# **Digital Signal Processing**

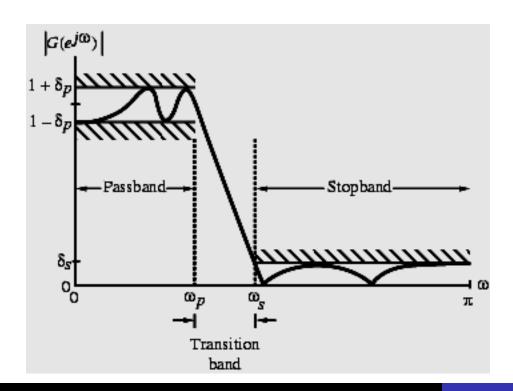
**IIR Filter Design** 

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## Filter Specification

### **Example: LPF**

$$|G(e^{j\omega})| \le \delta_s \quad \text{for } \omega_s \le |\omega| \le \pi$$
 $1 - \delta_P \le |G(e^{j\omega})| \le 1 + \delta_P \quad \text{for } |\omega| \le \omega_P$ 



 $Passband: \omega_P$ 

Stopband:  $\omega_S$ 

### Filter Selection

The *objective* of filter design is to design casual

H(z) that meets the specifications  $H(z)=rac{\displaystyle\sum_{k=0}^{}p_{k}z^{-k}}{N}$ 

IIR or FIR?

IIR:

low order to reduce computational complexity, but may not stable.

FIR:

with linear phase ,but high order

$$H[n] = \pm h[N-n]$$

$$egin{aligned} \mathsf{order} \ H[z] &= \sum_{k=0}^N h[k] z^{-k} \end{aligned}$$

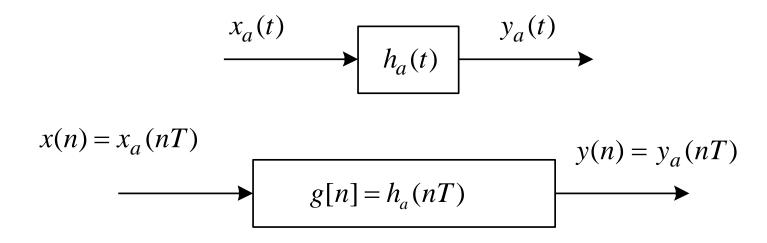
IIR design

The most common practice is to transform  $H_a(s)$  into the desired digital transfer function G(z).

convert the digital filter specifications to into analog lowpass prototype filter specifications determine the analog lowpass filter transfer function meeting these specifications transform the analog filter into the desired digital transfer function

- Apply a mapping from s-domain to the z-domain so that the essential properties of the analog frequency response are preserved.
- The mapping function should:
  - (1) The imaginary axis in the s-plane be mapped onto the unit circle of the z-plane.
  - (2) A stable analog transfer function be transferred into a stable digital transfer function.

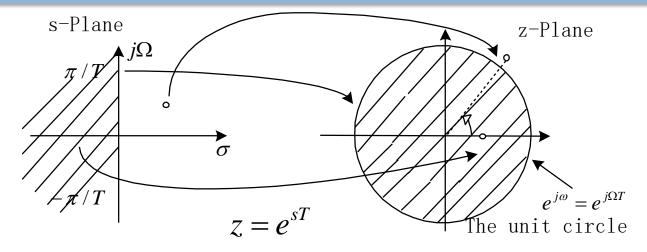
#### **Impulse Invariance Method**



$$\left| G(z) 
ight|_{z=e^{sT}} = rac{1}{T} \sum_{m=-\infty}^{\infty} H_a igg(s-jmrac{2\pi}{T}igg)$$

The mapping function  $z=e^{sT}$ 

#### **Impulse Invariance Method**



- $j\Omega$ -axis mapped onto the unit circle, stable region in s-plane mapped into the stable region in z-plane).
- j $\Omega$ -axis in the s-plane and the unit circle in  $\omega = \Omega T$
- Nyquist

$$G(e^{j\omega}) = rac{1}{T} H_a(j\Omega) \quad ext{for } |\omega| < \pi$$

### **Design Steps**

 $H_a(s)$  is partial-fractional expressed as:  $(h_a(t))$  is derived

$$H_a(s) = \sum_{i=1}^N rac{A_i}{s-s_i} \qquad \qquad \operatorname{Re}(s_i) < 0$$

(2) From  $g[n] = h_a(nT)$ 

$$G_1(z) = \sum_{i=1}^N rac{A_i}{1 - e^{s_i T} z^{-1}} \qquad \qquad G(z) = \sum_{i=1}^N rac{T A_i}{1 - e^{s_i T} z^{-1}}$$

#### **Proof**

$$h_a(t) = \mathcal{L}^{-1}\{H_a(s)\} = \sum_{i=1}^N A_i e^{s_i t} u(t)$$

$$g[n]=h_a(nT)=\sum_{i=1}^N A_i e^{s_i nT} u[n]$$

$$G_1(z) = \sum_{i=1}^N rac{A_i}{1 - e^{s_i T} z^{-1}}$$

$$H_{a}(s) = \frac{2}{s^{2} + 3s + 2}$$

$$H_{a}(s) = \frac{2}{s + 1} - \frac{2}{s + 2}$$

$$G(z) = T \frac{2}{1 - e^{-T} z^{-1}} - T \frac{2}{1 - e^{-2T} z^{-1}} = \frac{2T(e^{-T} - e^{-2T})z^{-1}}{1 - (e^{-2T} + e^{-T})z^{-1} + e^{-3T} z^{-2}}$$

$$G(z) = \frac{0.4651z^{-1}}{1 - 0.5032z^{-1} + 0.04979z^{-2}}$$

$$|G(e^{j\omega})|$$

$$|G(e^{j\omega})|$$

$$|G(e^{j\omega})|$$

#### **Bilinear Translation Method**

map from s-plane to z-plane

$$s = \frac{2}{T} \left( \frac{1 - z^{-1}}{1 + z^{-1}} \right)$$

$$G(z)=H_a(s)|_{s=rac{2}{T}\left(rac{1-z^{-1}}{1+z^{-1}}
ight)}$$

For  $s = \sigma_0 + j\Omega_0$ 

$$z = rac{1+s}{1-s} = rac{1+\sigma_0 + j\,\Omega_0}{1-\sigma_0 + j\,\Omega_0}$$

$$\sigma_0 = 0$$

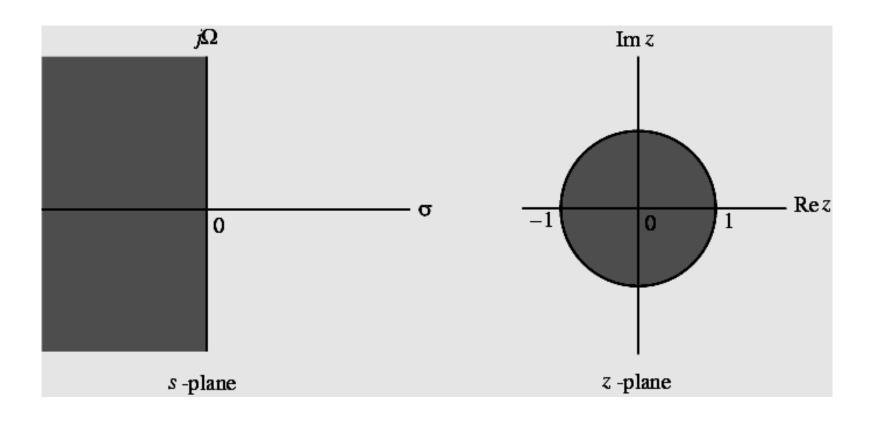
$$|z| = 1$$

$$|z|^2 = \frac{(1+\sigma_0)^2 + (\Omega_0)^2}{(1-\sigma_0)^2 + (\Omega_0)^2}$$

$$\sigma_0 < 0$$

$$\sigma_0 > 0$$

### **Bilinear Translation Method**

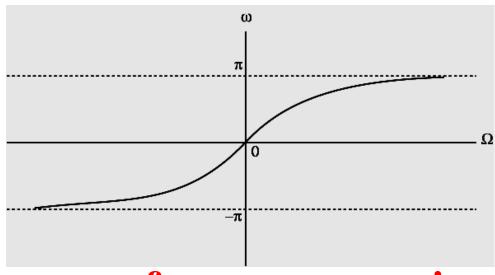


#### **Bilinear Translation Method**

• For  $z = e^{j\omega}$  with T = 2 we have

$$j\Omega = rac{1 - e^{-j\omega}}{1 + e^{-j\omega}} = rac{e^{-j\omega/2} \left(e^{j\omega/2} - e^{-j\omega/2}
ight)}{e^{-j\omega/2} \left(e^{j\omega/2} + e^{-j\omega/2}
ight)} = j an(\omega/2)$$

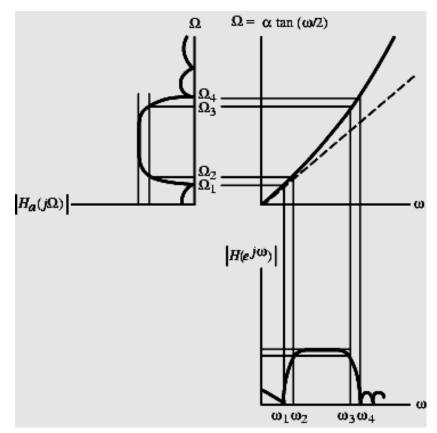
$$\Omega = \tan(\omega/2)$$



frequency warping

#### **Bilinear Translation Method**

Thus, to develop a digital filter meeting a specified magnitude, we must <u>first</u> <u>prewarp</u> the critical band edge frequencies( $\omega_P$  and  $\omega_S$ ) to find their analog Equivalents ( $\Omega_S$  and  $\Omega_P$ ) using Eq.(9.18).



#### **Bilinear Translation Method**

- Pre-warp  $(\omega_p, \omega_s)$  to find their analog equivalents  $(\Omega_p, \Omega_s)$
- Design the analog filter  $H_a(s)$
- Design the digital filter G(z) by applying bilinear transformation to  $H_a(s)$
- Transformation does not preserve phase response of analog filter

$$egin{align} H_a(s) &= rac{\Omega_c}{s+\Omega_c} \ G(z) &= H_a(s)|_{s=rac{2}{T}\left(rac{1-z^{-1}}{1+z^{-1}}
ight)} = rac{\Omega_c\left(1-z^{-1}
ight)}{\left(1-z^{-1}
ight)+\Omega_c\left(1+z^{-1}
ight)} \ &= rac{1-lpha}{2}rac{1+z^{-1}}{1-lpha z^{-1}} \qquad lpha = rac{1-\Omega_c}{1+\Omega_c} = rac{1- an\left(\omega_c/2
ight)}{1+ an\left(\omega_c/2
ight)} \end{split}$$

$$H_a(s) = rac{s^2 + \Omega_0^2}{s^2 + Bs + \Omega_0^2}$$

$$G(z)=H_a(s)|_{s=rac{2}{T}\left(rac{1-z^{-1}}{1+z^{-1}}
ight)}$$

$$|H_a(j\Omega_0)| = 0 |H_a(j0)| = |H_a(j\infty)| = 1$$

- $\Omega_0$  is called the notch frequency
- If  $|H_a(j\Omega_2)| = |H_a(j\Omega_1)| = 1/\sqrt{2}$ B =  $\Omega_2 - \Omega_1$  is the 3-dB notch bandwidth

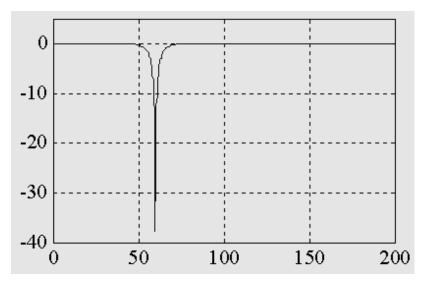
$$=\frac{(1+\Omega_0^2)-2(1-\Omega_0^2)z^{-1}+(1+\Omega_0^2)z^{-2}}{(1+\Omega_0^2+B)-2(1-\Omega_0^2)z^{-1}+(1+\Omega_0^2-B)z^{-2}}$$

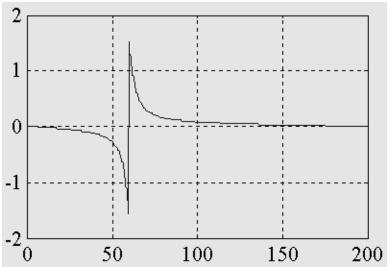
$$=rac{1+lpha}{2}rac{1-2eta z^{-1}+z^{-2}}{1-eta(1+lpha)z^{-1}+lpha z^{-2}}$$

$$lpha = rac{1 + \Omega_0^2 - B}{1 + \Omega_0^2 + B} = rac{1 - an(B_w/2)}{1 + an(B_w/2)} \hspace{1cm} eta = rac{1 - \Omega_0^2}{1 + \Omega_0^2} = \cos(\omega_0)$$

$$H_a(s) = \frac{s^2 + \Omega_o^2}{s^2 + B s + \Omega_o^2}$$

$$G(z) = \frac{0.954965 - 1.1226287 z^{-1} + 0.954965 z^{-2}}{1 - 1.1226287 z^{-1} + 0.90993 z^{-2}}$$





### Case Study

Design G(z) with a maximally flat magnitude, and a pass ripple not exceeding 0.5dB, and the minimum stopband attenuation 15dB.

$$20\log |G\left(e^{j\omega_p}
ight)|>-0.5dB$$
  $20\log |G\left(e^{j\omega_s}
ight)|<-15dB$   $\omega_p=0.25\pi,\,\omega_{_{
m S}}=0.55\pi$ 

### (1) Prewarpping

$$\Omega_P = \tan(\frac{\omega_P}{2}) = \tan(\frac{0.25\pi}{2}) = 0.4142136$$

$$\Omega_S = \tan(\frac{\omega_S}{2}) = \tan(\frac{0.55\pi}{2}) = 1.1708496$$

## (2) Design the parent analog filter $H_a(s)$

### From the specifications we obtain



$$20\log \left(1/\sqrt{1+arepsilon^2}
ight) = -0.5$$
  $arepsilon = 0.122$ 

stopband attenuation 15dB =>



$$20\log(1/A) = -15$$

$$A^2 = 31.6228$$

$$k = \frac{\Omega_s}{\Omega_p} = \frac{1.1708496}{0.4142136} = 2.8266809$$

$$k_1 = \frac{\varepsilon}{\sqrt{A^2 - 1}} = 0.0631234$$

$$N = \frac{\log_{10}(1/k_1)}{\log_{10}(1/k)} = \frac{\log_{10}(15.841979)}{\log_{10}(2.8266814)} = 2.6586997$$

The least order of Butterworth LPF is N=3.

### the 3-dB frequency

$$\Omega_c = (\varepsilon)^{-1/N} \Omega_p = 1.419915 \Omega_p = 0.588148$$

third-order normalized lowpass Butterworth transfer function

$$H_{an}(s) = \frac{1}{(s+1)(s^2+s+1)}$$

which has 3-dB frequency at  $\Omega_c$  = 1.

$$H_a(s) = H_{an}\left(\frac{s}{\Omega_c}\right) = \frac{0.203451}{(s+0.588148)(s^2+0.588148s+0.245918)}$$

Digital filter G(z) by applying bilinear transformation

$$\left. G(z) = H_a(s) 
ight|_{s=rac{2}{T}\left(rac{1-z^{-1}}{1+z^{-1}}
ight)}$$

### IIR Design—The Impulse Invariance Method

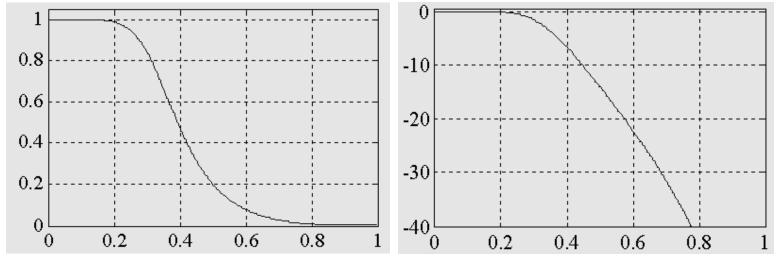
The third-order lowpass Butterworth with 3-dB frequency at  $\Omega_c$ .

$$H_a(s) = H_{an}\left(rac{s}{\Omega_c}
ight) = rac{1}{1+2rac{s}{\Omega_c}+2\left(rac{s}{\Omega_c}
ight)^2+\left(rac{s}{\Omega_c}
ight)^3}$$

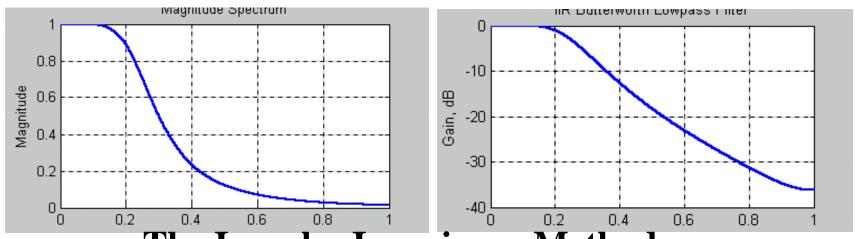
$$egin{aligned} H_a(s) &= rac{\Omega_c^3}{(s+\Omega_c)\,(s-\Omega_c e^{j2\pi/3})\,(s-\Omega_c e^{-j2\pi/3})} \ &= rac{\Omega_c}{s+\Omega_c} + rac{-\left(\Omega_c/\sqrt{3}
ight)e^{j\pi/6}}{s+\Omega_c\left(1-j\sqrt{3}
ight)/2} + rac{-\left(\Omega_c/\sqrt{3}
ight)e^{-j\pi/6}}{s+\Omega_c\left(1+j\sqrt{3}
ight)/2} \end{aligned}$$

#### digital transfer function

$$G(z) = rac{\omega_c}{1 - e^{\omega_c} z^{-1}} + rac{-\left(\omega_c/\sqrt{3}
ight) e^{j\pi/6}}{1 + e^{-\omega_c(1 - j\sqrt{3})/2} z^{-1}} + rac{-\left(\omega_c/\sqrt{3}
ight) e^{-j\pi/6}}{1 + e^{\omega_c(1 + j\sqrt{3})/2} z^{-1}} \;\; \omega_c = \pi/4$$



The Bilinear Translation Method



The Impulse Invariance Method

### IIR Design with Matlab

Read and exercise by yourself!

**Note:** LPF design directly in digital form

1. Order Estimation

```
[N,Wn] = buttord(Wp, Ws, Rp, Rs);
```

2. Filter Design

```
[b,a] = butter(N,Wn);
% Getting:G(z)=B(z)/A(z)
```

3. Other type filter

```
[b,a] = cheby1(N,Rp,Wp,'high');
%Wn=[W1, W2]
```

### IIR Design with Matlab

Note: Digital LPF design in analog form by Bilinear Transform

1. Order Estimation

```
[N,Wn] = ellipord(Wp,Ws,Rp,Rs,'s');
```

2. Filter Design

```
[bt,at] = ellip(N,Wn);
%Getting: Ha(z) = Bt(z)/At(z)
```

3. Bilinear Transform

```
[num,den]= bilinear(b,a,0.5);
% 0.5 means T=2,Fs=0.5
% Getting:G(z)=B(z)/A(z)
```