

Школа-семинар «Основы использования OpenFOAM, SALOME и ParaView»

ДЕМОНСТРАЦИЯ: ОБТЕКАНИЕ ОБРАТНОГО УСТУПА

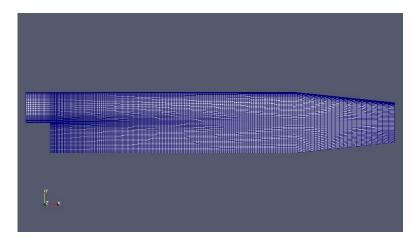
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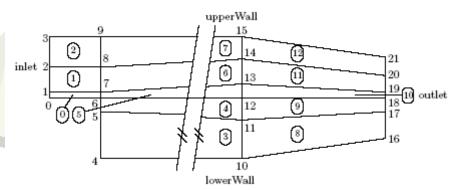
РАСЧЕТНАЯ ОБЛАСТЬ И ИСХОДНЫЕ ДАННЫЕ



Расчетная область и граничные условия



Блочная сетка — blockMeshDict



U = 10 m/c K-e model K-omega SST model LES 1 eq. model simpleFoam pisoFoam

Р.В. Питц, Дж.У. Дейли. Горение в турбулентном слое смешения за уступом. Аэрокосмическая техника. 1984. N7. c.74-82



МАТЕМАТИЧЕСКАЯ МОДЕЛЬ

Governing equations

Mass continuity for incompressible flow

$$\nabla \cdot \mathbf{U} = 0 \qquad (3.4)$$

Steady flow momentum equation

$$\nabla \cdot (UU) + \nabla \cdot R = -\nabla p \qquad (3.5)$$

where p is kinematic pressure and (in slightly over-simplistic terms) $\mathbf{R} = \nu_{eff} \nabla \mathbf{U}$ is the viscous stress term with an effective kinematic viscosity ν_{eff} , calculated from selected transport and turbulence models.

Initial conditions U = 0 m/s, p = 0 Pa — required in OpenFOAM input files but not necessary for the solution since the problem is steady-state.

Boundary conditions

- Inlet (left) with fixed velocity U = (10,0,0) m/s;
- Outlet (right) with fixed pressure p = 0 Pa;
- No-slip walls on other boundaries.

Transport properties

• Kinematic viscosity of air $\nu = \mu/\rho = 18.1 \times 10^{-6}/1.293 = 14.0 \ \mu m^2/s$

Turbulence model

- Standard k − ε;
- Coefficients: C_μ = 0.09; C₁ = 1.44; C₂ = 1.92; α_k = 1; α_ε = 0.76923.

Solver name simpleFoam: an implementation for steady incompressible flow.



ИСХОДНЫЕ ДАННЫЕ: КАТАЛОГ ЗАДАЧИ

[cfd1@master simpleFoam]\$ cd pitzDailyParallel/ [cfd1@master pitzDailyParallel]\$ II total 12 drwxr-xr-x 2 cfd1 sm3 4096 Dec 22 16:43 0 drwxr-xr-x 3 cfd1 sm3 4096 Dec 22 16:43 constant drwxr-xr-x 2 cfd1 sm3 4096 Dec 22 16:48 system [cfd1@master pitzDailyParallel]\$ [cfd1@master pitzDailyParallel]\$ cd system/ [cfd1@master system]\$ II total 16 -rw-r---- 1 cfd1 sm3 1222 Dec 22 16:43 controlDict -rw-r---- 1 cfd1 sm3 1206 Dec 22 16:48 decomposeParDict -rw-r---- 1 cfd1 sm3 1877 Dec 22 16:43 fvSchemes -rw-r---- 1 cfd1 sm3 1940 Dec 22 16:43 fvSolution





ГРАНИЧНЫЕ УСЛОВИЯ ДЛЯ СКОРОСТИ

```
dimensions
               [0 \ 1 \ -1 \ 0 \ 0 \ 0];
internalField uniform (0 0 0);
boundaryField
                                  fixedValue;
                                                               uniform (10 0 0); }
   inlet
                                                   value
                      type
outlet
                                zeroGradient; }
                    type
                                                               uniform (0 0 0); }
upperWall
                                  fixedValue;
                       type
                                                   value
lowerWall
                                  fixedValue;
                                                               uniform (0 0 0); }
                                                  value
                      type
frontAndBack
                        type
                                    empty; }}//
```



ГРАНИЧНЫЕ УСЛОВИЯ ДЛЯ КИНЕТИЧЕСКОЙ ЭНЕРГИИ ТУРБУЛЕНТНОСТИ

```
dimensions [0 2 -2 0 0 0 0];
internalField uniform 0.375;
boundaryField
                                           uniform 0.375; }
inlet {
       type
                   fixedValue;
                              value
outlet { type zeroGradient;
upperWall
                        kqRWallFunction;
                                          value
                                                     uniform 0.375; }
              type
lowerWall {
                      kgRWallFunction;
                                                     uniform 0.375; }
                                          value
              type
frontAndBack
                           empty;
                 type
```



УПРАВЛЕНИЕ РАСЧЕТОМ

```
application
             simpleFoam;
startFrom
             startTime;
startTime
             0:
            endTime;
stopAt
              10;
endTime
deltaT
writeControl timeStep;
writeInterval
purgeWrite
              0;
writeFormat
              ascii:
writePrecision 6:
writeCompression uncompressed;
timeFormat
              general;
timePrecision 6:
runTimeModifiable yes;
```



СХЕМЫ ДИСКРЕТИЗАЦИИ

```
gradSchemes{ default
                           Gauss linear:
grad(p) Gauss linear:
grad(U) Gauss linear;}
divSchemes{ default
                          none;
div(phi,U) Gauss GammaV 1.0;
div(phi,k) Gauss Gamma 1.0:
div(phi,epsilon) Gauss Gamma 1.0;
div(phi,omega) Gauss Gamma 1.0;
div(phi,R) Gauss Gamma 1.0;
           Gauss linear:
div(R)
div(phi,nuTilda) Gauss upwind;
div((nuEff*dev(grad(U).T()))) Gauss linear;}
laplacianSchemes{ default
                               none:
laplacian(nuEff,U) Gauss linear corrected;
laplacian((1|A(U)),p) Gauss linear corrected;
laplacian(DkEff,k) Gauss linear corrected;
laplacian(DepsilonEff,epsilon) Gauss linear corrected;
laplacian(DomegaEff,omega) Gauss linear corrected;
laplacian(DREff,R) Gauss linear corrected;
laplacian(DnuTildaEff,nuTilda) Gauss linear corrected;}
interpolationSchemes{ default
                                  linear:
                                           interpolate(U) linear;}
snGradSchemes{ default corrected;}
fluxRequired{ default
                          no; p;}
```



МЕТОДЫ РЕШЕНИЯ СЛАУ

```
FoamFile
Solvers {
p PCG { preconditioner DIC; tolerance 1e-06; relTol 0.01; };
U PBiCG { preconditioner DILU; tolerance 1e-05; relTol 0.1; };
k PBiCG { preconditioner DILU; tolerance 1e-05; relTol 0.1; };
epsilon PBiCG { preconditioner DILU; tolerance 1e-05; relTol 0.1; };
omega PBiCG { preconditioner DILU; tolerance 1e-05; relTol 0.1; };
R PBiCG { preconditioner DILU; tolerance 1e-05; relTol 0.1; };
nuTilda PBiCG { preconditioner DILU; tolerance 1e-05; relTol 0.1; };}
SIMPLE
{ nNonOrthogonalCorrectors 0;}
relaxationFactors
{ p 0.3; U 0.7; k 0.7; epsilon 0.7; omega 0.7; R
0.7; nuTilda 0.7;}
PISO
{ nCorrectors 4; nNonOrthogonalCorrectors 0; pRefCell 0; pRefValue
                                                     0;}
```



РЕЗУЛЬТАТЫ РАСЧЕТОВ

