

# Assignment 4 Report

## ELEC 4700

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Submitted: Sunday April 5<sup>th</sup>, 2019



## 1 Part 3: Report on the work done in PA 7

### 1.1 Part A: Write out the matrices C and G

```
%X = [V1,V2,IL,V3,V4,V0]

G =[1    0          0 0          0 0;
    G_1 -(G_1+G_2) -1 0          0 0;
    0   -1          0 1          0 0;
    0   0          1 -G_3        0 0;
    0   0          0 -alpha*G_3 1 0;
    0   0          0 0          G_4 -(G_4+G_0)];

C =[0          0          0 0 0 0;
    Capacitor -Capacitor 0 0 0 0;
    0          0          L 0 0 0;
    0          0          0 0 0 0;
    0          0          0 0 0 0;
    0          0          0 0 0 0];

%F = [Vin;0;0;0;0;0];
```

Figure 1: G and C matrices for modelling the circuit from PA 7

## 1.2 Part B: DC and AC sweeps of the circuit

### 1.2.1 Section i. DC sweep for input voltages -10 to 10V

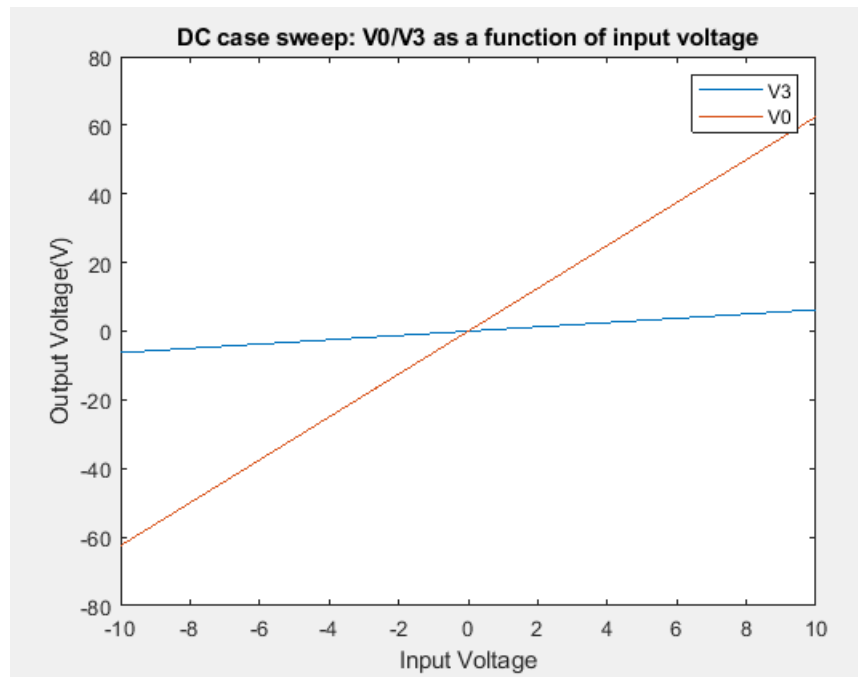


Figure 2: Sweep of the input voltage  $V_{in}$  from -10V to 10V and a plot of the output voltage  $V_O$  and the voltage at  $V_3$

### 1.2.2 Section ii. AC sweep for output voltage as a function of frequency $\omega$ and a plot of gain

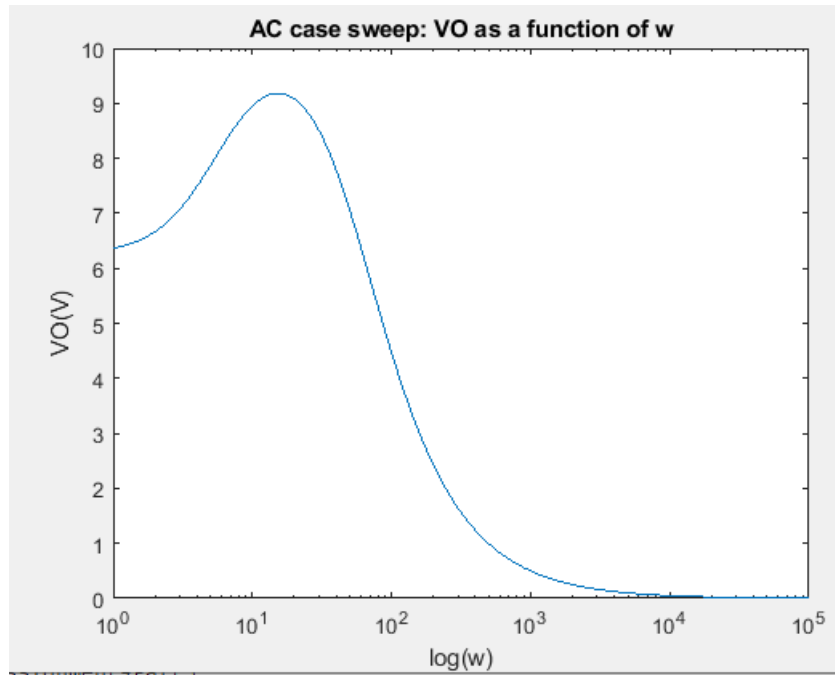


Figure 3: Plot for the AC case of the output voltage  $V_0$  as a function of  $\log(\omega)$

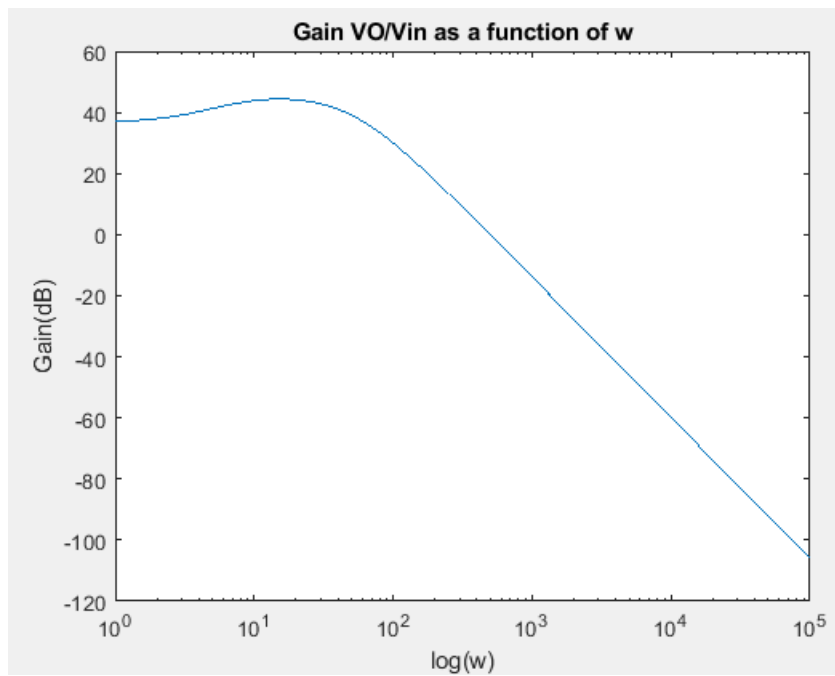


Figure 4: Plot of the gain  $V_0/V_{in}$  as function of  $\log(\omega)$

### 1.2.3 Section iii. AC gain as a function of random perturbations on C plotted on a histogram

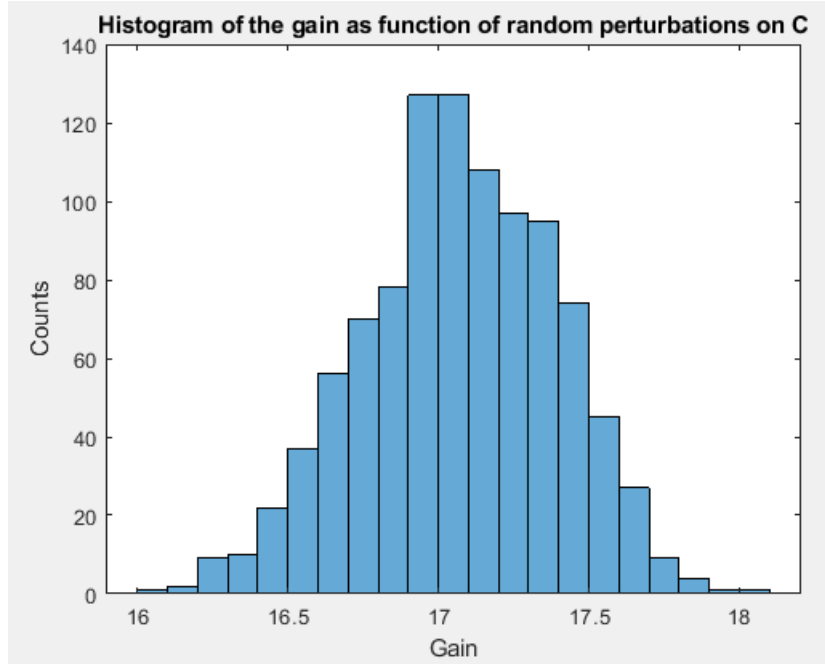


Figure 5: Histogram of the gain with random perturbations on the capacitor (C) using a normal distribution

## 2 Part 4: Transient circuit simulation

### 2.1 Part A: What type of circuit is this?

By inspection this circuit appears to be a low pass filter because the gain and output voltage is high at low frequencies. The gain/output voltage approach zero as the frequency increases.

### 2.2 Part B: What sort of frequency response would you expect?

Since this is a low pass filter we would expect the frequency to respond by being rejected/attenuated at higher frequencies while allowing the low frequencies to pass.

### 2.3 Part C: Derive a formulation using finite difference for the numerical solution of this equation in the time domain

Given the formula given to describe the circuit in the time domain,

$$C \frac{dV(t)}{dt} + GV(t) = F \quad (1)$$

this can be rearranged using finite difference to get the numerical solution to the equation in the time domain,

$$C \left[ \frac{V(t + dt) - V(t)}{dt} \right] + GV(t) = F$$
$$V(t) = \left[ \frac{C}{dt} + G \right]^{-1} \left[ F + C \frac{V(t)}{dt} \right] \quad (2)$$

## 2.4 Part D: Simulation

### 2.4.1 Plots of $V_{in}$ and $V_{out}$ from numerical solution in time domain

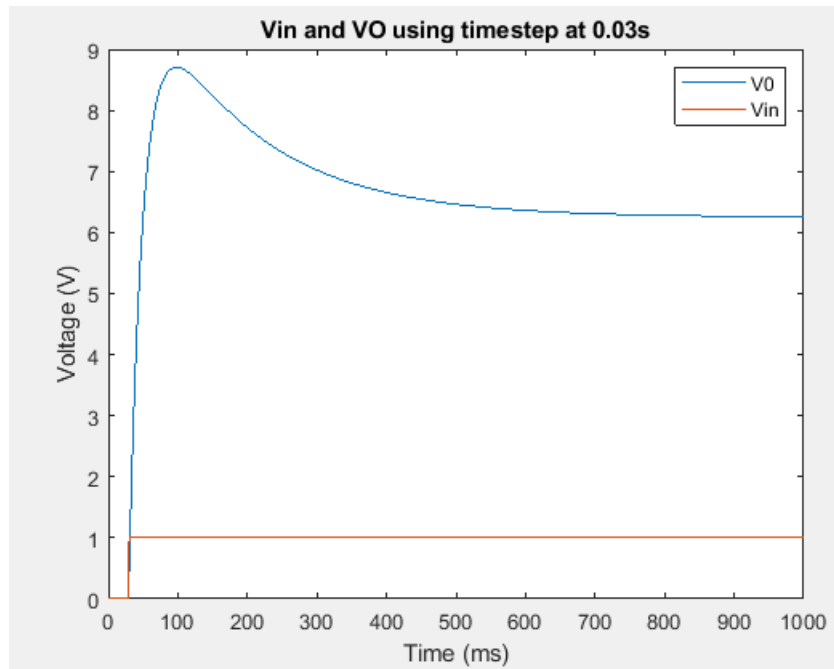


Figure 6: Plot of time step input signal that transitions from 0 to 1 at 0.03s. in the time domain

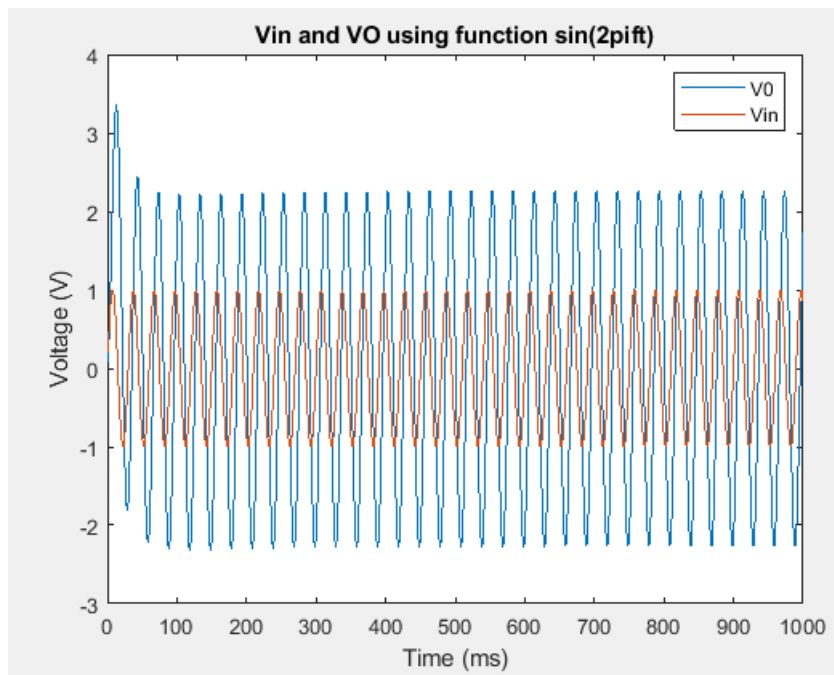


Figure 7: An input signal that is a  $\sin(2\pi f t)$  function with  $f = 1/(0.03)$  1/s in the time domain

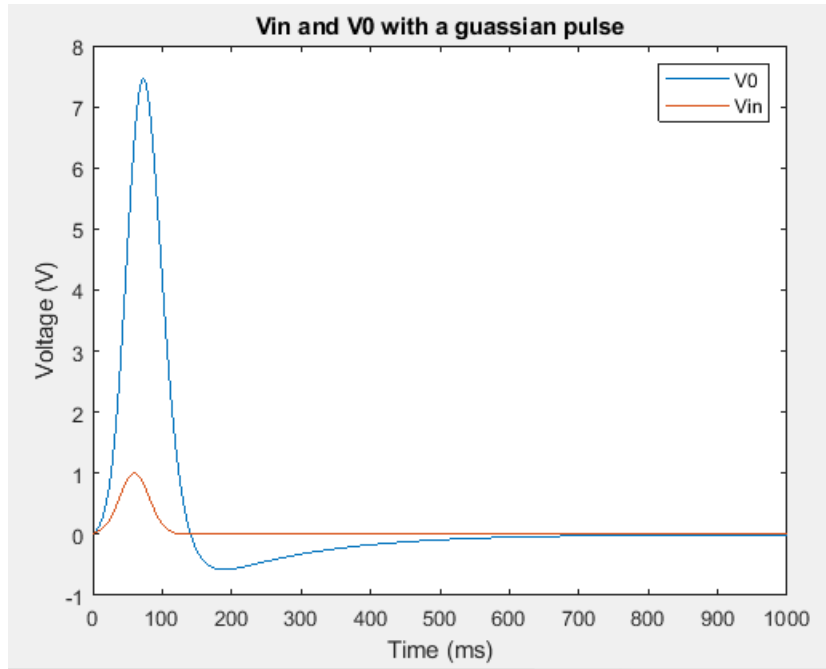


Figure 8: A Gaussian pulse with a magnitude of 1, std dev. of 0.03s and a delay of 0.06s in the time domain

#### 2.4.2 Plots of the frequency content of Vin and Vout from Fourier Transform plots of Frequency response

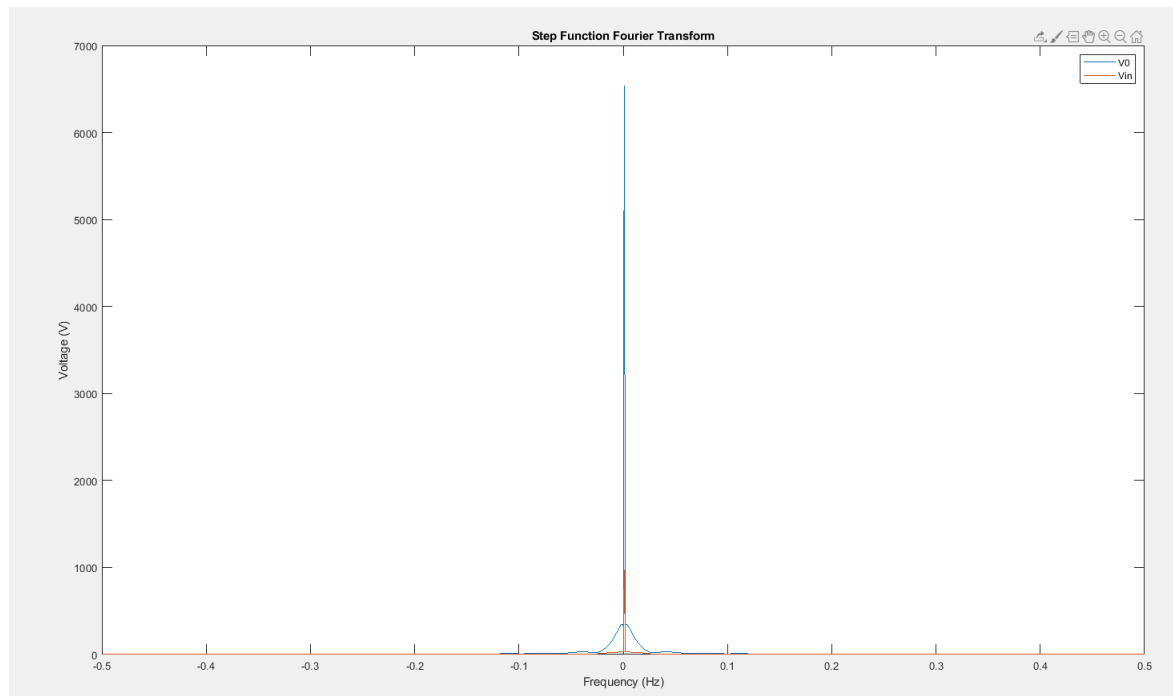


Figure 9: Fourier transform result of the time step

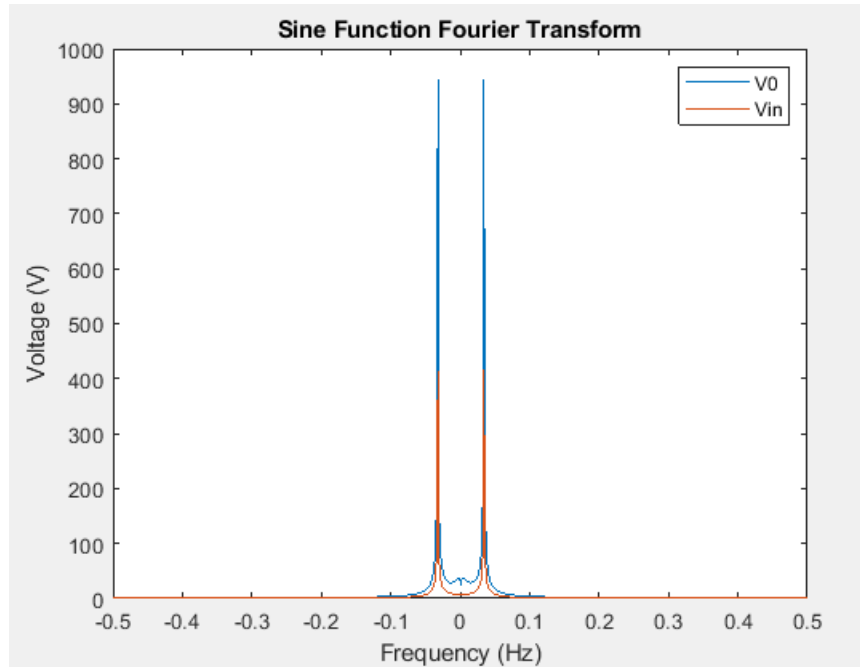


Figure 10: Fourier transform result of the sine wave input signal

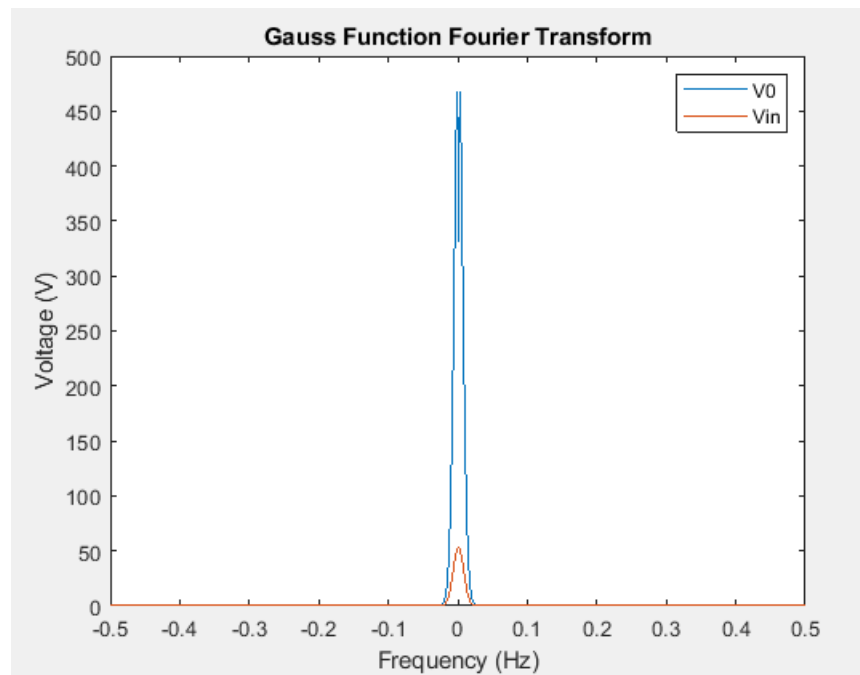


Figure 11: Fourier transform result of the Gaussian input signal



### 3 Part 5: Circuit with Noise

#### 3.1 Part A/B: Updated matrix due to added capacitor in circuit

```
%X = [V1,V2,IL,V3,V4,V0]

G =[1 0 0 0 0 0;
    G_1 -(G_1+G_2) -1 0 0 0;
    0 -1 0 1 0 0;
    0 0 1 -G_3 0 0;
    0 0 0 -alpha*G_3 1 0;
    0 0 0 0 G_4 -(G_4+G_0)];

C =[0 0 0 0 0 0;
    Capacitor -Capacitor 0 0 0 0;
    0 0 L 0 0 0;
    0 0 0 -C_n 0 0;
    0 0 0 0 0 0;
    0 0 0 0 0 0];

F = [Vin;0;0;0;0;0];
```

Figure 12: Updated matrix to include the new capacitor  $C_n$  that is in parallel with the  $R_3$  resistor

#### 3.2 Part C: Simulation

##### 3.2.1 Section iv. New output of V0

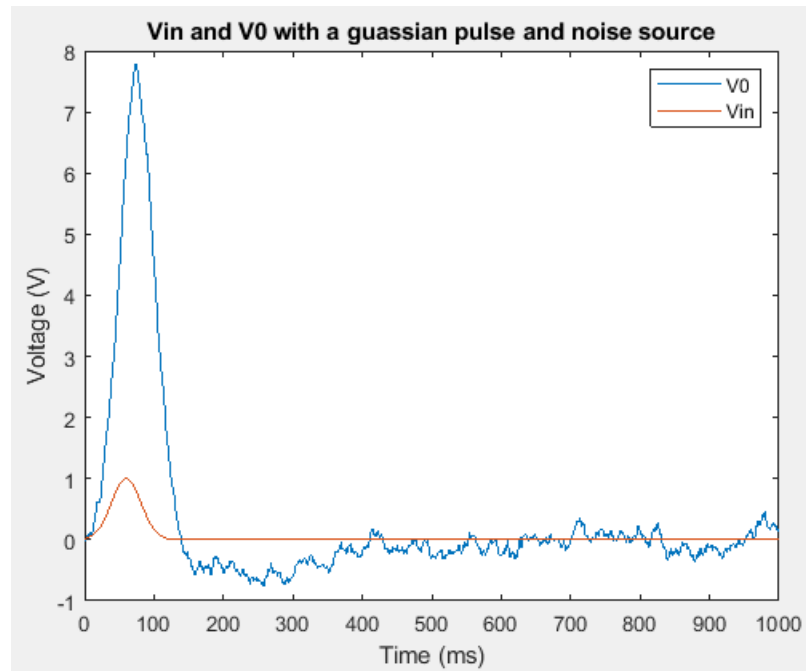


Figure 13: Model the output voltage (V0) signal with noise using the Gaussian excitation

### 3.2.2 Section v. Fourier transfer of V0

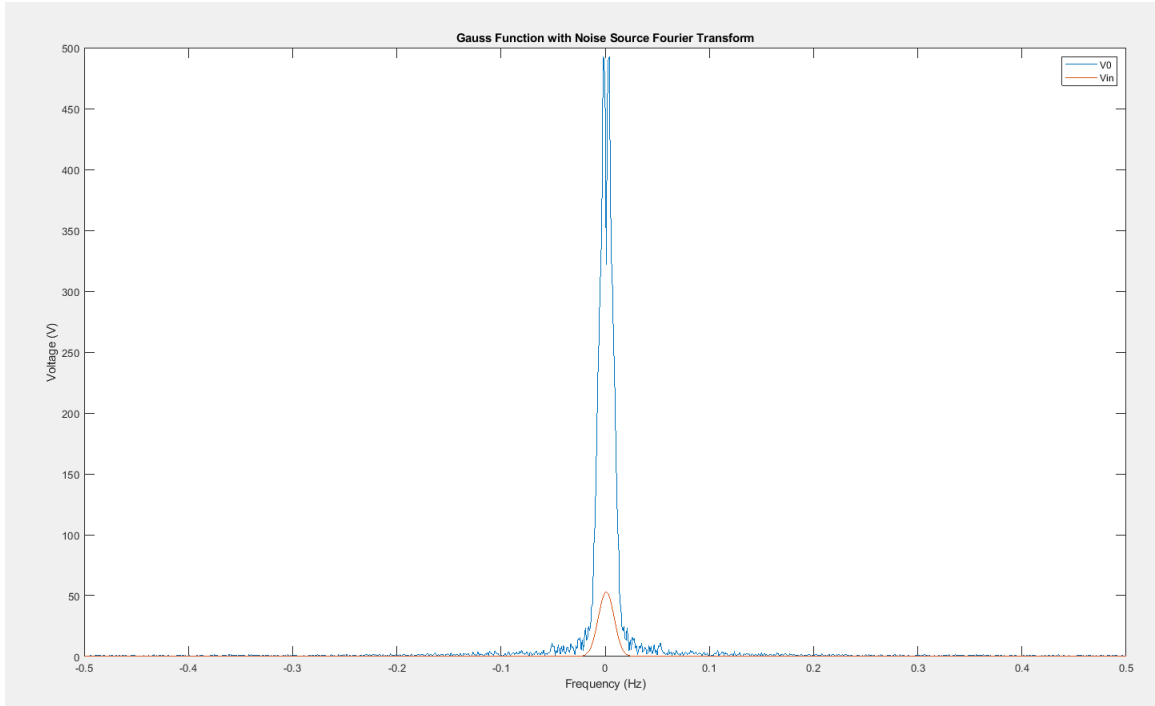


Figure 14: The Fourier transform of the noise plot

### 3.2.3 Section vi. Varying $C_n$ to see how the bandwidth changes

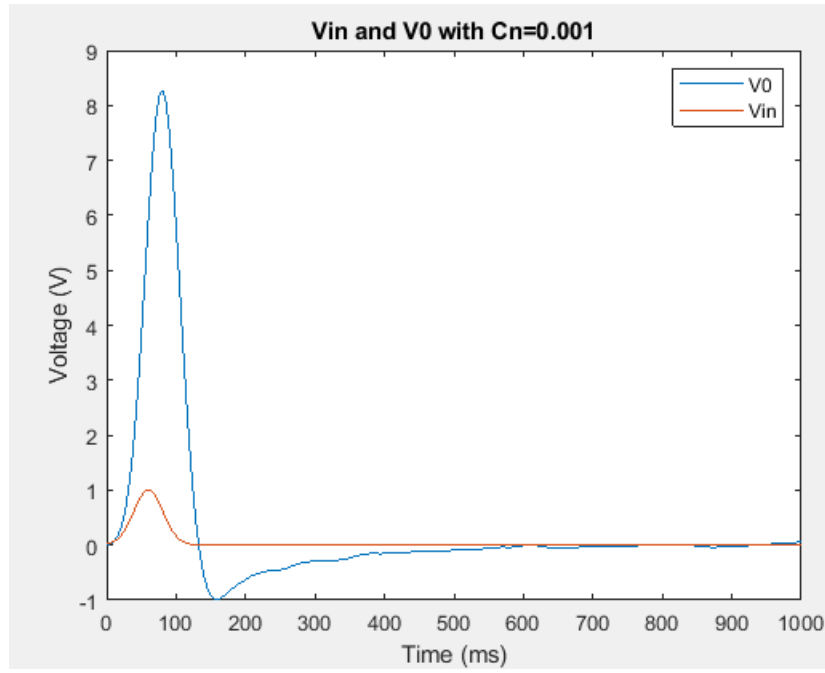


Figure 15: Plot of the output voltage using a capacitor of  $C_n=0.001$

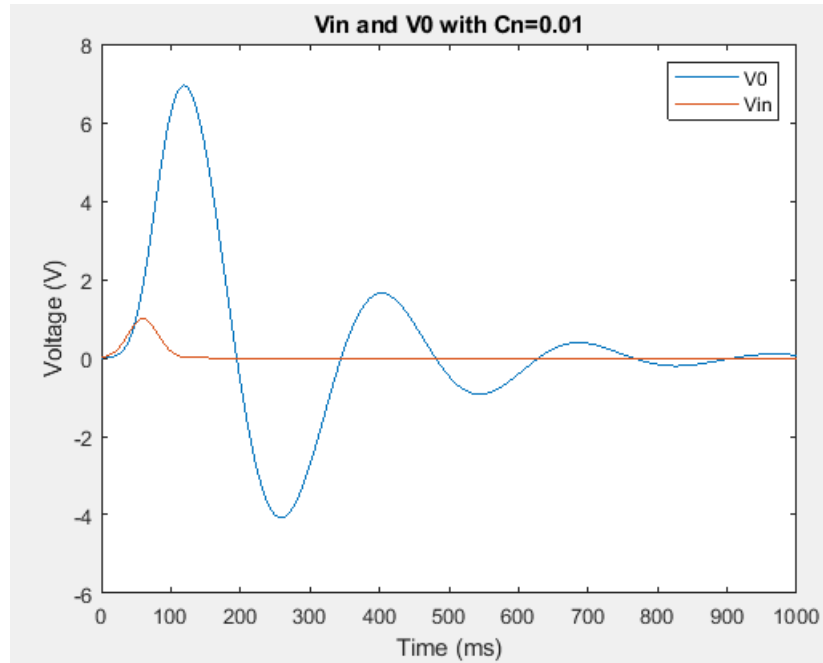


Figure 16: Plot of the output voltage using a capacitor of  $C_n=0.01$

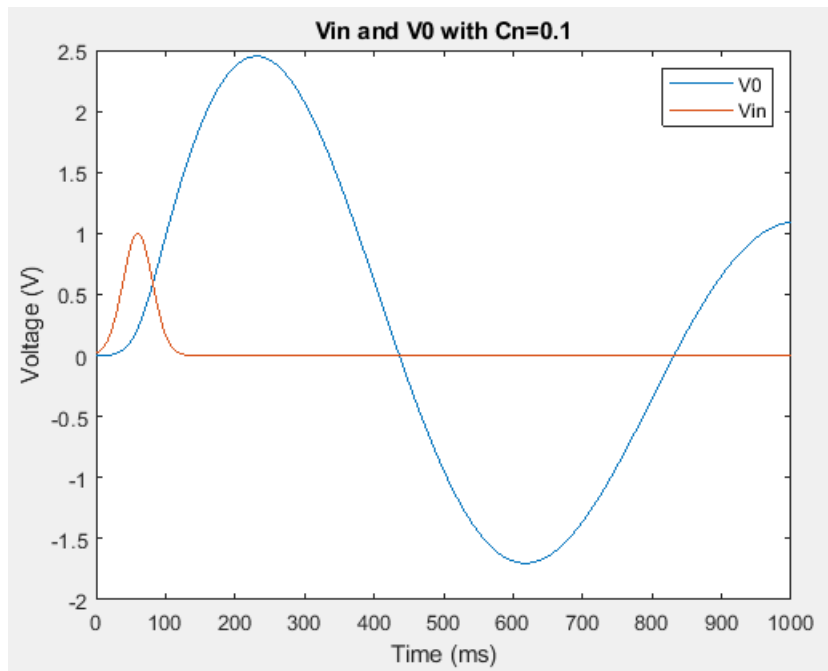


Figure 17: Plot of the output voltage using a capacitor of  $C_n=0.1$

Varying the capacitor seems to widen the bandwidth of the low pass filter to let more of the signal through, the signal becomes even more sinusoidal at higher capacitance.

### 3.2.4 Section vii. Varying time step

Lowering the time step seems to slow the rise and fall of the signal, increasing the timestep creates a sharper rise and fall in the signal.

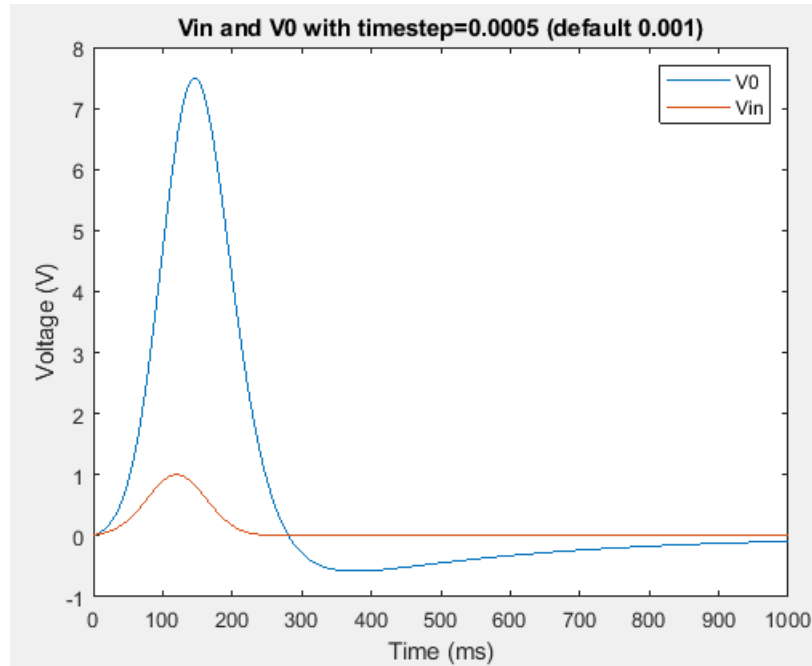


Figure 18: Output voltage with a time step of 0.0005s

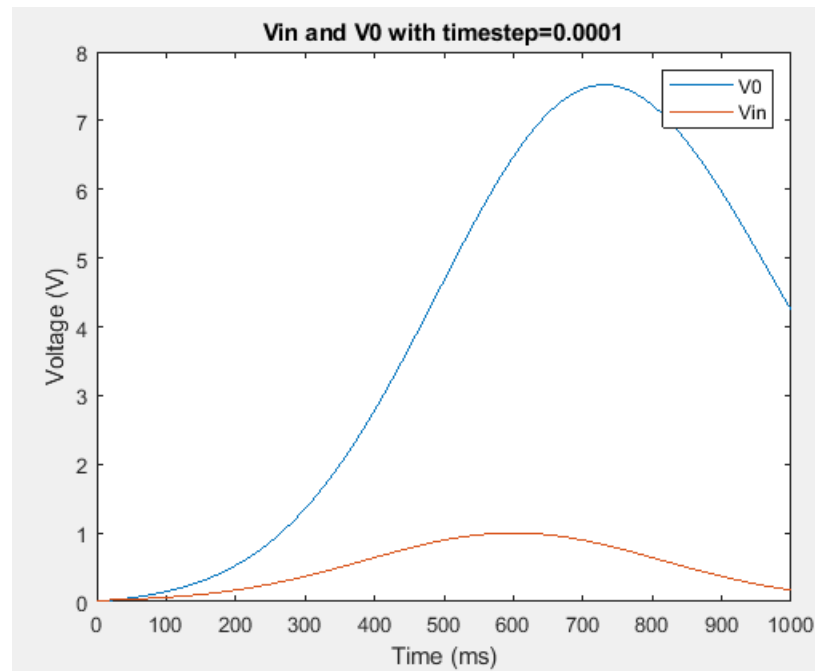


Figure 19: Output voltage with a time step of 0.0001s

## 4 Part 6: Non-linearity

If the voltage source on the output stage was instead modeled by  $V = \alpha I_3 + \beta I_3^2 + \gamma I_3^3$  we would need to use a non-linear method to solve the output voltage. This would need to be done iteratively using something like the Newton-Raphson method. Additionally we would need a non-linear vector  $B$  to describe the non-linear part and the solution would need to be found using a Jacobian.