

**Solving** 

a)

$$T^{2} = \frac{4\pi^{2}}{KM} \cdot a^{3};$$

$$a = \sqrt[3]{\frac{T^{2}KM}{4\pi^{2}}};$$

$$T = 4,2 \text{ ani} = 4,2 \cdot 365 \cdot 24 \cdot 3600 \text{ s};$$

$$a = \sqrt[3]{\frac{(4,2 \cdot 365 \cdot 24 \cdot 36)^{2} \cdot 10^{4} \cdot 6,67 \cdot 10^{-11} \cdot 9,1 \cdot 10^{30}}{4 \cdot (3,14)^{2}}} \text{ m};$$

$$a = \sqrt[3]{\frac{(4,2 \cdot 365 \cdot 24 \cdot 36)^{3} \cdot 10^{4} \cdot 6,67 \cdot 10^{-11} \cdot 9,1 \cdot 10^{30}}{4,2 \cdot 365 \cdot 24 \cdot 36 \cdot 4 \cdot (3,14)^{2}}} \text{ m};$$

$$a = 4,2 \cdot 365 \cdot 24 \cdot 36 \cdot \sqrt[3]{\frac{10^{4} \cdot 6,67 \cdot 10^{-11} \cdot 9,1 \cdot 10^{30}}{4,2 \cdot 365 \cdot 24 \cdot 36 \cdot 4 \cdot (3,14)^{2}}} \text{ m};$$

$$a \approx 4,2 \cdot 365 \cdot 24 \cdot 36 \cdot \sqrt[3]{\frac{6,67 \cdot 9,1 \cdot 10^{22}}{4,2 \cdot 365 \cdot 24 \cdot 36 \cdot 4}} \text{ m};$$

$$a \approx 1324512 \cdot \sqrt[3]{\frac{60697000 \cdot 10^{15}}{5298048}} \text{ m};$$

$$a \approx 1324512 \cdot \sqrt[3]{11,4564836} \cdot 10^{5} \text{ m}; \sqrt[3]{11,4564836} \approx 2,25;$$

$$a \approx 1324512 \cdot 2,25 \cdot 10^{5} \text{ m} = 2980152 \cdot 10^{5} \text{ m};$$

$$a \approx 3 \cdot 10^{11} \text{ m} = 3 \cdot 10^{8} \text{ km};$$

$$e = \sqrt{1 - \frac{b^{2}}{a^{2}}}; b = a \cdot \sqrt{1 - e^{2}};$$

$$b = 3 \cdot 10^{8} \cdot \sqrt{1 - (0,15)^{2}} \text{ km}; b \approx 2,96 \cdot 10^{8} \text{ km};$$

$$c = \sqrt{a^{2} - b^{2}} \approx 0,488 \cdot 10^{8} \text{ km};$$

$$r_{min} = a - c = 2,512 \cdot 10^{8} \text{ km};$$

$$r_{min} = a + c = 3,488 \cdot 10^{8} \text{ km}.$$

b.

$$Q_{\text{Soare}} = \frac{E_{\text{emis,Soare}}}{tS_{\text{Soare}}} = \sigma T_S^4,$$

unde  $\sigma$  este o constantă;



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$$rac{E_{
m emis,Soare}}{t} = P_{
m emis,Soare}; \ \sigma T_{
m S}^4 = rac{P_{
m emis,Soare}}{4\pi R_{
m S}^2}; \ P_{
m emis,Soare} = \sigma T_{
m S}^4 4\pi R_{
m S}^2.$$

Densitatea fluxului energetic al Soarelui, la distanța  $r_{AS}$  față de acesta (acolo unde se află Asteroidul), însemnează energia tuturor radiațiilor emise de Soare, care traversează unitatea de arie a unei suprafețe, sub incidență normală, în unitatea de timp, adică:

$$\phi_{\text{Soare},r_{\text{AS}}} = \frac{E_{\text{emis},\text{Soare}}}{St} = \frac{\frac{E_{\text{emis},\text{Soare}}}{t}}{S} = \frac{P_{\text{emis},\text{Soare}}}{S} = \frac{P_{\text{emis},\text{Soare}}}{4\pi r_{\text{AS}}^2};$$

$$\phi_{\text{Soare},r_{\text{AS}}} = \frac{\sigma T_{\text{S}}^4 4\pi R_{\text{S}}^2}{4\pi r_{\text{AS}}^2}.$$

Semisfera asteroidului expusă radiațiilor solare este echivalentă cu un disc plan circular, având raza  $R_A$  și aria suprafeței  $\pi R_A^2$ , așezat perpendicular pe direcția Soare – Asteroid, astfel încât fluxul radiațiilor solare incidente, F, la nivelul Asteroidului (adică energia solară incidentă le nivelul Asteroidului, în unitatea de timp), este:

$$\begin{split} F_{\text{incident}} &= \phi_{\text{Soare},r_{\text{AS}}} \cdot \pi R_{\text{A}}^2 = P_{\text{incident}} = P_{\text{emis},\text{Soare}}; \\ F_{\text{incident}} &= \frac{\sigma T_{\text{S}}^4 \, 4\pi R_{\text{S}}^2}{4\pi r_{\text{AS}}^2} \cdot \pi R_{\text{A}}^2 = P_{\text{incident}}; \\ \alpha &= \frac{P_{\text{reflectat},\text{Asteroid}}}{P_{\text{incident}}}; \\ P_{\text{reflectat},\text{Asteroid}} &= \alpha P_{\text{incident}} = \alpha \frac{\sigma T_{\text{S}}^4 \, 4\pi R_{\text{S}}^2}{4\pi r_{\text{AS}}^2} \cdot \pi R_{\text{A}}^2. \end{split}$$

În acord cu desenul din figura alăturată, ecuația bilanțului energetic al procesului analizat este:

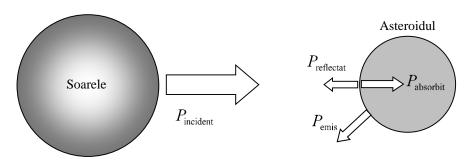


Fig.

$$\begin{split} P_{\text{incident,Asteroid}} &= P_{\text{reflectat,Asteroid}} + P_{\text{absorbitAsteroid}}; \\ \frac{\sigma T_{\text{S}}^4 4 \pi R_{\text{S}}^2}{4 \pi r_{\text{AS}}^2} \cdot \pi R_{\text{A}}^2 &= \alpha \, \frac{\sigma T_{\text{S}}^4 4 \pi R_{\text{S}}^2}{4 \pi r_{\text{AS}}^2} \cdot \pi R_{\text{A}}^2 + P_{\text{absorbitAsteroid}}. \end{split}$$



$$P_{\text{emis,Asteroid}} = \sigma T_{\text{A}}^4 \cdot 4\pi R_{\text{A}}^2$$
.

$$\begin{split} \text{Stationary} \\ P_{\text{emis,Asteroid}} &= P_{\text{absorbitAsteroid}} = \sigma T_{\text{A}}^{4} \cdot 4\pi R_{\text{A}}^{2}, \\ \frac{\sigma T_{\text{S}}^{4} 4\pi R_{\text{S}}^{2}}{4\pi r_{\text{AS}}^{2}} \cdot \pi R_{\text{A}}^{2} &= \alpha \frac{\sigma T_{\text{S}}^{4} 4\pi R_{\text{S}}^{2}}{4\pi r_{\text{AS}}^{2}} \cdot \pi R_{\text{A}}^{2} + \sigma T_{\text{A}}^{4} \cdot 4\pi R_{\text{A}}^{2}; \\ \frac{T_{\text{S}}^{4} R_{\text{S}}^{2}}{4r_{\text{AS}}^{2}} &= \alpha \frac{T_{\text{S}}^{4} R_{\text{S}}^{2}}{4r_{\text{AS}}^{2}} + T_{\text{A}}^{4}; \\ \left(1 - \alpha\right) \frac{T_{\text{S}}^{4} R_{\text{S}}^{2}}{4r_{\text{AS}}^{2}} &= T_{\text{A}}^{4}; \\ T_{\text{A}} &= T_{\text{S}} \cdot \sqrt[4]{1 - \alpha} \cdot \sqrt{\frac{R_{\text{S}}}{2r_{\text{A}}}}, \end{split}$$

Rezults

$$\begin{split} T_{\rm A,max} &= T_{\rm S} \cdot \sqrt[4]{1-\alpha} \cdot \sqrt{\frac{R_{\rm S}}{2r_{\rm AS,min}}}; \\ T_{\rm S} &= 6000~{\rm K};~R_{\rm S} \approx 7 \cdot 10^5~{\rm km};~r_{\rm AS,min} = 2{,}512 \cdot 10^8~{\rm km};~\alpha \approx 0{,}2; \\ T_{\rm A,max} &= 6000~{\rm K} \cdot \sqrt[4]{1-0{,}2} \cdot \sqrt{\frac{7 \cdot 10^5~{\rm km}}{2 \cdot 2{,}512 \cdot 10^8~{\rm km}}}; \\ &\sqrt[4]{1-0{,}2} = \sqrt[4]{0{,}8} \approx 0{,}945; \\ 6000 \cdot \sqrt{\frac{7 \cdot 10^5}{2 \cdot 2{,}512 \cdot 10^8}} = \sqrt{\frac{36 \cdot 7 \cdot 10^3}{2 \cdot 2{,}512}} \approx 223{,}96; \\ T_{\rm A,max} &= 223{,}96 \cdot 0{,}945~{\rm K} \approx 211{,}6422~{\rm K}, \end{split}$$

When the astheroid is at perihelium;

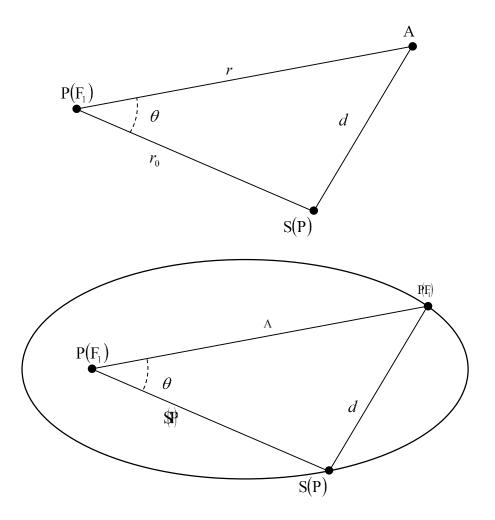
$$\begin{split} T_{\rm A,min} &= T_{\rm S} \cdot \sqrt[4]{1-\alpha} \cdot \sqrt{\frac{R_{\rm S}}{2r_{\rm AS,max}}}; \\ T_{\rm S} &= 6000~{\rm K};~R_{\rm S} \approx 7 \cdot 10^5~{\rm km};~r_{\rm AS,max} = 3,488 \cdot 10^8~{\rm km};~\alpha \approx 0,2; \\ T_{\rm A,min} &= 6000~{\rm K} \cdot \sqrt[4]{1-0,2} \cdot \sqrt{\frac{7 \cdot 10^5~{\rm km}}{2 \cdot 3,488 \cdot 10^8~{\rm km}}}; \\ &\sqrt[4]{1-0,2} = \sqrt[4]{0,8} \approx 0,945; \\ 6000 \cdot \sqrt{\frac{7 \cdot 10^5}{2 \cdot 3,488 \cdot 10^8}} = \sqrt{\frac{36 \cdot 7 \cdot 10^3}{2 \cdot 3,488}} \approx 190,06; \\ T_{\rm A,min} &= 190,06 \cdot 0,945~{\rm K} \approx 179,60~{\rm K}, \end{split}$$



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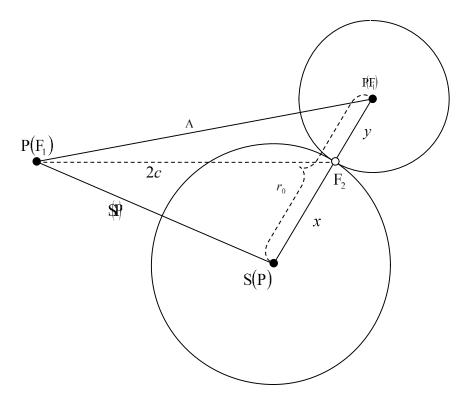
When the astheroid is at aphelium.





page





$$r_{0} + x = 2a; r + y = 2a;$$

$$r_{0} + x = r + y;$$

$$x - y = r - r_{0} = \Delta r;$$

$$x + y = d;$$

$$x = \frac{1}{2}(d + \Delta r); y = \frac{1}{2}(d - \Delta r);$$

$$a = \frac{1}{2}\left[r_{0} + \frac{1}{2}(d + \Delta r)\right] = \frac{1}{2}\left[r_{0} + \frac{1}{2}(d + r - r_{0})\right];$$

$$a = \frac{1}{2}\left[r_{0} + \frac{1}{2}(d + r) - \frac{r_{0}}{2}\right] = \frac{1}{4}(r_{0} + r + d);$$

$$2a = \frac{1}{2}(r_{0} + r + d);$$

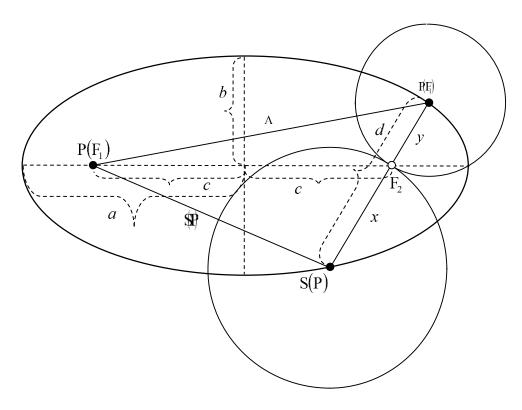
$$F_{1}F_{2} = 2c;$$

$$c = \sqrt{a^{2} - b^{2}}; b = \sqrt{a^{2} - c^{2}};$$

$$e = \sqrt{1 - \frac{b^{2}}{a^{2}}}; e = \frac{r_{\text{max}} - r_{\text{min}}}{r_{\text{max}} + r_{\text{min}}};$$

$$r_{\text{min}} = a(1 - e); r_{\text{max}} = a(1 + e); r_{\text{min}} + r_{\text{max}} = 2a.$$

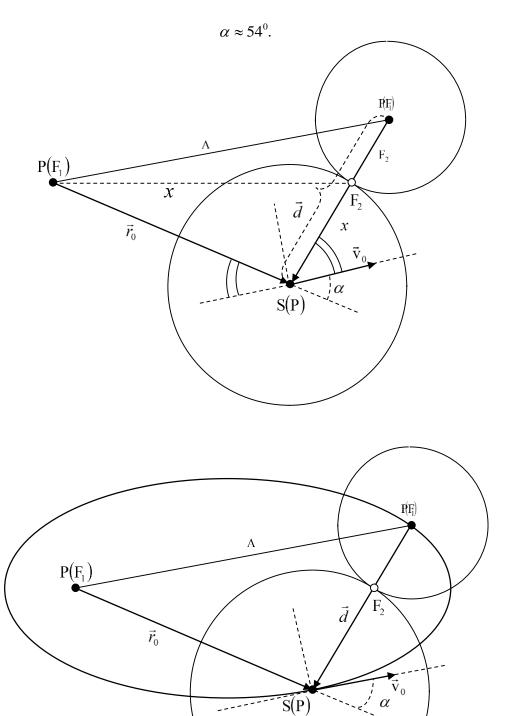




Din măsurători efectuate pe desen și din calcule, rezultă:

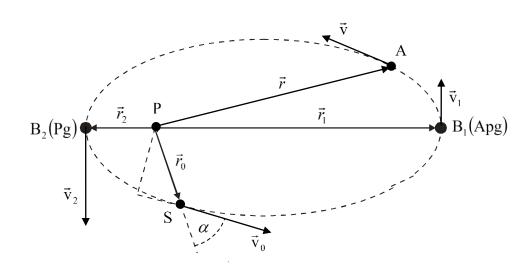
$$r_0 = 133 \text{ mm}; \ r = 153 \text{ mm}; \ d = 115 \text{ mm};$$
 
$$\Delta r = r - r_0 = 20 \text{ mm};$$
 
$$x = 67,5 \text{ mm}; \ y = 47,5 \text{ mm};$$
 
$$2a = 200 \text{ mm}; \ a = 100 \text{ mm};$$
 
$$2b = 148 \text{ mm}; \ b = 74 \text{ mm};$$
 
$$2c = 134 \text{ mm}; \ c = 67 \text{ mm};$$
 
$$e \approx 0,67; \ r_{\min} = 33 \text{ mm}; \ r_{\max} = 167 \text{ mm};$$
 
$$r_{\text{real}} = 30000 \text{ km}; \ r = 153 \text{ mm};$$
 
$$S = \frac{r_{\text{real}}}{r} = \frac{30000}{153} \frac{\text{km}}{\text{mm}};$$
 
$$r_{0,\text{real}} = r_0 S \approx 26078,43 \text{ km}; \ d_{\text{real}} = dS \approx 22549 \text{ km};$$
 
$$x_{\text{real}} = xS \approx 13235,3 \text{ km}; \ y_{\text{real}} = yS \approx 9313,7 \text{ km};$$
 
$$a_{\text{real}} \approx 19607,84 \text{ km}; \ b_{\text{real}} \approx 14509,80 \text{ km}; \ c_{\text{real}} \approx 13137,25 \text{ km};$$
 
$$r_{\text{min,real}} \approx 6470,58 \text{ km}; \ r_{\text{max,real}} \approx 32745,09 \text{ km}.$$

b)





c)



:

$$\frac{\mathbf{v}_{1,2}^2}{2} - K \frac{M}{r_{1,2}} = \frac{\mathbf{v}_0^2}{2} - K \frac{M}{r_0};$$

$$v_{1,2} r_{1,2} = v_0 r_0 \sin \alpha;$$

$$\left(\frac{\mathbf{v}_0^2}{2} - K\frac{M}{r_0}\right) r_{1,2}^2 + KMr_{1,2} - \frac{1}{2}\mathbf{v}_0^2 r_0^2 \sin^2 \alpha = 0.$$

 $r_1$  Apogee

r<sub>2</sub>, Perigee,:

$$a = \frac{1}{2}(r_1 + r_2),$$

$$a = \frac{KMr_0}{2KM - r_0 v_0^2},$$

relație independent of  $\,\alpha$  relationship for  $\,\vec{v}_{\scriptscriptstyle\,0}$ 

$$v_0 = \sqrt{KM \frac{2a_{\text{real}} - r_{0,\text{real}}}{a_{\text{real}}r_{0,\text{real}}}} = \sqrt{\frac{KM}{r_{0,\text{real}}} \cdot \frac{2a_{\text{real}} - r_{0,\text{real}}}{a_{\text{real}}}},$$

$$S = \frac{30000 \text{ km}}{153 \text{ mm}};$$

$$r_{0,\text{real}} = 133 \text{ mm} \cdot \frac{30000 \text{ km}}{153 \text{ mm}} \approx 26078 \text{ km};$$

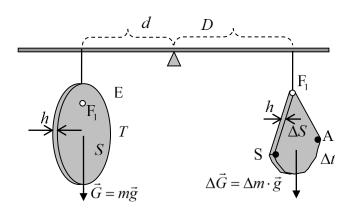
$$M = 6 \cdot 10^{24} \text{ kg}; \quad K = 6,67 \cdot 10^{-11} \text{ Nm}^2 \text{kg}^{-2};$$



$$\begin{aligned} 2a_{\text{real}} &= 200 \text{ mm} \cdot S; \\ \mathbf{v}_0 &= \sqrt{\frac{6,67 \cdot 10^{-11} \text{ Nm}^2 \text{kg}^{-2} \cdot 6 \cdot 10^{24} \text{ kg}}{26078 \cdot 10^3 \text{ m}} \cdot \frac{200 - 133}{100}}; \\ \mathbf{v}_0 &= \sqrt{\frac{6,67 \cdot 10^{-11} \cdot 6 \cdot 10^{24}}{26078 \cdot 10^3} \cdot \frac{200 - 133}{100}} \frac{\text{m}}{\text{s}} \approx 3200 \frac{\text{m}}{\text{s}} = 3,2 \frac{\text{km}}{\text{s}}. \end{aligned}$$

d) 
$$T^{2} = \frac{4\pi^{2}}{K(M+m)} \cdot a_{\text{real}}^{3}; \ m << M; \ T^{2} = \frac{4\pi^{2}}{KM} \cdot a_{\text{real}}^{3};$$
$$M = 6 \cdot 10^{24} \text{ kg}; \ K = 6,67 \cdot 10^{-11} \text{ Nm}^{2} \text{kg}^{-2};$$
$$S = \frac{30000 \text{ km}}{153 \text{ mm};}$$
$$a_{\text{real}} = 100 \text{ mm} \cdot S \approx 19608 \text{ km};$$
$$T = 2\pi \sqrt{\frac{a_{\text{real}}^{3}}{KM}} = 2 \cdot 3,14 \sqrt{\frac{19608^{3} \cdot 10^{9}}{6,67 \cdot 10^{-11} \cdot 6 \cdot 10^{24}}} \text{ s} \approx 27240 \text{ s};$$
$$T \approx 454 \text{ min} \approx 7,56 \text{ h}.$$

The system has to be done



$$G \cdot d = \Delta G \cdot D; \ mg \cdot d = \Delta m \cdot g \cdot D;$$
  

$$m \cdot d = \Delta m \cdot D; \ \rho \cdot V \cdot d = \rho \cdot \Delta V \cdot D;$$
  

$$V \cdot d = \Delta V \cdot D; \ S \cdot h \cdot d = \Delta S \cdot h \cdot D;$$
  

$$S \cdot d = \Delta S \cdot D; \ \frac{\Delta S}{S} = \frac{d}{D}.$$

According to the second Keppler law:

$$T$$
..... $S$ ;



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$$\Delta t \dots \Delta S;$$

$$\Delta t = \frac{\Delta S}{S} \cdot T = \frac{d}{D} \cdot T,$$

D	d	T	$\Delta t$
26 cm	11 cm	7,56 h	3,19 h

e) Measurements ao a wire along the elipse sector between S and A:

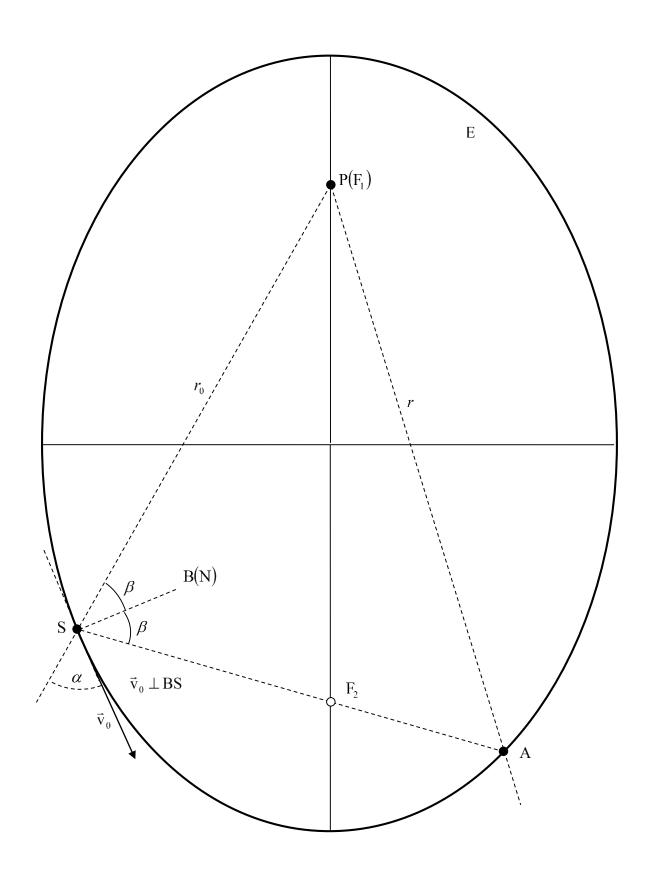
$$l_{\rm SA} = 135 \, \rm mm;$$

$$l_{\rm SA,real} = l_{\rm SA} \cdot S = 135 \; {\rm mm} \cdot \frac{30000 \, {\rm km}}{153 \, {\rm mm}} \approx 26470{,}58 \, {\rm km}.$$





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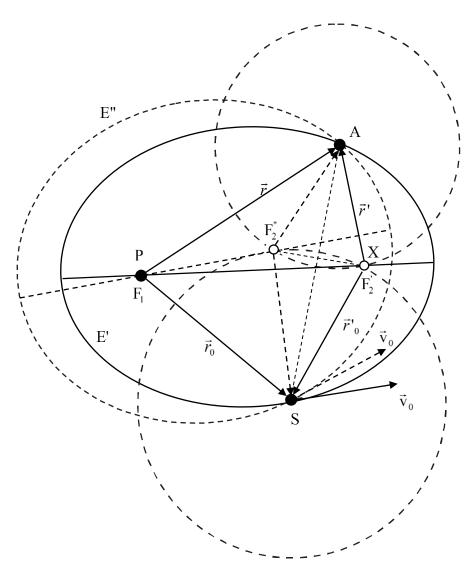
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B.

a) The 2 elipses have a common focar so the injection point will go in the same point  $\vec{r}_0$ , with initial velocity,  $v_0$ . The both elipses semiaxes are identical:

$$a = \frac{KMr_0}{2KM - r_0 \mathbf{v}_0^2}.$$

 $2c_1 \neq 2c_2$ ;,  $2b_1 \neq 2b_2$ ;  $e_1 \neq e_2$ .



PS + SX = PA + AX = 170 mm,



AAfter localizing the focuses of the elipses the axes can be drawn.

$$r_0 + r_0' = 2a$$
;  $r + r' = 2a$ .

Measuring  $r_0$  and  $r_0$ , or r and r', can be calculated:

$$S = \frac{30000 \text{ km}}{107 \text{ mm}};$$

$$r_0 = 95 \text{ mm} \cdot S; \ r'_0 = 75 \text{ mm} \cdot S;$$

$$r = 107 \text{ mm} \cdot S; \ r' = 63 \text{ mm} \cdot S;$$

$$2a = 170 \text{ mm} \cdot S \approx 47664 \text{ km};$$

$$a = \frac{1}{2} (r_0 + r'_0) = \frac{1}{2} (r + r') = 85 \text{ mm} \cdot S = 85 \text{ mm} \cdot \frac{30000 \text{ km}}{107 \text{ mm}} \approx 23832 \text{ km}.$$

$$F_1 F'_2 = 2c_1; \ b_1 = \sqrt{a^2 - c_1^2};$$

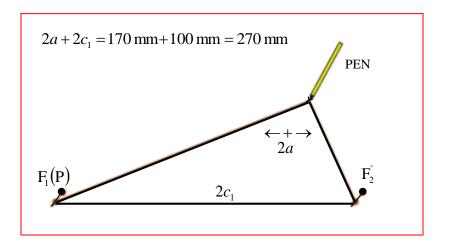
$$2c_1 = 100 \text{ mm} \cdot S; \ c_1 = 50 \text{ mm} \cdot S;$$

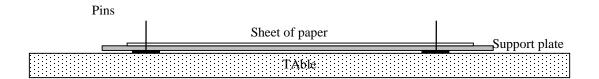
$$b_1 \approx 69 \text{ mm} \cdot S \approx 19346 \text{ km};$$

$$F_1 F'_2 = 2c_2; \ b_2 = \sqrt{a^2 - c_2^2};$$

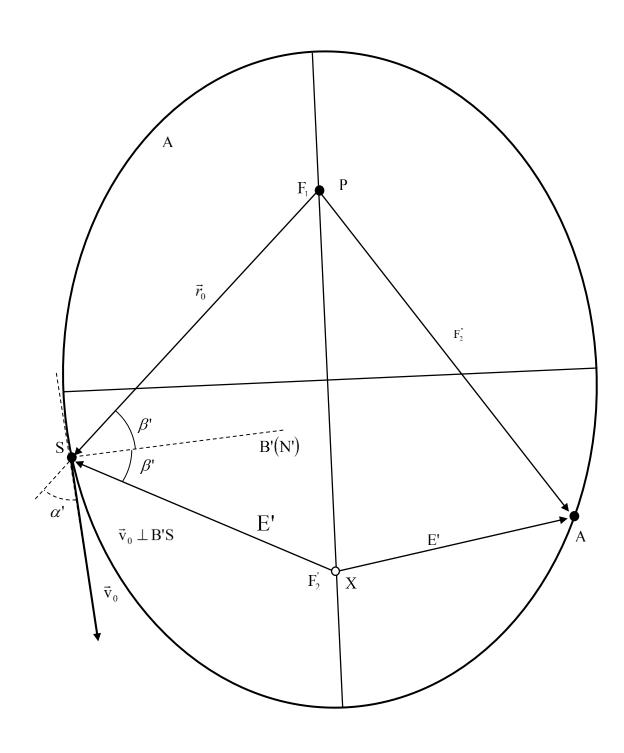
$$2c_2 = 60 \text{ mm} \cdot S; \ c_2 = 30 \text{ mm} \cdot S;$$

$$b_2 \approx 80 \text{ mm} \cdot S \approx 22430 \text{ km}.$$



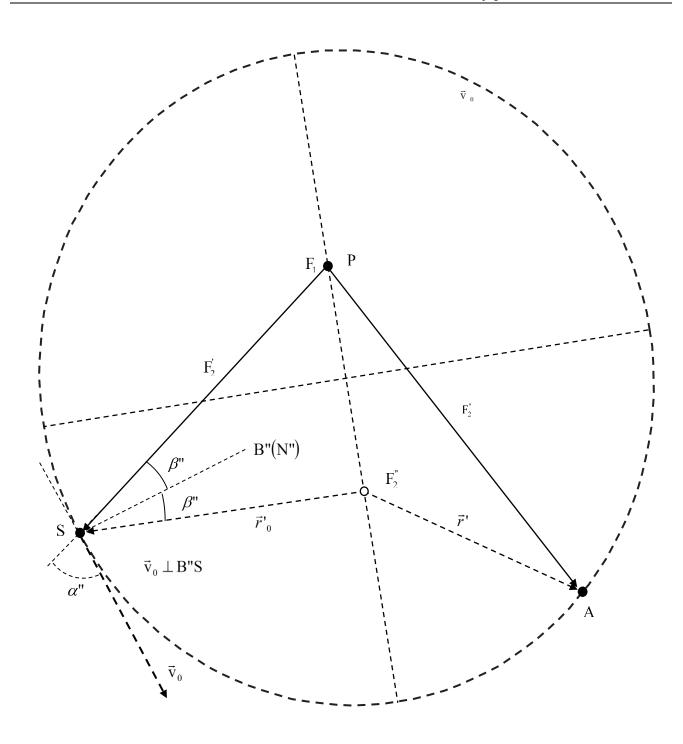








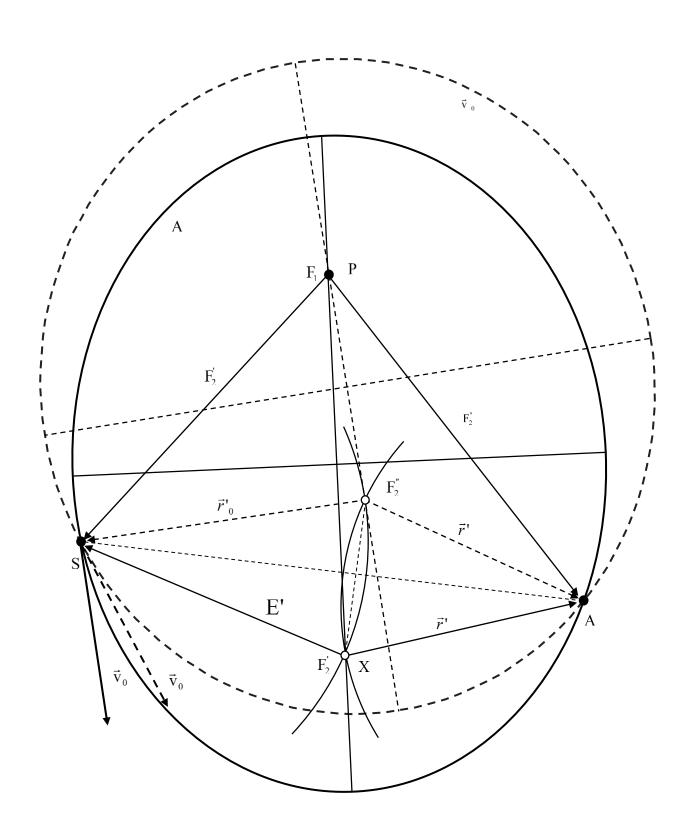
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b) 
$$\alpha' \approx 50^{\circ}; \ \alpha'' \approx 70^{\circ}.$$

c) 
$$v_{0} = \sqrt{KM \frac{2a_{\text{real}} - r_{0,\text{real}}}{a_{\text{real}} r_{0,\text{real}}}} = \sqrt{\frac{KM}{r_{0,\text{real}}}} \cdot \frac{2a - r_{0}}{a};$$

$$r_{0} = 95 \text{ mm} \cdot S; S = \frac{30000 \text{ km}}{107 \text{ mm}};$$

$$r_{0,\text{real}} \approx 26636 \text{ km}; 2a_{\text{real}} = 170 \text{ mm} \cdot S;$$

$$a = 85 \text{ mm} \cdot S; \ a_{\text{real}} = 23831,77 \text{ km};$$

$$2a = 170 \text{ mm}; \ 2a_{\text{real}} = 47663,55 \text{ km};$$

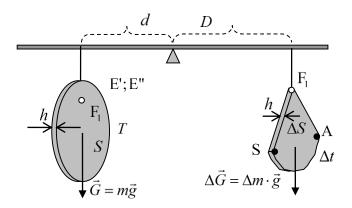
$$v_{0} = \sqrt{\frac{6,67 \cdot 10^{-11} \text{ Nm}^{2} \text{kg}^{-2} \cdot 6 \cdot 10^{24} \text{ kg}}{26636 \cdot 10^{3} \text{ m}}} \cdot \frac{170 - 95}{85};$$

$$v_{0} = \sqrt{\frac{6,67 \cdot 10^{-11} \cdot 6 \cdot 10^{24}}{26636 \cdot 10^{3}}} \cdot \frac{170 - 95}{85} \cdot \frac{\text{m}}{\text{s}} \approx 3640 \cdot \frac{\text{m}}{\text{s}} \approx 3,6 \cdot \frac{\text{km}}{\text{s}}.$$

d) 
$$T^{2} = \frac{4\pi^{2}}{K(M+m)} \cdot a_{\text{real}}^{3}; \ m << M; \ T^{2} = \frac{4\pi^{2}}{KM} \cdot a_{\text{real}}^{3};$$
$$M = 6 \cdot 10^{24} \text{ kg}; \ K = 6,67 \cdot 10^{-11} \text{ Nm}^{2} \text{kg}^{-2};$$
$$a_{\text{real}} = 23832 \text{ km};$$
$$T = 2\pi \sqrt{\frac{a_{\text{real}}^{3}}{KM}} = 2 \cdot 3,14 \sqrt{\frac{23832^{3} \cdot 10^{9}}{6,67 \cdot 10^{-11} \cdot 6 \cdot 10^{24}}} \text{ s} \approx 36523 \text{ s};$$
$$T \approx 608 \text{ min} \approx 10 \text{ h}.$$

For each of two elipses the device has to be used





$$G \cdot d = \Delta G \cdot D; \ mg \cdot d = \Delta m \cdot g \cdot D;$$

$$m \cdot d = \Delta m \cdot D; \ \rho \cdot V \cdot d = \rho \cdot \Delta V \cdot D;$$

$$V \cdot d = \Delta V \cdot D; \ S \cdot h \cdot d = \Delta S \cdot h \cdot D;$$

$$S \cdot d = \Delta S \cdot D; \ \frac{\Delta S}{S} = \frac{d}{D}.$$

$$T$$
...... $S$ ;  
 $\Delta t$ .... $\Delta S$ ;  

$$\Delta t = \frac{\Delta S}{S} \cdot T = \frac{d}{D} \cdot T;$$

For the projectile on elipse E', from measurements:

$$d = 12.8 \text{ cm}; D = 23 \text{ cm}; T = 10 \text{ h};$$

$$\Delta t = \frac{d}{D} \cdot T = \frac{12.8 \text{ cm}}{23 \text{ cm}} \cdot 10 \text{ h} \approx 5.56 \text{ h};$$

$$d = 10.7 \text{ cm}; D = 25 \text{ cm};$$

$$\Delta \tau = \frac{10.7 \text{ cm}}{25 \text{ cm}} \cdot 10 \text{ h} \approx 4.28 \text{ h};$$

$$\Delta t = T - \Delta \tau = 5.72 \text{ h};$$

$$\Delta t = \frac{5.56 \text{ h} + 5.72 \text{ h}}{2} = 5.64 \text{ h}.$$

For the projectile on elipse E", from measurements:

$$d = 8.5 \text{ cm}; D = 22.3 \text{ cm}; T = 10 \text{ h};$$
  

$$\Delta t = \frac{d}{D} \cdot T = \frac{8.5 \text{ cm}}{22.3 \text{ cm}} \cdot 10 \text{ h} \approx 3.81 \text{ h};$$
  
 $d = 13.5 \text{ cm}; D = 23 \text{ cm};$   

$$\Delta \tau = \frac{13.5 \text{ cm}}{23 \text{ cm}} \cdot 10 \text{ h} \approx 5.86 \text{ h};$$

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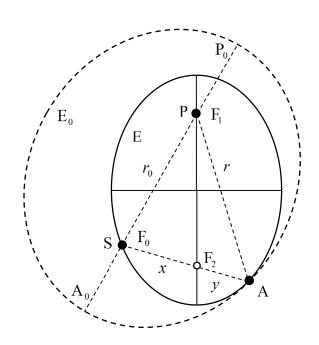
$$\Delta t = T - \Delta \tau = 4,14 \text{ h};$$
  

$$\Delta t = \frac{3,81 \text{ h} + 4,14 \text{ h}}{2} = 3,975 \text{ h}.$$

e) Modeling one wire on each sector SA:

$$l'_{\rm SA} = 183 \,\mathrm{mm}; \ l'_{\rm SA,real} = l'_{\rm SA}S = 183 \,\mathrm{mm} \cdot \frac{30000 \,\mathrm{km}}{107 \,\mathrm{mm}} \approx 51308,41 \,\mathrm{km};$$
  
 $l''_{\rm SA} = 156 \,\mathrm{mm}; \ l''_{\rm SA,real} = l'_{\rm SA}S = 156 \,\mathrm{mm} \cdot \frac{30000 \,\mathrm{km}}{107 \,\mathrm{mm}} \approx 43738,31 \,\mathrm{km}.$ 

**C.** a)



$$\begin{aligned} \text{PA} + \text{AS} &= 2a_0; \\ r + x + y &= 2a_0; \\ r_0 + x &= 2a; \ r + y = 2a: \\ 2a + 2a - r_0 &= 2a_0; \\ 2a_0 &= 4a - r_0, \end{aligned}$$

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$$2a_0 = 222 \text{ mm} - 74 \text{ mm} = 148 \text{ mm};$$
 
$$S = \frac{30000 \text{ km}}{85 \text{ mm}};$$
 
$$2a_{0,\text{real}} = 2a_0 S = 148 \text{ mm} \cdot \frac{30000 \text{ km}}{85 \text{ mm}} \approx 52235,29 \text{ km},$$

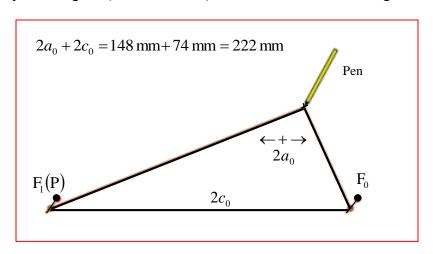
a-A:

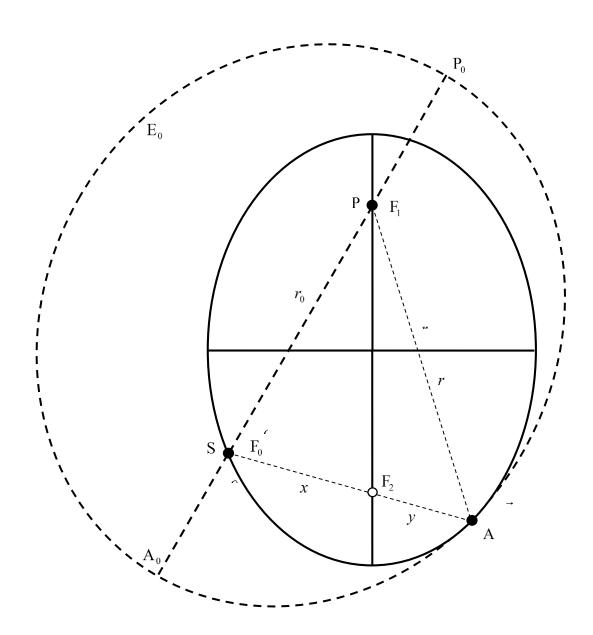
$$2a_0 = 400 \text{ mm} - 133 \text{ mm} = 267 \text{ mm};$$
 
$$S = \frac{30000 \text{ km}}{153 \text{ mm}};$$
 
$$2a_{0,\text{real}} = 2a_0 S = 267 \text{ mm} \cdot \frac{30000 \text{ km}}{153 \text{ mm}} \approx 52352,94 \text{ km}; \ a_{0,\text{real}} = 26176,47 \text{ km}.$$

Security elipse.

$$\begin{split} 2c_{0,\text{real}} &= r_{0,\text{real}} = 26078 \, \text{km}; \ c_{0,\text{real}} = 13039 \, \text{km}; \\ b_{0,\text{real}} &= \sqrt{a_{0,\text{real}}^2 - c_{0,\text{real}}^2} \approx 22697,\!84 \, \text{km}; \\ e_0 &= \sqrt{1 - \frac{b_{0,\text{real}}^2}{a_{0,\text{real}}^2}} \approx 0,\!5. \end{split}$$

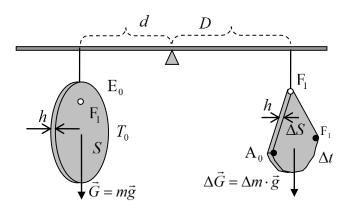
Conturul elipsei de siguranță se trasează așa cum indică desenul din figura alăturată.





- b) c)





$$G \cdot d = \Delta G \cdot D; \ mg \cdot d = \Delta m \cdot g \cdot D;$$
  

$$m \cdot d = \Delta m \cdot D; \ \rho \cdot V \cdot d = \rho \cdot \Delta V \cdot D;$$
  

$$V \cdot d = \Delta V \cdot D; \ S \cdot h \cdot d = \Delta S \cdot h \cdot D;$$
  

$$S \cdot d = \Delta S \cdot D; \ \frac{\Delta S}{S} = \frac{d}{D}.$$

$$M = 6 \cdot 10^{24} \text{ kg}; \quad K = 6.67 \cdot 10^{-11} \text{ Nm}^2 \text{kg}^{-2};$$

$$T_0 = 2\pi \cdot a_{0,\text{real}} \cdot \sqrt{\frac{a_{0,\text{real}}}{KM}} \approx 42042,42 \text{ s};$$

$$T_0 \approx 700,7 \text{ min } \approx 11,67 \text{ h}.$$

$$d = 8.5 \text{ cm}; D = 23 \text{ cm}; T = 11.67 \text{ h};$$
  

$$\Delta \tau = \frac{d}{D} \cdot T = \frac{8.5 \text{ cm}}{23 \text{ cm}} \cdot 11.67 \text{ h} \approx 4.31 \text{ h};$$

$$\Delta t = T_0 - \Delta \tau = 7.36 \text{ h},$$