BJT and BJT Circuit

Ve311 Electronic Circuits (Summer 2020)

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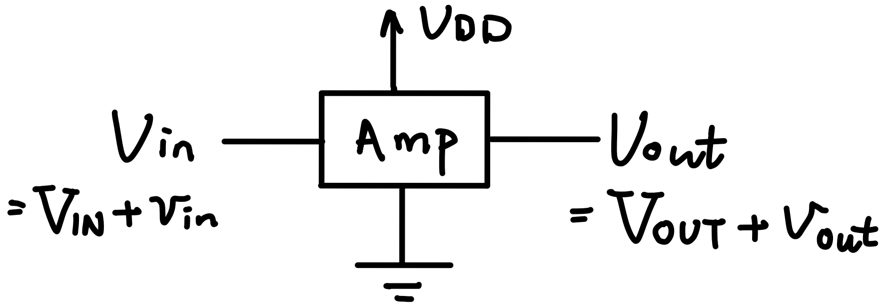
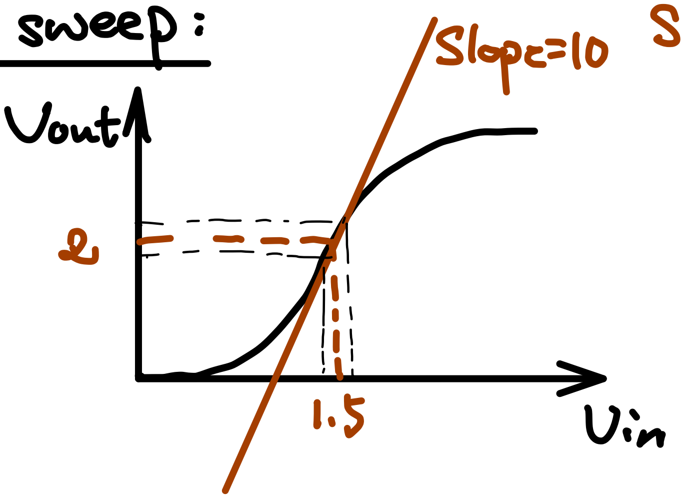
For a general amplifier model:



$$V_{out} = \underbrace{V_{OUT}}_{\substack{\text{DC} \\ \text{complete circuit}}} + A_v \cdot v_{in}$$

DC sweep:



Suppose $V_{in} = 1.5 + \overbrace{0.001 \sin(2\pi 60 t)}^{v_{in}}$

$V_{out} = 2 + \underbrace{0.01 \sin(2\pi 60 t)}_{v_{out}}$

$$A_v = \left.\frac{dV_{out}}{dV_{in}}\right|_{@V_{IN}} = \frac{v_{out}}{v_{in}} = 10$$

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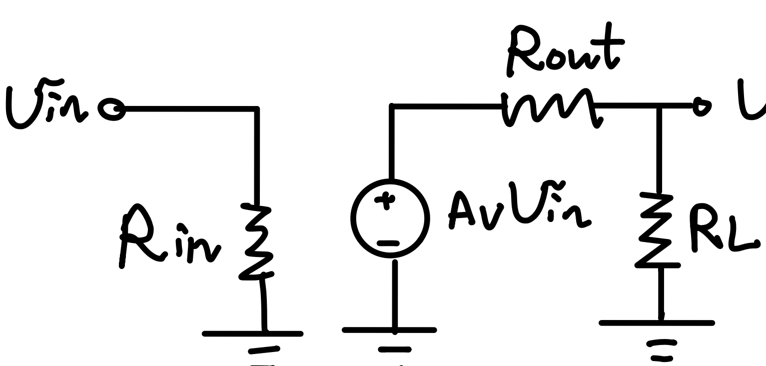
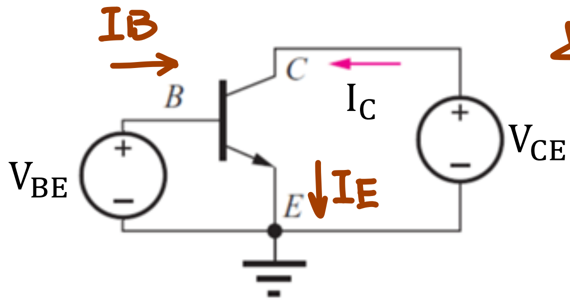
final 重要

Generalized small-signal model: (more important in final exam, no need to understand this deeply for now)



$$V_{out} = A_v \cdot V_{in} \cdot \frac{R_L}{R_{out} + R_L}$$

Summary



$$\boxed{V_{CE} \geq V_{BE}}$$

$\Rightarrow$ **Forward – Active**

$$\mathbf{I_C = I_S\left(e^{\frac{qV_{BE}}{kT}} - 1\right)} \left(1 + \frac{V_{CE}}{V_A}\right)$$

$V_A = \infty$.

$$\boldsymbol{\alpha} = \frac{\mathbf{I_C}}{\mathbf{I_E}} \cong \mathbf{1}$$

$$\boldsymbol{\beta} = \frac{\mathbf{I_C}}{\mathbf{I_B}} = \frac{\boldsymbol{\alpha}}{\mathbf{1 - \boldsymbol{\alpha}}}$$

$I_E = I_B + I_C$

I_S is a constant in the spice model.

Ideal case

$$\mathbf{I_C = I_S\left(e^{\frac{qV_{BE}}{kT}} - 1\right)}$$

$$\boldsymbol{\alpha} = \frac{\mathbf{I_C}}{\mathbf{I_E}} = \mathbf{1}$$

$$\boldsymbol{\beta} = \frac{\mathbf{I_C}}{\mathbf{I_B}} = \infty$$

$I_C = I_E$.

完全理想：门电压 V_{BE} 一定，$I_C = I_E$ 固定

第一种非理想：门漏电 $I_E = I_B + I_C$.

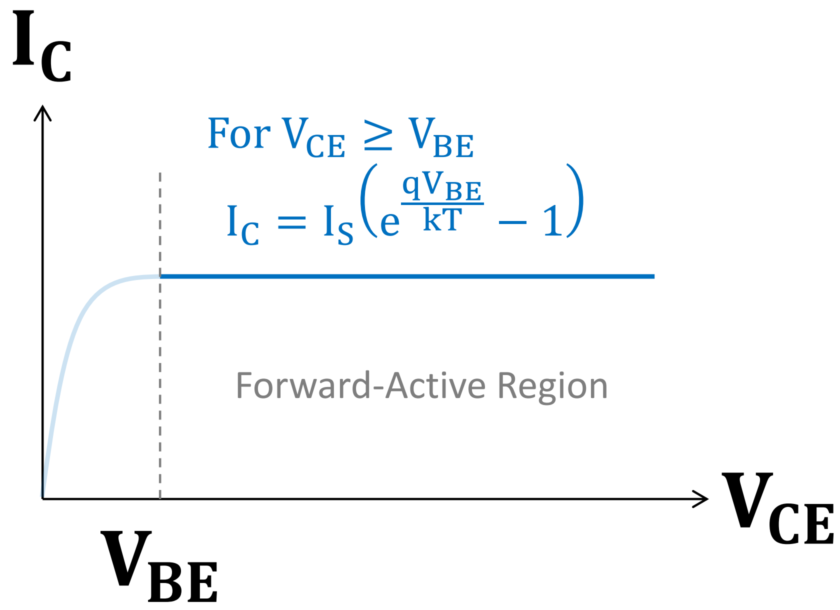
第二种非理想：随着 $V_{CE}\uparrow$，$I_C\uparrow \Rightarrow$ Early effect $V_A \neq \infty$.

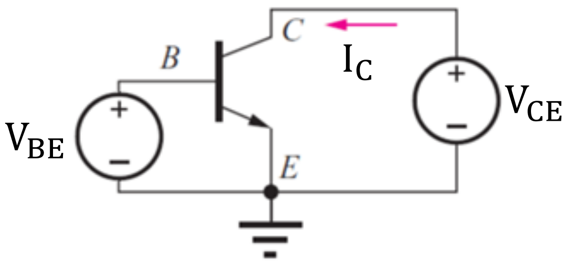
集电压对集电流有影响

I_C vs V_{CE} and I_C vs V_{BE} in Forward-Active Region

I_C vs V_{CE} (not considering Early Effect)

At given V_{BE}, DC sweep V_{CE}





I_C vs V_{CE} (considering Early Effect)

At given V_{BE}, DC sweep V_{CE}

V_A is a constant

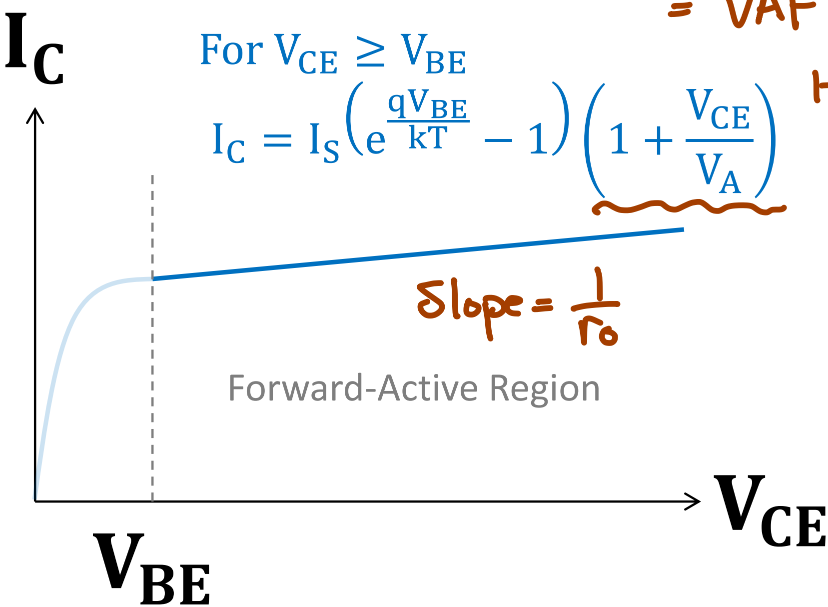
$= VAF$ in Pspice model

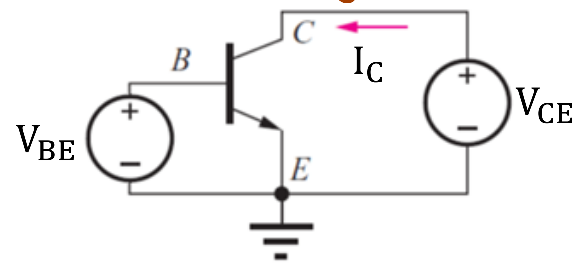
If $V_A \to \infty$,

no early-effect

For $V_{CE} \geq V_{BE}$

$$I_C = I_S\left(e^{\frac{qV_{BE}}{kT}} - 1\right)\left(1 + \frac{V_{CE}}{V_A}\right)$$





V_A is a constant in the spice model.

I_C vs V_{BE}

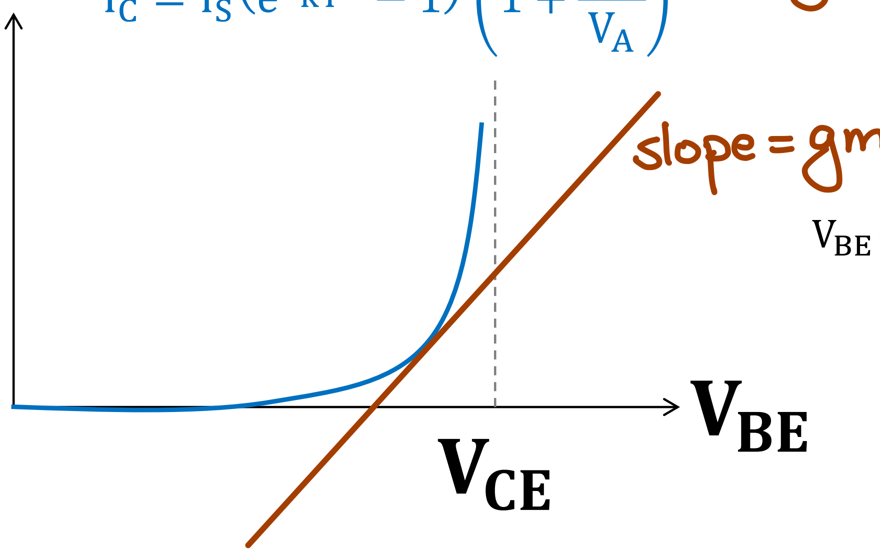
At given V_{CE}, DC sweep V_{BE}

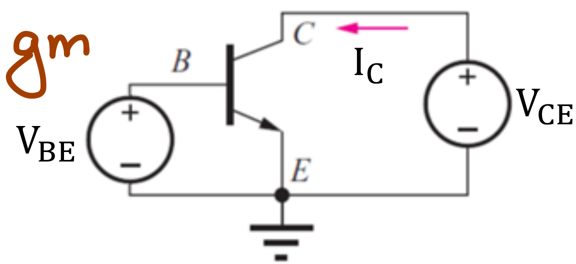
For $V_{CE} \geq V_{BE}$

$$I_C = I_S\left(e^{\frac{qV_{BE}}{kT}} - 1\right)\left(1 + \frac{V_{CE}}{V_A}\right)$$

$$g_m = \frac{dI_C}{dV_{BE}} \cong \frac{I_C}{kT/q}$$ 0.026

I_C

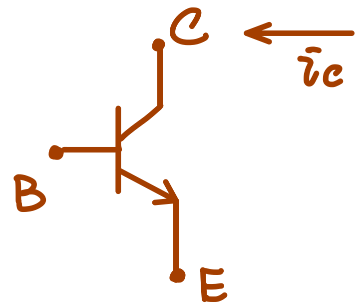




Small-Signal Model

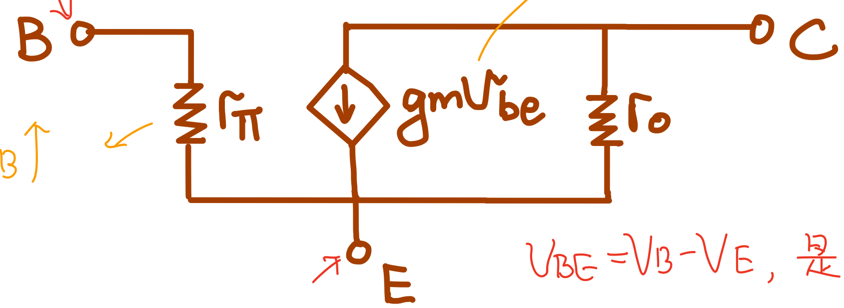
Conclusion first:

For a BJT as:



Its small signal model is:

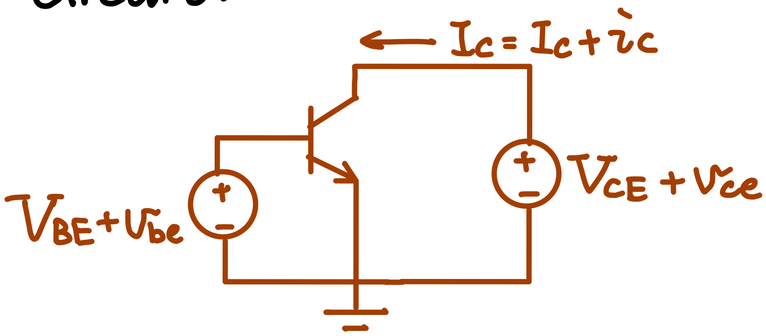
v_{be}对I_c: $I_c = I_s(e^{\frac{V_{BE}}{kT/q}} - 1)$ ···



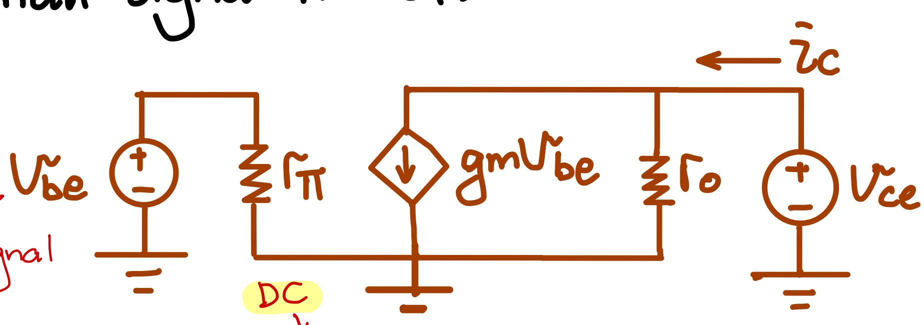
$V_{BE}\uparrow$, $I_C\uparrow$, $I_B\uparrow$

$V_{BE} = V_B - V_E$, 是这两点电势之差

Typical circuit:



Small signal model:



small-signal

small-signal

DC

DC

用DC求

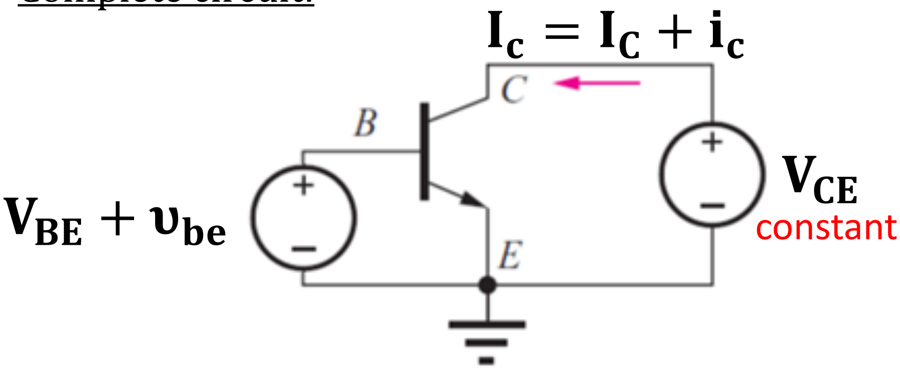
$$\begin{cases} I_c = I_s(e^{\frac{qV_{BE}}{kT}} - 1)(1 + \frac{V_{CE}}{V_A}) \\ g_m \simeq \frac{I_C}{kT/q} \\ r_o \simeq \frac{V_A}{I_C} \leftarrow \text{VAF in Pspice model} \\ r_\pi = \frac{\beta}{g_m} \leftarrow \text{BF in Pspice model} \end{cases}$$

If no early-effect.

$V_A \to \infty$, $r_o \to \infty$

Hybrid-π Model (how to get gm and r_π)

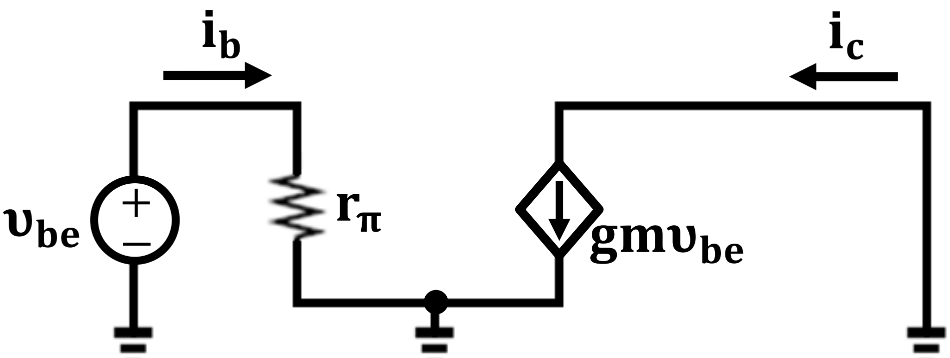
Complete circuit:



$$V_{CE} \geq V_{BE}$$
$\Rightarrow$ Forward – Active

$$I_C = I_S\left(e^{\frac{qV_{BE}}{kT}} - 1\right)\left(1 + \frac{V_{CE}}{V_A}\right)$$

Small-signal circuit:

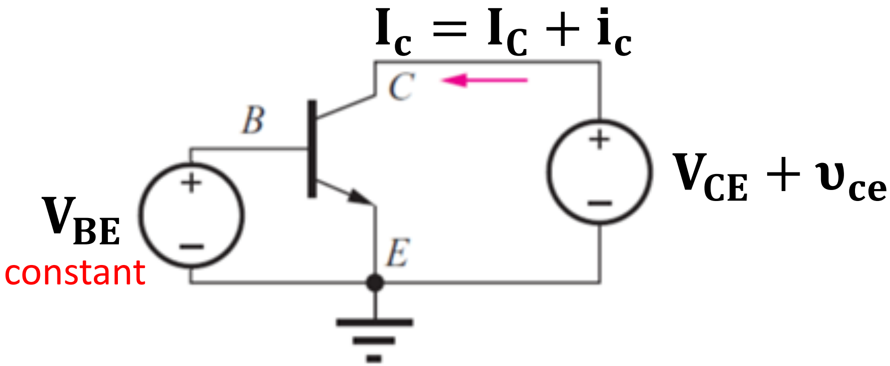


$$r_\pi = \frac{dV_{BE}}{dI_B} = \frac{1}{\frac{dI_C}{\beta dV_{BE}}} = \frac{1}{\frac{gm}{\beta}} = \frac{\beta}{gm}$$

$$gm = \frac{dI_C}{dV_{BE}} \cong \frac{I_C}{kT/q}$$

Hybrid-π Model (how to get r_o)

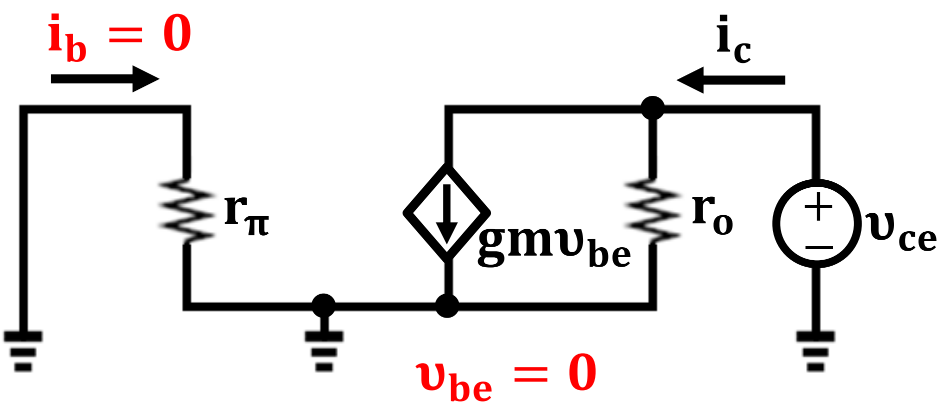
Complete circuit:



$V_{CE} \geq V_{BE}$
$\Rightarrow$ Forward – Active

$$\boxed{I_C = I_S\left(e^{\frac{qV_{BE}}{kT}} - 1\right)\left(1 + \frac{V_{CE}}{V_A}\right)}$$

Small-signal circuit:



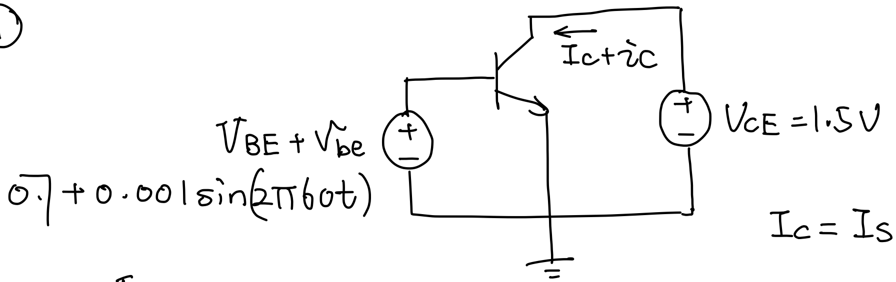
$$r_\pi = \frac{1}{\frac{dI_B}{dV_{BE}}} = \frac{1}{\frac{dI_C}{\beta dV_{BE}}} = \frac{1}{\frac{gm}{\beta}} = \frac{\beta}{gm}$$

$$gm = \frac{dI_C}{dV_{BE}} \cong \frac{I_C}{kT/q}$$

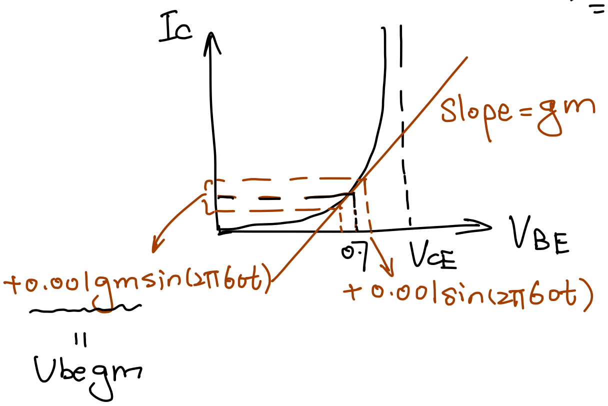
$$r_o = \frac{1}{\frac{dI_C}{dV_{CE}}} \cong \frac{V_A}{I_C}$$

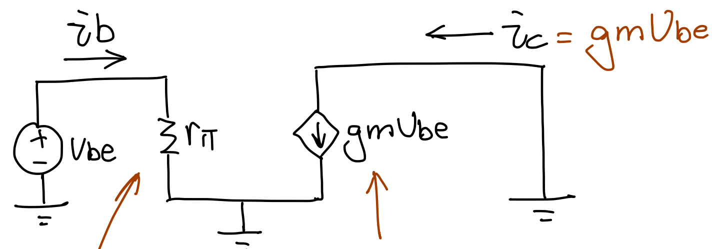
Note: Why do we have r_o, r_π, g_m in small signal model?
(**Skip** this page if you already understand)

①



$$I_C = I_S\left(e^{\frac{qV_{BE}}{kT}} - 1\right)\left(1 + \frac{V_{CE}}{V_A}\right)$$





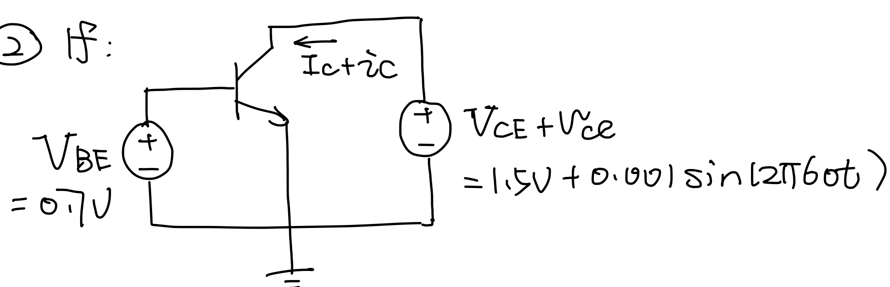
So, here's a dependent current source that simulates $i_c = g_m v_{be}$

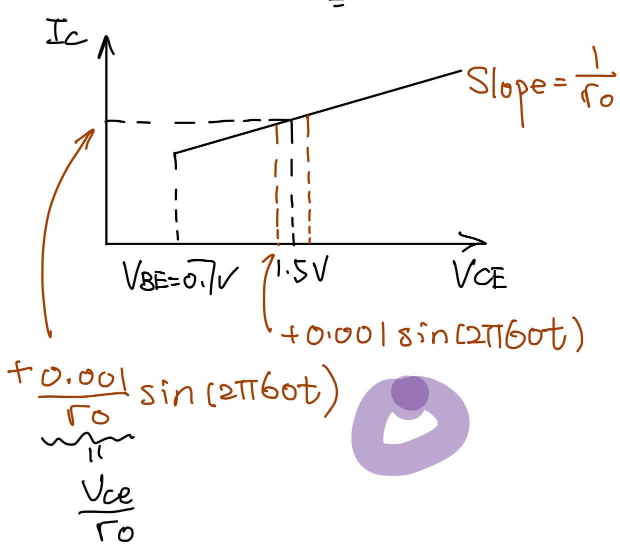
Since $\beta = \frac{I_C}{I_B} = 100$

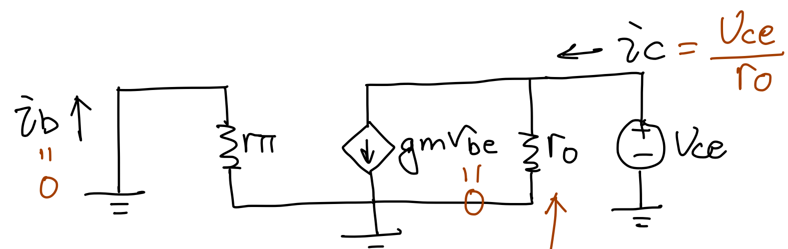
If $v_{be} \uparrow \Rightarrow i_c \uparrow \Rightarrow i_B \uparrow$

"feels like" r_π exists

② If:





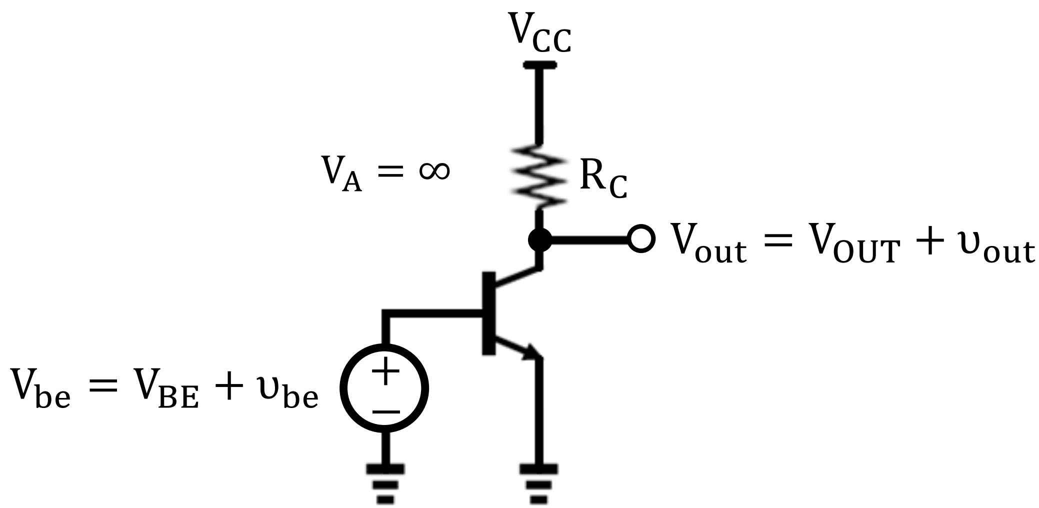


since $i_c = \frac{v_{ce}}{r_o}$

"feels like" r_o exists here

Common-Emitter Amplifier

Common-Emitter Amplifier ($V_A = \infty$)

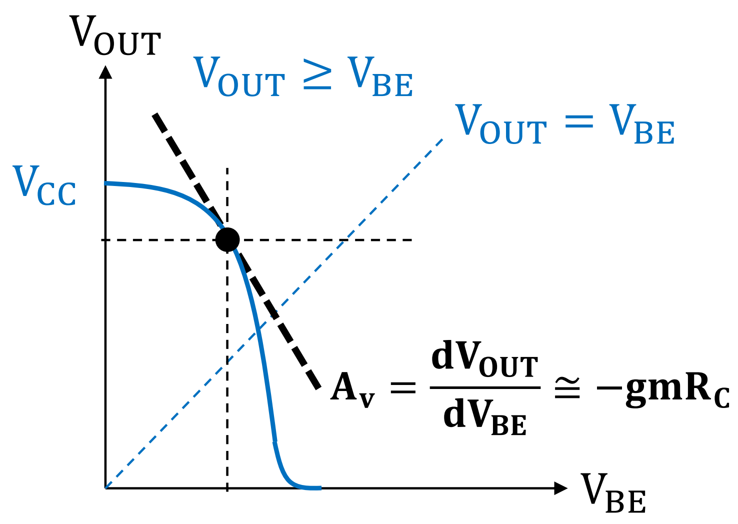


- **DC Analysis**

$$V_{OUT} = V_{CC} - I_C R_C$$

$$= V_{CC} - \frac{AqD_n n_i^2}{N_a W_B}\left(e^{\frac{qV_{BE}}{kT}} - 1\right)R_C$$

$$\boxed{A_v = \frac{dV_{OUT}}{dV_{BE}} \cong -\frac{I_C}{kT/q}R_C = -gmR_C}$$

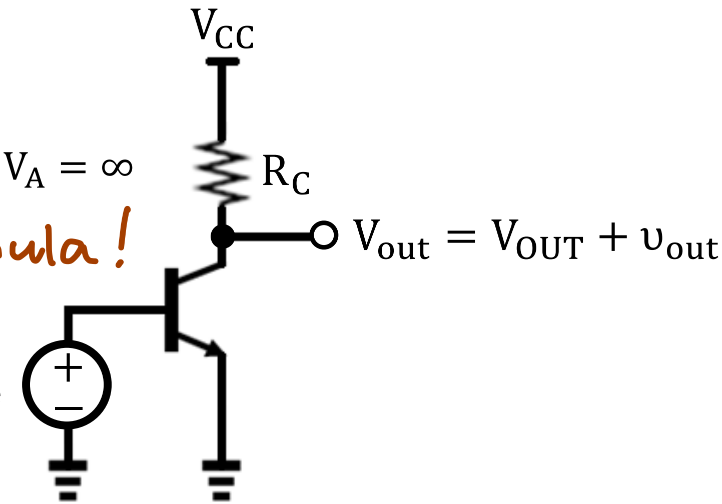


Common-Emitter Amplifier ($V_A = \infty$)

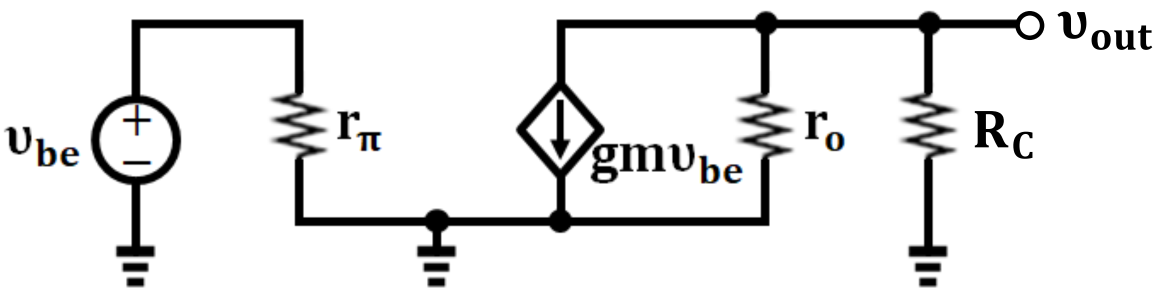
$A_V = \dfrac{dV_{OUT}}{dV_{BE}} = \boxed{\dfrac{v_{out}}{v_{be}}}$

Use small-signal model to calculate Av's formula!

$V_A = \infty$

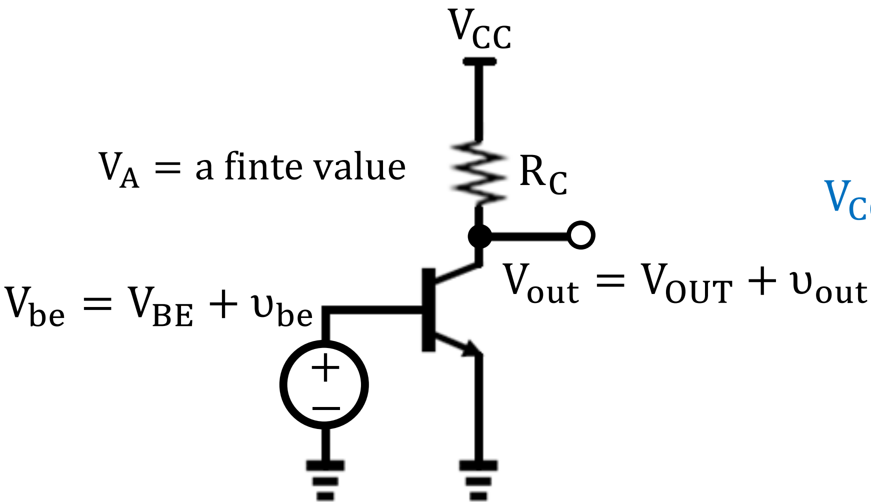


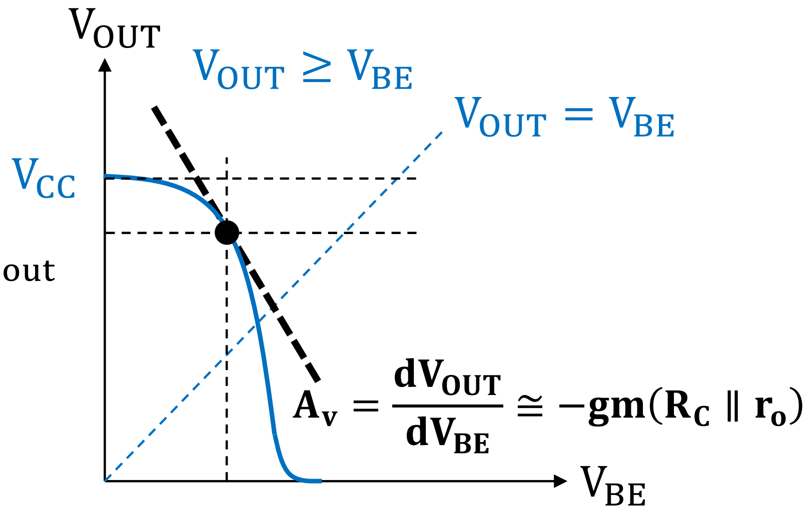
- **Small-Signal Analysis**



$$\boxed{A_v = \frac{\upsilon_{out}}{\upsilon_{be}} = -gm(R_C \parallel r_o) = -gmR_C}$$ (since $r_o = \infty$)

Common-Emitter Amplifier (V_A = a finite value)





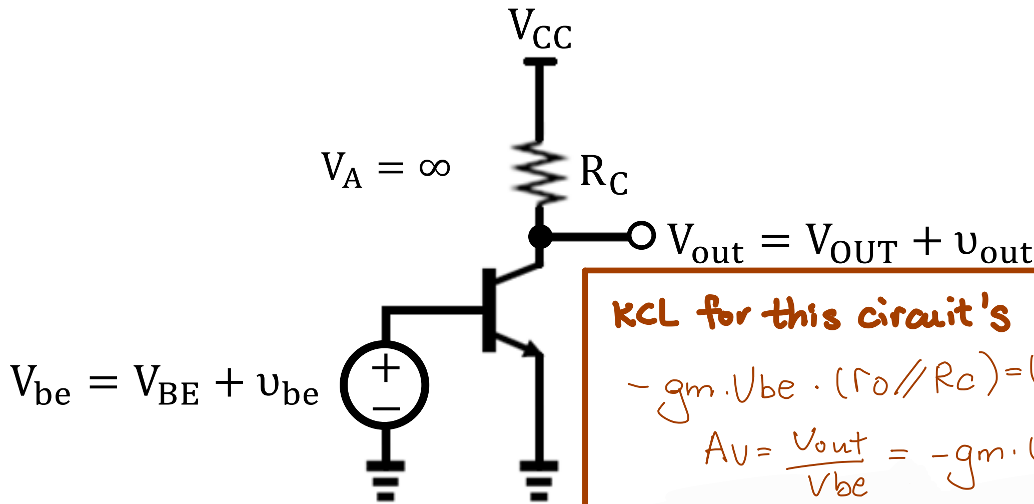
- **DC Analysis**

$$V_{OUT} = V_{CC} - I_C R_C = V_{CC} - I_S\left(e^{\frac{qV_{BE}}{kT}} - 1\right)\left(1 + \frac{V_{OUT}}{V_A}\right) R_C$$

$$\frac{dV_{OUT}}{dV_{BE}} = -\frac{q}{kT} I_S e^{\frac{qV_{BE}}{kT}}\left(1 + \frac{V_{OUT}}{V_A}\right) R_C - I_S\left(e^{\frac{qV_{BE}}{kT}} - 1\right)\frac{1}{V_A}\frac{dV_{OUT}}{dV_{BE}} R_C \cong -gmR_C - \frac{1}{r_o}\frac{dV_{OUT}}{dV_{BE}} R_C$$

$$\boxed{A_v = \frac{dV_{OUT}}{dV_{BE}} \cong -gm(R_C \parallel r_o)}$$

Common-Emitter Amplifier (V_A = a finite value)

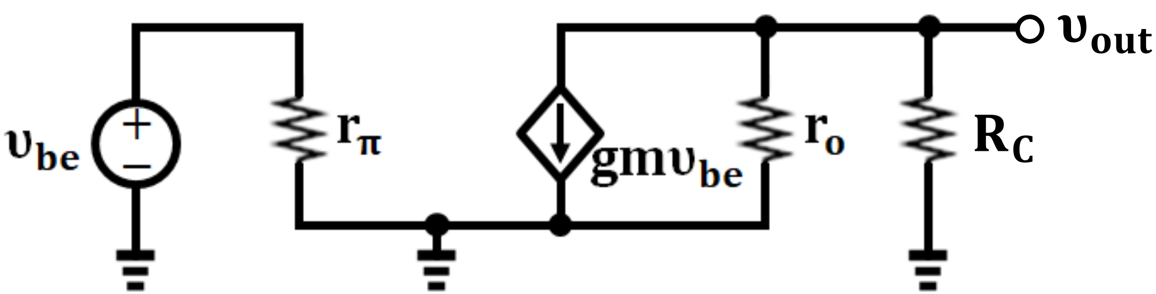


KCL for this circuit's Av:

$-gm \cdot Vbe \cdot (ro // Rc) = Vout$

$Av = \frac{Vout}{Vbe} = -gm \cdot (ro // Rc)$

- Small-Signal Analysis



对不同circuit求Av用
KCL分析small-signal circuit

$$\boxed{A_v = \frac{\upsilon_{out}}{\upsilon_{be}} = -gm(R_C \parallel r_o)}$$

Convert to small-signal model:

DC voltage → short to small-signal ground

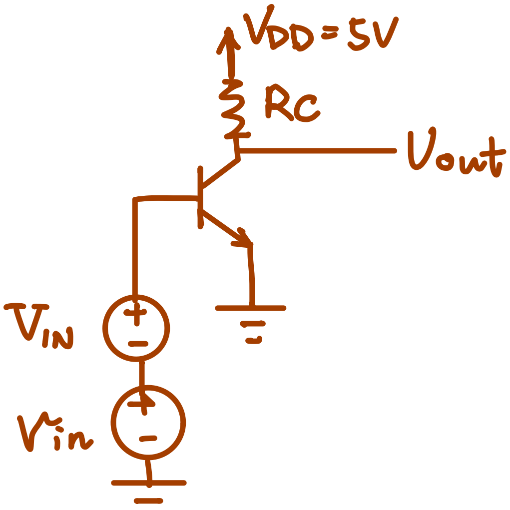
DC current → open circuit

R → still R

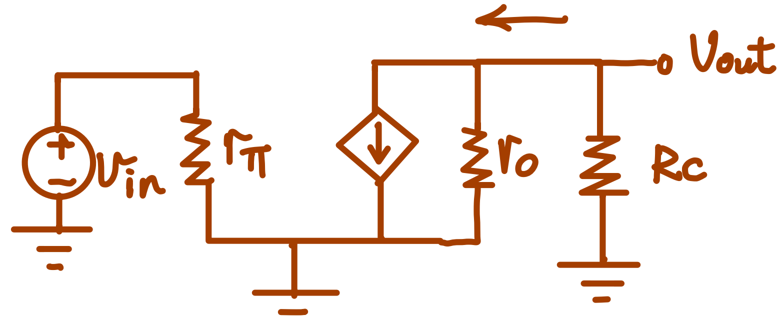
capacitor → short circuit

Ex :

Complete circuit:

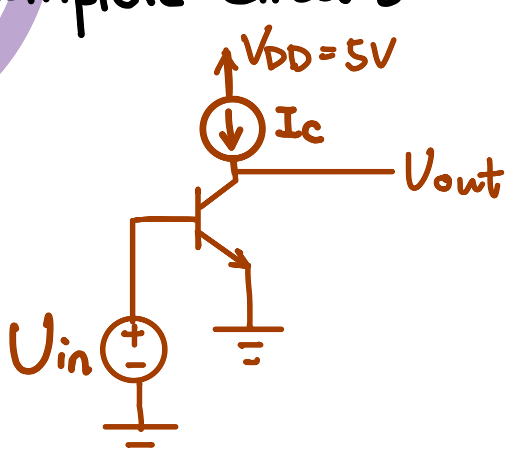


Small-signal:

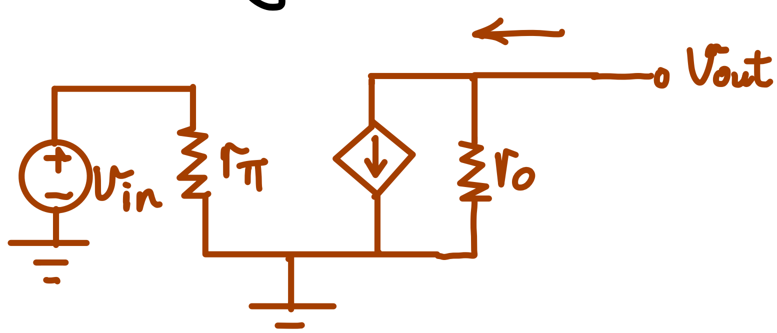


$$A_v = \frac{v_{out}}{v_{in}} = -g_m(r_o // R_C)$$

Complete circuit:

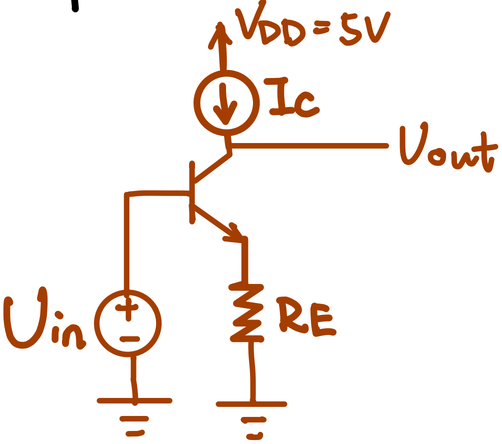


Small-signal:

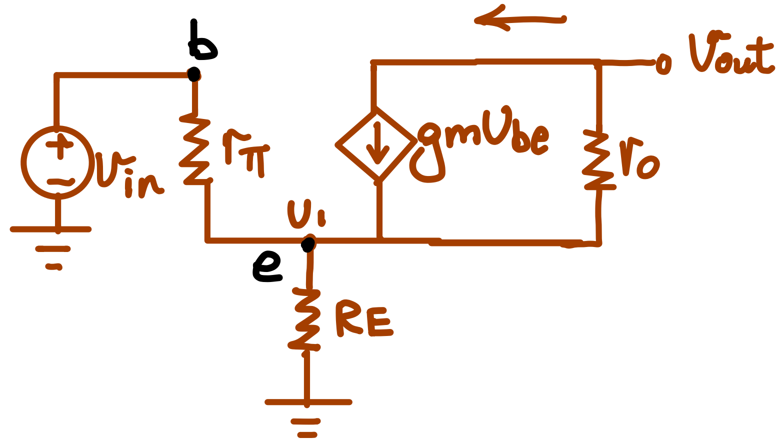


$$A_v = \frac{v_{out}}{v_{in}} = -g_m r_o$$

Complete circuit:



* Small-signal:



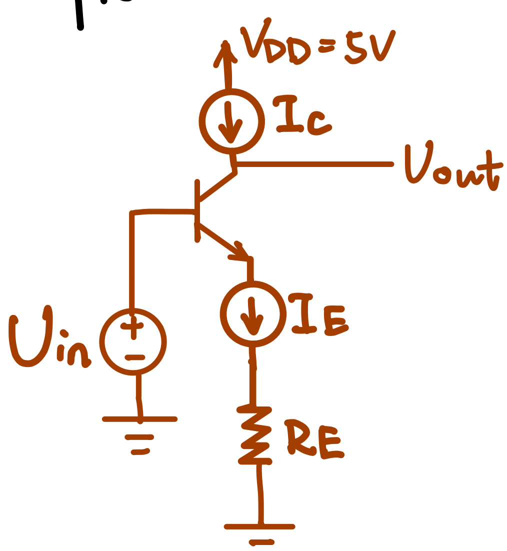
* mind Vbe used in gmVbe doesn't necessarily equals to Vin !

KCL:

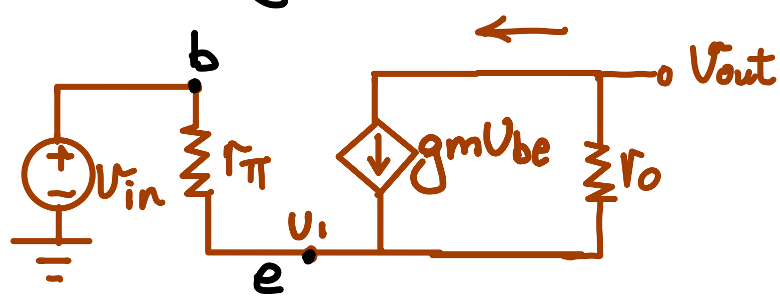
$$\begin{cases} \frac{V_1}{R_E} = \frac{V_{in}-V_1}{r_\pi} + g_m V_{be} + \frac{V_{out}-V_1}{r_o} \\ V_{be} = V_{in} - V_1 \\ g_m V_{be} + \frac{V_{out}-V_1}{r_o} = 0 \end{cases}$$

$\Rightarrow$ Calculate $A_V = \frac{V_{out}}{V_{in}}$

Complete circuit:



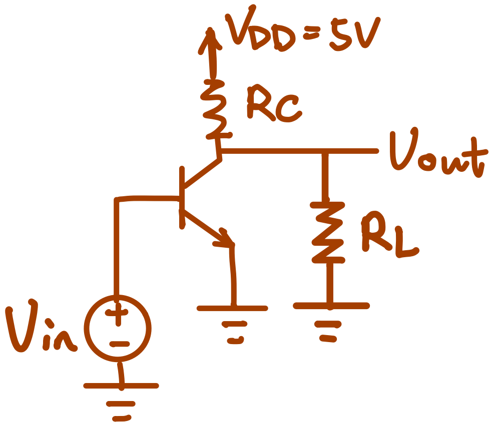
Small-signal:



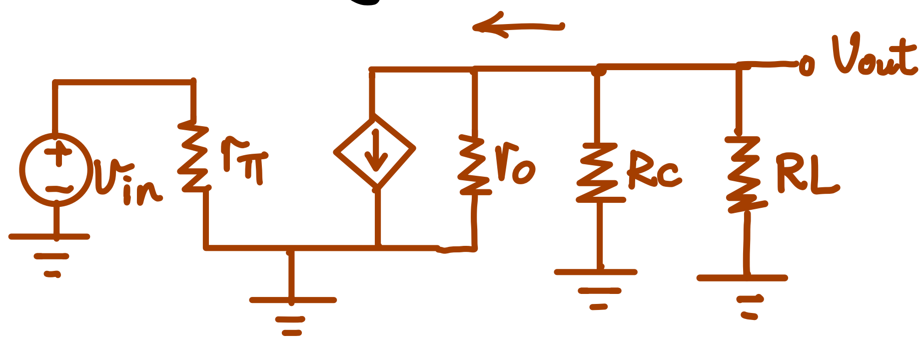
open circuit here

$$A_V = \frac{V_{out}}{V_{in}} = \frac{V_{in}}{V_{in}} = 1$$

Complete circuit:

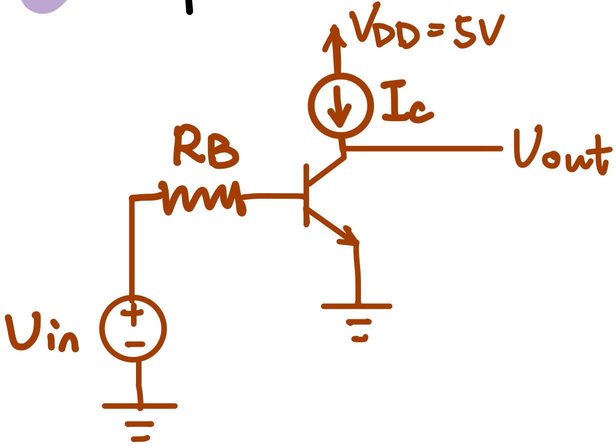


Small-signal:

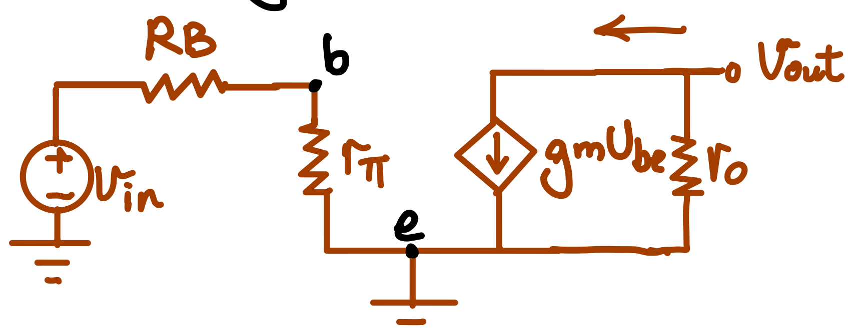


$$A_V = \frac{V_{out}}{V_{in}} = -g_m(r_o // R_C // R_L)$$

Complete circuit:



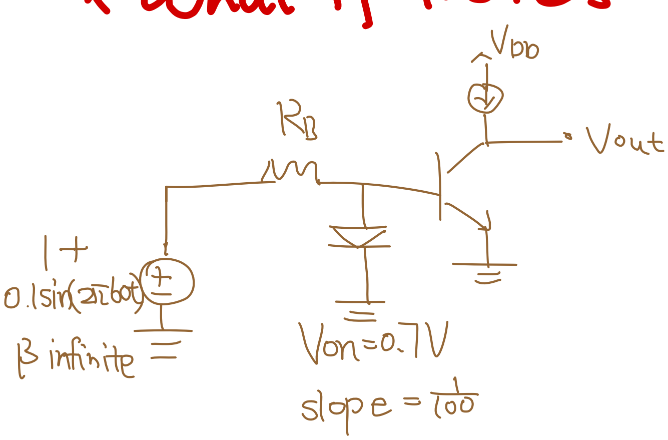
Small-signal:



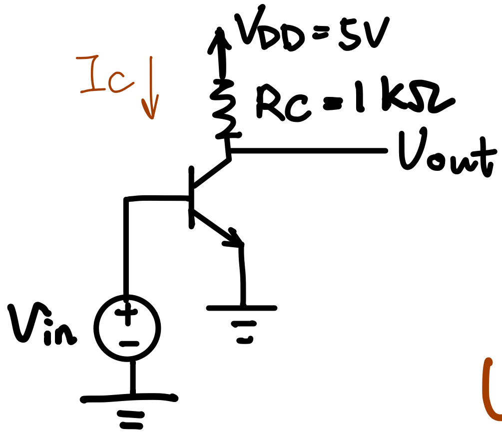
KCL: $V_{be} = V_{in} \dfrac{r_\pi}{r_\pi + R_B}$

$$A_V = -g_m r_o \cdot \frac{r_\pi}{r_\pi + R_B}$$

* What if there's a diode connected?



A typical complete question for BJT common-emitter:



Given $V_{in} = 0.5 + 0.001\sin(2\pi 60t)$

plot the waveform of V_{out}

(.model VAF = 100)

$$V_{out} = V_{OUT} + A_V \cdot 0.001\sin(2\pi 60t)$$

Step 1: Find V_{OUT} (DC part of V_{out})

$V_{OUT} = 5 - I_C \cdot (1K)$

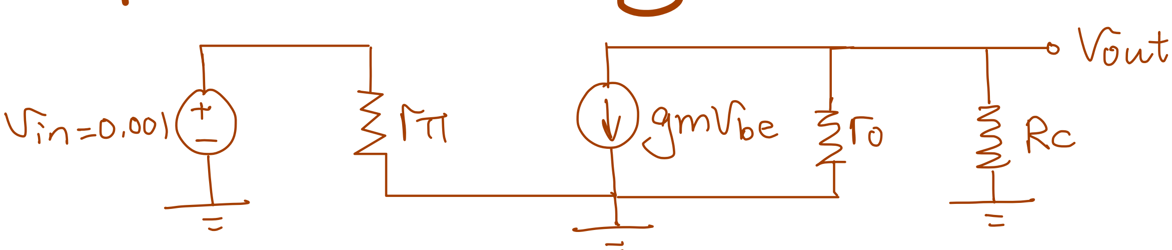
Plug in $I_C = I_S \cdot (e^{q\frac{V_{BE}}{KT}} - 1)(1 + \frac{V_{CE}}{V_A})$ $\quad$ * $\frac{KT}{q} \cong 0.026$

$\Rightarrow V_{OUT} = 5 - (1 \times 10^{-18}) \times (e^{\frac{0.5}{0.026}} - 1)(1 + \frac{V_{OUT}}{100}) \cdot (1K)$

Solve the Eq. $\Rightarrow V_{OUT} \cong 5V$

* Check if $V_{out} > V_{BE}$

Step 2: Use small-signal circuit to find A_V



$$A_V = \frac{V_{out}}{V_{in}} = -g_m(r_o // R_C)$$

(If $V_A \to \infty$, no this term, $A_V = -g_m R_C$)

Step 3: find I_c, g_m, r_o, r_π if needed in A_v

$$I_c = I_s \cdot \left(e^{\frac{qV_{BE}}{KT}} - 1\right)\left(1 + \frac{V_{CE}}{V_A}\right)$$

plug in V_{OUT} calculated in Step 1

$$\Rightarrow I_c = 2.36 \times 10^{-10}\ A$$

$$\Rightarrow g_m = \frac{I_c}{KT/q} = 9.079 \times 10^{-9}$$

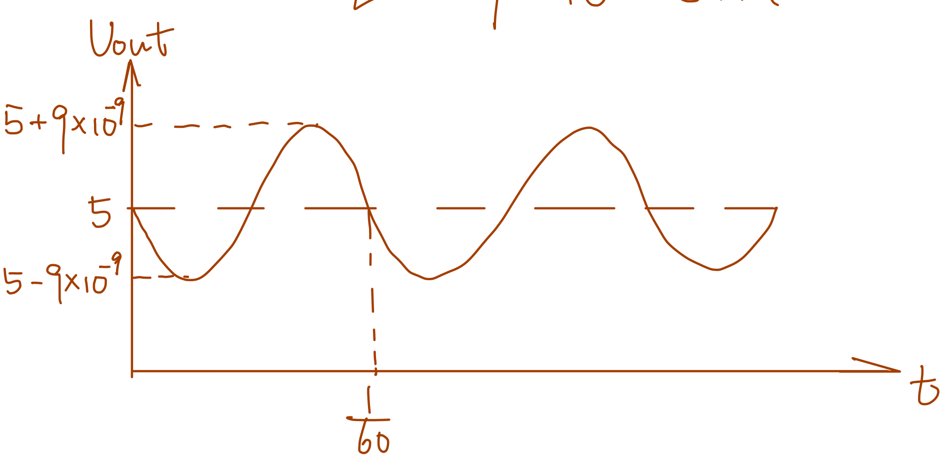
$$\Rightarrow r_o = \frac{V_A}{I_c} = \frac{100}{I_c} = 4.24 \times 10^{11}\ \Omega$$

$$A_v = -g_m(r_o // R_c) \cong -9 \times 10^{-6}$$

Step 4: Combine all to obtain V_{out}

$$V_{out} = V_{OUT} + A_v \cdot 0.001 \sin(2\pi 60 t)$$

$$= 5 - 9 \times 10^{-9} \sin(2\pi 60 t)$$



npn BJT Pspice Model

.model Qbreakn NPN IS=1e-18 BF=100 VAF=100

$$I_C = \mathbf{IS}\left(e^{\frac{qV_{BE}}{kT}} - 1\right)\left(1 + \frac{V_{CE}}{\mathbf{VAF}}\right)$$

$$\mathbf{BF} = \frac{I_C}{I_B} \qquad I_E = I_C + I_B$$

$$gm \cong \frac{I_C}{kT/q} \qquad r_\pi = \frac{\mathbf{BF}}{gm} \qquad r_o \cong \frac{\mathbf{VAF}}{I_C}$$