

# Wettability control by DLC coated nanowire topography

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Received 29 November 2010, in final form 18 January 2011

Published 22 February 2011

Online at [stacks.iop.org/Nano/22/135302](http://stacks.iop.org/Nano/22/135302)

## Abstract

Here we have developed a convenient method to fabricate wettability controllable surfaces that can be applied to various nanostructured surfaces with complex shapes for different industrial needs. Diamond-like carbon (DLC) films were synthesized on titanium substrate with a nanowire structured surface using plasma immersion ion implantation and deposition (PIII&D). The nanostructure of the DLC films was characterized by field emission scanning electron microscopy and found to grow in a rippling layer-by-layer manner. Raman spectroscopy was used to investigate the different bonding presented in the DLC films. To determine the wettability of the samples, water contact angles were measured and found to vary in the range of 50°–141°. The results indicated that it was critical to construct a proper surface topography for high hydrophobicity, while suitable  $I_D/I_G$  and  $sp^2/sp^3$  ratios of the DLC films had a minor contribution. Superhydrophobicity could be achieved by further CF<sub>4</sub> implantation on suitably structured DLC films and was attributed to the existence of fluorine. In order to maintain the nanostructure during CF<sub>4</sub> implantation, it was favorable to pre-deposit an appropriate carbon content on the nanostructure, as a nanostructure with low carbon content would be deformed during CF<sub>4</sub> implantation due to local accumulation of surface charge and the following discharge resulting from the low conductivity.

## 1. Introduction

Wettability is one of the most important surface properties of materials, especially when the materials are used for self-cleaning [1], water–oil separation [2], no-loss transport of microdroplets [3], and biomedical applications such as blood-contacting medical devices [4, 5] and cell-contacting hard tissue implants [6, 7]. Wettability can be characterized by measuring the contact angle of a static water droplet on the material surface. Usually a surface with a contact angle less than 90° is defined as hydrophilic, while one with a contact angle greater than 90° is defined as hydrophobic. Wettability of material is mainly dominated by its surface topography and chemical composition, and can be modified by altering these two dominant factors. In recent years, high

hydrophobic surfaces, especially superhydrophobic surfaces with water contact angle greater than 150°, have gained much attention for both fundamental research and practical applications [8]. Inspired by the ‘lotus effect’, a fascinating phenomenon in Nature which has the attractive ability of self-cleaning, researchers concluded that there were mainly two ways to obtain high hydrophobic surfaces: by constructing a proper nanostructure on a hydrophobic surface, or by coating a nanostructure surface with a layer of low surface energy material [9, 10]. Titanium is widely used in the fields of the aerospace industry, the chemical industry, machinery and medical devices. Tailoring the wettability of titanium by surface treatment has both theoretical and practical importance, as wettability is closely related to other surface properties, such as photocatalytic activity [11], adhesive bonding [12], blood compatibility [13] and cell function [14]. Researches have indicated that titanium based implants with a hydrophobic

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surface would strongly affect the initial interaction with the physiological environment, including the adhesion of some specific proteins [15, 16], behavior regulation of different cells [17–19], etc, which might enable us to tailor the biological responses to titanium surface according to different clinical needs.

Diamond-like carbon (DLC) is an effective material to modify the surface wettability by lowering the surface energy and altering the surface topography [20–22]. DLC films can be constructed onto smooth surfaces as well as various nanostructured surfaces, such as ablation aluminum substrate and electroplating copper foil [23], via many available techniques such as chemical vapor deposition (CVD) [20], electrodeposition [22], cathodic micro-arc discharge [24], and magnetron sputtering [21]. The combination of the structural variability of carbon and the controlled structured surface will surely extend the application of the wettability alterable carbon thin films, as wettability and surface structure are both considered as important factors for materials.

Plasma immersion ion implantation and deposition (PIII&D) is one of the surface modification technologies which has been frequently used to prepare surface coatings in the last few decades. PIII&D is suitable for modifying large-scale surface and multifaceted devices with complex 3D shapes due to its non-line-of-sight nature, which makes it superior to the line-of-sight methods such as conventional beam-line ion implantation and CVD. Carbon thin films synthesized by PIII&D have attracted much attention in recent years and were reported to have potential applications as biomedical materials [6, 25–27], precision bearing materials in the aerospace industry [28], and other materials which required superior hardness, corrosion resistance and wear resistance. However, as far as we know, modification of the surface wettability by fabricating DLC films on nanostructured surface using PIII&D has not been explored, even though the PIII&D technique is a convenient method for depositing surface coatings and tailoring the surface topography.

The objective of this work was to modify the surface topography and hence the surface wettability by combining DLC films with a nanostructured surface. DLC films were synthesized on a titanium surface with a nanowire structure by PIII&D at various experimental conditions using acetylene as a carbon precursor.  $\text{CF}_4$  implantation was further conducted to achieve superhydrophobicity. The changes in surface topography, chemistry and thereby on wettability of the DLC films were studied, which provided an opportunity to understand the relationship between wettability and surface character of the material. Herein, we develop a feasible method for the fabrication of wettability controllable DLC films coated on nanostructured surfaces.

## 2. Experimental details

### 2.1. Materials preparation

Commercial pure Ti plates with dimensions of 10 mm × 10 mm × 1 mm were ultrasonically cleaned in ethanol and deionized water several times, followed by pickling in a 5 wt% oxalic acid solution at 100 °C for 2 h to remove the oxide

**Table 1.**  $\text{C}_2\text{H}_2$  deposition parameters.

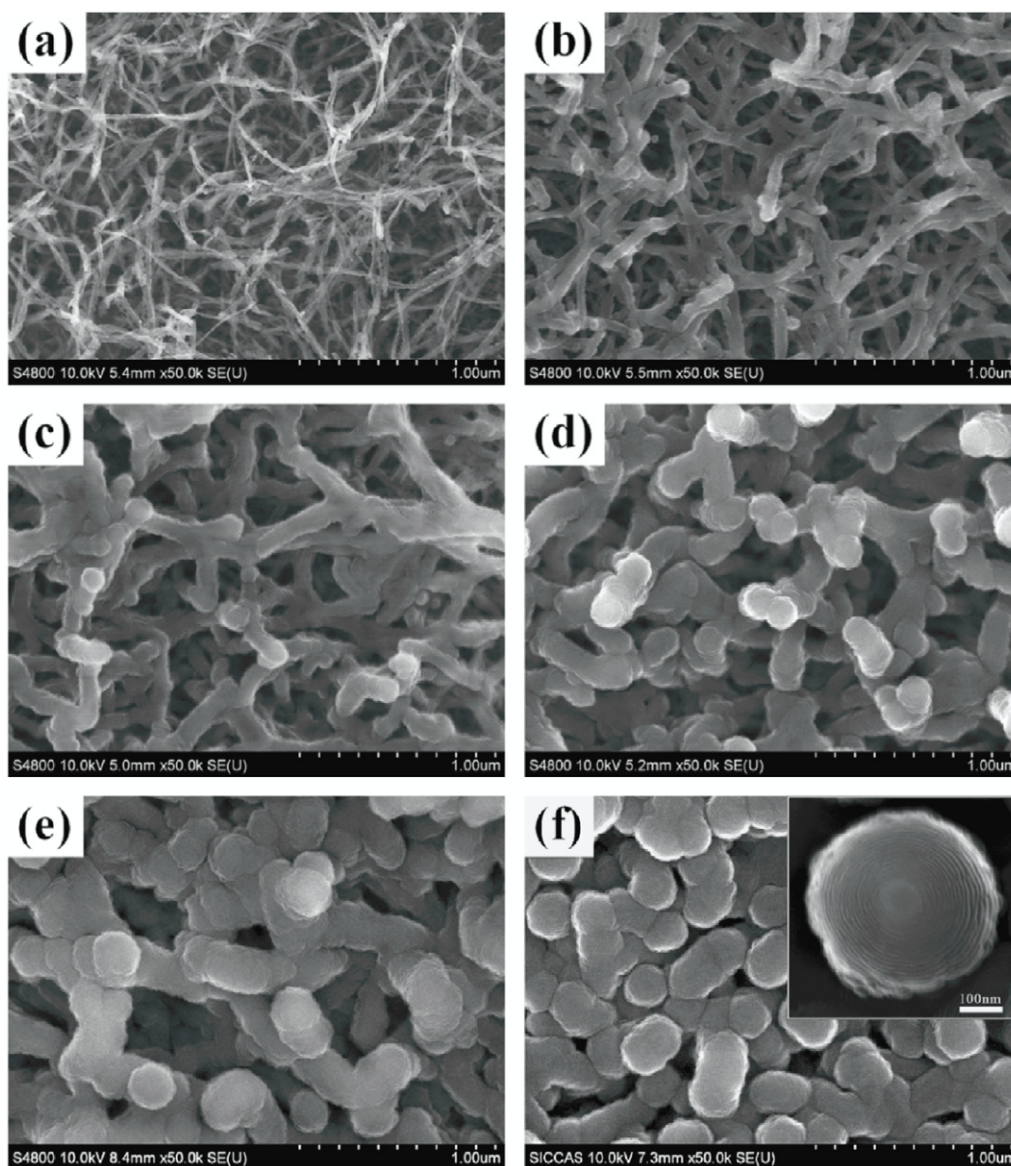
Sample	DC bias voltage (V)	Deposition time (min)
I-NT	0	0
I&D-1	0	5
I&D-2	20	5
I&D-3	40	5
I&D-4	40	10

layer and obtain a homogeneous rough surface [29]. Then the samples were ultrasonically cleaned in deionized water and dried in ambient atmosphere for further use. The  $\text{TiO}_2$  nanowire structure on the Ti surface was prepared according to the literature [29]. Briefly, each pretreated Ti plate was immersed in a mixed solution of 5 ml  $\text{H}_2\text{O}_2$  (30 wt%) and 5 ml NaOH (5 M) in a reaction vessel with Teflon liner at 80 °C for 24 h. After the reaction vessel cooled to room temperature, the Ti plates were gently rinsed with deionized water and protonated in 0.1 M HCl for 2 h. Then the Ti plates were rinsed to neutral with deionized water, dried in ambient atmosphere, and finally calcined at 450 °C for 1 h. Ti substrates with nanowire structured surfaces were obtained and denoted as NT.

A series of DLC films were prepared on the surface of as-prepared NT by PIII&D using acetylene ( $\text{C}_2\text{H}_2$ ) as a carbon precursor. The background pressure of the plasma chamber was evacuated to  $5 \times 10^{-3}$  Pa before the experiment. A  $\text{C}_2\text{H}_2$  flow of 50 standard cubic centimeters per minute (sccm) was introduced into the chamber under an implantation voltage of 15 kV during the 5 min implantation procedure. The pulse frequency and pulse duration were 70 Hz and 50  $\mu\text{s}$ , respectively. The working pressure was about  $10^{-1}$  Pa. The samples which were only conducted by the implantation process were denoted as I-NT. During the following deposition procedure, a 50 sccm  $\text{C}_2\text{H}_2$  flow was introduced into the chamber and the plasma was triggered using a radio frequency power of 300 W with pulse bias voltage of 550 V. The samples which were treated by the deposition procedure with different direct current (DC) bias voltages and deposition times were denoted as I&D- $x$  ( $x = 1-4$ ), as listed in table 1. Then the as-prepared NT and the DLC films on nanowire structured Ti substrates were treated by tetrafluoromethane ( $\text{CF}_4$ ) implantation. The  $\text{CF}_4$  flow was 50 sccm, the implantation voltage was 15 kV and the pulse duration was 50  $\mu\text{s}$ . The pulse frequency was set as 50 Hz in order to maintain the surface nanostructure.

### 2.2. Surface characterization

The surface morphologies and chemical compositions of the samples were characterized by field emission scanning electron microscopy (FE-SEM; S-4800, HITACHI, Japan) and Auger electron spectroscopy with x-ray photoelectron spectrum (AES with XPS; Microlab 310-F Scanning Auger Microprobe with a dual anode (Al/Mg) x-ray source). An accelerating voltage of 10 kV was used in the FE-SEM analysis. An Al  $K\alpha$  (1486.6 eV) source was used in the XPS analysis. Raman spectroscopy was used to investigate the



**Figure 1.** Surface views of various samples: (a) NT, (b) I-NT, (c) I&D-1, (d) I&D-2, (e) I&D-3 and (f) I&D-4, the inset is a higher magnification of the layered spherical carbon structure of I&D-4.

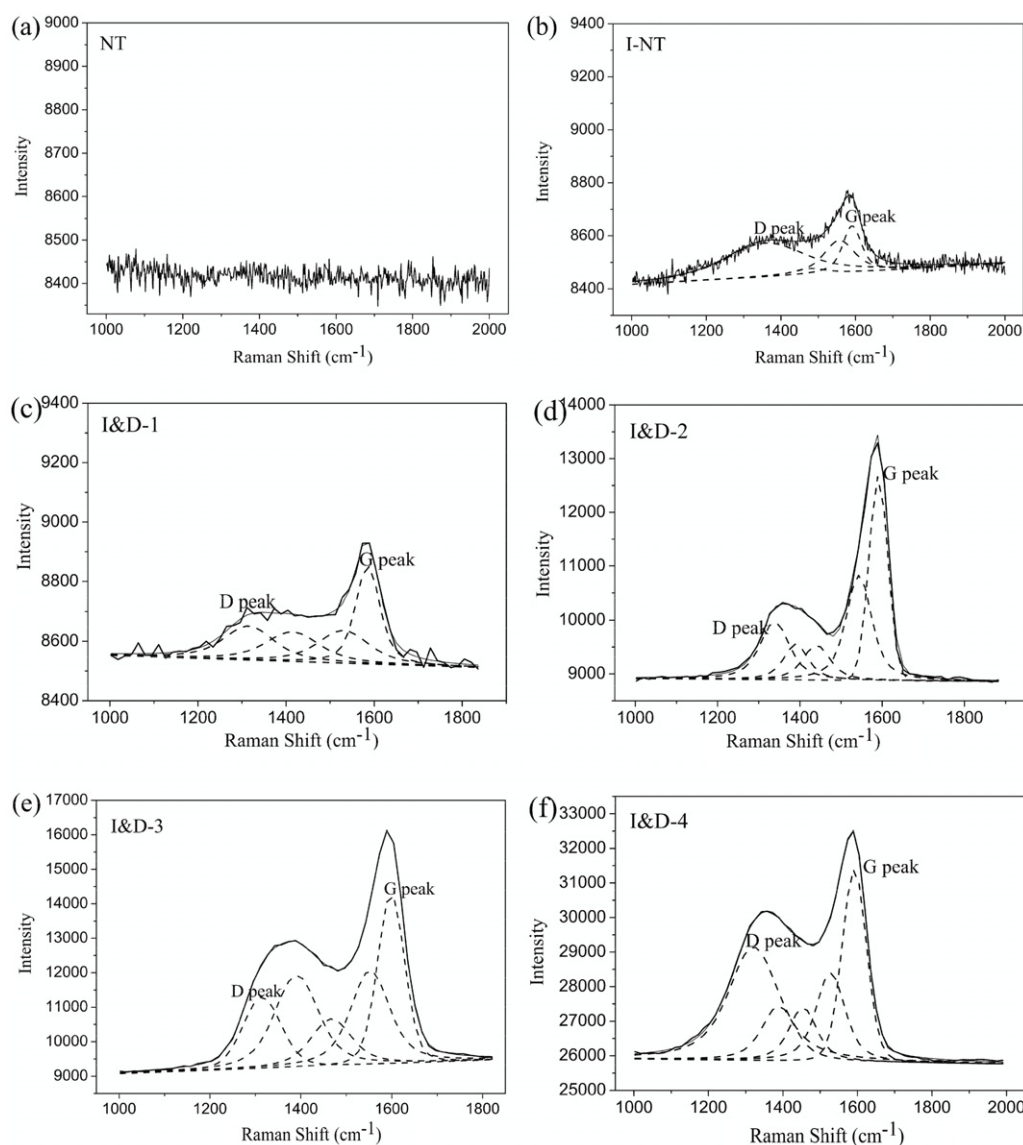
different bondings presented in the samples using a Raman microscope system (Horiba Jobin Yvon HR800, France) with an Ar-ion laser at 20 mW (514.5 nm) for excitation. The surface wettability of the samples was measured by contact angle measurement (Automatic Contact Angle Meter Model SL200B, Solon (Shanghai) information technology Co., Ltd, China), conducted in ambient environment using 2  $\mu$ l sessile distilled water droplets.

### 3. Results and discussion

Figure 1 shows the surface photographs of NT, I-NT, I&D-1, I&D-2, I&D-3 and I&D-4 respectively. The porous NT surface contained numerous nanowires with diameters of 30–40 nm, which entangled with each other and formed a network (figure 1(a)). After treatment by  $C_2H_2$  plasma immersion ion implantation, the as-prepared interconnected nanowires were

coated with a thin layer of carbon films (figure 1(b)). The diameter of the nanowires was increased to about 80 nm and the nanowire network was well maintained. Figure 1(c) depicts the surface topography of I&D-1, where the deposition step was conducted with a pulse bias voltage of 550 V and a direct current bias voltage of 0 V for 5 min. The amount of carbon obtained in the deposition step was governed by the direct current bias voltage. The deposition rate was relatively low without direct current bias voltage and the diameter of the obtained nanowires was about 130 nm (figure 1(c)). The diameter of the nanowires continued to grow larger to 170–180 nm with the direct current bias voltage increasing to 20 V (figure 1(d)). The bottom of the porous structure was partially filled with deposited carbon. When the direct current bias voltage was increased to 40 V, part of the porous surface was connected by deposited carbon films while some remained as porous nanowire structure (figure 1(e)). By extending





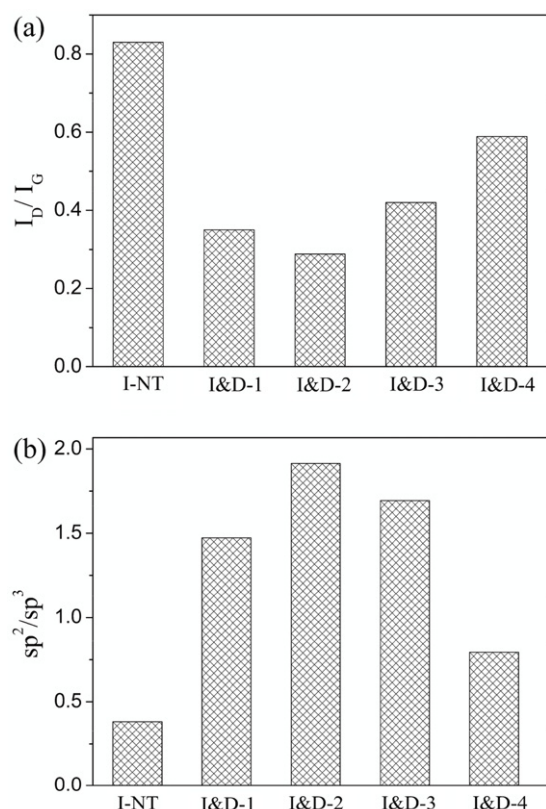
**Figure 2.** Raman spectra of the as-prepared nanowire structured Ti (NT) (a) and the synthesized DLC films: (b) I-NT, (c) I&D-1, (d) I&D-2, (e) I&D-3 and (f) I&D-4.

the deposition time from 5 to 10 min under a direct current bias voltage of 40 V, the porous nanowire network almost disappeared and the surface was covered by continuous carbon films (figure 1(f)).

Interestingly, we found that the DLC films coated on the nanowire structured surface synthesized by PIII&D grew in a layer-by-layer manner. When the films grew to a certain extent and exceeded the top of the nanowire, a layered spherical structure appeared (figures 1(d)–(f)). A higher magnification of the layered spherical carbon in figure 1(f) is displayed in the inset. It has been reported that carbon films with spherical structures were synthesized using CVD methods [20, 30]. However, the subtle structure of the sphere has not been reported. The formation of this rippling layered structure may be partially attributed to the growth mode of nucleation and deposition in gas atmosphere [20]. The nature of carbon was another important factor for the layer-by-layer manner. The

properties of the DLC films were actually more similar to those of graphite, which has a layered structure.

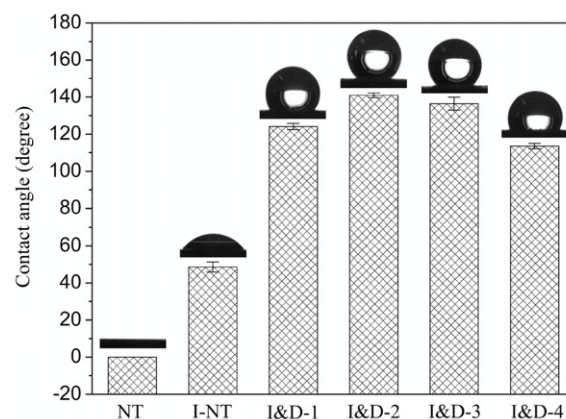
Raman spectra of the as-prepared nanowire structured Ti (NT) and the synthesized DLC films are shown in figure 2, the order of which corresponds to the sequence of the surface photographs in figure 1. There was no peak between the Raman shifts at 1000 and 2000  $\text{cm}^{-1}$  in figure 2(a), indicating that NT did not cause Raman scattering in this area. The Raman spectra in figures 2(b)–(f) were deconvoluted into several peaks using a multiple Lorentzian peak fit. The presence of typical D and G peaks at around 1340  $\text{cm}^{-1}$  and 1590  $\text{cm}^{-1}$ , respectively, confirmed the formation of DLC films. The G peak is a measure of all  $\text{sp}^2$  sites while the D peak is only due to the six-fold ring structure in the DLC films [31]. The ratio of the intensity of the D peak to the intensity of the G peak ( $I_D/I_G$ ) as well as the relative presence of  $\text{sp}^2$  and  $\text{sp}^3$  bonds ( $\text{sp}^2/\text{sp}^3$ ) were evaluated and are shown in figure 3. Figure 3(a)



**Figure 3.**  $I_D/I_G$  ratio (a) and  $sp^2/sp^3$  ratio (b) of the synthesized DLC films.

indicates that the synthesized DLC films had a lower  $I_D/I_G$  ratio after the deposit step. I&D-2 had the lowest  $I_D/I_G$  ratio, followed by I&D-1, I&D-3 and I&D-4 sequentially, while I-NT had the highest  $I_D/I_G$  ratio. It was reported that the relative intensity of the D and G peaks increased with substrate temperature [32]. The ion bombardment as well as the surface charge accumulation due to the low conductive surface in the implantation step caused thermal accumulation on the surface of I-NT, which contributed to the highest  $I_D/I_G$  ratio. However, the temperature rise in the deposition step would be relatively lower. The high  $I_D/I_G$  ratio of I&D-4 was attributed to the thermal accumulation due to the prolonged deposition time. From figure 3(b) we can see that the  $sp^2/sp^3$  ratio increased rapidly from I-NT to I&D-1, reached the highest level in I&D-2, and then decreased gradually in I&D-3 and I&D-4. The  $sp^2/sp^3$  ratio in DLC films depended on experimental conditions such as substrate deposition temperature [33], type and pressure of the precursor gas [34]. In the present study, a possible reason for the change of  $sp^2/sp^3$  ratio might be that as the DC bias voltage increased in the deposition step, the particle bombardment function was enhanced and the  $sp^3$ -bond carbon density was reduced [35].

The water contact angles of NT and the synthesized DLC films are displayed in figure 4. They represented the wettability of the surfaces and mainly depended on the surface topography. The as-prepared nanowire structured surface was superhydrophilic with a contact angle of  $0^\circ$ , indicating that the water droplets would spread rapidly when they made contact with the surface. The hydrophilic property of  $TiO_2$  [36]



**Figure 4.** Contact angle of NT and the synthesized DLC films.

was magnified by the porous nanowire structure and became superhydrophilic, because it is much easier for water to penetrate into the surface layer. The contact angle of I-NT was close to  $50^\circ$ , mainly due to the hydrophobicity of DLC films. But the surface remained hydrophilic because the pores among the nanowires were still large enough for the water droplet to penetrate. After the deposition step was conducted the samples all exhibited hydrophobic behavior with the contact angle varying between  $112^\circ$  and  $141^\circ$ . The largest contact angle, about  $141^\circ$ , appeared on the surface of I&D-2. It was a result of the appropriate nanostructure with suitable pore size and porosity. The contact angle hysteresis of I&D-2 was very high. The water droplet on its surface could not roll off even when the sample was tilted vertically, while it still appeared spherical in shape. Those samples with oversize pores (I&D-1) and too small a porosity (I&D-3) were less hydrophobic. The surface of I&D-4 was covered up by DLC films and the primary nanowire structure was hardly found, resulting in a contact angle of around  $112^\circ$ .

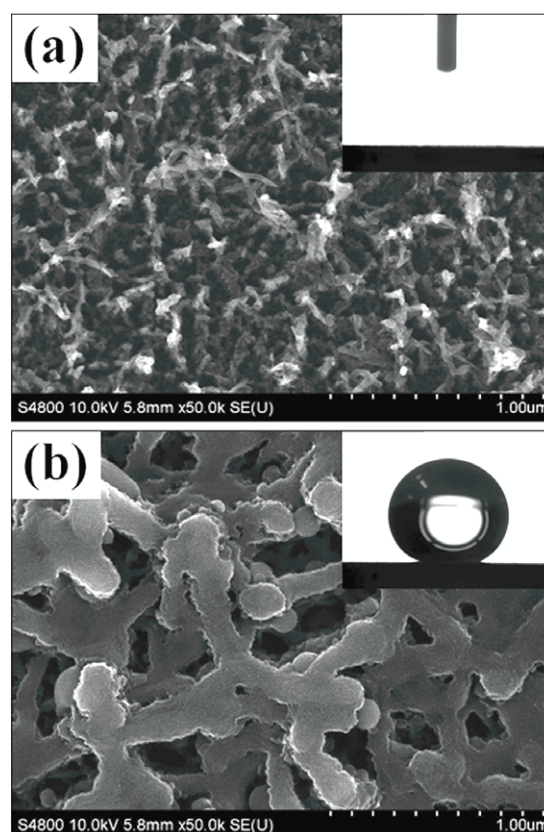
In general, the surface topography, porosity and roughness are major factors for wettability [10, 20, 37]. A nanostructured surface should have the ability to form a large amount of entrapped air pockets so as to achieve high hydrophobicity, as air is an effective hydrophobic media [38]. When water was dropped onto the nanowire structured surface coated with DLC films, air was entrapped in the pores to form air pockets and the liquid–air contact area was enlarged. However, the entrapped air pockets were unstable and could easily collapse if the pores on the surface were too large. The reason why I-NT was still hydrophilic might be the overlarge pore size. From figure 1(b) we can see that the original interconnected nanowire network was well maintained despite the nanowire being coated with a thin layer of DLC films. Water could still penetrate into the large pores when the droplet was connected with the surface. To achieve a high hydrophobic surface, the topography of the surface was tailored by altering the PIII&D parameters. The surface of I&D-1 was more suitable for the formation of stable air pockets and hence more hydrophobic, because the pore size of the surface layer was smaller while the diameter of the DLC coated nanowire was enlarged (figure 1(c)). The most hydrophobic I&D-2 was considered to have a proper surface topography with suitable pore size and porosity and

hence could form a high fraction of liquid–air contact area when contacting with a water droplet (figure 1(d)). On the other hand, ultrasmall pore size and porosity could result in less hydrophobicity because of the limited amount of air pockets. When the DLC films became thicker the pore size and porosity were smaller accordingly, which made I&D-3 less hydrophobic than I&D-2 (figure 1(e)). Figure 1(f) shows that the surface of I&D-4 was relatively flat with a few small pores, which led to its lowest hydrophobicity among the samples from implantation and deposition. So it was critical to form a surface topography with suitable pore size and porosity for high hydrophobicity.

The Cassie–Baxter equation,  $\cos \theta_r = f_1 \cos \theta - f_2$ , could be used to explain the high hydrophobicity of I&D-2 [39–41]. Here  $\theta_r$  ( $141^\circ$ ) and  $\theta$  ( $51^\circ$ ) were the contact angles of I&D-2 and the smooth titanium surface coated with DLC films under the same experimental conditions, respectively;  $f_1$  and  $f_2$  were the contact area fractions of liquid–solid and liquid–air, respectively ( $f_1 + f_2 = 1$ ). According to the equation, the value of  $f_1$  was 0.14, which indicated that only 14% of the total liquid-contacting area was liquid–solid contact, whereas the other 86% of the area was liquid–air contact. As a result, the water droplet appeared as a spherical shape to minimize its liquid–air interfacial energy.

On the other hand, chemical bonding and surface passivation also had impact on the surface wetting behavior, but with less influence than the previous factors [20]. There were two minor factors here which should be taken into account besides the crucial factor: the  $I_D/I_G$  and  $sp^2/sp^3$  ratios. It was reported that the contact angle decreased rapidly with increasing  $I_D/I_G$  ratio, which measured the fraction of the ring organized  $sp^2$  phase [22]. In the present study, I-NT had the lowest contact angle and the highest  $I_D/I_G$  ratio. There was a decrease of the  $I_D/I_G$  ratio from I&D-1 and I&D-2 and the contact angle increased sharply. Then the  $I_D/I_G$  ratio increased and hence the contact angle became lower again, which corresponded with the previous research [22]. Some researchers indicated that the increasing  $sp^2$  content in the carbon film caused a reduction of surface free energy and hence enhanced the hydrophobicity [20, 42, 43]. From figures 3(b) and 4 we can see that the sequence of  $sp^2/sp^3$  ratio corresponds well with the wetting behavior, which confirms the previous rule. The highest  $sp^2/sp^3$  ratio of I&D-2 was attributed partially to its high hydrophobicity, while the hydrophilic I-NT had the lowest  $sp^2/sp^3$  ratio. However, the DLC films could not achieve a contact angle as high as  $141^\circ$  merely by modifying the  $I_D/I_G$  and  $sp^2/sp^3$  ratios. Control experiments showed that the contact angle of DLC films synthesized on smooth Ti surfaces without nanowire structure using PIII&D varied between  $33^\circ$  and  $60^\circ$ . Generally speaking, the surface topography was playing a leading role in making I&D-2 the most hydrophobic sample, while the properties of the DLC films had a relatively minor contribution.

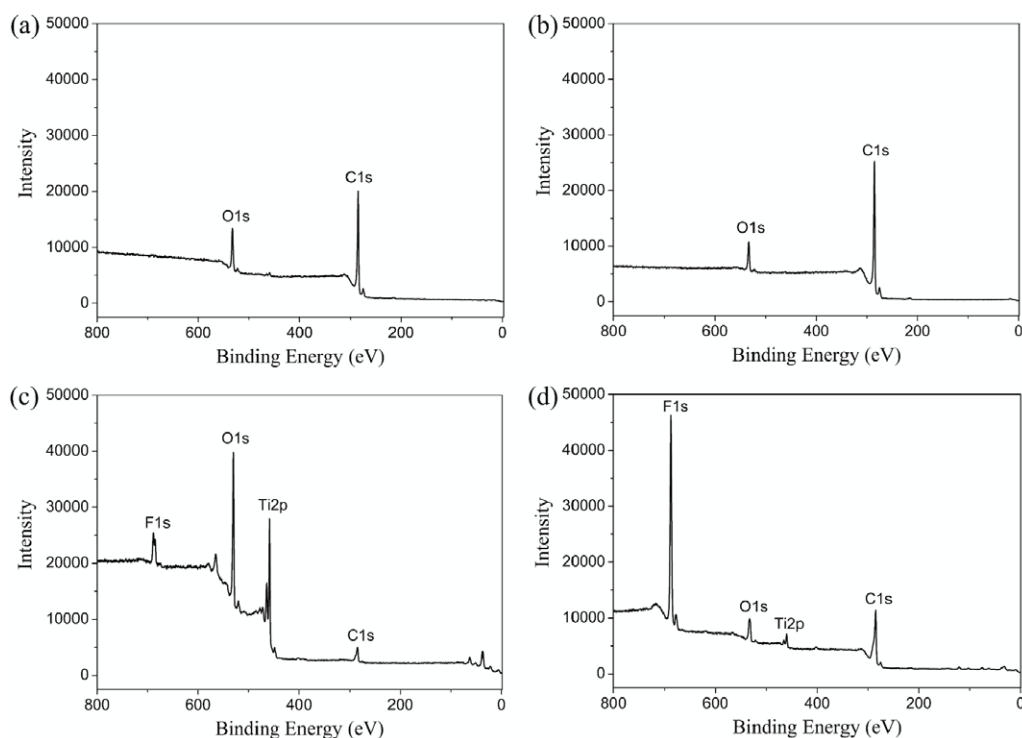
CF<sub>4</sub> implantation had different effects on the series of nanowire structures with or without DLC films. It was reported that the existence of fluorine would remarkably reduce the surface energy and enhance hydrophobicity [21]. However, in the present study we found that CF<sub>4</sub> implantation did not



**Figure 5.** Surface topography of CF<sub>4</sub> implanted I-NT (a) and I&D-2 (b), the insets show the shapes of the water droplets on the corresponding surfaces.

always cause an increase in contact angle. NT remained superhydrophilic and, unexpectedly, the contact angle of I-NT decreased from around  $50^\circ$  to  $0^\circ$  after CF<sub>4</sub> implantation. I&D-1, I&D-2, I&D-3 and I&D-4 exhibited much larger contact angles after CF<sub>4</sub> implantation, varying between  $132^\circ$  and  $150^\circ$ . I&D-2 became superhydrophobic with a contact angle of  $150^\circ$  after CF<sub>4</sub> implantation. Figure 5 depicts the surface topography of CF<sub>4</sub> implanted I-NT and I&D-2 and the insets show the shapes of the water droplets on the corresponding surfaces. The surface topography of the samples revealed the reason why CF<sub>4</sub> implantation caused converse change on the wettability of I-NT and other samples. From figure 5(a) we can see that CF<sub>4</sub> implantation caused deformation of the nanowire structure on the I-NT surface, resulting in a random porous surface through which water could penetrate easily. The reason may be that the conductivity of the I-NT surface was fairly low due to the relatively low carbon content. During CF<sub>4</sub> implantation, the low conductive surface caused local accumulation of surface charge, and the following surface discharge destroyed the nanostructure. However, the nanowire structure on the surface of I&D-2 was quite well maintained after CF<sub>4</sub> implantation, mainly due to the good conductivity of the DLC films (figure 5(b)). The surface topography of the DLC films on CF<sub>4</sub> implanted I&D-2 was slightly different from that before CF<sub>4</sub> implantation, mainly due to the low carbon content in the CF<sub>4</sub> plasma.





**Figure 6.** XPS full spectra of various samples: (a) I-NT, (b) I&D-2, (c) CF<sub>4</sub> implanted I-NT and (d) CF<sub>4</sub> implanted I&D-2.

CF<sub>4</sub> molecules were reported to be decomposed easily to various radicals in the plasma [21]. During CF<sub>4</sub> implantation, the unsaturated C bonds of the DLC films were saturated by the CF<sub>x</sub> bonds during the plasma treatment and the hydrophobicity of the DLC films was enhanced. However, a control experiment showed that the contact angle of CF<sub>4</sub> implanted DLC films synthesized on smooth Ti surface varied between 45° and 76°, indicating that the CF<sub>x</sub> bonds alone could not lead to superhydrophobicity. Figure 6 shows the XPS full spectrum of I-NT and I&D-2 before and after CF<sub>4</sub> implantation, respectively. The carbon content of I&D-2 was obviously higher than that of I-NT, which was confirmed previously by their surface views (figures 1(b) and (d)) and Raman spectra (figures 2(b) and (d)). The fluorine content of CF<sub>4</sub> implanted I&D-2 (figure 6(d)) was much higher than that of CF<sub>4</sub> implanted I-NT (figure 6(c)), indicating that higher carbon content would facilitate the bonding between DLC films and CF<sub>x</sub>, as there were more unsaturated C bonds on the outermost surface. On the other hand, figures 6(c) and (d) reveal the different extents of surface deformation. The surface nanostructure of CF<sub>4</sub> implanted I-NT was destroyed to a large extent and the deformed TiO<sub>2</sub> nanowire structure was exposed on the surface, resulting in a relatively high Ti content in figure 6(c). The bonding of fluorine to TiO<sub>2</sub> was weaker than to carbon, which also attributed to the lower fluorine content on the surface of CF<sub>4</sub> implanted I-NT. Figure 6(d) shows that only a small amount of TiO<sub>2</sub> was detected on the surface of CF<sub>4</sub> implanted I&D-2, indicating that the damage of the surface caused by CF<sub>4</sub> implantation was limited and hence the content of CF<sub>x</sub> bonding on the surface DLC films was greatly increased. The superhydrophobicity of CF<sub>4</sub> implanted I&D-2

was attributed to the suitable surface topography as well as the existence of fluorine in the DLC films.

#### 4. Conclusions

The wettability of titanium was controlled by synthesizing DLC films on its nanowire structured surface using PIII&D technology in this work. The DLC films on the nanowire structured titanium surface grow in a layer-by-layer manner into a spherical structure. The high hydrophobicity of the nanowire structured titanium with DLC films is attributed to the proper nanostructure topography with suitable pore size and porosity, while a lower  $I_D/I_G$  ratio and a higher sp<sup>2</sup>/sp<sup>3</sup> ratio of the DLC films also have a relatively minor contribution. Further CF<sub>4</sub> implantation on suitably structured DLC films can lead to superhydrophobicity. This study provides a convenient method to control the wettability of substrates with complex shapes from hydrophilic to superhydrophobic according to practical needs.

#### Acknowledgments

This work was jointly supported by Shanghai-Unilever Research and Development Fund 09520715200, Shanghai Science and Technology R&D Fund under grants 0952nm04400 and 1052nm06600, National Natural Science Foundation of China No. 51071168, Innovation Fund of SICCAS under grant Y06ZC3130G.

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