

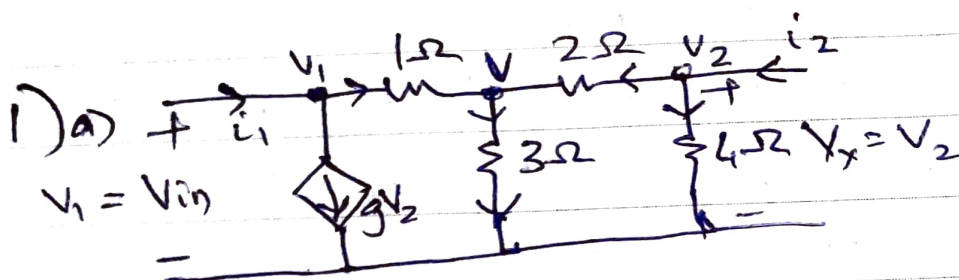


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## Analog Circuits

### Assignment-1



From the above circuit, by using KCL,

$$\frac{V_1 - V}{1} + \frac{V_2 - V}{2} = \frac{V}{3} \Rightarrow V_1 + \frac{V_2}{2} = V \left[ \frac{11}{6} \right]$$

$$\Rightarrow \boxed{V = \frac{3}{11} [2V_1 + V_2]} = \frac{6V_1}{11} + \frac{3V_2}{11}$$

$$\Rightarrow i_1 = gV_2 + \frac{V_1 - V}{1} = gV_2 + V_1 - \frac{6V_1}{11} - \frac{3}{11} V_2$$

$$\boxed{i_1 = \frac{5}{11} V_1 + \left( g - \frac{3}{11} \right) V_2}$$

$$\text{And } i_2 = \frac{V_2}{4} + \frac{V_2 - V}{2} = \frac{V_2}{4} + \frac{V_2}{2} - \frac{1}{2} \left[ \frac{6V_1}{11} + \frac{3V_2}{11} \right]$$

$$= \frac{3V_2}{4} - \frac{3V_1}{11} - \frac{3V_2}{22} = \frac{33V_2 - 6V_2}{44} - \frac{3V_1}{11}$$

$$= \frac{27}{44} V_2 - \frac{3V_1}{11} \Rightarrow \boxed{i_2 = -\frac{3V_1}{11} + \frac{27}{44} V_2}$$

$$\Rightarrow \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} \frac{5}{11} & g - \frac{3}{11} \\ -\frac{3}{11} & \frac{27}{44} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

Y-parameters



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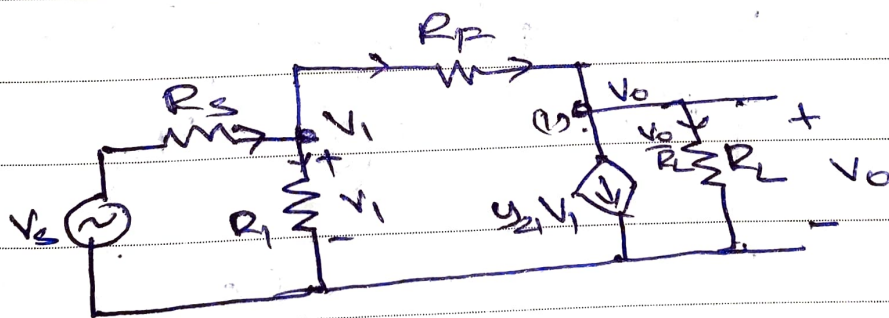
b) An unilateral network is a circuit network in which the effect of change in input parameter is traversed to the other port but is not affected in the other way round. Hence, for admittance circuit,  $y_{21}$  or  $y_{12}$  is zero. (anyone)

Hence in the found  $y$  matrix,

$$y = \begin{bmatrix} 5/11 & 3-3/11 \\ -3/11 & 27/44 \end{bmatrix}, \text{ here } y_{12} \text{ must be zero}$$

$$\Rightarrow 3 - \frac{3}{11} = 0 \Rightarrow \boxed{3 = \frac{3}{11}}$$

2)



By applying Nodal analysis:

$$(1) \Rightarrow V_1 - V_0 = R_F \left[ y_{21} V_1 + \frac{V_0}{R_L} \right]$$

$$V_1 \left[ 1 - R_F y_{21} \right] = V_0 \left[ 1 + \frac{R_F}{R_L} \right]$$

$$\boxed{V_1 = \frac{V_0 \left( 1 + \frac{R_F}{R_L} \right)}{1 - R_F y_{21}}}$$



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$$(2) \quad V_s - V_1 = R_s \left[ \frac{V_1}{R_1} + y_{21} V_1 + \frac{V_o}{R_L} \right] = \left( \frac{R_s}{R_1} + \frac{R_s}{R_F} \right) V_1 - \frac{R_s}{R_F} V_o$$

$\underbrace{\hspace{10em}}_{\frac{V_1 - V_o}{R_F}}$

$$\Rightarrow V_s = V_1 \left( \frac{R_s}{R_1} + \frac{R_s}{R_F} + 1 \right) - \frac{R_s}{R_F} V_o$$

$$= V_o \left[ \frac{(1 + R_F/R_L)}{(1 - R_F y_{21})} \left( 1 + \frac{R_s}{R_1} + \frac{R_s}{R_F} \right) - \frac{R_s}{R_F} \right]$$

$$\Rightarrow \boxed{\frac{V_o}{V_s} = \frac{1}{\frac{(1 + R_F/R_L)}{(1 - R_F y_{21})} \left( 1 + \frac{R_s(R_1 + R_F)}{R_1 R_F} \right) - \left( \frac{R_s}{R_F} \right)}}$$

(b) When  $y_{21} \rightarrow \infty$ , the term in denominator converges to zero, which gives

$$\frac{V_o}{V_s} \approx \frac{1}{0 - \frac{R_s}{R_F}} = -\frac{R_F}{R_s}$$

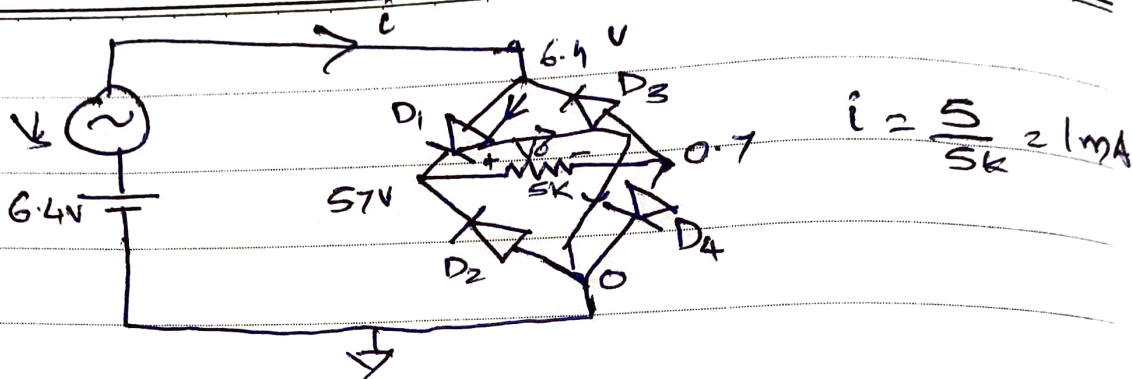




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3)



a) As we can see  $D_1$  and  $D_4$  will be in forward bias and  $D_2$  and  $D_3$  will be in reverse bias. Assuming the cut-in voltage of diodes be  $0.7V$ , we get

$$V_o = 5.7V - 0.7V = 5V$$

And correspondingly the D.C operating point are

	$V_D$	$I_D$
$D_1$	$0.7V$	$1mA$
$D_2$	$-5.7V$	$\sim 0A$
$D_3$	$-5.7V$	$\sim 0A$
$D_4$	$0.7V$	$1mA$

b) The D.C current through the  $5k$  resistor is  $I = \frac{5V}{5k} = 1mA$ .

c) Now applying a small input signal voltage of  $V_s$ , we see the voltage across resistor

$$V_o' = (5.7 + V_s) - 0.7 = 5 + V_s$$

$$\Rightarrow V_o' - V_o = (5 + V_s) - (5) = V_s \Rightarrow \frac{\Delta V_o}{V_s} \approx 1$$

$\therefore$  Small signal gain  $\approx 1 = \frac{V_o}{V_s}$



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4) Given input-output characteristics of 2 non-linear networks:

$$N_1: V_o = \frac{V_{in}^2}{V_A}$$

$$N_2: V_o = V_A \exp\left(\frac{V_{in}}{V_A}\right)$$

a) i) For  $N_1$ :  $V_o = \frac{V_{in}^2}{V_A} \Rightarrow \left. \frac{\partial V_o}{\partial V_{in}} \right|_{V_{in}=V} = \frac{2V_{in}}{V_A} \Big|_V$

$$\Rightarrow \frac{2V_o}{V_A} = \frac{5}{10} \Rightarrow \boxed{V = 5V_A}$$

Hence,  $V_{in} = 5V_A$  for incremental gain to be 10.

ii) For  $N_2$ :  $V_o = V_A \exp\left(\frac{V_{in}}{V_A}\right)$

$$\Rightarrow \left. \frac{\partial V_o}{\partial V_{in}} \right|_{V_{in}=V} = V_A \cdot \left( \frac{1}{V_A} \exp\left(\frac{V_{in}}{V_A}\right) \right) \Big|_{V_{in}=V} = 10$$

$$\Rightarrow \boxed{V_{in} = V_A \ln 10} \text{ for incremental gain to be 10.}$$

b) To find which network is more linear, we can find the second derivative and observe which is more closer to zero.

$$\text{For } N_1: \left. \frac{\partial^2 V_o}{\partial V_{in}^2} \right|_{V_{in}=V_A \times 5} = \frac{2}{V_A}$$

$$N_2: \left. \frac{\partial^2 V_o}{\partial V_{in}^2} \right|_{V_{in}=V_A \ln 10} = \frac{1}{V_A} \exp\left(\frac{V_A \ln 10}{V_A}\right) = \frac{10}{V_A}$$

As  $\frac{2}{V_A} < \frac{10}{V_A}$ ,  $N_1$  network is more linear than  $N_2$