15.468	13.01	A-507	2	2	13%	41/2	24.75	18.70
A-801	11/4	11/4	23/8	43/16	15.50	6.88	+A-480	213/16	13/32	13/4	411/16	25.20	12.90
A-511	213/16	13/16	15%	43/16	15,537	8.36	A-502	21/2	19/16	17/16	41/2	25.25	16.9
A-469	13/4	11/8	15%	47/8	15.60	8.42	A-192	17/8	11/4	2	57/16	25.489	11.40
L-514	33/8	11/6	13/6	3	15.663	12.10	A-982	21/2	11/2	15%	43/16	25.50	15.80
A-810	33%	11/8	13%	3	15.70		A-893	21/2	1	21/8		25.90	11.10
A-287	21/4	1	13/4	4	15.752	8.50	A-711	31/2	13%	13/8	47/6	25.645	18.2
A-777	11/2	11/2	13/4	4	15.752	9.43	A-488	21/2	11/2	15/8	37/8	25.90	16.0
1 -625	33%	11/8	13%	31/16	15.987	12.13	A-1134	21/2	1 1	21/4	41/4 45/6	26.00	10.9
L-388	2	13/16	15%	43/18	16.17	9.42	A-743	31/2	13/32	15%	43/16	26.058	14.8
L-734	1 1/6	11/4	13/4	4	16.408	9.32	A-460	213/16	13/8	15%		26.317	15.9
L-433	21/4	13%	13%	37/8	16.484	11.84	A-478	213/16	113/32	15%	43/16		
-710	31/4	11/4	11/4	31/4	16.507	13.51	A-722	31/2	13/16	15%	43/16	26.908 27.028	16.40 15.80
L-630	2	11/2	19/16	39/16	16.692	11.60	A-1167	21/6	15/16	13/4		28.00	15.60
L-500	213/16	7/8	15%	43/16	16.748	9.13	A-635	3	13/6	15%	41/4	28.00	17.00
1-122	21/2	1	13%	47/8	16.76	10.10	A-778	213/16	17/8	13/8	43/16		22.30
-615	31/4	11/8	15/16	31/2	16.79	12.42	A-411	13/4	13/4		31/6	28.094	
L-113	134	13/16	13/4	411/16	17.055	8.94	A-580	213/16	15/16	13/4	51/4	28.14 28.245	15.47 15.60
-593	21/4	11/6	15%	43/16	17.225	9.44	A-503	213/16	13/8	13/4	4%	28.76	16,3
L-721	31/4	11/16	17/16	31/2	17.364	11.65	A-621	3¾	13/6	11/2	33⁄4	29.003	19.73
L-759	213/16	2	11/16	3	17.919	20.46	A-748	13/4	21/4	13/4			
-389	15%	15%	15%	43/16	17.975	11.43	+A-431	2			41/4	29.291	19.46
-337	21/4	11/8	13/4	41/16	17.925		+A-519	213/16	71/2	2 ⁷ /8	25/16	30.345	3.35
484	21/4	13/4	15/16	31/2	18.085	9.91	A-1074	2 9/16	13/32	13/4	5	30.76	13.90
-218	15%	15%				15.40	A-775		17/8		43/4	31.20	18.40
-512	21/4		15/8	41/4	18.241	11.50	A-775 A-997	15%	19/16	23/16	5% 9	31.236	13.40
-274		11/2	15/8	33/8	18.509	12.80	A-997 A-907	13/4	11/2	11/2	8	31.60	16.10
-430	2½ 2	13/32	15%	43/16	18.611	9.68	32	33/8	1 13/32	15%	43/16	32.30	19.50
1-513		1	2	411/16	18.752	8.54	A-1069 A-616	33/8	3/4	21/8	61/16	32.60	12.30
	33/6	11/2	13/16	31∕8 I	18.797	17.41	A-616	31/2	11/4	13/4	41/4	32.538	18,00

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catalog	dimen		inche	•	relative	weight:	zatalog	dimen	sions in	inche	-	relative	
number	strip width D	build up E	win- dow width F	win- dow length G	power handl'g capac'y	pounds	number	strip width D	build up E	win- dow width F	win- dow length G	power handl'g capac'y	pound
12 mil	series	A					12 mil						
A-648	31/2	13%	15%	43/16	32.754	19.85	A-1151	AI/	11/	21/	E7/	78.00	35.80
A-481	213/16		21/4	39/16	33.807	17.82	A-1151 A-618	41/2	11/2	21/8 21/8	57/16	78.914	26.00
A-636	33/8	15/16		57/16	34.384	14.59	+A-757	4	21/4	17/8	5½ 4¾	80.156	46.47
A-296	21/2	13/4	13/4	41/2	34.452	20.38	A-652	33/4	121/32		61/8	80.826	34.96
+A-516	31/8	11/4	113/16		34.505	17.48	+A-526	4	19/16	21/8	61/8	81.322	34.80
A-515	33%	15/16	113/16		35.105	19.00	A-857	33/4	13/4	21/8	57/8	81.90	36.20
A-736	21/4	11/2	21/4	43/4	36.072	16.20	+A-537	33/4	115/32	21/4	63/4	83.666	32.70
A-517	31/8	13%	113/16		37.957	19.70	+A-555	21/2	125/32	23/4	73/16	88.024	29.50
+A-627	31/8	11/8	17/8	513/16		17.22	A-871	3	213/16	17/B	55%	89.00	52,30
A-599	31/8	11/2	11/2	51/2	38.676	22,70	A-602	4	113/16		57g	90.487	40.80
A-742	31/2	15⁄8	15%	43/16	38.71	24.30	A-821	3¾	1 1/B	21/4	53/4	91.00	39.40
A-723	4	15/16	13/4	41/4	39.032	21.87	+A-530	4	19/16	21/8	73/16	95.435	38.60
A-657	31/2	1/4	13/4	51/4	40,194	20.30	A-545	21/4	21/4	23∕8	8	96.20	36.20
+A-518	31/8	17/32	1 1/B	513/16		18.90	A-752	4	19/16	21/8	79/16	100.401	39.40
A-629	213/16		15/8	43/16	41.876	29.40	A-739	3	2	213/16		105.45	37.55
A-780	21/2	21/4	13/4	41/4	41.90	27.20	+A-558	21/2	125/32	23/4	85%	105.622	34.00
A-649	31/B	15/32	2	57/16	42.43	18.69	A-547	31/2	11/2	21/2	81/16	105.814	35,30
A-522	21/2	123/32	2	5	42.98	21.60	+A-559	21/2	113/16		85%	107.45	33.20
A-535	3	11/8	21/4	53/4	43.666	17.10	A-1140	21/2	35%	2	6	108.00	62.80
►A-533	31/8	15/32	23/16	55%	44.466	18.00	+A-833	4	121/32	21/4	71/4	108.054	41.74
A-604 A-527	213/16 21/8	2 5/16 13/4	11/4	45%	47.749	45.00 24.90	A-556	33/8	11/2	23/4	77/8	109.644	34.40
A-908	213/16		21/8	6½ 8	48.406 48.50		+A-543 +A-539	4	121/32	23/ ₈	75/16	115.032	42.70
A-632	31/8	11/16	1½ 2½	5	48.825	24.30 19.14	A-667	4	113/16	21/4	71/4	118.233	46.50
A-921	3	13/4	11/4	71/2	49.20	32.60	A-531	4	19/16 2	25/16	81/4	119.171	42.40 50.70
A-949	33%	17/4 17/8	13/4	41/2	49.90	29.60	A-538	4	21/32	21/8	73/16	122.196	51.50
A-520	4	11/4	2	5	50.00	23.20	A-741	213/16	13/4	21/4 31/16	63/4	123.383 124.311	35.90
A-856	31/2	13/6	11/8	55%	50.70	24.00	A-951	21/2	21/2	211/16	81/4	126.00	46.00
+A-523	33%	13/6	2	57/15	50.466	23.08	A-1071	4	2	21/2	63/6	127.50	50.00
+A-745	13/4	3	2	5	52.50	31.20	A-1133	4	21/2	23/8	53/g	127.70	62.10
A-737	21/2	111/16	21/2	5	52.75	21.87	+A-540	4	1 13/16	21/4	81/8	132.503	50.30
A-603	31/8	215/16	11/4	45%	53.063	50.00	A-1177	41/2	21/4	21/8	61/4	134.60	61.60
A-617	4	11/2	11/8	43/4	53.438	27.90	+A-564	213/16	129/32	31/16	81/4	135.399	40.30
A-724	41/4	17/16	113/16	4 1/B	53.947	27.88	A-1147	4	21/4	21/4	63/4	136.70	57.50
A-524	33/8	11/4	21/8	61/15	54.346	22.20	A-1073	4	11/2	23/4	81/2	140.30	42.00
A-753	33/4	1 15/32	2	5	55.09	27.00	A-977	33/4	21/2	21/4	63/4	142.40	62.90
+A- 521	4	17/16	2	5	57.48	27.60	A-967	51/2	21/2	15%	67/16	144.20	84.10
+A-763	4	15/8	17⁄B	43/4	57.893	30.53	A-532	4	19/16	21/8	11	146.00	50.60
A-664	31/2	13/8	17⁄8	67/16	58.00	24.00	A-549	4	113/16	21/2	81/16	146.083	51.00
+A-525	3%	111/32	21/B	61/16	58.432	24.20	A-830	4	27/16	2	75%	148.70	67.10
A-638 •A-529	31/2	21/4	13/4	41/4	58.569	39.00	A-544	4	23/16	23/B	75/16	151.987	59.80
A-969	33/8	113/32		65/16	63.644	26.20	+A-548	4	129/32	21/2	81/16	153.662	53.70
-505 -A-534		2	15/8	51/8	66.60	40.30	A-914	31/8	21/2	23/4	71/4	155.70	59.70
A-872	33/4	113/32		61/16	69.90	29.00	A-1135 A-740	4	27/16	2	81/8	158.40	70.60
A-960	23/4	23/4	13/4	51/4	69.50	44.00		31/4	23/16	31/4	67⁄8	158.888	49.45
A-738	33/4	13/4	21/4	43/4	70.10	32.60	+A-566	213/16		31/16	93/8	159.00	45.10
A-725	23/4	113/16		51/4	71.941	27.62	A-541	31/2	25/8	21/4	81/8	167.968	69.20
A-1009	41/2	15%	2	5	73.13	35.36	A-968	51/2	25/8	17/16	81/8	168.20	101.00
-1005 -A-536	23/4	23/4	11/8	51/4	74.50	44.90	A-546	41/4	23/16	21/2	75/16	170.00	64.20
A-1-034	334	113/32	2/4	69/16	77.852	30.60	A-890	31/4	31/4	21/2	61/2	171,60	77.40

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pg /2

catalog	dimen	sions is	ı inche	4	relative	weight:	catalog	dimen	sions is	n inche	4	relative	
number	strip width D	build up E	win- dow width F	win- dow length G	power handl'g capac'y	pounds	number	strip width D	build up E	win- dow width F	win- dow length G	power handl'g capac'y	pound
12 mil		'	ı r	G	!	<u> </u>	12 mil :			į F	<u> </u>		l
	<u> </u>									l	l I	l	·
A-1148	41/2	31/8	21/8	57/8	176.00	90.50	A-1179	5	3	3	103%	466.90	140.00
∔A -571	213/16		31/8	95%	176.00	49.10	A-1149	6	31/4	31/16	81/4	492.50	164.00
A-867	31/4	3%	21/2	61/2	178.10	79.50	A-1198	5	31/4	3	103/6	506.00	152.00
A-569	31/8	2	31/8	95%	187.00	51.60	A-966	71/2	3	19/16	141/2	510.40	241.00
₽A-570 A-557	31/8 5	2 1/16 12 1/32	31/8 23/4	95%	193.00 196.00	54.00 60.20	A-961 A-925	31/4 6	4 3½	31/2	115%	528.90 530.60	143.00 181.00
A-572	31/8	21/16	35/16	85% 95%	205.00	54.30	A-1138	6	31/8	31/16	81/4 93/6	538.00	163.00
A-870	33/4	33/6	21/2	61/2	205.60	91.60	A-965	71/2	31/4	19/16	141/2	552.50	265.00
∔A -561	31/8	27/32	3	10	208.00	58.90	A-928	6	33/4	31/16	81/4	568.50	201.00
A-551	4	129/32	21/2	111/4	214.00	66.60	A-1240	71/2	23/16	35/16	101/2	570.00	147.00
A-550	4	211/16	21/2	81/16	216.707	80.90	A-1200	5%	35%	3%	91/16	596.00	179.00
A-1100	45%	33/4	21/4	63/4	217.80	131.50	A-1099	71/2	43%	21/4	81/2	627.30	301.00
A-562	33/8	27/32	3	10	224.00	64.00	A-970	71/2	4%	21/4	81/2	627.30	293.00
A-1188 A-957	4 5½	31/4	23/6	75/16	226.00	96.00	A-1104 A-936	71/2	33/4	19/16	141/2	636.60	316.00
A-542	4	23/4 31/8	17/16 21/4	10 ⁷ / ₁₆	226.50 228.516	125.60 99.40	A-929	7½ 6¼	31/2 211/16	35/8 31/8	63/4 127/8	642.30 675.90	212.30 175.00
A-573	31/8	25/16	35/16	95%	230.00	62.20	A-1197	53%	41/4	33/6	91/16	698.00	222.00
A-1263	6	2	25%	75/16	230.00	83.00	A-1228	5	43/4	3	103%	739.00	252.40
A-1160	41/2	4	21/8	61/16	232.20	132.00	A-1199	5%	45%	3%	91/16	761.00	247.00
A-575	21/2	21/2	31/2	103/4	233.00	59.20	A-1037	6	51/4	31/16	81/4	795.90	320.00
A-552	41/2	129/32	21/2	111/4	242.00	75.00	A-937	5%	31/8	33⁄4	115%	799.80	191.50
A-987	4	3	21/2	81/8	243.80	94.20	A-1056	71/2	33/4	2	141/2	814.90	335.00
A-553	4	23/16	21/2	111/4	246.00	81.10	A-942 A-958	6	31/8	33/4	115%	817.40	196.00
A-1249 A-1259	71/2	13/4	21/4 25/8	8½ 75/16	251.00 259.00	94.50 94.50	A-946	6	43/4	31/16 6	93% 123%	818.40 918.00	297.80 145.00
A-565	55%s	129/32	31/16	81/4	270.00	79.50	A-1245	61/2	213/16	41/8	121/2	944.00	198.00
A-577	31/4	21/8	4	10	276.00	62.40	A-1105	71/2	5	37/8		1008.00	354.00
A-1002	31/2	41/4	23/4	63/4	276.80	125.30	A-927	61/2	3	4	131/8	1024.00	219.00
A-554	4	211/16	21/2	111/4	277.00	98.50	A-1229	5	4	4	135/16	1065.00	242.00
A-1248	71/2	2	21/4	81/2	287.00	112.00	A-959	71/8	37/8	41/2	11	1190.00	304.00
A-563	31/8	31/8	3	10	292,00	91.50	A-953	57⁄8	43/4	43/4	83/4	1195.00	299.00
A-567	5%	129/32		9%	307.00	86.00	A-1084	71/2	51/2	2	141/2	1196.00	543.00
A-574 A-578	5	21/ ₃₂	33% 4	91/16	312.00 312.00	82.50 68.00	A-954 A-1154	57/8 67/8	5 4½	43/4	83⁄4 10	1221,00 1236.00	320.00 333.00
A-956	71/2	23%	19/16	111/4	312.80	151.00	A-1090	71/2	61/4	37/ ₈	t I	1260.00	484.30
A-1162	5	33%	23/4	634	313.20	130.00	A-935	61/2	37/8	4	131/8	1323.00	300.00
A-568	55%	131/32		95%	332.00	92.00	A-1024	51/2	49/16	43/4	121/4	1455.00	310.00
A-1243	5	33/4	23/4	634	348.00	150.00	A-989	67/8	6	4	10	1650.00	504.00
A-950	4 1/8	33/4	23/6	8%	363.50	155.50	A-1196	61/2	51/4	4	131/8	1790.00	438.00
A-955	71/2	27/8	19/16	111/4	379.70	192.00	A-1224	6	4	5	18	2160,00	360.00
A-938	6	31/4	37/8	51/8	387.50	140.00							
A-994	47/8	4	23/8	8%	387.80	173.00							
A-930 A-964	61/2	3	31/4	63/18	392.20	139.50							
A-579	5 33⁄4	31/2	19/16	141/2	395.90 418.00	194.00 83.60							
A-1255	61/2	25/32	3	10	420.00	119.00							
A-576	41/2	21/4	33/4	115%	440.00	97.20							
A-1146	47/8	31/2	25%	97/8	443.40	160.00							
A-1239	51/4	35%	23/4	85%	451.00	170.00							
A-988	71/2	25/16	37/8		464.80	130.00							

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catalog number	dimen		n inche	5	relative	weight:	catalog number	dimen	sions in	inche	S	relative	
aumber	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pounds	, number	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pound
	D	E	F	G				D	E	F	G		
mil s	eries	H		'	-		4 mil s	eries	H				
H-459	14	14	1/4	14	.004	.013	H-504	34	34	14	7/-	.061	.23
H-568	½ ½	1/8 1/8	1/4	1/2 5/8	.005	.013	-304 ♣H -39	3/4 3/8	3/8 1/4	1/4 1/2	⁷ ⁄8 15∕₁6	.062	.10
H-121	3/4	/8 //8	1/4	78 1/2	.006	.02	→H-114	78 1/2	1/4	1/2	1 1	.063	.12
H-447	1/4	3/16	1/4	5/8	.008	.026	∔H -139	3/8	3/8	3/8	13/16	.063	.14
H-669	3%	7/64	1/4	3/4	.008	.133	+H-456	1/2	3/8	5/16	11/16	.063	.1
H-231	3%	3/16	1/4	5%	.011	.039	H-513	3 ₄	17/64	1/2	11/4	.063	.10
H-283	1/4	1/4	1/4	7/8	.014	.046	∔H -363	5%	9/32	3/8	1	.066	.15
H-172	3/8	1/4	1/4	5%	.015	.056	+H-552	3/4	9/32	5/16	1	.066	.13
H-549	1/2	3/16	1/4	5%	.015	.053	H-619	3/4	5/16	5/16	15/16	.068	.19
H-671	11/2	3/16	1/2	11/8	.016	.26	∔H -137	5%	1/4	3√8	13/16	.07	.14
H-530	1/2	7/32	1/4	5∕8	.018	.063	∔H-1	1/2	1/4	1/2	11/8	.071	.13
H-629	1/4	1/8	1/2	11/8	.018	.025	H-607	5%	3%	5/16	1	.073	.2
H-676	1	3/6	1/2	11/8	.021	.402	H-307	3/8	3/8	3∕8	17/16	.076	.10
H-525	3/8	1/4	1/4	7 ∕8	.021	.068	H-98	5/8	1/4	7/16	11/8	.077	.1.
-H-550 -H-569	5/6	7/32	1/4	5/8	.021	.081	H-679	1/2	5/16	7/16	11/8	.077	.1:
-H-99	3 / 8	1/4	5/16	, 7∕8	.025	.071	H-342	1/2	1/2	5/16	1	.078	.2
H-215	3 / 8	7/32	5/16	1 7/	.026	.065 .091	+H-2	3/4	3/16	1/2	1 1/8	.08	.1
H-430	1/2 3/8	1/4 3/16	1/4 3/8	1 7/8 1	.027	.056	H-677 H-197	3/8	3/8 3/8	1/2	11/8	.08 80.	.1 .1
H-246	78 3/8	916 1/4	5/16	i	.029	.077	+H-407	1/2 3/4	78 1/4	3/8 3/8	1 1/8 1 1/8	.08	.1
H-606	3%	3/16	3/8	11/8	.03	.06	∔H -251	1/2	5/16	7/16	13/16	.081	.1
H-531	1/2	1/4	5/16	√ ₈	.034	.095	H-446	1/2	3/8	7/16	1	.082	.1
H-615	1/2	3/16	3/8	1	.035	.075	∔H-4 0	1/2	1/4	1/2	15/16	.083	.13
H-115	3/8	1/4	3/8	1	.035	.08	∔H -217	1/2	3/8	3/8	13/16	.084	.1
H-425	3/4	7/32	1/4	₹/B	.036	.112	∔H -553	7/8	5/16	5/16	1	.085	.2
H-116	3/8	1/4	3/8	11/8	.039	.085	HL-356	5∕8	9/32	7/16	11/8	.087	.1
H-402	1/2	3/16	3/8	11/8	.039	.081	H-140	5%	1/4	1/2	11/8	.088	.1
H-125	5%	1/4	5/16	13/16	.04	.113	H-364	1/2	5/16	1/2	11/8	.088	.1
H-588	1/2	3/8	1/4	7/8	.041	.153	H-567	1/2	1 1/32	7/16	13/16	.089	.1
-H-38	1/4	1/4	1/2	15/16	.042	.067	+H-380	7∕8	1/4	3/8	11/8	.092	.2
H-235	3/8	1/4	3/8	13/16	.042	.088	H-622	3/4	5/16	7/16	15/16	.096	.2
H -156 H -551	1/2	1/4	1/2	11/16		.094	+H-201	1/2	3/8	3/8	13/8	.098	.2
-H-210	5/8	1/4	5/16	7/8	.043	.12	H-678	1/2	5/16	9/16	11/8	.099	.1
H-532	3/8	3/8	5/16	1	.044	.129	H-111	1/2	1/2	3/8	11/16	.10	.2
H-250	1/2	7/32	5/16	1	.044	.118	+H-252	5/8	5/16	7/16	13/16	.101	.2
H-636	1/2	1/4 1/4	3/8 1/4	19/16	.047	.107	+H-41 +H-108	5% 5%	1/4	1/2	15/16	.102	.1 .2
H-276	1/2	3/16	3/8	13/6	.048	.093	+H-3	78 34	3/8	348 1/4	13/16	.105	.1
H-110	1/4	1/4	978 578	15/16	.051	.071	H-174	3/4 3/8	1/4 1/2	1/2	11/8	.106	.1
H-367	3/8	5/16	3/8	13/16	.051	.116	∔H -187	1/2	3/8	1/2 1/2	1½ 1½	.106	.2
H-672	3/8	1/4	1/2	11/8	.053	.092	H -621	11/8	5/16	11/32	7 ⁄8	.106	.2
H-233	1/4	1/8	3/4	25/16	.053	.049	H-180	56	5/16	1/2 32	11/8	.11	.2
H-620	1/2	3/16	5/16	13/16		.064	+H-4 3	3 [∞] 8	5/16	54	19/16	.114	.1
H-398	1/2	7/32	1/2	1 1	.055	.098	H-404	56	346	1/2	ı i	117	.2
H-684	1/2	1/4	7/16	11/16	.058	.114	H-385	3/4	1/4	1/2	11/4	,118	.1
H-365	1/2	7/32	1/2	11/16	.058	.101	H-261	5%	3%	3/8	13%	.121	.2
H-199	1/2	7/32	3/8	1	.059	.141	∔H-328	3/4	11/32	3/8	11/4	.121	.2
H-203	1/2	1/4	3/8	11/4	.059	.122	+H-554	7/8	5/16	346	13/16	.121	.2
H-382	5%	1/4	3/8	1	.059	.133	+H-42	34	1/4	1/2	15/16	.123	.2
-H-360	5%	5/16	5/16	1	.061		+H-269	1 1/2	3/8	1/2	15/16	.123	ı

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19 14

catalog			n inche		relative power	weight:	catalog number			n inche		relative	weigh pound
number	strip width	build up	win- dow width	win- dow	handl'g capac'y	pounds	number	strip width	build up	win- dow	dow	handl'g capac'y	pound
	D	E	F	length G				D	E	width F	length G		
4 mil s	eries	Н					4 mil s	eries	Н				
H-270	1/2	7/16	1/2	11/8	.124	.245	H -101	1	1/4	1/2	111/16	.211	31
H-327	7⁄8	3/16	1/2	11/2	.125	.183	H-216	3/4	3%	1/2	11/2	.212	.35
+ H -361	3/4	3/8	3/8	13/16	.125	.293	H-351	3/4	1/2	1/2	11/8	.212	.43
H-519	5∕8	3/8	3/8	17/16	.126	.273	H-189	11/8	1/4	1/2	19/16	.22	.33
H-637	1	3/4	3/4	25/16	.13	1.60	∔H-24 5	3/4	3%	1/2	19/16	.22	.36
H-160	5∕8	3∕8	1/2	11/8	.132	.252	H-428	3/4	3%	5/8	11/4	.22	.33
∔H -391	3∕8	3/8	%	11/2	.132	.186	H-243	5∕8	5∕8	1/2	11/8	.221	.49
H-674	1	3/16	5∕8	11/8	.132	.185	+H-46	3/4	5/16	5/8	19/16	.228	.30
H-173	1/2	1/2	1/2	11/16	.133	.284	H-214	1	9/32	1/2	1%	.229	.3
H-316	3∕8	3∕8	%	19/16	.137	.19	H-424	3/4	1/4	5/8	115/16	.229	.27
H-484	11/4	1/4	3/8	13/16	.139	.297	H-230	1	1/4	1/2	17/8	.234	.33
+H -138 H -169	1/2 1/2	1/2 3/8	1/2	11/8	.141	.293 .237	H-345 H-103	1 5%	5/16 5/	½ %	1½ 115/16	.234	.37
H-4	7/2 7/8	78 7/32	1/2	11/2	.144	.237	H-277	1 78	5/16 5/16	78 1/2	19/16	.236	.31
H-157	11/4	3/8	5/16	1	.146	.431	H-338	î	1/4	5/8	19/16	.244	.3
H-405	5/8	78 3⁄8	1/2	11/4	.146	.266	H-177	5%	1/2	1/2	19/16	.245	.43
H-176	3 _{/8}	1/2	1/2	19/16	.147	.26	H-186	11/4	1/4	1/2	19/16	.245	.3
₽H-304	5%	5/16	1/2	11/2	.147	.237	∔H -105	3/4	3%	34	13/16	.251	.34
H-124	7%	1/4	7/16	19/16	.15	.254	+H-129	7/8	7/16	1/2	15/16	.251	.40
₽ H -9	5/8	1/4	5/8	19/16	.153	.196	H-282	5%	1/2	5%	15/16	.257	.43
H-44	1/2	5/16	5%	1%6	.153	.204	H -631	5%	7/16	1/2	17/8	.257	.40
∔H-2 53	5∕8	3∕8	1/2	15/16	.154	.273	H -158	1	3/8	5/16	21/4	.263	.50
H-127	1/2	3/8	5/8	15/16	.155	.23	H-348	1	3%	9/16	11/4	.264	.4
∔H -310	3/4	3/8	1/2	11/8	.159	.303	+H-47	₹ 8	5/16	5/8	19/16	.267	.3
H-318 H-109	1	1/4	1/2	15/16	.164	.268	H-314	11/8	1/4	9/16	111/16		.2
H-149	3/4 5/8	1/2 9/32	1/2	7/8 19/16	.165 .172	.392 .225	H-190 +H-50	1/2 1/2	3/8 3/8	7/8 3/4	15/8 115/16	.268	.30
H-584			5/8	19/16	.172	.225	+H-11	1 2	9/32	5% 5%	19/16	.275	.3
H-202	7∕8 5∕8	1/4 3/8	1/2 1/2	11/2	.176	.201	+H-556	11/8	3/32 3/8	78 1/2	15/16	.277	.4
H-290	1/2	9/16	1/2	11/4	.176	.361	+H-408	7/8 7/8	7/16	7/16	111/16		.5
-H -175	5%	1/2	1/2	11/8	.177	.366	H -663	7/8	7/16	1/2	11/2	.288	.5
H-457	7/8	5/16	1/2	15/16	.18	.305	+H -6	3/4	1/2	1/2	19/16	.294	.5
H-434	1/2	1/4	3/4	115/16	.182	.188	+H -7	1	3/8	1/2	19/16	.294	.4
H-383	3/4	5/16	1/2	19/16	.183	.29	+H-4 09	7∕8	13/32	7/16	115/16		.5
H-374	3/4	1/4	5∕8	19/16	.184	.257	H -179	13%	9/32	1/2	19/16	.301	.4
-H-254	3/4	3∕8	1/2	15/16	.185	.328	+H-4 8	1	5/16	5%	1%16	.305	.4
-H -5	1	1/4	1/2	11/2	.188	.291	H-219	5/8	5/8	5/8	11/4	.305	.5
H-279	1/2	1/2	1/2	11/2	.188	.34	H-668	11/16		5/8	13/4	.305	.4
+H-464 +H- 555	1 1½	1/2 3/8	3/8 3/8	13/16	.188 .188	.523 .441	H-171 H-585	5/8 3/4	1/2	5% 5%	19/16 15/16	.306	.4
H-45				1	10:	054	** 150		7,	12/	100	010	
H-308	5⁄8	5/16 3/	5⁄8	19/16	.191	.254	H-152	,1/2	7/16	13/16	13/4	.312	.3
H-308	5% 14	3/8 1/-	5⁄8	15/16	.192	.287	H-349	1	13/32		11/4	.318	.49
H-104	1/2 3/4	1/2 3/	1/2 5/	19/16	.195	.346	H-371 +H-376	7∕8 1	3/8	%	19/16	.32	.4
H-326	3/4 3/4	3/8 11/32	5/8 1/2	1½ 1½	.198	.319 .326	+H-376 H-675	_	7/16 3/	7/16	111/16		.60 .50
H-377	5/4 5/8	3/8	½ %	13%	.201	.326	H-075	11/4	3/8 3/4	1/2	13/8	.323	.5
H-335	78 1/2	78 1/2	78 1/2	15%	.201	.355	H-200 H-51	1 5%	3% 3%	1/2 3/4	13/4	.329 .341	.5
H-683	1	1/4	9/16	17/16	.203	.303	H-117	78 5%	9/16	%4 5%	19/16	.341	.5
H-49	3/8	74 3%	3/4	115/16		.225	+H-403	78 7/8	1/2	1/2	19/16	.342	.5,
-H-381	78 78	7/16	3/ ₈	17/16	.205	.465	+H-379	1 78	13/32	7/16	115/16		.59

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atalog	dimen	sions in	inche	8	relative		catalog	dimen	sions i	inche	5	relative	weigl
umber	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pounds	number	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	poun
	D	E	F	G			1	D	E	F	G		
mil s	eries	H					4 mil s	eries	H				
H-632	3/4	3%	5/8	115/16	.343	.428	H-58	5%	7/16	7/8	21/4	.538	.5
H-557	11/4	7/16	1/2	15/16	.358	.664	+H-54	l 1 ′°	3/8	3/4	115/16		.5
H-100	1	3/8	5%	19/16	.366	.506	H-458	11/2	3/8	5%	19/16	.55	.7
H-255	3/4	1/2	5%	19/16	.366	.543	H-350	1	1/2	11/16		.559	.7
H -510	1	15/32	1/2	19/16	.367	.637	H-237	11/8	9/16	3/4	13/16	.563	3.
H-14	11/8	5/16	5/8	111/16	.37	.479	+H -558	11/2	1/2	1/2	11/2	.563	1.0
H-372	7∕8	7/16	5/8	19/16	.373	.536	H-6 18	1	1/2	1/2	21/4	.563	3.
H-223	1	1/2	1/2	11/2	.375	.679	∔H -17	11/4	3/8	5∕8	1 1 5/16		.7
H-161	5∕8	5/8	5/8	19/16	.381	.604	H-512	3/4	₹6	5/8	115/16		3.
H-384	11/4	5/16	5∕8	19/16	.381	.509	H-2 57	3/4	9/16	3/4	113/16	.574	.7
H-8	1	1/2	1/2	19/16	.391	.694	H -168	1	3/8	3/4	21/16	.579	.6
H-260	5∕8	5/8	1	1	.391	.568	H-151	1	15/32	1/2	21/2	.588	3.
H-102	11/8	23/64		19/16	.395	.543	H-331	5%	5% 7/	1/2	3	.588	٤.
H-208 H-386	11/8	5/8	1/2	11/8	,396	.892	+H-369	11/8	7/16	11/16	13/4	.592	.7
H-681	3/4	3/8	3/4	17/8	,396	.441	H-357 +H-411	11/8	7/16	5% 54	115/16	.597 .598	
H-191	11/4	3/8	3/8	21/4	.396	.724	+H-224	7/8 11/8	7/16 9/16	5/8 9/16	21/2		
H-600	11/4	3/8 5/8	11/8 3/8	17/8 13/4	.398	1.03	H-341	1 1 78	1/2	5/16 5/8	115/16	.606	
H-52	3/4	78 3/8	978 3/4	115/16		.45	H-206	11/2	1/2	13/32	2	.61	1.3
H-340	1	7/16	3/8	21/2	.41	.749	+H-13	1	5%	5/8	19/16	.611	2.0
H-226	3/4	3/6	13/16	113/16	.413	.441	H-55	11/8	3/6	3/4	1 15/16	.614	. (
H-280	3/4	1/2	3/4	11/2	.422	.555	H-296	7/8	3/8	3/4	21/2	.615	. (
H-57	1/2	7/16	7∕8	21/4	.432	.403	H-135	7/8	5∕8	11/16	111/16	.635	3.
H-205	11/4	23/64	5/8	19/16	.439	.601	H-112	3/4	5/8	3/4	113/16	.638	3.
H-303	1	9/16	1/2	19/16	.439	.808	H-65	1/2	1/2	1	29/16	.641	
H -178	11/2	3/8	1/2	19/16	.44	.725	H-59	3/4	7/16	₹ 8	21/4	.646).
H-333	3/4	1/2	7/16	23/4	.451	.72	H-120	1	3/8	3/4	25/16	.65	. (
H-362	1	5/16	3/4	115/16		.485	+H-2 0	11/4	5/16	3/4	25/16	.677	٠. ا
H-478	1	3/8	₹	115/16		.577	+H -56	11/4	3%	3/4	115/16		-
H-306	1	7/16	5/8	111/16	.461	.64	H-212	11/2	3%	5/ 8	115/16	.682	ا. ا
H-387 H-107	7/8	3/8	3/4	17/8	.461	.514	H-312	3/4	3/4	5/8	115/16	.682	1.0
H-292	11/8	3/8	5/8	13/4	.462	.611	H-395	3/4	5/8	3/4	115/16	.682	
H-53	11/4	5/16	5/8	115/16		.582	H-572	1 13%	1/2 34	3/4	115/16		
H-353	1 7/8	3/8 7/16	3/4 5/8	113/16	.477	.524 .655	H-119 H-162	11/2	3/8 1/2	11/16 5/8	2 1/16 19/16	.732	1.0
H-435	1/2	3/8	1 78	29/16	.482	.376	H-60	7/8	7/ ₁₆	78 78	21/4	.752	1 13
H-12	1 2	1/2	5%	19/16	.482	.724	+H-15	1 78	5/8	5/8	115/16		1.0
H-401	11/4	1/2	1/2	19/16	.489	.868	H-479	11/4	1/2	5/8	115/16		1.0
H-482	1/2	1/2	7/8	21/4	.493	.472	H-323	7/8	7/16	1	2	.764	[]
H-4 96	11/4	3%	5%	111/16		.661	H-24	7/8	3/8	15/16		.768	,
H -118	3/4	34	3/4	13/16	.501	.855	+H-410	11/8	7/16	5%	1/4	.77	ی
·H-300	1	3/8	3/4	113/16	.509	.576	H-132	1	3∕8	13/16	13/4	.781).
H-339	1	7/16	5/8	1 1/8	.512	.68	H-388	11/2	3/8	3/4	17/8	.791	٤.
H-494	5%	1/2	11/16	19/16	.519	.52	H-66	5∕6	1/2	1	29/16	.802	. €
H-136	7∕8	9/16	5/8	111/10		.768	H-673	7∕8	9/16	7∕8	17/8	.808	3.
H-474	5∕8	1/2	19/16	11/16	.52	.537	H-131	11/4	3∕8	3/4	25/16	.814	.8
H-159	1	5/8	3%	21/4	.527	1.083	+H-370	11/8	1/2	3/4	115/16		9.
H-209	1	7/16	5/8	115/10			H-602	11/2	3∕8	3/4	115/16		3.
H-196	1	11/32	3/4	21/16	.532	.553	H-355	1	11/16	11/16	13/4	.828	1.1
⊦H-10	1/8	1 5/8	1 5%	19/16	.534	.846	∔H -16	11/8	5%	5%	115/16	.85	1.2

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eatalog aumber	dimen		n inche		relative	weight:	catalog number	dimen	sions ir	inche	s	relative	
umber	strip width	build up E	win- dow width F	win- dow length G	power handl'g capac'y	pounds	number	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	poun
	D .		r	G		<u></u>		D	E	F	G		
4 mil s	eries	H			.—-		4 mil s	eries	H				
H-236	13/8	7/16	11/16	21/16	.852	.997	H-241	3/4	13/32	13/8	3	1.257	.74
H-305	11/8	7/16	3/4	25/16	.853	.89	H-69	1 ~	1/2	1	29/16	1.281	1.0
+H-61	1	7/16	7/8	21/4	.86	.805	+H-415	11/4	5%	5/8	25%	1.281	1.6
-H-559	15%	9/16	9/16	111/16	.866	1.389	+H-27	11/2	3/8	15/16	21/2	1.32	1.0
H-232	1	1/2	3/4	25/16	.867	.929	H-181	3/4	3/4	15/16	21/2	1.32	1.2
H-239	1	5/8	3/4	115/16		1.12	H-146	134	5/8	5/8	115/16		1.8
H-265	1	3/4	5%	115/16		1.375	+H-534	13%	11/16	11/16	21/16	1.342	1.7
H-436	3/4	3/8	11/8	27/8	.909	.626	H-289	11/8	11/16	3/4	25/16	1.343	1.5
H-143	7⁄8	3/8	15/16	3	.921	.72	H-76	3/4	9/16	11/8	27/8	1.366	1.0
H-413	11/8	17/32	5/8	21/2	.933	1.14	H-571	1 7	5%	5%	31/2	1.369	1.5
H-612	2	1/2	1/2	11/8	.938	1.33	H-266	11/8	5%	7 ⁄8	21/4	1.384	1.3
H-397	1	1/2	5∕8 ∣	3	.939	1.07	H-164	13/8	23/32	11/16	21/16	1.402	1.8
H-123	13/8	13/32	3/4	21/4	.943	.978	+H-414	13%	5∕8	5∕8	25/8	1.41	1.7
H-18	11/4	5∕8	5∕8	115/16		1.353	H-141	11/8	15/32	11/8	23/8	1.411	1.0
H-302	7∕8	%	3/4	25/16	.948	1.077	H-154	13%	19/32	3/4	25/16	1.417	1.5
H-455	7∕8	3/4	3/4	115/16	.953	1.242	∔H- 560	17/8	5∕8	5∕8	115/16	1.42	2.0
H-67	3/4	1/2	1	29/16	.961	1.791	H-354	11/4	9/16	7∕8	25/16	1.422	1.3
H-150	13/8	13/32	3/4	25/16	.969	.997	H-70	11/8	1/2	1	29/16	1.442	1.1
H-62	11/8	7/16	7∕8	21/4	.97	.907	H-4 71	11/4	9/16	3/4	23/4	1.449	1.4
H-22	11/2	3∕8	3/4	25/16	.976	.989	H-263	13%	3/4	1 1/16	21/16	1.462	1.9
H-170	3/4	3/4	3/4	25/16	.976	1.153	+H-19	11/8	3/4	3/4	25/18	1.463	1.7
H-134	7∕8	5∕8	11/16	111/16	.981	1.00	+H-26	11/4	1/2	15/16	21/2	1.465	1.2
H-301	.7/8	3∕8	1	3	.984	.73	H-604	1%	5/8	3/4	115/16		1.8
H-272	1	1/2	7/8	21/4	.986	.945	H-399	1	3/4	3/4	25/8	1.478	1.6
H-352	11/8	5/8	5/8	21/4	.988	1.31	H-437 H-334	3/4	1/2	11/4	33/16	1.495	9.
H-613	11/8	9/16	13/16	115/16	.996		a I	1	1/2	11/2	2	1.50	1.0
H-680	11/4	1/2	13/16	2	1.02	1.10	H-390	1	1/2	1	3	1.50	1.1
H-491	11/2	9/16	5/8	115/16		1.42	H-113	13/4	1/2	3/4	25/16	1.517	1.6
H-412	11/4	17/32	5/8	21/2	1.038	1.222	H-220	13/4	3/8	15/16	21/2	1.538	1.2
H-429	1	1/2	13/16	1¾	1.04	.911	H-322	11/4	<i>7</i> ⁄8	5∕8	21/4	1.539	2.3
H-389 H-336	2 %	3% 3%	3/4 15/16	1 1/8 21/2	1.056 1.075	1.183 .699	H-228 +H-86	1½ %	19/32	3/4	25/16	1.544 1.559	1.7
H-63					1.075	1.007	H-449		5/8	11/4	33/16		1.0
H-347	11/4	7/16	7/8 3/4	21/4 25/16	1.026	1.162	H-142	13/8 11/8	9/16 15/32	7⁄8 13∕₁6	25/16	1.563 1.568	1.5
H-537	1 1	½ %	9/4 3/4	25/16	1.084	1.102	+H-541	11/4	5/32 5/8	7/8	2½ 25/16	1.579	1.5
H-540	11/8	78 9/16	13/16	21/8	1.094	1.166	H-295	11/4	13/16	% %	21/2	1.579	2.1
H-605	2 2	3/8	3/4	115/32	1.091	1.20	H-77	7/8	9/16	78 1½	2½ 2½	1.593	1.1
H-392	11/8	78 9/16	74 3⁄4	25/16	1.096	1.207	H-71	11/4	1/2	1 /8	29/16	1.601	1.3
H-346	7/8	5%	13/16	111/16	1.097	1.032	H-248	11/2	5/8	3/4	25/16	1.628	1.8
H-432	13%	9/16	11/16	21/16	1.097	1.358	H-313	13/8	19/32	13/16	21/2	1.658	1.6
H-68	7∕8	1/2	1	29/16	1.122	.922	H-293	11/8	3/4	3/4	2¾	1.741	1.9
H-75	5/8	9/18	11/8	21/8	1.136	.834	+H-28	11/2	1/2	15/16	21/2	1.758	1.5
H-332	7/8	7/16	1	3	1.146	.873	H-221	2	3/6	15/16	21/2	1.758	1.4
H-35	3/4	3/4	13/16	13/4	1.171	1.135	H-72	13%	1/2	1	29/16	1.763	1.4
H-64	13/8	7/16	7/8	21/4	1.184	1.106	+H-21	13%	3/4	3/4	25/16	1.787	2.1
H-259	11/4	5/8	5/8	27/16	1.189	1.525	H-489	11/8	3/4	1	21/8	1.794	1.7
H-366	1	3/4	5%	29/16	1.202	1.58	H-467	11/8	5%	1	29/16	1.801	1.5
H-153	11/4	9/16	3/4	25/16	1.218	1.343	H-309	13%	9/16	15/16		1.81	1.6
H-502	11/2	5/8	7/8	11/2	1,232	1.536	H-431	1½	5/8	15/16	21/16	1.812	1.8

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catalog	dimen	sions ir	n inche	8	relative		catalog	dimen	sions ir	inche	S	relative	weigh
number	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pounds	number	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pound
	D	E	F	G	l	<u> </u>		D	E	F	G		
mil s	eries	Н					4 mil s	eries	H				
H-325	1	25/32	15/16	21/2	1.83	1.77	+H-542	15%	3/4	1	29/16	3.123	2.79
H-204	13%	3/4	34	23/8	1.836	2.144	H-84	13/4	9/16	11/8	27/8	3.183	2.33
H-87	3/4	5/8	11/4	33/16	1.868	1.237	H-421	11/8	1/2	15/8	31/2	3.203	1.62
H-472	11/2	17/32		21/2	1.868	1.649	H-264	13/4	5/8	1	3	3.282	2.63
H-73	11/2	1/2	1	29/16	1.922	1.581	∔H -188	11/2	3/4	1	3	3.375	2.83
H-211	11/2	9/16	1	25/16	1.949	1.71	H-85	17/8	9/16	11/8	27/8	3.41	2.5
·H-23	11/2	3/4	3/4	25/16	1.951	2.309	H-92	13%	₹8	11/4	33/16	3.424	2.2
H -417	1%	1 1/16	11/16	3	1.953	1.60	H -311	13%	11/16	11/8	31/4	3.458	2.50
H-561	2	11/16	11/16	21/16	1.953	2.555	H-242	11/2	15/16				3.4
H-106	11/2	5%	15/16	21/4	1.978	1.901	H -37	13/4	1/2	1%	3	3.609	2.20
H-267	11/8	3/4	15/16	21/2	1.978	1.892	H-344	11/4	1/2	11/2	37/8	3.635	1.8
H-498	11/4	1/2	11/8	27/8	2.021	1.45	H-501	11/2	3/4	15/16		3.689	3.1
H-79	11/8	9/16	11/8	27/8	2.044	1.502	∔H -418	17/8	3/4	3/4	31/2	3.693	3.7
H-80	11/8	9/16	11/8	27/8	2.044	1.686	H-505	11/4	3/4	15/16		3.736	2.9
H-499	11/4	5∕8	3/4	31/2	2.051	1.99	H-93	11/2	5∕8	11/4	33/16	3.74	2.4
H-74	15/8	1/2	1	29/16	2.083	1.712	H-128	2	1/2	11/4	3	3.75	2.4
H-268	1	3/4	7 ⁄8	31/4	2.132	1.93	+H -36	13/8	5/8	15/16	31/2	3.945	2.4
H-288	11/2	5/8	1	25/16	2.169	1.95	H-94	15%	5/8	11/4	33/16	4.049	2.6
H-88	7 ⁄8	5%	11/4	33/16	2.181	1.44	+H -563	21/2	13/16			4.12	4,5
H-29	11/2	5%	15/16	21/2	2.198	2,001	H-337	11/4	5%	13%	37/8	4.162	2.3
H-4 50	3/4	3/4	11/4	33/16	2.244	1.54	H-493	21/4	5/8	1	3	4.218	3.4
H-30	11/2	1/2	1	3	2.25	1.744	H-439	1	5/8	15%	43/16	4.255	2.0
H-490	11/8	3/4	11/8	23/8	2.256	1,91	H-291	13/4	3/4	15/16	31/2	4.305	3.5
H-423	13/4	5∕8	3/4	23/4	2.258	2.377	+H-95	13/4	.5%	11/4	33/16	4.361	2.8
H-438	1	1/2	15/16	31/2	2.296	1.363	+H -31	11/2	1	1	3	4.50	4.0
H-329	7∕8	7/8	1	3	2.298	2.003	H-492	2	3/4	1	3	4.50	3.7
H-416	15%	11/16		3	2.307		+H-543	13/4	13/16	11/8	21/8	4.597	3.6 3.0
H-122	11/2	1/2	11/4	21/2	2.345	1.65	H-503	11/2	3/4	13/8	3	4.641	
H-218	11/2	5/8	15/16	211/16		2.09	H-96	17/8	5/8	11/4	33/16	4.67	3.0
H-406	13%	11/16	1	29/16	2.424	2.129	H-294	11/8	3/4	19/16	39/16	4.695	2.5
H-271	11/2	3/4	15/16	25/16	2.437	2.41	H-44 1	13%	3/4	15/16	31/2	4.736	3.0
H-603	21/4	3/4	3/4	115/16		3.15	H-192	13/4	3/4	11/8	31/4	4.80 4.853	3.5
H-523	17/8	1/2	3/4	31/2	2.464	2.30	H-227	21/4	3/4	1	27/8		4.1
H-89 H-81	1	5/8	11/4	33/16	2.49	1.649	H-422 H-32	13%	% 1	13%	4½ 3	4.872 4.875	2.7
H-165	1%	9/16	11/8	27/8	2,501	1.833 1.562	H-32 H-617	15%	7/16	1	41/2	4.875	3.3
H-394	1	9/16	15/16	31/2	2.58		H-451	21/2	1 716	15/16	21/2	4.92	3.9
H-213	11/2	1	3/4	25/16	2.601 2.635	3.376 2.299	H-451	11/2	5/8	11/4	33/16	4.92	3.9
H-500	21/4	1/2	15/16	21/2			H-486	1 -		11/4	33/16	5.047	3.8
H-82	11/2	3/4	15/16		2.635 2.726	2.516 1.998	H-420	11/8 15/8	11/8	13/8	35/8	5.064	2.9
11-02	11/2	9/16	11/8	27/8	2.720	1,996	H-420	178	78	1 78	378	3.004	2.0
H-225 H-258	13/4	5/8	15/16	211/16	2.755 2.765	2,444 1,925	+H-33 H-330	13/4	1	1	3 31/2	5.25 5.25	4.7
H-258 H-90	11/2	9/16	15/16	21/2			RS		1	1 -	3 1/2	5.25	3.1
H-90 H-273	11/8	5/8	11/4	33/16	2.802	1.855	H-195	11/2	3/4	19/16	43/16	5.271	2.5
H-273	11/2	3/4	1	21/2	2.813	2.55	H-440	11/4	5/8	1%	3		3.6
H-83	21/4	3/4	3/4	25/16	2,927	3.47	H-460 H-274	15%	13/16		3	5.445 5.697	4.9
H-63 H-419	15%	9/16	1 1/8	27/8	2.953	2.168	607	21/4	27/32	19/-		5.735	3.1
H-396	1½ 2	3/4	3/4	31/2	2.954 3.00	2.973	H-324 H-426	13/8	3/4	19/16	39/16 37/8	5.735	3.5
H-25	_	1/2	1 15/				906	-/-	7/8 15/-				5.7
H-91	13/8	15/16		21/2	3.018	3.074	+H-564	21/2	15/16				1
77-21	1 1/4	1 5/8	11/4	33/16	3.111	2,056	H-565	2	3/4	11/4	33/16	3.970	1 44,1

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	dimen	sions ir	inche	8	relative	
number	strip	build	win-	win-	power handl'g	pounds
	width	up	dow	dow	capac'y	
	D	E	width F	length G		
4 mil s	eries	H				
H-147	11/2	3/4	13%	37/ _R	5.995	3.531
+H-34	2	1	1	3	6.00	5.432
+H-155	2	3/4	13%	3	6.189	4.05
+H-358	13%	1	15/16	31/2	6.314	4.287
H-198	13/4	7/8	13%	3	6.315	4.278
H-524	21/4	1	1	3	6.75	6.10
H-184	2	5%	15%	33/8	6.855	3.65
H-443	11/2	1	15/16	31/2	6.888	4.675
4H-544	13/4	7∕8	15/16	31/2	7.032	4.62
H-535	21/4	13/16	13%	3	7.536	5.02
H-373	2	25/32	17/16	37/16	7.716	4,656
H-454	21/2	1	11/16	3./16	7.965	6,85
H-461	2 2	i	13%	3	8.25	5.791
H-182	21/2	29/32	13/16	31/8	8.409	6.35
H-393	21/4	11/4	19/16	3 /8	8.439	8.187
H-427	11/2	13%	13%	3	8.511	6,606
H-130	2	23/32	17/16	41/8	8.522	4.69
H-150	1				8.856	5.19
H-506	21/8	15/16	1½ 1%	41/2	8.869	
H-497	2 /8	3/4 1		39/16		4.90
H-491	4	1	17/16	37/16	9.878	6,29
+H -545	2	1	13%	35%	9.969	6.41
H-400	21/2	3/4	1%	31/8	9.99	5.893
H-256	21/2	1	1	4	10.00	8.00
H -616	21/2	7/16	2	411/16		3.96
H-249	13/4	1	11/2	4	10.50	6.063
H-516	2	7∕8	11/2	4	10.50	5.88
H-475	2	1	11/4	41/4	10.625	6.926
H-507	11/2	13%	1%	33/16	10.686	7.025
H-481	21/2	31/32	15/16	31/2	11.127	7.479
H-319	2	1	11/4	41/2	11.25	7.16
H-611	21/4	1	13%	37/8	12.00	7.47
+H-546	21/4	1	11/2	4	13.50	7.77
H-628	11/2	11/2	15%	43/16	15.30	8.91
H-717	71/4	5	7		4060.00	546.00
	- /4		-		,	0.0.00

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atalog	dimen	sions i	n inche		relative		catalog	dimen	sions i	n inche	s	relative	
umber	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pounds	number	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pound
	D .	E	F	G	!	<u> </u>		D	E	F	G		
2 mil s	eries	L					2 mil s	eries	L				
-L -1	1/4	1/8	1/4	1/2	.004	.013	+L-12	1/2	7/16	1/2	11/8	.124	.244
L-66	1/4	1/8	1/4	9/16	.004	.016	+L-11	34	3/8	3/8	13/16	.125	.293
L-163	1/4	5/32	1/4	1/2	.005	.019	L-216	3%	¾	5%	19/16	.137	.19
L-305	3/6	1/8	1/4	1/2	.006	.021	+L-135	1/2	7/16	9/16	11/8	.138	.25
-L-2	1/4	3/16	1/4	548	.008	.027	L-167	1/2	7/16	1/2	11/4	.138	.25
L-143	1/4	1/4	1/4	1/2	.008	.035	L-208	96	5/16	7/16	15%	.138	.24
-L-147	1/4	1/8	5/16	1	.01	.023	L-33	1/2	1/2	1/2	11/8	.141	.29
L-161	1/4	1/4	1/4	56	.01	.039	L-142	3/4	3/8	1/2	11/8	.159	.30
+L-3	3/6	3/16	1/4	5/8	.011	.039	+L-78	34	5/16	5/16	21/4	.164	.34
+L-4	1/4	1/4	1/4	₹⁄B	.014	.047	L-97	₹6	3/18	5/8	2	.176	.21
L-306	1/2	3/16	1/4	5 / 6	.015	.06	L-136	1/2	9/16	1/2	11/4	.176	.36
L-284	₹6	5/32	5/16	1	.018	.044	L-83	3/4	5/16	5%	11/4	.183	.26
-L-5	3/6	1/4	1/4	7∕8	.020	.067	L-107	5%	6/16	5∕8	11/2	.183	.24
L-281	5/16	1/4	6/16	7∕8	.021	.058	L-45	% 5€	1/2	7/16	13%	.188	.39
L-71	₹8	3/16	5/16	1	.022	.053	+L-14	1/2	1/2	1/2	19/16	.195	.34
L-269	3%	9/32	1/4	7∕8	.023	.079	L-152	1/2	1/2	1/2	15%	.203	.35
-L -7	3/6	7/32	6/16	1	.026	.064	L-202	1/2	7/16	1/2	1 7/B	.206	.32
-L-6	1/2	1/4	1/4	7∕8	.027	.091	+L-18	1/2	7/16	5∕8	19/16	.214	.30
L-76	₹8	3/16	3%	1	.027	.05	L-131	1	7/16	1/2	1	.219	.46
L-37	₹6	7/32	6/16	11/16	.028	.068	L-207	1/2	7/16	1/2	2	.22	.33
L-114 L-132	3/8 2/	7/32	5/16	11/8	.029	.072	L-211	3/4	3/8	1/2	19/16	.22	.36
L-132 L-151	3/8	1/4	5/16	1	.029	.076	L-181	_%6	5/8	1/2	11/8	.221	.49
L-131	5/8	1/4	3/16	1 1/8	.033	.116	L-153	1	31∕8	1/2	13/16	.223	.41
L-02 L-124	1/4	1/4	1/2	11/8	.036	.063	L-169	1/2	7/16	5%	15%	.223	.31
L-69	1/2	1/4	6/16	1	.039	.103	L-308	3/4	1/4	5%	129/32	.225	.06
L-51	3%	1/4 5/16	1/2	11/4	.04	.067	L-254	3/4	7/16	5/16	21/4	.23	.50
L-240	78 3%		15/32	3/4	.041	.10 .087	L-75 L-268	1,	11/32		11/4	.241	,39
L-88	1	1/4	3/6 5/	13/16 1	.042	.129	L-200 +L-15	1/2	1/2	5/6	19/16	.244	.36
L-247	3/8 1/4	3/6 1/4	5/16 7/16	19/16	.044	.071	L-32	5% 1	1/2 1/16	1/2	19/16 11/8	.245 .246	.43 .49
L-261	3%	9/32	3/8	13/16	.046	.101	L-190	1/2	3%	7 ⁄8	11/2	.248	.27
L-123	1/2	1/4	3%	1	.047	.106	L-166	3/4	1/2	5%	11/8	.263	.46
L-138	3%	1/4	1/2	1	.047	.084	L-219	1/2	7/16	5%	115/16		.34
L-40	1/4	1/4	1/2	19/16	.05	.081	L-42	96 96	5/8	1/2	13%	.27	.54
L-267	1/4	1/4	5%	19/16	.061	.081	L-28	l ı´	7/16	1/2	11/4	.274	.53
L-121	3/6	1/4	1/2	15/16	,062	.099	L-203	1	1/2	1/2	11/8	.281	.58
L-8	3%	3%	3/6	13/16	.063	.147	+L-16	3/4	1/2	1/2	19/16	.294	.51
L-232	1/2	1/4	1/2	11/8	.071	.121	L-217	1/2	1/2	5%	115/16	.302	.40
L-280	1 %	6/16	3%	l i'	.073	.105	L-86	l 1′	1/2	1/2	11/4	.313	.61
-L-9	1/2	3/8	₹6	13/16	.084	.197	L-250	i	5%	3/8	13%	.322	.82
-L -13	5%	1/4	1/2	11/8	.088	.153	L-43	5%	5%	5%	19/16	.381	.60
L-159	1/2	1/2	3/6	1	.094	.261	L-210	3/4	3%	3/4	113/16	.382	.43
L-227	1/2	7/16	3/8	13/16	.097	.238	L-30	7∕8	9/16	5/8	11/4	.385	.66
L-41	₹6	₹6	1/2	13%	.098	.169	+L -17	1	1/2	1/2	19/16	.391	.69
L-50	5%	1/4	1/2	11/4	.098	.162	L-39	5/8	1/2	5%	2	.392	.58
L-94	5%	5/16	5/16	15%	.099	.228	L-307	7⁄в	3/6	5/8	115/16	.397	.50
L-272	5%	9/32	1/2	11/8	.099	.174	L-184	1	7/16	5/6	11/2	.41	.60
L-192	3√8	3/16	11/8	11/4	.10	.091	L-220	1/2	1/2	3/4	25/16	.435	.46
-L-10	5%	3/6	3/6	13/16	.105	.243	L-241 L-266	1/2	1/2	1	13/4	.438	.42
L-238	1/2	7/16	1/2	1	.11	.23	L-266	3/4	3/4	5%	11/4	.44	.84

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atalog	dimen	sions is	n inche	8	relative	weight:	catalog	dimen	sions i	inche	•	relative	
umber	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pounds	number	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pound
	D	E	F	G		<u> </u>		D	E	F	G		
mil s	eries	L					2 mil s	eries	L				
L-236	1	3∕8	5%	115/16	.453	.57	L-84	3/4	3/4	15/16	21/2	1.32	1.26
L-243	1	15/32	5/8	19/16	.458	.662	L-157	7∕8	7∕8	1	13/4	1.341	1.54
L-127	3/4	3/4	3/4	1 1/e	.475	.844	L-303	13%	19/32	3/4	25/16	1.42	1.56
L-154	3/4	3%∈	3/4	21/4	.475		L-99	1	% 8	15/16	21/2	1.465	1.33
L-19	1	1/2	5/8	19/16	.489	.724	L-201	11/2	1	5/8	19/16	1.465	2.76
L-204 L-174	1	5/8	5/8	11/4	.489 .493	.87 1.278	L-197	11/4	9/16	5/8	31/2	1.537	1.7
L-200		7∕8 3∕	1/2 1/8	1 1/8 23/8	.504	.374	L-31	2	3% 9/a	13/16	13/4	1.559	1.2
L-200 L-92	1/2	% 1/2	13/16	13/4	.504	.455	L-177 L-259	7/8 3/4	9/16 3/4	1 1/e 1	21/8 3	1.593 1.689	1.1
L-92 L-271	1/2 1/8	7∕2 5∕8	5/8	19/16	.52		L-255 L-47	% 1	1 7/4	3/4	25/16	1.734	2.2
	78	78			.554		8	•	•		2716	1.754	2.2
L-122	3/4	3/4	13/16	13/16	.543	.88	L-120 L-128	1	3/4	15/16	21/2	1,758	1.6
L-244	3/4	1/2	3/4	115/16			8 	11/8	11/16	15/16	21/2	1.813	1.8
L-21 L-91	3/4	5/8 L/	5/8	115/16	.568 .585	.81 .51	L-100 L-175 L-133	1	, 5/8	1	3	1.875	1.5
L-91 L-112	1 1/2 1	1/2	15/16	21/2	.602	.785	L-175 L-133	5%s 1	13/16	1 15/16	3 2½	1.875 1.903	1.6 1.8
L-20	i	1/2 5/8	5/8	13/4	.611	.965	L-133 L-277	1	13/16	15/16	21/2	1.903	1.8
L-155	li l	7/16	5/8	21/4	.614	.743	L-172	i	5/8	11/4	21/2	1.953	1.4
L-245	i l	1/2	7 /8	11/2	.657	.764	L-252	11/32	19/32	11/4	27/8	1.981	1.4
L-288	7∕8	1/2	1/2	3	.657	.904	+L-25	1	7⁄8	15/16	21/2	2.05	2.0
L-196	11/8	1/2	7/16	23/4	.677	1.082	L-49	11/8	25/32	15/16	21/2	2.06	1.9
L-149	1	1/2	1/2	23/4	.688	.965	L-251	11/8	21/32	1	21/8	2.122	1.7
L-296	1/2	1/2	11/4	21/4	.703	.514	L-95	1	5%	1	31/2	2.188	1.6
L-85	1	7/16	7∕8	1 1/8	.716	.915	L-188	13/8	7∕8	13/16	21/4	2.198	2.5
L-64	11/8	1/2	7/16	3	.738	1.142	L-60	11/2	1/2	3/4	4	2.252	2.0
L-239 L-22	3/4 1	3√a	11/8	23/6	.751	.551	L-110	11/8 1	, ⁷ ⁄8	15/16	21/2	2.305	2.2
L-22 L-65	i	5%s 3%s	5% 13/-	115/16 13/4	.757 .781	1.08 .645	L-102 L-150	-	1	15/16	2½ 1¾	2.343 2.429	2.4 1.8
L-214	11/6	718 516	13/16 5/8	115/16		1,22	L-150 L-46	7⁄8 11∕8	7/8 7/8	1 13/16 15/16	211/16		2.3
L-186	1	78 3√6	15/16	21/2	.878	.729	L-93	1 7B	78 5%	1	4	2.50	1.8
L-38	3/4	₹8	3/4	21/2	.88	.956	L-106	21/2	19/32	3/4	25/16	2.576	2.8
L-44	3/4	5√6	3/4	29/16	.902	.983	L-212	11/4	11/4	3/4	25/16	2.73	3.8
L-228	1	5/B	3/4	1/5/16		1.12	+L-248	11/8	3/4	1/8	21/8	2.731	2.1
L-23	11/4	5∕8	5%	115/16	.945	1.352	L-170	11/8	5/8	11/4	33/16	2.802	1.8
L-108	3/4	3/4	3/4	21/4	.95	1.14	L-179	11/4	13/16	11/4	21/4	2.855	2.3
L-182	3/4	3/4	3/4	25/16	.976	1.16	L-73	1	⅓ 8	15/16	31/2	2.87	2.4
L-258	3/4	7/16	1	3	.984	.74	L-103	11/4	1	15/16	21/2	2.928	3,0
L-191	1	1/2	7∕8	21/4	.986	.944	L-53	13/6	7∕8	15/16	211/16		2.9
L-209	3/4	7/16	13/16	29/16	.999	.701	L-77	11/4	3/4	11/8	3	3.165	2.4
L-178 L-165	11/2	11/16 9/16	5√8 5√8	19/16 25/16	1.007	1.645 1.292	L-189 L-81	15% 11/8	25/32 1	16/16 1	211/16 3	3.196 3.375	2.9 3.0
L-24	1				1.084	1,22	L-61		29/	15/	211/16		3,3
L-24 L-145	11/4	% %a	3/4 29/32	25/16 19/16	1.106	1.307	L-61 L-140	1½ 1¾	²⁹ / ₃₂ ⁷ / ₈	15/16 1	27/8	3.422	3.0
L-139	7/8	787 5√8	13/16	13/4	1.138	1.05	L-249	11/8	3/4	13%	3	3.483	2.2
L-48	11/2	1/4	13/4	13/4	1.148	.70	L-111	13/4	74 7/8	15/16	21/2	3.588	3.5
L-74	7/8	9/16	15/16	21/2	1.153	1.03	L-35	11/4	1	1	3	3.75	3.3
L-187	13%	9/16	1/2	3	1.161	1.644	∔L-98	1	5%	2 .	3	3.75	1.8
L-195	11/4	5/8	1/2	3	1.173	1.692	L-164	1	1	11/4	3	3.75	2.8
L-173	3/4	5√8	1	29/16	1.202	1.03	L-115	13/4	3/4	1	3	3.939	3.3
L-194	11/4	9/16	3/4	25/16	1.218	1.345	L-70	13%	5∕8	15/16	31/2	3.945	2.4
L-119	1	5%	13/16	21/2	1.27	1.31	L-101	13/4	29/32	15/16	211/16	3.994	3.8

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atalog		sions i	inche	8	relative		catalog	dimen	sions i	n inche		relative	
umber	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pounds	number	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pound
	D	E	F	G				D	E	F	G		
mil s	eries	L					2 mil s	eries	L				
L-27	2	7∕8	15/16	21/2	4.10	4.08	L-180	15%	19/16	1 13/16	41/8	22, 4 2	11.2
L-118	11/4	15/16	17/16	21/2	4.208		L-56	15%	11/2	2 /10	411/16		10.7
L-279	11/2	7/8	11/16	31/16	4.268	3.48	L-237	21/2	1 1/8	13%	37/8	24.978	18.6
L-226	13/4	5/8	15/16		4.356	3.30	L-276	11/2	11/2	3	4	27.00	10.1
L -113	11/4	11/4	11/4	21/4	4.397	4.16	L-125	2	13%	2	5	27.50	12.3
L-54	2	3/4	3/4	4	4.50	4.325	L-225	2	11/2	2	411/16	28.128	13,3
L-130	11/2	1	1	3	4,50	4.06	L-224	2	11/2	2	5	30.00	13.6
L-146	11/4	11/4	3/4	3	4.688	5,125	L-246 L-263	21/2	2 25/	11/2	5	37.50 38.463	23.5 32.9
L-104 L-206	11/4 13/8	1 1/4 3/4	15/16	31/2	4.689 4.736	4.55 3.01	L-264	2¾ 2	25% 13%	1 3/6 23/4	31/a 6	45.378	14.8
L-36	11/4	1	13%	3	5.157	3.62	L-278	2	21/2	2	411/16	46.88	25.8
L-160	11/4	11/8	13/16	33/16	5.324	4.16	L-297	3	2	13/4	49/16	48.00	27.6
L-158	11/4	13/16	7∕8	41/8	5.358	4.93	L-285	21/2	11/8	21/4	913/16		34.1
L-213	15%	1	11/8	3	5.484	4.50	L-262	11/2	21/2	23/4	111/4	108.00	32.9
L-183 L-105	11/4	11/8	11/4	3 ³ / ₁₆	5.605	4.25	L-289 L-310	31/8	115/16	2½ 3	81/16	121.00	39.7
L-103 L-223	11/2	11/4	1 13%	3	5.625 5.862	5.48 3.91	L-310 L-313	4½ 3	1½ 3	31/2	83/4 141/2	177.00 457.00	46.2 97.1
L-223 L-29	13/4	11/8	1 78	3	5.907	5.54	L-302	31/B	43/16	6	1734	1385.00	195.0
L-59	2	1	i	3	6.00	5.25	L-301	61/4	43/16	6		2790.00	390.0
L-148	13/4	3/4	15/16	31/2	6.031	3.84		- /4	/ 10	-	74		
L-205	2	1	15/16	21/2	6.56	5,24	1						
L-144	2	11/8	1	3	6.75	6.33	1						
L-275	1	3/4	3	3	6.75	2.60	1						
L-52 L-117	15% 2	½ 1	1 15/16 13/16	211/16 31/8	7.403 7.425	3.31 5.72	3						
L-87	11/8	15%	13/6	3 3 3	7.542	6.19)						
L-215	2′°	3/4	11/4	43/16	7.853	4.80							
L-168	1	1~	2	4	8.00	3.67	4						
L-68	2	1	13%	3	8.25	5.78							
L-126	2	11/4	11/8	3	8.439	7.41	1						
L-260	2	1	11/4	31/2	8.75	6.12							
L-89 L-63	3/4	11/4	11/4 3	3	9.375	7.58							
L-72	2 74	11/2	13%	3	10.125 10.314	4.48 7.73							
L-221	11/2	11/2	15/16	31/2	10.314	7.88							
L-299	2	1	11/4	41/4	10.60	6.85							
L-176	11/2	13%	11/4	41/4	10.961	7.75							
L-199	15%	11/4	15/16	45%	12.326	7.85							
L -171	1	11/4	2	5	12.50	5.44	1						
L-198	2	11/4	11/4	43/16	13.088	9.20							
L-242 L-193	2 21/2	11/4	11/4	41/4	13.281	9.04	\$						
L-193 L-185	2 2	11/4	19/16	4½ 3%	14.063	11.40 11.00	À						
L-141	11/2	11/2	11/2	5	16.692 16.875	9.50							
L-233	2	11/4	11/2	41/2	16.875	9.50							
L-55	15%	11/2	13/4	41/16	17.333	9.50	d						
L-218	11/4	11/4	2	6	18.756	7.56							
L-67	15%	11/2	13/4	411/16	20.004	10.49							
L-222 L-129	2 2	11/2	11/2	41/2	20.25	12,30							

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append	lix b—	core I	isting	K-18		/	og.	22					7
catalog number	dimen strip width	build up	win- dow width	win- dow length	relative power handl'g capac'y		catalog number	strip width	build up	win- dow width	win- dow length	relative, power handl g capac y	weight: pounds
1 \- 21 -	D	E	F	G		<u> </u>	1 1 -	D	E	F	G	<u> </u>	
1 mil s	eries	IAT .					1 mil s	eries	IAT	- \	-/		
+M-3 M-1 M-21 M-10 M-6 M-2 M-4 M-8 +M-7 M-34	1/4 1/4 1/4 1/4 1/4 1/8 1/2 1/2 1/8	1/8 3/16 1/4 3/16 1/4 1/4 1/4 1/32 1/4	1/4 1/4 1/4 1/4 1/4 1/4 5/16 1/4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.004 .008 .008 .01 .014 .021 .026 .027	.014 .027 .033 .036 .038 .043 .068 .064 .088	M-52 M-35 M-20 M-54 M-50 M-66 M-59 M-47 M-57 M-28	1 1 1 34 1 134 1½ 1	56 1 78 11/8 1 34 9/16 1 1	3/4 5/6 15/16 15/16 11/8 11/8 11/8 11/2	25/16 1 1 5/16 2 1/2 2 1/16 2 7/8 3 2 7/8 3 3/8 3	1.084 1.211 2.05 2.173 2.427 2.427 4.059 4.853 5.063 7.542	1.198 1.985 2.00 2.55 1.99 1.85 2.47 3.99 3.08 6.05
M-5 M-30 M-37 M-70 M-15 M-11 M-33 M-42 M-24 M-16	78 % % % % % % % % % % % % % % % % % % %	74 34 34 34 34 34 14 34 34 34 34 34 34 34 34 34 34 34 34 34	72 7/16 7/16 1/2 1/2 1/3 1/3 1/3 1/3	13/16 11/8 13/8 13/16 11/8 11/4 13/16 11/8	.063 .07 .08 .081 .084 .088 .103 .105 .124	.143 .143 .147 .114 .193 .155 .12 .239 .24	M-58 M-25	2/3/4	7/8 11/2	15/16	31/2	10036 10025	5.16
M-36 M-61 M-71 M-55 M-53 M-12 M-49 M-43 M-22 M-31	1/2 1/2 5/8 1/2 1/2 1/2 3/4 1/2 5/8	7/16 1/2 3/6 1/16 3/8 1/2 1/16 1/16 1/2 1/16	9/16 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	1 1/8 1 1/4 1 3/8 1 9/16 1 1/8 1 9/16 1 1/4 1 9/16 1 1/8	.138 .156 .161 .172 .192 .195 .205 .214 .245	.246 .301 .26 .286 .257 .341 .378 .299 .425							
M-40 M-60 M-13 M-19 M-56 M-45 M-14 M-48 M-38	3/4 5/8 3/4 1 3/4 1 3/4 1 3/4 1	1/2 3/6 1/2 1/2 1/2 1/16 3/6 5/6	56 13/16 1/2 1/2 56 3/4 5/8 5/8 29/32 5/8	1 1/8 17/16 19/16 19/16 1 15/16 1 1/8 19/16 1 2 5/32 1 3/8	.475 .489 .505	.452 .30 .508 .681 .60 .816 .711 .81 .545							
M-67 M-9 M-65 M-39 M-64 M-62 M-27 M-28 M-51 M-41	3/4 3/4 1 1 3/4 3/4 1 1 1 1/2 1/4	1/2 5/8 1/2 5/8 9/16 5/8 7/16 5/8 1 1/16	34 56 11/16 56 34 34 78 56 56	1 5 6 1 5 1 1 1 1 1 1 1 1	.568 .602 .611 .614 .682	.948 .742 .832 .915 1.06 1.615							

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atalog	dimen	sions i	n inche	S	relative	weight:	catalog	dimen	sions is	inche	5	relative	weight
umber	strip width	build up	win- dow width	win- dow length	power handl'g capac'y	pounds	number	strip width	build up E	win- dow width F	win- dow length G	power handl'g capac'y	pound
	D	E	F	G		L				F	<u> </u>		
mil s	eries	Z					4 mil s	eries	<u></u>				
Z-164	1/4	1/8	1/4	1/2	.004	.014	+ Z -147	3/4	3%	1/2	15/16	.185	.32
Z-568	1/4	1/8	1/4	5/8	.005	.015	Z-124	1	1/2	3/8	1	.188	.52
Z-152	1/2	1/8	1/4	1/2	.008	.027	+Z -555	11/8	3/8	3/8	13/16	.188	.43
.Z-2	3/8	3/16	1/4	5/8	.011	.038	Z-101	3/4	3/8	7/16	15%	.20	.36
Z-127	3/8	13/64	1/4	5/8	.012	.043	Z -117	11/8	9/32	9/16	11/8	.20	.32
Z-110	3/8	1/4	1/4	5/8	.015	.056	+Z -381	₹ ₈	7/16	3/8	17/16	.205	.46
Z-549	1/2	3/16	1/4	5/8	.015	.052	Z -216	3/4	3/8	1/2	11/2	.212	.3
Z-530	1/2	7/32	1/4	5/8	.018	.063	+Z-5	3/4	3/8	5/8	11/4	.220	.33
Z-550	5/8	7/32	1/4	5/8	.021	.079	Z -80	11/8	5/16	9/16	11/8	.222	.30
Z-594	3/8	1/4	5/16	3/4	.022	.065	Z -19	3/4	5/16	5%	19/16	.228	.30
Z-569	3/8	1/4	5/16	7⁄8	.025	.071	Z-3 0	1	9/32	1/2	15%	.229	.3!
Z-4	3/8	3/16	3/8	1	.026	.056		3/4	13/32		11/4	.239	.37
Z-111	1/2	1/4	1/4	7∕8	.027	.091	Z -102	3/4	3/8	1/2	13/4	.247	.38
Z -128	3∕8	13/64	3/8	1	.029	.062	+Z -215	7∕8	7/16	1/2	15/16	.251	.46
Z-177	3∕8	3/8	3/8	5%	.033	.136	Z -591	3/4	3/8	3/4	13/16	.251	.34
Z-531	1/2	1/4	5/16	7∕8	.034	.094	Z -165	3/4	7/16	5/16	21/2	.255	.5
Z-586	3/4	7/32	1/4	1	.041	7.2.0	Z -50	5∕8	1/2	5/8	15/16	.257	.4:
· Z -551	5%	1/4	5/16	7∕8	.043	.118	Z -582	11/2	13/32	3/8	11/8	.257	.6
Z -89	3/8	1/4	3/8	11/4	.044	.094	Z -72	1	9/32	5/8	19/16	.275	.3
Z-532	1/2	9/32	5/16	1	.044	.119	+Z-556	11/8	3/8	1/2	15/16	.277	.49
Z-112	1/2	1/4	3/8	1	.047	.106	+Z-4 08	7/8	7/16	7/16	111/16	.282	.5
Z-382	5/8	1/4	3/8	1	.059	.133	Z -145	7∕8	7/16	1/2	19/16	.298	.5
Z-360	5/8	5/16	5/16	1	.061	.169	+Z-409	7∕8	13/32		115/16		.52
Z-552	3/4	9/32	5/16	1	.066	.178	Z-58	5/8	5/8	5%	11/4	.305	.54
Z-1	1/2	1/4	1/2	11/8	.070	.122	Z-371	√8 , 7⁄8	3/8	5/8	19/16	.32	.59
Z-77 Z-88	1/2	1/4	1/2	11/8	.071	.126	+Z-376	1	7/16	7/16	111/16		.5
Z-129	3/8	3/8	7/16	13/16	.074		+Z-379 Z-67	1 5%	13/32		115/16	.353	.3
	1/2	17/64	1/2	11/8	.075	.131			1/2	11/16	11/16	.358	.6
Z-407 Z-251	3/4 1/2	1/4 5/16	3/8 7/16	13/16	.08	.171 .16	+Z-557 Z-103	1 1/4 7/8	7/16 7/16	1/2 9/16	15/16 111/16		.5
Z -553	7/8	5/-		1	.085	.237	+Z-372	7/8	7/16	5/8	19/16	.373	.5
-Z-533	/8 5/8	5/16	5/16 3/8	13/16	.085	.193	+Z-223	1 78		78 /2	11/2	.375	.6
Z-87	78 5%	5/16			.087	.153	Z-148	11/4	/2 5/-	5/8	19/16	.381	.5
Z-587	78 7 ₈	1/4	1/2	11/8	.089	.213	Z-140 Z-31	11/4	5/16 23/64		19/16	.395	.5
Z-380	7/8 7/8	1/4	5/16 3/8	11/8	.092	.20	Z-31 Z-104	7/8	7/16	78 5%	115/16		.6
Z-173	78 1	1/4	78 3/8	1 1/8	.092	.213	Z-104 Z-132	1 78	25/64	78 5%	115/16		.6
Z-100	5%	5/16	7/16	13/16	.101	.213	Z-132 Z-353	l i	7/16	78 5%	13/4	.478	.6
Z-94	78 1/2	5/16		19/16	.106	.189	Z-116	1/2	1/2	78 78	21/4	.493	.4
Z-3	72 3/4		7/16		.106	.183	Z-115 Z-125	11/8	3/8	5/8	115/16		.6
Z-130	3/4	17/64	1/2	11/8	.113	.196	Z-57	7/8	9/16	5%	111/16	.52	.76
Z-149	3/8	54-	5/8	19/16	114	.157	Z -581	11/8	9/16	11/16		.544	8.
Z-149 Z-554	7/8 7/8	5/16 5/16	78 3/8	13/16	.114	.157	Z-561 +Z-558	11/2	1/2	1/2	11/2	.563	1.0
Z-17					.121	.245	Z-139	11/4	3/8	5/8	115/16		.7
Z-361	1/2 3/4	7/16 34	1/2 34	11/8	.124	.292	±Z-369	11/8	7/16	78 11/16	134	.592	.7
Z-146	5/4 5/8	3/8 5/16	3/8 1/2	13/16 15/16	.125	.292	+Z-309	7/8 7/8	7/16	5/8	21/2	.598	.70
Z-304	78 5%	5/16			.129	.218	+Z-411	11/8		9/16	111/16		.9
Z-64	78 5%		1/2	11/2	.153	.196	Z-105	1 78	9/16 1/2	5/16	19/16	.606	.8
		3/4	5/8 1/-	19/16				_					.9
						.273	Z-122						.5
						.259	Z-123			ı			.8
Z-144 Z-153 Z-109	5/8 1 5/8	3/8 1/4 1/2	1	/2 /2 /16	/2 15/16 /2 11/4	/2 15/ ₁₆ .154 /2 11/ ₄ .156	6 15/6 154 273	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6 15/a 154 273 7126 1	6 15/a 154 273 7126 1 56	6 15/a 154 273 Z-126 1 56 56	6 15/6 154 273 Z-126 1 56 56 19/6	6 15/6 154 273 7.126 1 56 56 19/6 611

[•] preferred core sizes: These cores should be used wherever possible in designing new transformers. They are subject to maximum discount regardless of quantity ordered. See selling policy 46-700.

Pg 24

catalog number	dimen		inche			weight:		dimen	sions ir	inche	8	relative	
umber	strip width	build up	win- dow	win- dow	power handl'g	pounds	number	strip width	build up	win- dow	win- dow	power handl'g	pound
	D	E	width	length G	capac'y			D	E	width F	length G	capac'y	
mil s							4 mil s			-	G		
												Ι — —	
Z-163	11/4	3%	3/4	115/16		.755	Z -16	11/2	11/16		3	3.096	2.54
Z-119 Z-589	1 1 1/4	5/8 15/ ₃₂	5% 5%	13/4 115/16	.684	1.023 .94	+Z-542 Z-135	15/8	3/4 45/64	1	29/16 3	3.123 3.165	2.80 2.61
Z-150	7/8	7/16	7/8 7/8	21/4	.752	.705	4Z-418	17/8	3/4	3/4	31/2	3.693	3.71
-Z-410	11/8	7/16	5∕8	21/2	.77	.905	Z-122	11/4	3/4	15/16		3.736	2.91
Z-15	1	3/8 9/	13/16	13/4	.781	.65	+Z-563	21/2	13/16	13/16		4.12	4.51
Z-141 Z-154	1½ 1½	% %	11/ ₁₆ 3/4	1 13/16 17/8	.788 .791	1.048 .882	+Z-543 Z-592	13/4	13/16 3/4	1 1/8 2	27/8 3	4.597 5.64	3.64 2.82
Z-151	13/8	3/8	5/8	21/2	.808	.923	Z-332 Z-13	13/4	13/16		3	5.862	3.90
Z-160	11/4	3/8	3/4	25/16	.814	.824	+Z-564	21/2	15/16	15/16			5.80
-Z-370	11/8	1/2	3/4	115/16		.955	Z-136	13/4	53/64	13%	3	5,976	3,99
Z-106	1	1/2	5/8	25%	.822	.974	+Z-544	13/4	7∕8	15/16	31/2	7.032	4.61
Z-137 Z-68	1 11/8	13/ ₃₂ 5/8	13/16 5/8	13/4 115/ ₁₆	.844 .850	.615 1.219	+Z-545 +Z-546	21/4	1	13/8 11/2	35% 4	9.969 13.50	6.41 7.77
Z-595	1	7/16	7/8	21/4	.862	.803	4Z-547	21/2	11/6	15%	43/16	19.143	10.42
-Z-559	1%	9/16	9/16	111/16		1.39				, , ,			
Z-155	11/2	3/8	5/8	21/2	.88	1,008							
Z-121 Z-413	11/8 11/8	9/16 17/ ₃₂	¾ ₩	1 15/16 21/2	.918 .933	1.10 1.14							
Z-213	11/4	5/8	% %	115/16		1.35							
Z-140	11/8	9/16	13/16	115/16	.994	1.123							
Z-412	11/4	17/32	5/8	21/2	1.038	1.27							
Z-540 Z-107	1½ 1½	9/16 9/16	13/ ₁₆ 3/ ₄	21/8 25/16	1.09 1.096	1.16 1.205							
Z-6 0	7∕8	5/8	13/16	111/16		1.03							
Z-90	11/4	5∕8	5∕6	25/16	1.128	1.281							
Z-86	₹ 8	7/16	1	3	1.146	.87							
Z-10 -Z-415	1½ 1¼	5/8 5/8	1 %	1¾ 25%	1.23	1.28 1.60							
Z-534	13%	11/16			1.342	1.74							
Z-414	13%	5/8	5%	25%	1.41	1.76	ĺ						
Z-27	13/8	19/32	3/4	25/16	1.417	.997							
-Z-560 Z-354	1 1/ ₈ 1 1/ ₄	% 19∕16	5% 7∕8	1 15/16 25/16	1.42 1.422	2.02 1.38							
Z-541	11/4	5/16 5/8	7/8 7/8	25/16	1.579	1.57	VI.						
Z-23	7/8	9/16	11/8	27/8	1.593	1.166	ii ii						
Z-108	11/4	5/8	3/4	23/4	1.612	1.70							
Z-590 Z-142	11/2	19/32	3/4	21/2	1.67 1.83	1.80 1.67							
Z-84	11/4 1	₹8 29⁄ ₃₂	15/16 15/16	2½ 2¼	1.91	1.50							
Z-4 17	13%	11/16	11/16	3	1.953	2.184							
Z -561	2	11/16	11/16	21/16	1.953	2.53							
Z-7	11/2	5/8	1	21/8	1.993	1.859							
Z-134 Z-62	11/2	41/64 9/16	1 1½	2½ 2½	2.044	1.928 1.686	*						
Z-416	15%	11/16		3	2,307	2.585							
Z -214	11/2	3/4	3/4	215/16		2.30	No.						
Z -24	13%	9/16	11/8	27/8	2.501	1.833							
-Z-562	21/4	3/4	3/4	25/16	2.927	3.46							
+Z-4 19	11/2	3/4	l 3/ ₄	31/2	2.954	2.96	iii						

Perferred core sizes: These cores should be used wherever possible in designing new transformers. They are subject to maximum discount regardless of quantity ordered. See selling policy 46-700.

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catalog	dimen	sions ir	inche	s	relative	weight:	catalog		sions i	n inche	s	relative	weigh
number	strip width	build up	win- dow	win- dow	power handl'g	pounds	number	strip width	build up	win- dow	win- dow	power handl'g	pound
	D	E	width F	length G	capac'y		ĺ	D	E	width F	length G	capac'y	
12 mil			-				12 mil						
TA-21	1	1/2	1/2	11/2	.375	1.15	TA-53	5	37/8	35%	9	633.00	299.00
TA-2	3/8	3/4	11/4	21/2	.877	1.174	TA-28	4	5	41/4	81/2	723.00	350.00
TA-10	11/4	5√8	11/16	21/16	1.107	2.65		4	5	51/4	81/2	893.00	375.00
TA-9	11/4	5%	<i>7</i> ∕8	113/16		2.42	TA-38	6	71/4	35/8	9	1419.00	336.0
TA-11 TA-7	11/8	3/4	₹ 8	21/4	1.662 1.848	3.011 2.21	•						
TA-18	11/8	1/2 3/4	11/4	25/8	2.932	3.899							
TA-42	21/2	1 74	5%	115/16		8.56							
TA-19	11/2	3/4	11/4	21/2	3.515	4.679							
TA-37	21/4	1	5∕8	25%	3.68	8.84							
TA-20 TA-5	13/4	3⁄4 1	11/4	21/2	4.102 5.157	5.43 6.74							
TA-12	11/2	1	11/4	2½ 3	6.00	9.22	i i						
TA-4	13%	11/4	13%	3	7.092	9.15							
+TA-1	13/4	1	13/8	3	7.218	8.75							
TA-3	13/4	1	13/8	37/8	9.323	9.94							
TA-17	13/4	1	13/4	37/8	11.869	10.651							
TA-13 TA-41	15% 23/4	1 1/16	1½ 1%	5 1/16 43/16	12.341 16.50	10.98 19.20							
TA-16	1%	15%	21/2	23/8	18.092	19.805							
+TA-6	21/2	11/2	13%	37/8	19.979	23.75							
TA-23	15%	17/8	11/2	51/16	23.138	24.10							
TA-53	21/2	11/4	13/4	41/2	24.70	21.60							
TA-22 TA-651	21/2	11/8	13/8 17/8	3 1/8 4 1/8	24,978 28,90	32.00 26.50							
TA-34	3	117/32		51/16	29.10	33.00							
TA-27	25%	11/8	2	525/32		23,60							
TA-32	25/8	11/4	2	51/2	36.10	26.00							
TA-668		2	2	51/4	47.30	39.10							
TA-652	31/8	13/4	21/8	45%	53.70	43.90							
TA-667 TA-39	31/2	134 134	21/4	417/ ₃₂ 63/8	62,50 75,30	49,50 50,20							
TA-653	1 "	2	23/8	51/8	82.00	60.80							
TA-659		21/8	25%	51/6	107.00	74.90							
TA-654		21/4	25%	51/8	114.00	80.90							
TA-661		23/8	35/16	61/2	122.00	65.10							
TA-666	, · ·	21/2	25%	51/8	126.00	93.00							
TA-47	2	23/4	21/8	11	129.00	81.70							
TA-40 TA-655	2 1/8 4	21/4	23/4 31/8	7½ 6%	133.40 211.00	73.20 127.00	á						
TA-45	4	33%	23/4	53/4	214.00	158,00							
TA-665		2	4	12	240.00	80.60							
TA-658	- /-	21/2	313/16		246.00	118.00							
TA-35	31/2	31/2	21/2	81/2	260.00	167.60							
TA-663 TA-44	4	23/4	33/4	8	330,00	150.40							
TA-44 TA-664		3 2	33/4	8	360.00 360.00	168.00 120.70	Ĭ						
TA-650	- /-	27/8	5	131/2	437.00	126.00							
TA-656		33/4	33/4	8	450.00	225.20	4						
TA-662		47/16	41/4	83/4	618.00	283.00	1						

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catalog	dimen	sions i	n inche	8	relative	weight:	catalog	dimer	sions i	n inche	s	relative	weigh
number	strip width D	build up E	win- dow width F	win- dow length G	power handl'g capac'y	weight: pounds	number	strip width	build up E	win- dow width	win- dow length G	power handl'g capac'y	pound
4 mil se	eries	TH					4 mil s	eries	TH				
TH- 112	1/4	1/4	5/16	I	.02	.082	TH-51	1	1	13/16	11/4	1.015	3.10
TH-105	3/8	1/4	5/16	1	.029	.123	TH-5	11/4	13/16	13/16		1.03	2.62
+TH-97	3∕8	1/4	7/16	1	.041	.14	+ TH-58	11/4	56	11/16	21/16	1,107	2.34
TH-656	3/8	1/4	1/2	11/2	.069	.17	TH -107	11/8	5/8	7∕8	113/16	1.114	2.07
TH-43	3/8	3/8	1/2	11/8	.079	.246	TH -131	11/4	5∕8	3/4	2	1.17	2.28
+TH-69 +TH-96	1/2	3/8	7/16	1	.082	.309	TH-32	3/4	3/4	15/16	21/4	1.188	2.04
TH-49	3/4	5/16	7/16	11/8	.115	.39	TH-9	7∕8	7/16	11/4	21/2	1.195	1.42
TH-110	5/8 5/	3/8 3/	1/2	11/8	.131	.42	+TH-61	11/4	5∕8	<i>7</i> ⁄8	113/16		2.37
TH-52	5/8 3/	3/8 3/	1/2	11/4	.146	.432		1	7/16	11/2	2	1.312	1,61
1 H-32	3/4	3/8	1/2	11/8	.158	.56	TH-95	1	3⁄4	1	13/4	1.312	2.50
TH-25	1/2 1/2	3/8 1/2	5% 5%	15% 15/16	.191 .204	.435 .544	TH-42 TH-102	11/4	3/4	13/16	2	1.524	3,13
TH-55	5/8	3/8	34 34	13/16	.209	.495	TH-102	1 1/4 1	9/16	11/8	I 15/16	1.534	2.25
TH-83	3/4	1/2	1/2	11/8	.211	.736	TH-94	i	1/2 3/4	11/4	21/2	1.562	1.90
TH-74	3/4	3/8	1/2	19/16	.22	.675	TH-71	11/8	74 3/4	, , ,	1¾ 2¼	1.641	2.69
TH-41	3/4	1/2	5/8	13%	.321	.856	+TH-33	1 78	74 3/4	. 7⁄8	21/4	1.662 1.687	2.95 2.71
TH-116	1 1	1/2	1/2	13/8	.343	.645	TH-664	21/8	9/16	3/4	17/8	1.69	3.32
TH-56	3/4	1/2	5/8	19/16	.365	.911	+TH-6	3/4	3/4	11/4	21/2	1.76	2,29
TH-62	1	1/2	1/2	11/2	.375	1.176	TH-10	11/8	1/2	11/4	21/2	1.76	2.14
TH-89	1/2	1/2	3/4	2	.376	.725	TH-85	1	3/4	1	23%	1.781	2.87
TH-84	5/8	1/2	3/4	15%	.381	.814	TH -132	11/4	13/16	15/16	17/8	1.79	3.33
	1	1/2	1/2	19/16	.39	1.15	TH-46	11/4	7∕8	7/8	17/8	1.794	3.70
TH-87	3/4	1/2	11/16	15%	.419	.953	TH-16	7∕8	1/2	13/8	3	1.806	1.83
TH-48	7∕8	1/2	% │	15%	.445	1.05	TH-60	3/4	3/4	11/4	25%	1.848	2.37
TH-67	. 5/8	1/2	3/4	2	.47	.905	TH-655	2	9/16	7∕a	17/8	1.85	3.08
	1	1/2	5/8	19/16	.488	1.214	+TH-70	11/4	7∕8	15/16	17/8	1.921	3.79
	1_,	1/2	5/8	19/16	.488	1.21	TH-660	21/8	% ∤	3/4	115/16	1.93	3.63
TH-66	7/8	1/2	11/16	15%	.489	1,11	TH-59	11/2	3/4	3/4	25/16	1.951	4.00
TH-40	.34	3/4	7∕8	11/8	.554	1.553	TH-659	1	1	13/16	21/2	2.03	3.80
TH-65	1	1/2	11/16	15%	.559	1.27	TH-118	11/4	3/4	1	21/4	2.11	3.27
TH-31 TH-99	3/4 13/8	3/4	13/16	11/4	.571	1.52	TH-117	11/8	3/4	.78	3	2.217	3.22
	1 78	1/2	5/8	19/16	.671	1.62	+TH-91	78	7/8 2/	1	3	2,298	3.33
TH-19	5%	½ ¾	11/16	21/16	.695 .702	1.418 .825	TH-101 TH-652	13/8	3/4	1	21/4	2,319	3.60
	11/2	1/2	5/8	19/16	.732	1.762	TH-15	11/4	19/32	11/4	2½ 3	2.32	2.90
TH-53	3/4	21/4	7/16	1 716	.738	.28	+TH-35	1 1/8	1/2 3/4	13/8	21/2	2.322	2.62 3.05
TH-7	7/8	5/8	3/4	113/16	.742	1.50	TH-81	11/4	3/4	11/8	21/4	2,345	3.51
	1	1/2	3/4	2	.75	1.45	TH-667	1	74 7/8	1	23/4	2,40	3.32
TH-80	1	3/4	11/16	15%	.838	2.14	TH-665	i	7/8	11/8	21/2		3.16
TH-109	1	1/2	3/4	21/4	.843	1.474	TH-661	13%	1 8	13/16	23/8	2.46 2.64	4.64
TH-18	3/4	3/8	11/2	2	.844	.987	TH-666	1	7∕8	11/8	23/4	2.70	3.32
TH-662	1	3/4	3/4	11/2	.845	1.92	TH-13	11/4	9/16	13%	3	2.901	3.06
	11/8	5/8	5/8	115/16	.85	2.02	TH-133	13/6	5/8	11/8	3	2.90	3.46
TH-12	3/4	3/8	13/6	25/16	.892	1.212	+TH-4	11/4	3/4	11/4	21/2	2.932	3.81
TH-28	3/4	1	13/16	11/2	.913	2.201	+TH-92	1	1	i	3	3.00	4.51
	11/4	5/8	5/8	115/16	.945	2.25	TH-135	11/4	i	15/32	21/8	3.08	4.84
	11/8	5⁄8	13/16	111/16	.963	2.10	+TH-34	1	1	11/4	21/2	3.125	4.39
TH-20	7∕8	3/8	11/2	2	.984	1.16	TH-39	11/2	1	15/16	21/4	3.163	5.94
TH-27	3/4	3/4	7∕8	2	.986	.495 1.98	TH-106	11/2	5∕8	11/2	21/4	3.165	3.60
TH-136	11/4	9/16	11/16	21/16	.996	1.98	TH-14		5%	13%	3	3.219	3.284

[•] preferred core sizes: These cores should be used wherever possible in designing new transformers. They are subject to maximum discount regardless of quantity ordered. See selling policy 46-700.



catalog	dimen	sions ir	inche	R	relative	weight:
number	strip	build	win-	win-	power	pounds
	width	up	dow	dow	handl'g capac'y	
	_	-	width F	length	Capac y	
4 10	<u>.</u>	E	F	G		
4 mil s	eries	TH				
						, i
TH-121	13/8	3/4	11/4	21/2	3.23	4.09
+TH-2	11/2	1	1	21/4	3.375	5.90
TH-64	11/2	3/4	11/4	21/2	3.515	4.57
TH-72 TH-119	11/8	1	11/4	21/2	3.515	4.94
+TH-79	15%	_		21/4	3.66	6.30
TH-45	13/4 11/6	3/4 1½	11/4	21/4 2	3,692 3,798	5.34 5.625
+TH-36	11/4	1 /8	11/4	21/2	3,907	4,39
TH-73	11/4	3/4	11/8	41/16	4.285	4.81
TH-658	13/4	74 7/8	1	3	4.59	3.00
	- /4	/8	•		4.03	5.00
TH-654	13/4	i	11/2	13/4	4.60	6.65
TH-6 57	13/4	11/8	1	23/8	4.68	8.20
TH-103	11/2	1	11/4	21/2	4.687	6.37
TH-111	2	3/4	11/4	21/2	4.687	5.905
TH-113	15%	1	1	3	4.875	7.094
TH-104	13/4	1	11/4	21/2	5,47	7.44
TH-57	11/4	11/16	13/8	3	5.478	6,66
TH-82 +TH-68	1 2	1 1	15% 1	33/8 3	5.484	5.42
TH-100	11/2	1	13%	3	6.00 6.189	9.02
I E1-100	1/2	1	17/8	3	0,109	7.11
TH-1	11/4	1	21/4	21/4	6,329	6.87
TH-8	11/4	<i>7</i> ∕8	1	61/8	6.70	7,295
TH-668	13/4	1	11/8	31/2	6.89	9.00
TH- 115	13/4	1	1%	3	7.218	8.30
TH-23	11/4	5%	2	411/16	7,322	5.045
TH-108	,,,	1	19/16	21/2	7.322	8.29
TH-21	11/4	11/16	2	411/16	8.053	4.90
TH-663	11/2	1	11/2	4	9.00	8.41
TH-76	13%	13%	15%	3	9.219	12.69
TH-134	13%	1	13%	55/16	10.04	8,88
TH-650	15%	3/4	11/2	51/2	10.07	7.91
TH-22	11/4	₹ 76	2	411/16	10,257	7.05
TH-24	11/2	3/4	2	411/16	10,548	7.24
TH- 86	2	1	13%	37/8	10,656	10.78
TH-3	2	13%	1%	3	11,343	14.685
TH-54	2	1	2	3	12.00	11,57
+TH-75	1%	1	11/2	51/16	12,341	10,73
TH-38	2	11/2	1%	3	12,375	16.71
TH-63 TH-50	2	1	1%	43/16	13,611	12.00
T W-20	11/2	1	2	411/i6	14.064	10.12
TH -137	3	1	15%	33%	16.47	15.80
TH-37	21/4	15%	13%	31/2	17.594	22,20
TH -147	134	13%	13/4	43/8	18.38	21,50
TH-122	3	1	15%	41/8	20.13	44.40
TH-114	3	11/8	1%	43/16	22,966	23.15

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catalog	dimen	relative	weight:			
number	strip	build	win-	win-	power handl'g	pounds
	width	up	dow width	dow length	capac'y	
4 mil s	D eries	TZ	F	G		
	<u> </u>					
TZ-14	3%	1/4	7/16	1	.041	.14
TZ-25 TZ- 17	1/2 1/2	½ ¾	7/16 7/16	1 ½ 1	.061 .082	.198 .309
TZ-26	3/4	1/4	7/16	1	.082	.27
TZ-36 TZ-35	3/4 3/4	1/4 5/16	1/2 1/2	1% 1% 1%	.146 .184	.361 .468
TZ-11	34	3/6 3/6	1/2	19/16	.22	.675
TZ-21	1	1/2	1/2	19/16	.39	1.11
TZ-28 +TZ-20	3/4 3/4	½ ¾	11/16 3/4	15% 2	.419 .422	.923 .768
•	''			_		
TZ -23 TZ -13	1½ 5%	1/2 1/2	1/2 3/4	19/16 2	.44 .47	1,25 .905
TZ-9	1	1/2	5/4 5/8	19/16	.488	1,214
TZ-18	1	1/2	11/16	15%	.559	1.27
TZ-34 TZ-22	1 1/4	¾ ¾	3/4	3	.562 .564	.994 3.81
TZ-2 7	1	1/2	11/16	21/16	.709	1.418
+TZ-12 TZ-42	1	1/2	3/4 11/16	2	.75	1.45
TZ-15	1	3/4 1/2	7/16	15% 21/4	.838 .985	2,076 1,535
TZ-5	11/4	5%	7/	113/16	1 007	0.07
TZ-30	1	78 3⁄4	78 1	13/4	1.237	2,37 2,38
TZ-29	1	1/2	1	3	1.50	1.877
TZ-40 TZ-16	11/4	3/4 3/4	1	13/4 21/4	1.641	2,972 2,774
TZ-6	11/4	3/4	- 7∕8	21/4	1.847	2.95
TZ-33 TZ-8	1	5/8 2/	1	3	1.875	2,442
TZ-44	11/2	3/4 29/ ₃₂	34	3 21/4	2,25 2,292	3,14 4,683
TZ-32	11/4	%	1	3	2,343	3.053
TZ-19	1	3/4	11/4	21/2	2,345	3.05
TZ-38	1%	13/16	1	21/4	2,515	3.85
TZ-10 TZ-49	1 3⁄4	3/4 5/8	1 2	3½ 3	2,625 2,808	3.32 2.29
TZ-39	11/2	29/32	1	21/4	3.057	5.019
TZ-3 TZ-7	11/8	1	17/16	2	3.234	4.69
TZ-2	11/2	1	1 17/16	21/4 2	3,375 3,592	5.90 5.13
TZ-3 7	1%	11/6	3/4	3	4.113	7.807
TZ-45	15%	1	%	3	4.266	6.893
TZ-31	11/4	34	11/8	41/16	4,285	4.664
TZ-4 TZ-43	11/2	1	11/4	2½ 3	4.687 4.875	6,36 7,094
TZ-41	13%	1	11/4	3	5.157	6.344
TZ-1	11/2	1	11/2	4	9.00	9.115
TZ-47 TZ-48	15% 15%	1	11/2	5½6 5½6	12.341 15.423	10.40 13.613
-2-10	- 78	-74 1	172	2716 1	10.423	13.013

preferred core sizes: These cores should be used wherever possible in designing new transformers. They are subject to maximum discount regardless of quantity ordered. See selling policy 46-700.

ring type cores

core	dimension	: inches			gross	relative
size	strip width: D	build up: E	inside dia.: F	outside dia.: A	volume: cubic inches+	power handling capacity
202	1 1/	1 ,,	1/	34	.061	.006
202	1/4	½ 1/8	1/2	13/16	.067	.008
206	1/4	/ ₈	9/16	1	.073	.009
	1/4	1/8	5/8	7/8 15/16	.111	.012
207 203	1/4	3/16	9/16	1	.148	.012
	1/4	1/4	1/2	1 1	.135	.013
208	1/4	7/32	9/16	_	.161	.013
210	1/4	1/4	9/16	11/16	.173	.02
213	1/4	1/4	5/8	11/8	.139	.02
217	1/4	3/16	3/4	11/8		.023
211	3%	1/4	9/16	11/16	.24	.023
234	1/4	1/8	1	11/4	.11	.024
219	1/4	1/4	3/4	11/4	.198	.027
204	5/8	1/4	1/2	1	.368	.031
218	3/8	3/16	3/4	11/8	.209	.031
209	5/8	7/32	9/16	1	.336	.034
223	1/4	5/16	3/4	13/8	.26	.035
237	1/4	3/16	1	13%	.175	.037
220	3%	1/4	3/4	11/4	.295	.042
205	1/2	7/16	1/2	13/8	.645	.043
240	1/4	1/4	1	11/2	.247	.049
221	1/2	1/4	3/4	11/4	.393	.055
238	3√6	3/16	1	13%	.265	.056
512	1/4	1/4	11/8	15%	.272	.063
259	1/4	1/4	13/16	111/16	.285	.07
225	3/8	7/16	3/4	15%	.612	.072
239	1/2	3/16	1	13%	.351	.074
241	3/8	1/4	1	11/2	.369	.074
233	1/2	7/32	15/16	13%	.40	.076
214	1/2	1/2	5/8	15%	.884	.077
236	5∕6	5/32	1	15/16	.356	.077
261	1/4	1/4	11/4	13/4	.297	.077
224	- 5%	5/16	3/4	13%	.651	.086
230	3%	9/16	3/4	17/8	.87	.093
256	3∕8	1/4	11/8	15%	.406	.093
281	1/4	1/4	13/8	17/8	.322	.093
215	5∕8	1/2	5∕6	15%	1.11	.096
263	1/4	5/16	11/4	17/8	.383	.096
222	7∕8	1/4	3/4	11/4	.688	.097
226	1/2	7/16	3/4	15%	.817	.097
309	1/4	3/16	15%	2	.268	.097
242	1/2	1/4	1	11/2	.491	.098
235	11/8	1/8	1	11/4	.498	,111
244	3/8	3/8	1	13/4	.609	.111
292	1/4	1/4	11/2	2	.346	.112
216	3/4	1/2	5/8	1%	1.32	.115
227	5∕8	7/16	3/4	15%	1.02	.121
243	5∕8	1/4	1	11/2	.613	.123
395	1/4	1/8	23/8	25%	.243	.137
289	3∕6	1/4	17/16	115/16	.498	.152
262	1/2	1/4	11/4	13/4	.589	.153

⁺ Nominal core weight in pounds is obtained by multiplying the gross volume by the following factors: 12 mil—.262, 4 mil—.248, 2 mil—.246, 1 mil—.229.

ring type cores

core	dimension	s: inches			gross	relative
size	strip width: D	build up: E	inside dia.: F	outside dia.: A	volume: cubic inches+	power handling capacity
258	1/2	5/16	11/8	13/4	.704	.155
385	1/4	5/32	21/4	29/16	.295	.155
295	1/4	3∕8	11/2	21/4	.554	.167
265	3%	3%	11/4	2	.72	.173
245	5∕8	3/8	1	13/4	1.01	.184
249	1/2	15/32	1	115/16	1.09	.185
231	5/8	19/32	13/16	2	1.64	.192
228	1	7/16	3/4	15%	1.63	.194
310	1/2	3/16	15%	2	.535	.195
250	1/2	1/2	1	2	1.18	.196
506	1	11/32	7/8	19/16	1.31	.207
284	3∕8	3/8	13%	21/B	.775	.21
246	3/4	3%	1	13/4	1.21	.221
291	1	1/8	11/2	13/4	.638	.221
293	1/2	1/4	11/2	2	.687	.221
322	1/4	3/8	13/4	21/2	.628	.226
330	3/8	7/32	17/8	25/16	.539	.226
266	1/2	3%	11/4	2	.96	.231
232	3/4	19/32	13/16	1 2	1.97	.231
283	1/2	5/16	13%	2	.827	.232
379	3%	3/16	21/16	27/16	.502	.237
264	5%	5/16	11/4	17/8	.957	.24
306	1/2	1/4	19/16	21/16	.712	.24
523	11/4	1/4	1	11/2	1.23	.246
296	3/8	3/8	11/2	21/4	.831	.249
247	7/8	3%	1	13/4	1.42	.258
248	3/4	7/16	1	17/8	1.49	.258
308	1 1	1/8	15%	17/8	.687	.259
311	1/2	1/4	15%	21/8	.736	.259
267	5%	3%	11/4	2	1,19	.287
255	11/4	15/64	11/8	119/32	1.25	.291
279	5∕8	11/32	15/16	2	1.12	.291
312	3%	3/8	15%	23%	.886	.292
268	1/2	1/2	11/4	21/4	1.37	.307
257	11/4	1/4	11/8	15%	1.35	.311
229	15%	7/16	3/4	15%	2.65	.315
331	1/2	15/64	17/8	211/32	.775	.323
260	11/4	7/32	11/4	111/16	1.27	.336
324	3/8	3/8	13/4	21/2	.941	.339
294	%	5/16	11/2	21/8	1,11	.345
328	1/2	1/4	17/8	23%	.835	.346
332	1/2	1/4	17/B	23/8	.835	.346
426	3%	3/16	29/16	215/16	.613	.366
353	1/4	15/32	2	215/16	.908	.368
341	1/2	17/64	129/32	27/16	.908	.379
297	1/2	7/16	11/2	23/8	1.33	.387
251	1 1 1	1/2	1 1 2	2	2.36	.393
344	1/2	1/4	2	21/2	.884	.393
282	l 1'*	9/32	13%	115/16	1.46	.417
252	3/4	3/4	1	21/2	3.10	.442
	74	74	1 1	4/2	1 3.10	.442

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ring type cores

ring typ	e cores					
core	dimension	s: inches			gross	relative
Bize	strip width: D	build up: E	inside dia.: F	outside dia.: A	volume: cubic inches+	power handling capacity
299 350	1/2 3/8	1/2 3/8	11/2	21/2 23/4	1.57	.442
307			19/16	25/16	1.42	.448
	5/8	3/8			1.19	.453
334 329	3%	7/16	17/8	23/4	1.19	.453
269	7∕8	3/16	17/8	21/4	2.06	.456
403	1 3/4	1/2	11/4	21/4	.766	.462
404	1 -	3/32	21/2	3	.812	.462
	3/8	1/4	21/2	1 -	1.67	.485
298 319	5% 1/4	7/16 15/16	1½ 15%	23/8 31/2	1.89	.488
300	5%	1/2	11/2	21/2	1.97	.553
354	3/8	15/32	2	215/16	1.36	.553
338	1/4	13/16	17/8	31/2	1.71	.561
343	1 1	3/16	2	23/8	1.29	.591
253	7∕8	7/8	1	23/4	4.51	.602
405	1/2	1/4	21/2	3	1.08	.613
270	1 1	1/2	11/4	21/4	2.75	.614
285	l i	7/16	13%	21/4	2.49	,65
301	3/4	1/2	11/2	21/2	2.36	.663
313	7/8	3/8	1%	23/8	2.06	.68
345	7∕8	1/4	2	21/2	1.55	.688
335	1/2	1/2	17/8	27/8	1.86	.69
317	1/2	11/16	15/8	3	2.50	.714
320	3/8	15/16	15%	31/2	2.83	.73
355	1/2	15/32	2	215/16	1.82	.738
287	1	1/2	13/8	23/8	2.95	.743
323	11/4	1/4	13/4	21/4	1.97	.753
406	5∕8	1/4	21/2	3	1.35	.766
336	1/2	9/16	17/8	3	2.15	.776
254	1	1	1	1	6.28	.785
346 356	1	1/4	2 2	2½ 3	1.77 1.96	.785 .785
370	1/2	1 1/2	2	4	2.36	.785
351	1/4 5/8	13/32	2	213/16	1.92	.798
384	15%		21/4	21/2	1.51	.807
302	1 178	½ ½	11/2	21/2	3.14	.884
453	1/4	1/2	3	4	1.38	.884
325	7/4 7/8	7/16	13/4	25%	2.63	.921
408	78 5/8	5/16	21/2	31/8	1.72	.957
321	1/2	15/16	15/8	31/2	3.78	.973
286	11/2	7/16	13/8	21/4	3.74	.975
520	2	5/32	2	25/16	2.11	.98
348	1	5/16	2	25/8	2.27	.98
357	5%	1/2	2	3	2.46	.983
333	11/2	1/4	17/8	23%	2.50	1.04
276	11/4	23/32	11/4	211/16	5.56	1.10
303	1	5∕8	11/2	23/4	4.17	1.10
349	11/8	5/16	2	25%	2.55	1.10
342	3/8	1 1/32	115/16	4	3.61	1.14
278	11/4	3/4	11/4	23/4	5.89	1.15

⁺ Nominal core weight in pounds is obtained by multiplying the gross volume by the following factors: 12 mil—.262, 4 mil—.248, 2 mil—.246, 1 mil—.229.

ring type cores

core	dimension	: inches			gross	relative
size	strip width: D	build up: E	inside dia.: F	outside dia.: A	volume: cubic inches+	power handling capacity
358 371 430 327 362 407 410 339 363 433	34 96 98 1 56 1 1/2 9/16 56	1/2 1 1/4 1/2 5/8 1/4 1/2 13/16 41/64 3/6	2 2 25% 13/4 2 21/2 21/2 21/8	3 4 3½ 2¾ 3¼ 3 3½ 3½ 3½ 3½ 39⁄32	2.95 3.53 1.98 3.53 3.22 2.16 2.36 3.85 3.33 2.21	1.18 1.19 1.20 1.23 1.23 1.23 1.26 1.26
352 428 304 452 364 434 505 288 450 382	1 5% 1 ½2 5% ½2 1 1¼4 5%	13/32 13/32 3/4 3/6 11/16 1/2 1/2 3/4 11/32 1/2	2 29/16 11/2 3 2 25/8 11/8 13/8 23/16	213/16 33/26 3 33/4 33/26 35/26 27/8 27/8 33/16	3.07 2.37 5.30 1.99 3.63 2.46 3.73 6.26 2.17 3.17	1.28 1.31 1.33 1.35 1.35 1.35 1.38 1.39 1.40
314 439 315 347 359 372 425 402 409 290	1 1/6 2 2 2 1 1/2 21/2 3/4 1 21/4	%	15/8 23/4 15/8 2 2 2 2 29/16 213/3/2 21/2 17/16	23/8 3 23/8 21/2 3 4 213/16 313/32 37/32 27/16	4.42 2.26 4.71 3.54 3.93 4.71 2.64 3.42 3.23 6.85	1.46 1.49 1.56 1.57 1.57 1.57 1.61 1.71 1.76 1.83
411 275 445 360 386 429 280 412 378 396	3/4 21/4 2 11/4 2 5/8 21/2 7/8 1/2	1/2 11/16 5/32 1/2 1/4 5/6 5/6 1/2 13/6	2½ 1¼ 2¹³/6 2 2¼ 2¹9⁄2 15⁄16 2½ 2	3½ 2½ 3½ 3 2¾ 327/32 29/16 3½ 4¾ 3¾	3.53 9.42 2.91 4.91 3.93 3.95 9.51 4.13 7.30 4.52	1.84 1.90 1.94 1.96 1.99 2.07 2.11 2.15 2.16 2.22
447 468 316 365 373 431 326 474 381 413	5/8 11/4 2 1 3/4 13/4 2 1 3/4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	19/ ₃₂ 1/4 9/16 3/4 1 1 1/4 1/2 1/4 59/64	213/16 31/16 15/6 2 2 25/6 13/4 31/2 21/6	4 39/16 23/4 31/2 4 31/8 23/4 4 331/32	3.97 3.26 7.72 6.48 7.07 3.96 7.07 2.95 6.62 4.71	2.30 2.31 2.33 2.36 2.36 2.37 2.41 2.41 2.45 2.45

⁺ Nominal core weight in pounds is obtained by multiplying the gross volume by the following factors: 12 mil—.262, 4 mil—.248, 2 mil—.246, 1 mil—.229.

ring type cores

ring type cores							
core	dimensions	: inches			gross	relative	
size	strip	build	inside	outside	volume:	power	
	width: D	up: E	dia.: F	dia.: A	cubic inches+	handling capacity	
				!	Inches.	Capacity	
=10	1.00	2,	12/	31/4	8.10	2.48	
519	13%	3/4	13/4		5.65	2.49	
387	1	5/8	21/4	31/2		2.45	
380	2	3%	21/8	27/8	5.89		
432	2	1/4	25/8	31/8	4.52	2.71	
374	7∕8	1	2	4	8.25	2.75	
486	7 ⁄8	1/4	4	41/2	2.92	2.75	
440	1	1/2	23/4	33/4	5.10	2.97	
435	11/8	1/2	25%	35%	5.53	3.05	
500	1/2	5/16	5	5%	2.60	3.06	
415	1	5%	21/2	33⁄4	6.14	3.07	
361	2	1/2	2	3	7.85	3.14	
375	1	1	2	4	9.43	3.14	
398	11/B	21/32	23%	311/16	7.03	3.27	
318	13/4	59/64	15%	315/32	12,90	3.35	
366	11/2	3/4	2	31/2	9.72	3.53	
454	1 2	1/2	3	4	5,50	3.53	
418	l i	3/4	21/2	4	7.66	3.68	
424		11/2	21/2	51/2	9.43	3.68	
469	2/2		31/16	39/16	5.20	3.68	
469 448	_	1/4	213/16	4	6,36	3.69	
448	1	19/32	219/16	'	0,30	3.03	
388	11/2	5%	21/4	31/2	8.47	3.73	
478	5%	5%	31/2	43/4	5.07	3.76	
416	11/4	5%	21/2	33/4	7.67	3,83	
305	2	11/8	11/2	33/4	18.60	3,98	
518	11/2	11/2	11/2	41/2	21,20	3.98	
421	i''	7/8	21/2	41/4	9.28	4.30	
376	13%	1 1 8	2	4	13.00	4.32	
391	11/8	li	21/4	41/4	11.50	4.47	
417	11/2	5%	21/2	33/4	9.21	4.61	
367	2	3/4	2 2	31/2	12,90	4.71	
301	*	74	, *	372	12,50	1	
377	11/2	1	2	4	14.10	4.71	
401	1	11/16	23/8	41/2	11.50	4.71	
337	21/2	11/16	17/8	31/4	13.80	4.75	
476	1	1/2	31/2	41/2	6.28	4.81	
427	21/2	3∕8	29/16	35/16	8.66	4.84	
515	13%	1/2	3	4	7.56	4.86	
389	2	5%	21/4	31/2	11.30	4.97	
436	11/4	3/4	25%	41/8	9.95	5.08	
446	17/8	7/16	213/16	311/16	8.38	5.10	
390	11/2	7/8	21/4	4	12.90	5.22	
368	2	27/32	2	311/16	15.10	5.30	
457	l ī	34	3	41/2	8.84	5.30	
465	1 1/2	11/2	3	6 -	10.60	5.301	
477	11/8	1/2	31/2	41/2	7.08	5.41	
479	3/4	3/4	31/2	5	7.52	5.42	
414	21/4	1/2	21/2	31/2	10.60	5.52	
419	11/2	3/4	21/2	4	11.50	5.52	
400	11/4	1 1 24	23%	436	13.20	5.54	
397	21/4	9/16	23/8	31/2	11.70	5.61	
487	1	1/2	4	5	7.07	6,28	
401		/2		, -		1 3/100	

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ring type cores

ring typ	e cores					
core	dimension	s: inches			gross	relative
size			1	1	volume:	power
	strip width: D	build up: E	inside dia.: F	outside dia.: A	cubic	handling
	wida. D	up. L	ula I	ula.: A	inches+	capacity
				T		
451	1/2	115/16	27/8	63/4	14.60	6.29
383	2	27/32	23/16	37/8	16.10	6.35
340	21/2	15/16	1 1/8	33/4	20.70	6.48
466	1/2	127/32	3	611/16	14.00	6.52
399	21/4	21/32	23/8	311/16	14.10	6.54
392	11/2	11/8	21/4	41/2	17.90	6.71
393	1	111/16	21/4	55/8	20.90	6.71
394	2	27/32	29/32	331/32	16.90	6.90
422	11/8	11/4	21/2	5	16,60	6.90
455	2	1/2	3	4	11.00	7.07
459	1	1	3	5	12.60	7.07
480	l i	3/4	31/2	5	10.00	7.22
420	2	3/4	21/2	4	15.30	7.36
475	21/2	5/16	31/2	41/8	9.34	7.50
369	213/16	15/16	2	37/8	24,40	8.29
456	13/4		3			
470		11/16		43/8	13.90	8.51
458	13/8	13/16	31/8	43/4	13.80	8.57
	11/2	7/8	3	43/4	16.00	9.28
510	1	1	31/2	51/2	14.10	9.62
461	11/4	11/8	3	51/4	18.20	9.94
491	1	13/16	4	55%	12.30	10.20
444	1	13/4	23/4	61/4	24.70	10.40
509	2	3/4	3	41/2	17.70	10.60
460	11/2	1	3	5	18.90	10.60
437	2	1	25%	45%	22.80	10.80
463	11/4	11/4	3	51/2	20.90	11.10
449	13%	15/16	213/16	57/16	23.40	11.20
488	11/4	3/4	4	51/2	14.00	11.80
441	2	1	23/4	43/4	23.60	11.90
423	2	11/4	21/2	5	29.50	12.30
471	2	3/4	31/4	43/4	18.80	12.50
462	11/2	13/16	3 74	53%	23.40	12.60
492	1	1 1916	4	6	15.70	12.60
489	11/5	3/4	4	51/2	16.80	14.10
438	213/16	11/16	25%	43/4	34.60	16.20
484	23/4		37/8	47/8	18.90	16.20
442	2 74	1½ 1¾	23/4	51/2	35.60	16.30
490	13/4	3/4	4	51/2	19.60	16.50
508	2	7/4 7/8	31/2	51/4	24.10	16.80
464	2	, , -	3	1 / -		
404	2	11/4	3	51/2	33.40	17.70
443	21/4	13%	23/4	51/2	40.10	18.30
472	21/4	1	31/4	51/4	30.00	18.70
493	11/2	1	4	6	23.60	18.90
495	11/4	11/4	4	61/2	25.80	19.60
473	21/2	1	31/4	51/4	33.40	20.70
498	13/8	11/16	45/16	67/16	24.60	21.30
483	17/8	32/1	33⁄4	513/16	29.00	21.40
467	13/4	17/8	3	63/4	50.20	23.20
481	21/2	1	31/2	51/2	35.30	24.10
502	1	1	5%	7%	20.80	24.80

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ring type cores

core	dimension	s: inches	gross	relative		
size	strip width: D	build up: E	inside dia.: F	outside dia.: A	volume: cubic inches+	power handling capacity
494	2	1	4	6	31.40	25.10
507	2	11/8	41/4	61/2	37.90	31.90
496	2	11/2	4	7	51.80	37.70
497	21/2	11/2	4	7	64.80	47.10
499	13%	21/8	47/8	91/8	64.30	54.50
485	4	13%	37/8	65%	90.70	64.90
501	2	13/4	5	81/2	74.20	68.70
503	21/4	15/16	55%	81/4	64.30	73.30
482	3	3	31/2	91/2	184.00	86.60

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