*Dear Editor,*

*We would like to thank the referees for reviewing our updated paper and producing second reports.*

*We have considered all comments, and we have applied several changes to the original version of the paper to address the issues raised. Detailed responses to all the comments can be found below. For ease of review, the original question is written in black font, the author response is written in blue font, and any modification to the paper draft is written in bolded green font.*

*We are at your disposal for any further clarifications and/or additional information.*

*Sincerely,*

*Artur, Si, Cristian, …etc*

Reviewer #2: Please consider reviwing the following remarks:

P(age)#L(ine)#

Abstract:  
The efficiency and timing resolution before irradiation were found to be 100% and 30-40 ps, respectively. A "no-response" area between pads ………..  
The sensors are divided in 'efficient' part, and no response area. This leads to 100% efficiency but it is misleading if the concept is not clarified (as the geometrical efficiency is not this value).

To distinguish efficiency from the no response area, we will use the term “sensitive” area. We have changed the text to:

**“The signal detection efficiency and timing resolution in the sensitive areas”**

P2L58 … pile-up contamination ….  
I would consider a different adjective…………..

We have changed the text to :

**“in order to overcome the event reconstruction challenges posed by  the high rate of concurrent collisions per beam crossing.”**

P3L67 …. We also compare the uniformity of 50 and 80 m LGAD sensors, as well as the HPK and CNM sensors irradiated to an equivalent neutron flux of 6 1014 n/cm2. Detailed measurements of irradiated HPK sensors were presented in Ref.  
of 50 and 80 m thick LGAD sensors ……  
…. As well as…   
Here you put in the same sentence two different comparison (thickness and manufacturer) which I found confusing.

We have separated the sentences as follows:

**“We  also compare the uniformity of 50 and 80 μm LGAD sensors. Uniformity and and time  resolution of the HPK and CNM sensors irradiated to an equivalent neutron fluence of  6 × 1014 n/cm2 are also presented.”**

. an equivalent neutron flux of 6 1014 n/cm2…   
The unit of flux are n/cm2/s. This is integrated flux.

We have changed “flux” to “fluence”:

**“…equivalent neutron fluence…”**

P2L102 The primary beam (bunched at 53 MHz) consists 102 of high energy protons (120 GeV) at variable intensities between 1 and 300 kHz.  
Incomprehensible. Thought Hz is frequency, not intensity.

We have changed the text to:

**“The beam is resonantly extracted in a slow spill for each Main Injector cycle delivering a single 4.2 sec long spill per minute. The primary beam (bunched at 53 MHz) consists of 120~GeV protons. All measurements presented in this paper were taken with the primary beam particles.”**

Figure 4: Photographs of the HPK 50D-PIX 22 array sensor (top left), the CNM-W9HG11 22 array sensor (top right), the 50D-GR single sensor (bottom left), and the CNM W11LGA35 single sensor (bottom right) are shown.  
….. , the 50D-GR single sensor…….                     
……., the HPK 50D-GR single sensor …………

We have changed the text to:

**“Photographs of the HPK 50D-PIX 2 × 2 array sensor (top left), the CNM W9HG11 2 × 2 array sensor (top right), the HPK 50D-GR single sensor (bottom left), and the CNM W11LGA35 single sensor (bottom right) are shown.  ”**

P6L129 ……. with a different p+ dose of the gain layer to study the optimal parameters of the charge multiplication mechanism.  
I do not think you are studying the optimal parameters for charge multiplication (could e.g. maximum gain….), but rather the parameters functional to time resolution.

We have modified the sentence to reflect the optimization for fast timing detectors:

**“Four gain splits, identified with the letters A (lowest gain) to D (highest gain), were produced identical in the mask design but with a different $p^+$ dose of the gain layer to study the optimal parameters for fast timing detectors.”**

P7L161 …. about 130 W per channel.   
I hope it is much less!

We have corrected the typo to 130 mW per channel.

P8L184 … The above choices of timestamp reconstruction algorithms used are motivated by the result of a dedicated study of different timestamp reconstruction algorithms for each of the three readout boards.  
The choice of the above timestamp reconstruction algorithms was motivated by the result of a dedicated study of various algorithms for each of the three readout boards.

Corrected according to reviewer suggestion.

P9L209 … timing resolution …  
… time resolution …..

Corrected according to reviewer suggestion.

P9L212 …. is the same for all runs and requires that  the signal amplitude is between 160 mV and 320 mV….  
This information is redundant as the mip signal, or a signal calibration, is not provided.

We have changed the sentence to say:

**“The signal selection in the Photek MCP-PMT is the same for all runs and requires that the signal is consistent with a MIP corresponding to amplitude values in the range between 160 mV and 320 mV.”**

P9L213 … The signal selection for LGAD boards was optimized for each board individually, by selecting the MIP signal peak fitted with a Landau function.   
What does this mean? The signal selection here is not distinguishing real events from noise?

We selected signal events by requiring that the pulse amplitude is above noise. The noise for each board was slightly different and therefore the amplitude cut was adjusted for that. We have changed the text as follows:

**“Signal events in LGAD sensors  are selected such that they are above the noise levels listed for each board in Sec. 4.  ”**

P10L237  
Fig. 5 Can explain the error bars? Why they are bigger for the CNM sensor, and bigger in the y-coordinate, and increasing with it?

The dataset accumulated with the HPK 50D-PIX sensor was the largest among various sensors we tested in these measurements, hence the plots with this sensor have the smallest statistical uncertainties. The measurements presented in the upper and lower panels of this figure were obtained from different datasets and therefore do not have the same statistical uncertainties. The reason that the error bars grow with increasing Y-coordinate is due to the fact that beam is more centered at low Y-coordinate, and hence there are more events at lower values of the Y-coordinate. We have added the following sentence in the end of last paragraph in Section 6, before Section 6.1:

**“Measurements presented for various sensors were obtained from different datasets and therefore the statistical precision is not always the same. The reason that in some measurements the error bars are not the same across either X- or Y-coordinate is due to the fact that the beam does not uniformly illuminate the whole sensor area, and hence the number of events is not the same across sensor surface.”**

P10L239 … impacts its timing ….  
… impacts on its timing ….

Corrected according to reviewer suggestion.

P10L241 …. Is fit to a Landau …..  
…. Is fitted to a Landau …..

Corrected according to reviewer suggestion.

P11 Figure caption.  
Figure 7: t measurement across the X- and Y-axes of the HPK 50D-PIX sensor mounted on the FNAL board. The scans of pixels 1 and 2 along the X-axis, and pixels 1 and 3 along the Y-axis are shown. The pixel numberng scheme is defined in Fig. 4.  
Why the caption does not mentions the CNM sensor?

We have added the CNM sensor to the caption as follows:

**“Δt measurement across the X- and Y-axes of the HPK 50D-PIX sensor mounted on the FNAL board, and the CNM W9HG11 sensor mounted on the UCSC board. “**

P10L249 … A possible explanation for this effect is a small difference in the rise time of the pulses that originate from the passage of particles in the metallized and non-metallized areas……  
Too much hand-waving. Is the rise time difference well identified? I would no try to give explanation of the effect before verification.

The rise time did not show a statistically significant difference to explain this effect. We have modified the text following your suggestion:

**“This effect cannot be attributed to the algorithm used to time-stamp the events, since the same behavior is observed with the CFD and CDT algorithms. Furthermore, the same behavior is observed on all HPK sensor varieties mounted on KU board, as presented in Sec. 6.3. Further studies are needed to understand the effect.”**

P11L254 The results for the CNM sensor also show hints of this behavior, though the larger statistical uncertainties make it less significant.  
They seem to go in the other direction (concerning the effect of metal), or not?

After further discussion among the authors, we have confirmed that there is no metalized area in the CNM sensor, and we believe that the feature alluded to in the original text is unconvincing. Therefore we have changed the sentence to:

**“The CNM sensor does not contain metalized areas on its surface and we do not observe the same effect.”**

P11L270 … We define the width of the \no-response" area as the distance between the half-maxima of the two  fitted S-curves, as shown in Fig. 9.   
This definition contradicts the statement before that the sensors are 100% efficient (excluding the interdetector region). The area between the 100% to 50% efficient is obviously not fully efficient. But with the current definition, it is part of the active sensor area. This must be corrected.  
Besides, if a definition of the inter-detector region should be chosen, the 0.5 value is not good, as it should be chosen a value high enough to be used in experimental condition (90%, 95%, ???).

Indeed, at 50% efficiency, the measurement would not be very powerful. We have changed all relevant plots to show the distance between the two sensors at the 90% efficiency level.

Fig. 9 Some of the not efficiency points (0%) for both ch1 and 2 are significantly higher than 0. What is the noise hit occupancy for these sensors?

We know that in a small fraction of events (<1%) the reconstructed position of the track is wrong. The points outside the sensor area in these plots actually had hit the sensor. These events are not a result of noise in the LGAD sensor.

We have added the following sentence in the text to clarify this point:

**“Data points outside the sensor area in Figs. 9, 10 actually  had hit the sensor active area, but the coordinate of the track is incorrectly assigned, due to a small  probability (< 1%) to misreconstruct the position of the track.”**

Fig. 10: same comments as above.

Please see the answer above.

P18L342 …. The distribution of the  t between the reference timestamp and the timestamp from the HPK 50D-PIX sensor is shown in Fig. 16. We observe no significant changes in the behavior of the  t as the temperature varies.  
It does look like there is a shift in the x-direction of about 1mm from high to low temperatures? Is it possible?

Indeed there is a very small shift in the sensor outline. To avoid confusing the reader, we have modified the plots to only show the points for which all three temperature conditions have data points.

Figure 16 and 17: please use the same markers in the two figures for corresponding temperatures.

We have modified the plots such that the colors and markers are consistent between the plots.

P21L367 .. The distribution on the right of Fig. 18 shows that the amplitude under the aluminum (periphery) is about 2.5 times larger than that without aluminum (center).  
How does it compare with the pre-irradiation spectra?

Unfortunately, we did not have unirradiated sensors for the measurements presented in this paper. However, measurements were presented on page 12 of Nicolo Cartiglia’s talk at RD50 meeting in Krakow:

<https://indico.cern.ch/event/637212/contributions/2608659/attachments/1471224/2276633/Cartiglia_BeamTest_FNAL.pdf>

As can be seen in the presentation above, a similar effect, but of much lesser magnitude (~10%) is observed in the pre-irradiated device.   
  
  
  
Reviewer #3: Dear authors, dear editor,  
The manuscript addresses the timing resolution of LGAD sensors measured in beam tests. These detectors are foreseen for both CMS and ATLAS after phase II upgrade for precise timing measurements and are currently very intensively studied. The presented work certainly importantly adds to understanding of their operation and their performance (different manufacturers, electronics, geometries analysed). The amount of data and the work done is impressive.   
However, I have several issues that need to be addressed before the paper can be recommended for publication. They are listed below.   
  
With best regards,  
  
Your reviewer  
  
MA - major remark that needs to be addressed  
MI - minor remark that needs to be addressed  
OP - optional remark or comment from reviewer  
  
Abstract:    
"…factor of 2.5 when" ->  at lower voltages should be less so "… of up to a factor of 2.5 …"

Corrected according to reviewer suggestion.

Experimental setup  
L88: MI - "electronic time resolution"  it is not clear to me what you mean by that. Please make it clearer.

The definition of the electronic time resolution has been added to Sec 2, third paragraph as follows:

**“One of the main parameters of  DAQ system for precise time measurements is the “electronic time resolution”, defined as  the measured time jitter between two signals that are split from the same source. These  two signals are used as “start” and “stop” signals to electronic system measuring the  time interval between them. The electronic time resolution of the CAEN V1742 digitizer  was measured to be less than 4 ps, and thus, its impact on the timing measurements  presented in these studies can be neglected.”**

L102: MI - "at variable intensities between 1 and 300 kHz" - it is not clear what the intensity refers to.

This sentence has been changed to improve clarity, also at the request of the other reviewer. It now reads:

**“The beam is resonantly extracted in a slow spill for each Main Injector cycle delivering a single 4.2 sec long spill per minute. The primary beam (bunched at 53 MHz) consists of 120~GeV protons. All measurements presented in this paper were taken with the primary beam particles.”**

L109-L114 : MI - the  detailed description of trigger board is in a way to detailed as not all terms can be explained in enough details such as "front end board". I would prefer a simpler statement. It is not crucial for the remainder of the paper. In this context I think Fig.3 isn't needed, particularly for an already lengthy paper.

We have removed the text and figure that details the trigger board from the new draft, as suggested by the reviewer.

LGAD Sensor Properties  
MA: Table 1 is not referenced in the text. It is vital to list also the information about the gain of the detectors at given voltage, current, and break down voltage. It would help the reader to understand manuscript better. There has been no mentioning of the difference between the dose of W9HG11 and W11LGA35 from CNM. Are these two different only in geometry or also in dose?

We have added a reference to Table 1 with further information on the detectors:

**“A brief summary of the sensors dimensions and capacitances is presented in Tab. 1”**

We added a table summarizing the bias voltages and corresponding gains that the sensors were operated at during the test beam campaign. These are listed in Table 2 of the new paper draft, and the following text was added in Sec. 3:

**“The list of sensors studied in this article, as well as the temperature and the sensor bias voltage used during their operation are listed in Tab 2.”**  
  
L131 : MI - Are they also identical in thermal budget ?

It was not completely clear to us what the question means exactly. We can answer the following:

* These sensors do behave in the same way with respect of changes in temperature
* These sensors do generate the same amount of leakage current at the same gain

Readout Electronics  
L161 : MI - "power consumption of the board is about 130 W …" . is  130 W a typo? This is hard to believe.

We have fixed this typo. The power consumption is 130 mW.

Timestamp Reconstruction  
L176 : MI -  "decay time" is not an appropriate wording, maybe "fall time"…

We have modified the sentence to say:

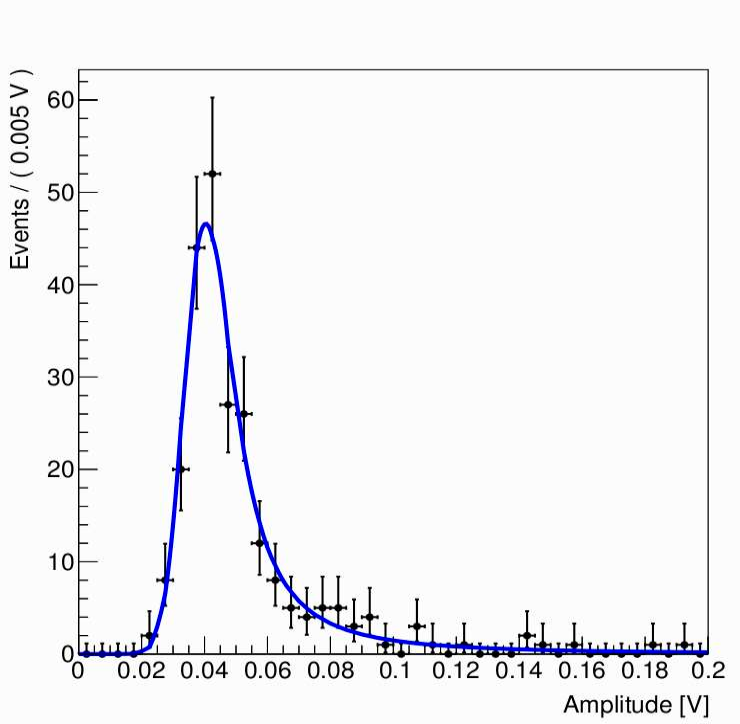
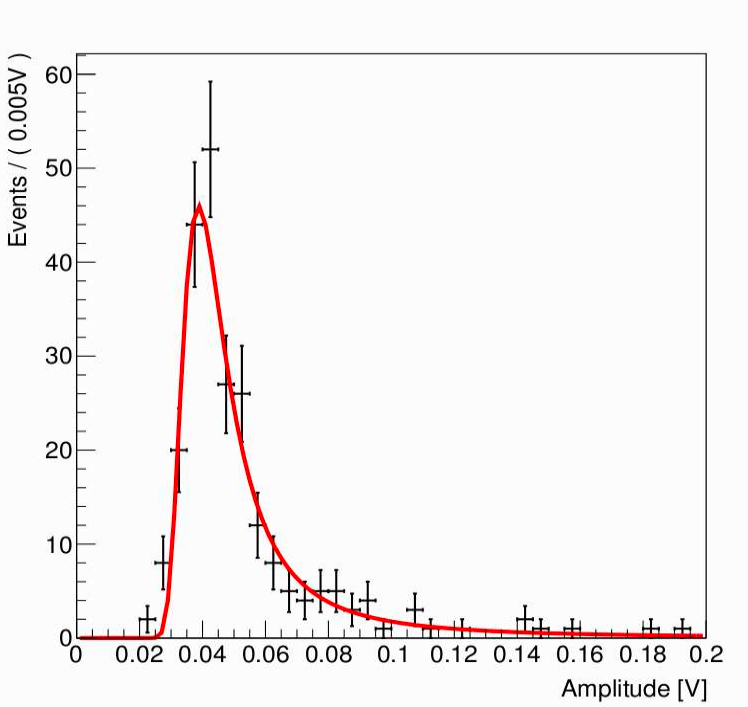
**“For the KU board, whose pulses take much longer to fall to the baseline, the timestamp is obtained by performing a linear fit to the
rising edge of the pulse,…”**

L194 : MI - "… by a linear function…" -> "… by linear dependence of timestamp on pulse height"

We have changed the text according to reviewer’s suggestion.

Sensor Studies and Analysis  
L215 : MA  - The Landau function doesn't accurately describe the data. The spectra are broadened by noise and also by fluctuations in multiplication/gain. Therefore convolution of Gaus+Landau would be more accurate. Can you comment on uncertainty arising from this in your analysis?

Following your suggestion, we have repeated the fit using the convolution of a landau and a Gaussian. Indeed we find that the Landau convoluted with a Gaussian yields a slightly improved fit quality. We show an example comparison of the two fits below. The red curve is the fit to the Landau, and the blue curve is the fit to the convolution of a Landau and a Gaussian.

****

We find that the fit to the convolution of a landau and Gaussian has a small and correlated impact on the value of the peak. The peak location shifts about 5% for all points. It does not impact the conclusions of the uniformity, as all points shift in the same direction. We have added the following sentence to the text in Section 6 regarding this systematic effect:

**As a study of systematic effects, we have also repeated the fit using the convolution
of a Landau function and a Gaussian function to model the impact of noise and fluctuations
in the multiplication process. We find that the peak location increases
systematically by about $5\%$ for all points in a correlated fashion.
However it does not appear to impact the conclusions drawn on the response uniformity.**

L227 : MA - What are the gains at these voltages?

This information has been added in Tab. 2 of the new paper draft.

L229-233 : MA -  What was the cut on LGAD signal to be considered as a signal (can be expressed in charge or gain fraction)?  If the cut is very low you may end up with 100% efficiency, but with very high noise occupancy, which would be unacceptable at real experiment. A value of noise occupancy would be also welcome.

The noise was measured using dedicated runs with no bam particles, and data collected using random triggers. The RMS of the amplitude of noise was measured to be 1.2 mV on FNAL boards. The cut used in the efficiency plots is at 20 mV, well above the noise level. We have added the following text in Sec. 6.1:

“Noise  values for different boards used in the experiments are listed in Sec. 4, and were measured using dedicated runs with no particles, and data collected using random triggers.”

Figure 5: MA - How did you determine the error bars? Why are they larger for W9HG11 (bottom right plot)?

The error bars are evaluated as Clopper–Pearson intervals for calculating binomial confidence intervals. They are larger for the CNM sensor since there was much more data collected for the 50D-PIX sensor. We have added this sentence in Section 6.1 to clarify the point for the reader:

“Error bars  in all efficiency measurements are evaluated as Clopper-Pearson intervals for calculating  binomial confidence intervals.”

L241 : MA - Can you show the fit of Landau to the data? This goes hand in hand with the previous comment in L215.

We have added an example Landau fit plot to Section 6.

Figure 6 : MA - Why is uncertainty of HPK smaller than for CNM? Can you convert MPV[V] into gain/charge? This conversion would be welcome already earlier in the text.

The gain vs voltage values have been added in Tab. 2 of the new paper draft. We have also added the following sentence in Section 6, last paragraph before Section 6.1:

**“Measurements presented  for various sensors were obtained from different datasets and therefore the statistical precision is not always the same. The reason that in some measurements the error bars  are not the same across either X- or Y-coordinate is due to the fact that the beam does  not uniformly illuminate the whole sensor area, and hence the number of events is not  the same across sensor surface.”**

L247 : OP - I think the reason for this difference in timestamp can be different signal formation in the  electrode for hit positions. The resistivity of n++ layers in not the same as that of Al electrodes, hence the difference in rise time. This holds for the section from L303-308.

Following the suggestion of the other reviewer, we have removed the speculation about the rise time. The modified text is as follows:

**“This effect cannot be attributed to the algorithm used to time-stamp the events, since the same behavior is observed with the CFD and CDT algorithms. Furthermore, the same behavior is observed on all HPK sensor varieties mounted on KU board, as presented in Sec. 6.3. Further studies are needed to understand the effect.”**

L256/Figure 8 : MA - It is a absolutely necessary to present the reader with the gain values for the data in Fig. 8 in order to mislead the reader into believing that HPK in "intrinsically better"- see a comment L227. The difference is already in average electric fields achieved for both sensors, gain and also in capacitances.

This information has been added in Tab. 2 of the new paper draft.

L268 : MI - This looks like a ROOT code - please write erf full form. "floated in the fit" is colloquial - "were free parameters of the fit" is better

We have changed the text following the suggestion of the reviewer.

Figure 12 - OP:  Is it clear why time stamp is negative for 50D-PIX device in the gap region?

To clarify, the plot shows the time difference ( Δt=t1-t0 ) between the reference timestamp in the Photek 240 MCP-PMT (t0) and the timestamp of the LGAD sensors (t1). All measurements are shown such that the central, flat part of these plots aligns with the Δt=0. It is not understood why the timestamp is negative ( LGAD signals arrive earlier ) for points in the gap region – though we only observe it for the 50D PIX sensor – and more studies are needed to understand that feature.

Figure 14 / L318-322 - MA: What is Landau fluctuations limit for the 80 um sensor timing resolution? It seems that more charge for 80 um detector (although at lower gain) compensates for longer rise time and Landau fluctuations.  Can you show also "constant function" fit to data, so that it would be more evident?

The Landau fluctuations are worse for thicker sensors, for 80 micron it is about 40 ps, e.g. see H. Sadrozinski, A. Seiden and N. Cartiglia, “4-Dimensional Tracking with Ultra-Fast Silicon Detectors”, 2018 Rep. Prog. Phys. **81** 026101.

We have added constant function fits to the data in the Figure as suggested by the reviewer.

Figure 15 - section 6.5 : MA -  There is one significant piece of information missing for the reader. It is true that lowering the temperature increases the gain (impact ionization depends strongly on temperature, also mobility), but also the breakdown voltage. Vbd shifts to higher values for larger temperatures hence higher gain at lower temperatures can be compensated by larger applied bias at higher temperatures. Hence, similar or only slightly worse resolutions can be obtained at 20C for non-irradiated sensors.

Yes, that is correct. The main reason we want to operate at lower temperatures is to avoid large currents for irradiated devices. We have added the following sentence following the suggestion of the reviewer:

**“The sensors yield higher gain at lower temperatures, but at the cost of a lower breakdown voltage. Therefore, it is important to study the impact of the temperature on the gain and time resolution, as well as their uniformity.”**

L355 : MA - There is no mentioning (even in a single sentence) of what radiation does to the LGADs nor citations to previous works on LGAD radiation hardness.

We have added references 15 and 16, and the following sentence in Sec. 6.6:

**“Effects of neutron irradiation on LGAD sensors is documented in [6], [16] and [17]”.**

L358-359 : MA - missing citation for spectrum and flux.

We have added citation [15] in Sec. 6.6

Figure 18 : MA -  What is the gain? What is the bias voltage of the W11LGA35 device?

This information has been added in Tab. 2 of the new paper draft.

L368 : MA - 2.5 times at what voltage?

This sentence describes the difference in signal size at the same bias voltage. We have clarified this in the new text:

**“The distribution on the right of Fig. 18 shows that at the same bias voltage the amplitude under the aluminum (periphery) is about 2.5 times larger than that without aluminum (center).”**

L372 : MA - Looking at Fig. 4, I would say that the whole active area of HPK50D is without metallization.

Indeed, we fixed the sentence to read:

**“In contrast to the CNM sensor, the whole surface of the active area of the HPK 50D sensor is without metallization.”**

L374 : MA - Please give the gain values - not only voltages. How close are the applied voltages to breakdown voltages?

This information has been added in Tab. 2 of the new paper draft. The breakdown voltage of HPK 50D sensor is about 650 V, and the breakdown voltage of the CNM sensor is about 450 V.

Figure 20 : OP - Is the data set size for CNM detector smaller, hence larger uncertainty?

Yes, that is correct. We have added a sentence in Section 6, last paragraph before Section 6.1 to explain this:

**“Measurements presented  for various sensors were obtained from different datasets and therefore the statistical precision is not always the same. The reason that in some measurements the error bars  are not the same across either X- or Y-coordinate is due to the fact that the beam does  not uniformly illuminate the whole sensor area, and hence the number of events is not  the same across sensor surface.”**

L390 : OP - Do you have any idea how is this possible?

We believe this is due to the same effect observed on non-irradiated HPK sensors with difference in time of arrival from metalized vs non-metalized areas of the sensor. More study is needed to understand why the time response is different in the metalized regions compared to the non-metalized regions.

L391 : MI - The decrease of timing resolution for CNM at higher voltages can only be due to increase of noise, hence jitter, as Fig. 21 shows the increase of MPV. Please mention this or even better give the relative increase of noise.

Indeed, for the CNM sensor we find that the noise RMS increases from about 5.5mV to about 10mV. We have added the following text in the paper to explain this effect:

We observe that while the signal amplitudes increases a bit, the RMS of the
noise also increases from about 5.5 mV to 10 mV. As a consequence, we observe a small degradation
of the time resolution for the CNM sensor as the bias voltage is increased.