

# System dynamics

## -Final Project

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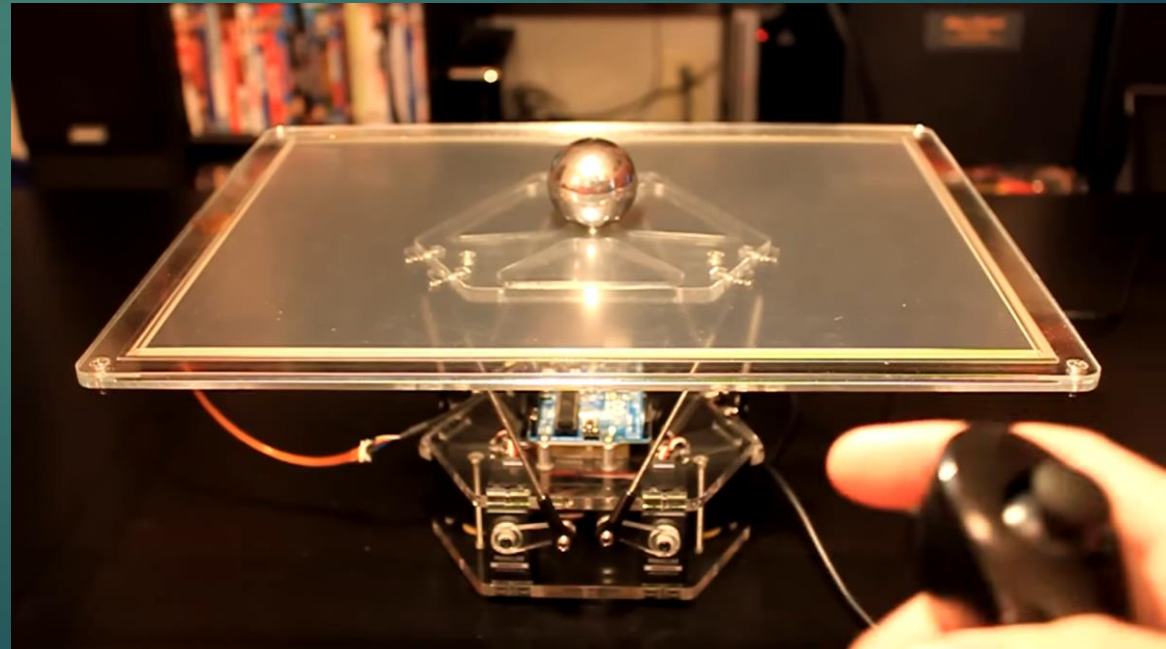
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# Outline

- ▶ Introduction
- ▶ Mathematical modelling
- ▶ State-space model
- ▶ Simulation

# Introduction

- ▶ Topic: Modelling and Control of Ball-Plate System
- ▶ Goal: To control the ball movement by manipulating the inclination of the plate using system dynamics modelling skills.



# Mathematical Modelling

Assumptions:

- ▶ There is no slipping for ball
- ▶ The ball is completely symmetric and homogeneous
- ▶ All frictions are neglected
- ▶ The ball and the plate contact all the time

# Mathematical Modelling

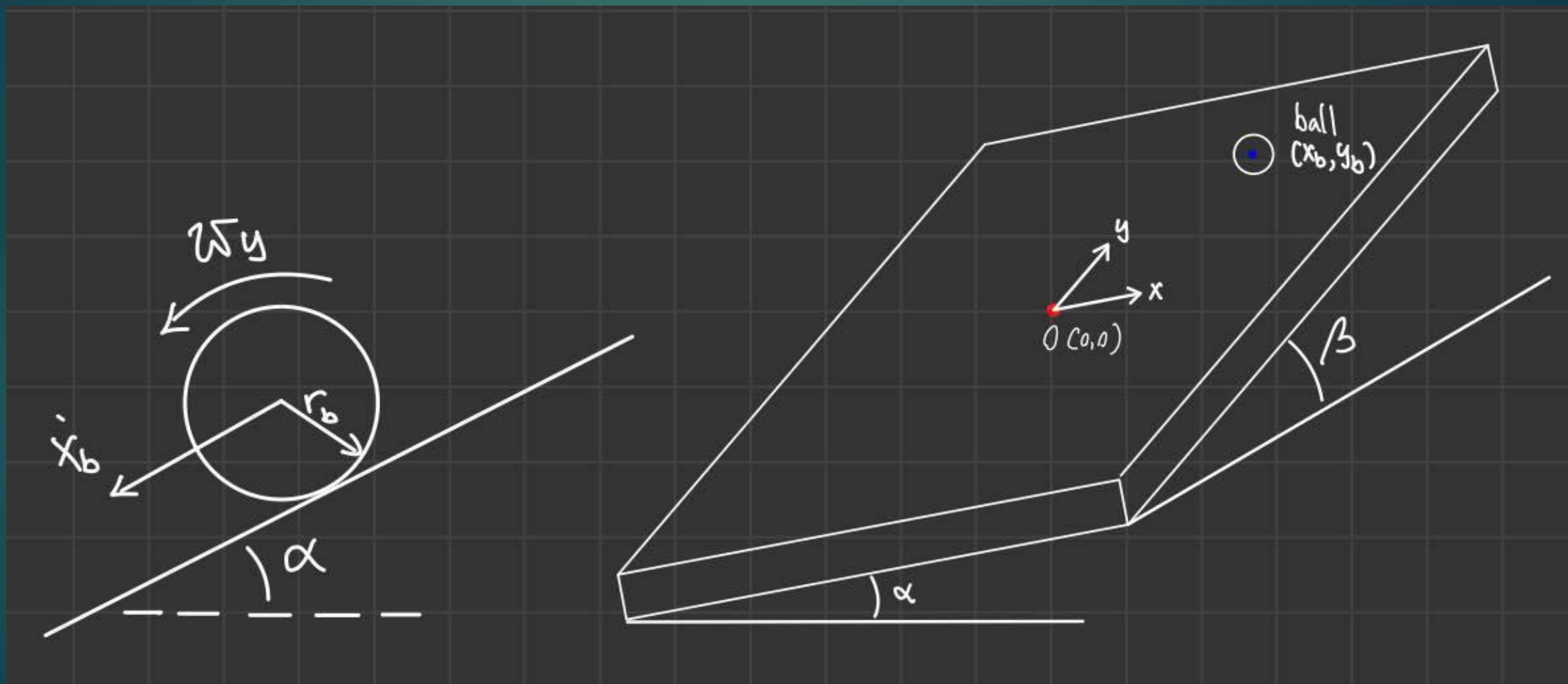
The system has 4 degree of freedom:

- ▶  $x_b, y_b$ : The position of the ball on the plate

(The center of x-y coordinate is at the center of the plate)

- ▶  $\alpha, \beta$ : The inclination of the plate

# Mathematical Modelling



# Mathematical Modelling

- ▶ Kinetic energy of the ball:

$$T_b = \frac{1}{2} m_b (\dot{x}_b^2 + \dot{y}_b^2) + \frac{1}{2} I_b (\omega_x^2 + \omega_y^2)$$

- ▶ Relationship between translational and rotational velocity

$$\dot{x}_b = r_b \omega_y, \dot{y}_b = r_b \omega_x$$

- ▶ Substitute the velocity relationship into kinetic energy

$$T_b = \frac{1}{2} \left( m_b + \frac{I_b}{r_b^2} \right) (\dot{x}_b^2 + \dot{y}_b^2)$$

# Mathematical Modeling

- Kinetic energy of the plate

$$T_p = \frac{1}{2}(I_p + I_b)(\dot{\alpha}^2 + \dot{\beta}^2) + \frac{1}{2}m_b(x_b\dot{\alpha} + y_b\dot{\beta})^2$$

- Kinetic energy of the system

$$\begin{aligned} T &= T_b + T_p \\ &= \frac{1}{2}\left(m_b + \frac{I_b}{r_b^2}\right)(\dot{x}_b^2 + \dot{y}_b^2) + \frac{1}{2}(I_p + I_b)(\dot{\alpha}^2 + \dot{\beta}^2) + \frac{1}{2}m_b(x_b\dot{\alpha} + y_b\dot{\beta})^2 \end{aligned}$$



# Mathematical Modelling

- Potential energy of the ball (relative to the center of the inclined plate)

$$V_b = m_b g (x_b \sin \alpha + y_b \sin \beta)$$

- Derive the system's equation using Lagrange's Equation

$$L = T_b + T_p - V_b$$

$$\frac{\partial L}{\partial \dot{\alpha}} = (I_p + I_b) \dot{\alpha}_x + m_b x_b (x_b \dot{\alpha} + y_b \dot{\beta}) \quad , \quad \frac{\partial L}{\partial \alpha} = -m_b g x_b \cos \alpha$$

$$\frac{\partial L}{\partial \dot{\beta}} = (I_p + I_b) \dot{\beta}_x + m_b y_b (x_b \dot{\alpha} + y_b \dot{\beta}) \quad , \quad \frac{\partial L}{\partial \beta} = -m_b g y_b \cos \beta$$

# Mathematical Modelling

► Conti.

$$\frac{\partial L}{\partial \dot{x}_b} = \left( m_b + \frac{I_b}{r_b^2} \right) \dot{x}_b \quad , \quad \frac{\partial L}{\partial x_b} = m_b (x_b \ddot{\alpha} + y_b \dot{\beta}) \dot{\alpha} - m_b g \sin \alpha$$

$$\frac{\partial L}{\partial \dot{y}_b} = \left( m_b + \frac{I_b}{r_b^2} \right) \dot{y}_b \quad , \quad \frac{\partial L}{\partial y_b} = m_b (x_b \ddot{\alpha} + y_b \dot{\beta}) \dot{\beta} - m_b g \sin \beta$$

# Mathematical Modelling

- From Lagrange-Euler equation:

$$\begin{aligned} \frac{d}{dt} \frac{\partial T}{\partial \dot{\alpha}} - \frac{\partial L}{\partial \alpha} \\ = (I_p + I_b) \ddot{\alpha} + 2m_b x_b \dot{x}_b \dot{\alpha} + m_b x_b^2 \ddot{\alpha} + m_b x_b y_b \ddot{\beta} + m_b \dot{x}_b y_b \dot{\beta} \\ + m_b x_b \dot{y}_b \dot{\beta} + m_b g x_b \cos \alpha = \tau_x \end{aligned}$$

$$\begin{aligned} \frac{d}{dt} \frac{\partial T}{\partial \dot{\beta}} - \frac{\partial L}{\partial \beta} \\ = (I_p + I_b) \ddot{\beta} + 2m_b y_b \dot{y}_b \dot{\beta} + m_b y_b^2 \ddot{\beta} + m_b x_b y_b \ddot{\alpha} + m_b \dot{x}_b y_b \dot{\alpha} \\ + m_b x_b \dot{y}_b \dot{\alpha} + m_b g y_b \cos \beta = \tau_y \end{aligned}$$

# Mathematical Modelling

► Conti.

$$\frac{d}{dt} \frac{\partial T}{\partial \dot{x}_b} - \frac{\partial L}{\partial x_b} = \left( m_b + \frac{I_b}{r_b^2} \right) \ddot{x}_b - m_b x_b \dot{\alpha}^2 - m_b y_b \dot{\alpha} \dot{\beta} + m_b g \sin \alpha = 0$$

$$\frac{d}{dt} \frac{\partial T}{\partial \dot{y}_b} - \frac{\partial L}{\partial y_b} = \left( m_b + \frac{I_b}{r_b^2} \right) \ddot{y}_b - m_b y_b \dot{\beta}^2 - m_b x_b \dot{\alpha} \dot{\beta} + m_b g \sin \beta = 0$$

# Mathematical Modelling

► Non-linear differential equations:

$$\left\{ \begin{array}{l} \left( m_b + \frac{I_b}{r_b^2} \right) \ddot{x}_b - m_b x_b \dot{\alpha}^2 - m_b y_b \dot{\alpha} \dot{\beta} + m_b g \sin \alpha = 0 \\ \left( m_b + \frac{I_b}{r_b^2} \right) \ddot{y}_b - m_b y_b \dot{\beta}^2 - m_b x_b \dot{\alpha} \dot{\beta} + m_b g \sin \beta = 0 \\ (I_p + I_b) \ddot{\alpha} + 2m_b x_b \dot{x}_b \dot{\alpha} + m_b x_b^2 \ddot{\alpha} + m_b x_b y_b \ddot{\beta} + m_b \dot{x}_b y_b \dot{\beta} + m_b x_b \dot{y}_b \dot{\beta} + m_b g x_b \cos \alpha = \tau_x \\ (I_p + I_b) \ddot{\beta} + 2m_b y_b \dot{y}_b \dot{\beta} + m_b y_b^2 \ddot{\beta} + m_b x_b y_b \ddot{\alpha} + m_b \dot{x}_b y_b \dot{\alpha} + m_b x_b \dot{y}_b \dot{\alpha} + m_b g y_b \cos \beta = \tau_y \end{array} \right.$$

# State-space Model of System

$$B = m/(m + I_b/r_b^2)$$

- Define state variable

$$X = [x_1, x_2, x_3, x_4, x_5, x_6, x_7, x_8]^T = [x_b, \dot{x}_b, \alpha, \dot{\alpha}, y_b, \dot{y}_b, \beta, \dot{\beta}]^T$$

- Input

$$U = [u_x, u_y]^T = [\ddot{\alpha}, \ddot{\beta}]^T$$

- State-space equation:  $\dot{x} = f(x, u)$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \\ \dot{x}_5 \\ \dot{x}_6 \\ \dot{x}_7 \\ \dot{x}_8 \end{bmatrix} = \begin{bmatrix} x_2 \\ B(x_1 x_4^2 + x_4 x_5 x_8 - g \sin x_3) \\ x_4 \\ 0 \\ x_6 \\ B(x_5 x_8^2 + x_1 x_4 x_8 - g \sin x_7) \\ x_8 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 1 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} u_x \\ u_y \end{bmatrix}$$

# Model Linearization

- ▶ The approximate value for a solid ball's momentum of inertia is

$$I_{ball} = \frac{2}{5} m_b r_b^2$$

- ▶ Small angle of inclination of the plate  
max  $\pm 5^\circ$

- ▶ Slow rate of change of the plate  
 $\dot{\alpha} \cong 0, \dot{\beta} \cong 0$

# Model linearization

- ▶ Using the assumption:

$$\begin{cases} \frac{7}{5}\ddot{x}_b + g\alpha = 0 \\ \frac{7}{5}\ddot{y}_b + g\beta = 0 \end{cases}$$

- ▶ Transfer function:

$$P_x(s) = \frac{X_b(s)}{\alpha(s)} = \frac{g}{\frac{7}{5}s^2}, P_y(s) = \frac{Y_b(s)}{\beta(s)} = \frac{g}{\frac{7}{5}s^2}$$



# Model linearization

$$B = m/(m + I_b/r_b^2)$$

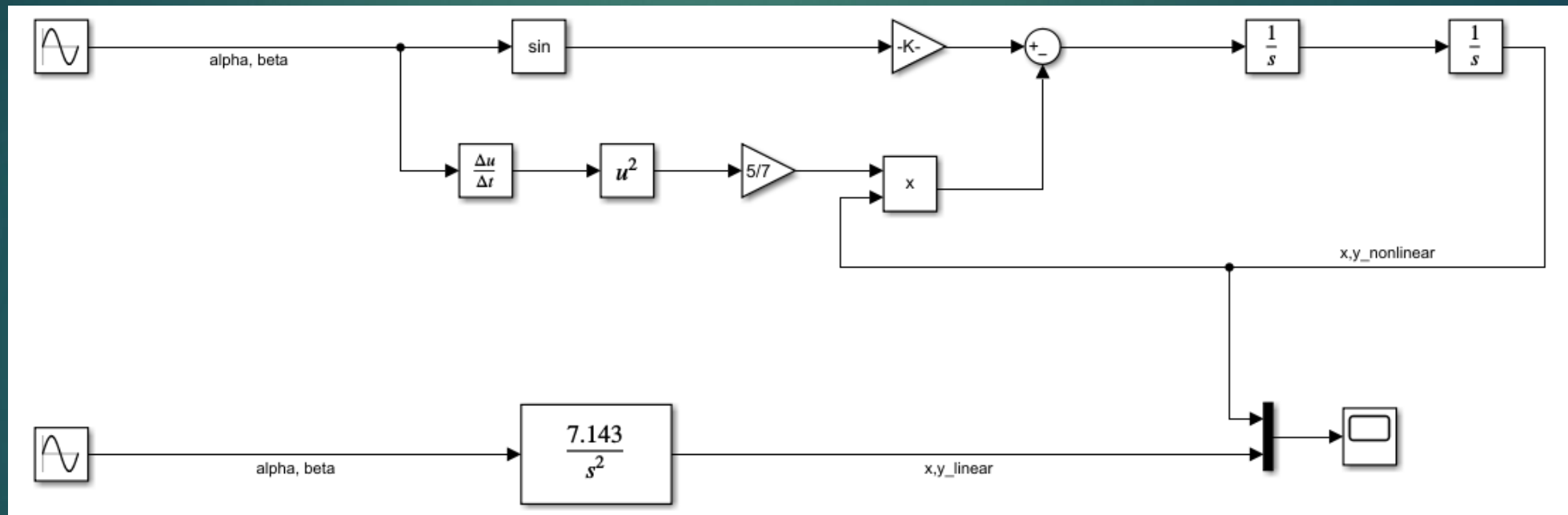
## ► Simplified State-space equations

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} x_2 \\ B(x_1 x_4^2 - g \sin x_3) \\ x_4 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} [u_x]$$

$$\begin{bmatrix} \dot{x}_5 \\ \dot{x}_6 \\ \dot{x}_7 \\ \dot{x}_8 \end{bmatrix} = \begin{bmatrix} x_6 \\ B(x_5 x_8^2 - g \sin x_7) \\ x_8 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} [u_y]$$

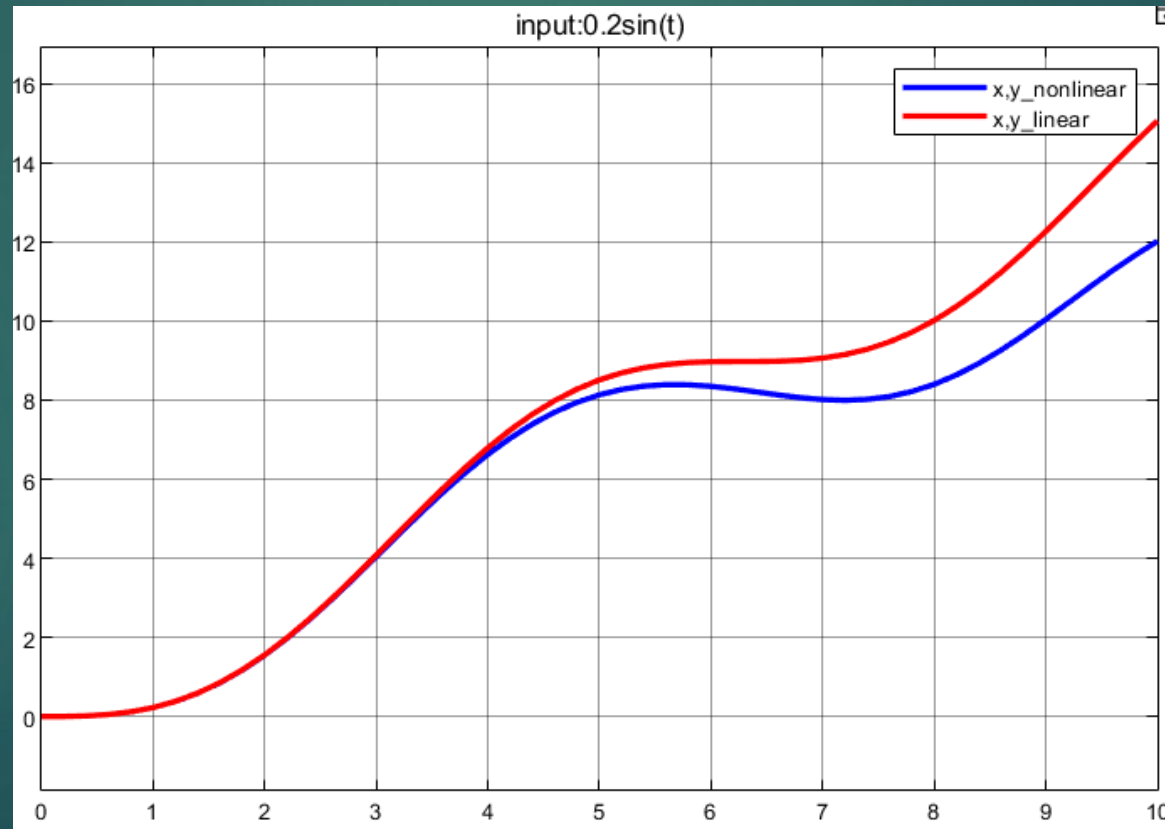
# Simulation

## ► Linear vs Nonlinear (Open-loop)



# Simulation

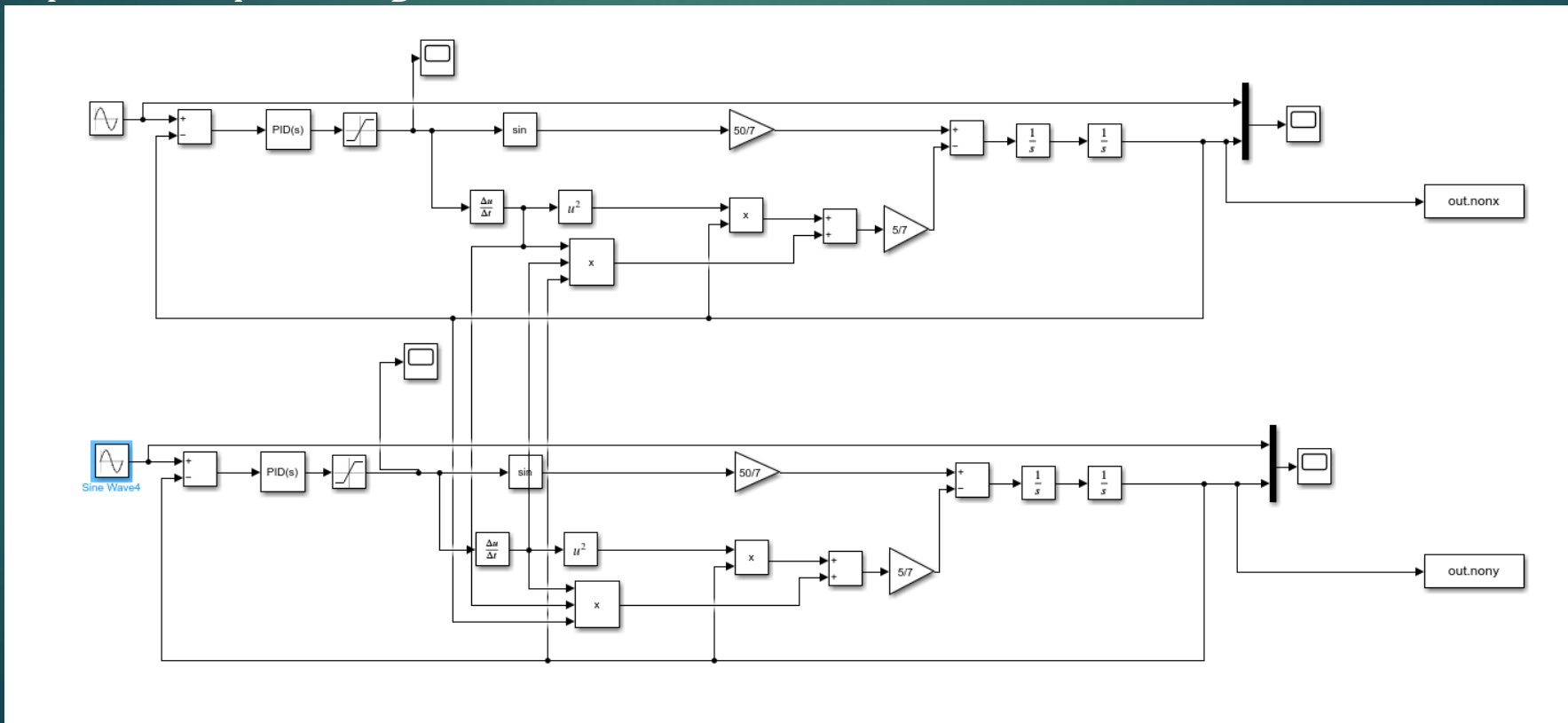
## ► Linear vs Nonlinear (Open-loop)



# Simulation

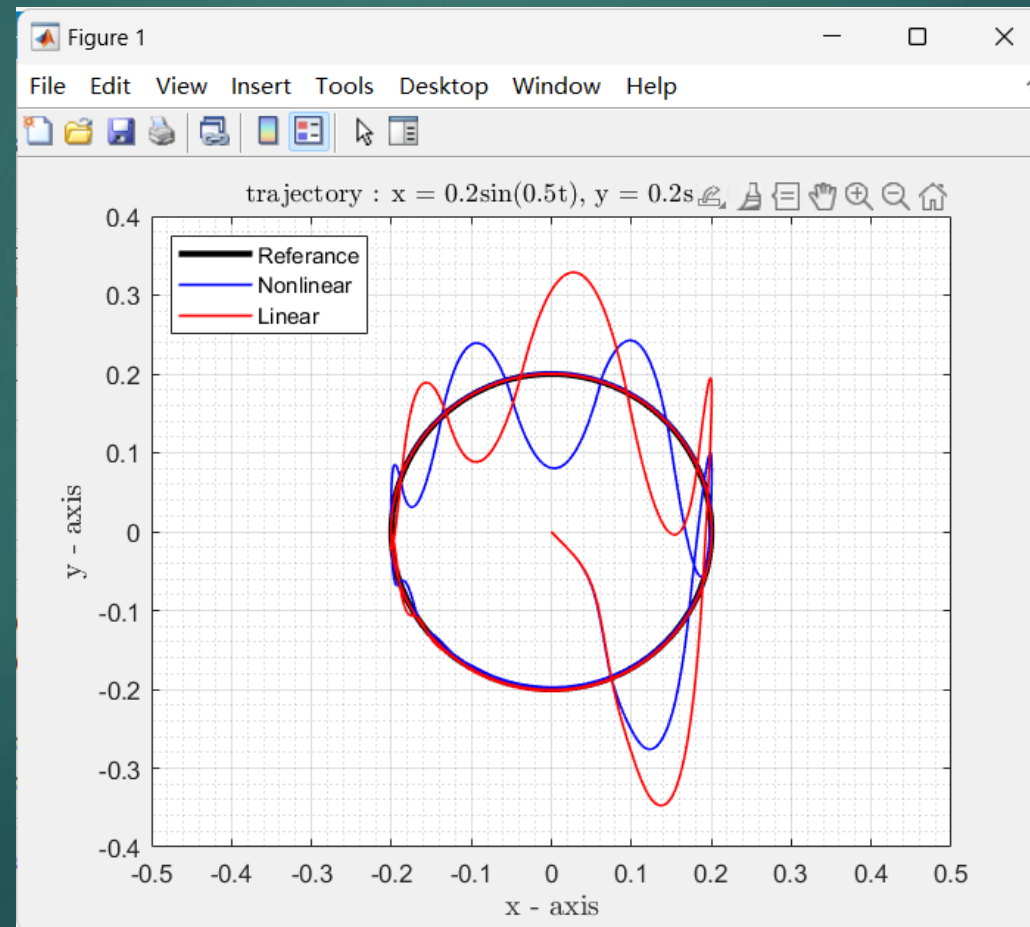
- ▶ Linear vs Nonlinear (Closed-loop with controller)

$$K_P = 20, K_I = 8, K_D = 0.8$$



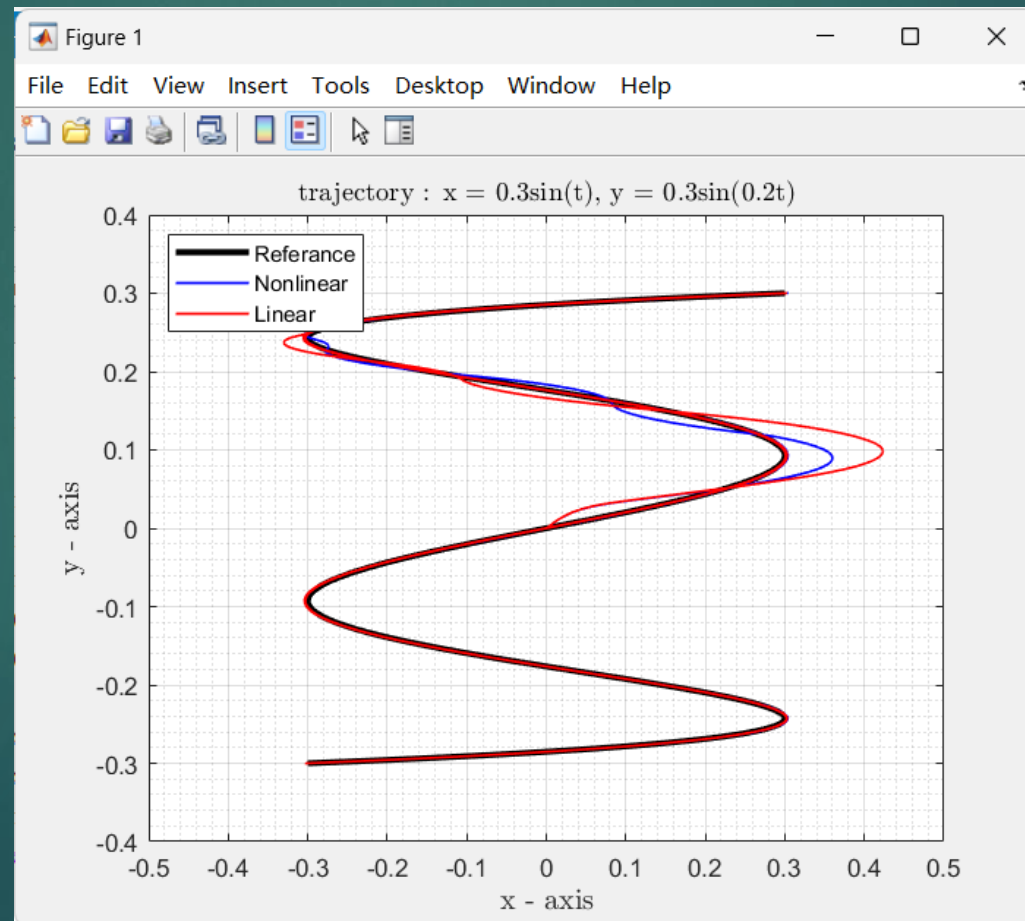
# Simulation

## ► Trajectory



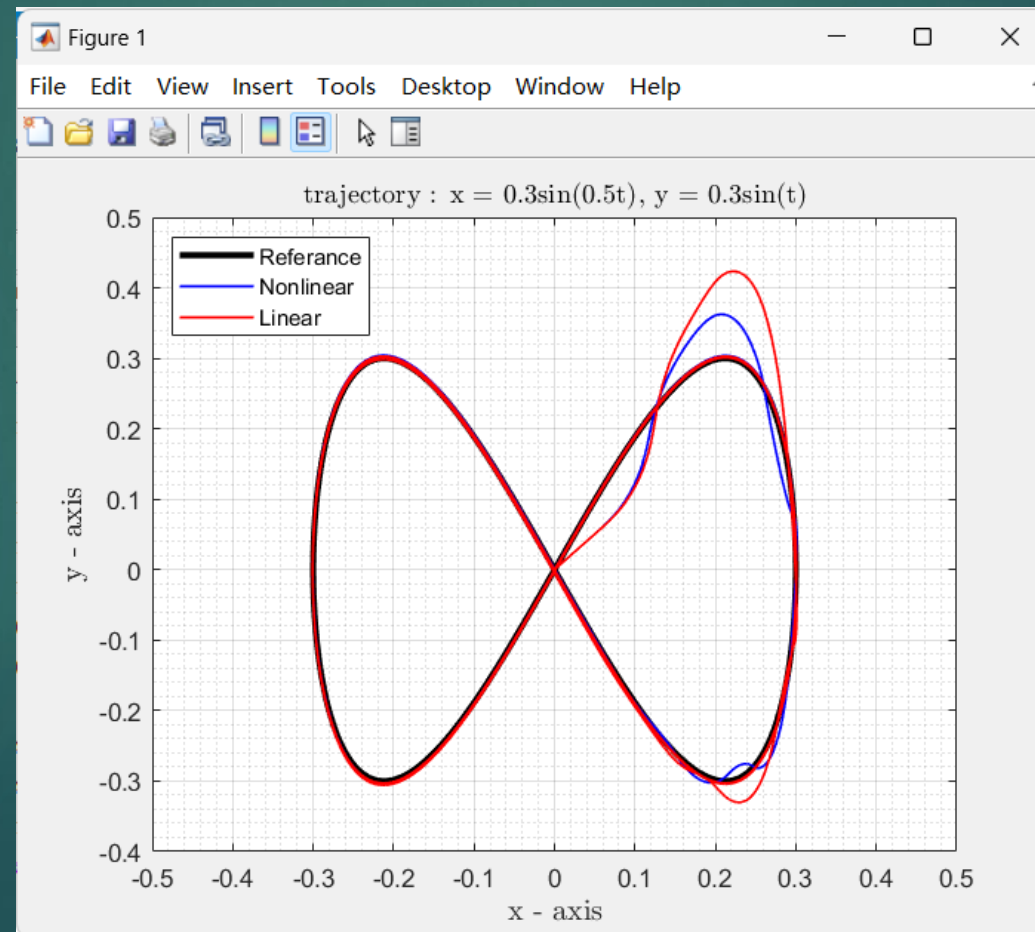
# Simulation

## ► Trajectory



# Simulation

## ► Trajectory



# Reference

- ▶ [https://danielkhashabi.com/files/2011\\_LinearControl/16.pdf?fbclid=IwAR32t0vXbLgzi49\\_VxvLlxpme5q-n2DMQGj-ARruBSO65rzpqx0SGznseoE](https://danielkhashabi.com/files/2011_LinearControl/16.pdf?fbclid=IwAR32t0vXbLgzi49_VxvLlxpme5q-n2DMQGj-ARruBSO65rzpqx0SGznseoE)
- ▶ <https://ieeexplore.ieee.org/document/5358057?fbclid=IwAR2CJaGvA5cRR3sEPtnjGX8TNj01idFzQ18fTaErlFWHLDgydlVeG3eMow>



Thank you!