

**Job No.:** Ray Gosling

**Address:** 282 Te Puke Quarry Road, Te Puke, New Zealand

**Date:** 8/10/2022

**Latitude:** -37.766413

**Longitude:** 176.280136

**Elevation:** 16.5 m

### General Input

Roof Live Load	0.25 KPa	Roof Dead Load	0.25 KPa	Roof Live Point Load	1.1 Kn
Snow Zone	N0	Ground Snow Load	0 KPa	Roof Snow Load	0 KPa
Earthquake Zone	2	Subsoil Category	D	Exposure Zone	C
Importance Level	1	Ultimate wind & Earthquake ARI	100 Years	Max Height	3.6 m
Wind Region	NZ1	Terrain Category	2.0	Design Wind Speed	39.16 m/s
Wind Pressure	0.92 KPa	Lee Zone	NO	Ultimate Snow ARI	50 Years
Wind Category	High				

Note: Wind lateral loads are governing over Earthquake loads, So only wind loads are considered in calculations

### Pressure Coefficients and Pressures

Shed Type = Mono Open

For roof  $C_{p,i} = -0.67$

For roof  $C_{p,e}$  from 0 m To 1.65 m  $C_{p,e} = -0.94$   $p_e = -0.78$  KPa  $p_{net} = -1.44$  KPa

For roof  $C_{p,e}$  from 1.65 m To 3.30 m  $C_{p,e} = -0.88$   $p_e = -0.73$  KPa  $p_{net} = -1.39$  KPa

For wall Windward  $C_{p,i} = 0.66$  side Wall  $C_{p,i} = -0.6$

For wall Windward and Leeward  $C_{p,e}$  from 0 m To 6 m  $C_{p,e} = 0.7$   $p_e = 0.58$  KPa  $p_{net} = -1.07$  KPa

For side wall  $C_{p,e}$  from 0 m To 3.30 m  $C_{p,e} =$   $p_e = -0.54$  KPa  $p_{net} = -1.20$  KPa

Maximum Upward pressure used in roof member Design = 1.44 KPa

Maximum Downward pressure used in roof member Design = 0.75 KPa

Maximum Wall pressure used in Design = 1.20 KPa

Maximum Racking pressure used in Design = 1 KPa

### Design Summary

#### Purlin Design

Purlin Spacing = 900 mm

Purlin Span = 3800 mm

Try Purlin 200x50 SG8 Dry

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Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1    K1 Medium term = 0.8    K1 Long term = 0.6    K4 =1    K5 =1    K8 Downward =1.00

K8 Upward =0.53    S1 Downward =11.27    S1 Upward =23.16

Shear Capacity of timber =3 MPa    Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

M <sub>1.35D</sub>	0.55 Kn-m	Capacity	2.39 Kn-m	Passing Percentage	<b>434.55 %</b>
M <sub>1.2D+1.5L 1.2D+S<sub>n</sub> 1.2D+W<sub>n</sub>D<sub>n</sub></sub>	1.71 Kn-m	Capacity	3.18 Kn-m	Passing Percentage	<b>185.96 %</b>
M <sub>0.9D-W<sub>n</sub>Up</sub>	-1.97 Kn-m	Capacity	-2.10 Kn-m	Passing Percentage	<b>106.60 %</b>
V <sub>1.35D</sub>	0.58 Kn	Capacity	9.65 Kn	Passing Percentage	<b>1663.79 %</b>
V <sub>1.2D+1.5L 1.2D+S<sub>n</sub> 1.2D+W<sub>n</sub>D<sub>n</sub></sub>	1.80 Kn	Capacity	12.86 Kn	Passing Percentage	<b>714.44 %</b>
V <sub>0.9D-W<sub>n</sub>Up</sub>	-2.08 Kn	Capacity	-16.08 Kn	Passing Percentage	<b>773.08 %</b>

**Deflections**

Modulus of Elasticity = 8000 MPa NZS3603 Amt 4, Table 2.3 considering at least 4 members acting together

k<sub>2</sub> for Long Term Loads = 2

Deflection under Dead and Live Load = 5.50 mm      Limit by AS1170.0 Table C1 Span/250 = 15.20 mm

Deflection under Dead and Service Wind = 8.02 mm      Limit by AS1170.0 Table C1 Span/120 = 31.67 mm

**Reactions**

Maximum downward =1.80 kn    Maximum upward = -2.08 kn

Number of Blocking = 0    if 0 then no blocking required, if 1 then one midspan blocking required

**Rafter Design Internal**

Internal Rafter Load Width = 4000 mm      Internal Rafter Span = 5850 mm      Try Rafter 2x240x45 LVL13

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1    K1 Medium term = 0.8    K1 Long term = 0.6    K4 =1    K5 =1    K8 Downward =1.00

K8 Upward =1.00    S1 Downward =6.71    S1 Upward =6.71

Shear Capacity of timber =5.3 MPa    Bending Capacity of timber =48 MPa NZS3603 Amt 4, table 2.3

**Capacity Checks**

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M1.35D	5.78 Kn-m	Capacity	22.34 Kn-m	Passing Percentage	<b>386.51 %</b>
M1.2D+1.5L 1.2D+Sn 1.2D+WnDn	17.97 Kn-m	Capacity	29.8 Kn-m	Passing Percentage	<b>165.83 %</b>
M0.9D-WnUp	-20.79 Kn-m	Capacity	-37.24 Kn-m	Passing Percentage	<b>179.12 %</b>
V1.35D	3.95 Kn	Capacity	36.82 Kn	Passing Percentage	<b>932.15 %</b>
V1.2D+1.5L 1.2D+Sn 1.2D+WnDn	12.29 Kn	Capacity	49.08 Kn	Passing Percentage	<b>399.35 %</b>
V0.9D-WnUp	-14.22 Kn	Capacity	-61.36 Kn	Passing Percentage	<b>431.50 %</b>

**Deflections**

Modulus of Elasticity = 11000 MPa NZS3603 Amt 4, Table 2.3

k2 for Long Term Loads = 2

Deflection under Dead and Live Load = 15.98 mm      Limit by AS1170.0 Table C1 Span/250 = 24.00 mm

Deflection under Dead and Service Wind = 25.895 mm      Limit by AS1170.0 Table C1 Span/120 = 50.00 mm

**Reactions**

Maximum downward = 12.29 kn    Maximum upward = -14.22 kn

**Rafter to Pole Connection check**

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J2 Joint Group for Pole = J5

Minimum Bolt edge, end and spacing for Load perpendicular to grains = 60 mm

Factor of Safety = 0.7

For Perpendicular to grain loading

K11 = 12.6 fpj = 22.7 Mpa for Rafter with effective thickness = 90 mm

For Parallel to grain loading

K11 = 2.0 fcj = 36.1 Mpa for Pole with effective thickness = 100 mm

Capacity under short term loads = 29.11 Kn > -14.22 Kn

**Rafter Design External**

External Rafter Load Width = 2000 mm      External Rafter Span = 5830 mm      Try Rafter 240x45 LVL13

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet

condition after installation)

K1 Short term = 1    K1 Medium term = 0.8    K1 Long term = 0.6    K4 = 1    K5 = 1    K8 Downward = 0.94

K8 Upward = 0.94    S1 Downward = 13.82    S1 Upward = 13.82

Shear Capacity of timber = 5.3 MPa    Bending Capacity of timber = 48 MPa NZS3603 Amt 4, table 2.3

#### Capacity Checks

M <sub>1.35D</sub>	2.87 Kn-m	Capacity	9.72 Kn-m	Passing Percentage	<b>338.68 %</b>
M <sub>1.2D+1.5L 1.2D+S<sub>n</sub> 1.2D+W<sub>n</sub>D<sub>n</sub></sub>	8.92 Kn-m	Capacity	12.96 Kn-m	Passing Percentage	<b>145.29 %</b>
M <sub>0.9D-W<sub>n</sub>Up</sub>	-10.32 Kn-m	Capacity	-16.20 Kn-m	Passing Percentage	<b>156.98 %</b>
V <sub>1.35D</sub>	1.97 Kn	Capacity	18.41 Kn	Passing Percentage	<b>934.52 %</b>
V <sub>1.2D+1.5L 1.2D+S<sub>n</sub> 1.2D+W<sub>n</sub>D<sub>n</sub></sub>	6.12 Kn	Capacity	24.54 Kn	Passing Percentage	<b>400.98 %</b>
V <sub>0.9D-W<sub>n</sub>Up</sub>	-7.08 Kn	Capacity	-30.68 Kn	Passing Percentage	<b>433.33 %</b>

#### Deflections

Modulus of Elasticity = 11000 MPa NZS3603 Amt 4, Table 2.3

k<sub>2</sub> for Long Term Loads = 2

Deflection under Dead and Live Load = 17.76 mm    Limit by AS1170.0 Table C1 Span/250 = 24.00 mm

Deflection under Dead and Service Wind = 25.89 mm    Limit by AS1170.0 Table C1 Span/120 = 50.00 mm

#### Reactions

Maximum downward = 6.12 kn    Maximum upward = -7.08 kn

#### Rafter to Pole Connection check

Bolt Size = M12 Number of Bolts = 2

Calculations as per NZS 3603:1993 Amend 2005 clause 4.4

Joint Group for Rafters = J2 Joint Group for Pole = J5

Factor of Safety = 0.7

For Perpendicular to grain loading

K<sub>11</sub> = 12.6 f<sub>pj</sub> = 22.7 Mpa for Rafter with effective thickness = 45 mm

For Parallel to grain loading

K<sub>11</sub> = 2.0 f<sub>cj</sub> = 36.1 Mpa for Pole with effective thickness = 100 mm

Eccentric Load check

$V = \phi \times k_1 \times k_4 \times k_5 \times f_s \times b \times d_s \dots\dots\dots$  (Eq 4.12) = -30.05 kn > -7.08 Kn

Single Shear Capacity under short term loads = -14.56 Kn > -7.08 Kn

### Intermediate Design Sides

Intermediate Spacing = 3000 mm      Intermediate Span = 3150 mm      Try Intermediate 2x140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1    K4 =1    K5 =1    K8 Downward =1.00

K8 Upward =1.00    S1 Downward =10.36    S1 Upward =0.61

Shear Capacity of timber =3 MPa    Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

### Capacity Checks

$M_{Wind+Snow}$	2.23 Kn-m	Capacity	3.74 Kn-m	Passing Percentage	<b>167.71 %</b>
$V_{0.9D-WnUp}$	2.83 Kn-m	Capacity	20.26 Kn-m	Passing Percentage	<b>715.90 %</b>

### Deflections

Modulus of Elasticity = 5400 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 41.5 mm      Limit by AS1170.0 Table C1 Span/120 = 26.25 mm

### Reactions

Maximum = 2.83 kn

### Girt Design Front and Back

Girt's Spacing = 900 mm      Girt's Span = 4000 mm      Try Intermediate 140x45 SG8

Moisture Condition = Dry (Moisture in timber is less than 16% and timber does not remain in continuous wet condition after installation)

K1 Short term = 1    K4 =1    K5 =1    K8 Downward =1.00

K8 Upward =0.58    S1 Downward =10.36    S1 Upward =21.85

Shear Capacity of timber =3 MPa    Bending Capacity of timber =14 MPa NZS3603 Amt 4, table 2.3

### Capacity Checks

$M_{Wind+Snow}$	1.08 Kn-m	Capacity	1.09 Kn-m	Passing Percentage	<b>100.93 %</b>
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V <sub>0.9D-W<sub>n</sub>Up</sub>	1.08 Kn-m	Capacity	10.13 Kn-m	Passing Percentage	<b>937.96 %</b>
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### Deflections

Modulus of Elasticity = 8000 MPa NZS3603 Amt 4, Table 2.3

Deflection under Snow and Service Wind = 21.87 mm      Limit by AS1170.0 Table C1 Span/120 = 33.33 mm  
 Sag during installation = 16.05 mm

### Reactions

Maximum = 1.08 kn

### Middle Pole Design

#### Geometry

200 UNI H5	Dry Use	Height	3300 mm
Area	31400 mm <sup>2</sup>	As	23550 mm <sup>2</sup>
I <sub>x</sub>	78500000 mm <sup>4</sup>	Z <sub>x</sub>	785000 mm <sup>3</sup>
I <sub>y</sub>	78500000 mm <sup>4</sup>	Z <sub>y</sub>	785000 mm <sup>3</sup>
Lateral Restraint	3300 mm c/c		

#### Loads

Total Area over Pole = 12 m<sup>2</sup>

Dead	3.00 Kn	Live	3.00 Kn
Wind	9.00 Kn	Snow	0.00 Kn
Moment wind	Kn-m		
Phi	0.8	K <sub>8</sub>	0.84
K <sub>1</sub> snow	0.8	K <sub>1</sub> Dead	0.6
K <sub>1</sub> wind	1		

#### Material

Shaving	Steaming	Normal	Dry Use
f <sub>b</sub> =	34.325 MPa	f <sub>s</sub> =	2.96 MPa
f <sub>c</sub> =	18 MPa	f <sub>p</sub> =	7.2 MPa
f <sub>t</sub> =	20.75 MPa	E =	8793 MPa

#### Capacities

PhiN <sub>Cx</sub> Wind	378.83 Kn	PhiM <sub>Nx</sub> Wind	18.06 Kn-m	PhiV <sub>Nx</sub> Wind	55.77 Kn
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PhiNcx Dead      227.30 Kn      PhiMnx Dead      10.84 Kn-m      PhiVnx Dead      33.46 Kn

#### Checks

$$(M_x/\Phi M_{nx}) + (N/\Phi N_{cx}) = 0.58 < 1 \text{ OK}$$

$$(M_x/\Phi M_{nx})^2 + (N/\Phi N_{cx}) = 0.33 < 1 \text{ OK}$$

$$\text{Deflection at top under service lateral loads} = 23.45 \text{ mm} < 44.00 \text{ mm}$$

### Drained Lateral Strength of Middle pile in cohesionless soils Free Head short pile

#### Soil Properties

Gamma    18 Kn/m<sup>3</sup>      Friction angle    30 deg    Cohesion    0 Kn/m<sup>3</sup>

$$K_0 = (1 - \sin(30)) / (1 + \sin(30))$$

$$K_p = (1 + \sin(30)) / (1 - \sin(30))$$

#### Geometry For Middle Bay Pole

Ds =      600 mm      Pile Diameter  
L =      1500 mm      Pile embedment length  
f1 =      2700 mm      Distance at which the shear force is applied  
f2 =      0 mm      Distance of top soil at rest pressure

#### Loads

Moment Wind =      9.70 Kn-m  
Shear Wind =      3.59 Kn

#### Pile Properties

Safety Factory      0.55  
Hu =      7.16 Kn      Ultimate Lateral Strength of the Pile, Short pile  
Mu =      11.65 Kn-m      Ultimate Moment Capacity of Pile

#### Checks

$$\text{Applied Forces/Capacities} = 0.83 < 1 \text{ OK}$$

### End Pole Design

#### Geometry For End Bay Pole

Ds =      600 mm      Pile Diameter

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L =	1500 mm	Pile embedment length
f1 =	2700 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

**Loads**

Total Area over Pole = 6 m<sup>2</sup>

Moment Wind =	4.85 Kn-m
Shear Wind =	1.80 Kn

**Pile Properties**

Safety Factory	0.55	
Hu =	7.16 Kn	Ultimate Lateral Strength of the Pile, Short pile
Mu =	11.65 Kn-m	Ultimate Moment Capacity of Pile

**Checks**

Applied Forces/Capacities = 0.42 < 1 OK

**Drained Lateral Strength of End pile in cohesionless soils Free Head short pile**

**Soil Properties**

Gamma	18 Kn/m <sup>3</sup>	Friction angle	30 deg	Cohesion	0 Kn/m <sup>3</sup>
K0 =	$(1 - \sin(30)) / (1 + \sin(30))$				
Kp =	$(1 + \sin(30)) / (1 - \sin(30))$				

**Geometry For End Bay Pole**

Ds =	600 mm	Pile Diameter
L =	1500 mm	Pile embedment length
f1 =	2700 mm	Distance at which the shear force is applied
f2 =	0 mm	Distance of top soil at rest pressure

**Loads**

Moment Wind =	4.85 Kn-m
Shear Wind =	1.80 Kn

**Pile Properties**

Safety Factory	0.55
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Hu = 7.16 Kn Ultimate Lateral Strength of the Pile, Short pile  
Mu = 11.65 Kn-m Ultimate Moment Capacity of Pile

#### Checks

Applied Forces/Capacities =  $0.42 < 1$  OK

#### Uplift Check

Density of Concrete = 24 Kn/m<sup>3</sup>

Density of Timber Pole = 5 Kn/m<sup>3</sup>

Due to cast in place pile, the surface interaction between soil and pile will be rough thus angle of friction between both is taken equal to soil angle of internal friction

Ks (Lateral Earth Pressure Coefficient) for cast into place concrete piles = 1.5

Formula to calculate Skin Friction = Safety factor (0.55) x Density of Soil(18) x Height of Pile(1500) x Ks(1.5) x  $\tan(30)$  x  $\pi$  x Dia of Pile(0.6) x Height of Pile(1500)

Skin Friction = 18.17 Kn

Weight of Pile + Pile Skin Friction = 22.31 Kn

Uplift on one Pile = 14.58 Kn

Uplift is ok