

Since I have already taken the midterm, I will only be completing the exercises related to the second part of the course (from differential kinematics onwards).

Question #5 [all students]

The direct kinematics and the initial configuration of a planar RP robot are given by

$$\mathbf{p} = \mathbf{f}(\mathbf{q}) = \begin{pmatrix} q_2 \cos q_1 \\ q_2 \sin q_1 \end{pmatrix}, \quad \mathbf{q}^{(0)} = \begin{pmatrix} \pi/4 \\ \varepsilon \end{pmatrix},$$

where $0 < \varepsilon \ll 1$ is a very small number. Given the following desired end-effector positions,

$$\mathbf{p}_{d,I} = \begin{pmatrix} -1 \\ 1 \end{pmatrix} \quad \text{and} \quad \mathbf{p}_{d,II} = \begin{pmatrix} 1 \\ 1 \end{pmatrix},$$

compute the first iteration (i.e., $\mathbf{q}^{(1)}$) of a Newton method and of a Gradient method for solving the two inverse kinematics problems. Discuss what happens in each of the four cases when $\varepsilon \rightarrow 0$.

the newton method use the following rule:

$$\mathbf{q}^{k+1} = \mathbf{q}^k + \mathbf{J}^{-1}(\mathbf{q}^k) (\mathbf{p}_d - \mathbf{f}_r(\mathbf{q}^k)) \quad \text{so, for } \mathbf{p}_{d,I} :$$

$$\mathbf{f}_r(\mathbf{q}^0) = \varepsilon \frac{\sqrt{2}}{2} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$\mathbf{J} = \begin{pmatrix} -q_2 s_1 & c_1 \\ q_2 c_1 & s_1 \end{pmatrix} \Rightarrow \mathbf{J}(\mathbf{q}^0) = \begin{pmatrix} -\varepsilon \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \\ \varepsilon \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \end{pmatrix}$$

$$\Leftrightarrow \mathbf{J}^{-1}(\mathbf{q}^0) = \begin{pmatrix} -\frac{1}{\varepsilon \sqrt{2}} & -\frac{1}{\varepsilon \sqrt{2}} \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \end{pmatrix}$$

$$\mathbf{q}_I^{(1)} = \begin{pmatrix} \pi/4 \\ \varepsilon \end{pmatrix} + \begin{pmatrix} -\frac{1}{\varepsilon \sqrt{2}} & -\frac{1}{\varepsilon \sqrt{2}} \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \end{pmatrix} \begin{pmatrix} 1 - \varepsilon \frac{\sqrt{2}}{2} \\ 1 - \varepsilon \frac{\sqrt{2}}{2} \end{pmatrix} = \begin{pmatrix} \frac{1}{3\sqrt{2}} + \frac{\varepsilon \sqrt{2}}{2\varepsilon \sqrt{2}} - \frac{1}{3\sqrt{2}} + \frac{\varepsilon \sqrt{2}}{2\varepsilon \sqrt{2}} + \frac{\pi}{4} \\ \frac{2}{\sqrt{2}} \end{pmatrix} = \begin{pmatrix} \frac{\pi}{4} + \frac{1}{2} \\ \frac{2}{\sqrt{2}} \end{pmatrix}$$

For $\mathbf{p}_{d,I} \Rightarrow$

$$\mathbf{q}_{II}^{(1)} = \begin{pmatrix} \pi/4 \\ \varepsilon \end{pmatrix} + \begin{pmatrix} -\frac{1}{\varepsilon \sqrt{2}} & -\frac{1}{\varepsilon \sqrt{2}} \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \end{pmatrix} \begin{pmatrix} 1 - \varepsilon \frac{\sqrt{2}}{2} \\ 1 - \varepsilon \frac{\sqrt{2}}{2} \end{pmatrix} = \begin{pmatrix} -\frac{2}{\varepsilon \sqrt{2}} + 1 + \frac{\pi}{4} \\ \frac{2}{\sqrt{2}} \end{pmatrix} \Rightarrow \lim_{\varepsilon \rightarrow 0} \mathbf{q}_{II}^{(1)} = \begin{pmatrix} \infty \\ \frac{2}{\sqrt{2}} \end{pmatrix} \text{ undefined } \mathbf{f}(\mathbf{q})$$

the gradient have the rule:

$$\mathbf{q}^{k+1} = \mathbf{q}^k + \alpha \mathbf{J}^T(\mathbf{q}^k) (\mathbf{r}_d - \mathbf{f}_r(\mathbf{q}^k))$$

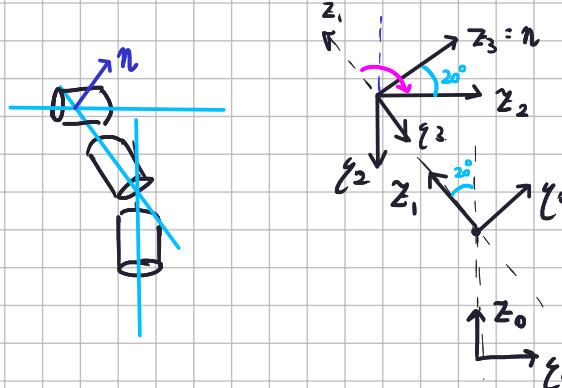
$$\mathbf{q}_I^{(1)} = \begin{pmatrix} \pi/2 \\ \varepsilon \end{pmatrix} + \alpha \begin{pmatrix} -\varepsilon \frac{\sqrt{2}}{2} & \varepsilon \frac{\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \end{pmatrix} \begin{pmatrix} 1 - \varepsilon \frac{\sqrt{2}}{2} \\ 1 - \varepsilon \frac{\sqrt{2}}{2} \end{pmatrix} = \begin{pmatrix} \pi/2 \\ \varepsilon \end{pmatrix} + \alpha \begin{pmatrix} \varepsilon \frac{\sqrt{2}}{2} \\ 0 \end{pmatrix} = \begin{pmatrix} \pi/2 + \alpha \varepsilon \sqrt{2} \\ \varepsilon \end{pmatrix} \underset{\varepsilon \rightarrow 0}{\lim} \mathbf{q}_I^{(1)} = \begin{pmatrix} \pi/2 \\ 0 \end{pmatrix} \Rightarrow \mathbf{f}(\mathbf{q}) = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

$$\mathbf{q}_{II}^{(1)} = \begin{pmatrix} \pi/2 \\ \varepsilon \end{pmatrix} + \alpha \begin{pmatrix} -\varepsilon \frac{\sqrt{2}}{2} & \varepsilon \frac{\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \end{pmatrix} \begin{pmatrix} 1 - \varepsilon \frac{\sqrt{2}}{2} \\ 1 - \varepsilon \frac{\sqrt{2}}{2} \end{pmatrix} = \begin{pmatrix} \pi/2 \\ \varepsilon \end{pmatrix} + \alpha \begin{pmatrix} 0 \\ \frac{\sqrt{2}}{2} - \varepsilon \end{pmatrix} = \begin{pmatrix} \pi/2 \\ \alpha \sqrt{2} \end{pmatrix}$$

Question #6 [all students]

The 3R robotic device in Fig. 3 has joint axes that intersect two by two. The second joint axis is inclined by an angle $\delta \approx 20^\circ$. This structure is mainly intended for pointing the final axis n at a moving target in 3D. Provide the explicit expression of the square angular part $J_A(q)$ of the geometric Jacobian of this robot. Find the singularities, if any, of the mapping $\omega = J_A(q)\dot{q}$. Compute the relation between $\dot{q} \in \mathbb{R}^3$ and the time derivative \dot{n} of the pointing axis.

We notice that, since we are interested only in the angular part, we can ignore the link lengths.



Joints	α_i	α_i	d_i	θ_i	
1	20°	0	0	q_1	$\cos(20^\circ) = 0.939$
2	-110°	0	0	q_2	$\sin(20^\circ) = 0.342$
3	20°	0	0	q_3	$\cos(-110^\circ) = -0.342$
					$\sin(-110^\circ) = -0.939$

$${}^0 R_1 = \begin{pmatrix} C_1 & -0.939S_1 & 0.342S_1 \\ S_1 & 0.939C_1 & -0.342C_1 \\ 0 & 0.342 & 0.939 \end{pmatrix} \quad {}^1 R_2 = \begin{pmatrix} C_2 & 0.342S_2 & -0.939S_2 \\ S_2 & -0.342C_2 & 0.939C_2 \\ 0 & -0.939 & -0.342 \end{pmatrix}$$

$${}^2 R_3 = \begin{pmatrix} C_3 & -0.939S_3 & 0.342S_3 \\ S_3 & 0.939C_3 & -0.342C_3 \\ 0 & 0.342 & 0.939 \end{pmatrix}$$

\Rightarrow

$${}^0 R_2 = \begin{pmatrix} C_1 & -0.939S_1 & 0.342S_1 \\ S_1 & 0.939C_1 & -0.342C_1 \\ 0 & 0.342 & 0.939 \end{pmatrix} \begin{pmatrix} C_2 & 0.342S_2 & -0.939S_2 \\ S_2 & -0.342C_2 & 0.939C_2 \\ 0 & -0.939 & -0.342 \end{pmatrix} \quad \text{I denote } a = 0.939 \\ b = 0.342$$

$$\begin{pmatrix} C_1C_2 - 2S_1S_2 & bC_1S_2 + dS_1C_2 - 2bS_3 & -2C_1S_2 - 2^2S_1C_2 - b^2S_3 \\ S_1C_2 + 2C_1S_2 & bS_1S_2 - dC_1C_2 + dC_1 & -2S_1S_2 + 2^2C_1C_2 + b^2C_1 \\ bS_2 & -b^2C_2 - 2^2 & dC_2 - d \end{pmatrix} \quad d = 2b = 0.321138$$

$\downarrow z_1$

${}^0 R_3 = {}^0 R_2 {}^2 R_3$; take only the last column

$$Z_2 = \begin{pmatrix} C_1C_2 - 2S_1S_2 & bC_1S_2 + dS_1C_2 - 2bS_3 & -2C_1S_2 - 2^2S_1C_2 - b^2S_3 \\ S_1C_2 + 2C_1S_2 & bS_1S_2 - dC_1C_2 + dC_1 & -2S_1S_2 + 2^2C_1C_2 + b^2C_1 \\ bS_2 & -b^2C_2 - 2^2 & dC_2 - d \end{pmatrix} \begin{pmatrix} 0.342S_3 \\ -0.342C_3 \\ 0.939 \end{pmatrix}$$

$$\begin{pmatrix} bS_3(C_1C_2 - 2S_1S_2) - bC_3(bC_1S_2 + dS_1C_2 - 2bS_3) + 2(-2C_1S_2 - 2^2S_1C_2 - b^2S_3) \\ bS_3(S_1C_2 + 2C_1S_2) - bC_3(bS_1S_2 - dC_1C_2 + dC_1) + 2(-2S_1S_2 + 2^2C_1C_2 + b^2C_1) \\ b^2S_2S_3 - bC_3(-b^2C_2 - 2^2) + 2d(C_2 - d) \end{pmatrix} \Rightarrow J_A = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \begin{pmatrix} Z_1 \\ Z_2 \end{pmatrix}$$

Question #8 [all students]

The planar 3R robot with unitary link lengths shown in Fig. 4 is initially in the configuration $q_{in} = (-\pi/9, 11\pi/18, -\pi/4)$. Commanded by a joint velocity $\dot{q}(t)$ that uses feedback from the current $q(t)$, the robot should perform a self-motion so as to reach asymptotically the final value $q_{3,fin} = -\pi/2$ for the third joint, while keeping the position of its end-effector always at the same initial point P_{in} . Verify first that such task is feasible. Design then a control scheme that completes the task in a robust way, i.e., by rejecting also possible transient errors and without encountering any singular situation in which the control law is ill conditioned. Hint: Use an approach based on joint space decomposition.

First, I need P_{in} . $q_1 + q_2 = \frac{\pi}{2}$ $q_1 + q_2 + q_3 = \frac{\pi}{4}$

$$P_{in} = f_r(q_{in}) = \begin{pmatrix} 1.6467 \\ 1.365 \\ \frac{\pi}{4} \end{pmatrix}. \text{ I check if exists } q^* \text{ s.t. } q_3^* = -\frac{\pi}{2} \text{ and } f(q^*) = P_{in}$$

$$\left\{ \begin{array}{l} C_1 + C_{12} + \cos(q_1 + q_2 - \frac{\pi}{2}) = 1.6467 \\ S_1 + S_{12} + \sin(q_1 + q_2 - \frac{\pi}{2}) = 1.365 \\ q_1 + q_2 - \frac{\pi}{2} = \frac{\pi}{3} \end{array} \right. \Rightarrow \left\{ \begin{array}{l} q_1 + q_2 + q_3 = \frac{\pi}{4} \\ q_1 + q_2 = q_1 + \frac{3}{4}\pi - q_1 = \frac{3}{4}\pi \\ q_2 = \frac{3}{4}\pi - q_1 \end{array} \right. q_2 = 2.385$$

$$\Rightarrow \left\{ \begin{array}{l} C_1 = 1.6467 \\ S_1 + \sqrt{2} = 1.365 \end{array} \right. \left\{ \begin{array}{l} C_1 = 1.6467 \\ S_1 = -0.049 \end{array} \right. \Rightarrow q_1 = 2.385 \times 2 \left\{ -0.049, 1.6467 \right\} = -0.020 \frac{\pi}{4}$$

\rightarrow it's possible

The error on the joint space is $e_3 = -\frac{\pi}{2} - q_3$

The error on the task space is $e_p = P_{in} - p$.

$$\Rightarrow \dot{q} = \alpha \begin{pmatrix} 0 \\ 0 \\ q_3 + \frac{\pi}{2} \end{pmatrix}$$

On the task space:

$$\dot{p} = -K e_p \quad \text{with } e_p = p - P_{in}$$

$$\dot{J} \dot{q} = -K e_p \Rightarrow \dot{q} = -J^* K e_p$$

$$\dot{e}_p: \dot{p} = J \dot{q} = -J J^* K e_p = -K e_p \Rightarrow \lim_{t \rightarrow \infty} e_p = 0$$

$$\Rightarrow \dot{q} = \beta (-J^* K e_p) + \alpha \begin{pmatrix} 0 \\ 0 \\ q_3 + \frac{\pi}{2} \end{pmatrix} \quad \alpha \cdot \beta = 1$$

$$\Rightarrow \dot{q} = -\beta J^* e_p + \alpha \begin{pmatrix} 0 \\ 0 \\ q_3 + \frac{\pi}{2} \end{pmatrix} = -\beta J^* (p - P_{in}) + \alpha \begin{pmatrix} 0 \\ 0 \\ q_3 + \frac{\pi}{2} \end{pmatrix}$$

