

Geometric Adaptive Control of Attitude Dynamics on SO(3) with State Inequality Constraints Shankar Kulumani and Christopher Poole

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between current and desired configuration

Attractive - drives system towards desired attitude

Repulsive - forces system away from constraint directions

Error function is the product of two terms

► Smooth, positive definite function which measures the error

 $\Psi(R) = A(R)B(R)$

 $A(R) = \frac{1}{2} tr \left[G \left(I - R_d^T R \right) \right]$

 $B(R) = 1 - \frac{1}{\alpha} \ln \left(\frac{\cos \theta - r^T R^T v}{1 + \cos \theta} \right)$





Background and Motivation

- Autonomous control of vehicles is critical for missions
- ► Typical operations require extensive planning and human interaction
- Vehicles must operate safely in hazardous environments
- Applicable to under-water, aerial, and spacecraft scenarios
- Key technology for autonomy is large angle reorientations in the presence obstacles
 - Spacecraft have sensitive payloads e.g. optical sensors
 - ▶ Reorient while not pointing in dangerous directions e.g. Sun, Moon





Hubble

Agile S/C

- Problem: reorient a vehicle while avoiding certain directions
- Sensor exclusion zone around the Sun
- UAVs manuevering in restricted and congested locations
- Laser emitters on industrial robots

Spacecraft Orientation

- Rigid body attitude dynamics has been extensively studied
- Configuration manifold is curved and nonlinear
- ▶ Dynamics evolve on the Special Orthogonal Group: SO(3)
- Unique properties: cannot be represented as a linear vector space
- Previous work is based on reduced attitude representations
- ► Euler angles: 24 possible combinations which suffer singularities Quaternions: no singularities but double cover SO(3)
- ► Geometric control: the development of control systems for systems evolving on nonlinear manifolds
- Many systems cannot be defined correctly on Euclidean spaces
- Innovative techniques avoid ambiguities and local coordinates and exactly describe the evolution of the system

Attitude Dynamics

Spacecraft is modeled as a rigid body rotating about its center of mass described by the Special Orthogonal Group

$$\mathsf{SO}(3) = \left\{ R \in \mathbb{R}^{3 \times 3} \,|\, R^T R = I, \det R = 1 \right\}$$

Euler's equations of motion govern the dynamics of a rigid body

$$J\dot{\Omega} + \Omega \times J\Omega = u + W(R,\Omega)\Delta,$$

 $\dot{R} = R\hat{\Omega},$

- $ightharpoonup R \in SO(3)$ defines the orientation of the spacecraft with respect to an inertial reference frame
- $\rightarrow W(R,\Omega)\Delta$ models a wide range of external disturbances
- Solar radiation pressure (SRP)
- Gravity gradient moment
- Air turbulence and gusts
- Unknown mass distribution

Adaptive Attitude Control with Collision Avoidance

Constraint is defined in terms of unit-vectors on the two-sphere:

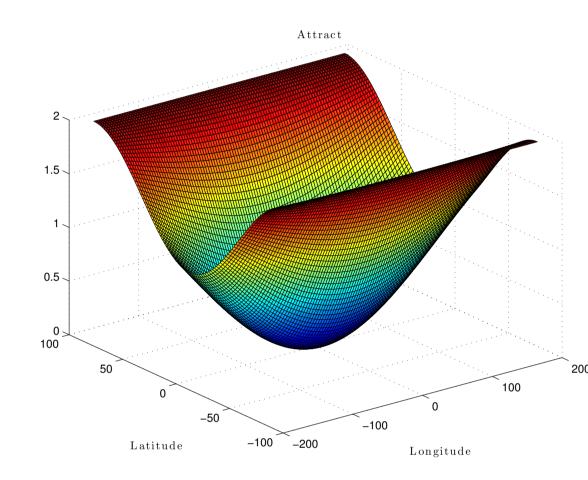
$$\mathsf{S}^2 = \left\{ q \in \mathbb{R}^3 \!\mid \|q\| = 1
ight\}$$

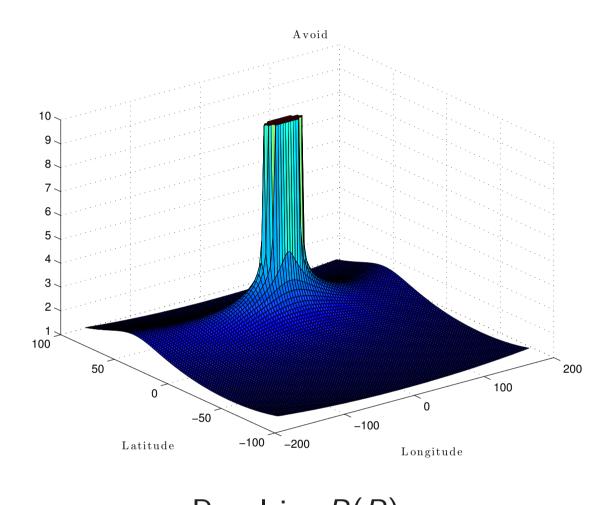
- ▶ We wish to avoid pointing spacecraft in a particular direction
- Sensitive optical sensor $r \in S^2$ defines the sensor direction
- ► Constraint direction $v \in S^2$ defines direction to distant object
- Hard cone constraint strictly avoid pointing sensor towards the celestial object

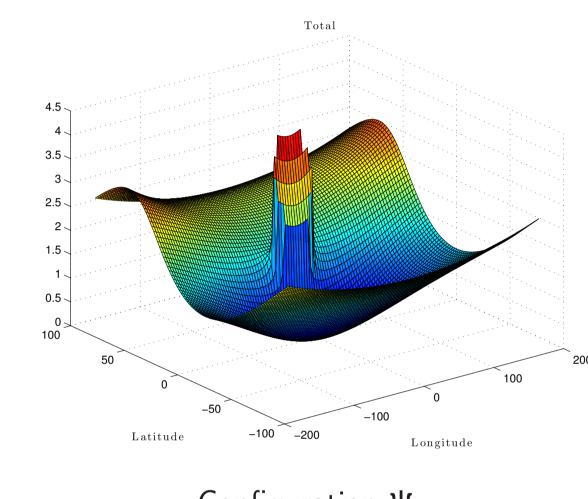
$$r^T R^T v \le \cos \theta$$

▶ Logarithmic barrier function causes the error to grow as $r^T R^T v \rightarrow \cos \theta$

- ▶ $B(R) \to \infty$ as the constraint boundary is neared $r^T R^T v \to \cos \theta$
- \triangleright B(R) has little impact on Ψ when far from constraint as the logarithmic function quickly decays







Attractive A(R)

Repulsive B(R)

Configuration Ψ

▶ We can easily generalize this technique to an arbitrary number of constraints

$$\Psi = A \left[1 + \sum_i C_i \right] \; ext{where} \; C_i = B-1$$

Lyapunov analysis is used to derive an adaptive control scheme which guarantees stability in the face of disturbances and obstacles

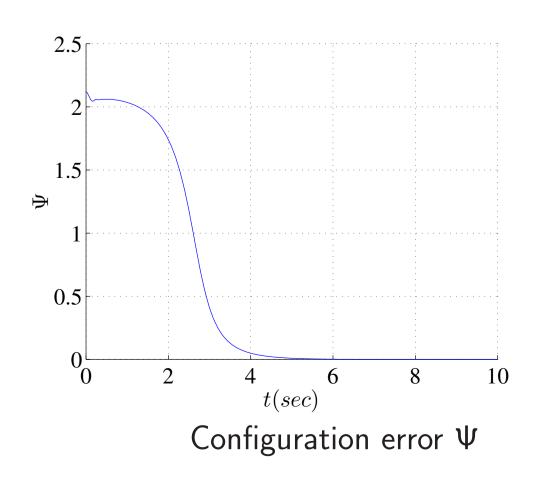
$$u = -k_R e_R - k_\Omega e_\Omega + \Omega \times J\Omega - W\bar{\Delta}$$
 $\dot{\bar{\Delta}} = k_\Delta W^T (e_\Omega + ce_R)$

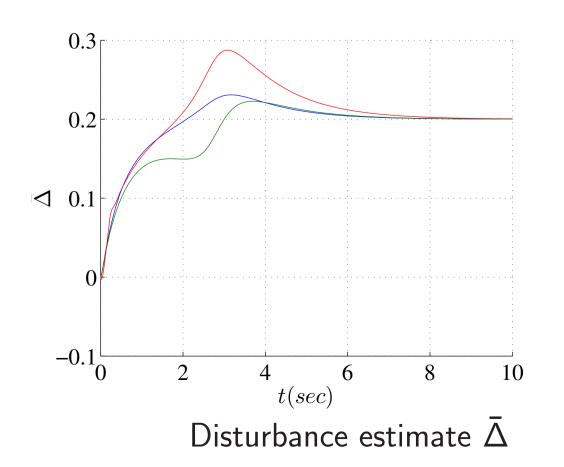
Numerical Simulation

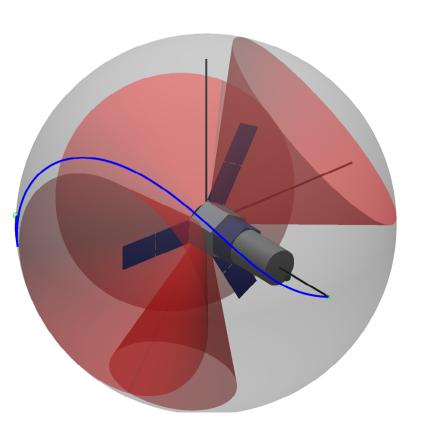
▶ Geometric Adaptive Controller is able to stabilize the rigid body while avoiding multiple constraints with a fixed but unknown external disturbance

Initial:
$$R_0 = \exp(225^\circ \times \frac{\pi}{180}\hat{e}_3)$$
 Final: $R_d = I$ Disturbance: $\Delta = \begin{bmatrix} 0.2 & 0.2 & 0.2 \end{bmatrix}^T$

▶ The adaptive controller accurately accounts for the disturbance and ensures all constraints are satisfied



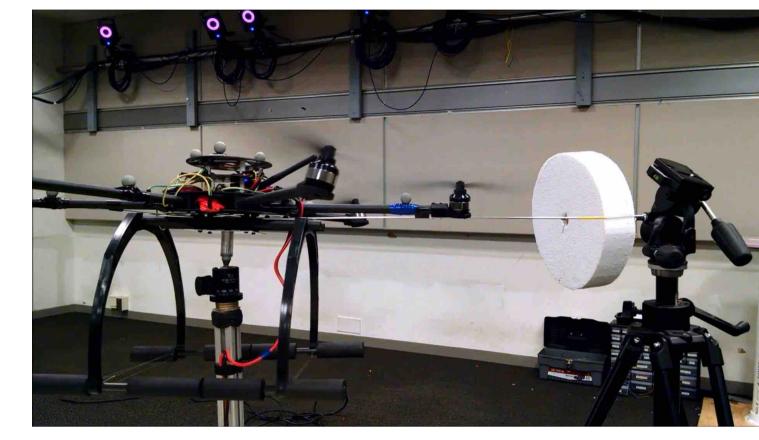




Attitude trajectory

UAV Validation

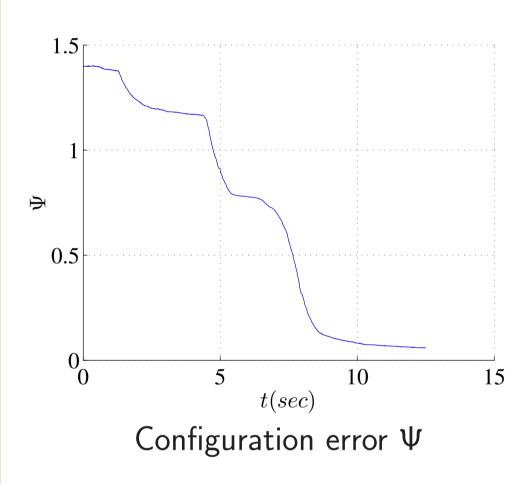
- Hexrotor UAV developed by the Flight Dynamics and Controls Laboratory
- Three pairs of counter-rotating propellers
- Attached to a spherical joint to emulate a fully actuated rigid body
- Onboard computer module receives measurements from Vicon motion capture system and computes control input in real-time

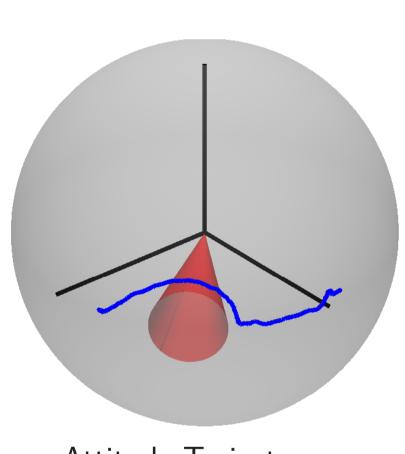


Attitude control testbed

Hexrotor rotates about vertical axis while automatically avoiding the obstacle

Initial:
$$R_0 = \exp(\frac{\pi}{2}\hat{e}_3)$$
 Final: $R_d = I$





Attitude Trajectory

Adaptive controller is robust to uncertainties and disturbances

Conclusions

- Constrained geometric adaptive controller on SO(3)
- Completely avoids singularities and ambiguities
- Geometrically exact and conceptually simple attitude controller
- Automatically satisfies multiple constraints without added complexity Obstacle avoidance computed in real-time with on-board
- software ► Typical planning methods are only able to determine an obstacle-free
- path after multiple iterations and extensive computation
- Large computation costs limit these methods to a priori calculation and make responsive control impossible
- ► Randomized search algorithms can only offer a stochastic guarantee of convergence as the computation time increases
- Our control system is capable of handling any number of obstacles and offers a rigorous stability proof
- ▶ Ideal for challenging scenarios with multiple obstacles or an environment which requires complex control
- Computationally efficient and ideal for embedded systems with energy or computation limitations
- Stability proof ensures manuvers always satisfy pointing constraints