One dimensional Burgers' equation

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1 Non-linear Burgers' equation

We consider the non-linear viscous Burgers' equation

$$w_t - \nu w_{xx} + w w_x = f_s \qquad \text{in} \quad (0, 1) \times (0, \infty)$$
 (1)

with boundary conditions

$$w(0,t) = u_s, w_x(1,t) = g_s (2)$$

and initial condition

$$w(x,0) = w_0(x) \tag{3}$$

1.1 Stationary Burgers' equation

The stationary Burgers' equation is given by

$$-\nu w_{xx} + ww_x = f_s \qquad \text{in} \quad (0,1) \tag{4}$$

with boundary conditions

$$w(0) = u_s, \qquad w_x(1) = g_s \tag{5}$$

An unstable stationary solution can be obtained as

$$w_s = -\frac{\nu\pi}{2}(1+\epsilon)\tan\left(\frac{\pi}{4}(1+\epsilon) + C_0\right) \tag{6}$$

with the conditions

$$0 < \epsilon < 1,$$
 $-\frac{\pi}{4} < C_0 < 0,$ $(1 + \epsilon) \tan \left(\frac{\pi}{4}(1 + \epsilon) + C_0\right) = 1$

We choose

$$\epsilon = 0.6$$
 \Longrightarrow $C_0 = \arctan(1/(1+\epsilon)) - \frac{\pi}{4}(1+\epsilon) = -0.69803774609235$

2 Nonlinear system without control

We set $z = w - w_s$. The equation satisfied by z is

$$\frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} + z \frac{\mathrm{d}z}{\mathrm{d}x} = \nu \frac{\partial^2 z}{\partial x^2} \quad \text{in} \quad (0, 1) \times (0, \infty)$$
 (7)

with boundary conditions

$$z(0,t) = 0,$$
 $z_x(1,t) = 0$ (8)

and initial conditions

$$z(x,0) = w_0(x) - w_s(x) (9)$$

We multiply by a test function ϕ with $\phi(0) = 0$ to obtain the weak formulation

$$\int_0^1 z_t \phi dx + \nu \int_0^1 \frac{\partial z}{\partial x} \frac{d\phi}{dx} dx + \int_0^1 w_s \frac{\partial z}{\partial x} \phi dx + \int_0^1 z \frac{\partial w_s}{\partial x} \phi dx + \int_0^1 z \frac{dz}{dx} \phi dx = 0$$

Divide domain into N elements with vertices

$$0 = x_0 < x_1 < \dots < x_N = 1, \qquad x_i = ih, \qquad h = \frac{1}{N}$$

The finite element solution can be written as

$$z(x,t) = \sum_{j=1}^{N} z_j(t)\phi_j(x)$$

while the stationary solution expressed as

$$w_s(x) = \sum_{i=1}^{N} w_s^j \phi_j(x) + u_s \phi_0(x)$$

where $w_s^j = w_s(x_j)$. Here the $\{\phi_j\}$ are the usual P_1 basis functions. The approximate weak formulation is

$$\int_{0}^{1} z_{t} \phi_{i} dx = -\nu \int_{0}^{1} \frac{\partial z}{\partial x} \frac{d\phi_{i}}{dx} dx - \int_{0}^{1} w_{s} \frac{\partial z}{\partial x} \phi_{i} dx - \int_{0}^{1} z \frac{\partial w_{s}}{\partial x} \phi_{i} dx$$
$$- \int_{0}^{1} z \frac{dz}{dx} \phi_{i} dx, \qquad \forall i = 1, 2, ..., N$$

or

$$\sum_{j=1}^{N} z'_{j}(t) \int_{0}^{1} \phi_{i} \phi_{j} dx = -\sum_{j=1}^{N} \sum_{k=1}^{N} z_{j}(t) z_{k}(t) \int_{0}^{1} \phi_{j} \phi'_{k} \phi_{i} dx
- \sum_{j=1}^{N} z_{j}(t) \left[\nu \int_{0}^{1} \phi'_{i} \phi'_{j} dx + u_{s} \int_{0}^{1} \phi_{i} (\phi_{0} \phi_{j})' dx \right]
- \sum_{j=1}^{N} z_{j}(t) \left[\sum_{k=1}^{N} w_{s}^{k}(t) \left(\int_{0}^{1} \phi_{j} \phi'_{k} \phi_{i} dx + \int_{0}^{1} \phi_{k} \phi'_{j} \phi_{i} dx \right) \right]$$

We use the following notations:

- $\mathbf{z} = [z_1, z_2, ..., z_N]^{\top}$
- $\mathbf{w}_s = [w_s^1, w_s^2, ..., w_s^N]^{\top}$
- $\mathbf{M} \in \mathbb{R}^{N \times N}$ with $\mathbf{M}(i, j) = \int_0^1 \phi_i \phi_j dx$
- $\mathbf{A}1 \in \mathbb{R}^{N \times N}$ with $\mathbf{A}1(i,j) = \int_0^1 \phi_i' \phi_j' dx$
- $\mathbf{A}2 \in \mathbb{R}^{N \times N}$ with $\mathbf{A}2(i,j) = \int_0^1 \phi_i(\phi_0 \phi_j)' \mathrm{d}x$
- $\mathbf{D}1 \in \mathbb{R}^{N \times N \times N}$ with $\mathbf{D}1(i, j, k) = \int_0^1 \phi_i \phi_j' \phi_k dx$

Thus we have a non-linear system of first order ODEs in z

$$\mathbf{M} \frac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} = \mathbf{RHS}$$

where

$$\mathbf{RHS}(i) = -\mathbf{z}^{\top}\mathbf{D}1(:,:,i)\mathbf{z} - \left[\nu\mathbf{A}1(i,:) + u_s\mathbf{A}2(i,:) + \mathbf{w}_s^{\top}(\mathbf{D}1(:,:,i) + \mathbf{D}1(:,:,i)^{\top})\right]\mathbf{z}$$

This is implemented and solved in burger.m

2.1 Excercises

1. The initial condition is chosen as

$$z(x,0) = \delta \sin(\pi x)$$

Run program burger.m with delta = 0. The zero solution does not change with time. This corresponds to the stationary solution for the original Burgers's equation.

- 2. Take different initial conditions by varying delta, and convince yourself that the zero solution is unstable. Choose values for delta to observe the following behaviors
 - The solution blows up
 - The solution converges to another steady state

3 Linearized Burgers' equation

3.1 Feedback control

Consider the linearized equation

$$\frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} = \nu \frac{\partial^2 z}{\partial x^2} \tag{10}$$

$$z(0,t) = u(t), \qquad \frac{\partial z}{\partial x}(1,t) = 0 \tag{11}$$

$$z(x,0) = w_0(x) - w_s(x)$$
(12)

The weak formulation is given by

$$\int_0^1 \left(\frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} \right) \phi \mathrm{d}x = -\nu \int_0^1 \frac{\partial z}{\partial x} \frac{\partial \phi}{\partial x} \mathrm{d}x$$

We look for a finite element solution of the form

$$z(x,t) = \sum_{j=1}^{N} z_j(t)\phi_j(x) + u(t)\phi_0(x)$$

The approximate weak formulation is

$$\int_0^1 \left(\frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} \right) \phi_i \mathrm{d}x = -\nu \int_0^1 \frac{\partial z}{\partial x} \frac{\partial \phi_i}{\partial x} \mathrm{d}x, \qquad i = 1, 2, \dots, N$$

Ignoring the $\frac{du}{dt}$ term gives us

$$\sum_{j=1}^{N} \frac{\mathrm{d}z_j}{\mathrm{d}t} \int_0^1 \phi_i \phi_j \mathrm{d}x = \sum_{j=1}^{N} z_j \left[-\nu \int_0^1 \phi_i' \phi_j' \mathrm{d}x - \int_0^1 w_s \phi_i \phi_j' \mathrm{d}x - \int_0^1 \phi_i \phi_j \frac{\mathrm{d}w_s}{\mathrm{d}x} \right]$$
$$+ u \left[-\int_0^1 w_s \phi_i \phi_0' \mathrm{d}x - \int_0^1 \phi_i \phi_0 \frac{\mathrm{d}w_s}{\mathrm{d}x} \mathrm{d}x - \nu \int_0^1 \phi_i' \phi_0' \mathrm{d}x \right]$$

Using the expression for w_s mentioned above, we get

$$\sum_{j=1}^{N} \frac{dz_{j}}{dt} \int_{0}^{1} \phi_{i} \phi_{j} dx = \sum_{j=1}^{N} z_{j} \left[-\nu \int_{0}^{1} \phi'_{i} \phi'_{j} dx - u_{s} \int_{0}^{1} \phi_{i} (\phi_{0} \phi_{j})' dx \right]
+ \sum_{j=1}^{N} z_{j} \left[-\sum_{k=1}^{N} w_{s}^{k} \int_{0}^{1} \phi_{j} \phi'_{k} \phi_{i} dx - \sum_{k=1}^{N} w_{s}^{k} \int_{0}^{1} \phi_{k} \phi'_{j} \phi_{i} dx \right]
+ u \left[-2u_{s} \int_{0}^{1} \phi_{i} \phi_{0} \phi'_{0} dx - \sum_{k=1}^{N} w_{s}^{k} \int_{0}^{1} \phi_{i} (\phi_{0} \phi_{k})' dx - \nu \int_{0}^{1} \phi'_{i} \phi'_{0} dx \right]$$

We use the following notations:

•
$$\mathbf{z} = [z_1, z_2, ..., z_N]^{\top}$$

•
$$\mathbf{w}_s = [w_s^1, w_s^2, ..., w_s^N]^{\top}$$

•
$$\mathbf{M} \in \mathbb{R}^{N \times N}$$
 with $\mathbf{M}(i,j) = \int_0^1 \phi_i \phi_j \mathrm{d}x$

•
$$\mathbf{A}1 \in \mathbb{R}^{N \times N}$$
 with $\mathbf{A}1(i,j) = \int_0^1 \phi_i' \phi_j' dx$

•
$$\mathbf{A}2 \in \mathbb{R}^{N \times N}$$
 with $\mathbf{A}2(i,j) = \int_0^1 \phi_i(\phi_0 \phi_j)' \mathrm{d}x$

•
$$\mathbf{D}1 \in \mathbb{R}^{N \times N \times N}$$
 with $\mathbf{D}1(i, j, k) = \int_0^1 \phi_i \phi_j' \phi_k dx$

•
$$\mathbf{A}(i,:) = -\nu \mathbf{A}1(i,:) - u_s \mathbf{A}2(i,:) - \mathbf{w}_s^{\top} \left[\mathbf{D}1(:,:,i) + \mathbf{D}1(:,:,i)^{\top} \right], \quad \forall i = 1, 2, ..., N$$

•
$$\mathbf{d}1 \in \mathbb{R}^N$$
 with $\mathbf{d}1(i) = \int_0^1 \phi_i \phi_0 \phi_0' dx$

•
$$\mathbf{d}2 \in \mathbb{R}^N$$
 with $\mathbf{d}2(i) = \int_0^1 \phi_i' \phi_0' \mathrm{d}x$

•
$$\mathbf{B} = -2u_s\mathbf{d}1 - \mathbf{A}2 \cdot \mathbf{w}_s - \nu \mathbf{d}2$$

This can be written in matrix form as

$$\mathbf{M}\frac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} = \mathbf{A}\mathbf{z} + \mathbf{B}u$$

The control u(t) is obtained in terms of the feedback matrix $\mathbf{K} = [K_1, K_2, ..., K_N]$

$$u(t) = -\sum_{j=1}^{N} K_j z_j(t)$$

The feedback gain \mathbf{K} is given by

$$\mathbf{K} = \mathbf{R}^{-1} \mathbf{B}^{\top} \mathbf{P} \mathbf{M}$$

where **P** is solution of algebraic Riccati equation (ARE)

$$\mathbf{A}^{\mathsf{T}}\mathbf{P}\mathbf{M} + \mathbf{M}^{\mathsf{T}}\mathbf{P}\mathbf{A} - \mathbf{M}^{\mathsf{T}}\mathbf{P}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^{\mathsf{T}}\mathbf{P}\mathbf{M} + \mathbf{Q} = 0$$

$$(\mathbf{M}, \mathbf{A} - \mathbf{B}\mathbf{K}) \text{ is stable}$$

3.2 Partial information with noise

Consider the linearized model with noise in the model

$$\frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} = \nu \frac{\partial^2 z}{\partial x^2} + \eta \tag{13}$$

$$z(0,t) = u(t), \qquad \frac{\partial z}{\partial r}(1,t) = 0 \tag{14}$$

$$z(x,0) = w_0(x) - w_s(x)$$
(15)

Assume that we have access to partial information corrupted by noise

$$y = Hz + \mu$$

H being a suitable observation operator. We shall consider the case where H is given by

$$Hz(t) = z(1,t)$$

In the FEM setup, we get

$$\mathbf{M} \frac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} = \mathbf{A}\mathbf{z} + \mathbf{B}u + \boldsymbol{\eta}$$
$$\mathbf{v} = \mathbf{H}\mathbf{z} + \boldsymbol{\mu}$$

where the observation operator is approximated as

$$\mathbf{H} = (0, 0, ..., 0, 1)^{\top} \in \mathbb{R}^{N-1}$$

3.3 Estimation problem

Consider the

$$\frac{\partial z_e}{\partial t} + w_s \frac{\partial z_e}{\partial x} + z_e \frac{\mathrm{d}w_s}{\mathrm{d}x} = \nu \frac{\partial^2 z_e}{\partial x^2} + L(Hz - Hz_e)$$
 (16)

$$z_e(0,t) = u(t), \qquad \frac{\partial z_e}{\partial x}(1,t) = 0$$
 (17)

$$z_e(x,0) = 0 (18)$$

In the FEM setup, we have

$$\mathbf{M} \frac{\mathrm{d} \mathbf{z}_e}{\mathrm{d} t} = \mathbf{A} \mathbf{z}_e + \mathbf{B} u + \mathbf{L} (\mathbf{y} - \mathbf{H} \mathbf{z}_e)$$

The filtering gain L is given by

$$\mathbf{L} = \mathbf{M} \mathbf{P}_e \mathbf{H}^{ op} \mathbf{R}_{m{\mu}}^{-1}$$

where \mathbf{P}_e is solution of

$$\mathbf{A}\mathbf{P}_{e}\mathbf{M} + \mathbf{M}\mathbf{P}_{e}\mathbf{A}^{\top} - \mathbf{M}\mathbf{P}_{e}\mathbf{H}^{\top}\mathbf{R}_{\mu}^{-1}\mathbf{H}\mathbf{P}_{e}\mathbf{M} + \mathbf{R}_{\eta} = 0$$

$$(\mathbf{M}, \mathbf{A} - \mathbf{L}\mathbf{H}) \text{ is stable}$$

3.4 Coupled linear system

The feedback is based on estimated solution $u = -\mathbf{K}\mathbf{z}_e$

$$egin{array}{ll} \mathbf{M}rac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} &=& \mathbf{A}\mathbf{z} - \mathbf{B}\mathbf{K}\mathbf{z}_e + oldsymbol{\eta} \ \mathbf{M}rac{\mathrm{d}\mathbf{z}_e}{\mathrm{d}t} &=& \mathbf{L}\mathbf{H}\mathbf{z} + (\mathbf{A} - \mathbf{B}\mathbf{K} - \mathbf{L}\mathbf{H})\mathbf{z}_e + \mathbf{L}oldsymbol{\mu} \end{array}$$

or in matrix form

$$\begin{bmatrix} \mathbf{M} & \mathbf{0} \\ \mathbf{0} & \mathbf{M} \end{bmatrix} \frac{\mathrm{d}}{\mathrm{d}t} \begin{bmatrix} \mathbf{z} \\ \mathbf{z}_e \end{bmatrix} = \begin{bmatrix} \mathbf{A} & -\mathbf{B}\mathbf{K} \\ \mathbf{L}\mathbf{H} & \mathbf{A} - \mathbf{B}\mathbf{K} - \mathbf{L}\mathbf{H} \end{bmatrix} \begin{bmatrix} \mathbf{z} \\ \mathbf{z}_e \end{bmatrix} + \begin{bmatrix} \mathbf{I} & \mathbf{0} \\ \mathbf{0} & \mathbf{L} \end{bmatrix} \begin{bmatrix} \boldsymbol{\eta} \\ \boldsymbol{\mu} \end{bmatrix}$$

The initial condition is given by

$$\mathbf{z}(0) = \mathbf{z}_0, \qquad \mathbf{z}_e(0) = 0$$

This is implemented in program lin_lqg.m

Excercises

- 1. Run program lin_lqg.m
- 2. Check stabilizabilty of (A, B) using the Hautus criterion.
- 3. Set $(\mathbf{Q} = 0)$ which corresponds to minimal norm control. Run the code and observe the solution and control.
- 4. Set $(\mathbf{Q} = I)$ and run the code. How has the solution and control beaviour changed?
- 5. Vary \mathbf{R} in the range (0.01, 10) and observe how the feedback gain \mathbf{K} varies.
- 6. How does the solution and control change when ν is decreased?
- 7. For $\mathbf{Q} = 0$, modify the code to solve the control and estimation problem for only the unstable components. Refer to the codes used for the 1D heat problem.

4 Non-linear system with control

$$\frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} + z \frac{\mathrm{d}z}{\mathrm{d}x} = \nu \frac{\partial^2 z}{\partial x^2}$$
$$z(0, t) = u(t), \quad z_x(1, t) = 0, \quad z(x, 0) = w^{\delta}(x)$$

We multiply by a test function ϕ with $\phi(0) = 0$ to obtain the weak formulation

$$\int_0^1 z_t \phi dx + \nu \int_0^1 \frac{\partial z}{\partial x} \frac{d\phi}{dx} dx + \int_0^1 w_s \frac{\partial z}{\partial x} \phi dx + \int_0^1 z \frac{\partial w_s}{\partial x} \phi dx + \int_0^1 w \frac{dw}{dx} \phi dx = 0$$

The finite element solution can be written as

$$z(x,t) = \sum_{j=1}^{N} z_j(t)\phi_j(x) + u(t)\phi_0(x)$$

while the stationary solution expressed as

$$w_s(x) = \sum_{i=1}^{N} w_s^j \phi_j(x) + u_s \phi_0(x)$$

The Galerkin approximation is

$$\int_{0}^{1} z_{t} \phi_{i} dx = -\nu \int_{0}^{1} \frac{\partial z}{\partial x} \frac{d\phi_{i}}{dx} dx - \int_{0}^{1} w_{s} \frac{\partial z}{\partial x} \phi_{i} dx - \int_{0}^{1} z \frac{\partial w_{s}}{\partial x} \phi_{i} dx$$
$$- \int_{0}^{1} z \frac{dz}{dx} \phi_{i} dx, \qquad \forall i = 1, 2, ..., N$$

Ignoring the $\frac{du}{dt}$ term and using the expression for w_s , we get

$$\begin{split} \sum_{j=1}^{N} z_j'(t) \int_0^1 \phi_i \phi_j \mathrm{d}x &= -\sum_{j=1}^{N} \sum_{k=1}^{N} z_j(t) z_k(t) \int_0^1 \phi_j \phi_k' \phi_i \mathrm{d}x \\ &- \sum_{j=1}^{N} z_j(t) \left[\nu \int_0^1 \phi_i' \phi_j' \mathrm{d}x + u_s \int_0^1 \phi_i (\phi_0 \phi_j)' \mathrm{d}x \right] \\ &- \sum_{j=1}^{N} z_j(t) \left[\sum_{k=1}^{N} w_s^k(t) \left(\int_0^1 \phi_j \phi_k' \phi_i \mathrm{d}x + \int_0^1 \phi_k \phi_j' \phi_i \mathrm{d}x \right) \right] \\ &- u(t) \left[\sum_{j=1}^{N} z_j \int_0^1 \phi_i (\phi_0 \phi_j)' \mathrm{d}x + \sum_{k=1}^{N} w_s^k \int_0^1 \phi_i (\phi_0 \phi_k)' \mathrm{d}x \right] \\ &- u(t) \left[\nu \int_0^1 \phi_i' \phi_0' \mathrm{d}x + 2u_s \int_0^1 \phi_i \phi_0 \phi_0' \mathrm{d}x \right] - u(t)^2 \int_0^1 \phi_i \phi_0 \phi_0' \mathrm{d}x \end{split}$$

Thus we have the system

$$\mathbf{M} \frac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} = \mathbf{R}\mathbf{H}\mathbf{S}_1 + \mathbf{R}\mathbf{H}\mathbf{S}_2$$

where

$$\mathbf{RHS}_1(i) = -\mathbf{z}^{\top} \mathbf{D}1(:,:,i)\mathbf{z} - \left[\nu \mathbf{A}1(i,:) + u_s \mathbf{A}2(i,:) + \mathbf{w}_s^{\top} (\mathbf{D}1(:,:,i) + \mathbf{D}1(:,:,i)^{\top})\right] \mathbf{z}$$

$$\mathbf{RHS}_2(i) = -u(t) \left[\mathbf{A}2(\mathbf{z} + \mathbf{w}_s) + 2u_s \mathbf{d}1 + \nu \mathbf{d}2\right] - u(t)^2 \mathbf{d}1$$

The control u(t) is obtained from the linear estimation problem

$$u(t) = -\sum_{j=1}^{N} K_j z_e^j$$

We solve the non-linear system and the linear estimator in a coupled manner.

$$\mathbf{M} \frac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} = \mathbf{R}\mathbf{H}\mathbf{S}_1 + \mathbf{R}\mathbf{H}\mathbf{S}_2$$

$$\mathbf{M} \frac{\mathrm{d}\mathbf{z}_e}{\mathrm{d}t} = \mathbf{L}\mathbf{H}\mathbf{z} + (\mathbf{A} - \mathbf{B}\mathbf{K} - \mathbf{L}\mathbf{H})\mathbf{z}_e$$

$$\mathbf{z}(0) = \mathbf{z}_0, \qquad \mathbf{z}_e(0) = 0$$

This is implemented in burger_lqg.m

4.1 Excercises

- 1. Run program burger_lqg.m
- 2. Vary \mathbf{R} in the range (0.01, 10) and observe how the feedback gain \mathbf{K} changes. How does the solution and control change with \mathbf{R} .

5 List of Programs

- 1. get_system_mat.m: Computes FEM matrices
- 2. feedback_matrix.m: Computes feedback matrix
- 3. stationarysol.m: Computes exact unstable stationary solution
- 4. burger.m: Solves the non-linear model, without feedback
- 5. lin_est.m: Solves the coupled estimation and control system for the linear problem
- 6. burger_lqg.m: Solves the coupled estimation and control system for the non-linear problem
- 7. rhs_burger.m: Computes the right hand side for the non-linear problem, without feedback

8.	<pre>rhs_burger_lqg.m: Computes the right hand side for coupled estimation and control system with the non-linear problem</pre>