

Since I have already taken the midterm, I will only be completing the exercises related to the second part of the course (from differential kinematics onwards).

Exercise #2

The absolute initial orientation of the end effector of a 6R robot with a spherical wrist is specified by the  $YXY$  sequence of Euler angles  $\alpha = (\alpha_1, \alpha_2, \alpha_3) = (45^\circ, -45^\circ, 120^\circ)$ . A different orientation is expressed instead by the rotation matrix

$${}^0R_f = \begin{pmatrix} 0 & \sin \phi & \cos \phi \\ 0 & \cos \phi & -\sin \phi \\ -1 & 0 & 0 \end{pmatrix}, \quad \text{with } \phi = \frac{\pi}{3}.$$

Find an axis-angle representation  $(\mathbf{r}, \theta)$  of the relative rotation between these two end-effector orientations. Further, if a motion is imposed to the end effector with constant angular velocity  $\omega = 1.1 \cdot \mathbf{r}$  [rad/s], what will be the time  $T_\omega$  needed to accomplish this change of orientation?

I denote the first orientation  ${}^0R_i$ . Since

$${}^0R_i = R_y(45^\circ)R_x(-45^\circ)R_y(120^\circ) = \begin{pmatrix} 0 & 0 & 1 \\ 0 & 1 & 0 \\ -1 & 0 & 0 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & -1 & 0 \end{pmatrix} \begin{pmatrix} -\frac{1}{2} & 0 & \frac{\sqrt{3}}{2} \\ 0 & 1 & 0 \\ \frac{\sqrt{3}}{2} & 0 & -\frac{1}{2} \end{pmatrix} = \begin{pmatrix} 0 & -1 & 0 \\ -0.866 & 0 & -0.5 \\ 0.5 & 0 & -0.866 \end{pmatrix}$$

Now i have to find  $\mathbf{r}, \theta$  s.t.  $R(\theta, \mathbf{r}) = {}^iR_f = {}^0R_i^T {}^0R_f$

$${}^iR_f = \begin{pmatrix} -0.5 & -0.433 & 0.75 \\ 0 & -0.866 & -0.5 \\ 0.866 & -0.25 & 0.433 \end{pmatrix} \Rightarrow 1 + 2\cos\theta = \text{trace}({}^iR_f) \Rightarrow 1 + 2\cos\theta = -0.933 \Rightarrow \cos\theta = -0.4665 \Rightarrow \theta = 2.882$$

$$\text{then: } \mathbf{r} = \frac{1}{2\sin\theta} \begin{pmatrix} R_{32} - R_{23} \\ R_{13} - R_{31} \\ R_{21} - R_{12} \end{pmatrix} \Rightarrow \mathbf{r} = 1.948 \begin{pmatrix} 0.25 \\ -0.116 \\ 0.433 \end{pmatrix} = \begin{pmatrix} 0.487 \\ -0.226 \\ 0.843 \end{pmatrix}$$

IF i consider  $R(t) = {}^0R_i R(\theta, \mathbf{r})$  with  $\theta(t) \in [0, 2.882]$  i have a parametrization of the orientation. the angular speed is  $\omega = \mathbf{r} \dot{\theta}$  so  $\dot{\theta} = 1.1 \Rightarrow \theta(t) = 1.1t = 2.882 \Rightarrow T_\omega = 2.62$  [sec].

Exercise #3

Assume that the motion of a 3R planar robot having equal links of unitary length is commanded by the joint acceleration  $\ddot{\mathbf{q}} \in \mathbb{R}^3$ . With reference to Fig. 2, the robot end effector should follow a desired smooth trajectory  $\mathbf{p}_d(t) = (p_{x,d}(t), p_{y,d}(t))^T \in \mathbb{R}^2$  in position, while keeping constant its angular speed at some value  $\omega_{z,d} \in \mathbb{R}$  (perhaps, after an initial transient).

- Provide the general form of the command  $\ddot{\mathbf{q}}$  that executes the full task in nominal conditions.
- Study the singularities that may be encountered during the execution of the task.

the desired trajectory is  $\mathbf{r}_d = (p_{x,d}, p_{y,d}, \omega_{z,d}t)^T$ .

Since  $\ddot{\mathbf{r}} = \mathbf{J}(\mathbf{q})\ddot{\mathbf{q}} + \dot{\mathbf{J}}(\mathbf{q})\dot{\mathbf{q}}$  i impose  $\ddot{\mathbf{q}} = \mathbf{J}^{-1}(\mathbf{q})(\ddot{\mathbf{r}}_d - \dot{\mathbf{J}}\dot{\mathbf{q}})$ , this might not be realizable if  $\mathbf{J}$  is not invertible. Since:

$$\mathbf{J} = \begin{pmatrix} -s_1 - s_{12} - s_{123} & -s_{12} - s_{123} & -s_{123} \\ c_1 + c_{12} + c_{123} & c_{12} + c_{123} & c_{123} \\ 1 & 1 & 1 \end{pmatrix} \quad \dot{\mathbf{J}} = \begin{pmatrix} -(c_1 + c_{12} + c_{123}) & -(c_{12} + c_{123}) & -c_{123} \\ -s_1 - s_{12} - s_{123} & -s_{12} - s_{123} & -s_{123} \\ 0 & 0 & 0 \end{pmatrix}$$

- Compute the numerical value of  $\ddot{\mathbf{q}}$  when the robot is in the nominal state  $\mathbf{x}_d = (q_d, \dot{q}_d) \in \mathbb{R}^6$  and for a desired  $\ddot{\mathbf{p}}_d \in \mathbb{R}^2$ , as given by

$$\mathbf{q}_d = \begin{pmatrix} \pi/4 \\ \pi/3 \\ -\pi/2 \end{pmatrix} \text{ [rad]}, \quad \dot{\mathbf{q}}_d = \begin{pmatrix} -0.8 \\ 1 \\ 0.2 \end{pmatrix} \text{ [rad/s]}, \quad \ddot{\mathbf{p}}_d = \begin{pmatrix} 1 \\ 1 \end{pmatrix} \text{ [m/s}^2\text{]}.$$

What are the values of  $p_d, \dot{p}_d$ , and of  $\omega_{z,d}$  in this nominal robot state?

For  $\mathbf{q} = (\frac{\pi}{4}, \frac{\pi}{3}, -\frac{\pi}{2})$ :

$$\mathbf{J} = \begin{pmatrix} -1.531 & -1.224 & -0.259 \\ \sqrt{2} & 0.707 & 0.966 \\ 1 & 1 & 1 \end{pmatrix} \quad \dot{\mathbf{J}} = \begin{pmatrix} -\sqrt{2} & -0.707 & -0.966 \\ -1.531 & -1.224 & -0.259 \\ 0 & 0 & 0 \end{pmatrix} \\ \Rightarrow \ddot{\mathbf{q}} = \mathbf{J}^{-1}(\mathbf{q})(\ddot{\mathbf{r}}_d - \dot{\mathbf{J}}\dot{\mathbf{q}}) = (0.585 \quad -1.81 \quad 1.225)^T$$

iv. If at some time  $t \geq 0$ , there is a position and/or a velocity error in the execution of the desired end-effector trajectory  $p_d(t)$ , how would you modify the commanded acceleration  $\ddot{q}(t)$  so as to recover exponentially<sup>1</sup> the error to zero, both in position and velocity? And what if also the angular velocity  $\omega_s(t)$  is not the desired one?

let's consider a pos. error given by  $e = r_d - r$  and i want that to go to zero. Since  $\dot{e} = \dot{r}_d - \dot{r} = \dot{r}_d - J\dot{q}$  and

$$\ddot{e} = \ddot{r}_d - \ddot{r} = \ddot{r}_d - J(\dot{q})\ddot{q} - \dot{J}(\dot{q})\dot{q} =$$

$\ddot{r}_d - J(\dot{q})[J^{-1}(\dot{q})(\ddot{r}_d - \dot{J}(\dot{q})\dot{q}) + C] - \dot{J}(\dot{q})\dot{q}$  where  $C$  is an unknown command that i need to realize:  $\ddot{e} = -K\dot{e}$  with  $K = \text{diag}\{2, 2, 2\}$  and  $2 \in \mathbb{R}^+$ .

$$\ddot{r}_d - J(\dot{q})[J^{-1}(\dot{q})(\ddot{r}_d - \dot{J}(\dot{q})\dot{q}) + C] - \dot{J}(\dot{q})\dot{q} = -K\dot{e} \quad \text{i solve for } C$$

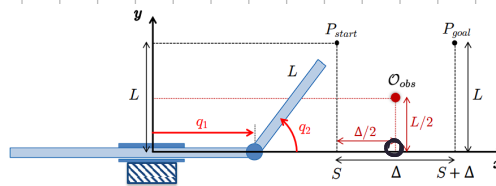
$$\ddot{r}_d - \ddot{r}_d + \dot{J}(\dot{q})\dot{q} - J(\dot{q})C - \dot{J}(\dot{q})\dot{q} = -K\dot{e} \Rightarrow -J(\dot{q})C = -K\dot{e} \Rightarrow C = J(\dot{q})K\dot{e} \quad \text{so}$$

$$\Rightarrow \text{new command is } \ddot{q} = J^{-1}(\dot{q})(\ddot{r}_d - \dot{J}(\dot{q})\dot{q}) + J(\dot{q})K\dot{e} \quad \text{so}$$

$\ddot{e} = -\dot{e} \Rightarrow$  the sol. for  $e$  is an exponential of the type  $e(t) = Ae^{-t}$

#### Exercise #4

Consider the situation in Fig. 3, with all data defined therein in symbolic form. The PR robot starts at rest with its end effector placed in  $P_{start} = (S, L)$  and should move the end effector to  $P_{goal} = (S + \Delta, L)$  in a given time  $T$  and stop there, without colliding with the obstacle  $O_{obs}$  located at  $(S + (\Delta/2), L/2)$ . Design a joint trajectory  $q_d(t) \in \mathbb{R}^2$ ,  $t \in [0, T]$ , that realizes the task with continuous acceleration  $\ddot{q}_d(t)$  and no instant of zero velocity in the open interval  $(0, T)$ . The solution should be parametric with respect to  $L > 0$  (length of the second link of the robot),  $S > 0$  ( $x$ -coordinate of  $P_{start}$ ),  $\Delta > L/2$  (distance of the two Cartesian points in the  $x$ -direction), and  $T$  (motion time). Provide then a numerical example, sketching the plot of  $q_d(t)$ .



I want the following conditions:

$$q_1(0) = S \quad q_1\left(\frac{T}{2}\right) = S + \frac{\Delta}{2} - L \quad q_1(T) = S + \Delta \quad \dot{q}_1(0) = 0$$

$$q_2(0) = \frac{\pi}{2} \quad q_2\left(\frac{T}{2}\right) = 0 \quad q_2(T) = \frac{\pi}{2} \quad \dot{q}_2(0) = 0$$

For both i use a 3-degree polynomial.

$$q_1(t) = at^3 + bt^2 + ct + d$$

$$q_2(t) = at^3 + bt^2 + ct + d$$

$$\begin{cases} q_1(0) = d = S \\ \dot{q}_1(0) = c = 0 \\ q_1\left(\frac{T}{2}\right) = \frac{a}{8}T^3 + \frac{b}{4}T^2 = \frac{\Delta}{2} - L \\ q_1(T) = aT^3 + bT^2 = \Delta \end{cases}$$

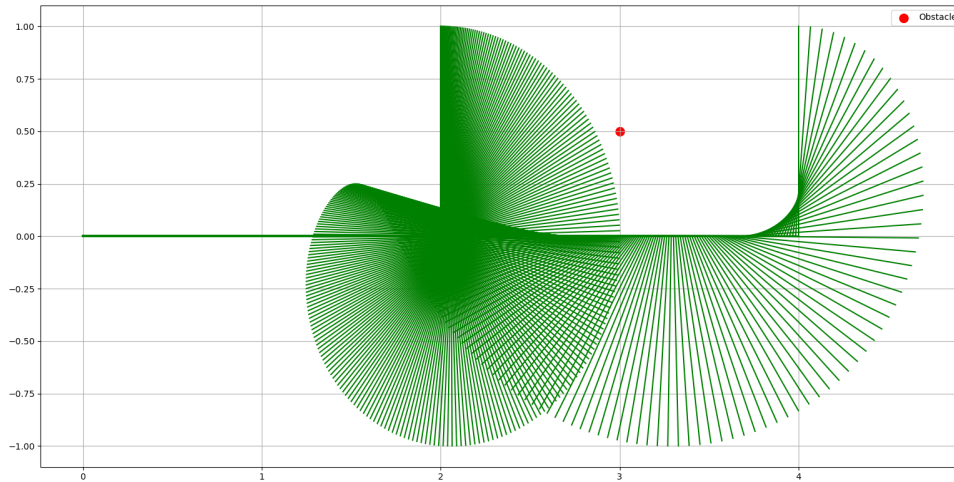
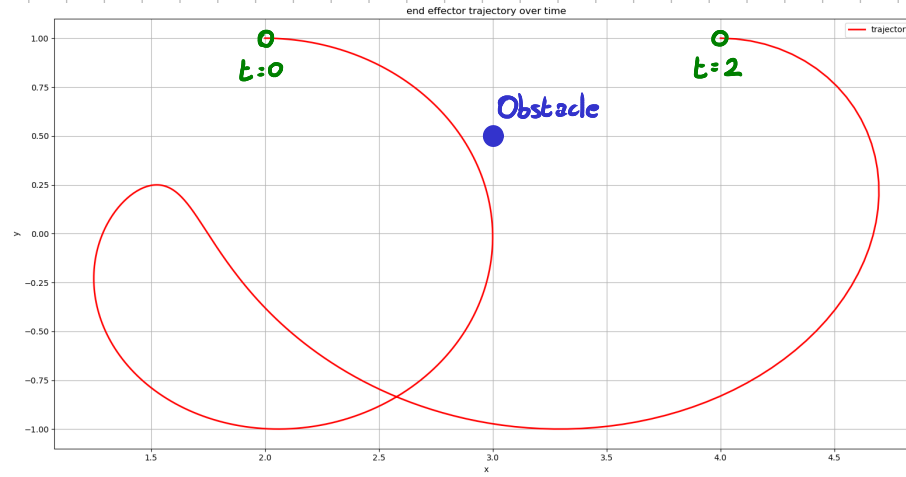
$$\begin{cases} q_2(0) = d = \frac{\pi}{2} \\ \dot{q}_2(0) = c = 0 \\ q_2\left(\frac{T}{2}\right) = \frac{a}{8}T^3 + \frac{b}{4}T^2 + \frac{\pi}{2} = 0 \\ q_2(T) = aT^3 + bT^2 = 0 \end{cases}$$

I choos the values  $L=1$ ,  $\Delta=2$ ,  $S=2$ ,  $T=2$

$$\begin{cases} q_1\left(\frac{T}{2}\right) = \frac{a}{8}T^3 + \frac{b}{4}T^2 = \frac{\Delta}{2} - L \\ q_1(T) = aT^3 + bT^2 = \Delta \end{cases} \Rightarrow \begin{cases} \frac{1}{8}a + \frac{1}{4}b = 0 \\ 8a + 4b = 2 \end{cases} \Rightarrow q_1(t) = \frac{1}{3}t^3 - \frac{1}{6}t^2 + 2$$

$$\begin{cases} q_2(T/2) = \frac{a}{8}T^3 + \frac{b}{4}T^2 + \frac{\pi}{2} = 0 \\ q_2(T) = aT^3 + bT^2 = 0 \end{cases} \Rightarrow \begin{cases} \frac{1}{8}a + \frac{1}{4}b = -\frac{\pi}{2} \\ 8a + 4b = 0 \end{cases} \Rightarrow q_2(t) = \frac{4}{3}\pi t^3 - \frac{8}{3}\pi t^2 + \frac{\pi}{2}$$

$$q(t) = \begin{cases} q_1(t) = \frac{1}{3}t^3 - \frac{1}{6}t^2 + 2 \\ q_2(t) = \frac{4}{3}\pi t^3 - \frac{8}{3}\pi t^2 + \frac{\pi}{2} \end{cases} \quad O_{obs} = (3, 1/2)$$



in this stroboscopic view is clear that the two arms of the manipulator never touch the obstacle.