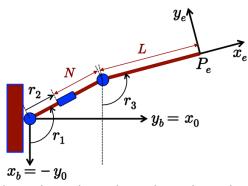


Exercise 1 [8 points]

Consider the 3-dof (PJP) planar robot in Fig. 1, where the joint coordinates  $\mathbf{r} = (r_1 \ r_2 \ r_3)^T$  have been defined in a free, arbitrary way, with reference to a base frame  $RF_b$ .

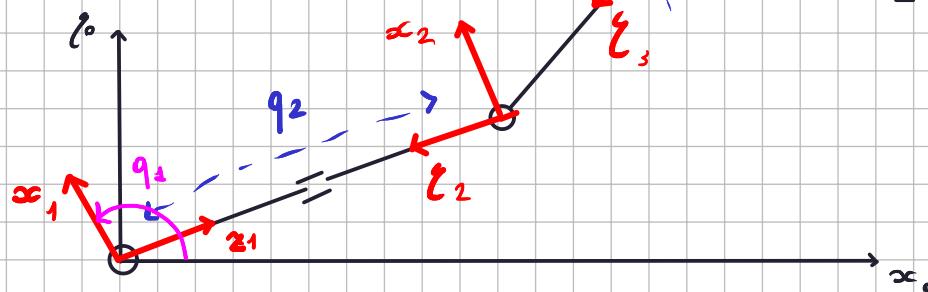


$$\begin{cases} p_x = (N + r_2) \cos r_1 + L \cos(r_1 + r_3) \\ p_y = (N + r_2) \sin r_1 + L \sin(r_1 + r_3) \end{cases} \text{ in reference frame } RF_B$$

$${}^B T_0 = \begin{bmatrix} 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

I now assign the DH Frames

$$\Rightarrow {}^3 T_e = \begin{bmatrix} R_x(\frac{\pi}{2}) & 0 \\ 0 & 1 \end{bmatrix}$$



	$a_i$	$d_i$	$\theta_i$	$\alpha_i$
1	$\pi/2$	0	0	$q_1$
2	$-\pi/2$	0	$q_2$	0
3	0	$L$	0	$q_3$

$$\begin{bmatrix} c_1 & 0 & s_1 & 0 \\ s_1 & 0 & -c_1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & q_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} c_3 & -s_3 & 0 & Lc_3 \\ s_3 & c_3 & 0 & Ls_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} =$$

$$\begin{bmatrix} c_1 & -s_1 & 0 & q_2 s_1 \\ s_1 & c_1 & 0 & -q_2 c_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c_3 & -s_3 & 0 & Lc_3 \\ s_3 & c_3 & 0 & Ls_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} =$$

$$\begin{bmatrix} c_1 c_3 - s_1 s_3 & -c_1 s_3 - s_1 c_3 & 0 & Lc_1 c_3 - Ls_1 s_3 + q_2 s_1 \\ s_1 c_3 + c_1 s_3 & -s_1 s_3 + c_1 c_3 & 0 & Ls_1 c_3 + Lc_1 s_3 - q_2 c_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

We have to solve:

$$\begin{cases} LC_{13} - LS_1S_3 + q_2S_1 = (N+r_2)\cos r_3 + L\cos(r_1+r_3) \\ LS_1C_3 + LC_1S_3 - q_2C_1 = (N+r_2)\sin r_1 + L\sin(r_1+r_3) \end{cases} \quad \text{for } q$$

$$\begin{cases} LC_{13} + q_2S_1 = (N+r_2)\cos r_3 + L\cos(r_1+r_3) \\ LS_1C_3 - q_2C_1 = (N+r_2)\sin r_1 + L\sin(r_1+r_3) \end{cases}$$

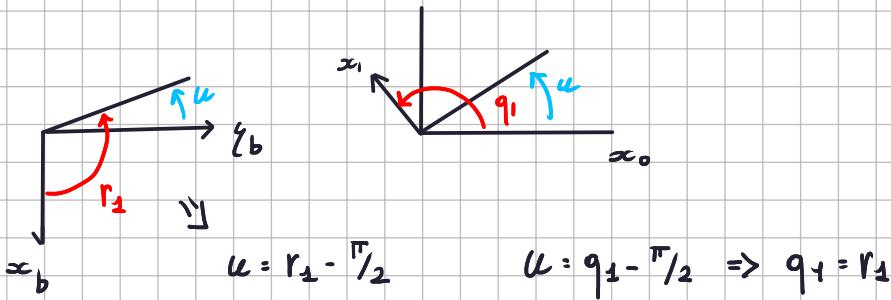
$$L^2 + q_2^2 + 2LC_{13}q_2S_1 - 2Lq_2C_1S_1 = (N+r_2)^2 + L^2 + 2(N+r_2)\cos r_1 \cdot L \cdot \cos(r_1+r_3) + 2(N+r_2)\sin r_1 \cdot L \sin(r_1+r_3)$$

$$\Rightarrow L^2 + q_2^2 - 2Lq_2S_3 = (N+r_2)^2 + L^2 - 2(N+r_2)L\cos(r_3) \quad \left\{ \text{I notice that } q_2 = N+r_2 \right.$$

$$\Rightarrow L^2 + q_2^2 - 2Lq_2S_3 = q_2^2 + L^2 - 2q_2L\cos(r_3) \Rightarrow$$

$$\sin(q_3) = \cos(r_3) \Rightarrow \cos(q_3) = \pm \sqrt{1 - \cos^2(r_3)} \Rightarrow q_3 = \arctan 2 \left\{ \cos(r_3), \pm \sqrt{1 - \cos^2(r_3)} \right\}$$

I notice that  $q_1 = r_1$



Given  $q_1$  and  $q_3$  the Following

$$\begin{cases} LC_{13} + q_2S_1 = (N+r_2)\cos r_3 + L\cos(r_1+r_3) \\ LS_1C_3 - q_2C_1 = (N+r_2)\sin r_1 + L\sin(r_1+r_3) \end{cases}$$

become a linear system in  $q_2$  and can be solved.

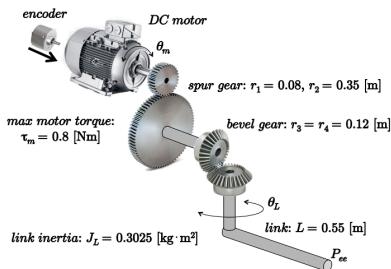


Figure 2: A DC servomotor that drives a robot link through transmissions.

With reference to the servo-drive sketched in Fig. 2 and the data therein, we need to measure the position of the tip point  $P_{ee}$  of the link with a resolution of 0.01 [mm]. A suitable incremental

A difference of 0.01 [mm], is in angle  $\Delta\theta_L$  such that  $\frac{360^\circ}{2\pi L} = \frac{x}{0.01}$   
we have to consider  $L = 0.55 \text{ m} = 550 \text{ mm} \Rightarrow$

$$\frac{360^\circ}{2\pi \cdot 550} = \frac{x}{0.01} \Rightarrow \Delta\theta_L = 1.04 \times 10^{-3} \text{ degrees.}$$

I have to calculate the reduction ratio Nr.

$$\text{From } \theta_m \text{ to spur gear} \Rightarrow n = \frac{0.35}{0.08} = \frac{35}{8}$$

The bevel gear ratio are 1:

$$\theta_m = \frac{35}{8} \theta_L \Rightarrow \text{the resolution to measure on the motor}$$

$$\text{should be } \Delta\theta_m = \frac{35}{8} \cdot 1.04 \times 10^{-3} = 4.55 \times 10^{-3} \text{ degrees.}$$

$$\Rightarrow \text{With quadrature, we have } \overset{\text{Angular res}}{\downarrow} AR = \frac{360^\circ}{PPR \cdot 4} \Rightarrow 19780.21978 \text{ PPR}$$

↑  
pulse per revolution

The number of bits should be  $\lceil \log_2 PPR \rceil = 15 \text{ bits}$

$$\text{The optimal ratio is } n_r = \sqrt{J_L/J_m} \Rightarrow \text{best } J_m = 0.0158 \text{ kg}\cdot\text{m}^2$$

$\Rightarrow$  the achievable acc. is  $\ddot{\theta}_L = 5.78 \frac{\text{degrees}}{\text{second}}$ .

**Exercise 3 [12 points]**

Consider the 6-dof robot Stäubli RX 160 in Fig. 3. In the extra sheet provided separately, the Denavit-Hartenberg (DH) table of parameters is specified, in part numerically and in part symbolically. The two DH frames 0 and 6 are already drawn on the manipulator (in two views). In the shown ‘straight upward’ robot configuration, the first and last joint variables take the values  $q_1 = q_6 = 0$ . Draw directly on the extra sheet the remaining DH frames, according to the DH table. Provide all parameters labeled in red in the table, i.e., the missing numerical values of the constant parameters and of the joint variables  $q_2$  to  $q_5$  when the robot is in the ‘straight upward’ configuration. [Please, make clean drawings and return the sheet with your name written on it.]



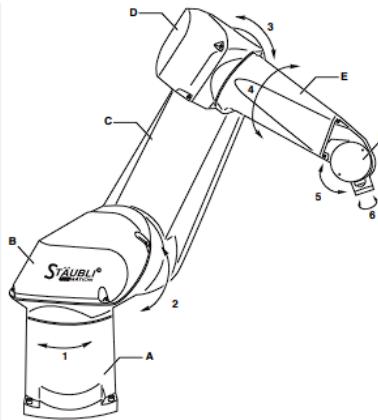
Staubli RX 160 – Assignment of frames according to the given DH table

	$\alpha_i$	$a_i$	$\gamma_i$	$\delta_i$	$\theta_i$
1	$\pi/2$	$d_1 > 0$	$d_1 > 0$	$\theta_1 = 0$	
2	0	$a_2 > 0$	$\theta_2 > 0$		
3	$\pi/2$	0	$\theta_3 = 0$		
4	0	$d_4 > 0$	$\theta_4 > 0$		
5	$\pi/2$	0	$\theta_5 = 0$		
6	0	$d_6 < 0$	$\theta_6 < 0$		

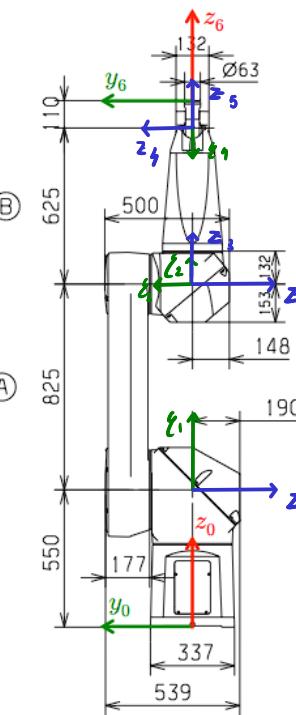
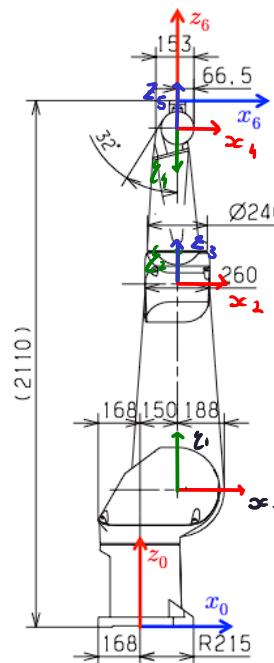
view from the right side  
the DH convention: nominally 200 mm

## Stäubli RX 160 – Assignment of frames according to the given DH table

Name:



$i$	$\alpha_i$	$a_i$	$d_i$	$\theta_i$
1	$\pi/2$	$a_1 > 0$	$d_1 > 0$	$q_1 = 0$
2	0	$a_2 > 0$	0	$q_2$
3	$\pi/2$	0	0	$q_3$
4	$\pi/2$	0	$d_4 > 0$	$q_4$
5	$-\pi/2$	0	0	$q_5$
6	0	0	$d_6 > 0$	$q_6 = 0$



*Robotics 1 Midterm classroom test November 24, 2017*

Exercise 4 [5 points]

The orientations of two right-handed frames  $RF_A$  and  $RF_B$  with respect to a third right-handed frame  $RF_0$  (all having the same origin) are specified, respectively, by the rotation matrices

$${}^0\mathbf{R}_A = \begin{pmatrix} \frac{3}{4} & \sqrt{\frac{3}{8}} & -\frac{1}{4} \\ -\sqrt{\frac{3}{8}} & \frac{1}{2} & -\sqrt{\frac{3}{8}} \\ -\frac{1}{4} & \sqrt{\frac{3}{8}} & \frac{3}{4} \end{pmatrix} \quad \text{and} \quad {}^0\mathbf{R}_B = \begin{pmatrix} \frac{1}{\sqrt{2}} & 0 & -\frac{1}{\sqrt{2}} \\ 0 & 1 & 0 \\ \frac{1}{\sqrt{2}} & 0 & \frac{1}{\sqrt{2}} \end{pmatrix}.$$

Determine, if possible, a unit vector  $\mathbf{r}$  and an angle  $\theta < 0$  such that the axis-angle rotation matrix  $\mathbf{R}(\mathbf{r}, \theta)$  provides the orientation of the frame  $RF_B$  with respect to the frame  $RF_A$ .

I have to calculate  ${}^A\mathbf{R}_B = {}^0\mathbf{R}_A^T {}^0\mathbf{R}_B =$

$$\begin{bmatrix} 0.35 & -0.61 & -0.7 \\ 0.86 & 0.5 & 0 \\ 0.35 & -0.61 & 0.7 \end{bmatrix}$$

only positive  
↑

$$\text{Since } \text{trace } \mathbf{R}(\mathbf{r}, \theta) = 1 + 2\cos\theta \Rightarrow 1.55 = 1 + 2\cos\theta \Rightarrow \cos\theta = 0.275 \Rightarrow \sin\theta = \pm 0.96 \Rightarrow -0.96$$

$$\Rightarrow \theta = -1.29$$

$$\text{Since } \mathbf{r} = \frac{1}{2\sin\theta} \begin{bmatrix} R_{32} - R_{23} \\ R_{13} - R_{31} \\ R_{21} - R_{12} \end{bmatrix} \Rightarrow \mathbf{r} = -0.52 \cdot \begin{bmatrix} -0.61 \\ -1.05 \\ 1.47 \end{bmatrix} = \begin{bmatrix} 0.3172 \\ 0.546 \\ -0.76 \end{bmatrix}$$

#### Exercise 4

The relative orientation of frame  $RF_B$  with respect to frame  $RF_A$  is expressed by the rotation matrix

$${}^A\mathbf{R}_B = {}^0\mathbf{R}_A^T \cdot {}^0\mathbf{R}_B = \begin{pmatrix} \frac{1}{2\sqrt{2}} & -\sqrt{\frac{3}{8}} & -\frac{1}{\sqrt{2}} \\ -\frac{\sqrt{3}}{2} & \frac{1}{2} & 0 \\ \frac{1}{2\sqrt{2}} & -\sqrt{\frac{3}{8}} & \frac{1}{\sqrt{2}} \end{pmatrix} = \begin{pmatrix} 0.3536 & -0.6124 & -0.7071 \\ 0.8660 & 0.5 & 0 \\ 0.3536 & -0.6124 & 0.7071 \end{pmatrix},$$

$\overset{\curvearrowright}{R_{12}}$   
 $\overset{\curvearrowleft}{R_{21}} \Rightarrow R_{21} - R_{12} = 1.1124$

whose elements will be denoted by  $R_{ij}$ . Therefore, the equation  $\mathbf{R}(\mathbf{r}, \theta) = {}^A\mathbf{R}_B$  should be solved for  $\mathbf{r}$  and  $\theta$ , using the inverse mapping of the axis-angle representation. Since

$$\sin \theta = \pm \frac{1}{2} \sqrt{(R_{12} - R_{21})^2 + (R_{13} - R_{31})^2 + (R_{23} - R_{32})^2} = \pm 0.9599 \neq 0, \quad (1)$$

II  
 $\frac{2781}{2500}$

the problem at hand is regular, and two distinct solutions can be found depending on the choice of the + or - sign in the expression of  $\sin \theta$ . From

$$\cos \theta = \frac{1}{2} (R_{11} + R_{22} + R_{33} - 1) = 0.2803,$$

taking the - sign in (1) will yield a solution angle  $\theta < 0$ , as requested. Thus

$$\theta = \text{ATAN2}\{-0.9599, 0.2803\} = -1.2867 \text{ [rad]} = -73.72^\circ$$

and

$$\mathbf{r} = \frac{1}{2 \sin \theta} \begin{pmatrix} R_{32} - R_{23} \\ R_{13} - R_{31} \\ R_{21} - R_{12} \end{pmatrix} = \begin{pmatrix} 0.3190 \\ 0.5525 \\ -0.7701 \end{pmatrix}.$$

\*\*\*\*\*

$\frac{1}{2 \sin \theta} = -0.5208$        $\hookrightarrow \frac{1}{2 \sin \theta} (R_{21} - R_{12}) =$   
 $(-0.5208) \cdot \frac{2781}{2500} = -0.5793$