

# 电动力学第二周作业

涂嘉乐 PB23151786

2025 年 3 月 14 日

## 1.6

证明 首先

$$\begin{aligned}\nabla \cdot \left( \frac{\vec{R}}{R^3} \right) &= \left( \nabla \frac{1}{R^3} \right) \cdot \vec{R} + \frac{1}{R^3} (\nabla \times \vec{R}) = -3 \frac{1}{R^4} \nabla R \cdot \vec{R} + \frac{1}{R^3} \cdot 3 \\ &= -\frac{3\vec{e}_r}{R^4} \cdot \vec{R} + \frac{3}{R^3} = 0 \\ \nabla \times \left( \frac{\vec{R}}{R^3} \right) &= \nabla \left( \frac{\vec{R}}{R^3} \right) \times \vec{R} + \frac{1}{R^3} (\nabla \times \vec{R}) \\ &= -\frac{3\vec{e}_r}{R^4} \times \vec{R} + \frac{1}{R^3} (\nabla \times \vec{R}) = 0 + 0 = 0\end{aligned}$$

使用公式

$$\nabla \times (\vec{f} \times \vec{g}) = (\vec{g} \cdot \nabla) \vec{f} + (\nabla \cdot \vec{g}) \vec{f} - (\vec{f} \cdot \nabla) \vec{g} - (\nabla \cdot \vec{f}) \vec{g}$$

则我们有

$$\begin{aligned}\nabla \times \left( \vec{m} \times \frac{\vec{R}}{R^3} \right) &= \left( \frac{\vec{R}}{R^3} \cdot \nabla \right) \vec{m} + \left( \nabla \cdot \frac{\vec{R}}{R^3} \right) \vec{m} - (\vec{m} \cdot \nabla) \frac{\vec{R}}{R^3} - (\nabla \cdot \vec{m}) \frac{\vec{R}}{R^3} \\ &= -(\vec{m} \cdot \nabla) \frac{\vec{R}}{R^3}\end{aligned}$$

使用公式

$$\begin{aligned}\nabla (\vec{f} \cdot \vec{g}) &= \vec{f} \times (\nabla \times \vec{g}) + (\vec{f} \cdot \nabla) \vec{g} + \vec{g} \times (\nabla \times \vec{f}) + (\vec{g} \cdot \nabla) \vec{f} \\ \nabla \left( \frac{\vec{m} \cdot \vec{R}}{R^3} \right) &= \vec{m} \times \left( \nabla \times \frac{\vec{R}}{R^3} \right) + (\vec{m} \cdot \nabla) \frac{\vec{R}}{R^3} + \frac{\vec{R}}{R^3} \times (\nabla \times \vec{m}) + \left( \frac{\vec{R}}{R^3} \cdot \nabla \right) \vec{m} \\ &= (\vec{m} \cdot \nabla) \frac{\vec{R}}{R^3}\end{aligned}$$

所以

$$\nabla \times \left( \vec{m} \times \frac{\vec{R}}{R^3} \right) = -\nabla \left( \frac{\vec{m} \cdot \vec{R}}{R^3} \right)$$

□

## 1.10

证明 首先, 电流圈  $L_1$  在电流圈  $L_2$  上的电流元  $I_2 d\mathbf{l}_2$  上产生的磁场为 (记  $\mathbf{r}_{12}$  是从  $I_1 d\mathbf{l}_1$  指向  $I_2 d\mathbf{l}_2$  的向量)

$$\mathbf{B}_1 = \frac{\mu_0}{4\pi} \oint_{L_1} \frac{I_1 d\mathbf{l}_1 \times \mathbf{r}_{12}}{r_{12}^3}$$

所以电流元  $I_2 d\mathbf{l}_2$  在该磁场下受到的作用力为

$$d\mathbf{F}_{12} = I_2 d\mathbf{l}_2 \times \mathbf{B}_1 = I_2 d\mathbf{l}_2 \times \frac{\mu_0}{4\pi} \oint_{L_1} \frac{I_1 d\mathbf{l}_1 \times \mathbf{r}_{12}}{r_{12}^3}$$

再在  $L_2$  上积分, 故电流圈  $L_1$  对  $L_2$  的作用力为

$$\begin{aligned}\mathbf{F}_{12} &= \oint_{L_2} d\mathbf{F}_{12} = \oint_{L_2} I_2 d\mathbf{l}_2 \times \frac{\mu_0}{4\pi} \oint_{L_1} \frac{I_1 d\mathbf{l}_1 \times \mathbf{r}_{12}}{r_{12}^3} \\ &= \frac{\mu_0 I_1 I_2}{4\pi} \oint_{L_2} d\mathbf{l}_2 \times \oint_{L_1} \frac{d\mathbf{l}_1 \times \mathbf{r}_{12}}{r_{12}^3} = \frac{\mu_0 I_1 I_2}{4\pi} \oint_{L_2} \oint_{L_1} d\mathbf{l}_2 \times \frac{d\mathbf{l}_1 \times \mathbf{r}_{12}}{r_{12}^3} \\ &= \frac{\mu_0 I_1 I_2}{4\pi} \oint_{L_2} \oint_{L_1} \left[ \frac{d\mathbf{l}_1 (\mathbf{r}_{12} \cdot d\mathbf{l}_2)}{r_{12}^3} - \frac{\mathbf{r}_{12} (d\mathbf{l}_1 \cdot d\mathbf{l}_2)}{r_{12}^3} \right]\end{aligned}$$

由 Stokes 定理

$$\begin{aligned}\oint_{L_2} \oint_{L_1} \frac{d\mathbf{l}_1 (\mathbf{r}_{12} \cdot d\mathbf{l}_2)}{r_{12}^3} &= \oint_{L_1} d\mathbf{l}_1 \oint_{L_2} \frac{\mathbf{r}_{12} \cdot d\mathbf{l}_2}{r_{12}^3} \\ &= \oint_{L_1} d\mathbf{l}_1 \iint_{S_2} \nabla \times \left( \frac{\mathbf{r}_{12}}{r_{12}^3} \right) \cdot d\mathbf{S} \\ &= \oint_{L_1} 0 \cdot d\mathbf{l}_1 = 0\end{aligned}$$

所以

$$\mathbf{F}_{12} = -\frac{\mu_0 I_1 I_2}{4\pi} \oint_{L_2} \oint_{L_1} \frac{\mathbf{r}_{12} (d\mathbf{l}_1 \cdot d\mathbf{l}_2)}{r_{12}^3}$$

同理, 交换下标 1, 2 得电流圈  $L_2$  对  $L_1$  的作用力

$$\mathbf{F}_{21} = -\frac{\mu_0 I_1 I_2}{4\pi} \oint_{L_1} \oint_{L_2} \frac{\mathbf{r}_{21} (d\mathbf{l}_2 \cdot d\mathbf{l}_1)}{r_{21}^3}$$

因为  $\mathbf{r}_{12} = -\mathbf{r}_{21}$ , 则对比上面两式, 显然有  $\mathbf{F}_{12} = -\mathbf{F}_{21}$ , 因此两个电流圈之间的相互作用力大小相等、方向相反; 但对于电流元  $I_1 d\mathbf{l}_1, I_2 d\mathbf{l}_2$  之间作用力

$$d\mathbf{F}_{12} = I_2 d\mathbf{l}_2 \times \frac{\mu_0}{4\pi} \frac{I_1 d\mathbf{l}_1 \times \mathbf{r}_{12}}{r_{12}^3}, \quad d\mathbf{F}_{21} = I_1 d\mathbf{l}_1 \times \frac{\mu_0}{4\pi} \frac{I_2 d\mathbf{l}_2 \times \mathbf{r}_{21}}{r_{21}^3}$$

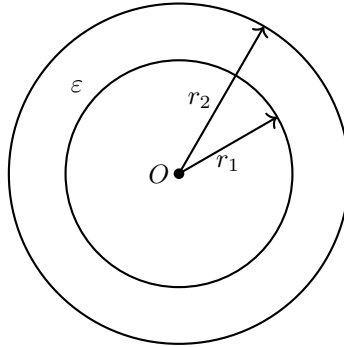
仅考虑方向,  $d\mathbf{l}_2 \times (d\mathbf{l}_1 \times \mathbf{r}_{12}), d\mathbf{l}_1 \times (d\mathbf{l}_2 \times \mathbf{r}_{21})$  都不一定反向: 考虑如下情形

$$\overrightarrow{d\mathbf{l}_1} \cdots \cdots \mathbf{r}_{12} \cdots \cdots \uparrow d\mathbf{l}_2$$

则  $d\mathbf{l}_2 \times (d\mathbf{l}_1 \times \mathbf{r}_{12}) = \mathbf{0}, d\mathbf{l}_1 \times (d\mathbf{l}_2 \times \mathbf{r}_{21}) \neq \mathbf{0}$ , 故显然不服从牛顿第三定律 □

## 1.7

解 (1).



取半径为  $r$  的 Gauss 面  $S$ , 则由均匀分布知

$$\oint_S \mathbf{D} \cdot d\mathbf{S} = 4\pi r^2 D$$

由 Gauss 定理知

$$\oint_S \mathbf{D} \cdot d\mathbf{S} = 4\pi r^2 D = \iiint_V \rho_f dV = \begin{cases} 0, & r < r_1 \\ \frac{4\pi}{3}(r^3 - r_1^3)\rho_f, & r_1 < r < r_2 \\ \frac{4\pi}{3}(r_2^3 - r_1^3)\rho_f, & r > r_2 \end{cases}$$

又因为  $\mathbf{D} = \varepsilon \mathbf{E}$ , 所以

$$\mathbf{E} = \begin{cases} 0, & r < r_1 \\ \frac{(r^3 - r_1^3)\rho_f}{3\varepsilon r^3} \mathbf{r}, & r_1 < r < r_2 \\ \frac{(r_2^3 - r_1^3)\rho_f}{3\varepsilon_0 r^3} \mathbf{r}, & r > r_2 \end{cases}$$

(2). 因为在介质内  $\mathbf{D} = \varepsilon_0 \mathbf{E} + \mathbf{P}$ , 所以

$$\mathbf{P} = \mathbf{D} - \varepsilon_0 \mathbf{E} = \left(1 - \frac{\varepsilon_0}{\varepsilon}\right) \frac{(r^3 - r_1^3)\rho_f}{3r^3} \mathbf{r}$$

所以

$$\rho_p = -\nabla \cdot \mathbf{P} = -\frac{\rho_f}{3} \left(1 - \frac{\varepsilon_0}{\varepsilon}\right) \nabla \cdot \left(\frac{r^3 - r_1^3}{r^3} \mathbf{r}\right) = -\left(1 - \frac{\varepsilon_0}{\varepsilon}\right) \rho_f, \quad r_1 < r < r_2$$

因为只有在  $r = r_1, r = r_2$  处, 极化强度发生改变, 当  $r = r_1$  时,  $\mathbf{n} = \mathbf{e}_r$ ,  $\mathbf{P}^{(2)} = \mathbf{P}|_{r=r_1}$ ,  $\mathbf{P}^{(1)} = 0$ , 所以

$$\sigma_P|_{r=r_1} = -\mathbf{n} \cdot (\mathbf{P}^{(2)} - \mathbf{P}^{(1)}) = 0$$

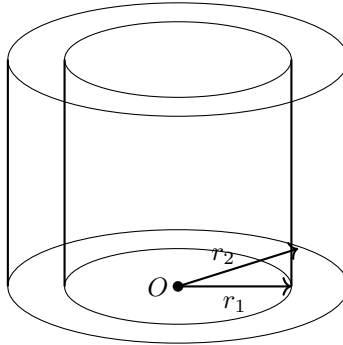
当  $r = r_2$  时,  $\mathbf{n} = \mathbf{e}_r$ ,  $\mathbf{P}^{(1)} = \mathbf{P}|_{r=r_2}$ ,  $\mathbf{P}^{(2)} = 0$ , 所以

$$\sigma_P|_{r=r_2} = -\mathbf{n} \cdot (\mathbf{P}^{(2)} - \mathbf{P}^{(1)}) = \frac{r_2^3 - r_1^3}{3r_2^2} \left(1 - \frac{\varepsilon_0}{\varepsilon}\right) \rho_f$$

□

## 1.8

解



取沿圆柱轴线向上为正方向, 取圆心在圆柱中轴线上的半径为  $r$  的圆环  $L$ , 由均匀分布知

$$\oint_L \mathbf{H} \cdot d\mathbf{l} = H \cdot 2\pi r$$

由安培环路定理知

$$\oint_L \mathbf{H} \cdot d\mathbf{l} = 2\pi r H = \iint_S \mathbf{J}_f \cdot d\mathbf{S} = \begin{cases} 0, & r < r_1 \\ \pi(r^2 - r_1^2) \mathbf{J}_f, & r_1 < r < r_2 \\ \pi(r_2^2 - r_1^2) \mathbf{J}_f, & r > r_2 \end{cases}$$

又因为  $\mathbf{B} = \mu \mathbf{H}$ , 所以

$$\mathbf{B} = \begin{cases} 0, & r < r_1 \\ \frac{\mu(r^2 - r_1^2)}{2r^2} \mathbf{J}_f \times \mathbf{r}, & r_1 < r < r_2 \\ \frac{\mu_0(r_2^2 - r_1^2)}{2r^2} \mathbf{J}_f \times \mathbf{r}, & r > r_2 \end{cases}$$

又因为  $\mathbf{H} = \frac{\mathbf{B}}{\mu_0} - \mathbf{M}$ , 所以当  $r_1 < r < r_2$  时

$$\mathbf{M} = \frac{\mathbf{B}}{\mu_0} - \mathbf{H} = \left( \frac{\mu}{\mu_0} - 1 \right) \mathbf{H} = \frac{\mu - \mu_0}{\mu_0} \frac{(r^2 - r_1^2)}{2r^2} \mathbf{J}_f \times \mathbf{r}$$

$$\mathbf{J}_M = \nabla \times \mathbf{M} = \left( \frac{\mu - \mu_0}{\mu_0} \right) \mathbf{J}_f$$

因为只有在  $r = r_1, r = r_2$  时,  $\mathbf{M}$  发生改变, 让  $r = r_1$  时,  $\mathbf{n} = \mathbf{e}_r, \mathbf{M}^{(2)} = \mathbf{M}|_{r=r_1}, \mathbf{M}^{(1)} = 0$ , 所以

$$\alpha_M|_{r=r_1} = \mathbf{n} \times (\mathbf{M}^{(2)} - \mathbf{M}^{(1)}) = 0$$

当  $r = r_2$  时,  $\mathbf{n} = \mathbf{e}_r, \mathbf{M}^{(2)} = 0, \mathbf{M}^{(1)} = \mathbf{M}|_{r=r_2}$ , 所以

$$\alpha_M|_{r=r_2} = \mathbf{n} \times (\mathbf{M}^{(2)} - \mathbf{M}^{(1)}) = - \left( \frac{\mu - \mu_0}{\mu_0} \right) \frac{r_2^2 - r_1^2}{2r_2} \mathbf{J}_f$$

□

## 1.9

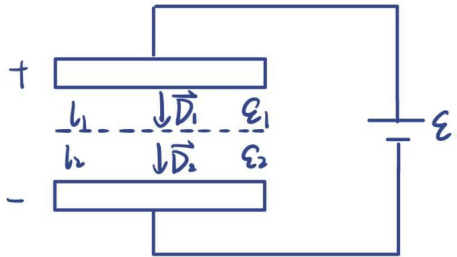
证明 因为各向同性线性均匀介质内有  $\mathbf{D} = \varepsilon \mathbf{E}$ , 且  $\mathbf{D} = \varepsilon_0 \mathbf{E} + \mathbf{P}$ , 所以  $\mathbf{P} = \left(1 - \frac{\varepsilon_0}{\varepsilon}\right) \mathbf{D}$

$$\begin{aligned} \rho_P &= -\nabla \cdot \mathbf{P} = - \left(1 - \frac{\varepsilon_0}{\varepsilon}\right) \nabla \cdot \mathbf{D} \\ &= - \left(1 - \frac{\varepsilon_0}{\varepsilon}\right) \rho_f \end{aligned}$$

□

## 1.11

解 (2).



因为介质内没有自由电荷, 所以在介质分界面上, 自由电荷密度  $\omega_f = 0$

(1). 因为在介质交界处, 自由电荷密度  $\omega_f = 0$ , 取向向下为正方向, 则

$$\mathbf{n} \cdot (\mathbf{D}_2 - \mathbf{D}_1) = \omega_f = 0$$

所以  $D_2 = D_1$ , 而  $D = \varepsilon E$ , 所以  $\varepsilon_1 E_1 = \varepsilon_2 E_2$ , 又因为  $E_1 l_1 + E_2 l_2 = \mathcal{E}$ , 联立二式解得

$$\begin{cases} E_1 = \frac{\varepsilon_2 \mathcal{E}}{\varepsilon_1 l_2 + \varepsilon_2 l_1} \\ E_2 = \frac{\varepsilon_1 \mathcal{E}}{\varepsilon_1 l_2 + \varepsilon_2 l_1} \end{cases} \Rightarrow D_2 = D_1 = E_1 = \frac{\varepsilon_1 \varepsilon_2 \mathcal{E}}{\varepsilon_1 l_2 + \varepsilon_2 l_1} \mathbf{n}$$

对于上极板,  $D^{(2)} = D_1, D^{(1)} = 0$ , 所以

$$\omega_{up} = \mathbf{n} \cdot (D^{(2)} - D^{(1)}) = \frac{\varepsilon_1 \varepsilon_2 \mathcal{E}}{\varepsilon_1 l_2 + \varepsilon_2 l_1}$$

对于下极板,  $D^{(2)} = 0, D^{(1)} = D_2$ , 所以

$$\omega_{down} = \mathbf{n} \cdot (D^{(2)} - D^{(1)}) = -\frac{\varepsilon_1 \varepsilon_2 \mathcal{E}}{\varepsilon_1 l_2 + \varepsilon_2 l_1}$$

若介质是漏电的, 由电荷守恒定理

$$\nabla \cdot \mathbf{J} + \frac{\partial \rho}{\partial t} = 0$$

因为稳恒条件下  $\frac{\partial \rho}{\partial t} = 0$ , 所以我们有  $\nabla \cdot \mathbf{J} = 0$ , 故对于介质 1, 2 的交界面, 我们有  $J_{1n} = J_{2n} = J_n$ , 又因为  $\mathbf{J} = \sigma \mathbf{E}$ , 所以  $\sigma_1 E_1 = \sigma_2 E_2 = J_n$ , 联立

$$\begin{cases} E_1 l_1 + E_2 l_2 = \mathcal{E} \\ \sigma_1 E_1 = \sigma_2 E_2 = J_n \end{cases} \Rightarrow J_n = \frac{\sigma_1 \sigma_2 \mathcal{E}}{\sigma_1 l_2 + \sigma_2 l_1}$$

对于上极板,  $D^{(2)} = D_1 = \varepsilon_1 E_1 = \frac{\varepsilon_1 J_n}{\sigma_1}, D^{(1)} = 0$ , 所以

$$\omega_{f_1} = \mathbf{n} \cdot (D^{(2)} - D^{(1)}) = \frac{\varepsilon_1 \sigma_2 \mathcal{E}}{\sigma_1 l_2 + \sigma_2 l_1}$$

对于下极板,  $D^{(2)} = 0, D^{(1)} = D_2 = \varepsilon_2 E_2 = \frac{\varepsilon_2 J_n}{\sigma_2}$ , 所以

$$\omega_{f_2} = \mathbf{n} \cdot (D^{(2)} - D^{(1)}) = -\frac{\varepsilon_2 \sigma_1 \mathcal{E}}{\sigma_1 l_2 + \sigma_2 l_1}$$

对于介质交界面,  $D^{(2)} = D_2, D^{(1)} = D_1$ , 所以

$$\omega_{f_3} = \mathbf{n} \cdot (D^{(2)} - D^{(1)}) = \frac{(\varepsilon_2 \sigma_1 - \varepsilon_1 \sigma_2) \mathcal{E}}{\sigma_1 l_2 + \sigma_2 l_1}$$

□

## 1.12

证明 (1). 分界面上没有自由电荷,  $\sigma_f = 0$ , 由边值关系

$$\begin{cases} \mathbf{n} \cdot (D^{(2)} - D^{(1)}) = 0 \\ \mathbf{n} \times (E^{(2)} - E^{(1)}) = 0 \end{cases}$$

故

$$E_{2\tau} = E_{1\tau}, \quad D_{2n} = D_{1n}$$

又因为  $\mathbf{D} = \varepsilon \mathbf{E}$ , 所以

$$\begin{cases} E_2 \sin \theta_2 = E_1 \sin \theta_1 \\ \varepsilon_2 E_2 \cos \theta_2 = \varepsilon_1 E_1 \cos \theta_1 \end{cases}$$

解得

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\varepsilon_2}{\varepsilon_1}$$

(2). 由于电流恒定时  $\frac{\partial \rho}{\partial t} = 0$ , 由边值关系

$$\begin{cases} \mathbf{n} \cdot (\mathbf{J}^{(2)} - \mathbf{J}^{(1)}) = 0 \\ \mathbf{n} \times (\mathbf{E}^{(2)} - \mathbf{E}^{(1)}) = 0 \end{cases}$$

故

$$E_{2\tau} = E_{1\tau}, \quad J_{2n} = J_{1n}$$

又因为  $\mathbf{J} = \sigma \mathbf{E}$ , 所以

$$\begin{cases} E_2 \sin \theta_2 = E_1 \sin \theta_1 \\ \sigma_2 E_2 \cos \theta_2 = \sigma_1 E_1 \cos \theta_1 \end{cases}$$

解得

$$\frac{\tan \theta_2}{\tan \theta_1} = \frac{\sigma_2}{\sigma_1}$$

□