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# **COST 507**

**Definition of thermochemical and  
thermophysical properties to provide a  
database for the development  
of new light alloys**

**Thermochemical database for  
light metal alloys**

**Volume 2**

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## Volume 2

*Edited by*

I. Ansara, A. T. Dinsdale, M. H. Rand

July 1998

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**COST 507**  
**COORDINATION GROUP C**

**Final Report Round 2**  
**July 1998**

Partners in Coordination Group C, whose results are presented in the pages of this report, are:

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## **INTRODUCTION**

The COST-Action 507 has the official title:

### **Measurement and Evaluation of Thermochemical and Thermophysical Properties to Provide a Database for the Development of New Light Alloys**

There are 14 signatory countries to the Action, which had an official commencement date on January 1, 1990.

The countries concerned are:

Austria	Germany	Norway	Switzerland
Belgium	Greece	Portugal	United Kingdom
France	Italy	Spain	
Finland	Netherlands	Sweden	

In addition, the Baikov Institute of Metallurgy, Moscow (Russia) is taking part in the Action.

The work of COST 507 is shared amongst partners in 4 Coordination Groups whose areas of interest are:

Coordination Group A : Experimental measurement of thermochemical properties

Coordination Group B : Critical compilation and assessment of constitutional data prior to thermodynamic calculation

Coordination Group D : Experimental measurement and compilation of thermophysical data

Coordination Group C, whose work is presented in this report, is concerned with the general theme:

*Critical thermodynamic evaluation of relevant binary, ternary and higher-order alloy systems to produce a set of optimized coefficients for the light metal alloy database.*

The evaluations of Group C incorporate experimental data from Group A and Group D partners, and use the critically compiled constitution data from Group B as basis for the evaluation work.

Using this computer database, which is now in an impressive state of development, it will be possible to calculate the phase equilibria to be expected in complex light alloy systems as a function of a wide range of compositions and temperatures. For example calculation can be made of liquidus and solidus temperatures, crystallization paths for equilibrium and non-equilibrium conditions, nature and amounts of precipitated phases, enthalpy effects associated with phase transformations, etc.

The rapid accessibility of such information will considerably assist the design, manufacture and utilization of a wide range of different alloy types.

The alloy systems towards which the experimental and evaluation work is being directed, together with some major applications, are listed below:

Al-Mg-Mn-Fe-Si	:	cans
Al-Mg-Si-Cu (-Fe)	:	extrusions, automobiles
Al-Zn-Cu-Mg (-Zr,Cr,rare earth metals)	:	aerospace, transport
Al-Li-Cu-Mg-Zr (-H)	:	airframes
Ti-Al-Mo-Zr (Cu,B,C,N,O,Si)	:	gas turbines
Ti-Al (-V,Cr,Mn,Ni,Fe,Nb), (B,C,N,O,Si)	:	gas turbines

### EVALUATION PROCEDURE

Bearing in mind the alloy categories defined by industrial partners at the beginning of the Action, a matrix was drawn up to define the binary systems forming the building blocks for the evaluation of higher-order systems. These binaries were then allocated to the different partners in Group C for evaluation.

All partners made use of the selected data for the elements published by A.T. Dinsdale<sup>1</sup> on behalf of SGTE.

There was also agreement amongst partners with respect to the modelling of particular phases so that consistency could be maintained on proceeding from binary to higher-order systems combining evaluations originating from different laboratories. All results were prepared in exactly the same format to facilitate exchange of data and to provide a standard format for computer storage of the data by the database manager, Dr.Ansara, in Grenoble.

Evaluations to produce optimized sets of coefficients were carried out using one or

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<sup>1</sup>A.T. Dinsdale, *Calphad*, 15, 4, 317-425 (1991).

both of the two programs *Bingss/Tergss* written by Lukas<sup>2</sup> and *Parrot* developed by Jansson<sup>3</sup> contained in the *Thermo-Calc* databank system<sup>4</sup>.

These programs make use of experimental thermodynamic and phase diagram data, which are fed in as measured values with error limits. Using defined models for the different phases of the systems concerned, optimized coefficients are produced which permit a self-consistent description of the thermodynamic properties and the phase boundaries of the alloys.

For some alloy systems the available experimental information is very scarce or unreliable. In such cases, only a part of the system may have been dealt with. In other cases, recourse may have had to be made to estimation procedures to obtain input data for the optimization process. The accuracy of the calculations involving these data will consequently be reduced.

The following pages present in summarized form a complete description of the evaluation work carried out by the partners in Coordination Group C during the course of Round 1 and 2 of COST 507. The brief reports for each system contain a calculated phase diagram, information on the structures of the phases in the system. The thermodynamic coefficients used to produce the calculated information are also given.

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<sup>2</sup>H.L. Lukas, J. Weiss, and E.-Th. Henig, *Calphad*, 6, 229-251 (1982)

<sup>3</sup>B. Jansson, Ph. D. Thesis, (1984), Div. Phys. Met., Royal Inst. Tech., Stockholm, Sweden.

<sup>4</sup>B. Sundman, B. Jansson, and J.-O. Andersson, *Calphad*, 2, 9, 153-190 (1985).

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# Thermodynamic Modelling

I. Ansara and N. Dupin

## Introduction

Standard CALPHAD procedures were used to assess the binary and ternary systems defined in the COST507 project. In Round 1, binary systems have been assessed. Several ternary systems have been analysed during Round 2.

In many ternary systems, the three pure elements exhibit different stable crystal structure. Hence data for metastable binary solutions have been obtained and are presented in the tables.

In these systems, there are also many binary phases stable on one binary edge which extend into the ternary system but not all the way across to the other binary edges. (for example, the Laves-*C*15 in the Cu-Mg-Zn system or the AlM-*D*0<sub>19</sub> in the Al-Ti-X (X=Mo, Nb, Ti, W) systems). Thus to model the intrusion of these phases into the ternary systems, the Gibbs energies of the metastable counterparts of the intruding phase must be defined in the other binary system(s). This means that when the data of these binary systems are retrieved, there will be data for these metastable "counterparts".

As the number of ternary systems increases, the number of metastable solution phases or counterphases will increase sharply and this may lead to increasing computing time and possible problems due to metastable equilibria which may appear during the calculation.

The main characteristics of each system are given in individual chapters which include:

- a summary of the various stable and metastable phases defined in the system, the thermodynamic model used to describe their thermodynamic properties, the name of the assessor and the reference of the publication in which the evaluation is described,
- the thermodynamic properties of the compound and solution phases,
- for the binary systems: the phase diagram,
- for the binary systems: a table giving the invariant reactions,
- a table presenting the crystal structure for each phase in a given system, the structural type, the Pearson Symbol and space group as well as the occupation of the sublattices and comments when necessary. This information is taken from Massalski *et al.* [90Mas] and Villars *et al.* [91Vil].

In Appendix I, the thermodynamic functions for the elements in stable or metastable states are listed as a function of temperature. For magnetic ordering the functions are given in Appendix II.

## Thermodynamic Description

### Elements

The Gibbs energy of the pure element i,  ${}^{\circ}G_i^{\phi}(T)$ , referred to the enthalpy for its stable state  $\phi$  at 298.15 K,  ${}^{\circ}H_i^{\phi}(298.15\text{K})$ , is denoted by GHSER<sub>i</sub>. This quantity is described as a function of temperature by the following equation:

$$\begin{aligned}\text{GHSER}_i &= {}^{\circ}G_i^{\phi}(T) - {}^{\circ}H_i^{\phi}(298.15 \text{ K}) \\ &= a + b T + c T \cdot \ln T + d T^2 + e T^3 + f T^{-1} + g T^7 + h T^{-9} \quad (1)\end{aligned}$$

The first and second derivatives of this quantity with respect to temperature are related to the absolute entropy and heat capacity of the compound at the same temperature. Experimental values for heat capacities can thus be directly used in the optimisation and will be related to the coefficients  $c, d, e, f, g$  and  $h$ .

For elements which display a magnetic ordering (Cr, Fe, Ni and Mn), the term GHISER will be referred to a para-magnetic state. The magnetic contribution is treated explicitly. An additional term is thus added to the molar Gibbs energy of the magnetic phase.

For elements as well as for solutions, this term is equal to:

$$G^{\text{mag}} = RT \ln(\beta + 1) f(\tau) \quad (2)$$

where  $\tau$  is  $T/T^*$ ,  $T^*$  being the critical temperature for magnetic ordering (Curie temperature  $T_c$  for ferromagnetic materials or the Néel temperature  $T_N$  for antiferromagnetic materials), and  $\beta$  the average magnetic moment per atom of the alloy expressed in Bohr magnetons.

The function  $f(\tau)$  is given as:

$$\tau < 1 : f(\tau) = 1 - [79\tau^{-1}/140p + (474/497)(1/p - 1)(\tau^3/6 + \tau^9/135 + \tau^{15}/600)]/A$$

$$\tau > 1 : f(\tau) = -[\tau^{-5}/10 + \tau^{-15}/315 + \tau^{-25}/1500]/A$$

with  $A = 518/1125 + (11692/15975)(1/p - 1)$ .

These equations were derived by Hillert *et al.* [78Hil] from an expression of the magnetic heat capacity  $C_p^{\text{mag}}$  proposed by Inden [81Ind].

The value of  $p$  depends on the structure. For example,  $p$  is equal to 0.28 for fcc and hcp metals and 0.40 for bcc metals [81Ind].

For each element, equation 1 is taken from the SGTE database [91Din]. These equations and the magnetic parameters for pure elements are given in Appendices I and II.

The function  $\text{GHSER}_i$  is also often used to express the thermodynamic functions of a structure  $\varphi^*$  different from the stable structure of the pure element. The expression  $G_i^{\circ,\varphi^*}(T) - H_i^{\circ,\phi}(298.15\text{K})$  is equivalent to  $G_i^{\circ,\varphi^*}(T) - G_i^{\circ,\phi}(T) + \text{GHSER}_i$ . The term  $G_i^{\circ,\varphi^*}(T) - G_i^{\circ,\phi}(T)$  is often called the lattice stability of element  $i$ .

### Binary Compounds

The Gibbs energy of formation of the compound  $A_aB_b$  is expressed as:

$$G_{A_aB_b}^{\circ}(T) - a H_A^{\circ,\phi}(298.15 \text{ K}) - b H_B^{\circ,\phi}(298.15 \text{ K}) = f(T) \quad (3)$$

The expression for  $f(T)$  is identical to that given by equation 1.

Equation 3 can be transformed by applying equation 1 for each component

$$\begin{aligned} f(T) &= G_{A_aB_b}^{\circ}(T) - a G_A^{\circ,\phi}(T) - b G_B^{\circ,\phi}(T) + a \text{GHSER}_A + b \text{GHSER}_B \\ &= \Delta_f G_{A_aB_b}^T + a \text{GHSER}_A + b \text{GHSER}_B \end{aligned} \quad (4)$$

The term  $\Delta_f G_{A_aB_b}^T(T)$  is the Gibbs energy of formation of the compound referred to the stable elements at temperature  $T$ .

### Gaseous species

An expression identical to equation 3 is used to describe the Gibbs energy of formation of the gaseous species with the additional  $RT \ln P$  term, where  $P$  is the total pressure. The gas phase is assumed to form an ideal solution. The reference state for each vapor species is taken to be the pure component at 0.1 MPa pressure.

### Condensed phases

#### 1: Substitutional solutions:

For the substitutional solution  $\phi$ , the Gibbs energy of mixing is expressed as follows:

$$G_m = G^{\phi,\text{id}} + G^{\phi,\text{xs}} \quad (5)$$

with

$$G^{\phi,\text{id}} = R T \sum_i x_i \ln x_i \quad (6)$$

The Redlich - Kister equation [48Red], a power series expansion, is used to express the excess Gibbs energy,  $G_m^{\phi,\text{xs}}$ , as follows:

$$G_m^{\phi,ss} = x_i x_j \sum_{\nu=0} L_{ij}^{\nu,\phi} (x_i - x_j)^\nu \quad (7)$$

$x_i$  is the molar fraction of component i with  $\sum_i x_i = 1$ . The model parameter  $L_{ij}^\nu$  can be temperature dependent as follows:

$$L_{i,j,i} = y'_i y'_j [a_0 + b_0 T + c_0 T \cdot \ln T (a_1 + b_1 T) (y'_i - y'_j)] \quad (8)$$

For a ternary solution, the excess Gibbs energy is expressed as follows:

$$G^{\phi,ss} = \sum_i \sum_{j>i} x_i^\phi x_j^\phi \sum_\nu L_{ij}^{\nu,\phi} - (x_i^\phi - x_j^\phi)^\nu \quad (9)$$

If experimental information relative to ternary solutions are available then an extra term can be added to 9. For a ternary system A-B-C, this term is equal to:

$$x_A x_B x_C (\alpha_1 x_A + \alpha_2 x_B + \alpha_3 x_C) \quad (10)$$

For magnetic alloys, the composition dependence of  $T_c$  and  $\beta$  are expressed by:

$$T_c^*(x) = \sum_i x_i T_{c,i}^{0,*} + T_c^{*,ss} \quad (11)$$

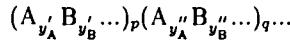
$$\beta(x) = \sum_i x_i \beta_i^0 + \beta^{ss} \quad (12)$$

where  $T^{*,ss}$  and  $\beta^{ss}$  are both represented by an equation similar to 7.

## 2: Ordered Phases:

The use of the sublattice model, developed by Hillert and Staffansson [70Hil] based on Temkin's model for ionic solutions [45Tem] and extended by Sundman and Ågren [81Sun], allows a variety of solution phases to be treated, in particular ordered phases.

As non-stoichiometric phases are formed by several sublattices, they can be schematically described as follows:



where the species A, B, ... can be atoms, vacancies or ions on the different sublattices ', ", .... The number of sites are  $p, q, \dots$  If  $p + q + \dots = 1$ , then the thermodynamic quantities are referred to one mole of sites.

For each sublattice  $s$ , the site fraction of the species  $i$  is equal to

$$y_i^s = \frac{n_i^s}{\sum_j n_j^s} = \frac{n_i^s}{n^s} \quad \text{with} \quad \sum_i y_i^s = 1 \quad \text{and} \quad \sum_s n^s = n \quad (13)$$

where  $n_i^s$  is the number of species  $i$  in sublattice  $s$ ,  $n^s$  the number of sites in sublattice  $s$ , and  $n$  the total number of sites.  $n^s$  is related to  $n$  by  $n^s = n \cdot p/(p + q + \dots)$ . The

number of sublattices and the species occupying them, is generally obtained from crystallographical information.

This model also describes stoichiometric phases, in which case the sublattices are occupied by a single atom, and substitutional phases which only contain one sublattice.

The molar Gibbs energy expressed by the sublattice model is equal to

$$G_m = G^{\text{ref}} + G^{\text{id}} + G^{\text{ex}} \quad (14)$$

For a two sublattice phase taken as an example, with two elements A and B in each of the sublattices, the term  $G^{\text{ref}}$ , which defines a surface of reference, is equal to

$$G^{\text{ref}} = y'_A y''_A G_{\text{A:A}}^{\circ} + y'_A y''_B G_{\text{A:B}}^{\circ} + y'_B y''_A G_{\text{B:A}}^{\circ} + y'_B y''_B G_{\text{B:B}}^{\circ} \quad (15)$$

The terms  $G_{\text{A:A}}^{\circ}$  and  $G_{\text{B:B}}^{\circ}$  represent the Gibbs energy of formation of the constituent elements A and B. The colon separates the different sublattices.

The terms  $G_{\text{A:B}}^{\circ}$  and  $G_{\text{B:A}}^{\circ}$  represent the Gibbs energy of formation of the stoichiometric compounds  $\text{A}_p\text{B}_q$  and  $\text{B}_p\text{A}_q$ , which may be stable or metastable.

The term  $G^{\text{id}}$  is related to the molar configurational entropy and is equal to:

$$G^{\text{id}} = R T [p(y'_A \ln y'_A + y'_B \ln y'_B) + q(y''_A \ln y''_A + y''_B \ln y''_B)] \quad (16)$$

Finally, the excess Gibbs energy  $G^{\text{ex}}$  is equal to

$$\begin{aligned} G^{\text{ex}} = & y'_A y'_B [y''_A L_{\text{A,B:A}} + y''_B L_{\text{A,B:B}}] \\ & + y''_A y''_B [y'_A L_{\text{A:A,B}} + y'_B L_{\text{B:A,B}}] \\ & + y'_A y'_B y''_A y''_B L_{\text{A,B:A,B}} \end{aligned} \quad (17)$$

The terms  $L_{i,j;i}$  and  $L_{i;i,j}$  represent the interaction parameters between the atoms on one sublattice for a given occupancy of the other, and can be described by a polynomial, as follows:

$$L_{i,j;i} = y'_i y'_j [a_0 + b_0 T + (a_1 + b_1 T)(y'_i - y'_j)] \quad (18)$$

The above equations can be expressed for ternary systems and they become more complicated when the number of species increases in each sublattice.

### 3. Order-disorder transformation:

For the COST project, only the order-disorder transformation relative to the bcc-A2 and bcc-B2 was considered. A unique function representing the Gibbs energy is used to describe the thermodynamic properties of both phases as follows:

$$G_m = G_m^{\text{dis}}(x_i) + \Delta G_m^{\text{ord}}(y_i^*) \quad (19)$$

where  $\Delta G_m^{ord}(y_i^s)$  and  $G_m^{dis}(x_i)$  are respectively the ordering energy, equal to zero in the disordered state, and  $G_m^{dis}(x_i)$  the molar Gibbs energy of the disordered phase.  $\Delta G_m^{ord}(y_i^s)$  is equal to:

$$\begin{aligned}\Delta G_m^{ord}(y_i^s) = & \sum_i \sum_j y_i^s y_j^s \Delta G_{i,j}^{ord} + RT \left( a \sum_i y_i^s \ln y_i^s + b \sum_i y_i^s \ln y_i^s \right) \\ & + y_A' y_B' \sum_i y_i^s L_{A,B,i}^{0,ord} + y_A' y_B (y_A - y_B) \sum_i y_i^s L_{A,B,i}^{1,ord} \\ & + y_A'' y_B'' \sum_i y_i^s L_{i:A,B}^{0,ord} + y_A'' y_B'' (y_A'' - y_B'') \sum_i y_i^s L_{i:A,B}^{1,ord} \\ & + y_A' y_B' y_A'' y_B'' L_{A,B:A,B}^{ord}\end{aligned}\quad (20)$$

$G_m^{dis}(x_i)$  is given in the Redlich-Kister formalism by equation 7.  $x_i$  and  $y_i^s$  are the molar fraction of element  $i$  in the phase and its site fraction in sublattice  $s$  respectively.

To ensure stability of the disordered phase, the first derivative of  $G_m$  with respect to the site occupation must be zero for any given composition. This condition and the fact that the ordering energy is zero for disorder leads to constraints between the thermodynamic parameters describing ordering [88Ans]. Using these constraints and converting the Gibbs energy of the disordered state into the sublattice formalism, allows to express the whole Gibbs energy of both phases ( $A2$  and  $B2$ ) in the sublattice formalism as follows:

$$\begin{aligned}G^\circ(T) - H_A^{\circ,ref}(298.15\text{ K}) = G(A:A) = \text{GREF}_A \\ G^\circ(T) - 0.5 H_A^{\circ,ref}(298.15\text{ K}) - 0.5 H_B^{\circ,ref}(298.15\text{ K}) = G(A:B) = \\ 0.5 \text{GREF}_A + 0.5 \text{GREF}_B + \Delta G_{A:B}^{ord} + \frac{1}{4} L_{A,B}^{0,dis} \\ G^\circ(T) - 0.5 H_A^{\circ,ref}(298.15\text{ K}) - 0.5 H_B^{\circ,ref}(298.15\text{ K}) = G(B:A) = \\ 0.5 \text{GREF}_A + 0.5 \text{GREF}_B + \Delta G_{A:B}^{ord} + \frac{1}{4} L_{A,B}^{0,dis} \\ G^\circ(T) - H_B^{\circ,ref}(298.15\text{ K}) = G(B:B) = \text{GREF}_B \\ L_{A,B:A}^0 = L_{A:A,B}^0 = -\Delta G_{A:B}^{ord} - L_{A,B:A}^{1,ord} + \frac{1}{4} L_{A,B}^{0,dis} + \frac{3}{8} L_{A,B}^{1,dis} + \frac{3}{16} L_{A,B}^{2,dis} \\ L_{A,B:A}^1 = L_{A:A,B}^1 = L_{A,B:A}^{1,ord} + \frac{1}{8} L_{A,B}^{1,dis} + \frac{4}{16} L_{A,B}^{2,dis} \\ L_{A,B:A}^2 = L_{A:A,B}^2 = \frac{1}{16} L_{A,B}^{2,dis} \\ L_{A,B:B}^0 = L_{B:A,B}^0 = -\Delta G_{A:B}^{ord} + L_{A,B:B}^{1,ord} + \frac{1}{4} L_{A,B}^{0,dis} - \frac{3}{8} L_{A,B}^{1,dis} + \frac{3}{16} L_{A,B}^{2,dis} \\ L_{A,B:B}^1 = L_{B:A,B}^1 = L_{A,B:B}^{1,ord} + \frac{1}{4} L_{A,B}^{1,dis} - \frac{4}{8} L_{A,B}^{2,dis} \\ L_{A,B:B}^2 = L_{B:A,B}^2 = \frac{1}{16} L_{A,B}^{2,dis} \\ L_{A,B:A,B} = 4L_{A,B:A}^{1,ord} - 4L_{A,B:B}^{1,ord} - \frac{24}{16} L_{A,B}^{2,dis}\end{aligned}\quad (21)$$

where  $\Delta G_{A:B}^{ord}$ ,  $L_{A,B:A}^{1,ord}$ ,  $L_{A,B:B}^{1,ord}$  are the independent ordering parameters and  $L_{A,B}^{0,dis}$ ,  $L_{A,B}^{1,dis}$ , and  $L_{A,B}^{2,dis}$ <sup>1</sup> are parameters of the disordered state.

In the binary systems Al-Fe, Cu-Mg, Cu-Zn, Fe-Si and Mg-Zn, the equations 21 were used with  $L_{A,B:A}^{1,ord}$  and  $L_{A,B:B}^{1,ord}$  equal to zero.

In a ternary system A-B-C, the relations 21 stand for each binary system. Moreover, the following constraints have to be fulfilled:

$$\begin{aligned}
 L_{C:A,B}^0 &= L_{A,B:C}^0 = L_{A,B:C}^{0,ord} + \frac{1}{4} L_{A,B}^{0,dis} - \frac{1}{8} (L_{A,C}^{1,dis} + L_{B,C}^{1,dis}) \\
 &\quad + \frac{1/2}{16} (L_{A,C}^{2,dis} + L_{B,C}^{2,dis}) \\
 L_{B:A,C}^0 &= L_{A,C:B}^0 = L_{A,C:B}^{0,ord} + \frac{1}{4} L_{A,C}^{0,dis} - \frac{1}{8} (L_{A,B}^{1,dis} - L_{B,C}^{1,dis}) \\
 &\quad + \frac{1/2}{16} (L_{A,B}^{2,dis} + L_{B,C}^{2,dis}) \\
 L_{A:B,C}^0 &= L_{B,C:A}^0 = L_{A,B:C}^{0,ord} + \frac{1}{4} L_{B,C}^{0,dis} + \frac{1}{8} (L_{A,B}^{1,dis} + L_{A,C}^{1,dis}) \\
 &\quad + \frac{1/2}{16} (L_{A,B}^{2,dis} + L_{A,C}^{2,dis}) \\
 L_{C:A,B}^1 &= L_{A,B:C}^1 = L_{A,B:C}^{1,ord} + \frac{1}{8} L_{A,B}^{1,dis} \\
 &\quad - \frac{1/2}{16} (L_{A,C}^{2,dis} - L_{B,C}^{2,dis}) \\
 L_{B:A,C}^1 &= L_{A,C:B}^1 = L_{A,C:B}^{1,ord} + \frac{1}{8} L_{A,C}^{1,dis} - \frac{1/2}{16} (L_{A,B}^{2,dis} - L_{B,C}^{2,dis}) \\
 L_{A:B,C}^1 &= L_{B,C:A}^1 = L_{B,C:A}^{1,ord} + \frac{1}{8} L_{B,C}^{1,dis} - \frac{1/2}{16} (L_{A,B}^{2,dis} - L_{A,C}^{2,dis}) \\
 L_{C:A,B}^2 &= L_{A,B:C}^2 = \frac{1}{16} L_{A,B}^{2,dis} \\
 L_{B:A,C}^2 &= L_{A,C:B}^2 = \frac{1}{16} L_{A,C}^{2,dis} \\
 L_{A:B,C}^2 &= L_{B,C:A}^2 = \frac{1}{16} L_{B,C}^{2,dis} \\
 L_{A,B:A,B} &= L_{A,C:A,B} = -\Delta G_{A:B}^{ord} - \Delta G_{A:C}^{ord} - \Delta G_{B:C}^{ord} - L_{A,B:C}^{0,ord} - L_{A,C:B}^{0,ord} \\
 &\quad - L_{B,C:A}^{0,ord} + L_{A,B:A}^{1,ord} - L_{A,B:C}^{1,ord} + L_{A,C:A}^{1,ord} - L_{A,C:B}^{1,ord} \\
 &\quad - \frac{1}{16} (5 L_{A,B}^{2,dis} + 5 L_{A,C}^{2,dis} + 2 L_{B,C}^{2,dis})
 \end{aligned}$$

<sup>1</sup>In the tables, the following substitutions were made:  $\Delta G_{A:B}^{ord} = G_{A:B:\square}^*$ ,  $\frac{1}{4} L_{A,B}^{0,dis} = L_{A,B}^0$ ,  $\frac{1}{8} L_{A,B}^{1,dis} = L_{A,B}^1$ ,  $\frac{1}{16} L_{A,B}^{2,dis} = L_{A,B}^2$

$$\begin{aligned}
L_{A,B:B,C} &= L_{B,C:A,B} = -\Delta G_{A:B}^{ord} - \Delta G_{A:C}^{ord} - \Delta G_{B:C}^{ord} - L_{A,B:C}^{0,ord} - L_{A,C:B}^{0,ord} \\
&\quad - L_{B,C:A}^{0,ord} + L_{A,B:B}^{1,ord} - L_{A,B:C}^{1,ord} + L_{B,C:A}^{1,ord} - L_{B,C:B}^{1,ord} \\
&\quad - \frac{1}{16} (5 L_{A,B}^{2,dis} + 2 L_{A,C}^{2,dis} + 5 L_{B,C}^{2,dis}) \\
L_{B,C:A,C} &= L_{A,C:B,C} = -\Delta G_{A:B}^{ord} - \Delta G_{A:C}^{ord} - \Delta G_{B:C}^{ord} - L_{A,B:C}^{0,ord} - L_{A,C:B}^{0,ord} \\
&\quad - L_{B,C:A}^{0,ord} + L_{A,C:B}^{1,ord} - L_{A,C:C}^{1,ord} + L_{B,C:A}^{1,ord} - L_{B,C:C}^{1,ord} \\
&\quad - \frac{1}{16} (2 L_{A,B}^{2,dis} + 5 L_{A,C}^{2,dis} + 5 L_{B,C}^{2,dis}) \\
L_{A:A,B,C} &= L_{A,B,C:A} = \frac{1}{32} (3 L_{A,B}^{2,dis} + 3 L_{A,C}^{2,dis}) \\
L_{B:A,B,C} &= L_{A,B,C:B} = \frac{1}{32} (3 L_{A,B}^{2,dis} + 3 L_{B,C}^{2,dis}) \\
L_{C:A,B,C} &= L_{A,B,C:C} = \frac{1}{16} (3/2 L_{A,C}^{2,dis} + 3/2 L_{B,C}^{2,dis}) \\
L_{A,B:A,B,C} &= L_{A,B,C:A,B} = 0 \\
L_{A,C:A,B,C} &= L_{A,B,C:A,C} = 0 \\
L_{B,C:A,B,C} &= L_{A,B,C:B,B} = 0 \\
L_{A,B,C:A,B,C} &= 0
\end{aligned} \tag{22}$$

where  $L_{A,B:C}^{0,ord}$ ,  $L_{A,C:B}^{0,ord}$ ,  $L_{B,C:A}^{0,ord}$ ,  $L_{A,B:C}^{1,ord}$ ,  $L_{A,C:B}^{1,ord}$ ,  $L_{B,C:A}^{1,ord}$  are the independent ternary parameters of ordering.

In the ternary system Cu-Mg-Zn, the regular interaction parameters  $L_{A,B:C}^{0,ord}$ ,  $L_{A,C:B}^{0,ord}$  and  $L_{B,C:A}^{0,ord}$ , were taken respectively identical to  $-\Delta G_{A:B}^{ord}$ ,  $-\Delta G_{A:C}^{ord}$  and  $-\Delta G_{B:C}^{ord}$ , and the sub-regular terms  $L_{A,B:C}^{1,ord}$ ,  $L_{A,C:B}^{1,ord}$  and  $L_{B,C:A}^{1,ord}$  equal to zero like in the corresponding binary systems.

Nevertheless, the use of this sublattice formalism to describe the order-disorder transformation requires the conversion of the parameters of the disordered state into the sublattice model which is cumbersome. A new treatment of the order-disorder transformation was introduced later on by Sundman [91Sun] where  $G_m$  is expressed as follows :

$$G_m = G_m^{dis}(x_i) + \Delta G^{ord*}(y_i, y_i^*) - \Delta G^{ord*}(x_i, x_i) \tag{23}$$

with

$$G_m^{dis}(x_i) = \sum_i x_i \Delta G_i^{dis} + RT \sum_i x_i \ln x_i + x_A x_B \sum_\nu L_{A,B}^{\nu,dis} (x_A - x_B)^\nu \tag{24}$$

$$\begin{aligned}\Delta G^{\text{ord*}}(y_i^*, y_i'') &= \sum_i \sum_j y_i^* y_j'' \Delta^* G_{i;j}^{\text{ord*}} + RT \left( a \sum_i y_i^* \ln y_i^* + b \sum_i y_i'' \ln y_i'' \right) \\ &\quad + y_A^* y_B^* \sum_i y_i'' L_{A,B;i}^{0,\text{ord*}} + y_A^* y_B^* (y_A^* - y_B^*) \sum_i y_i'' L_{A,B;i}^{1,\text{ord*}} \\ &\quad + y_A'' y_B'' \sum_i y_i^* L_{i:A,B}^{0,\text{ord*}} + y_A'' y_B'' (y_A'' - y_B'') \sum_i y_i^* L_{i:A,B}^{1,\text{ord*}} \\ &\quad + y_A^* y_B^* y_A'' y_B'' L_{A,B;A,B}^{\text{ord*}}\end{aligned}\quad (25)$$

$$\begin{aligned}\Delta G^{\text{ord*}}(x_i, x_i) &= \sum_i \sum_j x_i x_j \Delta^* G_{i;j}^{\text{ord*}} + RT \left( a \sum_i x_i \ln x_i + b \sum_i x_i \ln x_i \right) \\ &\quad + x_A x_B \sum_i x_i L_{A,B;i}^{0,\text{ord*}} + x_A x_B (x_A - x_B) \sum_i x_i L_{A,B;i}^{1,\text{ord*}} \\ &\quad + x_A x_B \sum_i x_i L_{i:A,B}^{0,\text{ord*}} + x_A x_B (x_A - x_B) \sum_i x_i L_{i:A,B}^{1,\text{ord*}} \\ &\quad + x_A x_B x_A x_B L_{A,B;A,B}^{\text{ord*}}\end{aligned}\quad (26)$$

Hence, the disordered and ordered phases can be treated separately. The parameters of the disordered phase,  $L_{A,B}^{\nu,\text{dis}}$ , and those describing the ordering  $\Delta^* G_{A:B}^{\text{ord*}}$ ,  $L_{A,B;i}^{\nu,\text{ord*}}$ ,  $L_{i:A,B}^{\nu,\text{ord*}}$  and  $L_{A,B;A,B}^{\text{ord*}}$  are introduced as usual thermodynamic parameters of the sublattice model and a special command then allows their combination to define the expression of the order-disorder sublattice following equation 23.

Constraints must still be introduced between the thermodynamic parameters of the function  $\Delta G(y_i, y_i'')$  to ensure stability of the disordered state. But the value zero for the ordering energy is now built in. This allows to simplify the expression of the constraints linking the ordering parameters.

The ternary systems Al–Ti–(Mo,Nb,Ta,W) were assessed with equation 23 assuming

$$\begin{aligned}\Delta^* G_{i;j}^{\text{ord*}} = \Delta^* G_{j;i}^{\text{ord*}} &= -L_{i,j;i}^{0,\text{ord*}} = -L_{i,j;j}^{0,\text{ord*}} = -L_{i,j;k}^{0,\text{ord*}} \\ &= -L_{i;i,j}^{0,\text{ord*}} = -L_{j;i,j}^{0,\text{ord*}} = -L_{k;i,j}^{0,\text{ord*}} = \alpha_{ij}\end{aligned}\quad (27)$$

These relations are identical to 21 and 22 when disordered parameters are not considered and sub-regular ordering terms are zero. The use of equation 23 allows a simpler but mathematically equivalent description with only two ordering parameters:

$$\Delta^* G_{i;j}^{\text{ord*}} = \Delta^* G_{j;i}^{\text{ord*}} = 2\alpha_{ij}\quad (28)$$

When such simplification is possible, the two descriptions (the original using equations 27 and the modified using equations 28) are presented in this report.

For sake of uniformity, the descriptions using the sublattice model with the constraints 21 and 22 were also converted for use of equation 23 in the simpler way possible.

Only the parameters derived from the simpler description are in the database. In this report, they are presented in a frame. An example is shown hereunder for a binary system.

**Phase bcc-B2**

$$G^\circ(T) - H_A^{\circ,\text{ref}}(298.15 \text{ K}) = G(\text{A:A}) = 0.0$$

$$G^\circ(T) - 0.5 H_A^{\circ,\text{ref}}(298.15 \text{ K}) - 0.5 H_B^{\circ,\text{ref}}(298.15 \text{ K}) = G(\text{A:B}) = 2.0 G_{\text{A:B}}^{\text{ord}}$$

$$G^\circ(T) - 0.5 H_A^{\circ,\text{ref}}(298.15 \text{ K}) - 0.5 H_B^{\circ,\text{ref}}(298.15 \text{ K}) = G(\text{B:A}) = 2.0 G_{\text{A:B}}^{\text{ord}}$$

$$G^\circ(T) - H_B^{\circ,\text{ref}}(298.15 \text{ K}) = G(\text{B:B}) = 0.0$$

**Phase bcc-A2**

$$G^\circ(T) - H_A^{\circ,\text{ref}}(298.15 \text{ K}) = \text{GREF}_A$$

$$G^\circ(T) - H_B^{\circ,\text{ref}}(298.15 \text{ K}) = \text{GREF}_B$$

$$L_{\text{A,B:}\square}^{0,\text{dis}} = 4 L_{\text{A,B}}^0$$

$$L_{\text{A,B:}\square}^{1,\text{dis}} = 8 L_{\text{A,B}}^1$$

$$L_{\text{A,B:}\square}^{2,\text{dis}} = 16 L_{\text{A,B}}^2$$

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## **BINARY SYSTEMS**



# System Al-B

Solution Phases:

Liquid, fcc-Al

Compounds:

AlB<sub>2</sub>, AlB<sub>12</sub>-L, AlB<sub>12</sub>-H

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-Al	:	Substitutional, Redlich-Kister
AlB <sub>2</sub>	:	Stoichiometric, (Al)(B) <sub>2</sub>
AlB <sub>12</sub> -L	:	Stoichiometric, (Al)(B) <sub>12</sub>
AlB <sub>12</sub> -H	:	Stoichiometric, (Al)(B) <sub>12</sub>

Assessor and Date:

H.L. Lukas 1992

Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)

**Phase AlB<sub>2</sub>**

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 2.0 \cdot H_{\text{B}}^{\circ,\beta-\text{rhombo}-\text{B}}(298.15 \text{ K}) = \\ - 85808.76 + 45.46923 \cdot T + \text{GHSER}_{\text{Al}} + 2.0 \cdot \text{GHSER}_{\text{B}}$$

**Phase AlB<sub>12</sub>-L**

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 12.0 \cdot H_{\text{B}}^{\circ,\beta-\text{rhombo}-\text{B}}(298.15 \text{ K}) = \\ - 198290.69 + 33.68638 \cdot T + \text{GHSER}_{\text{Al}} + 12.0 \cdot \text{GHSER}_{\text{B}}$$

**Phase AlB<sub>12</sub>-H**

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 12.0 \cdot H_{\text{B}}^{\circ,\beta-\text{rhombo}-\text{B}}(298.15 \text{ K}) = \\ - 75292.23 - 33.66376 \cdot T + \text{GHSER}_{\text{Al}} + 12.0 \cdot \text{GHSER}_{\text{B}}$$

**Phase fcc-Al**

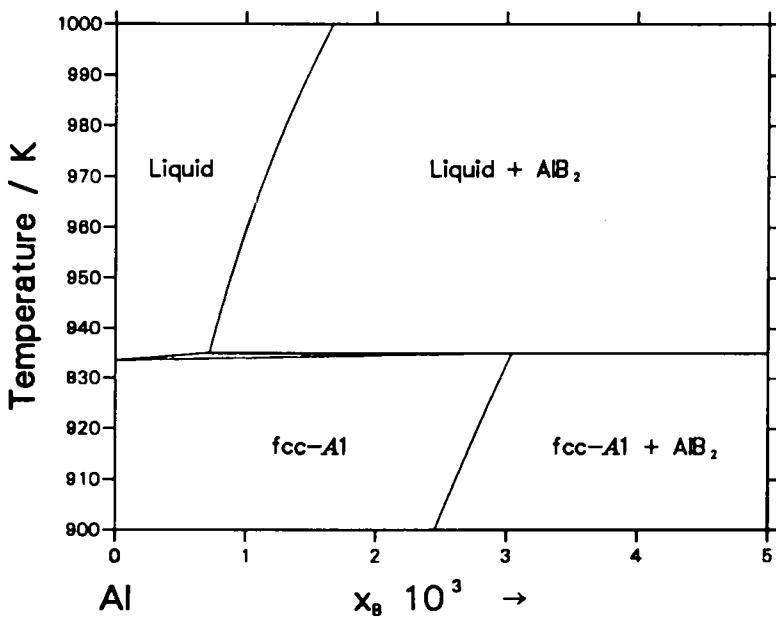
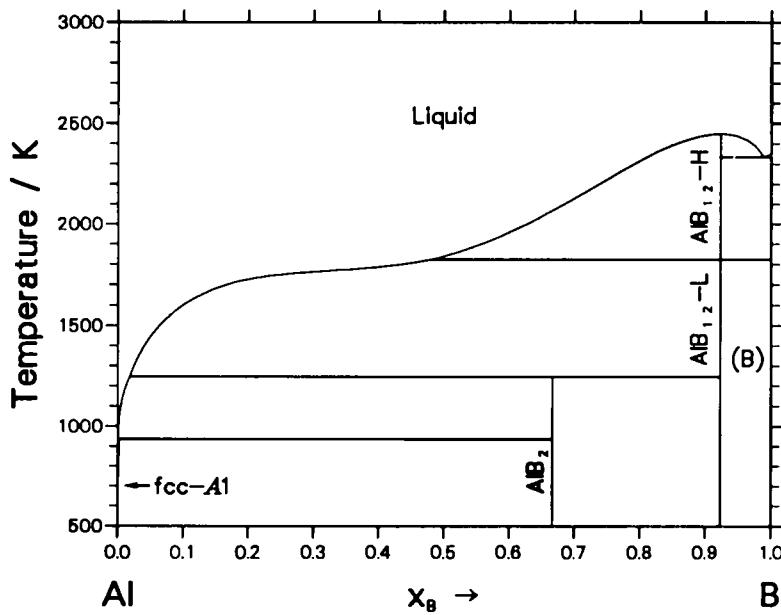
$$L_{\text{Al},\text{B}:□}^{0,\text{fcc}-\text{A}1} = 12242.44 - 1.74891 \cdot T$$

### Phase liquid

$$L_{\text{Al},\text{B}}^{0,\text{liquid}} = -12671.16 + 1.81016 \ T$$

$$L_{\text{Al},\text{B}}^{1,\text{liquid}} = 31988.28$$

$$L_{\text{Al},\text{B}}^{2,\text{liquid}} = -15873.74$$



**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_B$			$T / K$
Liquid + AlB <sub>2</sub> ⇌ fcc-Al	Peritectic	.003	.667	.0007	935.0
Liquid + AlB <sub>12</sub> -L ⇌ AlB <sub>2</sub>	Peritectic	.019	.923	.667	1245.8
AlB <sub>12</sub> -L ⇌ AlB <sub>12</sub> -H	Polymorphic	.923	.923	.....	1826.2
Liquid ⇌ AlB <sub>12</sub> -H + $\beta$ -rhombo-B	Eutectic	.988	.923	1.000	2336.0
AlB <sub>12</sub> -H ⇌ Liquid	Congruent	.923	.923	.....	2448.0

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-B	(Al)	Cu	<i>cF4</i> <i>Fm\bar{3}m</i>	M 4	
	(B)	$\beta$ -rhombo-B			not assessed
	AlB <sub>10</sub>	AlB <sub>10</sub>	<i>oC88</i> <i>Cmcm</i>		
	AlB <sub>12</sub> -L	AlB <sub>12</sub>	<i>oP384</i> <i>P2<sub>1</sub>2<sub>1</sub>2<sub>1</sub></i>		AlB <sub>12</sub> - $\alpha$ in [90Mas]
	AlB <sub>12</sub> -H	AlB <sub>12</sub>	<i>tP216</i> <i>P4<sub>1</sub>2<sub>1</sub>2</i>		AlB <sub>12</sub> - $\beta$ in [90Mas]
	AlB <sub>2</sub>	AlB <sub>2</sub>	<i>hP3</i> <i>P6/mmm</i>	Al 1 B 2	

# System Al-C

**Solution Phases:**

Liquid, fcc-Al

**Compound:**

Al<sub>4</sub>C<sub>3</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc-Al	:	Sublattice model , (Al)(C, $\square$ )
Al <sub>4</sub> C <sub>3</sub>	:	Stoichiometric, (Al) <sub>4</sub> (C) <sub>3</sub>

**Assessor and Date:**

J. Gröbner, H. L. Lukas, and F. Aldinger.

**Publication:**

Calphad, **20**, 2 (1996) 247-254.

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Al<sub>4</sub>C<sub>3</sub>**

$$G^\circ(T) - 4.0 \text{ } H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 3.0 \text{ } H_{\text{C}}^{\circ,\text{graphite}}(298.15 \text{ K}) = \\ - 286002.0 + 1030.273 \text{ } T - 161.709142 \text{ } T \cdot \ln T - 0.011523 \text{ } T^2 \\ + 2450000 \text{ } T^{-1} + 7E-07 \text{ } T^3$$

**Phase fcc-A1**

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{C}}^{\circ,\text{graphite}}(298.15 \text{ K}) = \\ 80 \text{ } T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{C}}$$

$$L_{\text{Al:C},\square}^{0,\text{fcc}-\text{A}1} = 80 \text{ } T$$

**Phase graphite**

$$L_{\text{Al,C}}^{0,\text{graphite}} = 80 \text{ } T$$

**Phase liquid**

$$L_{\text{Al,C}}^{0,\text{liquid}} = 40861.02 - 33.21138 \text{ } T$$

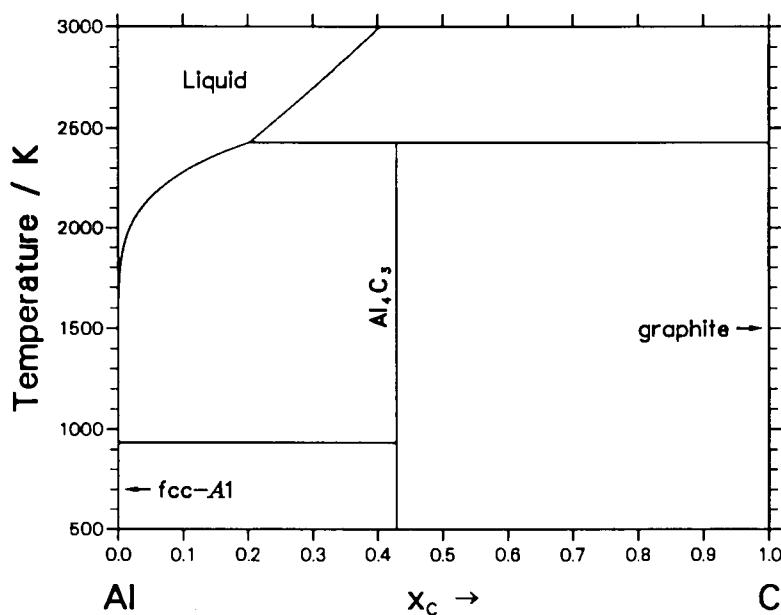


Table I - Invariant Reactions.

Reaction	Type	Compositions x <sub>C</sub>	T / K
Liquid + graphite ⇌ Al <sub>4</sub> C <sub>3</sub>	Peritectic	.198    1.000    .429	2429.0
Liquid ⇌ fcc-Al + Al <sub>4</sub> C <sub>3</sub>	Degenerate	.000    .000    .429	933.5

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices
Al-C	(Al)	Cu	cF4 Fm3m	M 4
	(C)	graphite		
	Al <sub>4</sub> C <sub>3</sub>	Al <sub>4</sub> C <sub>3</sub>	hR7 R3m	Al <sub>1</sub> 2 Al <sub>2</sub> 2 C <sub>1</sub> 1 C <sub>2</sub> 2

# System Al–Ce

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1

**Compounds:**

Al<sub>11</sub>Ce<sub>3</sub>, Al<sub>3</sub>Ce, AlCe, AlCe<sub>2</sub>, Al<sub>2</sub>Ce

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
Al <sub>11</sub> Ce <sub>3</sub>	:	Stoichiometric, (Al) <sub>11</sub> (Ce) <sub>3</sub>
Al <sub>3</sub> Ce	:	Stoichiometric, (Al) <sub>3</sub> (Ce)
Al <sub>2</sub> Ce	:	Stoichiometric, (Al) <sub>2</sub> (Ce)
AlCe	:	Stoichiometric, (Al)(Ce)
AlCe <sub>2</sub>	:	Stoichiometric, (Al)(Ce) <sub>2</sub>

**Assessor and Date:**

G. Cacciamani, G. Borzone, R. Ferro

**Publication:**

revised 1997

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Al<sub>11</sub>Ce<sub>3</sub>**

$$G^\circ(T) - 11.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 3.0 \ H_{\text{Ce}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = \\ - 574000 + 179.3087 \ T + 11.0 \ \text{GHSER}_{\text{Al}} + 3.0 \ \text{GHSER}_{\text{Ce}}$$

**Phase Al<sub>3</sub>Ce**

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Ce}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = \\ - 176000 + 54.97964 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Ce}}$$

**Phase AlCe**

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Ce}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = \\ - 92000 + 33.90118 \ T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Ce}}$$

**Phase  $\text{AlCe}_3$** 

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Ce}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = \\ - 108000 + 41.3726 T + \text{GIISER}_{\text{Al}} + 3.0 \text{ GIISER}_{\text{Ce}}$$

**Phase Laves-C15**

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ce}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = \\ - 150000.0 + 45.66405 T + 2.0 \text{ GIISER}_{\text{Al}} + \text{GIISER}_{\text{Ce}}$$

**Phase bcc-A2**

$$L_{\text{Al,Ce};\square}^{0,\text{bcc}-A2} = 80 T$$

**Phase fcc-A1**

$$L_{\text{Al,Ce};\square}^{0,\text{fcc}-A1} = 80 T$$

**Phase Liquid**

$$L_{\text{Al,Ce}}^{0,\text{liquid}} = - 167593.1 + 84.87628 T$$

$$L_{\text{Al,Ce}}^{1,\text{liquid}} = - 36060 + 5.89346 T$$

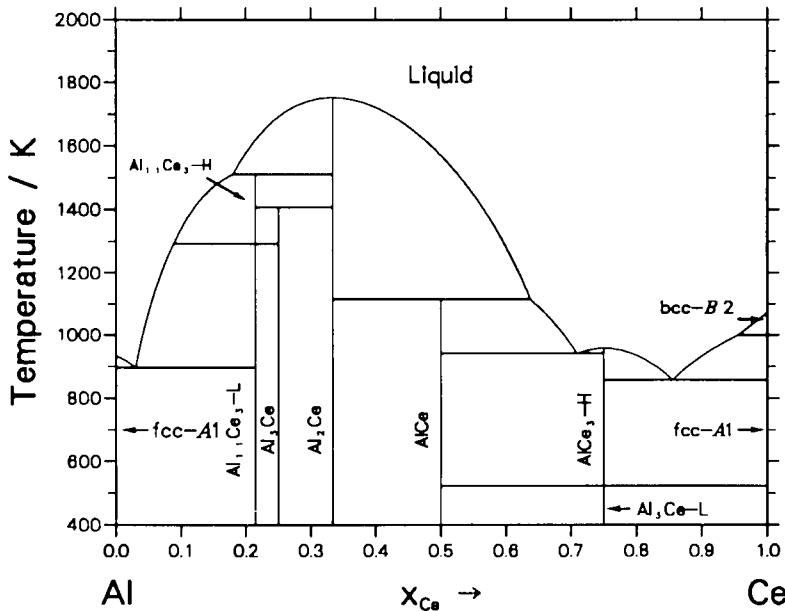


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{Ce}$			$T / K$
Liquid $\rightleftharpoons$ fcc-Al + Al <sub>11</sub> Ce <sub>3</sub>	Eutectic	.028	.000	.214	902.6
Liquid + Laves-C15* $\rightleftharpoons$ Al <sub>11</sub> Ce <sub>3</sub>	Peritectic	.179	.333	.214	1497.1
Liquid + Laves-C15* $\rightleftharpoons$ AlCe	Peritectic	.619	.333	.500	1116.9
Liquid $\rightleftharpoons$ AlCe + AlCe <sub>3</sub>	Eutectic	.704	.500	.750	911.3
Liquid $\rightleftharpoons$ AlCe <sub>3</sub> + fcc-Al	Eutectic	.854	.750	1.000	852.2
Liquid $\rightleftharpoons$ bcc-A2 + fcc-Al	Polymorphic	.956	1.000	1.000	1000.0
Al <sub>11</sub> Ce <sub>3</sub> + Laves-C15* $\rightleftharpoons$ Al <sub>3</sub> Ce	Peritectoid	.214	.333	.250	1408.0
Laves-C15* $\rightleftharpoons$ Liquid	Congruent	.333	.333	.....	1752.0

\* Laves-C15  $\equiv$  Al<sub>2</sub>Ce

Table II - Crystal Structure and Phase Description.

System	Phase	Structural Type	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Ce	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M 4	polymorphic trans. not considered
	(Ce)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M 4	
	(Ce)	W	<i>cI2</i> <i>Im</i> $\bar{3}m$	M 2	
	Al <sub>11</sub> Ce <sub>3</sub> - $\alpha$	Al <sub>11</sub> La <sub>3</sub>	<i>I</i> $mmm$ <i>o</i> $1\bar{2}\bar{8}$		
	Al <sub>11</sub> Ce <sub>3</sub> - $\beta$	Al <sub>4</sub> Ba	<i>I</i> <sub>4</sub> / <i>mmm</i> <i>t</i> $1\bar{1}0$		
	Al <sub>3</sub> Ce	Ni <sub>3</sub> Sn	<i>hP8</i> <i>P</i> <sub>6</sub> <sub>3</sub> / <i>mmc</i>		
	Al <sub>2</sub> Ce	Cu <sub>2</sub> Mg	<i>cF24</i> <i>Fd</i> $\bar{3}m$	Ce 8 Al 16	
	AlCe	AlCe	<i>oC16</i> <i>Cmcm</i>	Al <sub>1</sub> 4 Al <sub>2</sub> 4 Ce 8	
	AlCe <sub>3</sub> - $\alpha$	Ni <sub>3</sub> Sn	<i>hP8</i> <i>P</i> <sub>6</sub> <sub>3</sub> / <i>mmc</i>	Al 2 Ce 6	
	AlCe <sub>3</sub> - $\beta$	AuCu <sub>3</sub>	<i>cP4</i> <i>Pm</i> $\bar{3}m$	Al 1 Ce 3	

# System Al-Cr

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1

**Compounds:**

AlCr<sub>2</sub>, Al<sub>4</sub>Cr, Al<sub>8</sub>Cr<sub>5</sub>-L, Al<sub>8</sub>Cr<sub>5</sub>-H, Al<sub>9</sub>Cr<sub>4</sub>-L,  
Al<sub>9</sub>Cr<sub>4</sub>-H, Al<sub>11</sub>Cr<sub>2</sub>, Al<sub>13</sub>Cr<sub>2</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
AlCr <sub>2</sub>	:	Stoichiometric, (Al)(Cr) <sub>4</sub>
Al <sub>4</sub> Cr	:	Stoichiometric, (Al) <sub>4</sub> (Cr)
Al <sub>8</sub> Cr <sub>5</sub> -L	:	Stoichiometric, (Al) <sub>8</sub> (Cr) <sub>5</sub> -L
Al <sub>8</sub> Cr <sub>5</sub> -H	:	Stoichiometric, (Al) <sub>8</sub> (Cr) <sub>5</sub> -H
Al <sub>9</sub> Cr <sub>4</sub> -L	:	Stoichiometric, (Al) <sub>9</sub> (Cr) <sub>4</sub> -L
Al <sub>9</sub> Cr <sub>4</sub> -H	:	Stoichiometric, (Al) <sub>9</sub> (Cr) <sub>4</sub> -H
Al <sub>11</sub> Cr <sub>2</sub>	:	Stoichiometric, (Al) <sub>11</sub> (Cr) <sub>2</sub>
Al <sub>13</sub> Cr <sub>2</sub>	:	Stoichiometric, (Al) <sub>13</sub> (Cr) <sub>2</sub>

**Assessor and Date:**

N. Saunders, 1991

**Publication:**

based on the publication of N. Saunders and V.G. Rivlin  
in Z. für Metallkde, 78, (11) 795-801 (1987).

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase AlCr<sub>2</sub>**

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 2.0 \cdot H_{\text{Cr}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) = \\ - 32700.0 - 8.79 \cdot T + \text{GHSER}_{\text{Al}} + 2.0 \cdot \text{GHSER}_{\text{Cr}}$$

**Phase Al<sub>4</sub>Cr**

$$G^\circ(T) - 4.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Cr}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) = \\ - 89025.0 + 19.05 \cdot T + 4.0 \cdot \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cr}}$$

**Phase  $\text{Al}_8\text{Cr}_5\text{-L}$** 

$$G^\circ(T) - 8.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 5.0 \ H_{\text{Cr}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) = \\ - 229515.0 + 8.0 \ \text{GHSER}_{\text{Al}} + 5.0 \ \text{GHSER}_{\text{Cr}}$$

**Phase  $\text{Al}_8\text{Cr}_5\text{-H}$** 

$$G^\circ(T) - 8.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 5.0 \ H_{\text{Cr}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) = \\ - 147732.0 - 58.5 \ T + 8.0 \ \text{GHSER}_{\text{Al}} + 5.0 \ \text{GHSER}_{\text{Cr}}$$

**Phase  $\text{Al}_9\text{Cr}_4\text{-L}$** 

$$G^\circ(T) - 9.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 4.0 \ H_{\text{Cr}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) = \\ - 230750.0 + 16.094 \ T + 9.0 \ \text{GHSER}_{\text{Al}} + 4.0 \ \text{GHSER}_{\text{Cr}}$$

**Phase  $\text{Al}_9\text{Cr}_4\text{-H}$** 

$$G^\circ(T) - 9.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 4.0 \ H_{\text{Cr}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) = \\ - 134433.0 - 56.16 \ T + 9.0 \ \text{GHSER}_{\text{Al}} + 4.0 \ \text{GHSER}_{\text{Cr}}$$

**Phase  $\text{Al}_{11}\text{Cr}_2$** 

$$G^\circ(T) - 11.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 \ H_{\text{Cr}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) = \\ - 175500.0 + 25.805 \ T + 11.0 \ \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Cr}}$$

**Phase  $\text{Al}_{13}\text{Cr}_2$** 

$$G^\circ(T) - 13.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 \ H_{\text{Cr}}^{\circ,\text{bcc-A2,para}}(298.15 \text{ K}) = \\ - 174405.0 + 22.2 \ T + 13.0 \ \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Cr}}$$

**Phase bcc-A2**

$$L_{\text{Al,Cr:\square}}^{0,\text{bcc-A2}} = - 54900 + 10 \ T$$

**Phase fcc-A1**

$$L_{\text{Al,Cr:\square}}^{0,\text{fcc-A1}} = - 45900 + 6.0 \ T$$

**Phase liquid**

$$L_{\text{Al,Cr}}^{0,\text{liquid}} = - 29000.0$$

$$L_{\text{Al,Cr}}^{1,\text{liquid}} = - 11000.0$$

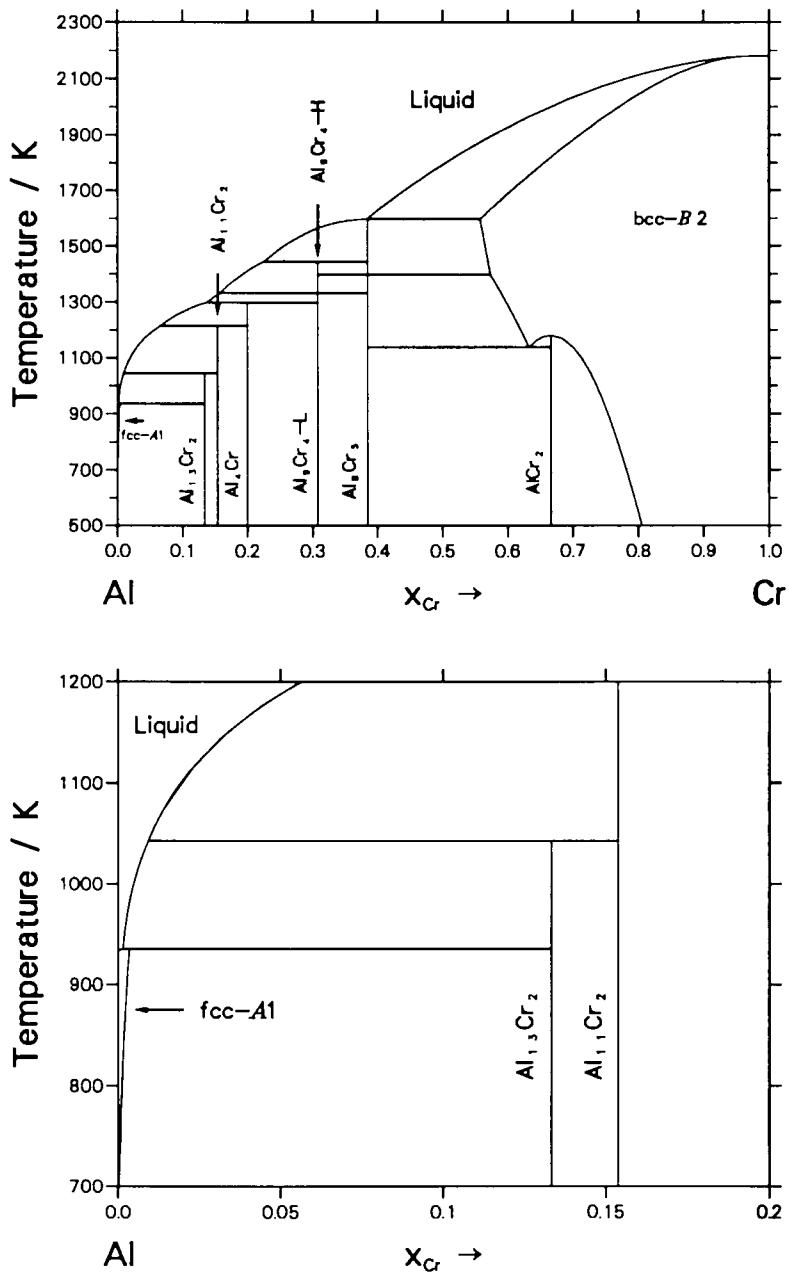


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{Cr}$			$T / K$
Liquid + $Al_{13}Cr_2 \rightleftharpoons fcc-Al$	Peritectic	.002	.133	.003	934.8
Liquid + $Al_{11}Cr_2 \rightleftharpoons Al_{13}Cr_2$	Peritectic	.009	.154	.133	1042.9
Liquid + $Al_4Cr \rightleftharpoons Al_{11}Cr_2$	Peritectic	.066	.200	.154	1214.6
Liquid + $Al_9Cr_4-L \rightleftharpoons Al_4Cr$	Peritectic	.137	.308	.200	1298.1
$Al_9Cr_4-H \rightleftharpoons Al_9Cr_4-L$	Polymorphic	.158	.158	...	1333.0
Liquid + $Al_8Cr_5-II \rightleftharpoons Al_9Cr_4-H$	Peritectic	.225	.385	.307	1443.1
Liquid $\rightleftharpoons Al_8Cr_5-H + bcc-A2$	Eutectic	.385	.383	.558	1597.0
$Al_8Cr_5-H \rightleftharpoons Al_8Cr_5-L$	Polymorphic	.385	.385	...	1398.0
$bcc-A2 \rightleftharpoons Al_8Cr_5-L + AlCr_2$	Eutectoid	.633	.385	.667	1139.3
$AlCr_2 \rightleftharpoons bcc-A2$	Congruent	.667	.667	...	1181.0

Table II:a - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Cr	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	also designated by $Al_5Cr$ in [90Mas]
	(Cr)	W	$cI2$ $Im\bar{3}m$	M 2	
	$AlCr_2$	$MoSi_2$	$tI6$ $I4/mmm$	Al 2	
	$Al_4Cr$	$Al_4Cr$	$mP180$ $P2/m$	Cr 4	
	$Al_{11}Cr_2$	$Al_5Cr$	$mP48$ $P2$		
	$Al_8Cr_5-L$	$Al_8Cr_5$	$hR26$ $R\bar{3}m$		
	$Al_8Cr_5-H$	$Al_8Cr_5$	$hR26$		
	$Al_9Cr_4-L$		$cI52$ $I\bar{4}3m$		
	$Al_9Cr_4-H$				

**Table II:b - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
	Al <sub>13</sub> Cr <sub>2</sub> - $\beta$	Al <sub>45</sub> V <sub>7</sub>	<i>mC104</i> <i>C2/m</i>	Al <sub>1</sub> 2 Al <sub>2</sub> 4 Al <sub>3</sub> 4 Al <sub>4</sub> 4 Al <sub>5</sub> 4 Al <sub>6</sub> 4 Al <sub>7</sub> 4 Al <sub>8</sub> 4 Al <sub>9</sub> 4 Al <sub>10</sub> 8 Al <sub>11</sub> 8 Al <sub>12</sub> 8 Al <sub>13</sub> 8 Al <sub>14</sub> 8 Al <sub>15</sub> 4 Al <sub>16</sub> 4 Cr <sub>1</sub> 2 Cr <sub>2</sub> 4 Cr <sub>3</sub> 8	also designated by by Al <sub>7</sub> Cr in [90Mas]

# System Al–Cu

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, fcc- <i>A</i> 1
(metastable)	hcp- <i>A</i> 3

**Compounds:**

(stable)	AlCu- $\delta$ , AlCu- $\epsilon$ , AlCu- $\eta$ , AlCu- $\theta$ , AlCu- $\gamma(D8_3)$ AlCu- $\gamma(H)$ , AlCu- $\zeta$
(metastable)	Laves- <i>C</i> 14, Laves- <i>C</i> 15, Laves- <i>C</i> 36

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
AlCu- $\delta$	:	Sublattice model, $(Al,Cu)_2(Cu)_3$
AlCu- $\epsilon$	:	Sublattice model, $(Al,Cu)(Cu)$
AlCu- $\eta$	:	Sublattice model, $(Al,Cu)(Cu)$
AlCu- $\theta$	:	Sublattice model, $(Al)(Al,Cu)_2$
AlCu- $\gamma(D8_3)$	:	Sublattice model, $(Al)_4(Al,Cu)(Cu)_8$
AlCu- $\gamma(H)$	:	Sublattice model, $(Al)_4(Al,Cu)(Cu)_8$
AlCu- $\zeta$	:	Stoichiometric, $(Al)_9(Cu)_{11}$
Laves- <i>C</i> 14	:	Sublattice model, $(Al,Cu)_2(Al,Cu)$
Laves- <i>C</i> 15	:	Sublattice model, $(Al,Cu)_2(Al,Cu)$
Laves- <i>C</i> 36	:	Sublattice model, $(Al,Cu)_2(Al,Cu)$

**Assessor and Date:**

N. Saunders, 1991

Data relative to the Laves phases evaluated in Round II.

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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**


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**Phase AlCu- $\delta$** 

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 3.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = \\ - 106700.0 + 3.0 \ T + 2.0 \ \text{GHSER}_{\text{Al}} + 3.0 \ \text{GHSER}_{\text{Cu}}$$

**Phase AlCu- $\epsilon$** 

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Al:Cu}) = \\ - 36976 + 1.2 \ T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 2.0 \ \text{GBCC}_{\text{Cu}}$$

$$L_{\text{Al,Cu:Cu}}^{0,\text{AlCu-}\epsilon} = 7600 - 24 \ T$$

$$L_{\text{Al,Cu:Cu}}^{1,\text{AlCu-}\epsilon} = - 72000$$

**Phase AlCu- $\eta$** 

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Al:Cu}) = \\ - 40560.0 + 3.14 \ T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 2.0 \ \text{GBCC}_{\text{Cu}}$$

$$L_{\text{Al,Cu:Cu}}^{0,\text{AlCu-}\eta} = - 25740 - 20 \ T$$

**Phase AlCu- $\theta$** 

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Al:Al}) = 3.0 \ \text{GBCC}_{\text{Al}}$$

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Al:Cu}) = \\ - 47406.0 + 6.75 \ T + 2.0 \ \text{GHSER}_{\text{Al}} + 1.0 \ \text{GHSER}_{\text{Cu}}$$

$$L_{\text{Al:Al:Cu}}^{0,\text{AlCu-}\theta} = 2211$$

**Phase AlCu- $\zeta$** 

$$G^\circ(T) - 9.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 11.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = \\ - 420000.0 + 18.0 \ T + 9.0 \ \text{GHSER}_{\text{Al}} + 11.0 \ \text{GHSER}_{\text{Cu}}$$

**Phase AlCu- $\gamma$ (D8<sub>3</sub>)**

$$G^\circ(T) - 5.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 8.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Al:Al:Cu}) = \\ - 300716.0 + 390.0 \ T - 52 \ T \cdot \ln T + 5.0 \ \text{GHSER}_{\text{Al}} \\ + 8.0 \ \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 4.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 9.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Al:Cu:Cu}) = \\ - 280501.0 + 379.6 \ T - 52 \ T \cdot \ln T + 4.0 \ \text{GHSER}_{\text{Al}} \\ + 9.0 \ \text{GHSER}_{\text{Cu}}$$

### Phase AlCu- $\gamma$ (H)

$$\begin{aligned} G^\circ(T) - 5.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 8.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Al:Al:Cu}) = \\ - 219258.0 - 45.5 \ T + 5.0 \ \text{GHSER}_{\text{Al}} + 8.0 \ \text{GHSER}_{\text{Cu}} \\ G^\circ(T) - 4.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 9.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Al:Cu:Cu}) = \\ - 200460.0 - 58.5 \ T + 4.0 \ \text{GHSER}_{\text{Al}} + 9.0 \ \text{GHSER}_{\text{Cu}} \end{aligned}$$

### Phase Laves-C14

$$\begin{aligned} G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Al:Al}) = \\ 15000.0 + 3.0 \ \text{GHSER}_{\text{Al}} \\ G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Al:Cu}) = \\ 15000.0 + 2.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}} \\ G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 2.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Cu:Al}) = \\ 15000.0 + \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Cu}} \\ G^\circ(T) - 3.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = \\ 15000.0 + 3.0 \ \text{GHSER}_{\text{Cu}} \\ L_{\text{Al,Cu:Al}}^{0,\text{Laves-C14}} = - 24000 + 2.44 \ T \\ L_{\text{Al,Cu:Cu}}^{0,\text{Laves-C14}} = - 24000 + 2.44 \ T \end{aligned}$$

### Phase Laves-C15

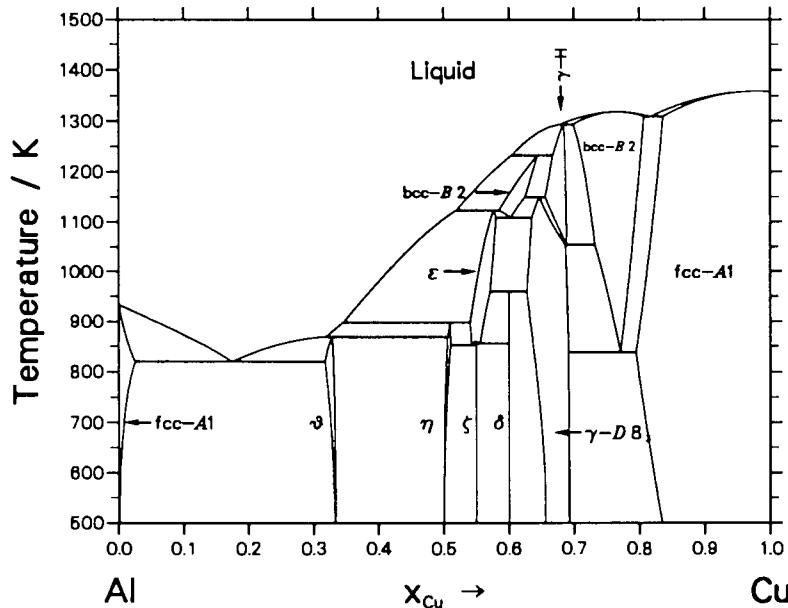
$$\begin{aligned} G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Al:Al}) = \\ 15000.0 + 3.0 \ \text{GHSER}_{\text{Al}} \\ G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Al:Cu}) = \\ 15000.0 + 2.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}} \\ G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 2.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Cu:Al}) = \\ 15000.0 + \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Cu}} \\ G^\circ(T) - 3.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = \\ 15000.0 + 3.0 \ \text{GHSER}_{\text{Cu}} \\ L_{\text{Al,Cu:Al}}^{0,\text{Laves-C15}} = - 105000 - 1.615 \ T \\ L_{\text{Al,Cu:Cu}}^{0,\text{Laves-C15}} = - 105000 - 1.615 \ T \end{aligned}$$

### Phase Laves-C36

$$\begin{aligned} G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Al:Al}) = \\ 15000.0 + 3.0 \ \text{GHSER}_{\text{Al}} \\ G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Al:Cu}) = \\ 15000.0 + 2.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}} \\ G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 2.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Cu:Al}) = \\ 15000.0 + \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Cu}} \\ G^\circ(T) - 3.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = \end{aligned}$$

$$L_{\text{Al,Cu:Al}}^{0,\text{Laves-C36}} = \frac{15000.0 + 3.0 \text{ GIISER}_{\text{Cu}}}{-126169 + 14.61 T}$$

$$L_{\text{Al,Cu:Cu}}^{0,\text{Laves-C36}} = \frac{-126169 + 14.61 T}{-126169 + 14.61 T}$$



### Phase bcc-A2

$$L_{\text{Al,Cu:□}}^{0,\text{bcc-A2}} = \frac{-73554 + 4.0 T}{-73554 + 4.0 T}$$

$$L_{\text{Al,Cu:□}}^{1,\text{bcc-A2}} = \frac{51500 - 11.84 T}{51500 - 11.84 T}$$

### Phase fcc-A1

$$L_{\text{Al,Cu:□}}^{0,\text{fcc-A1}} = \frac{-53520 + 2 T}{-53520 + 2 T}$$

$$L_{\text{Al,Cu:□}}^{1,\text{fcc-A1}} = \frac{38590 - 2 T}{38590 - 2 T}$$

$$L_{\text{Al,Cu:□}}^{2,\text{fcc-A1}} = \frac{1170}{1170}$$

### Phase liquid

$$L_{\text{Al,Cu}}^{0,\text{liquid}} = - 66622 + 8.1 \cdot T$$

$$L_{\text{Al,Cu}}^{1,\text{liquid}} = 46800 - 90.8 \cdot T + 10 \cdot T \cdot \ln T$$

$$L_{\text{Al,Cu}}^{2,\text{liquid}} = - 2812$$

**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Cu}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ fcc-A1 + AlCu- $\theta$	Eutectic	.175	.025	.318	820.7
Liquid + AlCu- $\eta$ $\rightleftharpoons$ AlCu- $\theta$	Peritectic	.319	.506	.329	869.0
Liquid + AlCu- $\epsilon$ $\rightleftharpoons$ AlCu- $\eta$	Peritectic	.345	.541	.510	898.0
Liquid + bcc-A2 $\rightleftharpoons$ AlCu- $\epsilon$	Peritectic	.519	.585	.576	1124.0
Liquid + AlCu- $\gamma(\text{H})$ $\rightleftharpoons$ bcc-A2	Peritectic	.604	.667	.644	1232.4
Liquid + bcc-A2 $\rightleftharpoons$ AlCu- $\gamma(\text{H})$	Peritectic	.678	.698	.684	1293.4
Liquid $\rightleftharpoons$ bcc-A2 + fcc-A1	Eutectic	.817	.807	.837	1309.3
bcc-A2 $\rightleftharpoons$ AlCu- $\gamma(D8_3)$ + fcc-A1	Eutectoid	.771	.691	.795	837.9
AlCu- $\gamma(\text{H})$ $\rightleftharpoons$ AlCu- $\gamma(D8_3)$ + bcc-A2	Eutectoid	.688	.686	.732	1054.2
bcc-A2 + AlCu- $\gamma(\text{H})$ $\rightleftharpoons$ AlCu- $\gamma(D8_3)$	Peritectoid	.625	.656	.647	1150.5
bcc-A2 $\rightleftharpoons$ AlCu- $\epsilon$ + AlCu- $\gamma(D8_3)$	Eutectoid	.602	.580	.635	1109.3
AlCu- $\epsilon$ + AlCu- $\gamma(D8_3)$ $\rightleftharpoons$ AlCu- $\delta$	Peritectoid	.572	.628	.600	959.7
AlCu- $\epsilon$ $\rightleftharpoons$ AlCu- $\zeta$ + AlCu- $\delta$	Eutectoid	.555	.550	.600	855.8
AlCu- $\epsilon$ $\rightleftharpoons$ AlCu- $\eta$ + AlCu- $\zeta$	Eutectoid	.543	.511	.550	852.4
AlCu- $\zeta$ $\rightleftharpoons$ AlCu- $\epsilon$	Congruent	.550	.550	...	861.0

**Table II:a – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Cu	(Al)	Cu	$cF\bar{4}$ $Fm\bar{3}m$	M 4	not considered
	(Cu)	Cu	$cF\bar{4}$ $Fm\bar{3}m$	M 4	
	$\beta$	W	$cI\bar{2}$ $I\bar{m}\bar{3}m$	M 2	
	$\beta_0$				

Table II:b – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol	Symbol Group	Sub- lattices	Comments
	AlCu- $\delta$		....			
	AlCu- $\eta_1$		$P\bar{b}an$ or $Cmmm$ $oP16$ or $oC16$			high $T$ phase
	AlCu- $\eta_2$	AlCu	$mC20$ $C2/m$			low $T$ phase
	AlCu- $\theta$	Al <sub>2</sub> Cu	$tI12$ $I4/mcm$	Al Cu	8 4	
	AlCu- $\delta$	....	....			
	AlCu- $\epsilon_1$	NiAs	$hP\bar{4}$ $P\bar{6}_3/mmc$			low $T$ phase
	AlCu- $\epsilon_2$	....	....			not considered
	AlCu- $\gamma(D8_3)$	Al <sub>4</sub> Cu <sub>9</sub>	$cP52$ $P\bar{4}3m$	Al <sub>1</sub> Al <sub>2</sub> Cu <sub>1</sub> Cu <sub>2</sub> Cu <sub>3</sub> Cu <sub>4</sub> Cu <sub>5</sub> Cu <sub>6</sub>	4 12 4 4 4 6 6 12	
	AlCu- $\gamma(H)$	....	....			
	AlCu- $\zeta_1$	....	$hP\bar{4}2$ $C2/m$			$\zeta_1$
	AlCu- $\zeta_2$	....				$\zeta_2$ not considered

## System Al-Fe

**Solution Phases:**

(stable) :	Liquid, fcc- <i>A</i> 1, bcc- <i>A</i> 2, bcc- <i>B</i> 2, $\text{Al}_5\text{Fe}_4$
(metastable) :	cbcc- <i>A</i> 12, cub- <i>A</i> 13, hcp- <i>A</i> 3

**Compounds:**

stable :	$\text{Al}_2\text{Fe}$ , $\text{Al}_5\text{Fe}_2$ , $\text{Al}_{13}\text{Fe}_4$ ,
metastable :	$\text{Al}_{11}\text{Mn}_4$ , $\text{Al}_{12}\text{Mn}$ , $\text{Al}_6\text{Mn}$

**Modelling:**

Liquid :	Substitutional, Redlich-Kister
cbcc- <i>A</i> 12 :	Substitutional, Redlich-Kister
cub- <i>A</i> 13 :	Substitutional, Redlich-Kister
fcc- <i>A</i> 1 :	Substitutional, Redlich-Kister
hcp- <i>A</i> 3 :	Substitutional, Redlich-Kister
bcc- <i>A</i> 2 :	see below
bcc- <i>B</i> 2 :	Sublattice model, $(\text{Al},\text{Fe})_{0.5}(\text{Al},\text{Fe})_{0.5}(\square)_3$ Two descriptions of the bcc- <i>A</i> 2:bcc- <i>B</i> 2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.
$\text{Al}_5\text{Fe}_4$ :	Substitutional, Redlich-Kister
$\text{Al}_{13}\text{Fe}_4$ :	Sublattice model, $(\text{Al})_{0.6275}(\text{Fe})_{0.235}(\text{Al},\square)_{0.1375}$
$\text{Al}_2\text{Fe}$ :	Stoichiometric, $(\text{Al})_2(\text{Fe})$
$\text{Al}_5\text{Fe}_2$ :	Stoichiometric, $(\text{Al})_5(\text{Fe})_2$
$\text{Al}_{11}\text{Mn}_4$ :	Stoichiometric, $(\text{Al})_{11}(\text{Mn})_4$
$\text{Al}_{12}\text{Mn}$ :	Stoichiometric, $(\text{Al})_{12}(\text{Mn})$
$\text{Al}_6\text{Mn}$ :	Stoichiometric, $(\text{Al})_6(\text{Mn})$

**Assessor and Date:**

M. Seierstein, 1991

**Comments:**

$\text{Al}_{11}\text{Mn}_4$ ,  $\text{Al}_{12}\text{Mn}$  and  $\text{Al}_6\text{Mn}$  and the hcp-*A*3 phase have been evaluated by Å. Jansson and T.G.Chart (1995) in the assessment of the Al-Fe-Mn system.

Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**Phase fcc-A1**

$$L_{\text{Al},\text{Fe}:□}^{0,\text{fcc}-\text{A}1} = -76066.1 + 18.6758 \ T$$

$$L_{\text{Al},\text{Fe}:□}^{1,\text{fcc}-\text{A}1} = 21167.4 + 1.3398 \ T$$

**Phase hcp-A3**

$$L_{\text{Al},\text{Fe}:□}^{0,\text{hcp}-\text{A}3} = -106903.0 + 20.0 \ T$$

**Phase liquid**

$$L_{\text{Al},\text{Fe}}^{0,\text{liquid}} = -91976.5 + 22.1314 \ T$$

$$L_{\text{Al},\text{Fe}}^{1,\text{liquid}} = -5672.58 + 4.8728 \ T$$

$$L_{\text{Al},\text{Fe}}^{2,\text{liquid}} = 121.9$$

**Phase Al<sub>2</sub>Fe**

$$\begin{aligned} G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) = \\ -98097.0 + 18.7503 \ T + 2.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Fe}} \end{aligned}$$

**Phase Al<sub>13</sub>Fe<sub>4</sub>**

$$\begin{aligned} G^\circ(T) - 0.765 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 0.235 \ H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) = \\ \text{G(Al:Fe:Al)} = -30714.4 + 7.44 \ T + 0.765 \ \text{GHSER}_{\text{Al}} + 0.235 \ \text{GHSER}_{\text{Fe}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 0.6275 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 0.235 \ H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) = \\ \text{G(Al:Fe:□)} = -27781.3 + 7.2566 \ T + 0.6275 \ \text{GHSER}_{\text{Al}} + 0.235 \ \text{GHSER}_{\text{Fe}} \end{aligned}$$

**Phase Al<sub>5</sub>Fe<sub>2</sub>**

$$\begin{aligned} G^\circ(T) - 5.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 2.0 \ H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) = \\ -228576 + 48.99503 \ T + 5.0 \ \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Fe}} \end{aligned}$$

### Phase $\text{Al}_5\text{Fe}_4$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = 12178.90 - 4.813 \cdot T + \text{GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) = 5009.03 + \text{GHSER}_{\text{Fe}}$$

$$L_{\text{Al},\text{Fe}}^{0,\text{Al}_5\text{Fe}_4} = -131649 + 29.4833 \cdot T$$

$$L_{\text{Al},\text{Fe}}^{1,\text{Al}_5\text{Fe}_4} = -18619.5$$

### Phase bcc-B2

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = \text{GBCC}_{\text{Al}}$$

$$G^\circ(T) - 0.5 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 \cdot H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) = G(\text{Fe:All:}\square) = -37890.5 + 7.9972 \cdot T + 0.5 \cdot \text{GBCC}_{\text{Al}} + 0.5 \cdot \text{GHSER}_{\text{Fe}}$$

$$T_{\text{c},\text{Fe:Al:}\square}^{\text{bcc}-B2} = 521.5 \quad \beta_{\text{Fe:Al:}\square}^{\text{bcc}-B2} = 1.11$$

$$G^\circ(T) - 0.5 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 \cdot H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) = G(\text{Al:Fe:}\square) = -37890.5 + 7.9972 \cdot T + 0.5 \cdot \text{GBCC}_{\text{Al}} + 0.5 \cdot \text{GHSER}_{\text{Fe}}$$

$$T_{\text{c,Al:Fe:}\square}^{\text{bcc}-B2} = 521.5 \quad \beta_{\text{c,Al:Fe:}\square}^{\text{bcc}-B2} = 1.11$$

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) = G(\text{Fe:Fe:}\square) = \text{GHSER}_{\text{Fe}}$$

$$T_{\text{c,Fe:Fe:}\square}^{\text{bcc}-B2} = 1043 \text{K} \quad \beta_{\text{c,Fe:Fe:}\square}^{\text{bcc}-B2} = 2.22$$

$$L_{\text{Al},\text{Fe:Al:}\square}^{0,\text{bcc}-B2} = L_{\text{Al:Al,Fe:}\square}^{0,\text{bcc}-B2} = -22485.07 + 7.9772 \cdot T$$

$$L_{\text{Al},\text{Fe:Al:}\square}^{1,\text{bcc}-B2} = L_{\text{Al:Al,Fe:}\square}^{1,\text{bcc}-B2} = 368.15$$

$$T_{\text{c,Al:Fe:Al:}\square}^{0,\text{bcc}-B2} = T_{\text{c,Al:Al,Fe:}\square}^{0,\text{bcc}-B2} = 189.0$$

$$T_{\text{c,Al:Fe:Al:}\square}^{1,\text{bcc}-B2} = T_{\text{c,Al:Al,Fe:}\square}^{1,\text{bcc}-B2} = 63.0$$

$$\beta_{\text{Al,Fe:Al:}\square}^{0,\text{bcc}-B2} = \beta_{\text{Al:Al,Fe:}\square}^{0,\text{bcc}-B2} = 0.0$$

$$T_{\text{c,Al:Fe:Fe:}\square}^{0,\text{bcc}-B2} = T_{\text{c,Fe:Al,Fe:}\square}^{0,\text{bcc}-B2} = -189.0$$

$$T_{\text{c,Al:Fe:Fe:}\square}^{1,\text{bcc}-B2} = T_{\text{c,Fe:Al,Fe:}\square}^{1,\text{bcc}-B2} = 63.0$$

$$\beta_{\text{Al,Fe:Fe:}\square}^{0,\text{bcc}-B2} = \beta_{\text{Fe:Al,Fe:}\square}^{0,\text{bcc}-B2} = 0.0$$

$$L_{\text{Fe:Al,Fe:}\square}^{0,\text{bcc}-B2} = L_{\text{Al:Fe:Fe:}\square}^{0,\text{bcc}-B2} = -24694.0 + 7.9772 \cdot T$$

$$L_{\text{Fe:Al,Fe:}\square}^{1,\text{bcc}-B2} = L_{\text{Al:Fe:Fe:}\square}^{1,\text{bcc}-B2} = 368.15$$

$$G_{\text{Al:Fe:}\square}^* = -860 R \quad (R = 8.31451)$$

$$L_{\text{Al,Fe}}^0 = -30740 + 7.9972 T$$

$$L_{\text{Al,Fe}}^1 = 386.15$$

### Phase bcc-B2

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Fe}}^{\circ,\text{fcc}-A1,\text{para}}(298.15 \text{ K}) = G(\text{Al:Fe:}\square) = 2.0 G_{\text{Al:Fe:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Fe}}^{\circ,\text{fcc}-A1,\text{para}}(298.15 \text{ K}) = G(\text{Fe:Al:}\square) = 2.0 G_{\text{Al:Fe:}\square}^*$$

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{fcc}-A1,\text{para}}(298.15 \text{ K}) = G(\text{Fe:Fe:}\square) = 0.0$$

### Phase bcc-A2

$$L_{\text{Al,Fe:}\square}^{0,\text{bcc}-A2} = 4.0 L_{\text{Al,Fe}}^0$$

$$L_{\text{Al,Fe:}\square}^{1,\text{bcc}-A2} = 8.0 L_{\text{Al,Fe}}^1$$

$$T_{\text{C,Al,Fe:}\square}^{1,\text{bcc}-A2} = 504$$

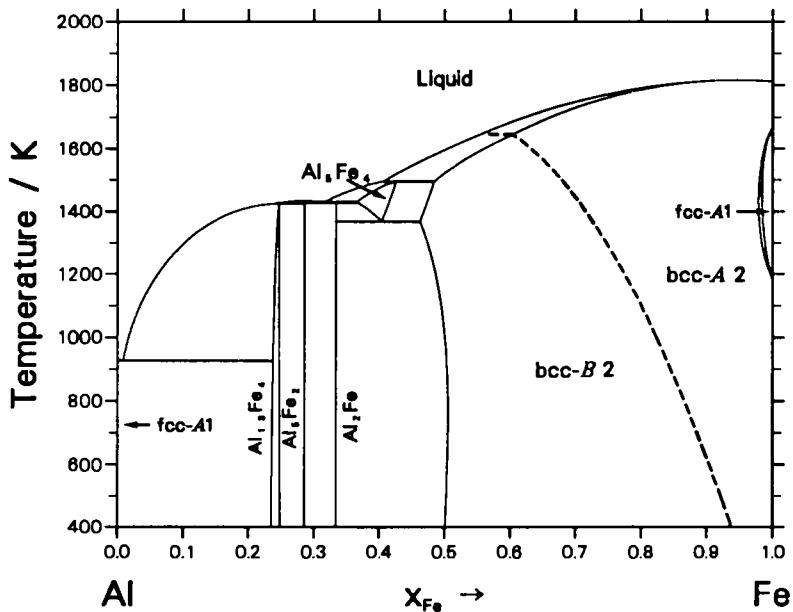


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Fe}}$	$T / \text{K}$
$\text{Al}_5\text{Fe}_4 \rightleftharpoons \text{bcc}-\text{B}2 + \text{Al}_2\text{Fe}$	Eutectoid	.403 .462 .333	1368.2
$\text{Al}_5\text{Fe}_2 \rightleftharpoons \text{Liquid}$	Congruent	.286 .286 ....	1434.5
$\text{Liquid} \rightleftharpoons \text{Al}_5\text{Fe}_2 + \text{Al}_5\text{Fe}_4$	Eutectic	.316 .286 .365	1430.0
$\text{Liquid} + \text{Al}_5\text{Fe}_2 \rightleftharpoons \text{Al}_{13}\text{Fe}_4$	Peritectic	.242 .286 .247	1424.4
$\text{Liquid} \rightleftharpoons \text{fcc}-\text{A}1 + \text{Al}_{13}\text{Fe}_4$	Eutectic	.009 .000 .237	927.1
$\text{Liquid} + \text{bcc}-\text{B}2 \rightleftharpoons \text{Al}_5\text{Fe}_4$	Peritectic	.405 .483 .425	1495.5
$\text{Al}_5\text{Fe}_2 + \text{Al}_5\text{Fe}_4 \rightleftharpoons \text{Al}_2\text{Fe}$	Peritectoid	.286 .366 .333	1428.1

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol Space Group	Sub-lattices	Comments
Al-Fe	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>	M 4	
	(Fe)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>	M 4	
	(Fe)	W	<i>cI2</i> <i>I</i> $\bar{m}$ $\bar{3}m$	M 2	
	AlFe	CsCl	<i>cP2</i> <i>Pm</i> $\bar{3}m$	M <sub>1</sub> 1 M <sub>2</sub> 1	
	AlFe <sub>3</sub>	BiF <sub>3</sub>	<i>cF16</i> <i>Fm</i> $\bar{3}m$	Al 4 Fe <sub>1</sub> 4 Fe <sub>2</sub> 8	not considered
	Al <sub>2</sub> Fe	Al <sub>2</sub> Fe	<i>aP18</i> <i>P1</i>		
	Al <sub>3</sub> Fe		<i>mC102</i> <i>C2/m</i>		designated by Al <sub>13</sub> Fe <sub>4</sub>
	Al <sub>5</sub> Fe <sub>2</sub>		<i>oC*</i> <i>Cmcm</i>		
	ε		<i>cI16?</i>		designated by Al <sub>5</sub> Fe <sub>4</sub>
	Al <sub>6</sub> Fe	Al <sub>6</sub> Fe	<i>oC28</i> <i>Cmc2</i> <sub>1</sub>	Al <sub>1</sub> 4 Al <sub>2</sub> 4 Al <sub>3</sub> 8 Al <sub>4</sub> 8 Fe 4	metastable
	Al <sub>9</sub> Fe <sub>2</sub>	Al <sub>9</sub> Co <sub>2</sub>	<i>mP22</i> <i>P2</i> <sub>1</sub> / <i>c</i>		metastable

# System Al-Li

**Solution Phases:**

(stable)	:	Liquid, bcc- <i>A</i> 2, fcc- <i>A</i> 1
(metastable)	:	hcp- <i>A</i> 3

**Compounds:**

(stable)	AllLi, Al <sub>2</sub> Li <sub>3</sub> , Al <sub>4</sub> Li <sub>9</sub>
(metastable)	AlMg- $\beta$ , Al <sub>2</sub> Zr, Al <sub>3</sub> Zr, Al <sub>3</sub> Zr <sub>2</sub> , Al <sub>12</sub> Mg <sub>17</sub>

**Modelling:**

bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Liquid	:	Substitutional, Redlich-Kister
AllLi	:	Sublattice model, (Al,Li)(Li, $\square$ )
Al <sub>2</sub> Li <sub>3</sub>	:	Stoichiometric, (Al) <sub>2</sub> (Li) <sub>3</sub>
Al <sub>4</sub> Li <sub>9</sub>	:	Stoichiometric, (Al) <sub>4</sub> (Li) <sub>9</sub>
Al <sub>12</sub> Mg <sub>17</sub>	:	Sublattice model, (Li) <sub>24</sub> (Al,Li) <sub>10</sub> (Al) <sub>24</sub>
Al <sub>2</sub> Zr	:	Sublattice model, (Al) <sub>2</sub> (Zr)
Al <sub>3</sub> Zr	:	Sublattice model, (Al) <sub>3</sub> (Zr)
Al <sub>3</sub> Zr <sub>2</sub>	:	Sublattice model, (Al) <sub>3</sub> (Zr) <sub>2</sub>

**Assessor and Date:**

N. Saunders

**Publication:**

Calphad, 1, (3), 237-251 (1977)

**Comments:**

Data below used to calculate the Al-Li-Mg and Al-Li-Zr systems.

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase hcp-*A*3**

$$L_{\text{Al,Li:}\square}^{0,\text{hcp-}A3} = -27000.0 + 8.0 \cdot T$$

**Phase bcc-A2**

$$L_{\text{Al,Li:}\square}^{0,\text{bcc}-A2} = -27000.0 + 8.0 \ T$$

$$L_{\text{Al,Li:}\square}^{1,\text{bcc}-A2} = 1.0E-06$$

$$L_{\text{Al,Li:}\square}^{2,\text{bcc}-A2} = 3000.0$$

**Phase fcc-A1**

$$L_{\text{Al,Li:}\square}^{0,\text{fcc}-A1} = -27000.0 + 8.0 \ T$$

$$L_{\text{Al,Li:}\square}^{1,\text{fcc}-A1} = 1.0E-06$$

$$L_{\text{Al,Li:}\square}^{2,\text{fcc}-A1} = 3000.0 + 0.1 \ T$$

**Phase liquid**

$$L_{\text{Al,Li}}^{0,\text{liquid}} = -41500.0 + 20.96 \ T$$

$$L_{\text{Al,Li}}^{1,\text{liquid}} = 10000.0 - 5.8 \ T$$

$$L_{\text{Al,Li}}^{2,\text{liquid}} = 15902.0 - 9.368 \ T$$

$$L_{\text{Al,Li}}^{3,\text{liquid}} = -250.0$$

**Phase AlLi**

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Li}) = \\ -41300.0 + 16.86 \ T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Li}}$$

$$G^\circ(T) - 2.0 \ H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Li:Li}) = 2.0 \ \text{GIISER}_{\text{Li}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:}\square) = 24000.0 + \text{GIISER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Li:}\square) = 50000.0 + \text{GIISER}_{\text{Li}}$$

$$L_{\text{Al,Li:Li}}^{0,\text{AlLi}} = 20000.0$$

$$L_{\text{Al,Li:Li}}^{1,\text{AlLi}} = -26000.0$$

$$L_{\text{Al,Li:}\square}^{0,\text{AlLi}} = 2000.0$$

$$L_{\text{Al:Li,}\square}^{0,\text{AlLi}} = -24000.0 + 10.0 \ T$$

**Phase  $\text{Al}_2\text{Li}_3$** 

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15\text{K}) - 3.0 \ H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 89640.0 + 32.79 \ T + 2.0 \ \text{GHSER}_{\text{Al}} + 3.0 \ \text{GHSER}_{\text{Li}}$$

**Phase  $\text{Al}_4\text{Li}_9$** 

$$G^\circ(T) - 4.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 9.0 \ H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Li}) = \\ - 185250.0 + 67.8 \ T + 4.0 \ \text{GHSER}_{\text{Al}} + 9.0 \ \text{GHSER}_{\text{Li}}$$

**Phase  $\text{Al}_{12}\text{Mg}_{17}$** 

$$G^\circ(T) - 34.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 24.0 \ H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Li:Al:Al}) = \\ - 800000 + 405 \ T + 34.0 \ \text{GHSER}_{\text{Al}} + 24.0 \ \text{GHSER}_{\text{Li}}$$

$$G^\circ(T) - 21.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 34.0 \ H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Li:Li:Al}) = \\ - 750000 + 405 \ T + 24.0 \ \text{GHSER}_{\text{Al}} + 34.0 \ \text{GHSER}_{\text{Li}}$$

**Phase  $\text{Al}_2\text{Zr}$** 

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Li}) = \\ - 24240 + 16.869 \ T + 2.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Li}}$$

**Phase  $\text{Al}_3\text{Zr}$** 

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Li}) = \\ - 24400 + 16.88 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Li}}$$

**Phase  $\text{Al}_3\text{Zr}_2$** 

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 \ H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Li}) = \\ - 46625 + 33.25 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Li}}$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{1,i}$			$T / \text{K}$
Liquid $\rightleftharpoons$ fcc-A1 + AlLi	Eutectic	.256	.155	.462	868.8
Liquid + AlLi $\rightleftharpoons$ $\text{Al}_2\text{Li}_3$	Peritectic	.775	.555	.600	793.6
Liquid + $\text{Al}_2\text{Li}_3$ $\rightleftharpoons$ $\text{Al}_4\text{Li}_9$	Peritectic	.912	.600	.692	607.6
Liquid $\rightleftharpoons$ $\text{Al}_4\text{Li}_9$ + bcc-A2	Eutectic	.989	.692	.999	447.8
Alli $\rightleftharpoons$ Liquid	Congruent	.500	.500	....	978.0

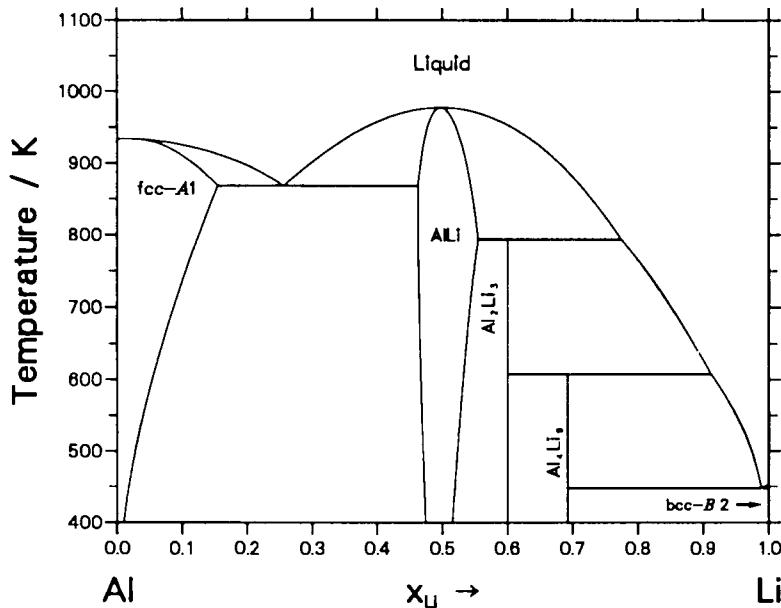


Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol	Symbol Group	Sub-lattices	Comments
Al-Li	(Al)	Cu	<i>cF</i> 4 <i>Fm</i> 3 <i>m</i>		M 4	
	(Li)	W	<i>cI</i> 2 <i>Im</i> 3 <i>m</i>		M 2	
	AlLi	NaTl	<i>cF</i> 16 <i>Fd</i> 3 <i>m</i>		M <sub>1</sub> 8 M <sub>2</sub> 8	
	Al <sub>2</sub> Li <sub>3</sub>	Ga <sub>2</sub> Te <sub>3</sub>	<i>hR</i> 15 <i>R</i> 3 <i>m</i>		Al 6 Li <sub>1</sub> 3 Li <sub>2</sub> 6	
	Al <sub>3</sub> Li	AuCu <sub>3</sub>	<i>cP</i> 4 <i>Pm</i> 3 <i>m</i>		Al 3 Li 1	metast.
	Al <sub>4</sub> Li <sub>9</sub>	Al <sub>4</sub> Li <sub>9</sub>	<i>mC</i> 26 <i>C</i> 2/ <i>m</i>			

# System Al-Mg

Version I

**Solution Phases:**

(stable)	Liquid, fcc-A1, hcp-A3
(metastable)	bcc-A2

**Compounds:**

(stable)	AlMg- $\beta$ , AlMg- $\epsilon$ , Al-Mg- $\zeta$ , Al <sub>12</sub> Mg <sub>17</sub>
(metastable)	AlLi

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Al <sub>12</sub> Mg <sub>17</sub>	:	Sublattice model, Mg <sub>24</sub> (Al,Mg) <sub>10</sub> (Al,Mg) <sub>24</sub>
AlMg- $\beta$	:	Stoichiometric, (Al) <sub>0.615</sub> (Mg) <sub>0.385</sub>
AlMg- $\epsilon$	:	Stoichiometric, (Al) <sub>0.56</sub> (Mg) <sub>0.44</sub>
AlMg- $\zeta$	:	Stoichiometric, (Al) <sub>0.525</sub> (Mg) <sub>0.475</sub>
AlLi	:	Sublattice model (Al,Mg)(Mg, $\square$ )

**Assessor and Date:**

N. Saunders, 1991

**Comments:**

The data below were used for the thermodynamic assessment of the Al-Li-Mg system in COST507 Round I .

**Thermodynamic properties of the solution and compound phases(J.mol<sup>-1</sup>)**

**Phase AlMg- $\beta$**

$$G^\circ(T) - 0.615 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 0.385 \ H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 1000.0 - 3.017 \ T + 0.615 \ \text{GHSER}_{\text{Al}} + 0.385 \ \text{GHSER}_{\text{Mg}}$$

### Phase AlMg- $\epsilon$

$$G^\circ(T) - 14.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 11.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 9275.0 - 104.0 \ T + 14.0 \ \text{GHSER}_{\text{Al}} + 11.0 \ \text{GHSER}_{\text{Mg}}$$

### Phase AlMg- $\zeta$

$$G^\circ(T) - 21.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 19.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 21040.0 - 163.76 \ T + 21.0 \ \text{GHSER}_{\text{Al}} + 19.0 \ \text{GHSER}_{\text{Mg}}$$

### Phase Al<sub>12</sub>Mg<sub>17</sub>

$$G^\circ(T) - 34.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 24.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Al:Al}) = \\ - 36800.0 - 140.0 \ T + 34.0 \ \text{GHSER}_{\text{Al}} + 24.0 \ \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 24.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 34.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg:Al}) = \\ - 123200.0 - 56.26 \ T + 24.0 \ \text{GHSER}_{\text{Al}} + 34.0 \ \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 10.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 48.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Al:Mg}) = \\ 151000.0 + 10.0 \ \text{GHSER}_{\text{Al}} + 48.0 \ \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 58.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg:Mg}) = \\ 290000 + 58.0 \ \text{GHSER}_{\text{Mg}}$$

$$L_{\text{Mg:Al,Mg:Al}}^{0,\text{Al}_{12}\text{Mg}_{17}} = - 17000$$

$$L_{\text{Mg:Al,Mg:Mg}}^{0,\text{Al}_{12}\text{Mg}_{17}} = - 17000$$

### Phase AlLi

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:}\square) = \\ 24000 + \text{GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:}\square) = \\ 50000 + \text{GBCC}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = \\ 2.0 \ \text{GBCC}_{\text{Mg}}$$

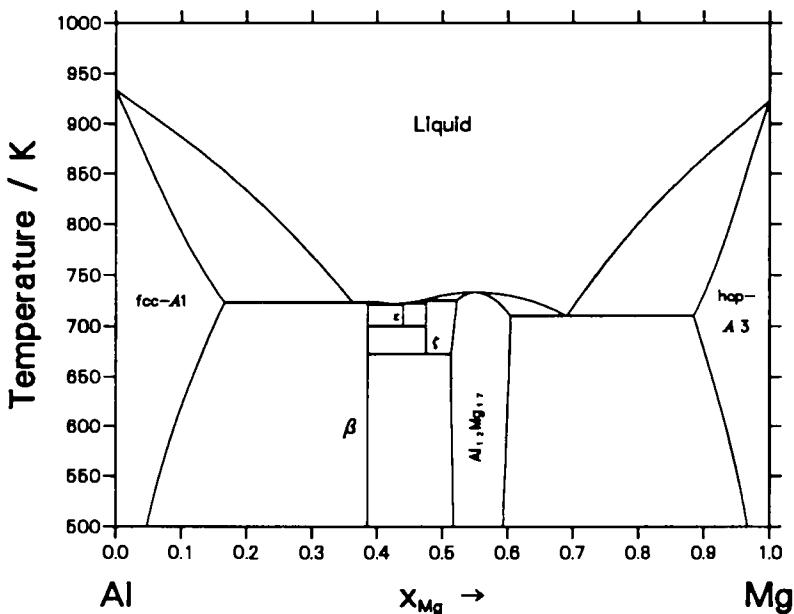
$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al:Mg}) = \\ 2486 - 1.75 \ T + \text{GBCC}_{\text{Al}} + \text{GBCC}_{\text{Mg}}$$

### Phase bcc-A2

$$L_{\text{Al,Mg:}\square}^{0,\text{bcc}-A2} = 4971.0 - 3.5 \ T$$

$$L_{\text{Al,Mg:}\square}^{1,\text{bcc}-A2} = 900.0 + 0.423 \ T$$

$$L_{\text{Al,Mg:}\square}^{2,\text{bcc}-A2} = 950.0$$



#### Phase fcc-A1

$$L_{\text{Al,Mg};\square}^{0,\text{fcc}-A1} = 4971.0 - 3.5 \cdot T$$

$$L_{\text{Al,Mg};\square}^{1,\text{fcc}-A1} = 900.0 + 0.423 \cdot T$$

$$L_{\text{Al,Mg};\square}^{2,\text{fcc}-A1} = 950.0$$

#### Phase hcp-A3

$$L_{\text{Al,Mg};\square}^{0,\text{hcp}-A3} = 1950.0 - 2.0 \cdot T$$

$$L_{\text{Al,Mg};\square}^{1,\text{hcp}-A3} = 1480.0 - 2.08 \cdot T$$

$$L_{\text{Al,Mg};\square}^{2,\text{hcp}-A3} = 3500.0$$

#### Phase liquid

$$L_{\text{Al,Mg}}^{0,\text{liquid}} = -12000.0 + 8.566 \cdot T$$

$$L_{\text{Al,Mg}}^{1,\text{liquid}} = 1894.0 - 3.0 \cdot T$$

$$L_{\text{Al,Mg}}^{2,\text{liquid}} = 2000.0$$

**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Mg}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ fcc-Al + AlMg- $\beta$	Eutectic	.363	.166	.385	723.3
Liquid $\rightleftharpoons$ AlMg- $\beta$ + AlMg- $\epsilon$	Eutectic	.423	.385	.440	721.5
Liquid + AlMg- $\zeta$ $\rightleftharpoons$ + AlMg- $\epsilon$	Peritectic	.436	.475	.440	722.0
Liquid + Al <sub>12</sub> Mg <sub>17</sub> $\rightleftharpoons$ AlMg- $\zeta$	Peritectic	.468	.522	.475	725.0
AlMg- $\epsilon$ $\rightleftharpoons$ AlMg- $\beta$ + AlMg- $\zeta$	Eutectoid	.440	.385	.475	700.0
AlMg- $\zeta$ $\rightleftharpoons$ AlMg- $\beta$ + Al <sub>12</sub> Mg <sub>17</sub>	Eutectoid	.475	.385	.513	673.0
Liquid $\rightleftharpoons$ Al <sub>12</sub> Mg <sub>17</sub> + hcp-A3	Eutectic	.690	.604	.884	710.0
AlMg- $\beta$ $\rightleftharpoons$ Liquid	Congruent	.385	.385	....	724.1
Al <sub>12</sub> Mg <sub>17</sub> $\rightleftharpoons$ Liquid	Congruent	.556	.556	....	733.3

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Mg	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M 4	
	(Mg)	Mg	<i>hP2</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>	M 2	
	Al <sub>12</sub> Mg <sub>17</sub>	$\alpha$ -Mn cbcc-A12	<i>cI58</i> <i>I43m</i>	Al 24 Mg <sub>1</sub> 2 Mg <sub>2</sub> 8 Mg <sub>3</sub> 24	$\gamma$ in Mas1
	Al <sub>3</sub> Mg <sub>2</sub>	Cd <sub>2</sub> Na	<i>cF112</i> <i>Fd</i> $\bar{3}m$		<i>cF1832</i> in [91Vil] designated as AlMg- $\beta$
	Al <sub>30</sub> Mg <sub>23</sub>	Co <sub>5</sub> Cr <sub>2</sub> Mo <sub>3</sub> (Mn <sub>44</sub> Si <sub>9</sub> )	<i>hR53</i> <i>R</i> $\bar{3}$	Al <sub>1</sub> 18 Al <sub>2</sub> 18 Al <sub>3</sub> 18 Al <sub>4</sub> 18 Al <sub>5</sub> 18 Mg <sub>1</sub> 3 Mg <sub>2</sub> 6 Mg <sub>3</sub> 6 Mg <sub>4</sub> 18 Mg <sub>5</sub> 18 Mg <sub>6</sub> 18	$\epsilon$
	Al <sub>49</sub> Mg <sub>32</sub>	Al <sub>6</sub> Mg <sub>11</sub> Zn <sub>11</sub>	<i>cI162</i> <i>I</i> $m\bar{3}$		$\zeta$

# System Al-Mg

Version II

**Solution Phases:**

(stable)	Liquid, fcc- <i>A1</i> , hcp- <i>A3</i>
(metastable)	bcc- <i>A2</i> ,hcp-Zn

**Compounds:**

(stable)	AlMg- $\beta$ , AlMg- $\epsilon$ , AlMg- $\gamma$
(metastable)	Laves- <i>C14</i> , Laves- <i>C15</i> , Laves- <i>C36</i> , Mg <sub>2</sub> Zn <sub>11</sub> , Mg <sub>2</sub> Zn <sub>3</sub> , MgZn, $\varphi$ -phase, $\tau$ -phase

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A2</i>	:	Substitutional, Redlich-Kister
fcc- <i>A1</i>	:	Substitutional, Redlich-Kister
hcp- <i>A3</i>	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister
AlMg- $\beta$	:	Stoichiometric, (Al) <sub>0.615</sub> (Mg) <sub>0.385</sub>
AlMg- $\epsilon$	:	Stoichiometric, (Al) <sub>0.56</sub> (Mg) <sub>0.44</sub>
MgZn	:	Stoichiometric, (Al) <sub>13</sub> (Mg) <sub>12</sub>
Mg <sub>2</sub> Zn <sub>3</sub>	:	Stoichiometric, (Al) <sub>3</sub> (Mg) <sub>2</sub>
$\varphi$ -phase	:	Stoichiometric, (Al) <sub>5</sub> (Mg) <sub>6</sub>
Mg <sub>2</sub> Zn <sub>11</sub>	:	Stoichiometric, (Al) <sub>11</sub> (Mg) <sub>2</sub>
AlMg- $\gamma$	:	Sublattice model, Mg <sub>5</sub> (Al,Mg) <sub>12</sub> (Al,Mg) <sub>12</sub>
Laves- <i>C14</i>	:	Sublattice model (Al,Mg) <sub>2</sub> (Al,Mg)
Laves- <i>C15</i>	:	Sublattice model (Al,Mg) <sub>2</sub> (Al,Mg)
Laves- <i>C36</i>	:	Sublattice model (Al,Mg) <sub>2</sub> (Al,Mg)
$\tau$ -phase	:	Sublattice model (Mg) <sub>26</sub> (Al,Mg) <sub>6</sub> (Al,Mg) <sub>48</sub> (Al)

**Assessor and Date:**

H.-L. Lukas

**Comments:**

The data for the Laves-*C15* phase were evaluated by T. Bühler for the thermodynamic assessment of the Al-Cu-Mg system

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)****Phase liquid**

$$L_{\text{Al,Mg}}^{0,\text{liquid}} = -12000 + 8.566 \cdot T$$

$$L_{\text{Al,Mg}}^{1,\text{liquid}} = 1894 - 3 \cdot T$$

$$L_{\text{Al,Mg}}^{2,\text{liquid}} = 2000$$

**Phase AlMg- $\beta$** 

$$\begin{aligned} G^\circ(T) - 140.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 89.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 246175 - 675.55 \cdot T + 140.0 \cdot \text{GHSER}_{\text{Al}} + 89.0 \cdot \text{GHSER}_{\text{Mg}} \end{aligned}$$

**Phase AlMg- $\epsilon$** 

$$\begin{aligned} G^\circ(T) - 30.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 23.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 52565.4 - 173.1775 \cdot T + 30.0 \cdot \text{GHSER}_{\text{Al}} + 23.0 \cdot \text{GHSER}_{\text{Mg}} \end{aligned}$$

**Phase AlMg- $\gamma$** 

$$\begin{aligned} G^\circ(T) - 24.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 5.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \text{G(Mg:Al:Al)} = \\ 97875 - 101.5 \cdot T + 24.0 \cdot \text{GHSER}_{\text{Al}} + 5.0 \cdot \text{GHSER}_{\text{Mg}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 12.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 17.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \text{G(Mg:Mg:Al)} = \\ - 52780 - 50.75 \cdot T + 12.0 \cdot \text{GHSER}_{\text{Al}} + 17.0 \cdot \text{GHSER}_{\text{Mg}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 12.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 17.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \text{G(Mg:Al:Mg)} = \\ 284124.6 - 138.069 \cdot T + 12.0 \cdot \text{GHSER}_{\text{Al}} + 17.0 \cdot \text{GHSER}_{\text{Mg}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 29.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \text{G(Mg:Mg:Mg)} = \\ 133469.6 - 87.319 \cdot T + 29.0 \cdot \text{GHSER}_{\text{Mg}} \end{aligned}$$

$$L_{\text{Mg:Al:Al,Mg}}^{0,\text{Al}_{12}\text{Mg}_{17}} = 113100 - 14.5 \cdot T$$

$$L_{\text{Mg:Al:Al,Mg}}^{0,\text{Al}_{12}\text{Mg}_{17}} = 113100 - 14.5 \cdot T$$

**Phase fcc-A1**

$$L_{\text{Al,Mg:}\square}^{0,\text{fcc}-A1} = 4971 - 3.5 \cdot T$$

$$L_{\text{Al,Mg:}\square}^{1,\text{fcc}-A1} = 900 + 0.423 \cdot T$$

$$L_{\text{Al,Mg:}\square}^{2,\text{fcc}-A1} = 950$$

**Phase hcp-A3**

$$L_{\text{Al,Mg};\square}^{0,\text{hcp}-A3} = 1950 - 2 \cdot T$$

$$L_{\text{Al,Mg};\square}^{1,\text{hcp}-A3} = 1480 - 2.08 \cdot T$$

$$L_{\text{Al,Mg};\square}^{2,\text{hcp}-A3} = 3500$$

**Phase hcp-Zn**

$$L_{\text{Al,Mg};\square}^{0,\text{hcp}-Zn} = 1950 - 2 \cdot T$$

$$L_{\text{Al,Mg};\square}^{1,\text{hcp}-Zn} = 1480 - 2.08 \cdot T$$

$$L_{\text{Al,Mg};\square}^{2,\text{hcp}-Zn} = 3500$$

**Phase Laves-C14**

$$G^\circ(T) - 3.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = 15000 + 3.0 \cdot \text{GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Al}) = 17329 - 16.8 \cdot T + \text{GHSER}_{\text{Al}} + 2.0 \cdot \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al:Mg}) = 12671.1 + 16.8 \cdot T + 2.0 \cdot \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 3.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000 + 3.0 \cdot \text{GHSER}_{\text{Mg}}$$

$$L_{\text{Al,Mg};\text{Al}}^{0,\text{Laves}-C14} = 15000$$

$$L_{\text{Al:Al,Mg}}^{0,\text{Laves}-C14} = 8000$$

$$L_{\text{Mg:Al,Mg}}^{0,\text{Laves}-C14} = 8000$$

$$L_{\text{Al,Mg};\text{Mg}}^{0,\text{Laves}-C14} = 15000$$

**Phase Laves-C15**

$$G^\circ(T) - 3.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = 15000 + 3.0 \cdot \text{GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Al}) = 104970.96 - 16.46448 \cdot T + \text{GHSER}_{\text{Al}} + 2.0 \cdot \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al:Mg}) = 30000 + 4.0 \cdot T + 2.0 \cdot \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 3.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000 + 3.0 \cdot \text{GHSER}_{\text{Mg}}$$

$$L_{\text{Al,Mg:Al}}^{0,\text{Laves-C15}} = 15000$$

$$L_{\text{Al:Al,Mg}}^{0,\text{Laves-C15}} = 8000$$

$$L_{\text{Mg:Al,Mg}}^{0,\text{Laves-C15}} = 8000$$

$$L_{\text{Al,Mg:Mg}}^{0,\text{Laves-C15}} = 15000$$

### Phase Laves-C36

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Al:Al}) =$$

$$15000 + 3.0 \ \text{GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 \ H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Al}) =$$

$$84970.96 - 16.46448 \ T + \text{GHSER}_{\text{Al}} + 2 \ \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Al:Mg}) =$$

$$21734 + 11.02 \ T + 2.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 3.0 \ H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) = G(\text{Mg:Mg}) =$$

$$15000 + 3.0 \ \text{GHSER}_{\text{Mg}}$$

$$L_{\text{Al,Mg:Al}}^{0,\text{Laves-C36}} = 15000$$

$$L_{\text{Al:Al,Mg}}^{0,\text{Laves-C36}} = 8000$$

$$L_{\text{Mg:Al,Mg}}^{0,\text{Laves-C36}} = 8000$$

$$L_{\text{Al,Mg:Mg}}^{0,\text{Laves-C36}} = 15000$$

### Phase Mg<sub>2</sub>Zn<sub>11</sub>

$$G^\circ(T) - 11.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 \ H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) =$$

$$+ 130000 - 26.0 \ T + 11.0 \ \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Mg}}$$

### Phase Mg<sub>2</sub>Zn<sub>3</sub>

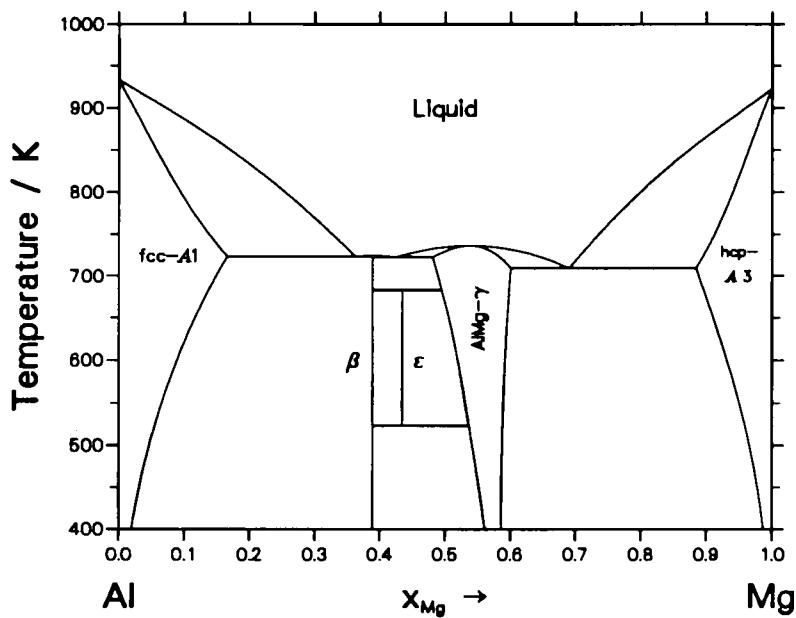
$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 \ H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) =$$

$$1000 - 0.2 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Mg}}$$

### Phase MgZn

$$G^\circ(T) - 13.0 \ H_{\text{Al}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 12.0 \ H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) =$$

$$- 10000 + 2.5 \ T + 13.0 \ \text{GHSER}_{\text{Al}} + 12.0 \ \text{GHSER}_{\text{Mg}}$$



#### Phase \$\varphi\$-phase

$$G^\circ(T) = 5.0 \cdot H_{Al}^{\circ, fcc-Al}(298.15 \text{ K}) - 6.0 \cdot H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = \\ - 15400 - 16.5 \cdot T + 5.0 \cdot GHSER_{Al} + 6.0 \cdot GHSER_{Mg}$$

#### Phase \$\tau\$-phase

$$G^\circ(T) = 55.0 \cdot H_{Al}^{\circ, fcc-Al}(298.15 \text{ K}) - 26.0 \cdot H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = \\ G(Mg:Al:Al:Al) = - 105.3 \cdot T + 55.0 \cdot GHSER_{Al} + 26.0 \cdot GHSER_{Mg}$$

$$G^\circ(T) = 49.0 \cdot H_{Al}^{\circ, fcc-Al}(298.15 \text{ K}) - 32.0 \cdot H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = \\ G(Mg:Mg:Al:Al) = - 81000 - 186.3 \cdot T + 49.0 \cdot GHSER_{Al} + 32.0 \cdot GHSER_{Mg}$$

$$G^\circ(T) = 7.0 \cdot H_{Al}^{\circ, fcc-Al}(298.15 \text{ K}) - 74.0 \cdot H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = \\ G(Mg:Al:Mg:Al) = 1053000 + 405 \cdot T + 7.0 \cdot GHSER_{Al} + 74.0 \cdot GHSER_{Mg}$$

$$G^\circ(T) = H_{Al}^{\circ, fcc-Al}(298.15 \text{ K}) - 80.0 \cdot H_{Mg}^{\circ, hcp-A3}(298.15 \text{ K}) = \\ G(Mg:Mg:Mg:Al) = 405000 + 243 \cdot T + GHSER_{Al} + 80.0 \cdot GHSER_{Mg}$$

$$L_{Mg:Al:Al,Mg:Al}^{0,\tau\text{-phase}} = - 202500 - 40.5 \cdot T$$

$$L_{Mg:Mg:Al,Mg:Al}^{0,\tau\text{-phase}} = - 202500 - 40.5 \cdot T$$

**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Mg}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ fcc-Al + AlMg- $\beta$	Eutectic	.363	.166	.389	723.6
Liquid $\rightleftharpoons$ AlMg- $\beta$ + AlMg- $\gamma$	Eutectic	.424	.389	.480	722.7
AlMg- $\beta$ + AlMg- $\gamma$ $\rightleftharpoons$ AlMg- $\epsilon$	Peritectoid	.389	.494	.434	682.9
AlMg- $\epsilon$ $\rightleftharpoons$ AlMg- $\beta$ + AlMg- $\gamma$	Eutectoid	.434	.389	.536	523.2.0
Liquid $\rightleftharpoons$ AlMg- $\gamma$ + hcp-A3	Eutectic	.690	.601	.884	709.4
AlMg- $\beta$ $\rightleftharpoons$ Liquid	Congruent	.385	.385	....	724.7
Al <sub>12</sub> Mg <sub>17</sub> $\rightleftharpoons$ Liquid	Congruent	.523	.523	....	736.3

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Mg	(Al)	Cu	<i>cF</i> 4 <i>Fm</i> $\bar{3}m$	M 4	
	(Mg)	Mg	<i>hP</i> 2 <i>P</i> 6 <sub>3</sub> / <i>mmc</i>	M 2	
	AlMg- $\gamma$	$\alpha$ -Mn cbcc-Al12	<i>cI</i> 58 <i>I</i> $\bar{4}3m$	Al 24 Mg <sub>1</sub> 2 Mg <sub>2</sub> 8 Mg <sub>3</sub> 24	designated as Al <sub>12</sub> Mg <sub>17</sub>
	Al <sub>3</sub> Mg <sub>2</sub>	Cd <sub>2</sub> Na	<i>cF</i> 112 <i>F</i> d3 <i>m</i>		<i>cF</i> 1832 in [91Vii] designated as AlMg- $\beta$
	AlMg- $\epsilon$	Co <sub>5</sub> Cr <sub>2</sub> Mo <sub>3</sub>	<i>hR</i> 53	Al <sub>1</sub> 18	<i>R</i> phase in [Mas1]
		(Mn <sub>44</sub> Si <sub>9</sub> )	<i>R</i> $\bar{3}$	Al <sub>2</sub> 18 Al <sub>3</sub> 18 Al <sub>4</sub> 18 Al <sub>5</sub> 18 Mg <sub>1</sub> 3 Mg <sub>2</sub> 6 Mg <sub>3</sub> 6 Mg <sub>4</sub> 18 Mg <sub>5</sub> 18 Mg <sub>6</sub> 18	

# System Al-Mn

## Solution Phases:

Liquid, bcc-*A*2, cbcc-*A*12,  
cub-*A*13, fcc-*A*1, hcp-*A*3

## Stoichiometric Compounds:

(stable)	Al <sub>11</sub> Mn <sub>4</sub> , Al <sub>6</sub> Mn, Al <sub>4</sub> Mn, Al <sub>8</sub> Mn <sub>5</sub> -D8 <sub>10</sub>
(metastable)	Al <sub>2</sub> Fe, Al <sub>5</sub> Fe <sub>2</sub> , Al <sub>13</sub> Fe <sub>4</sub>

## Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
cbcc- <i>A</i> 12	:	Substitutional, Redlich-Kister
cub- <i>A</i> 13	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Al <sub>8</sub> Mn <sub>5</sub> -D8 <sub>10</sub>	:	Sublattice model, (Al) <sub>12</sub> (Mn) <sub>4</sub> (Al,Mn) <sub>10</sub>
Al <sub>2</sub> Fe	:	Stoichiometric, (Al) <sub>2</sub> (Fe) <sub>1</sub>
Al <sub>5</sub> Fe <sub>2</sub>	:	Stoichiometric, (Al) <sub>5</sub> (Fe) <sub>2</sub>
Al <sub>13</sub> Fe <sub>4</sub>	:	Sublattice model, (Al) <sub>.6275</sub> (Fe) <sub>.235</sub> (Al,□) <sub>.1375</sub>

## Assessor and Date:

Å. Jansson

## Publication:

Trita-Mac-0462, May 1991, Materials Research Center,  
The Royal Institute of Technology, Stockholm

## Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)

### Phase Al<sub>11</sub>Mn<sub>4</sub>

$$G^\circ(T) - 11.0 \ H_{\text{Al}}^{\circ,\text{fcc-}A1}(298.15 \text{ K}) - 4.0 \ H_{\text{Mn}}^{\circ,\text{cbcc-}A12,\text{para}}(298.15 \text{ K}) = \\ - 354690.0 + 103.031 \ T + 11.0 \ \text{GHSER}_{\text{Al}} + 4.0 \ \text{GHSER}_{\text{Mn}}$$

### Phase Al<sub>12</sub>Mn

$$G^\circ(T) - 12.0 \ H_{\text{Al}}^{\circ,\text{fcc-}A1}(298.15 \text{ K}) - H_{\text{Mn}}^{\circ,\text{cbcc-}A12,\text{para}}(298.15 \text{ K}) = \\ - 125730.0 + 54.98103 \ T + 12.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mn}}$$

**Phase Al<sub>4</sub>Mn**

$$G^\circ(T) - 4.0 \quad H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) = \\ - 100005.0 + 30.0 \quad T + 4.0 \quad \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mn}}$$

**Phase Al<sub>6</sub>Mn**

$$G^\circ(T) - 6.0 \quad H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) = \\ - 124564.3 + 53.6593 \quad T + 6.0 \quad \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mn}}$$

**Phase Al<sub>8</sub>Mn<sub>5</sub>-D8<sub>10</sub>**

$$G^\circ(T) - 22.0 \quad H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 4.0 \quad H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) = G(\text{Al:Mn:Al}) = \\ - 308671 + 56.6488 \quad T + 22.0 \quad \text{GHSER}_{\text{Al}} + 4.0 \quad \text{GHSER}_{\text{Mn}} \\ G^\circ(T) - 12.0 \quad H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 14.0 \quad H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) = \\ G(\text{Al:Mn:Mn}) = - 596867 + 94.612 \quad T + 12.0 \quad \text{GHSER}_{\text{Al}} + 14.0 \quad \text{GHSER}_{\text{Mn}}$$

$$L_{\text{Al:Mn:Al,Mn}}^{0,\text{Al}_8\text{Mn}_5-\text{D}8_{10}} = - 546234 + 387.348 \quad T$$

**Phase Al<sub>2</sub>Fe**

$$G^\circ(T) - 2.0 \quad H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) = \\ - 14065.0 \quad T + 2.0 \quad \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mn}}$$

**Phase Al<sub>5</sub>Fe<sub>2</sub>**

$$G^\circ(T) - 5.0 \quad H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 \quad H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) = \\ 5.0 \quad \text{GHSER}_{\text{Al}} + 2.0 \quad \text{GHSER}_{\text{Mn}}$$

**Phase Al<sub>13</sub>Fe<sub>4</sub>**

$$G^\circ(T) - 0.765 \quad H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.235 \quad H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) = \\ - 20000.0 + 10.0 \quad T + 0.765 \quad \text{GHSER}_{\text{Al}} + 0.235 \quad \text{GHSER}_{\text{Mn}} \\ G^\circ(T) - 0.6275 \quad H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.235 \quad H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) = \\ - 17000.0 + 10.0 \quad T + 0.6275 \quad \text{GHSER}_{\text{Al}} + 0.235 \quad \text{GHSER}_{\text{Mn}}$$

**Phase bcc-A2**

$$L_{\text{Al,Mn:}\square}^{0,\text{bcc}-A2} = - 120077 + 52.851 \quad T \quad L_{\text{Al,Mn:}\square}^{1,\text{bcc}-A2} = - 40652 + 29.2764 \quad T$$

**Phase cbcc-A12**

$$L_{\text{Al,Mn:}\square}^{0,\text{cbcc}-A12} = - 101410 + 43.0 \quad T$$

**Phase cub-A13**

$$L_{\text{Al,Mn:}\square}^{0,\text{cub}-A13} = - 119022 + 52.507 \quad T \quad L_{\text{Al,Mn:}\square}^{1,\text{cub}-A13} = - 1763$$

**Phase fcc-A1**

$$L_{\text{Al,Mn}:□}^{0,\text{fcc}-\text{A1}} = -69300 + 25.0 \ T \quad L_{\text{Al,Mn}:□}^{1,\text{fcc}-\text{A1}} = 8800$$

**Phase hcp-A3**

$$L_{\text{Al,Mn}:□}^{0,\text{hcp}-\text{A3}} = -108066 + 43.83 \ T \quad L_{\text{Al,Mn}:□}^{1,\text{hcp}-\text{A3}} = -54519.8 + 40 \ T$$

**Phase liquid**

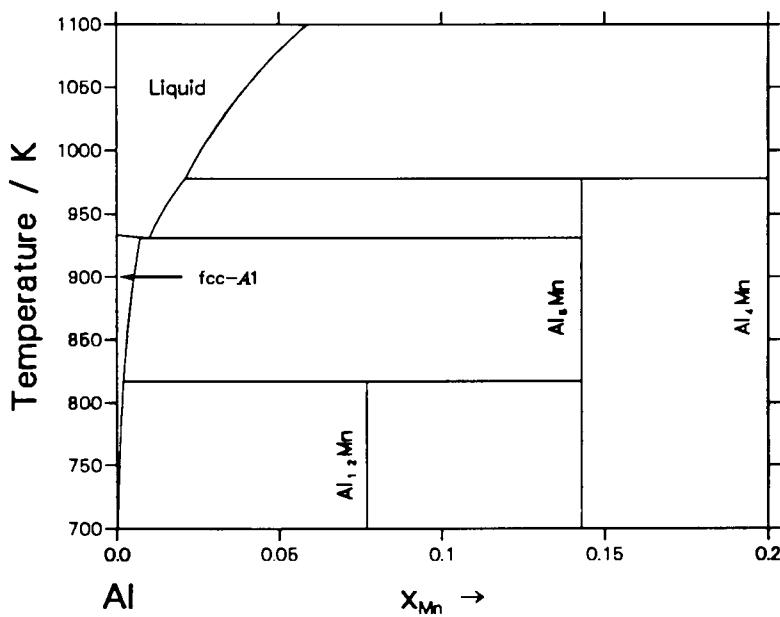
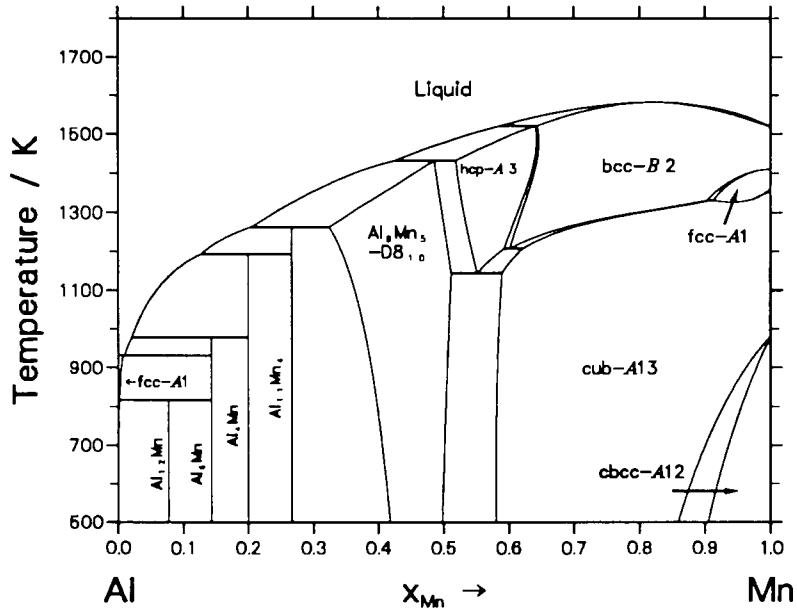
$$L_{\text{Al,Mn}}^{0,\text{liquid}} = -66174 + 27.0988 \ T$$

$$L_{\text{Al,Mn}}^{1,\text{liquid}} = -7509 + 5.4836 \ T$$

$$L_{\text{Al,Mn}}^{2,\text{liquid}} = -2639$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Mn}}$			$T / \text{K}$
Liquid + $\text{Al}_4\text{Mn} \rightleftharpoons \text{Al}_6\text{Mn}$	Peritectic	.021	.200	.143	978.0
Liquid $\rightleftharpoons$ fcc-A1 + $\text{Al}_6\text{Mn}$	Eutectic	.010	.007	.143	931.1
fcc-A1 + $\text{Al}_6\text{Mn} \rightleftharpoons \text{Al}_{12}\text{Mn}$	Peritectoid	.002	.143	.077	817.0
Liquid + $\text{Al}_{11}\text{Mn}_4 \rightleftharpoons \text{Al}_4\text{Mn}$	Peritectic	.127	.266	.200	1193.1
Liquid + $\text{Al}_8\text{Mn}_5\text{-D}8_{10} \rightleftharpoons \text{Al}_{11}\text{Mn}_4$	Peritectic	.205	.324	.266	1262.4
Liquid + hcp-A3 $\rightleftharpoons \text{Al}_8\text{Mn}_5\text{-D}8_{10}$	Peritectic	.425	.519	.486	1433.3
hcp-A3 $\rightleftharpoons \text{Al}_8\text{Mn}_5\text{-D}8_{10} + \text{cub-A}13$	Eutectoid	.551	.511	.590	1143.7
bcc-A2 $\rightleftharpoons$ hcp-A3 + cub-A13	Eutectoid	.601	.592	.621	1207.0
fcc-A1 + bcc-A2 $\rightleftharpoons$ cub-A13	Peritectoid	.913	.903	.910	1330.9
Liquid + bcc-A2 $\rightleftharpoons$ hcp-A3	Peritectic	.588	.644	.641	1522.3
bcc-A2 $\rightleftharpoons$ Liquid	Congruent	.816	.816	....	1582.0



**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
Al-Mn	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>	M <sub>1</sub> 4	
	$\alpha$ -Mn	$\alpha$ -Mn	<i>c58</i> <i>I</i> $\bar{4}3$ <i>m</i>		cbcc- <i>A1</i>
	$\beta$ -Mn	$\beta$ -Mn	<i>cP20</i> <i>P</i> $\bar{4}1$ <i>32</i>		cub- <i>A13</i>
	$\gamma$ -Mn	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>		fcc- <i>A1</i>
	$\delta$ -Mn	W	<i>cI2</i> <i>I</i> $\bar{m}\bar{3}$ <i>m</i>		bcc- <i>A2</i>
	AlMn	Al <sub>1</sub> Cu-L <sub>10</sub>	<i>tP2</i> <i>P</i> <sub>4</sub> / <i>mmm</i>	M <sub>1</sub> 1 M <sub>2</sub> 1	metast.
	$\lambda$	Al <sub>4</sub> Mn	<i>oP60</i> <i>P</i> <sub>6</sub> <i>n</i>		reported as Al <sub>4</sub> Mn
	Al <sub>6</sub> Mn	Al <sub>6</sub> Mn	<i>oC28</i> <i>C</i> <sub>mc</sub> <i>m</i>	Al <sub>1</sub> 8 Al <sub>2</sub> 8 Al <sub>3</sub> 8 Mn 4	
	Al <sub>10</sub> Mn <sub>3</sub>	Al <sub>5</sub> Mn <sub>2</sub>	<i>hP28</i> <i>P</i> <sub>6</sub> <sub>3</sub> / <i>mmc</i>	Al <sub>1</sub> 2 Al <sub>2</sub> 6 Al <sub>3</sub> 12 Mn 6	
	Al <sub>11</sub> Mn <sub>4</sub> -L	Al <sub>11</sub> Mn <sub>4</sub>	<i>aP30</i> <i>P</i> <sub>1</sub>		transformation not taken into account reported as <i>aP15</i> in [91Vil]
	Al <sub>11</sub> Mn <sub>4</sub> -H	.....	<i>oP160</i> <i>P</i> <sub>nma</sub>		not in [90Mas] metast.
	Al <sub>12</sub> Mn	Al <sub>12</sub> W	<i>cI26</i> <i>I</i> $\bar{m}\bar{3}$		not quoted in [90Mas] metast.
	Al <sub>8</sub> Mn <sub>5</sub>	Al <sub>8</sub> Cr <sub>5</sub>	<i>hR26</i> <i>R</i> <sub>3</sub> <i>m</i>		Al <sub>8</sub> Mn <sub>5</sub> -D <sub>0</sub> <sub>8</sub>

# System Al-Mo

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, fcc- <i>A</i> 1
(metastable)	bcc- <i>B</i> 2, hcp- <i>A</i> 3

**Compounds:**

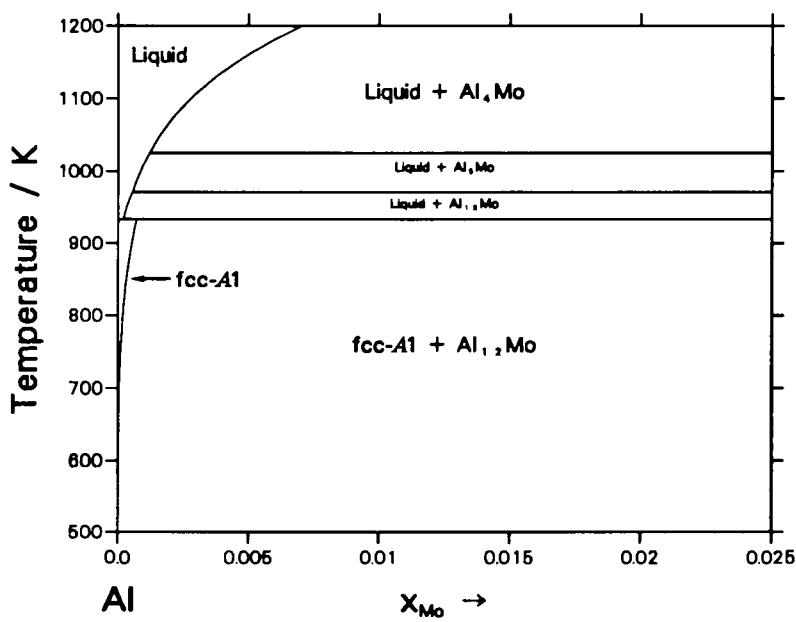
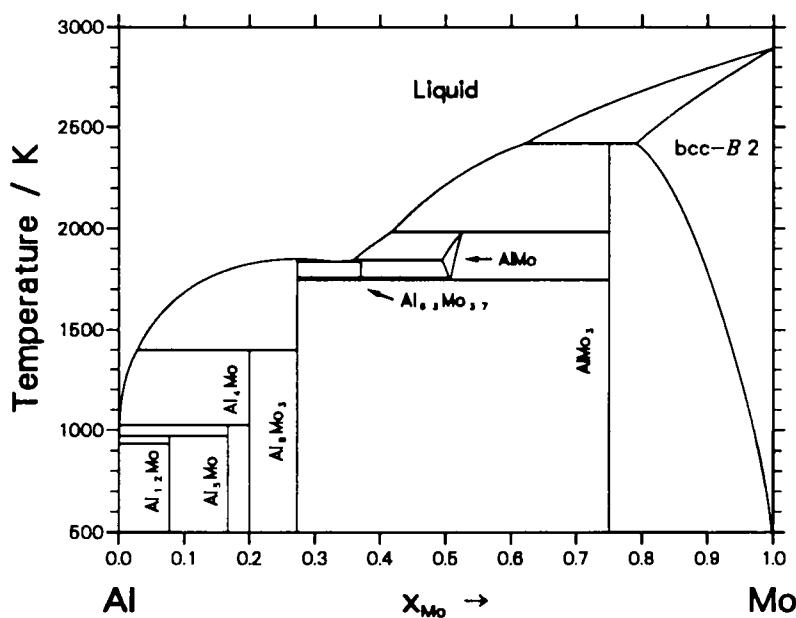
(stable)	Al <sub>12</sub> Mo, Al <sub>4</sub> Mo, Al <sub>5</sub> Mo, Al <sub>63</sub> Mo <sub>37</sub> , Al <sub>8</sub> Mo <sub>3</sub> , AlMo, cub- <i>A</i> 15
(metastable)	AlM- <i>D</i> 0 <sub>19</sub> , AlTi- <i>L</i> 1 <sub>0</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Al <sub>12</sub> Mo	:	Stoichiometric, (Al) <sub>12</sub> (Mo)
Al <sub>5</sub> Mo	:	Stoichiometric, (Al) <sub>5</sub> (Mo)
Al <sub>4</sub> Mo	:	Stoichiometric, (Al) <sub>4</sub> (Mo)
Al <sub>63</sub> Mo <sub>37</sub>	:	Stoichiometric, (Al) <sub>63</sub> (Mo) <sub>37</sub>
Al <sub>8</sub> Mo <sub>3</sub>	:	Stoichiometric, (Al) <sub>8</sub> (Mo) <sub>3</sub>
cub- <i>A</i> 15	:	Stoichiometric, (Al)(Mo) <sub>3</sub>
AlMo	:	Sublattice model, (Al,Mo)(Al,Mo)
bcc- <i>B</i> 2	:	Sublattice model, (Al,Mo) <sub>0.5</sub> (Al,Mo) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc- <i>B</i> 2 takes into account the ordering reaction bcc- <i>A</i> 2 ⇌ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Al,Mo) <sub>3</sub> (Al,Mo)(□) <sub>0.5</sub>
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Al,Mo)(Al,Mo)

**Assessor and Date:**

N. Saunders (1996)



**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)****Phase Al<sub>12</sub>Mo**

$$G^\circ(T) - 12.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 139100 + 26.975 \ T + 12.0 \ \text{GHSER}_{\text{Al}} + \text{GIISER}_{\text{Mo}}$$

**Phase Al<sub>4</sub>Mo**

$$G^\circ(T) - 4.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 137570 + 29.69 \ T + 4.0 \ \text{GIISER}_{\text{Al}} + \text{GIISER}_{\text{Mo}}$$

**Phase Al<sub>5</sub>Mo**

$$G^\circ(T) - 5.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 139104 + 30.156 \ T + 5.0 \ \text{GHSER}_{\text{Al}} + \text{GIISER}_{\text{Mo}}$$

**Phase Al<sub>63</sub>Mo<sub>37</sub>**

$$G^\circ(T) - 63.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 37.0 \ H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 2268100 + 167.2 \ T + 63.0 \ \text{GHSER}_{\text{Al}} + 37.0 \ \text{GIISER}_{\text{Mo}}$$

**Phase Al<sub>8</sub>Mo<sub>3</sub>**

$$G^\circ(T) - 8.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 \ H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 412500 + 105.05 \ T + 8.0 \ \text{GHSER}_{\text{Al}} + 3.0 \ \text{GIISER}_{\text{Mo}}$$

**Phase cub-A15**

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 \ H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 89000 + 20 \ T - 0.003 \ T^2 + \text{GHSER}_{\text{Al}} + 3.0 \ \text{GIISER}_{\text{Mo}}$$

**Phase AlMo**

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = \\ 2.0 \ \text{GBCC}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Mo}) = \\ - 36850 + T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mo}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Al}) = \\ - 36850 + T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Mo}}$$

$$G^\circ(T) - 2.0 \ H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Mo}) = \\ 2.0 + \text{GIISER}_{\text{Mo}}$$

$$L_{\text{Al},\text{Mo}: \text{Al}}^{0,\text{AlMo}} = L_{\text{Al}: \text{Al}, \text{Mo}}^{0,\text{AlMo}} = -5000$$

$$L_{\text{Mo}: \text{Al}, \text{Mo}}^{0,\text{AlMo}} = L_{\text{Al}, \text{Mo}: \text{Mo}}^{0,\text{AlMo}} = 25000$$

$$L_{\text{Mo}: \text{Al}, \text{Mo}}^{1,\text{AlMo}} = L_{\text{Al}, \text{Mo}: \text{Mo}}^{1,\text{AlMo}} = -10000$$

### Phase $\text{AlM}-D0_{19}$

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = \\ 4.0 \text{ GHCP}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Al}) = \\ -64000 + 15.32 T + \text{GHCP}_{\text{Al}} + 3.0 \text{ GHCP}_{\text{Mo}}$$

$$G^\circ(T) - 3.0 \text{ GHCP}_{\text{Al}} - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Mo}) = \\ -64000 + 15.32 T + 3.0 \text{ GHCP}_{\text{Al}} + \text{GHCP}_{\text{Mo}}$$

$$G^\circ(T) - 4.0 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Mo}) = \\ 4.0 \text{ GHSER}_{\text{Mo}}$$

### Phase liquid

$$L_{\text{Al}, \text{Mo}}^{0,\text{liquid}} = -100000 + 35 T$$

$$L_{\text{Al}, \text{Mo}}^{1,\text{liquid}} = -15000 + 6.3 T$$

### Phase fcc-A1

$$L_{\text{Al}, \text{Mo}: \square}^{0,\text{fcc}-A1} = -92220 + 20 T$$

### Phase bcc-A2

$$L_{\text{Al}, \text{Mo}: \square}^{0,\text{bcc}-A2} = -75000 + 25 T$$

### Phase bcc-B2

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}: \square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Al}: \square) = \\ -7050 + T$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Mo}: \square) = \\ -7050 + T$$

$$G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Mo}: \square) = 0.0 \\ L_{\text{Al}: \text{Al}, \text{Mo}: \square}^{0,\text{bcc}-B2} = 7050 - T$$

$$L_{\text{Mo}: \text{Al}, \text{Mo}: \square}^{0,\text{bcc}-B2} = 7050 - T$$

$$L_{\text{Al}, \text{Mo}: \text{Al}: \square}^{0,\text{bcc}-B2} = 7050 - T$$

$$L_{\text{Al}, \text{Mo}: \text{Al}: \square}^{0,\text{bcc}-B2} = 7050 - T$$

**Phase bcc-B2**

$$G_{\text{Al:Mo:}\square}^* = -7050 + T$$

$$G^\circ(T) - \underset{\text{Al}}{H^{\circ,\text{fcc}-A1}}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 \underset{\text{Al}}{H^{\circ,\text{fcc}-A1}}(298.15 \text{ K}) - 0.5 \underset{\text{Mo}}{H^{\circ,\text{bcc}-A2}}(298.15 \text{ K}) = G(\text{Al:Mo:}\square) = 2.0 \quad G_{\text{Al:Mo:}\square}^*$$

$$G^\circ(T) - 0.5 \underset{\text{Cu}}{H^{\circ,\text{fcc}-A1}}(298.15 \text{ K}) - 0.5 \underset{\text{Mo}}{H^{\circ,\text{bcc}-A2}}(298.15 \text{ K}) = G(\text{Mo:Al:}\square) = 2.0 \quad G_{\text{Al:Mo:}\square}^*$$

$$G^\circ(T) - \underset{\text{Mo}}{H^{\circ,\text{bcc}-A2}}(298.15 \text{ K}) = G(\text{Mo:Mo:}\square) = 0.0$$

**Phase bcc-A2**

$$L_{\text{Al,Mo:}\square}^{0,\text{bcc}-A2} = -75000 + 25 \quad T$$

**Phase hcp-A3**

$$L_{\text{Al,Mo:}\square}^{0,\text{hcp}-A3} = -85570 + 25 \quad T$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Mo}}$			$T / \text{K}$
$\text{AlMo} \rightleftharpoons \text{Al}_8\text{Mo}_3 + \text{cub}-A15$	Eutectoid	.507	.273	.750	1745.6
$\text{Al}_{63}\text{Mo}_{37} \rightleftharpoons \text{Al}_8\text{Mo}_3 + \text{AlMo}$	Eutectoid	.370	.273	.505	1759.6
$\text{Liquid} \rightleftharpoons \text{Al}_8\text{Mo}_3 + \text{Al}_{63}\text{Mo}_{37}$	Eutectic	.333	.273	.370	1836.4
$\text{Liquid} + \text{AlMo} \rightleftharpoons \text{Al}_{63}\text{Mo}_{37}$	Peritectic	.358	.4955	.370	1844.7
$\text{Liquid} + \text{cub}-A15 \rightleftharpoons \text{AlMo}$	Peritectic	.417	.750	.525	1983.6
$\text{Liquid} + \text{bcc}-A2 \rightleftharpoons \text{cub}-A15$	Peritectic	.621	.791	.750	2418.9
$\text{Liquid} + \text{Al}_4\text{Mo} \rightleftharpoons \text{Al}_5\text{Mo}$	Peritectic	.0012	.200	.166	1025.2
$\text{Liquid} + \text{Al}_5\text{Mo} \rightleftharpoons \text{Al}_{12}\text{Mo}$	Peritectic	.0005	.167	.077	971.6
$\text{Liquid} + \text{Al}_{12}\text{Mo} \rightleftharpoons \text{fcc}-A1$	Peritectic	.0002	.077	.0007	933.8
$\text{Liquid} + \text{Al}_8\text{Mo}_3 \rightleftharpoons \text{Al}_4\text{Mo}$	Peritectic	.028	.273	.200	1397.7
$\text{Al}_8\text{Mo}_3 \rightleftharpoons \text{Liquid}$	Congruent	.273	.273	...	1850.5

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Symbol Group	Sub-lattices	Comments
Al-Mo	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>	M 4	
	(Mo)	W	<i>cI2</i> <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	Al <sub>12</sub> Mo	Al <sub>12</sub> W	<i>cI26</i> <i>Im</i> $\bar{3}$	Al 24 Mo 2	
	Al <sub>5</sub> Mo	Al <sub>5</sub> W	<i>hP12</i> <i>P6</i> <sub>3</sub>		
	Al <sub>4</sub> Mo	Al <sub>4</sub> W	<i>mC30</i> <i>Cm</i>	Al <sub>1</sub> 2 Al <sub>2</sub> 2 Mo <sub>1</sub> 2 Al <sub>3</sub> 4 Al <sub>4</sub> 4 Al <sub>5</sub> 4 Al <sub>6</sub> 4 Al <sub>7</sub> 4 Mo <sub>2</sub> 4	
	Al <sub>8</sub> Mo <sub>3</sub>	Al <sub>8</sub> Mo <sub>3</sub>	<i>mC22</i> <i>C2/m</i>	Mo <sub>1</sub> 2 Al <sub>1</sub> 48 Al <sub>2</sub> 4 Al <sub>3</sub> 4 Al <sub>4</sub> 4 Mo <sub>2</sub> 4	
	Al <sub>23</sub> V <sub>4</sub>	Al <sub>23</sub> V <sub>4</sub>	<i>hP54</i> <i>P6</i> <sub>3</sub> /mmc		
	Al <sub>63</sub> Mo <sub>37</sub>				
	AlMo	W	<i>cI2</i> <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	AlMo <sub>3</sub>	Cr <sub>3</sub> Si	<i>cP8</i> <i>Pm</i> $\bar{3}$ <i>n</i>	Al 2 Mo 6	cub-A15

# System Al-N

**Solution Phases:**

(stable)	Liquid, fcc- <i>A1</i>
(metastable)	bcc- <i>A2</i> , hcp- <i>A3</i>

**Compound:**

AlN

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A2</i>	:	Sublattice model, (Al)(C, $\square$ ) <sub>3</sub>
fcc- <i>A1</i>	:	Sublattice model, (Al)(C, $\square$ )
hcp- <i>A3</i>	:	Sublattice model, (Al)(C, $\square$ ) <sub>0.5</sub>
gas	:	ideal (Al,Al <sub>2</sub> N,N <sub>2</sub> ,N <sub>3</sub> )
AlN	:	Stoichiometric, (Al)(N)

**Assessor and Date:**

H.L. Lukas 1992

Data relative for the bcc-*A2* and hcp-3 phases were evaluated by R. Fetzer and K. Zeng for the Al-N-Ti system.

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase AlN**

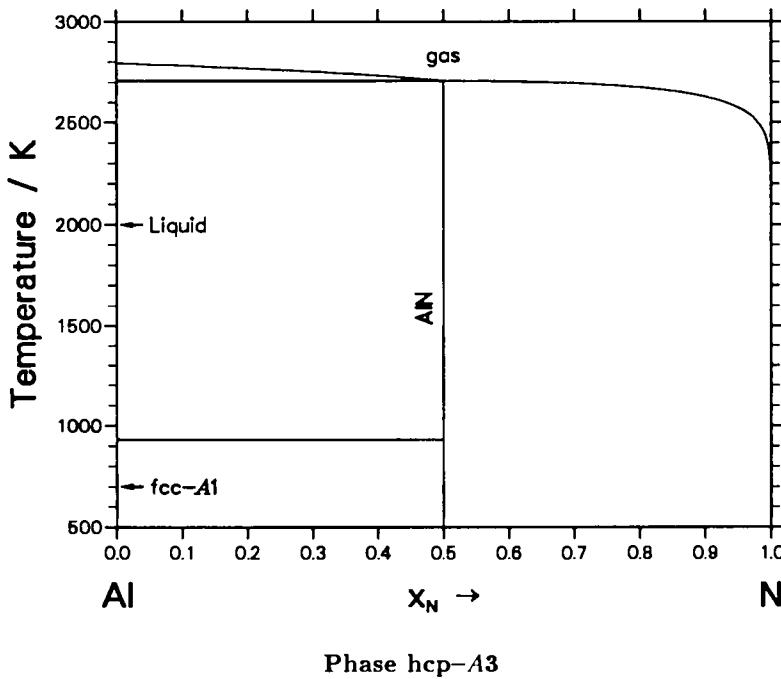
$$\begin{aligned}
 G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-}A1}(298.15 \text{ K}) - 2.0 \cdot H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) = \\
 - 338005.5 + 305.211 \cdot T - 46.94867 \cdot T \cdot \ln T - 0.00189068 \cdot T^2 \\
 + 874528 \cdot T^{-1} + 1.3756E-07 \cdot T^3
 \end{aligned}$$

**Phase bcc-*A2***

$$\begin{aligned}
 G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-}A1}(298.15 \text{ K}) - 3.0 \cdot H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) = \\
 23000 + 10 \cdot T + \text{GHSER}_{\text{Al}} + 3.0 \cdot \text{GHSER}_{\text{N}}
 \end{aligned}$$

**Phase fcc-*A1***

$$\begin{aligned}
 G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc-}A1}(298.15 \text{ K}) - H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) = \\
 80 \cdot T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{N}}
 \end{aligned}$$



### Phase hcp-A3

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - 0.5 \cdot H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) = \\ 80000 \cdot T + \text{GHSER}_{\text{Al}} + 0.5 \cdot \text{GHSER}_{\text{N}}$$

### Phase liquid

$$L_{\text{Al},\text{N}}^{0,\text{liquid}} = -336826.61 + 103.22478 \cdot T$$

### Phase gas(Al,Al<sub>2</sub>,N,N<sub>2</sub>,N<sub>3</sub>) (P = 0.1 MPa)

$$G_{\text{Al}}^{\circ,\text{gas}}(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) = RT \ln P + \\ \begin{aligned} 298.15 < T < 4300.00 : & 323947.58 - 25.1480948 \cdot T - 20.859 \cdot T \cdot \ln T \\ & + 4.5665E-05 \cdot T^2 - 3.942E-09 \cdot T^3 - 24275.5 \cdot T^{-1} \\ 4300.00 < T < 8200.00 : & 342017.234 - 54.0526114 \cdot T - 17.7891 \cdot T \cdot \ln T \\ & + 6.822E-05 \cdot T^2 - 1.9111E-08 \cdot T^3 \\ & - 14782200 \cdot T^{-1} \\ 8200.00 < T < 10000.00 : & 542396.07 - 411.214335 \cdot T + 22.2419 \cdot T \cdot \ln T \\ & - 0.00349619 \cdot T^2 + 4.0491E-08 \cdot T^3 \\ & - 2.0366965E+08 \cdot T^{-1} \end{aligned}$$

$$\begin{aligned}
G_{\text{Al}_2}^{\circ,\text{RGA}}(T) - 2.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) &= RT \ln P + \\
298.15 < T < 900.00 &: 496408.232 + 35.4797382 \cdot T - 41.6397 \cdot T \cdot \ln T \\
&\quad + 0.00249636 \cdot T^2 - 4.9050\text{E-}07 \cdot T^3 \\
&\quad + 85390.3 \cdot T^{-1} \\
900.00 < T < 10000.00 &: + 497613.221 + 17.3681302 \cdot T - 38.85476 \cdot T \cdot \ln T \\
&\quad - 2.249805\text{E-}04 \cdot T^2 - 9.49003167\text{E-}09 \cdot T^3 \\
&\quad - 5287.23 \cdot T^{-1} \\
G_{\text{N}_2}^{\circ,\text{RGA}}(T) - H_{0.5\text{N}_2}^{\circ,\text{RGA}}(298.15 \text{ K}) &= RT \ln P + \\
298.15 < T < 2950.00 &: 466446.153 + 2788.78662 \cdot T^{-1} - 13.2660528 \cdot T \\
&\quad - 20.8939295 \cdot T \cdot \ln T + 8.4552092\text{E-}05 \cdot T^2 \\
&\quad - 1.00186856\text{E-}08 \cdot T^3 \\
2950.00 < T < 6000.00 &: 481259.023 - 7559107.28 \cdot T^{-1} - 52.4348889 \cdot T \\
&\quad - 16.3761342 \cdot T \cdot \ln T - 2.28373808\text{E-}04 \cdot T^2 \\
&\quad - 2.78997209\text{E-}08 \cdot T^3 \\
G_{\text{N}_2}^{\circ,\text{RGA}}(T) - 2.0 \cdot H_{0.5\text{N}_2}^{\circ,\text{RGA}}(298.15 \text{ K}) &= 2.0 \cdot \text{GHSER}_{\text{N}} + RT \ln P \\
G_{\text{N}_3}^{\circ,\text{RGA}}(T) - 3.0 \cdot H_{0.5\text{N}_2}^{\circ,\text{RGA}}(298.15 \text{ K}) &= RT \ln P + \\
298.15 < T < 800.00 &: 403075.636 - 14.3245228 \cdot T - 29.5595416 \cdot T \cdot \ln T \\
&\quad - 0.02413122 \cdot T^2 + 3.6156036\text{E-}06 \cdot T^3 \\
&\quad + 55714.144 \cdot T^{-1} \\
800.00 < T < 2000.00 &: 388937.207 + 158.809275 \cdot T - 55.404528 \cdot T \cdot \ln T \\
&\quad - 0.0026570492 \cdot T^2 + 1.9365644\text{E-}07 \cdot T^3 \\
&\quad + 1536448.48 \cdot T^{-1} \\
2000.00 < T < 6000.00 &: 380898.006 + 210.207464 \cdot T - 62.295576 \cdot T \cdot \ln T \\
&\quad + 6.5726456\text{E-}06 \cdot T^2 - 7.868012\text{E-}10 \cdot T^3 \\
&\quad + 3336949.2 \cdot T^{-1}
\end{aligned}$$

Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{\text{N}}$	$T / \text{K}$
Liquid $\rightleftharpoons$ fcc-Al + AlN	Degenerate	.000 .000 .500	933.3
Liquid + gas $\rightleftharpoons$ AlN	Peritectic-like	.001 .503 .500	2707.7

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Al-N	(Al) AlN	Cu ZnS	$cF\bar{4}$ $Fm\bar{3}m$ $hP\bar{4}$ $P6_3mc$	Wurtzite

# System Al-Nb

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, fcc- <i>A</i> 1
(metastable)	bcc- <i>B</i> 2, hcp- <i>A</i> 3

**Compounds :**

(stable)	AlM- <i>D</i> 0 <sub>22</sub> , $\sigma$ , AlNb <sub>3</sub> - <i>A</i> 15
(metastable)	AlTi- <i>L</i> 1 <sub>0</sub> , AlM- <i>D</i> 0 <sub>19</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
bcc- <i>B</i> 2	:	Sublattice model, (Al,Nb) <sub>0.5</sub> (Al,Nb) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc- <i>B</i> 2 takes into account the ordering reaction bcc- <i>A</i> 2 ⇌ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlM- <i>D</i> 0 <sub>22</sub>	:	Sublattice model, (Al) <sub>3</sub> (Nb)
AlNb <sub>3</sub> - <i>A</i> 15	:	Sublattice model, (Al,Nb)(Nb) <sub>3</sub>
$\sigma$	:	Sublattice model , (Al) <sub>8</sub> (Nb) <sub>4</sub> (Al,Nb) <sub>18</sub>
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Al)(Nb)
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Al,Nb) <sub>3</sub> (Al,Nb)(□)

**Assessor and Date:**

N. Saunders, 1997.

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)****Phase AlM-D0<sub>22</sub>**

$$G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = \\ - 136000 + 24 T + 3.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Nb}}$$

**Phase AlM-D0<sub>19</sub>**

$$G^\circ(T) - 4.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 4.0 \text{ GHCP}_{\text{Al}} \\ G^\circ(T) - 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Nb:}\square) = \\ - 98000 + 22 T + 3.0 \text{ GHCP}_{\text{Al}} + \text{GHCP}_{\text{Nb}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Al:}\square) = \\ - 98000 + 10 T + \text{GHCP}_{\text{Al}} + 3.0 \text{ GHCP}_{\text{Nb}}$$

$$G^\circ(T) - 4.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Nb:}\square) = 4.0 \text{ GHCP}_{\text{Nb}} \\ L_{\text{Al,Nb:Al:}\square}^{0,\text{AlM-D0}_{19}} = - 137400 + 60 T$$

$$L_{\text{Al:Al,Nb:}\square}^{0,\text{AlM-D0}_{19}} = - 45760 + 20 T$$

$$L_{\text{Nb:Al,Nb:}\square}^{0,\text{AlM-D0}_{19}} = 4000$$

$$L_{\text{Al,Nb:Nb:}\square}^{0,\text{AlM-D0}_{19}} = 12000$$

**Phase AlNb<sub>3</sub>-A15**

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Al}) = \\ - 77920 + 4.88 T + \text{GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Nb}}$$

$$G^\circ(T) - 4.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Nb}) = \\ 20000 + 10 T + 4.0 \text{ GHSER}_{\text{Nb}}$$

$$L_{\text{Nb:Al,Nb}}^{0,\text{AlNb}_3-\text{A15}} = - 68000 + 20 T$$

$$L_{\text{Nb:Al,Nb}}^{1,\text{AlNb}_3-\text{A15}} = 1.0E-04$$

$$L_{\text{Nb:Al,Nb}}^{2,\text{AlNb}_3-\text{A15}} = - 12000$$

**Phase  $\sigma$** 

$$G^\circ(T) - 26.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 4.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Nb:Al}) = \\ - 150000 + 96 T + 26.0 \text{ GHSER}_{\text{Al}} + 4.0 \text{ GHSER}_{\text{Nb}}$$

$$G^\circ(T) - 8.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 22.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Nb:Nb}) = \\ - 635250 + 60 T + 8.0 \text{ GHSER}_{\text{Al}} + 22.0 \text{ GHSER}_{\text{Nb}}$$

$$L_{\text{Al:Nb:Al,Nb}}^{0,\sigma} = - 990000 + 270 T$$

$$L_{\text{Al:Nb:Al,Nb}}^{1,\sigma} = 420000$$

### Phase AlTi- $L_{10}$

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = 4 + 2.0 \text{ GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Nb}) =$$

$$- 44400 + 5.5 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Nb}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Al}) =$$

$$- 44400 + 5.5 T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Nb}}$$

$$G^\circ(T) - 2.0 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Nb}) = 2.0 \text{ GFCC}_{\text{Nb}}$$

$$L_{\text{Al},\text{Nb:Al}}^{0,\text{AlTi}-L_{10}} = - 80800 + 30 T$$

$$L_{\text{Al:Al,Nb}}^{0,\text{AlTi}-L_{10}} = - 80800 + 30 T$$

$$L_{\text{Nb:Al,Nb}}^{0,\text{AlTi}-L_{10}} = - 37600$$

$$L_{\text{Al,Nb:Nb}}^{0,\text{AlTi}-L_{10}} = - 37600$$

### Phase bcc-A2

$$L_{\text{Al},\text{Nb:}\square}^{0,\text{bcc}-A2} = - 104050 + 30 T$$

$$L_{\text{Al},\text{Nb:}\square}^{1,\text{bcc}-A2} = 9140 - 4 T$$

$$L_{\text{Al},\text{Nb:}\square}^{2,\text{bcc}-A2} = 12000$$

### Phase bcc-B2

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = 0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Nb})$$

$$- 8650 + T$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Al})$$

$$- 8650 + T$$

$$G^\circ(T) - H_{\text{Nb}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Nb}) = 0$$

$$L_{\text{Al:Al,Nb:}\square}^{0,\text{bcc}-B2} = 8650 - T$$

$$L_{\text{Nb:Al,Nb:}\square}^{0,\text{bcc}-B2} = 8650 - T$$

$$L_{\text{Al,Nb:Nb:}\square}^{0,\text{bcc}-B2} = 8650 - T$$

**Phase bcc-B2**

$$G_{\text{Al:Nb:}\square}^* = -8650 + T$$

$$G^\circ(T) - \overset{\circ}{H}_{\text{Al}}^{\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 \overset{\circ}{H}_{\text{Al}}^{\text{fcc}-A1}(298.15 \text{ K}) - 0.5 \overset{\circ}{H}_{\text{Nb}}^{\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Nb:}\square) = 2.0 \text{ } G_{\text{Al:Nb:}\square}^*$$

$$G^\circ(T) - 0.5 \overset{\circ}{H}_{\text{Cu}}^{\text{fcc}-A1}(298.15 \text{ K}) - 0.5 \overset{\circ}{H}_{\text{Nb}}^{\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Al:}\square) = 2.0 \text{ } G_{\text{Al:Nb:}\square}^*$$

$$G^\circ(T) - \overset{\circ}{H}_{\text{Nb}}^{\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Nb:}\square) = 0.0$$

**Phase bcc-A2**

$$L_{\text{Al,Nb:}\square}^{0,\text{bcc}-A2} = -104050 + 30 \text{ } T$$

$$L_{\text{Al,Nb:}\square}^{1,\text{bcc}-A2} = 9140 - 4 \text{ } T$$

$$L_{\text{Al,Nb:}\square}^{2,\text{bcc}-A2} = 12000$$

**Phase fcc-A1**

$$L_{\text{Al,Nb:}\square}^{0,\text{fcc}-A1} = -113500 + 21.1 \text{ } T$$

$$L_{\text{Al,Nb:}\square}^{1,\text{fcc}-A1} = 5000$$

$$L_{\text{Al,Nb:}\square}^{2,\text{fcc}-A1} = 10000$$

**Phase hcp-A3**

$$L_{\text{Al,Nb:}\square}^{0,\text{hcp}-A3} = -113500 + 21.1 \text{ } T$$

$$L_{\text{Al,Nb:}\square}^{1,\text{hcp}-A3} = 5000$$

$$L_{\text{Al,Nb:}\square}^{2,\text{hcp}-A3} = 10000$$

**Phase liquid**

$$L_{\text{Al,Nb}}^{0,\text{liquid}} = -91000 + 25 \text{ } T$$

$$L_{\text{Al,Nb}}^{1,\text{liquid}} = 6000$$

$$L_{\text{Al,Nb}}^{2,\text{liquid}} = 15000$$

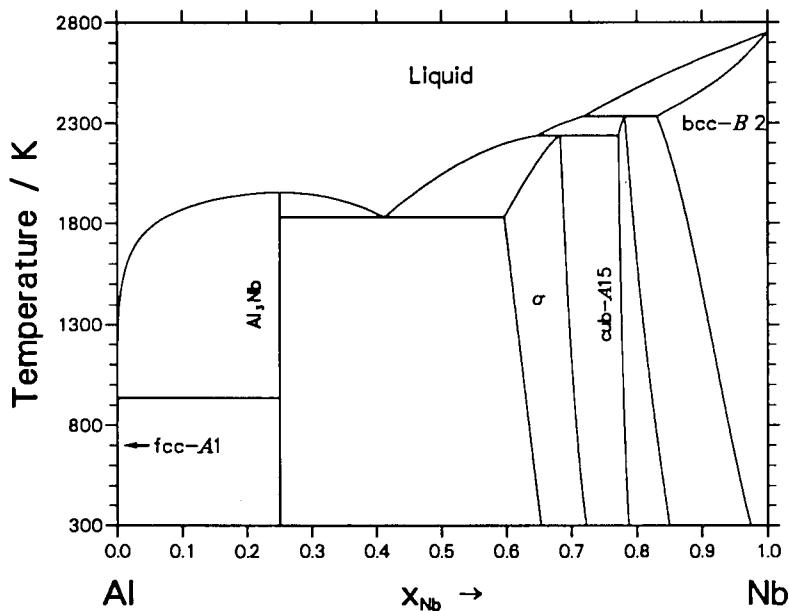


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{Nb}$	$T / K$
Liquid + Al <sub>3</sub> Nb <sup>*</sup> ⇌ fcc-A1	Peritectic	.000 .250 .001	934.2
Liquid ⇌ Al <sub>3</sub> Nb <sup>*</sup> + σ	Eutectic	.412 .250 .596	1832.1
Liquid + AlNb <sub>3</sub> <sup>**</sup> ⇌ σ	Peritectic	.647 .772 .683	2237.6
Liquid + bcc-A2 ⇌ AlNb <sub>3</sub> <sup>**</sup>	Peritectic	.718 .831 .782	2333.7
Al <sub>3</sub> Nb <sup>*</sup> ⇌ Liquid	Congruent	.250 .250 ...	1955.5

<sup>\*</sup> Al<sub>3</sub>Nb-D0<sub>22</sub><sup>\*\*</sup> Cr<sub>3</sub>Si-A15

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Symbol Group	Sub- lattices	Comments
Al-Nb	(Al)	Cu	<i>cF</i> 4 <i>Fm</i> $\bar{3}m$	M 4	
	(Nb)	W	<i>cI</i> 2 <i>Im</i> $\bar{3}m$	M 2	
	AlNb <sub>3</sub>	Cr <sub>3</sub> Si	<i>cP</i> 8 <i>Pm</i> $\bar{3}n$	Al 2 Nb 6	cub-A15
	AlNb <sub>2</sub>	$\sigma$ -CrFe	<i>tP</i> 30 <i>P4</i> <sub>2</sub> / <i>mnm</i>	Al <sub>1</sub> 2 Nb <sub>1</sub> 4 Al <sub>2</sub> 8 Nb <sub>2</sub> 8 Nb <sub>3</sub> 8	
	Al <sub>3</sub> Nb	Al <sub>3</sub> Ti	<i>tI</i> 8 <i>I4</i> / <i>mm</i> $\bar{3}m$	Nb 2 Al <sub>1</sub> 2 Al <sub>1</sub> 42	AlM-D0 <sub>22</sub>

# System Al-Nd

**Solution Phases:**

Liquid, bcc-*A*2, dhcp

**Compounds:**

Al<sub>11</sub>Nd<sub>3</sub>-H, Al<sub>11</sub>Nd<sub>3</sub>-L, Al<sub>3</sub>Nd, AlNd, AlNd<sub>2</sub>, AlNd<sub>3</sub>, Laves-*C*15

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
dhcp	:	Substitutional, Redlich-Kister
Al <sub>11</sub> Nd <sub>3</sub> -H	:	Stoichiometric, (Al) <sub>11</sub> (Nd) <sub>3</sub>
Al <sub>11</sub> Nd <sub>3</sub> -L	:	Stoichiometric, (Al) <sub>11</sub> (Nd) <sub>3</sub>
Al <sub>3</sub> Nd	:	Stoichiometric, (Al) <sub>3</sub> (Nd)
AlNd	:	Stoichiometric, (Al)(Nd)
AlNd <sub>2</sub>	:	Stoichiometric, (Al)(Nd) <sub>2</sub>
AlNd <sub>3</sub>	:	Stoichiometric, (Al)(Nd) <sub>3</sub>
Laves- <i>C</i> 15	:	Stoichiometric, (Al) <sub>2</sub> (Nd)

**Assessor and Date:**

G. Cacciamani, G. Borzone, R. Ferro

**Publication:**

G. Cacciamani, G. Borzone, R. Ferro, Anales de Fisica  
86B, 160-162 (1991)  
Revised in 1997.

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Al<sub>11</sub>Nd<sub>3</sub>-H**

$$G^\circ(T) - 11.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 3.0 \ H_{\text{Nd}}^{\circ,\text{dhcp}}(298.15 \text{ K}) = \\ - 526776.18 + 114.5827 \ T + 11.0 \ \text{GHSER}_{\text{Al}} + 3.0 \ \text{GHSER}_{\text{Nd}}$$

**Phase Al<sub>11</sub>Nd<sub>3</sub>-L**

$$G^\circ(T) - 11.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 3.0 \ H_{\text{Nd}}^{\circ,\text{dhcp}}(298.15 \text{ K}) = \\ - 548308.18 + 132.1646 \ T + 11.0 \ \text{GHSER}_{\text{Al}} + 3.0 \ \text{GHSER}_{\text{Nd}}$$

**Phase Laves-C15**

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Nd}}^{\circ,\text{dhcp}}(298.15 \text{ K}) = \\ - 158935.47 + 41.37165 \ T + 2.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Nd}}$$

**Phase  $\text{Al}_3\text{Nd}$** 

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Nd}}^{\circ,\text{dhcp}}(298.15 \text{ K}) = \\ - 181169.24 + 47.75868 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Nd}}$$

**Phase  $\text{AlNd}_2$** 

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 \ H_{\text{Nd}}^{\circ,\text{dhcp}}(298.15 \text{ K}) = \\ - 107787.66 + 37.00017 \ T + \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Nd}}$$

**Phase  $\text{AlNd}$** 

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Nd}}^{\circ,\text{dhcp}}(298.15 \text{ K}) = \\ - 99854.84 + 34.32248 \ T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Nd}}$$

**Phase  $\text{AlNd}_3$** 

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 \ H_{\text{Nd}}^{\circ,\text{dhcp}}(298.15 \text{ K}) = \\ - 107474.72 + 35.0142 \ T + \text{GHSER}_{\text{Al}} + 3.0 \ \text{GHSER}_{\text{Nd}}$$

**Phase bcc-A2**

$$L_{\text{Al},\text{Nd}:□}^{0,\text{bcc}-A2} = - 113226 + 45.05 \ T$$

$$L_{\text{Al},\text{Nd}:□}^{1,\text{bcc}-A2} = 10340 - 15.93 \ T$$

**Phase fcc-A1**

$$L_{\text{Al},\text{Nd}:□}^{0,\text{fcc}-A1} = 0$$

**Phase Liquid**

$$L_{\text{Al},\text{Nd}}^{0,\text{liquid}} = - 125909.87 + 56.16354 \ T - 21805836 \ T^{-1}$$

$$L_{\text{Al},\text{Nd}}^{1,\text{liquid}} = 35170.81 - 33.34898 \ T - 32643234 \ T^{-1}$$

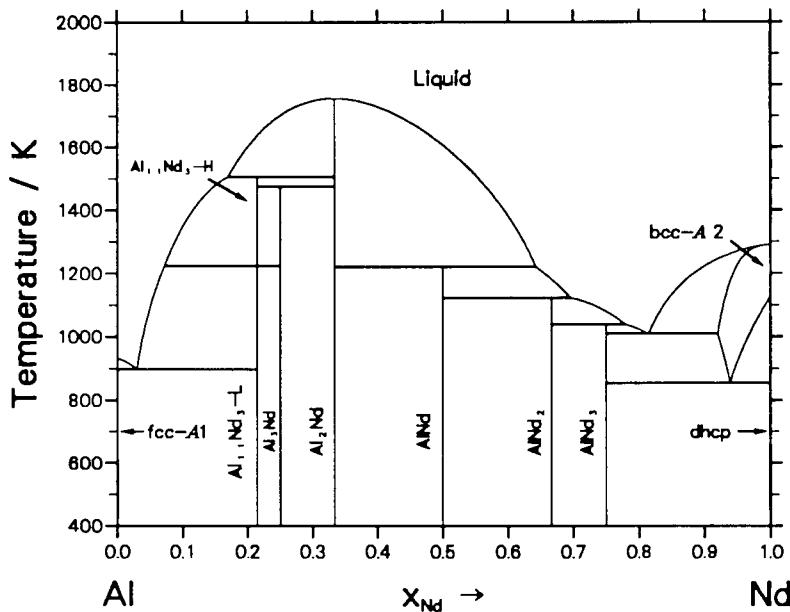


Table I - Invariant Reactions.

Reaction	Type	Compositions \$x_{\text{Nd}}	\$T / \text{K}
Liquid \$\rightleftharpoons\$ Al <sub>11</sub> Nd <sub>3</sub> -L + fcc-A1	Eutectic	.030 .000 .214	898.6
Liquid + Laves-C15* \$\rightleftharpoons\$ Al <sub>11</sub> Nd <sub>3</sub> -H	Peritectic	.170 .333 .214	1506.6
Al <sub>11</sub> Nd <sub>3</sub> -H + Al <sub>2</sub> Nd * \$\rightleftharpoons\$ Al <sub>3</sub> Nd	Peritectic	.214 .333 .250	1475.8
Liquid + AlNd \$\rightleftharpoons\$ Al <sub>2</sub> Nd	Peritectic	.643 0.500 .333	1220.3
Liquid + AlNd \$\rightleftharpoons\$ AlNd <sub>2</sub>	Peritectic	.696 .500 .667	1122.2
Liquid + AlNd <sub>2</sub> \$\rightleftharpoons\$ AlNd <sub>3</sub> -L	Peritectic	.780 .667 .750	1037.9
Liquid \$\rightleftharpoons\$ AlNd <sub>3</sub> -L + bcc-A2	Eutectic	.815 .750 .920	1008.9
bcc-A2 \$\rightleftharpoons\$ AlNd <sub>3</sub> -L + dhcp	Eutectoid	.939 .750 1.000	855.3
Al <sub>2</sub> Nd \$\rightleftharpoons\$ Liquid	Congruent	.333 .333 ...	1758.0
Al <sub>11</sub> Nd <sub>3</sub> -L \$\rightleftharpoons\$ Al <sub>11</sub> Nd <sub>3</sub> -H	Polymorphic	.214 .214 ...	1224.7

\* Laves-C15 \$\equiv\$ Al<sub>2</sub>Nd

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
Al-Nd	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M 4	
	(Nd)	La- $\alpha$	<i>hP4</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>	M 4	
	(Nd)	W	<i>cI2</i> <i>Im</i> $\bar{3}m$	M 2	
	Al <sub>11</sub> Nd <sub>3</sub> - $\alpha$	Al <sub>11</sub> La <sub>3</sub> - $\alpha$	<i>oI28</i> <i>Imm</i> <sub>m</sub>		Al <sub>11</sub> Nd <sub>3</sub> -L
	Al <sub>11</sub> Nd <sub>3</sub> - $\beta$	Al <sub>4</sub> Ba	<i>tI28</i> <i>I4/mmm</i>		Al <sub>11</sub> Nd <sub>3</sub> -II
	Al <sub>3</sub> Nd	Ni <sub>3</sub> Sn	<i>hP8</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>		
	Al <sub>2</sub> Nd	Cu <sub>2</sub> Mg	<i>cF24</i> <i>Fd</i> $\bar{3}m$	Nd 8 Al 16	Laves-C15
	AlNd	AlEr	<i>oP16</i> <i>Pmma</i>	Al 1 Nd 1	
	AlNd <sub>2</sub>	Co <sub>2</sub> Si	<i>oP12</i> <i>Pnma</i>	Al 1 Nd 3	
	AlNd <sub>3</sub>	Ni <sub>3</sub> Sn	<i>hP8</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>	Al 1 Nd 3	

# System Al-Si

**Solution Phases:**

(stable)	Liquid, fcc-Al
(metastable)	hcp-A3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc-Al	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
diamond	:	Substitutional, Redlich-Kister

**Assessor and Date:**

J. Gröbner, H.-L. Lukas, and F. Aldinger.

**Publication:**

Calphad, **20**, 2 (1996) 247-254.

**Thermodynamic properties of the solution phases(J.mol<sup>-1</sup>)**

**Phase fcc-Al**

$$L_{\text{Al},\text{Si}:0}^{0,\text{fcc}-\text{A}1} = -3143.78 + 0.39297 \ T$$

**Phase hcp-A3**

$$L_{\text{Al},\text{Si}:0}^{0,\text{hcp}-\text{A}3} = -3143.78 + 0.39297 \ T$$

**Phase diamond**

$$L_{\text{Al},\text{Si}}^{0,\text{diamond}} = 113246.16 - 47.5551 \ T$$

**Phase liquid**

$$L_{\text{Al},\text{Si}}^{0,\text{liquid}} = -11340.1 - 1.23394 \ T$$

$$L_{\text{Al},\text{Si}}^{1,\text{liquid}} = -3530.93 + 1.35993 \ T$$

$$L_{\text{Al},\text{Si}}^{2,\text{liquid}} = 2265.39$$

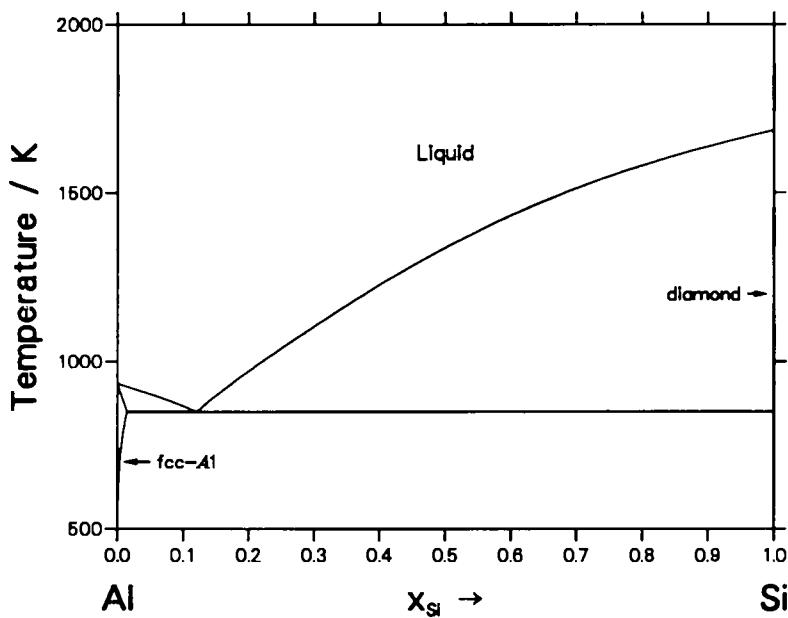


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Si}}$	$T / \text{K}$
$\text{Liquid} \rightleftharpoons \text{fcc-Al} + \text{diamond}$	Eutectic	.122 .016 1.000	850.1

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Al-Si	(Al)	Cu	$cF4$ $Fm\bar{3}m$
	(Si)	diamond	$cF8$ $Fd\bar{3}m$

# System Al-Sn

**Solution Phases:**

(stable)	:	Liquid, fcc- <i>A</i> 1, bct- <i>A</i> 5
(metastable)	:	hcp- <i>A</i> 3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
bct- <i>A</i> 5	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister

**Assessor and Date:**

S. Fries, and H.L. Lukas,

**Publication:**

"Cost507 New Light Alloys", Leuven Proceedings,  
Ed. G. Effenberg (1991)

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase bct-*A*5**

$$I_{\text{Al},\text{Sn}}^{0,\text{bct-}A5} = 14136.95 - 4.71231 \cdot T$$

**Phase fcc-*A*1**

$$I_{\text{Al},\text{Sn}:□}^{0,\text{fcc-}A1} = 45297.84 - 8.39814 \cdot T$$

**Phase hcp-*A*3**

$$I_{\text{Al},\text{Sn}:□}^{0,\text{hcp-}A3} = 0.00001$$

**Phase liquid**

$$I_{\text{Al},\text{Sn}}^{0,\text{liquid}} = 16329.85 - 4.98306 \cdot T$$

$$I_{\text{Al},\text{Sn}}^{1,\text{liquid}} = 4111.97 - 1.15145 \cdot T$$

$$I_{\text{Al},\text{Sn}}^{2,\text{liquid}} = 1765.43 - 0.57390 \cdot T$$

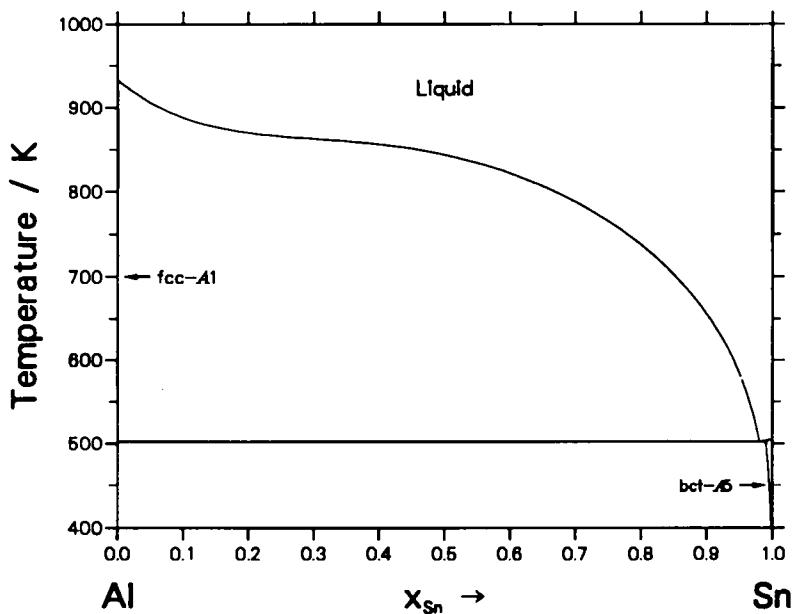


Table I – Invariant Reactions.

Reaction	Type	Compositions \$x_{\text{Sn}}	\$T / \text{K}
Liquid $\rightleftharpoons$ fcc-Al + bct-A5	Eutectic	.980 .000 .990	502.4

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Al-Sn	(Al)	Cu	$cF_4$ $Fm\bar{3}m$
	(Sn)	$\beta$ -Sn	$tI_4$ $I4_1/AMD$

# System Al-Ta

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, fcc- <i>A</i> 1
(metastable)	bcc- <i>B</i> 2, hcp- <i>A</i> 3

**Compounds :**

(stable)	AlM- <i>D</i> 0 <sub>22</sub> , $\sigma$
(metastable)	AlTi- <i>L</i> 1 <sub>0</sub> , AlM- <i>D</i> 0 <sub>19</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
bcc- <i>B</i> 2	:	Sublattice model, (Al,Ta) <sub>0.5</sub> (Al,Ta) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc- <i>A</i> 2 $\rightleftharpoons$ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28.
AlM- <i>D</i> 0 <sub>19</sub>	:	For the latter, the parameters are given in a frame.
AlM- <i>D</i> 0 <sub>22</sub>	:	Sublattice model, (Al,Ta) <sub>3</sub> (Al,Ta)(□)
$\sigma$	:	Sublattice model, (Al) <sub>3</sub> (Ta)
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Al) <sub>8</sub> (Ta) <sub>4</sub> (Al,Ta) <sub>18</sub>
		Sublattice model, (Al,Ta) <sub>0.5</sub> (,TaTa) <sub>0.5</sub>

**Assessor and Date:**

N. Saunders, 1997.

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase AlM-*D*0<sub>22</sub>**

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Ta}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ - 130456 + 23 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Ta}}$$

**Phase  $\text{Al}_3\text{Ta}_2\text{-H}$** 

$$G^\circ(T) = 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 145000 + 17.325 T + 3.0 \text{ GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Ta}}$$

**Phase  $\text{Al}_3\text{Ta}_2\text{-L}$** 

$$G^\circ(T) = 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 155000 + 24 T + 3.0 \text{ GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Ta}}$$

**Phase  $\text{AlM-D0}_{19}$** 

$$G^\circ(T) = 4.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 4.0 \text{ GHCP}_{\text{Al}} \\ G^\circ(T) = 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Ta:}\square) = \\ - 96000 + 22.52 T + 3 \text{ GHCP}_{\text{Al}} + \text{GHCP}_{\text{Ta}}$$

$$G^\circ(T) = H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Al:}\square) = \\ - 96000 + 22.52 T + \text{GHCP}_{\text{Al}} + 3 \text{ GHCP}_{\text{Ta}}$$

$$G^\circ(T) = 4 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Ta:}\square) = 4 + 4 \text{ GHCP}_{\text{Ta}} \\ L_{\text{Al,Ta:Al:}\square}^{0,\text{AlM-D0}_{19}} = - 200000 + 60 T$$

$$L_{\text{Al:Al,Ta:}\square}^{0,\text{AlM-D0}_{19}} = - 66000 + 20 T$$

$$L_{\text{Ta:Al,Ta:}\square}^{0,\text{AlM-D0}_{19}} = 8000$$

$$L_{\text{Al,Ta:Ta:}\square}^{0,\text{AlM-D0}_{19}} = 20000$$

**Phase  $\sigma$** 

$$G^\circ(T) = 26 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 4 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Ta:Al}) = \\ - 300000 + 90 T + 26 \text{ GHSER}_{\text{Al}} + 4 \text{ GHSER}_{\text{Ta}}$$

$$G^\circ(T) = 8 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 22 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Ta:Ta}) = \\ - 657000 + 90 T + 8 \text{ GHSER}_{\text{Al}} + 22 \text{ GHSER}_{\text{Ta}}$$

$$L_{\text{Al:Ta:Al,Ta}}^{0,\sigma} = - 1230000 + 450 T$$

$$L_{\text{Al:Ta:Al,Ta}}^{1,\sigma} = 1.0E-4$$

$$L_{\text{Al:Ta:Al,Ta}}^{2,\sigma} = 300000$$

**Phase AlTi-L1<sub>0</sub>**

$$G^\circ(T) - 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = 4 + 2.0 \text{ GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Ta}) =$$

$$- 71000 + 15.0 T + \text{GHSER}_{\text{Al}} + \text{GHFCC}_{\text{Ta}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Al}) =$$

$$- 71000 + 15.0 T + \text{GHSER}_{\text{Al}} + \text{GHFCC}_{\text{Ta}}$$

$$G^\circ(T) - 2 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Ta}) = 2 \text{ GFCC}_{\text{Ta}}$$

$$L_{\text{Al},\text{Ta:Al}}^{0,\text{AlTi}-L1_0} = - 56000 + 20 T$$

$$L_{\text{Al},\text{Ta:Al}}^{1,\text{AlTi}-L1_0} = 30000$$

$$L_{\text{Al},\text{Ta:Al}}^{2,\text{AlTi}-L1_0} = 20000$$

$$L_{\text{Al:Al,Ta}}^{0,\text{AlTi}-L1_0} = - 56000 + 20 T$$

$$L_{\text{Al:Al,Ta}}^{1,\text{AlTi}-L1_0} = 30000$$

$$L_{\text{Al:Al,Ta}}^{2,\text{AlTi}-L1_0} = 20000$$

**Phase bcc-A2**

$$L_{\text{Al,Ta:}\square}^{0,\text{bcc}-A2} = - 89000 + 30 T$$

$$L_{\text{Al,Ta:}\square}^{1,\text{bcc}-A2} = - 5000$$

$$L_{\text{Al,Ta:}\square}^{2,\text{bcc}-A2} = 15000$$

**Phase bcc-B2**

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = 0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Ta}) = - 8250 + T$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Al}) = - 8250 + T$$

$$G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Ta}) = 0$$

$$L_{\text{Al:Al,Ta:}\square}^{0,\text{bcc}-B2} = 8250 - T$$

$$L_{\text{Ta:Al,Ta:}\square}^{0,\text{bcc}-B2} = 8250 - T$$

$$L_{\text{Al,Ta:Al:}\square}^{0,\text{bcc}-B2} = 8250 - T$$

**Phase bcc-B2**

$$G_{\text{Al:Ta:}\square}^* = -8250 + T$$

$$G^\circ(T) - \overset{\circ}{H}_{\text{Al}}^{\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 \overset{\circ}{H}_{\text{Al}}^{\text{fcc}-A1}(298.15 \text{ K}) - 0.5 \overset{\circ}{H}_{\text{Ta}}^{\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Ta:}\square) = 2.0 \ G_{\text{Al:Ta:}\square}^*$$

$$G^\circ(T) - 0.5 \overset{\circ}{H}_{\text{Cu}}^{\text{fcc}-A1}(298.15 \text{ K}) - 0.5 \overset{\circ}{H}_{\text{Ta}}^{\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Al:}\square) = 2.0 \ G_{\text{Al:Ta:}\square}^*$$

$$G^\circ(T) - \overset{\circ}{H}_{\text{Ta}}^{\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Ta:}\square) = 0.0$$

**bcc-A2**

$$L_{\text{Al,Ta:}\square}^{0,\text{bcc}-A2} = -89000 + 30 \ T$$

$$L_{\text{Al,Ta:}\square}^{1,\text{bcc}-A2} = -5000$$

$$L_{\text{Al,Ta:}\square}^{2,\text{bcc}-A2} = 15000$$

**Phase fcc-A1**

$$L_{\text{Al,Ta:}\square}^{0,\text{fcc}-A1} = -100000 + 30 \ T$$

**Phase hcp-A3**

$$L_{\text{Al,Ta:}\square}^{0,\text{hcp}-A3} = -100000 + 30 \ T$$

**Phase liquid**

$$L_{\text{Al,Ta}}^{0,\text{liquid}} = -108000 + 30 \ T$$

$$L_{\text{Al,Ta}}^{1,\text{liquid}} = 6000$$

$$L_{\text{Al,Ta}}^{2,\text{liquid}} = 17000$$

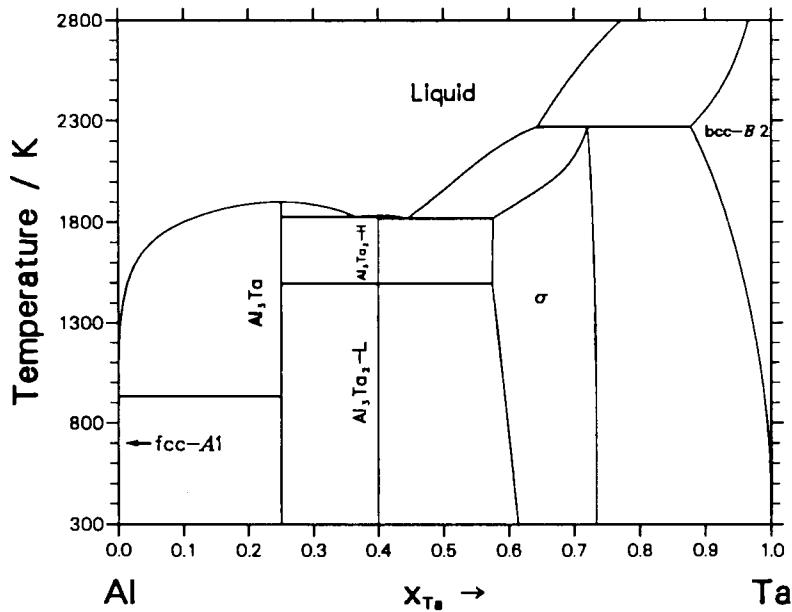


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Ta}}$	$T / \text{K}$
Liquid + AIM-D0 <sub>22</sub> $\rightleftharpoons$ fcc-Al	Peritectic	.00001 .250 .0008	934.0
Liquid $\rightleftharpoons$ + AIM-D0 <sub>22</sub> + Al <sub>3</sub> Ta <sub>2</sub> -II	Eutectic	.366 .250 .400	1826.8
Liquid $\rightleftharpoons$ Al <sub>3</sub> Ta <sub>2</sub> -H $\rightleftharpoons$ + $\sigma$	Eutectic	.444 .400 .576	1819.8
Liquid + bcc-A2 $\rightleftharpoons$ $\sigma$	Peritectic	.643 .877 .720	2270.4
Al <sub>3</sub> Ta* $\rightleftharpoons$ Liquid	Congruent	.250 .250 ...	1901.0
Al <sub>3</sub> Ta <sub>2</sub> -H $\rightleftharpoons$ Al <sub>3</sub> Ta <sub>2</sub> -II	Polymorphic	.400 .400 ...	1498.1

\* AIM-D0<sub>22</sub>  $\equiv$  Al<sub>3</sub>Ta

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
Al-Ta	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>	M 4	AlM-D0 <sub>22</sub>
	(Ta)	W	<i>cI2</i> <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	AlTa <sub>2</sub>	$\sigma$ -CrFe	<i>tP30</i> <i>P4</i> <sub>2</sub> / <i>mnm</i>	Al <sub>1</sub> 2 Ta <sub>1</sub> 4 Al <sub>2</sub> 8 Ta <sub>2</sub> 8 Ta <sub>3</sub> 8	
	Al <sub>3</sub> Ta	Al <sub>3</sub> Ti	<i>tI8</i> <i>I4/mmm</i> <i>3m</i>	Ta 2 Al <sub>1</sub> 2 Al <sub>1</sub> 42	
	Al <sub>3</sub> Ta <sub>2</sub> -L		$\sigma^{**}$		
	Al <sub>3</sub> Ta <sub>2</sub> -II		$\sigma^{*24}$		

# System Al-Ti

**Solution Phases:**

(stable) Liquid, bcc-*A*2, fcc-*A*1, hcp-*A*3, AlM-*D*0<sub>19</sub>, AlTi-*L*1<sub>0</sub>  
 (metastable) bcc-*B*2

**Compounds:**

AlM-*D*0<sub>22</sub>, Al<sub>2</sub>Ti, Al<sub>11</sub>Ti<sub>5</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
bcc- <i>B</i> 2	:	Sublattice model, (Al,Ti) <sub>0.5</sub> (Al,Ti) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc- <i>A</i> 2 ⇌ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Al,Ti)(Al,Ti) <sub>3</sub> (□) <sub>0.5</sub>
L <sub>1</sub> <sub>0</sub> -AlTi	:	Sublattice model, (Al,Ti)(Al,Ti)
AlM- <i>D</i> 0 <sub>22</sub>	:	Stoichiometric, (Al) <sub>3</sub> (Ti)
Al <sub>2</sub> Ti	:	Stoichiometric, (Al) <sub>2</sub> (Ti)
Al <sub>11</sub> Ti <sub>5</sub>	:	Stoichiometric, (Al) <sub>11</sub> (Ti) <sub>5</sub>

**Assessor and Date:**

N. Saunders (1992)

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase AlTi-*L*1<sub>0</sub>**

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Al:Al}) = 2.0 \ \text{GHSER}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Ti:Al}) = \\ - 79644.0 + 19.2 \ T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al}: \text{Ti}) = \\ - 79644.0 + 19.2 \text{ } T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 2.0 \text{ } H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Ti}) = 2.0 \text{ } \text{GFCCTi} \\ L_{\text{Al}, \text{Ti}: \text{Al}}^{0, \text{AlTi}-L^{10}} = - 89892 + 44 \text{ } T$$

$$L_{\text{Al}, \text{Ti}: \text{Al}}^{1, \text{AlTi}-L^{10}} = 30000$$

$$L_{\text{Al}, \text{Ti}: \text{Al}}^{2, \text{AlTi}-L^{10}} = 20000$$

$$L_{\text{Al}: \text{Al}, \text{Ti}}^{0, \text{AlTi}-L^{10}} = - 89892 + 44 \text{ } T$$

$$L_{\text{Al}: \text{Al}, \text{Ti}}^{1, \text{AlTi}-L^{10}} = 30000$$

$$L_{\text{Al}: \text{Al}, \text{Ti}}^{2, \text{AlTi}-L^{10}} = 20000$$

$$L_{\text{Ti}: \text{Al}, \text{Ti}}^{0, \text{AlTi}-L^{10}} = - 15134 - 2.36 \text{ } T$$

$$L_{\text{Al}, \text{Ti}: \text{Ti}}^{0, \text{AlTi}-L^{10}} = - 15134 - 2.36 \text{ } T$$

### Phase AlM-D0<sub>19</sub>

$$G^\circ(T) - 4.0 \text{ } H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al}: \text{Al}: \square) = 4.0 \text{ } \text{GIICPAI}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 \text{ } H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Al}: \square) = \\ - 110080 + 23.88 \text{ } T + \text{GHSER}_{\text{Al}} + 3.0 \text{ } \text{GIISER}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 \text{ } H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al}: \text{Ti}: \square) = \\ - 99120.0 + 32.28 \text{ } T + 3.0 \text{ } \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 4.0 \text{ } H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Ti}: \square) = 4.0 \text{ } \text{GIISER}_{\text{Ti}}$$

$$L_{\text{Al}, \text{Ti}: \text{Al}: \square}^{0, \text{AlM}-D^{019}} = - 298200 + 100 \text{ } T$$

$$L_{\text{Al}, \text{Ti}: \text{Ti}: \square}^{0, \text{AlM}-D^{019}} = 32000 - 4 \text{ } T$$

$$L_{\text{Al}: \text{Al}, \text{Ti}: \square}^{0, \text{AlM}-D^{019}} = - 98968 + 33.3 \text{ } T$$

$$L_{\text{Ti}: \text{Al}, \text{Ti}: \square}^{0, \text{AlM}-D^{019}} = 10656 - 1.332 \text{ } T$$

### Phase Al<sub>2</sub>Ti

$$G^\circ(T) - 2.0 \text{ } H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 121500 + 31.2 \text{ } T + 2.0 \text{ } \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Ti}}$$

**Phase AlM-D0<sub>22</sub>**

$$\begin{aligned}
 G^\circ(T) - 3.0 & H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al}: \text{Ti}) = \\
 & - 144592.0 + 37.024 T + 3.0 \text{ GIISER}_{\text{Al}} + \text{GHSER}_{\text{Ti}} \\
 G^\circ(T) - 4.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Ti}) = \\
 & \text{GFCC}_{\text{Ti}} \\
 L_{\text{Al}, \text{Ti}: \text{Ti}}^{0,\text{AlM}-D0_{22}} & = - 60000
 \end{aligned}$$

**Phase "Al<sub>11</sub>Ti<sub>5</sub>"**

$$\begin{aligned}
 G^\circ(T) - 17.0 & H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 8.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\
 & - 971125.0 + 236.4 T + 17.0 \text{ GIISER}_{\text{Al}} + 8.0 \text{ GIISER}_{\text{Ti}}
 \end{aligned}$$

**Phase bcc-A2**

$$\begin{aligned}
 L_{\text{Al}, \text{Ti}: \square}^{0,\text{bcc}-A2} & = - 128500 + 39 T \\
 L_{\text{Al}, \text{Ti}: \square}^{1,\text{bcc}-A2} & = 6000 \\
 L_{\text{Al}, \text{Ti}: \square}^{2,\text{bcc}-A2} & = 21200
 \end{aligned}$$

**Phase bcc-B2**

$$\begin{aligned}
 G^\circ(T) - H_{\text{Al}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) & = G(\text{Al}: \text{Al}: \square) = 0 \\
 G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) & = G(\text{Al}: \text{Ti}: \square) \\
 & - 8750 + 1.25 T \\
 G^\circ(T) - 0.5 H_{\text{Al}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) & = G(\text{Ti}: \text{Al}: \square) \\
 & - 8750 + 1.25 T \\
 G^\circ(T) - H_{\text{Ti}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) & = G(\text{Ti}: \text{Ti}: \square) = 0 \\
 L_{\text{Al}: \text{Al}, \text{Ti}: \square}^{0,\text{bcc}-B2} & = 8750 - 1.25 T \\
 L_{\text{Ti}: \text{Al}, \text{Ti}: \square}^{0,\text{bcc}-B2} & = 8750 - 1.25 T \\
 L_{\text{Al}, \text{Ti}: \text{Al}: \square}^{0,\text{bcc}-B2} & = 8750 - 1.25 T \\
 L_{\text{Al}, \text{Ti}: \text{Al}: \square}^{0,\text{bcc}-B2} & = 8750 - 1.25 T
 \end{aligned}$$

**Phase bcc-B2**

$$G_{\text{Al}: \text{Ti}: \square}^{\bullet} = -8750 + 1.25 T$$

$$G^{\circ}(T) - H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al}: \text{Al}: \square) = 0.0$$

$$G^{\circ}(T) - 0.5 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al}: \text{Ti}: \square) = 2.0 G_{\text{Al}: \text{Ti}: \square}^{\bullet}$$

$$G^{\circ}(T) - 0.5 H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Al}: \square) = 2.0 G_{\text{Al}: \text{Ti}: \square}^{\bullet}$$

$$G^{\circ}(T) - H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Ti}: \square) = 0.0$$

**Phase bcc-A2**

$$L_{\text{Al}, \text{Ti}: \square}^{0, \text{bcc}-A2} = -128500 + 39 T$$

$$L_{\text{Al}, \text{Ti}: \square}^{1, \text{bcc}-A2} = 6000$$

$$L_{\text{Al}, \text{Ti}: \square}^{2, \text{bcc}-A2} = 21200$$

**Phase fcc-A1**

$$L_{\text{Al}, \text{Ti}: \square}^{0, \text{fcc}-A1} = -128970 + 39 T$$

$$L_{\text{Al}, \text{Ti}: \square}^{1, \text{fcc}-A1} = -5000$$

$$L_{\text{Al}, \text{Ti}: \square}^{2, \text{fcc}-A1} = 20000$$

**Phase hcp-A3**

$$L_{\text{Al}, \text{Ti}: \square}^{0, \text{hcp}-A3} = -133500 + 39 T$$

$$L_{\text{Al}, \text{Ti}: \square}^{1, \text{hcp}-A3} = 750.0$$

$$L_{\text{Al}, \text{Ti}: \square}^{2, \text{hcp}-A3} = 17500.0$$

## Phase liquid

$$L_{\text{Al,Ti}}^{0,\text{liquid}} = -108250 + 38 T$$

$$L_{\text{Al,Ti}}^{1,\text{liquid}} = -6000 + 5 T$$

$$L_{\text{Al,Ti}}^{2,\text{liquid}} = 15000$$

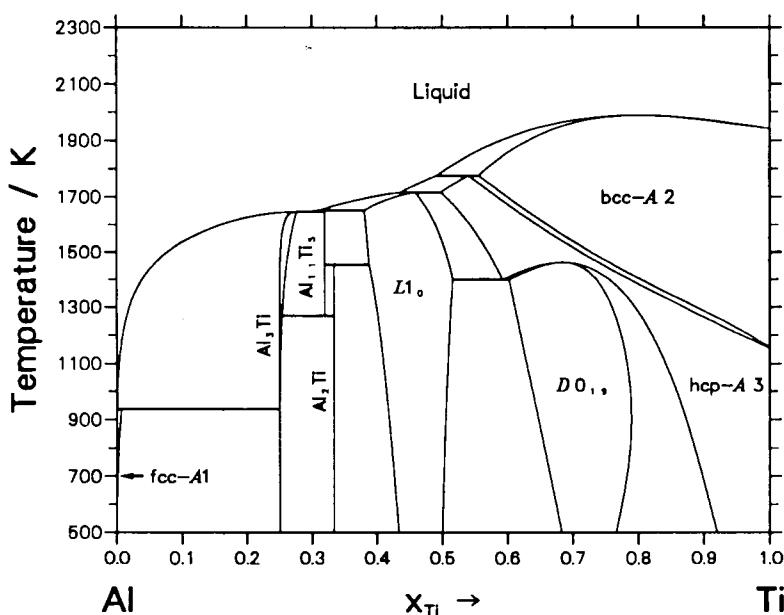


Table I – Invariant Reactions.

Reaction	Type	Compositions \$x_{\text{Ti}}			\$T / \text{K}
$\text{Al}_{11}\text{Ti}_5 + \text{AlTi}-\text{L}1_0 \rightleftharpoons \text{Al}_2\text{Ti}$	Peritectoid	.320	.388	.333	1454.3
$\text{Al}_{11}\text{Ti}_5 \rightleftharpoons \text{AIM}^* + \text{Al}_2\text{Ti}$	Eutectoid	.320	.250	.333	1259.8
$\text{Liquid} + \text{Al}_{11}\text{Ti}_5 \rightleftharpoons \text{AlM-DO}_{22}^*$	Peritectic	.247	.320	.250	1627.7
$\text{Liquid} + \text{AlM-DO}_{22}^* \rightleftharpoons \text{fcc-A1}$	Degenerate	.001	.250	.000	934.2
$\text{Liquid} + \text{AlTi-L}1_0 \rightleftharpoons \text{Al}_{11}\text{Ti}_5$	Peritectic	.310	.380	.320	1651.9
$\text{Liquid} + \text{hcp-A3} \rightleftharpoons \text{AlTi-L}1_0$	Peritectic	.436	.498	.459	1716.7
$\text{Liquid} + \text{bcc-A2} \rightleftharpoons \text{hcp-A3}$	Peritectic	.491	.555	.540	1775.9
$\text{hcp-A3} \rightleftharpoons \text{L}1_0-\text{AlTi} + \text{AlM-DO}_{19}$	Eutectoid	.595	.518	.607	1384.4
$\text{AlM-DO}_{19} \rightleftharpoons \text{hcp-A3}$	Congruent	.682	.682	....	1452.0
$\text{bcc-A2} \rightleftharpoons \text{liquid}$	Congruent	.788	.788	....	1989.0

\*  $\text{AIM-DO}_{22} \equiv \text{Al}_3\text{Ti}$

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	
Al-Ti	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M 4	
	(Ti)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	(Ti)	W	<i>cI2</i> <i>Im</i> $\bar{3}m$	M 2	
	AlTi	AlCu	<i>tP4</i> <i>P4/mmm</i>	Al 2 Ti <sub>1</sub> 1 Ti <sub>2</sub> 1	AlTi- <i>L1<sub>0</sub></i>
	AlTi <sub>3</sub>	Ni <sub>3</sub> Sn	<i>hP8</i> <i>P6<sub>3</sub>/mmc</i>		AlM- <i>D0<sub>19</sub></i>
	Al <sub>2</sub> Ti	Ga <sub>2</sub> Hf	<i>tI24</i> <i>I4<sub>1</sub>/amd</i>		
	Al <sub>2</sub> Ti- $\alpha$	Ga <sub>2</sub> Zr	<i>oCt2</i> <i>Cmmm</i>		transformation not taken into account in [90Mas]
	Al <sub>3</sub> Ti	Al <sub>3</sub> Ti	<i>tI8</i> <i>I4/mmm</i>	Al <sub>1</sub> 2 Al <sub>2</sub> 4 Ti 2	AlM- <i>D0<sub>22</sub></i>
	Al <sub>5</sub> Ti <sub>3</sub>		<i>tP32</i> <i>I4/mbm</i>		
	$\delta$	Al <sub>3</sub> Zr	<i>tI16</i>		Al <sub>11</sub> Ti <sub>5</sub> from [91Vil]
	Al <sub>5</sub> Ti <sub>3</sub>		<i>tP32</i> <i>I4/mbm</i>		metastable

# System Al-V

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1

**Compounds:**

Al<sub>10</sub>V, Al<sub>7</sub>V, Al<sub>23</sub>V<sub>4</sub>, AIM-D0<sub>22</sub>, Al<sub>8</sub>V<sub>5</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
Al <sub>10</sub> V	:	Stoichiometric, (Al) <sub>10</sub> (V)
Al <sub>7</sub> V	:	Stoichiometric, (Al) <sub>7</sub> (V)
Al <sub>23</sub> V <sub>4</sub>	:	Stoichiometric, (Al) <sub>23</sub> (V) <sub>4</sub>
AIM-D0 <sub>22</sub>	:	Stoichiometric, (Al) <sub>3</sub> (V)
Al <sub>8</sub> V <sub>5</sub>	:	Stoichiometric, (Al) <sub>8</sub> (V) <sub>5</sub>

**Assessor and Date:**

N. Saunders (1991)

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Al<sub>10</sub>V**

$$G^\circ(T) - 10.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{V}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ - 111221 + 18.909 \ T + 10.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{V}}$$

**Phase Al<sub>23</sub>V<sub>4</sub>**

$$G^\circ(T) - 23.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 4.0 \ H_{\text{V}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ - 430650 + 64.665 \ T + 23.0 \ \text{GHSER}_{\text{Al}} + 4.0 \ \text{GHSER}_{\text{V}}$$

**Phase AIM-D0<sub>22</sub>**

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{V}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ - 104308.0 + 15.2 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{V}}$$

**Phase Al<sub>7</sub>V**

$$G^\circ(T) - 7.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{V}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 108800.0 + 16.8 \ T + 7.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{V}}$$

**Phase Al<sub>8</sub>V<sub>5</sub>**

$$G^\circ(T) - 8.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 5.0 \ H_{\text{V}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ - 294320.0 - 13.0 \ T + 8.0 \ \text{GHSER}_{\text{Al}} + 5.0 \ \text{GHSER}_{\text{V}}$$

**Phase bcc-A2**

$$L_{\text{Al},\text{V};\square}^{0,\text{bcc}-A2} = - 95000 + 20 \ T$$

$$L_{\text{Al},\text{V};\square}^{1,\text{bcc}-A2} = - 6000$$

**Phase fcc-A1**

$$L_{\text{Al},\text{V};\square}^{0,\text{fcc}-A1} = - 69800 + 15 \ T$$

$$L_{\text{Al},\text{V};\square}^{1,\text{fcc}-A1} = - 8000$$

**Phase liquid**

$$L_{\text{Al},\text{V}}^{0,\text{liquid}} = - 50725 + 9 \ T$$

$$L_{\text{Al},\text{V}}^{1,\text{liquid}} = - 15000 + 8 \ T$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions xv			T / K
Liquid + AlM-D0 <sub>22</sub> ⇌ Al <sub>23</sub> V <sub>4</sub>	Peritectic	.003	.250	.148	1007.3
Liquid + Al <sub>23</sub> V <sub>4</sub> ⇌ Al <sub>7</sub> V	Peritectic	.002	.148	.125	969.0
Liquid + Al <sub>7</sub> V ⇌ Al <sub>10</sub> V	Peritectic	.001	.125	.091	945.2
Liquid + Al <sub>10</sub> V ⇌ fcc-A1	Peritectic	.000	.091	.001	935.3
Liquid + Al <sub>8</sub> V <sub>5</sub> ⇌ AlM-D0 <sub>22</sub>	Peritectic	.167	.384	.250	1640.1
Liquid + bcc-A2 ⇌ Al <sub>8</sub> V <sub>5</sub>	Peritectic	.376	.471	.384	1932.7

\* AlM-D0<sub>22</sub> ≡ Al<sub>3</sub>V

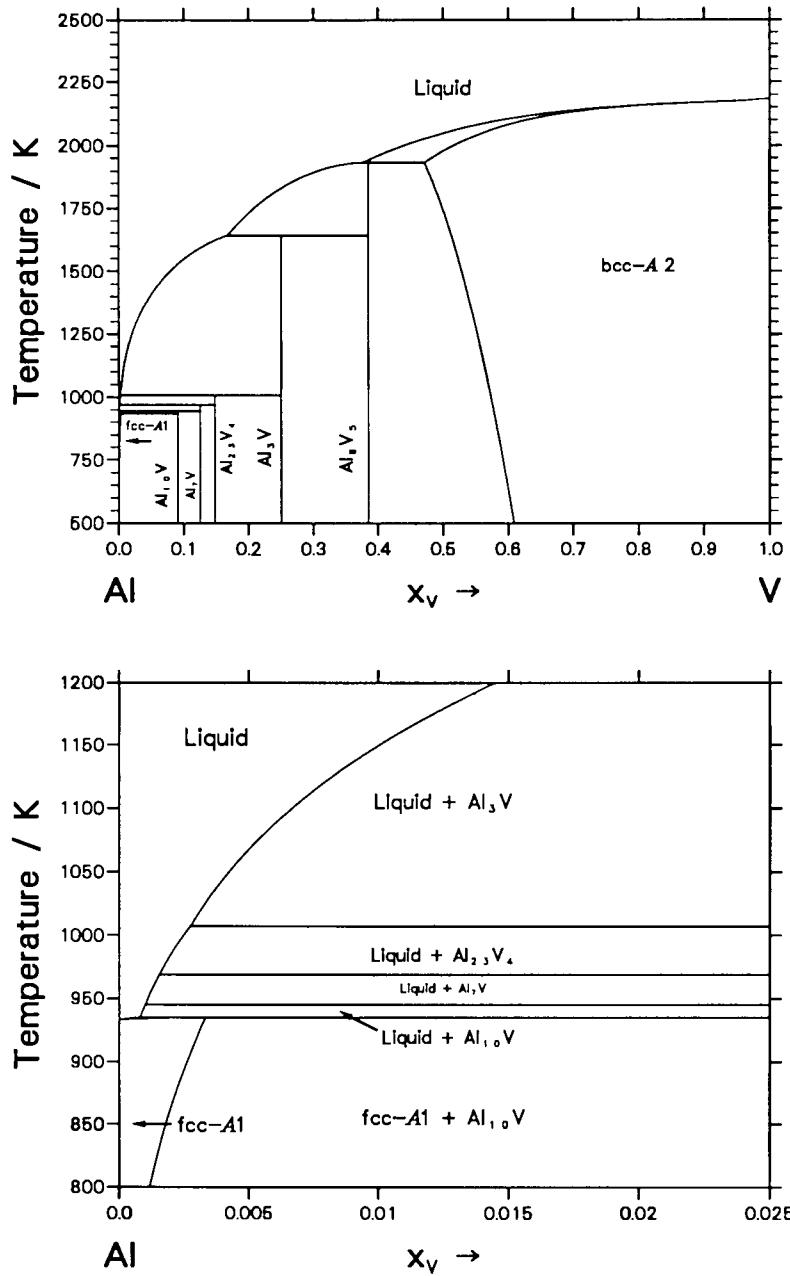


Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol	Symbol Group	Sub- lattices	Comments
Al-V	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M	4	
	(V)	W	<i>cI2</i> <i>I</i> $m\bar{3}m$	M	2	
	Al <sub>3</sub> V	Al <sub>3</sub> Ti	<i>tI8</i> <i>I</i> <sub>4</sub> /mmm	Al <sub>1</sub> Al <sub>2</sub> V	2 4 2	AlM-D0 <sub>22</sub>
	Al <sub>8</sub> V <sub>5</sub>	Cu <sub>5</sub> Zn <sub>8</sub>	<i>cI52</i> <i>I</i> <sub>4</sub> $\bar{3}m$	A <sub>1</sub> M <sub>1</sub> M <sub>2</sub> V	24 8 12 8	
	Al <sub>21</sub> V <sub>2</sub>	Al <sub>21</sub> V <sub>2</sub>	<i>cF176</i> <i>Fd</i> $\bar{3}m$	Al <sub>1</sub> Al <sub>2</sub> Al <sub>3</sub> V	16 48 96 16	described as Al <sub>10</sub> V
	Al <sub>23</sub> V <sub>4</sub>	Al <sub>23</sub> V <sub>4</sub>	<i>hP54</i> <i>P</i> <sub>6</sub> $_3/mmc$			
	Al <sub>45</sub> V <sub>7</sub>	Al <sub>45</sub> V <sub>7</sub>	<i>mC104</i> <i>C</i> <sub>2</sub> / <i>m</i>			described as Al <sub>7</sub> V
	AlV <sub>3</sub>	Cr <sub>3</sub> Si	<i>cP8</i> <i>Pm</i> $\bar{3}n$	Al V	2 6	A <sub>15</sub> stable?

# System Al-Y

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1, hcp-*A*3

**Compounds:**

Al<sub>3</sub>Y, Al<sub>2</sub>Y, AlY, Al<sub>2</sub>Y<sub>3</sub>, Al<sub>3</sub>Y<sub>5</sub>, AlY<sub>2</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Al <sub>3</sub> Y	:	Stoichiometric, (Al) <sub>3</sub> (Y)
Al <sub>2</sub> Y	:	Stoichiometric, (Al) <sub>2</sub> (Y)
AlY	:	Stoichiometric, (Al)(Y)
Al <sub>2</sub> Y <sub>3</sub>	:	Stoichiometric, (Al) <sub>2</sub> (Y) <sub>3</sub>
Al <sub>3</sub> Y <sub>5</sub>	:	Stoichiometric, (Al) <sub>3</sub> (Y) <sub>5</sub>
AlY <sub>2</sub>	:	Stoichiometric, (Al)(Y) <sub>2</sub>

**Assessor and Date:**

H.L. Lukas, 1993

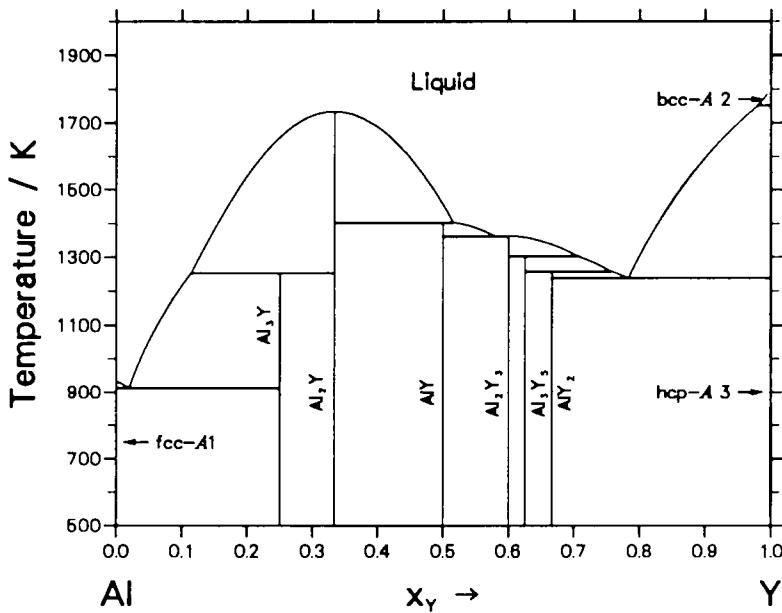
**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Al<sub>2</sub>Y**

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ, \text{fcc}-\text{A}1}(298.15 \text{ K}) - H_Y^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 246018.0 + 35.32809 \ T + 2.0 \ \text{GIISER}_{\text{Al}} + \text{GIISER}_Y$$

**Phase Al<sub>2</sub>Y<sub>3</sub>**

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ, \text{fcc}-\text{A}1}(298.15 \text{ K}) - 3.0 \ H_Y^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 373605.0 + 84.410 \ T + 2.0 \ \text{GIISER}_{\text{Al}} + 3.0 \ \text{GIISER}_Y$$



### Phase Al<sub>3</sub>Y

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Y}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 267460.0 + 46.48084 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Y}}$$

### Phase Al<sub>3</sub>Y<sub>5</sub>

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 5.0 \ H_{\text{Y}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 564479.2 + 127.7201 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + 5.0 \ \text{GHSER}_{\text{Y}}$$

### Phase AlY

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Y}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 173810.0 + 40.86834 \ T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Y}}$$

### Phase AlY<sub>2</sub>

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 2.0 \ H_{\text{Y}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 190908.0 + 44.38629 \ T + \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Y}}$$

**Phase bcc-A2**

$$L_{\text{Al,Y}:□}^{0,\text{bcc}-A2} = 90 \text{ } T$$

**Phase hcp-A3**

$$L_{\text{Al,Y}:□}^{0,\text{hcp}-A3} = 90 \text{ } T$$

**Phase liquid**

$$L_{\text{Al,Y}}^{0,\text{liquid}} = -202611.28 + 4.63942 \text{ } T$$

$$L_{\text{Al,Y}}^{1,\text{liquid}} = -54350.11 + 0.28402 \text{ } T$$

$$L_{\text{Al,Y}}^{2,\text{liquid}} = 83347.01 - 34.76401 \text{ } T$$

$$L_{\text{Al,Y}}^{3,\text{liquid}} = 15488.69 - 0.7988 \text{ } T$$

$$L_{\text{Al,Y}}^{4,\text{liquid}} = -51205.9 + 30.2161 \text{ } T$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_Y$			$T / K$
Liquid $\rightleftharpoons$ Al <sub>3</sub> Y + fcc-A1	Eutectic	.020	.000	.250	913.0
Liquid + Al <sub>2</sub> Y $\rightleftharpoons$ Al <sub>3</sub> Y	Peritectic	.114	.333	.250	1253.0
Liquid + Al <sub>2</sub> Y $\rightleftharpoons$ AlY	Peritectic	.516	.330	.500	1403.0
Liquid $\rightleftharpoons$ AlY + Al <sub>2</sub> Y <sub>3</sub>	Eutectic	.581	.500	.600	1361.2
Liquid + Al <sub>2</sub> Y <sub>3</sub> $\rightleftharpoons$ Al <sub>3</sub> Y <sub>5</sub>	Peritectic	.707	.600	.625	1302.5
Liquid + Al <sub>3</sub> Y <sub>5</sub> $\rightleftharpoons$ AlY <sub>2</sub>	Peritectic	.757	.625	.666	1258.0
Liquid $\rightleftharpoons$ AlY <sub>2</sub> + hcp-A3	Eutectic	.667	.783	1.000	1239.0
hcp-A3 $\rightleftharpoons$ bcc-A2	Allotropic	1.000	1.000	.....	1752.0
Liquid $\rightleftharpoons$ Al <sub>2</sub> Y	Congruent	.333	.333	.....	1734.0
Liquid $\rightleftharpoons$ Al <sub>2</sub> Y <sub>3</sub>	Congruent	.600	.600	.....	1364.0

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Y	(Al)	Cu	<i>cF4</i> <i>Fm3m</i>	M 4	
	(Y)	Mg	<i>hP2</i> <i>P63/mmc</i>	M 2	
	(Y)	W	<i>cI2</i> <i>Im3m</i>	M 4	
	Al <sub>3</sub> Y- $\alpha$	Ni <sub>3</sub> Sn	<i>hP8</i> <i>P63/mmc</i>	Al 6 Y 2	
	Al <sub>3</sub> Y- $\beta$	BaPb <sub>3</sub>	<i>hR12</i> <i>R3m</i>	Al <sub>1</sub> 9 Al <sub>2</sub> 18 Y <sub>1</sub> 3 Y <sub>2</sub> 6	
	Al <sub>2</sub> Y	Cu <sub>2</sub> Mg	<i>cF24</i> <i>Fd3m</i>	Al 16 Y 8	
	AlY	CrB	<i>oC8</i> <i>Cmcm</i>	Al 4 Y 4	
	Al <sub>2</sub> Y <sub>3</sub>	Al <sub>2</sub> Zr <sub>3</sub>	<i>tP20</i> <i>P42/mnm</i>	Al 8 Y <sub>1</sub> 4 Y <sub>2</sub> 4 Y <sub>3</sub> 4	
	AlY <sub>2</sub>	Co <sub>2</sub> Si	<i>oP12</i> <i>Pnma</i>	Al 4 Y <sub>1</sub> 4 Y <sub>2</sub> 4	
	AlY <sub>3</sub>	Al <sub>11</sub> Cu <sub>3</sub>	<i>cP4</i> <i>Pm3m</i>	Al 1	L1 <sub>2</sub>
	Al <sub>3</sub> Y <sub>5</sub>	Mn <sub>5</sub> Si <sub>3</sub>	<i>hP16</i> <i>P63/mcm</i>	Y 3	metastable impurity stabilized [91Vil]?

# System Al-W

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, fcc- <i>A</i> 1
(metastable)	bcc- <i>B</i> 2, hcp- <i>A</i> 3

**Compounds:**

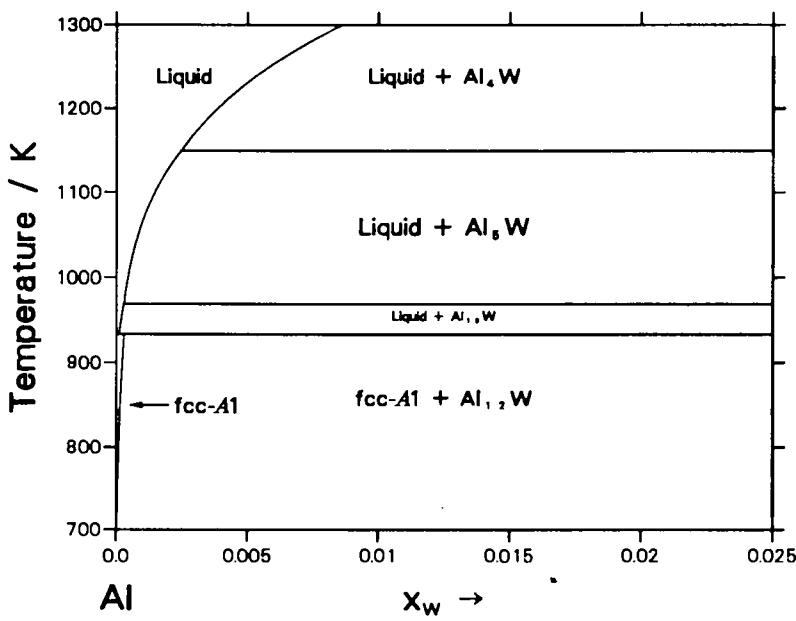
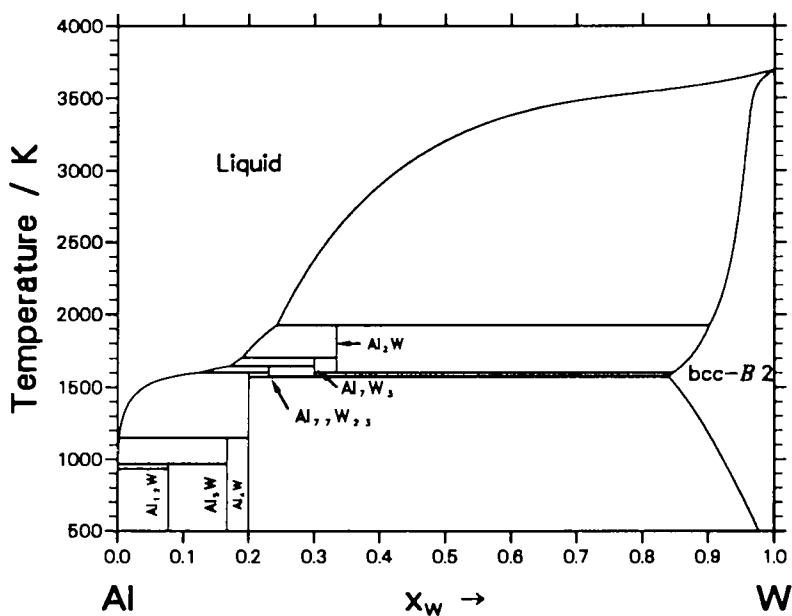
(stable)	Al <sub>12</sub> W, Al <sub>4</sub> W, Al <sub>5</sub> W, Al <sub>77</sub> W <sub>23</sub> , Al <sub>7</sub> W <sub>3</sub> , Al <sub>2</sub> W
(metastable)	AlM- <i>D</i> 0 <sub>19</sub> , AlTi- <i>L</i> 1 <sub>0</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Al <sub>12</sub> W	:	Stoichiometric, (Al) <sub>12</sub> (W)
Al <sub>5</sub> W	:	Stoichiometric, (Al) <sub>5</sub> (W)
Al <sub>4</sub> W	:	Stoichiometric, (Al) <sub>4</sub> (W)
Al <sub>77</sub> W <sub>23</sub>	:	Stoichiometric, (Al) <sub>77</sub> (W) <sub>23</sub>
Al <sub>7</sub> W <sub>3</sub>	:	Stoichiometric, (Al) <sub>7</sub> (W) <sub>3</sub>
cub- <i>A</i> 15	:	Stoichiometric, (Al)(W) <sub>3</sub>
Al <sub>2</sub> W	:	Sublattice model, (Al) <sub>2</sub> (W)
bcc- <i>B</i> 2	:	Sublattice model, (Al,W) <sub>0.5</sub> (AlW) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc- <i>A</i> 2 ⇌ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Al,W) <sub>3</sub> (Al,W)(□) <sub>0.5</sub>
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Al,W)(Al,W)

**Assessor and Date:**

N. Saunders, 1996.



**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)****Phase Al<sub>12</sub>W**

$$G^\circ(T) - 12.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ -62400 + 9.49 \ T + 12.0 \ \text{GIISER}_{\text{Al}} + \text{GIISER}_{\text{W}}$$

**Phase Al<sub>4</sub>W**

$$G^\circ(T) - 4.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ -57500 + 9.73 \ T + 4.0 \ \text{GIISER}_{\text{Al}} + \text{GIISER}_{\text{W}}$$

**Phase Al<sub>5</sub>W**

$$G^\circ(T) - 5.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ -58446 + 8.4 \ T + 5.0 \ \text{GIISER}_{\text{Al}} + \text{GIISER}_{\text{W}}$$

**Phase Al<sub>2</sub>W**

$$G^\circ(T) - 2.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ 13536 - 22.38 \ T + 2.0 \ \text{GIISER}_{\text{Al}} + \text{GIISER}_{\text{W}}$$

**Phase Al<sub>77</sub>W<sub>23</sub>**

$$G^\circ(T) - 77.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 23.0 \ H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ -189300 - 400 \ T + 77.0 \ \text{GHSER}_{\text{Al}} + 23.0 \ \text{GHSER}_{\text{W}}$$

**Phase Al<sub>7</sub>W<sub>3</sub>**

$$G^\circ(T) - 7.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 \ H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ 34700 - 70 \ T + 7.0 \ \text{GHSER}_{\text{Al}} + 3.0 \ \text{GHSER}_{\text{W}}$$

**Phase AlM-D0<sub>19</sub>**

$$G^\circ(T) - 4.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al}) = \\ 4.0 \ \text{GIICP}_{\text{Al}}$$

$$G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 \ H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{W:Al}) = \\ -12716 + 15.16 \ T + \text{GIICP}_{\text{Al}} + 3.0 \ \text{GIICP}_{\text{W}}$$

$$G^\circ(T) - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:W}) = \\ -12716 + 15.16 \ T + 3.0 \ \text{GIICP}_{\text{Al}} + \text{GIICP}_{\text{W}}$$

$$G^\circ(T) - 4.0 \ H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{W:W}) = \\ 4.0 \ \text{GIISER}_{\text{W}}$$

**Phase bcc-A2**

$$L_{\text{Al}, \text{W}: \square}^{0, \text{bcc}-A2} = -27000 + 25 T$$

$$L_{\text{Al}, \text{W}: \square}^{1, \text{bcc}-A2} = -10000$$

**Phase bcc-B2**

$$G^\circ(T) - H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{W}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) = G(\text{W:Al:}\square) = 1.0E-4$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{W}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:W:}\square) = 1.0E-4$$

$$G^\circ(T) - H_{\text{W}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) = G(\text{W:W:}\square) = 0.0$$

$$L_{\text{Al:Al}, \text{W}: \square}^{0, \text{bcc}-B2} = 1.0E-4$$

$$L_{\text{Al}, \text{W:Al}: \square}^{0, \text{bcc}-B2} = 1.0E-4$$

$$L_{\text{Al}, \text{W:Al}: \square}^{0, \text{bcc}-B2} = 1.0E-4$$

**Phase bcc-B2**

$$G_{\text{Al:W}: \square}^* = 1.0E-4$$

$$G^\circ(T) - H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) = G(\text{Al:Al:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{W}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:W:}\square) = 2.0 G_{\text{Al:W}: \square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{W}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) = G(\text{W:Al:}\square) = 2.0 G_{\text{Al:W}: \square}^*$$

$$G^\circ(T) - H_{\text{W}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) = G(\text{W:W:}\square) = 0.0$$

**Phase bcc-A2**

$$L_{\text{Al}, \text{W}: \square}^{0, \text{bcc}-A2} = -27000 + 25 T$$

$$L_{\text{Al}, \text{W}: \square}^{1, \text{bcc}-A2} = -10000$$

**Phase fcc-A1**

$$L_{\text{Al},\text{W};\square}^{0,\text{fcc}-A1} = -19250 + 20.2 T$$

$$L_{\text{Al},\text{W};\square}^{1,\text{fcc}-A1} = -10000$$

**Phase hcp-A3**

$$L_{\text{Al},\text{W};\square}^{0,\text{hcp}-A3} = -19250 + 20.2 T$$

$$L_{\text{Al},\text{W};\square}^{1,\text{hcp}-A3} = -10000$$

**Phase liquid**

$$L_{\text{Al},\text{W}}^{0,\text{liquid}} = -70000 + 35 T$$

$$L_{\text{Al},\text{W}}^{1,\text{liquid}} = 1.0E-4$$

$$L_{\text{Al},\text{W}}^{2,\text{liquid}} = 15000$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $z_W$			$T / K$
$\text{Al}_2\text{W} \rightleftharpoons \text{Al}_7\text{W}_3 + \text{bcc}-A2$	Eutectoid	.333	.300	.847	1602.6
Liquid + $\text{Al}_2\text{W} \rightleftharpoons \text{Al}_7\text{W}_3$	Peritectic	.190	.333	.300	1706.8
Liquid + $\text{bcc}-A2 \rightleftharpoons \text{Al}_2\text{W}$	Peritectic	.243	.901	.333	1925.7
Liquid + $\text{Al}_7\text{W}_3 \rightleftharpoons \text{Al}_{77}\text{W}_{23}$	Peritectic	.172	.300	.230	1648.2
Liquid + $\text{Al}_{77}\text{W}_{23} \rightleftharpoons \text{Al}_4\text{W}$	Peritectic	.125	.230	.200	1604.1
$\text{Al}_{77}\text{W}_{23} \rightleftharpoons \text{Al}_4\text{W} + \text{bcc}-A2$	Eutectoid	.023	.200	.840	1571.0
$\text{Al}_{77}\text{W}_{23} + \text{bcc}-A2 \rightleftharpoons \text{Al}_7\text{W}_3$	Eutectoid	.230	.841	.300	1580.0
Liquid + $\text{Al}_4\text{W} \rightleftharpoons \text{Al}_5\text{W}$	Peritectic	.0025	.200	.167	1149.6
Liquid + $\text{Al}_5\text{W} \rightleftharpoons \text{Al}_{12}\text{W}$	Peritectic	.0003	.167	.077	969.4
Liquid + $\text{Al}_{12}\text{W} \rightleftharpoons \text{fcc}-A$	Peritectic	.0002	.077	.0003	933.6
$\text{Al}_8\text{W}_3 \rightleftharpoons \text{Liquid}$	Congruent	.273	.273	...	1850.5

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-W	(Al)	Cu	<i>cF4</i> <i>Fm3m</i>	M 4	
	(W)	W	<i>cI2</i> <i>Im3m</i>	M 2	
	Al <sub>12</sub> W	Al <sub>12</sub> W	<i>cl26</i> <i>Im3</i>	Al 24 W 2	
	Al <sub>5</sub> W	Al <sub>5</sub> W	<i>hP12</i> <i>P63</i>		
	Al <sub>4</sub> W	Al <sub>4</sub> W	<i>mC30</i> <i>Cm</i>	Al <sub>1</sub> 2 Al <sub>2</sub> 2 W <sub>1</sub> 2 Al <sub>3</sub> 4 Al <sub>4</sub> 4 Al <sub>5</sub> 4 Al <sub>6</sub> 4 Al <sub>7</sub> 4 W <sub>2</sub> 4	
	Al <sub>2</sub> W				not quoted in [Mas1] nor in [Vill]
	Al <sub>7</sub> W <sub>3</sub>				not quoted in [Mas1] nor in [Vill]
	Al <sub>77</sub> W <sub>23</sub>				not quoted in [Mas1] nor in [Vill]

# System Al-Zn

**Solution Phases:**

(stable)	Liquid, fcc-A1, hcp-Zn
(metastable)	hcp-A3

**Compounds:**

(metastable)	AlCu- $\eta$ , Laves-C14
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**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister
AlCu- $\eta$	:	Stoichiometric, (Al)(Zn)
Laves-C14	:	Sublattice model, (Al,Zn) <sub>2</sub> (Al,Zn)

**Assessor and Date:**

S. an Mey (1991)

**Publication:**

Z. für Metallkde, 84, 7, 451-455 (1993).

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase fcc-A1**

$$f_{\text{Al}, \text{Zn}: \square}^{0, \text{fcc}-\text{A1}} = 7297.48 + 0.47512 \cdot T$$

$$f_{\text{Al}, \text{Zn}: \square}^{1, \text{fcc}-\text{A1}} = 6612.88 - 4.59110 \cdot T$$

$$f_{\text{Al}, \text{Zn}: \square}^{2, \text{fcc}-\text{A1}} = -3097.19 + 3.30635 \cdot T$$

**Phase hcp-A3**

$$L_{\text{Al}, \text{Zn}: \square}^{0, \text{hcp}-\text{A3}} = 18820.95 - 8.95255 \cdot T$$

$$L_{\text{Al}, \text{Zn}: \square}^{1, \text{hcp}-\text{A3}} = 1.0 \text{E-}6$$

$$L_{\text{Al}, \text{Zn}: \square}^{2, \text{hcp}-\text{A3}} = 1.0 \text{E-}6$$

$$L_{\text{Al}, \text{Zn}: \square}^{3, \text{hcp}-\text{A3}} = -702.79$$

**Phase hcp-Zn**

$$L_{\text{Al}, \text{Zn}: \square}^{0, \text{hcp}-\text{Zn}} = 18820.95 - 8.95255 \cdot T$$

$$L_{\text{Al}, \text{Zn}: \square}^{1, \text{hcp}-\text{Zn}} = 1.0 \text{E-}6$$

$$L_{\text{Al}, \text{Zn}: \square}^{2, \text{hcp}-\text{Zn}} = 1.0 \text{E-}6$$

$$L_{\text{Al}, \text{Zn}: \square}^{3, \text{hcp}-\text{Zn}} = -702.79$$

**Phase AlCu- $\eta$** 

$$\begin{aligned} G^\circ(T) - H_{\text{Cu}}^{\circ, \text{fcc}-\text{A1}}(298.15 \text{K}) - H_{\text{Zn}}^{\circ, \text{hcp}-\text{Zn}}(298.15 \text{ K}) = \\ 15000.0 + \text{GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Zn}} \end{aligned}$$

**Phase Laves-C14**

$$\begin{aligned} G^\circ(T) - 3.0 \cdot H_{\text{Cu}}^{\circ, \text{fcc}-\text{A1}}(298.15 \text{K}) = \text{G(Al:Al)} = \\ 15000.0 + 3.0 \cdot \text{GHSER}_{\text{Cu}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 2.0 \cdot H_{\text{Cu}}^{\circ, \text{fcc}-\text{A1}}(298.15 \text{K}) - H_{\text{Zn}}^{\circ, \text{hcp}-\text{Zn}}(298.15 \text{ K}) = \text{G(Al:Zn)} = \\ 15000.0 + 2.0 \cdot \text{GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Zn}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - H_{\text{Cu}}^{\circ, \text{fcc}-\text{A1}}(298.15 \text{K}) - 2.0 \cdot H_{\text{Zn}}^{\circ, \text{hcp}-\text{Zn}}(298.15 \text{ K}) = \text{G(Zn:Al)} = \\ 15000.0 + \text{GHSER}_{\text{Cu}} + 2.0 \cdot \text{GHSER}_{\text{Zn}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 3.0 \cdot H_{\text{Zn}}^{\circ, \text{hcp}-\text{Zn}}(298.15 \text{ K}) = \text{G(Zn:Zn)} = \\ 15000.0 + 3.0 \cdot \text{GHSER}_{\text{Zn}} \end{aligned}$$

$$L_{\text{Al:Al}, \text{Zn}: \square}^{0, \text{Laves}-\text{C14}} = L_{\text{Zn:Al}, \text{Zn}: \square}^{0, \text{Laves}-\text{C14}} = -7500 - 18 \cdot T$$

**Phase liquid**

$$L_{\text{Al}, \text{Zn}}^{0, \text{liquid}} = 10465.55 - 3.39259 \cdot T$$

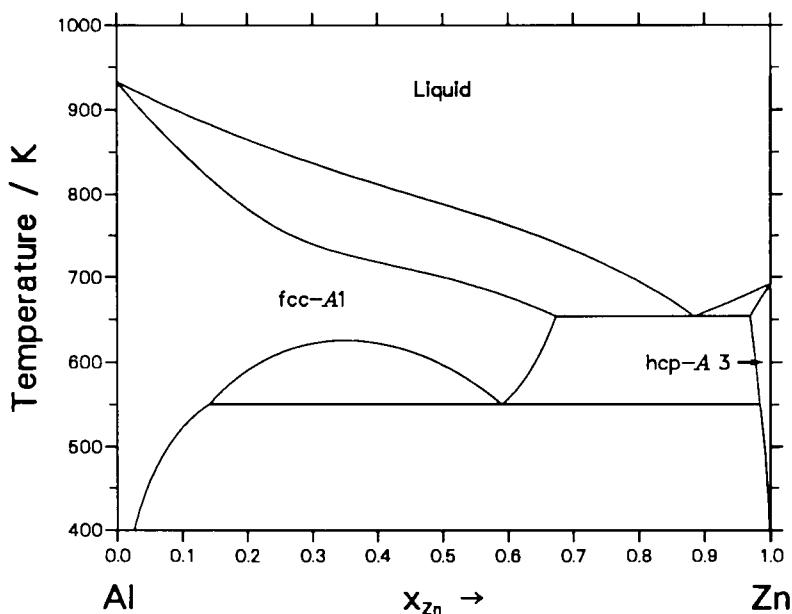


Table I - Invariant Reactions.

Reaction	Type	Compositions \$x_{\text{Zn}}	\$T / \text{K}
$\text{Liquid} \rightleftharpoons \text{fcc}-\text{Al} + \text{hcp}-\text{A3}$	Eutectic	.884 .673 .969	654.0
$\text{fcc}-\text{Al}' \rightleftharpoons \text{fcc}-\text{Al}'' + \text{hcp}-\text{A3}$	Monotectic	.590 .141 .984	550.4

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol Group
Al-Zn	(Al) (Zn)	Cu Mg	$cF\bar{4}$ $Fm\bar{3}m$ $hP2$ $P6_3/mmc$

# System Al-Zr

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1, hcp-*A*3

**Compounds:**

Al<sub>2</sub>Zr, Al<sub>2</sub>Zr<sub>3</sub>, Al<sub>3</sub>Zr, Al<sub>3</sub>Zr<sub>2</sub>, Al<sub>3</sub>Zr<sub>5</sub>,  
Al<sub>4</sub>Zr<sub>5</sub>, AlZr, AlZr<sub>2</sub>, AlZr<sub>3</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Al <sub>2</sub> Zr	:	Stoichiometric, (Al) <sub>2</sub> (Zr)
Al <sub>2</sub> Zr <sub>3</sub>	:	Stoichiometric, (Al) <sub>2</sub> (Zr) <sub>3</sub>
Al <sub>3</sub> Zr	:	Stoichiometric, (Al) <sub>3</sub> (Zr)
Al <sub>3</sub> Zr <sub>2</sub>	:	Stoichiometric, (Al) <sub>3</sub> (Zr) <sub>2</sub>
Al <sub>3</sub> Zr <sub>5</sub>	:	Stoichiometric, (Al) <sub>3</sub> (Zr) <sub>5</sub>
Al <sub>4</sub> Zr <sub>5</sub>	:	Stoichiometric, (Al) <sub>4</sub> (Zr) <sub>5</sub>
AlZr	:	Stoichiometric, (Al)(Zr)
AlZr <sub>2</sub>	:	Stoichiometric, (Al)(Zr) <sub>2</sub>
AlZr <sub>3</sub>	:	Stoichiometric, (Al)(Zr) <sub>3</sub>

**Assessor and Date:**

N. Saunders (1991)

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Al<sub>2</sub>Zr**

$$G^\circ T - 2.0 \ H_{\text{Al}}^{\circ, \text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 137430.0 + 25.44 \ T + 2.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Zr}}$$

**Phase Al<sub>2</sub>Zr<sub>3</sub>**

$$G^\circ T - 2.0 \ H_{\text{Al}}^{\circ, \text{fcc}-\text{A}1}(298.15 \text{ K}) - 3.0 \ H_{\text{Zr}}^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 192135.0 + 33.0 \ T + 2.0 \ \text{GHSER}_{\text{Al}} + 3.0 \ \text{GHSER}_{\text{Zr}}$$

**Phase Al<sub>3</sub>Zr**

$$G^\circ T - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 162500.0 + 28.92 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Zr}}$$

**Phase Al<sub>3</sub>Zr<sub>2</sub>**

$$G^\circ T - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 \ H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 234700.0 + 44.1 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Zr}}$$

**Phase Al<sub>3</sub>Zr<sub>5</sub>**

$$G^\circ T - 3.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 5.0 \ H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 217488.0 + 48.72 \ T + 3.0 \ \text{GHSER}_{\text{Al}} + 5.0 \ \text{GHSER}_{\text{Zr}}$$

**Phase Al<sub>4</sub>Zr<sub>5</sub>**

$$G^\circ T - 4.0 \ H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 5.0 \ H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 369000.0 + 62.55 \ T + 4.0 \ \text{GHSER}_{\text{Al}} + 5.0 \ \text{GHSER}_{\text{Zr}}$$

**Phase AlZr**

$$G^\circ T - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 89000.0 + 17.0384 \ T + \text{GHSER}_{\text{Al}} + \text{GHSER}_{\text{Zr}}$$

**Phase AlZr<sub>2</sub>**

$$G^\circ T - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 \ H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 100125.0 + 17.553 \ T + \text{GHSER}_{\text{Al}} + 2.0 \ \text{GHSER}_{\text{Zr}}$$

**Phase AlZr<sub>3</sub>**

$$G^\circ T - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 \ H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 108000.0 + 22.38 \ T + \text{GHSER}_{\text{Al}} + 3.0 \ \text{GHSER}_{\text{Zr}}$$

**Phase bcc-A2**

$$L_{\text{Al},\text{Zr}:□}^{0,\text{bcc}-A2} = - 122300 + 32 \ T$$

$$L_{\text{Al},\text{Zr}:□}^{1,\text{bcc}-A2} = - 11000$$

$$L_{\text{Al},\text{Zr}:□}^{2,\text{bcc}-A2} = 15000$$

**Phase fcc-A1**

$$L_{\text{Al,Zr}:□}^{0,\text{fcc}-A1} = -120000 + 30 \cdot T$$

$$L_{\text{Al,Zr}:□}^{1,\text{fcc}-A1} = -10000$$

$$L_{\text{Al,Zr}:□}^{2,\text{fcc}-A1} = 15000$$

**Phase hcp-A3**

$$L_{\text{Al,Zr}:□}^{0,\text{hcp}-A3} = -122300 + 32 \cdot T$$

$$L_{\text{Al,Zr}:□}^{1,\text{hcp}-A3} = -8000$$

$$L_{\text{Al,Zr}:□}^{2,\text{hcp}-A3} = 17000$$

**Phase liquid**

$$L_{\text{Al,Zr}}^{0,\text{liquid}} = -125000 + 35 \cdot T$$

$$L_{\text{Al,Zr}}^{1,\text{liquid}} = -10000 + 5.57 \cdot T$$

$$L_{\text{Al,Zr}}^{2,\text{liquid}} = 15750$$

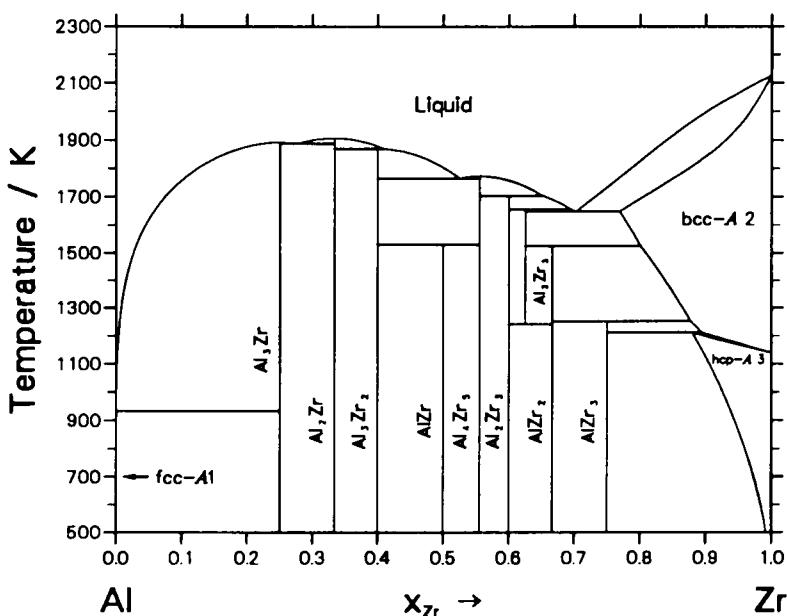


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Zr}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ fcc-Al + Al <sub>3</sub> Zr	Peritectic	.0002	.0008	.250	933.8
Al <sub>3</sub> Zr $\rightleftharpoons$ Liquid	Congruent	.250	.250	...	1893.0
Liquid $\rightleftharpoons$ Al <sub>3</sub> Zr + Al <sub>2</sub> Zr	Eutectic	.277	.250	.333	1888.0
Al <sub>2</sub> Zr $\rightleftharpoons$ Liquid	Congruent	.333	.333	...	1907.0
Liquid + Al <sub>2</sub> Zr $\rightleftharpoons$ Al <sub>3</sub> Zr <sub>2</sub>	Peritectic	.410	.333	.400	1869.1
Liquid $\rightleftharpoons$ Al <sub>3</sub> Zr <sub>2</sub> + Al <sub>4</sub> Zr <sub>5</sub>	Eutectic	.525	.400	.556	1765.3
Al <sub>4</sub> Zr <sub>5</sub> $\rightleftharpoons$ Liquid	Congruent	.555	.555	...	1773.0
Liquid + Al <sub>4</sub> Zr <sub>5</sub> $\rightleftharpoons$ Al <sub>2</sub> Zr <sub>3</sub>	Peritectic	.653	.556	.600	1701.8
Liquid + Al <sub>2</sub> Zr <sub>3</sub> $\rightleftharpoons$ Al <sub>3</sub> Zr <sub>5</sub>	Peritectic	.696	.600	.625	1655.8
Liquid $\rightleftharpoons$ Al <sub>3</sub> Zr <sub>5</sub> + bcc-A2	Eutectic	.702	.625	.768	1648.7
Al <sub>2</sub> Zr <sub>3</sub> + bcc-A2 $\rightleftharpoons$ AlZr <sub>2</sub>	Peritectoid	.600	.801	.666	1524.2
Al <sub>3</sub> Zr <sub>5</sub> $\rightleftharpoons$ Al <sub>2</sub> Zr <sub>3</sub> + AlZr <sub>2</sub>	Eutectoid	.625	.600	.666	1241.7
AlZr <sub>2</sub> + bcc-A2 $\rightleftharpoons$ AlZr <sub>3</sub>	Peritectoid	.667	.877	.750	1252.3
AlZr <sub>3</sub> + bcc-A2 $\rightleftharpoons$ hcp-A3	Peritectoid	.750	.894	.879	1212.2
Al <sub>3</sub> Zr <sub>2</sub> + Al <sub>4</sub> Zr <sub>5</sub> $\rightleftharpoons$ AlZr	Peritectoid	.400	.556	.500	1529.5

Table II:a - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Zr	(Al)	Cu	cF4 <i>Fm</i> 3 <i>m</i>	M 4	
	(Zr)	Mg	hP2 <i>P</i> 63/ <i>mmc</i>	M 2	
	(Zr)	W	cI2 <i>I</i> m3 <i>m</i>	M 4	
	AlZr	BCr	oC8 <i>C</i> mcm	Al 4 Zr 4	
	AlZr <sub>2</sub>	InNi <sub>2</sub>	hP6 <i>P</i> 63/ <i>mmc</i>	Al 2 Zr <sub>1</sub> 2 Zr <sub>2</sub> 4	

Table II:b - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol	Symbol Group	Sub- lattices	Comments
	AlZr <sub>3</sub>	AuCu <sub>3</sub>	<i>cP4</i> <i>Pm</i> <sup>3</sup> <i>m</i>		Al 1 Zr 3	
	Al <sub>2</sub> Zr	MgZn <sub>2</sub>	<i>hP12</i> <i>P6</i> <sub>3</sub> /mmc			
	Al <sub>2</sub> Zr <sub>3</sub>	Al <sub>2</sub> Zr <sub>3</sub>	<i>tP20</i> <i>P4</i> <sub>2</sub> /mnmm		Al 8 Zr <sub>1</sub> 4 Zr <sub>2</sub> 4 Zr <sub>3</sub> 4	
	Al <sub>3</sub> Zr	Al <sub>3</sub> r	<i>tI16</i> <i>I</i> <sub>4</sub> /mmm		Al <sub>1</sub> 4 Al <sub>2</sub> 4 Al <sub>3</sub> 4 Zr 4	
	Al <sub>3</sub> Zr <sub>2</sub>	Al <sub>3</sub> Zr <sub>2</sub>	<i>oF40</i> <i>Fdd</i> 2		Al <sub>1</sub> 8 Al <sub>2</sub> 16 Al <sub>3</sub> 16	
	Al <sub>3</sub> Zr <sub>4</sub>	Al <sub>3</sub> Zr <sub>4</sub>	<i>hP7</i> <i>P</i> <sub>6</sub>		Al 3 Zr <sub>1</sub> 1 Zr <sub>2</sub> 1 Zr <sub>3</sub> 2	
	Al <sub>3</sub> Zr <sub>5</sub>	Mn <sub>5</sub> Si <sub>3</sub>	<i>hP16</i> <i>P6</i> <sub>3</sub> /mcmm		Al 6 Zr <sub>1</sub> 4 Zr <sub>2</sub> 6	not in Masl
	Al <sub>3</sub> Zr <sub>5</sub>	Si <sub>3</sub> W <sub>5</sub>	<i>tI32</i> <i>I</i> <sub>4</sub> /mcmm		Al <sub>1</sub> 4 Al <sub>1</sub> 8 Zr <sub>1</sub> 4 Zr <sub>2</sub> 16	
	Al <sub>4</sub> Zr <sub>5</sub>	Ga <sub>4</sub> Ti <sub>5</sub>	<i>hP18</i> <i>P6</i> <sub>3</sub> /mcmm		Al <sub>1</sub> 2 Al <sub>2</sub> 6 Zr <sub>1</sub> 4 Zr <sub>2</sub> 6	not in Masl

# System B-C

**Solution Phases:**

Liquid, graphite,  $\beta$ -rhombo-B,  $B_4C$

**Modelling:**

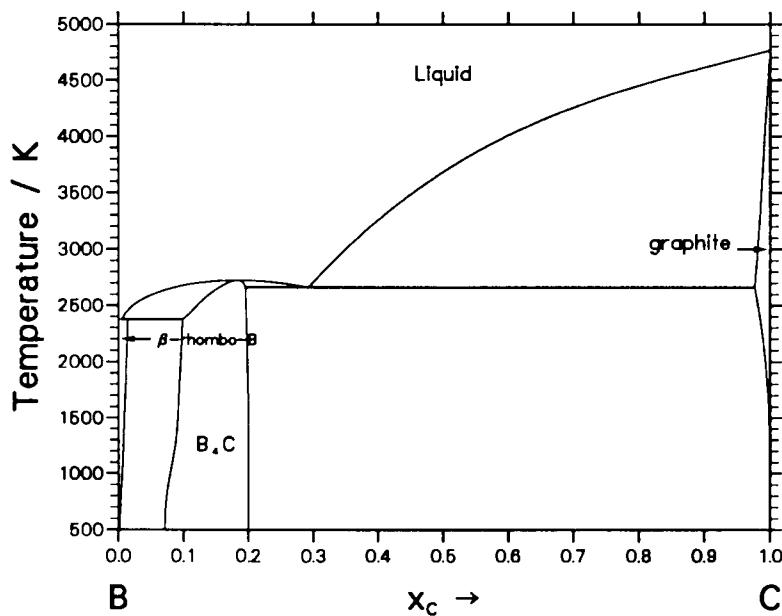
Liquid	:	Substitutional, Redlich-Kister
graphite	:	Substitutional, Redlich-Kister
$\beta$ -rhombo-B	:	Sublattice model $(B)_{93}(B,C)_{12}$
$B_4C$	:	Sublattice model $(B_{11},B_{12})(B_2,C_2B,CB_2)$

**Assessor and Date:**

B. Kasper, H.L. Lukas, (1992).

**Publication:**

B. Kasper, Thesis, Univ. Stuttgart (Germany).



### Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)

#### Phase B<sub>4</sub>C

$$G^\circ(T) - 13.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - H_C^{\circ,\text{graphite}}(298.15 \text{ K}) = G(B_{11}:B_2) = \\ -170978.12 + 22.909095 \ T + 16.0 \ \text{GHSER}_B + \text{GHSER}_C$$

$$G^\circ(T) - 14.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) = G(B_{12}:B_2) = \\ 10000 + 22.909095 \ T + 14.0 \ \text{GHSER}_B$$

$$G^\circ(T) - 12.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - 3.0 \ H_C^{\circ,\text{graphite}}(298.15 \text{ K}) = G(B_{11}:C_2B) = \\ -347121.82 + 22.909095 \ T + 12.0 \ \text{GHSER}_B + 3.0 \ \text{GHSER}_C$$

$$G^\circ(T) - 13.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - 2.0 \ H_C^{\circ,\text{graphite}}(298.15 \text{ K}) = G(B_{12}:C_2B) = \\ -294040.52 + 22.909095 \ T + 13.0 \ \text{GHSER}_B + 2.0 \ \text{GHSER}_C$$

$$G^\circ(T) - 13.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - 2.0 \ H_C^{\circ,\text{graphite}}(298.15 \text{ K}) = G(B_{11}:CB_2) = \\ -304040.52 + 22.909095 \ T + 13.0 \ \text{GHSER}_B + 2.0 \ \text{GHSER}_C$$

$$G^\circ(T) - 14.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - H_C^{\circ,\text{graphite}}(298.15 \text{ K}) = G(B_{12}:CB_2) = \\ -169978.12 + 22.909095 \ T + 14.0 \ \text{GHSER}_B + \text{GHSER}_C$$

$$L_{B_{11}C,B_{12}:B_2}^{0,B_4C} = 1.0E-4$$

#### Phase β-rhombo-B

$$G^\circ(T) - 105.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) = G(B:B) = \\ 105 \ \text{GHSER}_B$$

$$G^\circ(T) - 93.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - 12.0 \ H_C^{\circ,\text{graphite}}(298.15 \text{ K}) = G(B:C) = \\ 1000000 + 93.0 \ \text{GHSER}_B + 12.0 \ \text{GHSER}_C$$

$$L_{B:B,C}^{0,\beta-\text{rhombo-B}} = -2769690.3$$

#### Phase graphite

$$L_{B,C}^{0,\text{graphite}} = 34385.95 + 8.6792 \ T$$

#### Phase liquid

$$L_{B,C}^{0,\text{liquid}} = -67045.16 + 4.46969 \ T$$

$$L_{B,C}^{1,\text{liquid}} = -36682.57 + 2.44551 \ T$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_C$			$T / K$
Liquid $\rightleftharpoons$ B <sub>4</sub> C + graphite	Eutectic	.292	.195	.977	2663.4
Liquid + B <sub>4</sub> C $\rightleftharpoons$ $\beta$ -rhombo-B	Peritectic	.0056	.099	.010	2375.9
B <sub>4</sub> C $\rightleftharpoons$ Liquid	Congruent	.184	.184	....	2725.3

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
B-C	(B) (C) B <sub>4</sub> C	$\beta$ -rhombo-B graphite B <sub>4</sub> C	$hR15$ $R\bar{3}m$	B <sub>1</sub> 3 B <sub>2</sub> 18 B <sub>3</sub> 18 C 6	B <sub>13</sub> C <sub>2</sub> in [91Vil]

# System B–Hf

**Solution Phases:**

Liquid, bcc-*A*2, hcp-*A*3

**Compounds:**

(stable) BHf, B<sub>2</sub>Hf  
(metastable) B<sub>4</sub>Hf<sub>3</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
BHf	:	Stoichiometric, (B)(Hf)
B <sub>2</sub> Hf	:	Stoichiometric, (B) <sub>2</sub> (Hf)
B <sub>4</sub> Hf <sub>3</sub>	:	Stoichiometric, (B) <sub>4</sub> (Hf) <sub>3</sub>

**Assessor and Date:**

II. Bitterman, Univ. Vienna, Austria

**Thermodynamic properties of the solution and compound phases (J·mol<sup>-1</sup>)**

**Phase BHf**

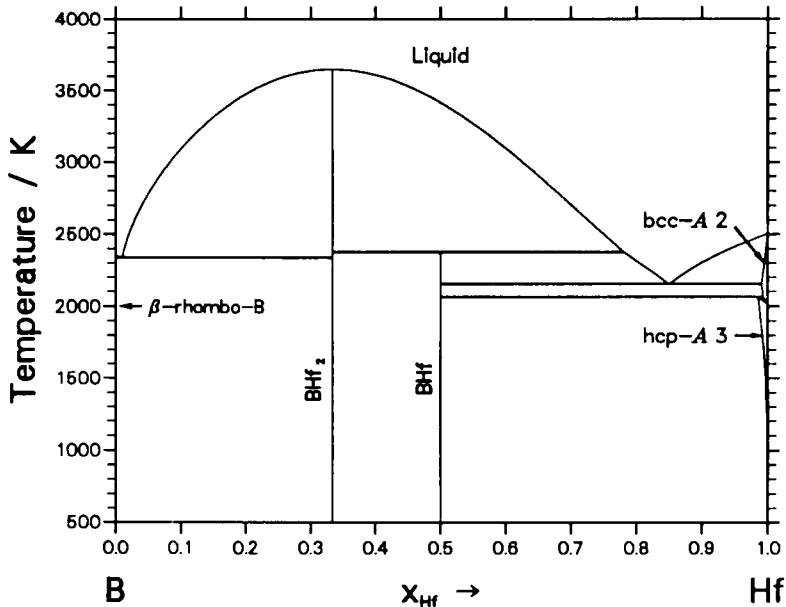
$$G^\circ(T) - H_B^{\circ,\beta-\text{rhombo}-\text{B}}(298.15\text{K}) - H_{\text{Hf}}^{\circ,\text{hcp}-\text{A}3}(298.15\text{K}) = \\ -159810 + 4.98602 \cdot T + \text{GIISER}_\text{B} + \text{GIISER}_\text{Hf}$$

**Phase B<sub>4</sub>Hf<sub>3</sub>**

$$G^\circ(T) - 4.0 \cdot H_B^{\circ,\beta-\text{rhombo}-\text{B}}(298.15\text{K}) - 3.0 \cdot H_{\text{Hf}}^{\circ,\text{hcp}-\text{A}3}(298.15\text{K}) = \\ -535000 - 14.5754 \cdot T + 4.0 \cdot \text{GIISER}_\text{B} + 3.0 \cdot \text{GIISER}_\text{Hf}$$

**Phase B<sub>2</sub>Hf**

$$G^\circ(T) - 2.0 \cdot H_B^{\circ,\beta-\text{rhombo}-\text{B}}(298.15\text{K}) - H_{\text{Hf}}^{\circ,\text{hcp}-\text{A}3}(298.15\text{K}) = \\ -351445 + 469.146 \cdot T - 73.868 \cdot T \cdot \ln T - 0.0036789 \cdot T^2 \\ + 1517800 \cdot T^{-1} - 5.2E+09T^{-3}$$



### Phase bcc-A2

$$\begin{aligned}
 G^\circ(T) - 3.0 H_B^{\circ,\beta-\text{rhombo}-B}(298.15\text{K}) - H_{\text{Hf}}^{\circ,\text{hcp}-A3}(298.15\text{K}) = \\
 - 137926 + 3.0 \text{ GIISER}_B + \text{GHSER}_{\text{Hf}} \\
 L_{\text{Hf};B,\square}^{0,\text{bcc}-A2} = 1.0E-4
 \end{aligned}$$

### Phase hcp-A3

$$\begin{aligned}
 G^\circ(T) - 0.5 H_B^{\circ,\beta-\text{rhombo}-B}(298.15\text{K}) - H_{\text{Hf}}^{\circ,\text{hcp}-A3}(298.15\text{K}) = \\
 - 44765.7 + 0.5 \text{ GIISER}_B + \text{GHSER}_{\text{Hf}} \\
 L_{\text{Hf};B,\square}^{0,\text{hcp}-A3} = 1.0E-4
 \end{aligned}$$

### Phase liquid

$$L_{\text{B},\text{Hf}}^{0,\text{liquid}} = - 170625 - 4.85541 T$$

$$L_{\text{B},\text{Hf}}^{1,\text{liquid}} = - 39128$$

$$L_{\text{B},\text{Hf}}^{2,\text{liquid}} = 16331.1$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Hf}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ $\beta$ -rhombo-B + $\text{B}_2\text{Hf}$	Eutectic	.010	.000	.333	2337.9
Liquid + $\text{B}_2\text{Hf} \rightleftharpoons$ + $\text{BHf}$	Peritectic	.780	.333	.500	2377.1
Liquid $\rightleftharpoons$ $\text{BHf}$ + bcc-A2	Eutectic	.850	.500	.990	2153.6
bcc-A2 + $\text{BHf} \rightleftharpoons$ hcp-A3	Peritectic	.993	.500	.985	2063.8
$\text{B}_2\text{Hf} \rightleftharpoons$ Liquid	Congruent	.333	.333	.....	3650.0

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
B-Hf	(B)	$\beta$ -rhombo-B	$hP2$ $P6_3/mmc$	M 2	(metastable)
	(Hf)	Mg			
	(Hf)	W	$cI2$ $Im\bar{3}m$	M 2	
	BHf	BFe	$oP8$ $Pnma$	B 4 Hf 4	
	$\text{B}_2\text{Hf}$	$\text{AlB}_2$	$hP3$ $P6/mmm$	B 2 Hf 1	
	$\text{B}_4\text{Hf}_3$	$\text{B}_4\text{Ta}_3$	$oI14$ $Immm$		

# System B-N

Solution Phases:

Liquid, gas

Compound:

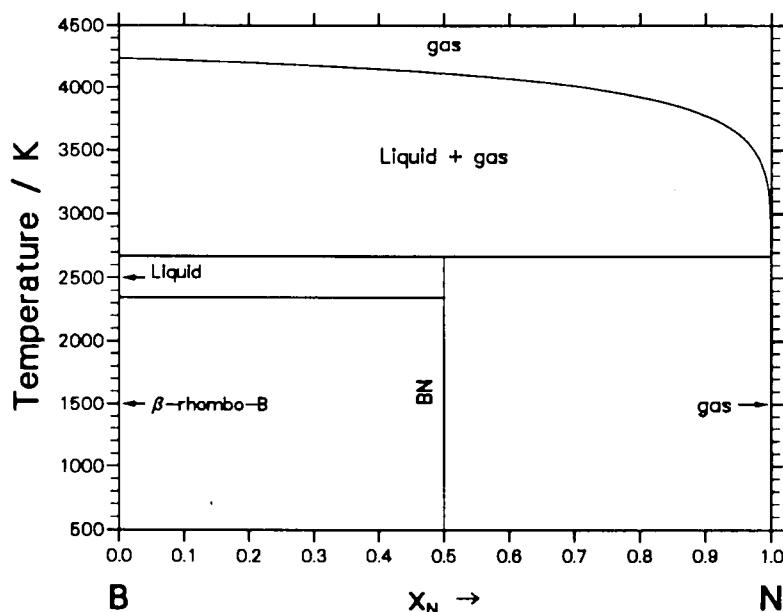
BN

Modelling:

Liquid	:	Substitutional, Redlich-Kister
gas	:	ideal (B,B <sub>2</sub> ,N,N <sub>2</sub> ,N <sub>3</sub> ,BN)
BN	:	Stoichiometric (B)(N)

Assessor and Date:

H. Wen, and H.L. Lukas 1992



Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**Phase BN**

$$G^\circ(T) - H_B^{\circ,\beta-\text{rhombo}-\text{B}}(298.15 \text{ K}) - H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) = \\ - 250600 + 91.281942 T + \text{GHSER}_B + \text{GHSER}_N$$

**Phase liquid**

$$L_{\text{B},\text{N}}^{0,\text{liquid}} = 30000.0 - 4.0 T$$

**Phase gas(B,B<sub>2</sub>,N,N<sub>2</sub>,N<sub>3</sub>,BN) (P = 0.1 MPa)**

$$G_B^{\circ,\text{gas}}(T) - H_B^{\circ,\beta-\text{rhombo}-\text{B}} = R T \ln P + \\ \begin{aligned} 298.15 < T < 700.00 : & 564913.402 - 13.9693124 T \\ & + 1.6646044E-05 T^2 - 20.80858 T \cdot \ln T \\ 700.00 < T < 2800.00 : & 564920.973 - 14.1156663 T - 20.786112 T \cdot \ln T \\ 2800.00 < T < 4075.00 : & 565086.023 - 15.0515115 T - 20.6682069 T \cdot \ln T \\ & - 2.10566E-05 T^2 \end{aligned}$$

$$G_{\text{B}_2}^{\circ,\text{gas}}(T) - 2.0 H_B^{\circ,\beta-\text{rhombo}-\text{B}} = R T \ln P + \\ \begin{aligned} 298.15 < T < 550.00 : & 824867.604 - 125.766398 T - 8.168 T \cdot \ln T \\ & - 0.0430888612 T^2 + 1.00098016E-05 T^3 \\ & - 136465.972 T^{-1} \\ 550.00 < T < 2150.00 : & 809306.765 + 132.643168 T - 48.851589 T \cdot \ln T \\ & + 0.00423205742 T^2 - 3.22751598E-07 T^3 \\ & + 980387.558 T^{-1} \\ 2150.00 < T < 6000.00 : & 826793.716 + 32.6504991 T - 35.6295549 T \cdot \ln T \\ & - 4.58209505E-04 T^2 + 1.70149264E-10 T^3 \\ & - 3665441.32 T^{-1} \end{aligned}$$

$$G_N^{\circ,\text{gas}}(T) - 2.0 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) = R T \ln P + \\ \begin{aligned} 298.15 < T < 2950.00 : & 466446.153 + 2788.78662 T^{-1} - 13.2660528 T \\ & - 20.8939295 T \cdot \ln T + 8.4552092E-05 T^2 \\ & - 1.00186856E-08 T^3 \\ 2950.00 < T < 6000.00 : & 481259.023 - 7559107.28 T^{-1} - 52.4348889 T \\ & - 16.3761342 T \cdot \ln T - 2.28373808E-04 T^2 \\ & - 2.78997209E-08 T^3 \end{aligned}$$

$$G_{\text{N}_2}^{\circ,\text{gas}}(T) - 2.0 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) = 2.0 \text{ GHSER}_N + R T \ln P$$

$$G_{N_2}^{\text{o,gas}}(T) - 3.0 \cdot H_{0.5N_2}^{\text{o,gas}}(298.15 \text{ K}) = R \cdot T \cdot \ln P +$$

298.15 <  $T$  < 800.00 :  $403075.636 - 14.3245228 \cdot T - 29.5595416 \cdot T \cdot \ln T$   
                            $- 0.02413122 \cdot T^2 + 3.6156036E-06 \cdot T^3$   
                            $+ 55714.144 \cdot T^{-1}$   
 800.00 <  $T$  < 2000.00 :  $388937.207 + 158.809275 \cdot T - 55.404528 \cdot T \cdot \ln T$   
                            $- 0.0026570492 \cdot T^2 + 1.9365644E-07 \cdot T^3$   
                            $+ 1536448.48 \cdot T^{-1}$   
 2000.00 <  $T$  < 6000.00 :  $380898.006 + 210.207464 \cdot T - 62.295576 \cdot T \cdot \ln T$   
                            $+ 6.5726456E-06 \cdot T^2 - 7.868012E-10 \cdot T^3$   
                            $+ 3336949.2 \cdot T^{-1}$

$$G_{BN}^{\text{o,gas}}(T) - H_{B}^{\text{o},\beta-\text{rhombo-B}}(298.15 \text{ K}) - H_{0.5N_2}^{\text{o,gas}}(298.15 \text{ K}) = R \cdot T \cdot \ln P +$$

298.15 <  $T$  < 1000.00 :  $469920.773 - 57.4937871 \cdot T - 22.339422 \cdot T \cdot \ln T$   
                            $- 0.0105569014 \cdot T^2 + 1.41488236E-06 \cdot T^3$   
                            $- 69873.2184 \cdot T^{-1}$   
 1000.00 <  $T$  < 3500.00 :  $462619.822 + 28.1899597 \cdot T - 35.0100802 \cdot T \cdot \ln T$   
                            $- 7.99851096E-04 \cdot T^2 + 1.10267925E-08 \cdot T^3$   
                            $+ 719942.972 \cdot T^{-1}$   
 3500.00 <  $T$  < 6000.00 :  $449529.29 + 65.7741362 \cdot T - 39.4662494 \cdot T \cdot \ln T$   
                            $- 1.95814338E-04 \cdot T^2 - 9.14385307E-10 \cdot T^3$   
                            $+ 7491452 \cdot T^{-1}$

Table I - Invariant Reactions.

Reaction	Type	Compositions $x_N$	$T / \text{K}$
Liquid + gas $\rightleftharpoons$ BN	Peritectic-like	.000    1.000    .500	2670.0
Liquid $\rightleftharpoons$ BN + gas	Degenerate	.000    .000    .500	2670.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
B-N	$\beta$ -rhombo-B BN	$\beta$ -rhombo-B .....	$hR108$ $R\bar{3}m$  $hP\bar{4}$ $P\bar{6}_3mc$	$hR105$ in [91Vil]

## System B-Si

**Solution Phases:**

Liquid, diamond,  $\beta$ -rhombo-B,  $B_nSi$ ,  $B_3Si$ ,  $B_6Si$

**Modelling:**

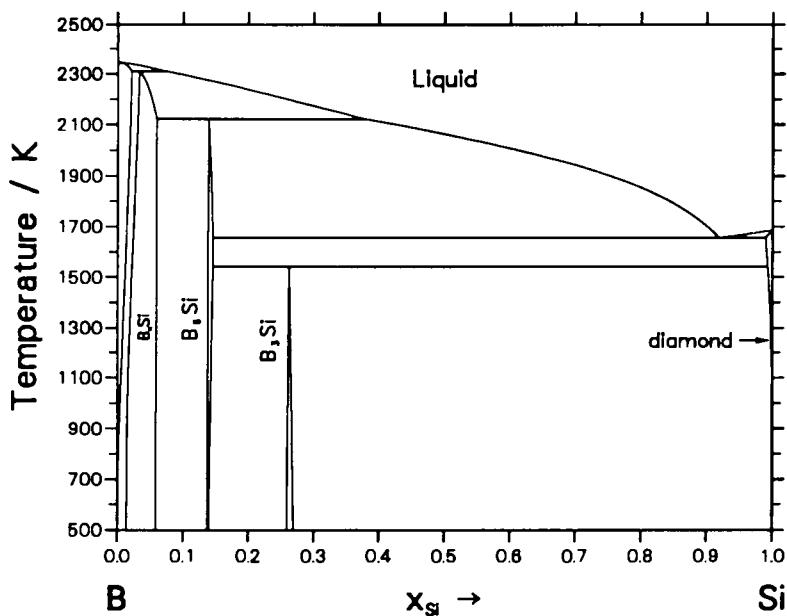
Liquid	:	Substitutional, Redlich-Kister
diamond	:	Substitutional, Redlich-Kister
$\beta$ rhombo-B	:	Sublattice model $(B)_{93}(B, Si)_{12}$
$B_nSi$	:	Sublattice model $(B)_{61}(Si)(B, Si)_8$
$B_3Si$	:	Sublattice model $(B)_6(Si)_2(B, Si)_6$
$B_6Si$	:	Sublattice model $(B)_{210}(Si)_{23}(B, Si)_{48}$

**Assessor and Date:**

S. Fries, and H.L. Lukas,

**Publication:**

"Cost507 New Light Alloys", Leuven Proceedings,  
Ed. G. Effenberg (1991)



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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**


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**Phase B<sub>3</sub>Si**

$$G^\circ(T) - 12.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - 2.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{B:Si:B}) = \\ 112000 + 12.0 \ \text{GHSER}_B + 2.0 \ \text{GHSER}_{\text{Si}}$$

$$G^\circ(T) - 6.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - 8.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{B:Si:Si}) = \\ 112000 + 6.0 \ \text{GHSER}_B + 8.0 \ \text{GHSER}_{\text{Si}}$$

$$L_{\text{B:Si:B,Si}}^{0,\text{B}_3\text{Si}} = - 2400475 + 240.0475 \ T$$

**Phase B<sub>6</sub>Si**

$$G^\circ(T) - 258.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - 23.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ G(\text{B:Si:B}) = 729824.4 - 72.98244 \ T + 258.0 \ \text{GHSER}_B + 23.0 \ \text{GHSER}_{\text{Si}}$$

$$G^\circ(T) - 210.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - 71.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ G(\text{B:Si:Si}) = 5454560 - 545.456 \ T + 210.0 \ \text{GHSER}_B + 71.0 \ \text{GHSER}_{\text{Si}}$$

$$L_{\text{B:Si:B,Si}}^{0,\text{B}_6\text{Si}} = - 15715630 + 1571.563 \ T$$

**Phase B<sub>n</sub>Si**

$$G^\circ(T) - 69.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{B:Si:B}) = \\ - 89819.86 + 8.981986 \ T + 69.0 \ \text{GHSER}_B + \text{GHSER}_{\text{Si}}$$

$$G^\circ(T) - 61.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - 9.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{B:Si:Si}) = \\ - 176659.7 + 17.66597 \ T + 61.0 \ \text{GHSER}_B + 9.0 \ \text{GHSER}_{\text{Si}}$$

$$L_{\text{B:Si:B,Si}}^{0,\text{B}_n\text{Si}} = - 281573.6 + 28.15736 \ T$$

**Phase β-rhombo-B**

$$G^\circ(T) - 93.0 \ H_B^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) - 12.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{B:Si}) = \\ - 6160.245 + 0.6160245 \ T + 93.0 \ \text{GHSER}_B + 12.0 \ \text{GHSER}_{\text{Si}}$$

$$L_{\text{B:H,Si}}^{0,\beta-\text{rhombo-B}} = - 725614.0 + 72.5614 \ T$$

**Phase diamond**

$$L_{\text{B,Si:}\square}^{0,\text{diamond}} = 57978.16$$

**Phase liquid**

$$L_{\text{B,Si}}^{0,\text{liquid}} = 17631.92 - 1.76321 \ T$$

$$L_{\text{B,Si}}^{1,\text{liquid}} = - 3526.99 + 0.3527 \ T$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Si}}$			$T / \text{K}$
$\text{B}_6\text{Si} + \text{diamond} \rightleftharpoons \text{B}_3\text{Si}$	Peritectoid	.145	.993	.262	1543.0
Liquid $\rightleftharpoons \text{B}_6\text{Si} + \text{diamond}$	Eutectic	.919	.146	.989	1657.6
Liquid + $\text{B}_n\text{Si} \rightleftharpoons \text{B}_6\text{Si}$	Peritectic	.379	.059	.138	2123.0
Liquid + $\beta\text{-rhombo-B} \rightleftharpoons \text{B}_n\text{Si}$	Peritectic	.074	.021	.033	2310.0

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
B-Si	(B)	$\beta\text{-rhombo-B}$	$cF8$ $Fd\bar{3}m$	M 8	$hR14$ in [91Vil]
	(Si)	diamond			
	$\text{B}_n\text{Si}$	B	$hR12$ $P\bar{3}m$		
	$\text{B}_3\text{Si}$	$\text{B}_4\text{C}$	$hR15$ $R\bar{3}m$	B 18 M 18 $\text{Si}_1$ 6 $\text{Si}_2$ 3	
	$\text{B}_6\text{Si}$	$\text{B}_6\text{Si}$	$oP280$ $Pnnm$		$oP340$ in [Vil91]

# System B-Ti

**Solution Phases:**

Liquid, bcc-*A*2, hcp-*A*3

**Compounds:**

BTi, B<sub>4</sub>Ti<sub>3</sub>, B<sub>2</sub>Ti

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
BTi	:	Stoichiometric, (B)(Ti)
B <sub>4</sub> Ti <sub>3</sub>	:	Stoichiometric, (B) <sub>4</sub> (Ti) <sub>3</sub>
B <sub>2</sub> Ti	:	Stoichiometric, (B) <sub>2</sub> (Ti)

**Assessor and Date:**

C. Bätzner, June 1994

**Publication:**

Thesis, Univ. Stuttgart, Germany (1994)

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase BTi**

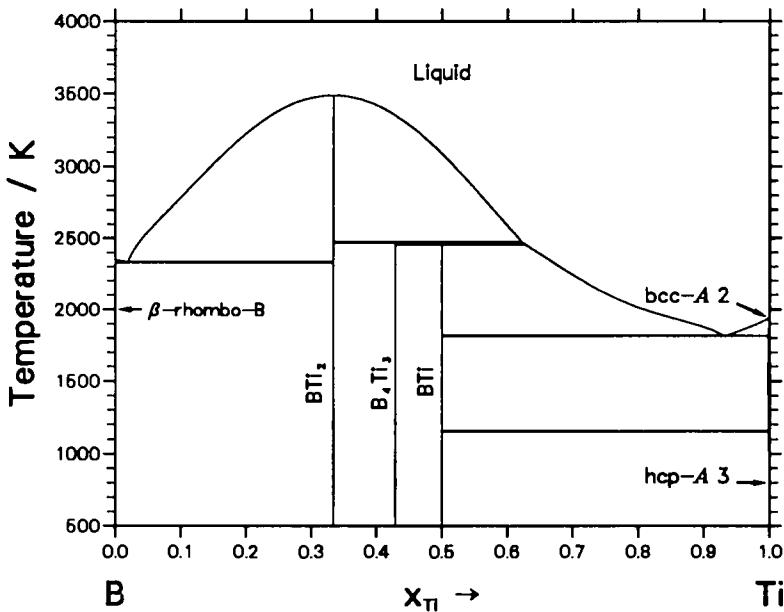
$$G^\circ(T) - H_B^{\circ,\beta-\text{rhombo-B}}(298.15\text{K}) - H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15\text{K}) = \\ - 166196.8 + 3.2968 \cdot T + \text{GIISER}_B + \text{GIISER}_{\text{Ti}}$$

**Phase B<sub>4</sub>Ti<sub>3</sub>**

$$G^\circ(T) - 4.0 \cdot H_B^{\circ,\beta-\text{rhombo-B}}(298.15\text{K}) - 3.0 \cdot H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15\text{K}) = \\ - 660745.8 + 4.3472923 \cdot T + 2.162216 \cdot T \cdot \ln T \\ + 4.0 \cdot \text{GIISER}_B + 3.0 \cdot \text{GIISER}_{\text{Ti}}$$

**Phase B<sub>2</sub>Ti**

$$G^\circ(T) - 2.0 \cdot H_B^{\circ,\beta-\text{rhombo-B}}(298.15\text{K}) - H_{\text{Ti}}^{\circ,\text{hcp-A}3}(298.15\text{K}) = \\ - 318253.47 - 2.5557 \cdot T + 0.799221 \cdot T \cdot \ln T \\ + 0.002843367 \cdot T^2 + 2.0 \cdot \text{GIISER}_B + \text{GIISER}_{\text{Ti}}$$



### Phase bcc-A2

$$\begin{aligned}
 G^\circ(T) - 3.0 H_B^{\text{o},\beta-\text{rhombo}-\text{B}}(298.15\text{K}) - H_{\text{Ti}}^{\text{o},\text{hcp}-\text{A}3}(298.15\text{K}) = \\
 - 200000 + 14.0 T + 3.0 \text{ GIISER}_B + \text{GIISER}_{\text{Ti}} \\
 L_{\text{Ti};\text{B},\square}^{0,\text{bcc}-\text{A}2} = - 260162.96 + 156.48207 T
 \end{aligned}$$

### Phase hcp-A3

$$\begin{aligned}
 G^\circ(T) - 0.5 H_B^{\text{o},\beta-\text{rhombo}-\text{B}}(298.15\text{K}) - H_{\text{Ti}}^{\text{o},\text{hcp}-\text{A}3}(298.15\text{K}) = \\
 - 50000 + 15.0 T + 0.5 \text{ GIISER}_B + \text{GIISER}_{\text{Ti}} \\
 L_{\text{Ti};\text{B},\square}^{0,\text{hcp}-\text{A}3} = - 21213.442
 \end{aligned}$$

### Phase liquid

$$L_{\text{B},\text{Ti}}^{0,\text{liquid}} = - 265414.4 + 15.543418 T$$

$$L_{\text{B},\text{Ti}}^{1,\text{liquid}} = - 134303.03 + 17.709482 T$$

$$L_{\text{B},\text{Ti}}^{2,\text{liquid}} = 61691.479$$

$$L_{\text{B},\text{Ti}}^{3,\text{liquid}} = 52656.13$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{Ti}$			$T / K$
Liquid $\rightleftharpoons$ $\beta$ -rhombo-B + $B_2Ti$	Eutectic	.019	.000	.333	2332.5
Liquid + $B_2Ti \rightleftharpoons B_4Ti_3$	Peritectic	.578	.333	.428	2474.0
Liquid + $B_4Ti_3 \rightleftharpoons BTi$	Peritectic	.627	.428	.500	2456.0
Liquid $\rightleftharpoons BTi + bcc\text{-}A2$	Eutectic	.931	.500	.997	1814.1
$bcc\text{-}A2 \rightleftharpoons BTi + hcp\text{-}A3$	Transformation	.998	.500	1.000	1156.1
$B_2Ti \rightleftharpoons$ Liquid	Congruent	.333	.333	.....	3490.0

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices
B-Ti	(B)	$\beta$ -rhombo-B		
	(Ti)	Mg	$hP2$ $P6_3/mmc$	M 2
	(Ti)	W	$cI2$ $I\bar{m}\bar{3}m$	M 2
	BTi	BFe	$oP8$ $Pnma$	B 4 Ti 4
	$B_2Ti$	$AlB_2$	$hP3$ $P6/mmm$	B 2 Ti 1
	$B_4Ti_3$	$B_4Ta_3$	$oI14$ $Immm$	

# System C–Si

**Solution Phases:**

Liquid, diamond

**Compounds:**

SiC, Si<sub>4</sub>C<sub>3</sub> (metastable)

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
diamond	:	Substitutional, Redlich-Kister
SiC	:	Stoichiometric, (Si)(C)
Si <sub>4</sub> C <sub>3</sub>	:	Stoichiometric, (Si) <sub>4</sub> (C) <sub>3</sub>

**Assessor and Date:**

J. Gröbner, H. L. Lukas, and F. Aldinger.

**Publication:**

Calphad **20**, 2 (1996) 247-254.

## Thermodynamic properties of the solution and compound phases (J·mol<sup>-1</sup>)

### Phase SiC

$$\begin{aligned} G^\circ(T) - H_C^{\circ,\text{graphite}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 88583.96 + 271.1462 \cdot T - 41.27945 \cdot T \cdot \ln T \\ - 0.00436266 \cdot T^2 + 2E-07 \cdot T^3 + 800000 \cdot T^{-1} \end{aligned}$$

### Phase Al<sub>4</sub>C<sub>3</sub> (metastable)

$$\begin{aligned} G^\circ(T) - 3.0 \cdot H_C^{\circ,\text{graphite}}(298.15 \text{ K}) - 4.0 \cdot H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 135043.86 + 949.01177 \cdot T - 144.478096 \cdot T \cdot \ln T \\ - 0.01527 \cdot T^2 + 7E-07 \cdot T^3 + 2800000 \cdot T^{-1} \end{aligned}$$

### Phase liquid

$$L_{\text{C},\text{Si}}^{\circ,\text{liquid}} = 25644.97 - 6.381115 \cdot T$$

### Phase diamond

$$L_{\text{C},\text{Si}}^{\circ,\text{diamond}} = 93386.78$$

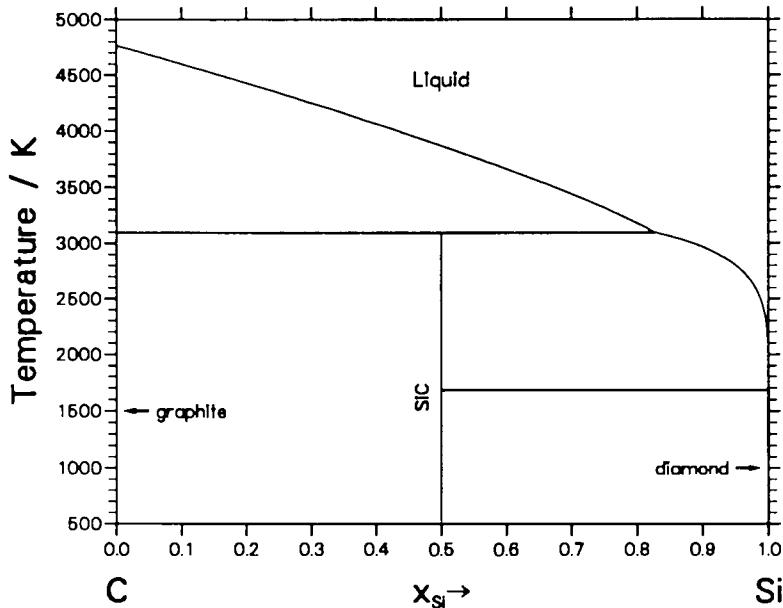


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Si}}$	$T / \text{K}$
$\text{Liquid} \rightleftharpoons \text{diamond} + \text{SiC}$	Degenerate	1.000    1.000    .500	1687.0
$\text{Liquid} + \text{graphite} \rightleftharpoons \text{SiC}$	Peritectic	.826    .000    .500	3096.4

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Group	Sub-lattices
C-Si	(C)	graphite	$cF8$ $Fd\bar{3}m$	M      8
	(Si)	diamond		
	$\text{SiC}-\beta$	ZnS (sphalerite)	$cF8$ $F\bar{4}\bar{3}m$	C      4 Si      4

# System C-Ti

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1, hcp-*A*3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Sub-lattice, (Ti)(C, $\square$ )
fcc- <i>A</i> 1	:	Sub-lattice, (Ti)(C, $\square$ )
hcp- <i>A</i> 3	:	Sub-lattice, (Ti)(C, $\square$ )

**Assessor and Date:**

S. Jonsson

**Publication:**

Thesis, Royal Institute of Technology, Stockholm,  
Sweden (1993)

**Thermodynamic properties of the solution and compound phases ( $J \cdot mol^{-1}$ )**

**Phase fcc-*A*1**

$$\begin{aligned} G^\circ(T) - H_{C,graphite}^{\circ,graphite}(298.15 \text{ K}) - H_{Ti}^{\circ,hcp-A3}(298.15 \text{ K}) &= G(Ti:C) = \\ &= -207709.0 + 307.438 T - 48.0195 T \cdot \ln T - 0.00272 T^2 \\ &\quad - 2.03E+09 T^{-3} + 819000 T^{-1} \\ L_{Ti:C\square}^{0,fcc-A1} &= -85115 + 6.756 T \end{aligned}$$

$$L_{Ti:C\square}^{1,fcc-A1} = -129429 + 31.79 T$$

**Phase bcc-*A*2**

$$\begin{aligned} G^\circ(T) - 3.0 H_{C,graphite}^{\circ,graphite}(298.15 \text{ K}) - H_{Ti}^{\circ,hcp-A3}(298.15 \text{ K}) &= G(Ti:C) \\ &= 2295533 + GHSER_{TiC} + 2.0 GHSER_C \\ L_{Ti:C\square}^{0,bcc-A2} &= -2590609 \end{aligned}$$

**Phase hcp-*A*3**

$$\begin{aligned} G^\circ(T) - 0.5 H_{C,graphite}^{\circ,graphite}(298.15 \text{ K}) - H_{Ti}^{\circ,hcp-A3}(298.15 \text{ K}) &= G(Ti:C) \\ &= -1432 - 4.1241 T + 0.5 GHSER_{TiC} + 0.5 GHSER_C \end{aligned}$$

**Phase liquid**

$$L_{C,Ti}^{0,liquid} = -214678 - 14.314 T$$

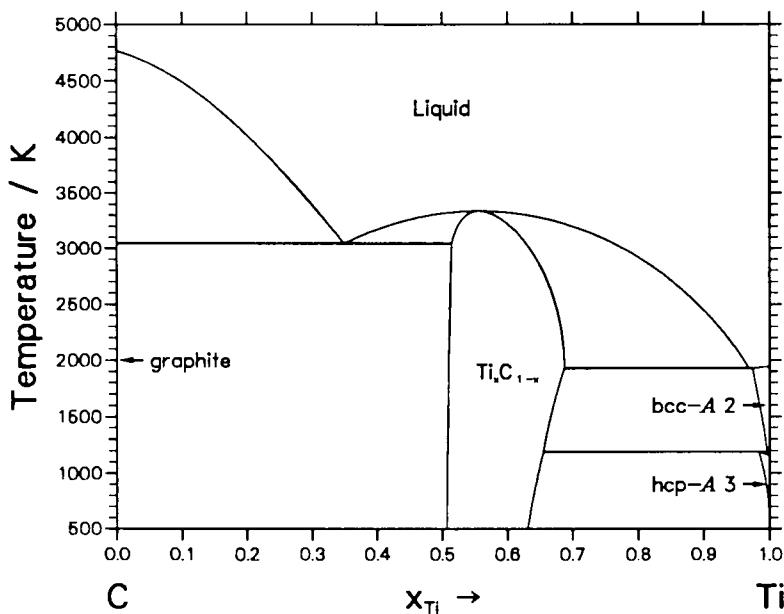


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{Ti}$	$T / K$
Liquid $\rightleftharpoons$ fcc-A1* + bcc-A2	Eutectic	.968 .687 .974	1925.2
fcc-A1* + bcc-A2 $\rightleftharpoons$ hcp-A3	Peritectoid	.655 .996 .984	1190.0
Liquid $\rightleftharpoons$ graphite + fcc-A1	Eutectic	.349 .000 .515	3044.0
fcc-A1 $\rightleftharpoons$ Liquid	Congruent	.554 .554 ...	3338.0

\* fcc-A1  $\equiv$  Ti<sub>x</sub>C<sub>1-x</sub>

Table II:a - Crystal Structure and Phase Description.

System	Phase	Structural Type	Pearson Space Group	Sub-lattices	Comments
C-Ti	(C)	graphite			
	(Ti)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	(Ti)	W	<i>I2</i> <i>Im<sup>3</sup>m</i>	M 2	

**Table II:b - Crystal Structure and Phase Description.**

System	Phase	Structural Type	Pearson Symbol Space Group	Sub-lattices	Comments
	CTi	ClNa	cF8 <i>Fm</i> $\bar{3}m$	M <sub>1</sub> 4 M <sub>2</sub> 4	
	CTi <sub>2</sub>	Ca <sub>33</sub> Ge	cF48 <i>Fd</i> $\bar{3}m$	C 16 Ti 32	Ca <sub>33</sub> Ge in [91Vil] ord. TiC <sub>1-x</sub> phase not considered

# System Ce-Mg

Solution Phases:

Liquid, bcc-*A*2, fcc-*A*1, hcp-*A*3

Compounds:

CeMg, CeMg<sub>2</sub>, CeMg<sub>3</sub>, Ce<sub>5</sub>Mg<sub>41</sub>, Ce<sub>2</sub>Mg<sub>17</sub>, CeMg<sub>12</sub>

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
CeMg	:	Stoichiometric, (Ce)(Mg)
CeMg <sub>2</sub>	:	Stoichiometric, (Ce)(Mg) <sub>2</sub>
CeMg <sub>3</sub>	:	Stoichiometric, (Ce)(Mg) <sub>3</sub>
Ce <sub>5</sub> Mg <sub>41</sub>	:	Stoichiometric, (Ce) <sub>5</sub> (Mg) <sub>41</sub>
Ce <sub>2</sub> Mg <sub>17</sub>	:	Stoichiometric, (Ce) <sub>2</sub> (Mg) <sub>17</sub>
CeMg <sub>12</sub>	:	Stoichiometric, (Ce)(Mg) <sub>12</sub>

Assessor and Date:

G. Cacciamani, A. Saccone, and R. Ferro,  
Calphad XXII - Salou, Spain (1993).

Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)

**Phase Ce<sub>2</sub>Mg<sub>17</sub>**

$$G^\circ(T) = 2.0 \ H_{\text{Ce}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 17.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 217170.0 + 104.5 \ T + 2.0 \ \text{GHSER}_{\text{Ce}} + 17.0 \ \text{GHSER}_{\text{Mg}}$$

**Phase Ce<sub>5</sub>Mg<sub>41</sub>**

$$G^\circ(T) = 5.0 \ H_{\text{Ce}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 41.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 575000.0 + 299.0 \ T + 5.0 \ \text{GHSER}_{\text{Ce}} + 41.0 \ \text{GHSER}_{\text{Mg}}$$

**Phase CeMg**

$$G^\circ(T) = H_{\text{Ce}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 46000.0 + 23.32 \ T + \text{GHSER}_{\text{Ce}} + \text{GHSER}_{\text{Mg}}$$

**Phase CeMg<sub>12</sub>**

$$G^\circ(T) - H_{\text{Ce}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 12.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 139880.0 + 84.5 T + \text{GHSER}_{\text{Ce}} + 12.0 \text{ GHSER}_{\text{Mg}}$$

**Phase CeMg<sub>2</sub>**

$$G^\circ(T) - H_{\text{Ce}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 52744.6 + 15.163 T + \text{GHSER}_{\text{Ce}} + 2.0 \text{ GHSER}_{\text{Mg}}$$

**Phase CeMg<sub>3</sub>**

$$G^\circ(T) - H_{\text{Ce}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 76800.0 + 26.5 T + \text{GHSER}_{\text{Ce}} + 3.0 \text{ GHSER}_{\text{Mg}}$$

**Phase bcc-A2**

$$L_{\text{Ce,Mg};\square}^{0,\text{bcc}-A2} = - 27000 + 3.3 T$$

$$L_{\text{Ce,Mg};\square}^{1,\text{bcc}-A2} = 25338.56 - 11.86885 T$$

$$L_{\text{Ce,Mg};\square}^{2,\text{bcc}-A2} = - 15106.9$$

**Phase fcc-A1**

$$L_{\text{Ce,Mg};\square}^{0,\text{fcc}-A1} = - 15000 + 0.5 T$$

**Phase hcp-A3**

$$L_{\text{Ce,Mg};\square}^{0,\text{hcp}-A3} = - 94337.51 + 79.95155 T$$

**Phase Liquid**

$$L_{\text{Ce,Mg}}^{0,\text{liquid}} = - 39381.19 + 16.34052 T$$

$$L_{\text{Ce,Mg}}^{1,\text{liquid}} = 25338.56 - 11.86885 T$$

$$L_{\text{Ce,Mg}}^{2,\text{liquid}} = - 15106.9$$

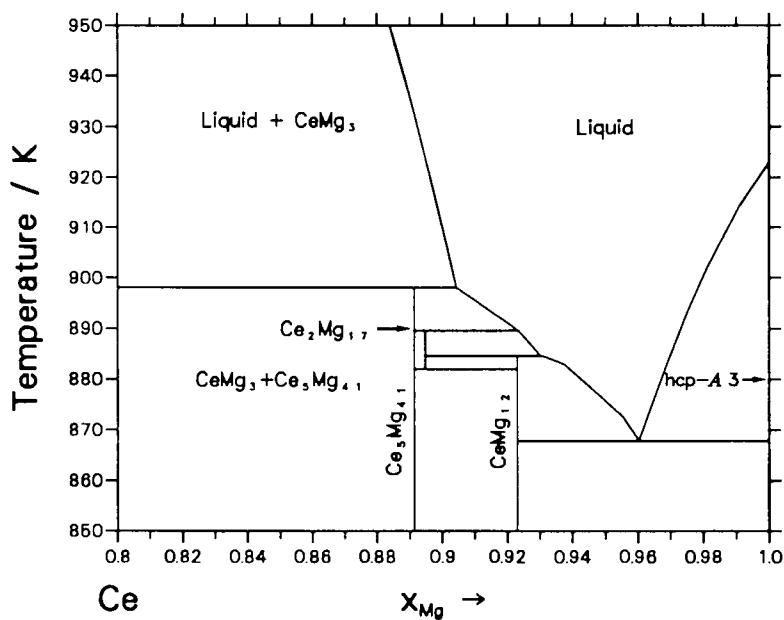
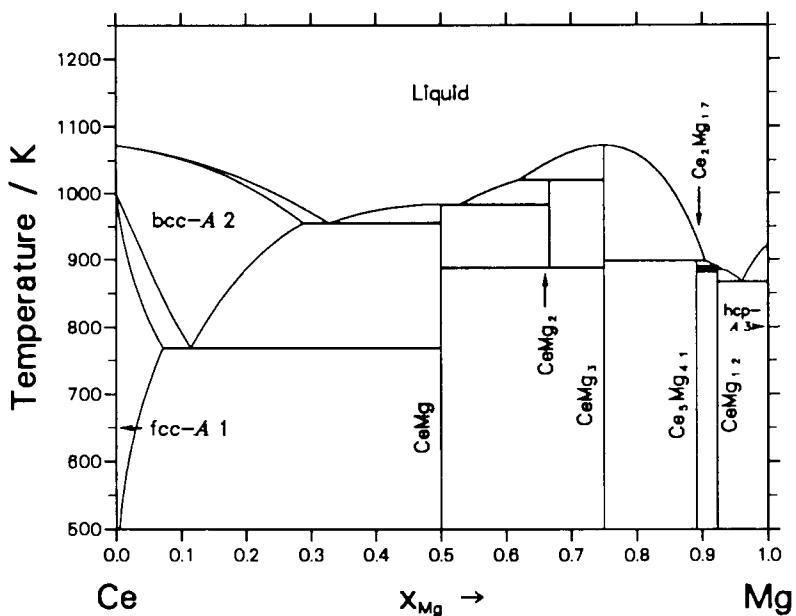


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Mg}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ bcc-A2 + CeMg	Eutectic	.328	.288	.500	955.1
Liquid $\rightleftharpoons$ CeMg + CeMg <sub>2</sub>	Eutectic	.528	.500	.667	982.9
Liquid + CeMg <sub>3</sub> $\rightleftharpoons$ CeMg <sub>2</sub>	Peritectic	.620	.750	.667	1020.1
Liquid + CeMg <sub>3</sub> $\rightleftharpoons$ Ce <sub>5</sub> Mg <sub>41</sub>	Peritectic	.904	.750	.891	898.1
Liquid + Ce <sub>5</sub> Mg <sub>41</sub> $\rightleftharpoons$ Ce <sub>2</sub> Mg <sub>17</sub>	Peritectic	.923	.891	.895	889.6
Liquid + Ce <sub>2</sub> Mg <sub>17</sub> $\rightleftharpoons$ CeMg <sub>12</sub>	Peritectic	.930	.895	.923	884.7
Liquid $\rightleftharpoons$ CeMg <sub>12</sub> + hcp-A3	Eutectic	.960	.923	1.000	867.9
Ce <sub>2</sub> Mg <sub>17</sub> $\rightleftharpoons$ Ce <sub>5</sub> Mg <sub>41</sub> + CeMg <sub>12</sub>	Eutectoid	.895	.891	.923	882.0
CeMg <sub>2</sub> $\rightleftharpoons$ CeMg + CeMg <sub>3</sub>	Eutectoid	.667	.500	.750	888.0
bcc-A2 $\rightleftharpoons$ fcc-A1 + CeMg	Eutectoid	.114	.072	.500	768.7
CeMg $\rightleftharpoons$ Liquid	Congruent	.500	.500	....	983.8
CeMg <sub>3</sub> $\rightleftharpoons$ Liquid	Congruent	.750	.750	....	1073.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Ce-Mg	(Ce)	Cu	cF4 <i>Fm</i> 3̄ <i>m</i>		
	(Ce)	W	cI2 <i>Im</i> 3̄ <i>m</i>		
	(Mg)	Mg	hP2 <i>P6</i> 3/mmc		
	CeMg	CsCl	cP2 <i>Pm</i> 3̄ <i>m</i>	Ce 1 Mg 1	
	CeMg <sub>2</sub>	Cu <sub>2</sub> Mg	cF24 <i>Fd</i> 3̄ <i>m</i>	Ce 8 Mg 16	
	CeMg <sub>3</sub>	BiF <sub>3</sub>	cF16 <i>Fm</i> 3̄ <i>m</i>	Ce 4 Mg <sub>1</sub> 4 Mg <sub>2</sub> 8	
	Ce <sub>5</sub> Mg <sub>41</sub>	Ce <sub>5</sub> Mg <sub>41</sub>	tI92 <i>I</i> 4/ <i>m</i>		10 sublattices [91Vil]
	CeMg <sub>10.3</sub>	Th <sub>2</sub> Ni <sub>17</sub>	hP38 <i>P6</i> 3/mmc		6 sublattices [91Vil] Ce <sub>2</sub> Mg <sub>17</sub>
	CeMg <sub>12(I)</sub>	ThMg <sub>12</sub>	tI26 <i>I</i> 4/mmm		ThMn <sub>12</sub> in [91Vil]
	CeMg <sub>12(II)</sub>	CeMg <sub>12(II)</sub>	oI338 ( <i>I</i> mmm)		not considered

# System Cr-Cu

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, fcc- <i>A</i> 1
(metastable)	hcp- <i>A</i> 3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister

**Assessor and Date:**

K. Zeng and M. Hämäläinen

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A*2**

$$L_{\text{Cr,Cu}:□}^{0,\text{bcc-}A2} = 200000$$

**Phase fcc-*A*1**

$$L_{\text{Cr,Cu}:□}^{0,\text{fcc-}A1} = 88112 - 30.38315 \ T$$

**Phase hcp-*A*3**

$$L_{\text{Cr,Cu}:□}^{0,\text{hcp-}A3} = 60000$$

**Phase liquid**

$$L_{\text{Cr,Cu}}^{0,\text{liquid}} = 35495.913 - 2.958 \ T$$

$$L_{\text{Cr,Cu}}^{1,\text{liquid}} = -1001.1765$$

$$L_{\text{Cr,Cu}}^{2,\text{liquid}} = 5704.648$$

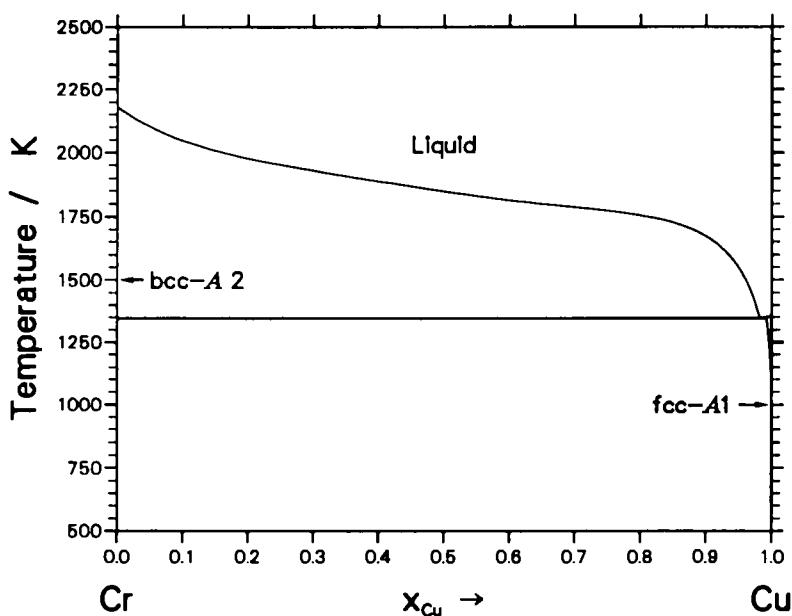


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Cu}}$	$T / \text{K}$
$\text{Liquid} \rightleftharpoons \text{bcc-}A2 + \text{fcc-}A1$	Eutectic	.982 .000 .992	1347.9

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Cr-Cu	(Cr)	W	<i>cI2</i> <i>Im</i> $\bar{3}$ <i>m</i>
	(Cu)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>

# System Cr-Mg

**Solution Phases:**

(stable)	Liquid, bcc-A2, hcp-A3
(metastable)	cbcc-A12, fcc-A1, hcp-Zn

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
cbcc-A12	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister

**Assessor and Date:**

I. Ansara, 1991

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**
**Phase bcc-A2**

$$L_{\text{Cr,Mg};\square}^{0,\text{bcc}-\text{A2}} = 80 \text{ } T$$

**Phase cbcc-A12**

$$L_{\text{Cr,Mg};\square}^{0,\text{cbcc}-\text{A12}} = 80 \text{ } T$$

**Phase fcc-A1**

$$L_{\text{Cr,Mg};\square}^{0,\text{fcc}-\text{A1}} = 80 \text{ } T$$

**Phase hcp-A3**

$$L_{\text{Cr,Mg};\square}^{0,\text{hcp}-\text{A3}} = 80 \text{ } T$$

**Phase hcp-Zn**

$$L_{\text{Cr,Mg};\square}^{0,\text{hcp}-\text{Zn}} = 80 \text{ } T$$

**Phase liquid**

$$L_{\text{Cr,Mg}}^{0,\text{liquid}} = 94500.0$$

$$L_{\text{Cr,Mg}}^{1,\text{liquid}} = 12500.0$$

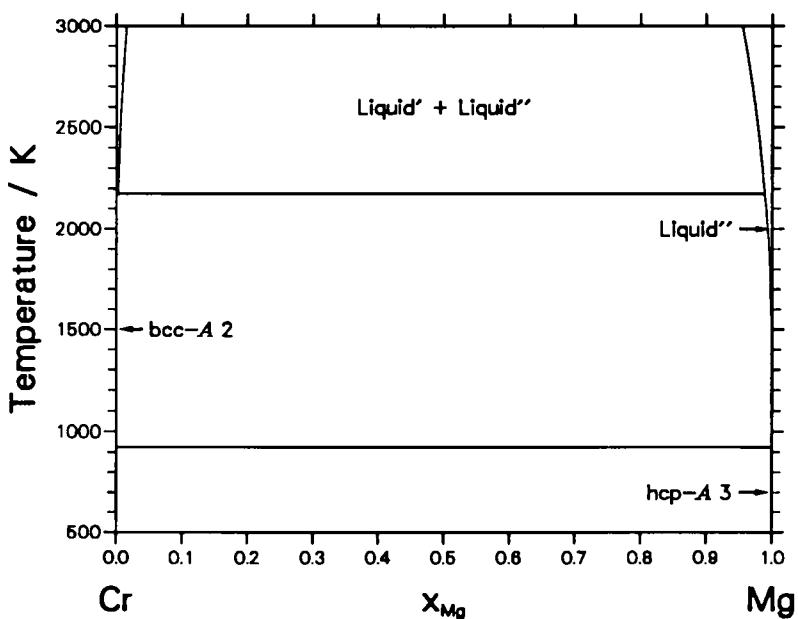


Table I - Invariant Reactions.

Reaction	Type	Compositions \$x_{Mg}\$	\$T / K\$
Liquid' \$\rightleftharpoons\$ Liquid'' + bcc-A2	monotectic	.000 .003 .988	2174.9
Liquid'' \$\rightleftharpoons\$ bcc-A2 + hcp-A3	Degenerate	.000 1.000 1.000	923.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Cr-Mg	(Cr)	W	\$c\bar{I}2\$ $I\bar{m}\bar{3}m$
	(Mg)	Mg	\$hP2\$ $P6_3/mmc$

# System Cr-Mn

**Solution Phases:**

Liquid, bcc-A2, fcc-A1, hcp-A3, cbcc-A12,  
cub-A13,  $\sigma$ -I,  $\sigma$ -II

**Compound:**

$\text{Cr}_3\text{Mn}_5$

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
cbcc-A12	:	Substitutional, Redlich-Kister
cub-A13	:	Substitutional, Redlich-Kister
$\sigma$ -I	:	Sublattice model, $(\text{Mn})_8(\text{Cr})_4(\text{Cr},\text{Mn})_{18}$
$\sigma$ -II	:	Sublattice model, $(\text{Mn})_8(\text{Cr})_4(\text{Cr},\text{Mn})_{18}$
$\text{Cr}_3\text{Mn}_5$	:	Stoichiometric, $\text{Cr}_3\text{Mn}_5$

**Publication:**

Scientific Group Thermodata Europe Database

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**Thermodynamic properties of the solution and compound phases ( $\text{J}\cdot\text{mol}^{-1}$ )**

**Phase  $\text{Cr}_3\text{Mn}_5$**

$$G^\circ(T) = 3.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-\text{A2},\text{para}}(298.15 \text{ K}) - 5.0 \ H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A12},\text{para}}(298.15 \text{ K}) = \\ - 72550.0 + 21.1732 \ T + 3.0 \ \text{GHSER}_{\text{Cr}} + 5.0 \ \text{GHSER}_{\text{Mn}}$$

**Phase fcc-A1**

$$L_{\text{Cr,Mn}:0}^{0,\text{fcc}-\text{A1}} = -19088 + 17.5123 \ T$$

**Phase cbcc-A12**

$$L_{\text{Cr,Mn}:0}^{0,\text{cbcc}-\text{A12}} = -36796 + 20.385 \ T$$

**Phase liquid**

$$L_{\text{Cr,Mn}}^{0,\text{liquid}} = -15009 + 13.6587 \ T$$

$$L_{\text{Cr,Mn}}^{1,\text{liquid}} = 501 + 0.9479 \ T$$

**Phase cub-A13**

$$L_{\text{Cr,Mn:\square}}^{0,\text{cub}-A13} = -31260 + 16.4919 T$$

**Phase bcc-A2**

$$L_{\text{Cr,Mn:\square}}^{0,\text{bcc}-A2} = -20328 + 18.7339 T$$

$$L_{\text{Cr,Mn:\square}}^{0,\text{bcc}-A2} = -9162 + 4.4183 T$$

$$\beta_{\text{Cr,Mn:\square}}^{0,\text{bcc}-A2,\text{mag}} = 0.48643$$

$$\beta_{\text{Cr,Mn:\square}}^{2,\text{bcc}-A2,\text{mag}} = -0.72035$$

$$\beta_{\text{Cr,Mn:\square}}^{4,\text{bcc}-A2,\text{mag}} = -1.93265$$

$$T_{\text{c,Cr,Mn:\square}}^{0,\text{bcc}-A2} = -1325$$

$$T_{\text{c,Cr,Mn:\square}}^{2,\text{bcc}-A2} = -1133$$

$$T_{\text{c,Cr,Mn:\square}}^{4,\text{bcc}-A2} = -10294$$

$$T_{\text{c,Cr,Mn:\square}}^{6,\text{bcc}-A2} = 26706$$

$$T_{\text{c,Cr,Mn:\square}}^{8,\text{bcc}-A2} = -28117$$

**Phase  $\sigma$ -L**

$$G^\circ(T) - 8.0 H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 22.0 H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) = \\ G(\text{Mn:Cr:Cr}) = 65859.5 + 8.0 \text{ GFCC}_{\text{Mn}} + 22.0 \text{ GHSER}_{\text{Cr}}$$

$$G^\circ(T) - 26.0 H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 4.0 H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) = \\ G(\text{Mn:Cr:Mn}) = -172946.0 + 69.0245 T + 8.0 \text{ GFCC}_{\text{Mn}} + 4.0 \text{ GHSER}_{\text{Cr}} \\ + 18.0 \text{ GBCC}_{\text{Mn}}$$

$$L_{\text{Mn:Cr:Cr,Mn}}^{0,\sigma-\text{L}} = -1095771 + 862.0312 T$$

**Phase  $\sigma$ -H**

$$G^\circ(T) - 8.0 H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 22.0 H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) = \\ G(\text{Mn:Cr:Cr}) = -192369.0 + 152.4742 T + 8.0 \text{ GFCC}_{\text{Mn}} + 22.0 \text{ GHSER}_{\text{Cr}}$$

$$G^\circ(T) - 26.0 H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 4.0 H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) = \\ G(\text{Mn:Cr:Mn}) = -74263.0 - 10.7082 T + 18.0 \text{ GBCC}_{\text{Mn}} + 8.0 \text{ GFCC}_{\text{Mn}} \\ + 4.0 \text{ GHSER}_{\text{Cr}}$$

$$L_{\text{Mn:Cr:Cr,Mn}}^{0,\sigma-\text{H}} = 90000$$

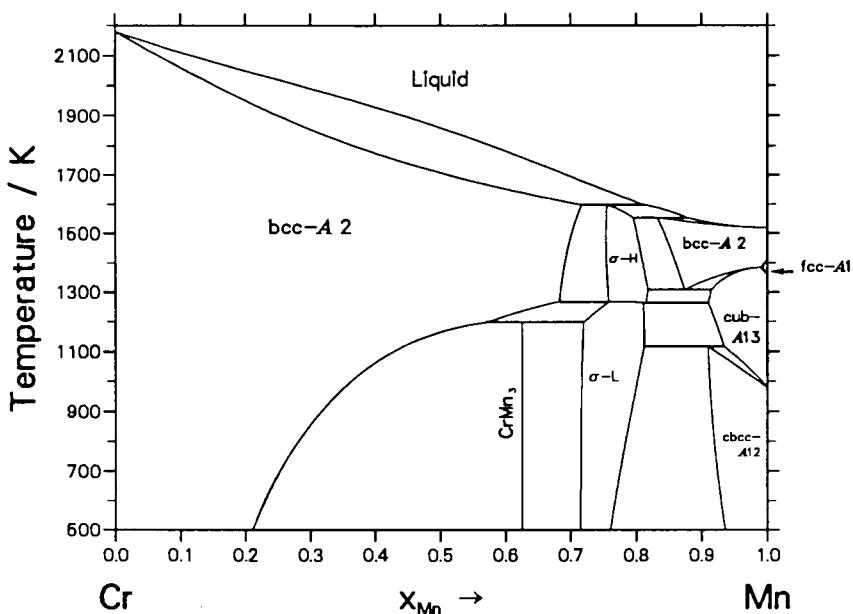


Table I - Invariant Reactions.

Reaction	Type	Compositions \$x_{Mn}\$	\$T / K\$
bcc-A2 + \$\sigma\$-L \$\rightleftharpoons\$ Cr\$_3\$Mn\$_5\$	Peritectoid	.570 .719 .625	1197.8
\$\sigma\$-H \$\rightleftharpoons\$ bcc-A2 + \$\sigma\$-L	Eutectoid	.758 .683 .760	1268.1
Liquid + bcc-A2 \$\rightleftharpoons\$ \$\sigma\$-H	Peritectic	.813 .717 .755	1598.4
Liquid + \$\sigma\$-H \$\rightleftharpoons\$ bcc-A2	Peritectic	.876 .794 .831	1556.2
bcc-A2 \$\rightleftharpoons\$ cub-A13 + \$\sigma\$-H	Eutectoid	.880 .873 .894	1293.6
bcc-A2 + fcc-A1 \$\rightleftharpoons\$ cub-A13	Peritectoid	.898 .993 .913	1382.1
\$\sigma\$-H \$\rightleftharpoons\$ \$\sigma\$-L + cub-A13	Eutectoid	.815 .811 .910	1264.4
\$\sigma\$-L + cub-A13 \$\rightleftharpoons\$ cbcc-A12	Peritectoid	.812 .934 .910	1117.4

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Cr-Mn	(Cr)	W	cI2 Im $\bar{3}m$	
	$\alpha$ -Mn	$\alpha$ -Mn	c58 I4 $\bar{3}m$	bcc-A12
	$\beta$ -Mn	$\beta$ -Mn	cP20 P $\bar{4}_132\bar{3}m$	cub-A13
	$\gamma$ -Mn	Cu	cF4 Fm $\bar{3}m$	fcc-A1
	$\delta$ -Mn	W	cI2 Im $\bar{3}m$	bcc-A2
	$\alpha'$ Cr <sub>x</sub> Mn <sub>1-x</sub> HT	$\alpha$ -Mn		
	$\alpha''$ Cr <sub>x</sub> Mn <sub>1-x</sub> LT	$\alpha$ -Mn		
	$\sigma$ Cr <sub>x</sub> Mn <sub>1-x</sub> HT	$\sigma$ CrFe	tP30 P $\bar{4}_2/mnm$	
	$\sigma$ Cr <sub>x</sub> Mn <sub>1-x</sub> MT	$\sigma$ CrFe	tP30 P $\bar{4}_2/mnm$	
	$\sigma$ Cr <sub>x</sub> Mn <sub>1-x</sub> LT	$\sigma$ CrFe	tP30 P $\bar{4}_2/mnm$	

# System Cr–Si

Solution Phases:

Liquid, bcc-*A*2

Compounds:

Cr<sub>5</sub>Si<sub>3</sub>, CrSi<sub>1</sub>, Cr<sub>3</sub>Si-*A*15, CrSi<sub>2</sub>

Modelling:

Liquid	:	Substitutional, Redlich–Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich–Kister
Cr <sub>3</sub> Si- <i>A</i> 15	:	Sublattice model, (Cr,Si) <sub>3</sub> (Cr,Si)
CrSi <sub>2</sub>	:	Sublattice model, (Cr,Si)(Cr,Si) <sub>2</sub>
Cr <sub>5</sub> Si <sub>3</sub>	:	Stoichiometric, (Cr) <sub>5</sub> (Si) <sub>3</sub>
CrSi	:	Stoichiometric, (Cr)(Si)

Assessor and Date:

C.A. Coughnanowr, I. Ansara, and H.L. Lukas,

Publication:

Calphad, 18, 2, 125–140 (1994).

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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

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**Phase liquid**

$$L_{\text{Cr},\text{Si}}^{0,\text{liquid}} = -119216.90 + 16.11445 \ T$$

$$L_{\text{Cr},\text{Si}}^{1,\text{liquid}} = -47614.70 + 12.17363 \ T$$

**Phase bcc-*A*2**

$$L_{\text{Cr},\text{Si}}^{0,\text{bcc-}A2} = -104537.94 + 10.69527 \ T$$

$$L_{\text{Cr},\text{Si}}^{1,\text{bcc-}A2} = -47614.70 + 12.17363 \ T$$

### Phase Cr<sub>3</sub>Si-A15

$$G^\circ(T) - 4.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = \\ 20000.0 + 10.000 \ T + 4.0 \ \text{GHSER}_{\text{Cr}}$$

$$G^\circ(T) - 3.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Cr:Si}) = \\ - 126369.35 + 4.15051 \ T + 3.0 \ \text{GHSER}_{\text{Cr}} + \text{GIISER}_{\text{Si}}$$

$$G^\circ(T) - H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 3.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Cr:Si}) = \\ 233507.47 - 74.15051 \ T + \text{GIISER}_{\text{Cr}} + 3.0 \ \text{GHSER}_{\text{Si}}$$

$$G^\circ(T) - 4.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si}) = \\ 208000.0 - 80.000 \ T + 4.0 \ \text{GHSER}_{\text{Si}}$$

$$L_{\text{Cr},\text{Si:Cr}}^{0,\text{Cr}_3\text{Si}} = L_{\text{Cr},\text{Si:Si}}^{0,\text{Cr}_3\text{Si}} = - 107840.95$$

$$L_{\text{Cr:Cr},\text{Si}}^{0,\text{Cr}_3\text{Si}} = L_{\text{Si:Cr},\text{Si}}^{0,\text{Cr}_3\text{Si}} = - 13020.93$$

### Phase Cr<sub>5</sub>Si<sub>3</sub>

$$G^\circ(T) - 5.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 3.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 316433.0 + 1065.82816 \ T - 182.578184 \ T \cdot \ln T \\ - 23.919688E-3 \ T^2 - 2.31728E-06 \ T^3$$

### Phase CrSi

$$G^\circ(T) - H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 78732.28 + 311.58392 \ T - 51.62865 \ T \cdot \ln T \\ - 4.47355E-03 \ T^2 + 391330 \ T^{-1}$$

### Phase CrSi<sub>2</sub>

$$G^\circ(T) - 3.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = \\ 10000.00 - 1.0 \ T + 3.0 \ \text{GHSER}_{\text{Cr}}$$

$$G^\circ(T) - H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 2.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Cr:Si}) = \\ - 96694.43 + 333.33835 \ T - 57.855747 \ T \cdot \ln T \\ - 13.22769E-03 \ T^2 - 0.43203E-06 \ T^3$$

$$G^\circ(T) - 2.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Cr}) = \\ 148569.93 - 12.65342 \ T + 2.0 \ \text{GIISER}_{\text{Cr}} + \text{GIISER}_{\text{Si}}$$

$$G^\circ(T) - 3.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si}) = \\ 78860.26 - 15.77206 \ T + 3.0 \ \text{GIISER}_{\text{Si}}$$

$$L_{\text{Cr:Cr},\text{Si}}^{0,\text{CrSi}_2} = L_{\text{Si:Cr},\text{Si}}^{0,\text{CrSi}_2} = - 35879.97 + 7.17599 \ T$$

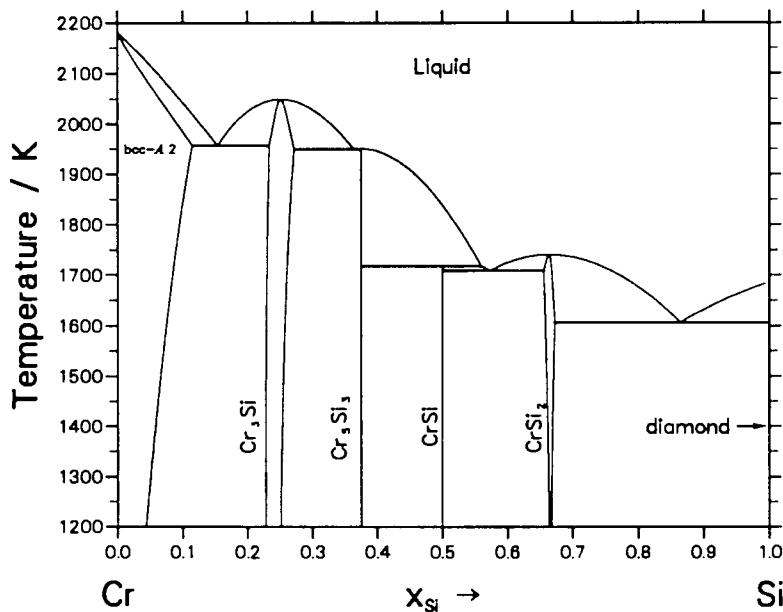


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Si}}$			$T / \text{K}$
$\text{Liquid} \rightleftharpoons \text{bcc}-\text{A}2 + \text{Cr}_3\text{Si}-\text{A}15$	Eutectic	.154	.115	.233	1957.4
$\text{Liquid} \rightleftharpoons \text{Cr}_3\text{Si}-\text{A}15 + \text{Cr}_5\text{Si}_3$	Eutectic	.364	.272	.375	1950.0
$\text{Liquid} + \text{Cr}_5\text{Si}_3 \rightleftharpoons \text{CrSi}$	Peritectic	.560	.375	.500	1718.5
$\text{Liquid} \rightleftharpoons \text{CrSi} + \text{CrSi}_2$	Eutectic	.574	.500	.656	1708.8
$\text{Liquid} \rightleftharpoons \text{CrSi}_2 + \text{diamond}$	Eutectic	.864	.673	1.000	1606.7
$\text{Cr}_3\text{Si}-\text{A}15 \rightleftharpoons \text{Liquid}$	Congruent	.025	.025	...	2049.5
$\text{Cr}_5\text{Si}_3 \rightleftharpoons \text{Liquid}$	Congruent	.375	.375	...	1951.0
$\text{Cr}_2\text{Si} \rightleftharpoons \text{Liquid}$	Congruent	.666	.666	...	1741.0

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol	Space Group	Sub- lattices	Comments
Cr-Si	(Cr)	W	<i>cI2</i> <i>Im3m</i>	M	2	
	(Si)	diamond-A4	<i>cF8</i> <i>Fd3m</i>			
	CrSi	FeSi	<i>cP8</i> <i>P213</i>	Cr Si	4 4	
	CrSi <sub>2</sub>	CrSi <sub>2</sub>	<i>hPg</i> <i>P6<sub>2</sub>22</i>	Cr Si	3 6	
	Cr <sub>3</sub> Si	Cr <sub>3</sub> Si	<i>cP8</i> <i>Pm3n</i>	Cr Si	6 2	Cr <sub>3</sub> Si-A15
	Cr <sub>5</sub> Si <sub>3</sub>	Si <sub>3</sub> W <sub>5</sub>	<i>tI92</i> <i>I4/mcm</i>	Cr <sub>1</sub> Cr <sub>2</sub> Si <sub>1</sub> Si <sub>2</sub>	4 16 4 8	<i>tI98</i> in Masl
	Cr <sub>5</sub> Si <sub>3</sub>	Mn <sub>5</sub> Si <sub>3</sub>	<i>hP16</i> <i>P6<sub>3</sub>/mcm</i>			not considered

# System Cr-Ti

**Solution Phases:**

Liquid, bcc-*A*2, hcp-*A*3

**Compounds:**

Laves-*C*14, Laves-*C*15

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Laves- <i>C</i> 14	:	Sublattice model, (Cr,Ti) <sub>2</sub> (Cr,Ti)
Laves- <i>C</i> 15	:	Sublattice model, (Cr,Ti) <sub>2</sub> (Cr,Ti)

**Assessor and Date:**

N. Saunders, 1992

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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

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**Phase Laves-*C*14**

$$G^\circ(T) - 3.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = 15000.0 + 3.0 \ \text{GIISER}_{\text{Cr}}$$

$$G^\circ(T) - 2.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Cr:Ti}) = \\ - 1440.0 - 6.75 \ T + 2.0 \ \text{GIISER}_{\text{Cr}} + \text{GIISER}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Cr}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) - 2.0 \ H_{\text{Ti}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Ti:Cr}) = \\ 15000.0 + \text{GIISER}_{\text{Cr}} + 2.0 \ \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 \ H_{\text{Ti}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = \\ 15000.0 + 3.0 \ \text{GHSER}_{\text{Ti}}$$

$$L_{\text{Cr:Cr,Ti}}^{0,\text{Laves-}\text{C}14} = L_{\text{Ti:Cr,Ti}}^{0,\text{Laves-}\text{C}14} = 60000.0$$

$$L_{\text{Cr,Ti:Cr}}^{0,\text{Laves-}\text{C}14} = L_{\text{Cr,Ti:Ti}}^{0,\text{Laves-}\text{C}14} = 60000.0$$

### Phase Laves-C15

$$G^\circ(T) - 3.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = 15000.0 + 3.0 \ \text{GHSER}_{\text{Cr}}$$

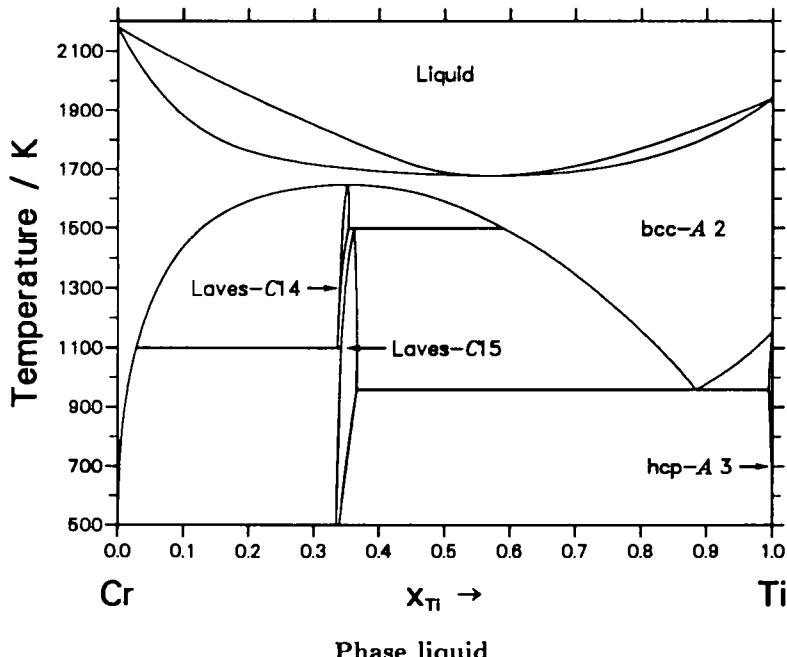
$$G^\circ(T) - 2.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cr:Ti}) = - 1780.0 - 6.3 \ T + 2.0 \ \text{GHSER}_{\text{Cr}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 2.0 \ H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Cr}) = 15000.0 + \text{GHSER}_{\text{Cr}} + 2.0 \ \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 \ H_{\text{Ti}}^{\circ,\text{hcp}-A2}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 15000.0 + 3.0 \ \text{GHSER}_{\text{Ti}}$$

$$L_{\text{Cr:Cr,Ti}}^{0,\text{Laves-C15}} = L_{\text{Ti:Cr,Ti}}^{0,\text{Laves-C15}} = 50000.0$$

$$L_{\text{Cr,Ti:Cr}}^{0,\text{Laves-C15}} = L_{\text{Cr,Ti:Ti}}^{0,\text{Laves-C15}} = 10800.0 + 27 \ T$$



### Phase liquid

$$L_{\text{Cr,Ti}}^{0,\text{liquid}} = 5250$$

$$L_{\text{Cr,Ti}}^{1,\text{liquid}} = 1500$$

### Phase hcp-A3

$$L_{\text{Cr,Ti:D}}^{0,\text{hcp}-A3} = 32500$$

**Phase bcc-A2**

$$I_{\text{Cr,Ti:}\square}^{0,\text{bcc-A2}} = 19100$$

$$I_{\text{Cr,Ti:}\square}^{1,\text{bcc-A2}} = 5500$$

$$I_{\text{Cr,Ti:}\square}^{2,\text{bcc-A2}} = 1750$$

**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Ti}}$	T / K
$\text{bcc-A2} \rightleftharpoons \text{Laves-C15} + \text{hcp-A3}$	Eutectoid	.884 .365 .994	959.7
$\text{bcc-A2} + \text{Laves-C15} \rightleftharpoons \text{Laves-C14}$	Peritectoid	.593 .353 .362	1495.3
$\text{Laves-C14} \rightleftharpoons \text{bcc-A2} + \text{Laves-C15}$	Eutectoid	.336 .027 .342	1093.4
$\text{Laves-C14} \rightleftharpoons \text{bcc-A2}$	Congruent	.333 .333 ....	1645.0
$\text{bcc-A2} \rightleftharpoons \text{Liquid}$	Congruent	.563 .563 ....	1677.0

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Cr-Ti	(Cr)	W	$cI2$ $I\bar{m}\bar{3}m$	
	(Ti)	Mg	$hP2$ $P6_3/mmc$	
	(Ti)	W	$cI2$ $I\bar{m}\bar{3}m$	
	$\alpha$ Cr <sub>2</sub> Ti	Cu <sub>2</sub> Mg	$cF24$ $Fd\bar{3}m$	Laves-C15
	$\beta$ Cr <sub>2</sub> Ti	MgZn <sub>2</sub>	$hP12$ $P6_3/mmc$	Laves-C14
	$\gamma$ Cr <sub>2</sub> Ti	MgNi <sub>2</sub>	$hP24$ $P6_3/mmc$	Laves-C36

## System Cr–V

**Solution Phases:**

Liquid, bcc-*A*2

**Modelling:**

Liquid : Substitutional, Redlich-Kister  
bcc-*A*2 : Substitutional, Redlich-Kister

**Publication:**

Scientific Group Thermodata Europe Database

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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

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**Phase bcc-*A*2**

$$L_{\text{Cr,V}: \square}^{0,\text{bcc}-A2} = - 9874 - 2.6964 \ T$$

$$L_{\text{Cr,V}: \square}^{1,\text{bcc}-A2} = - 1720 - 2.5237 \ T$$

**Phase liquid**

$$L_{\text{Cr,V}}^{0,\text{liquid}} = - 9874 - 2.6964 \ T$$

$$L_{\text{Cr,V}}^{1,\text{liquid}} = - 1720 - 2.5237 \ T$$

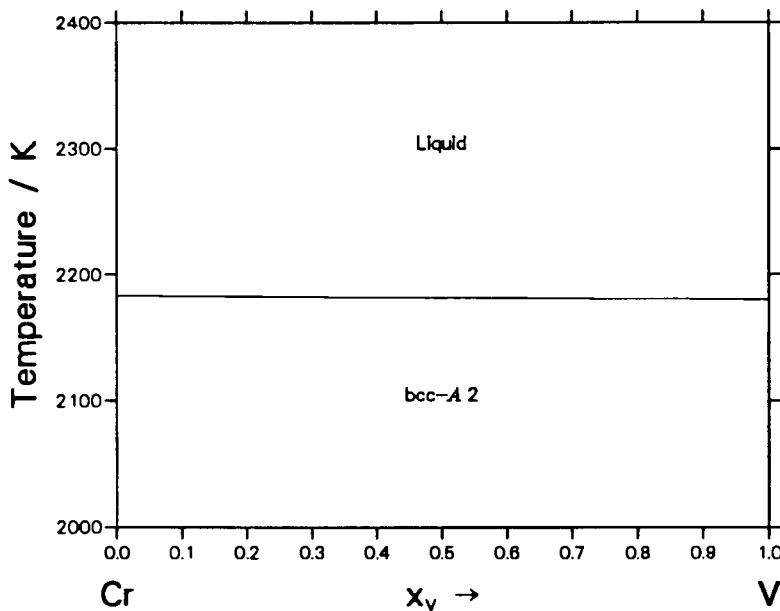


Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Cr-V	(Cr) (V)	W	cI2 <i>I</i> m $\bar{3}$ <i>m</i> cI2 <i>I</i> m $\bar{3}$ <i>m</i>

## System Cr-Zn

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, hcp-Zn
(metastable)	fcc- <i>A</i> 1

**Compounds:**

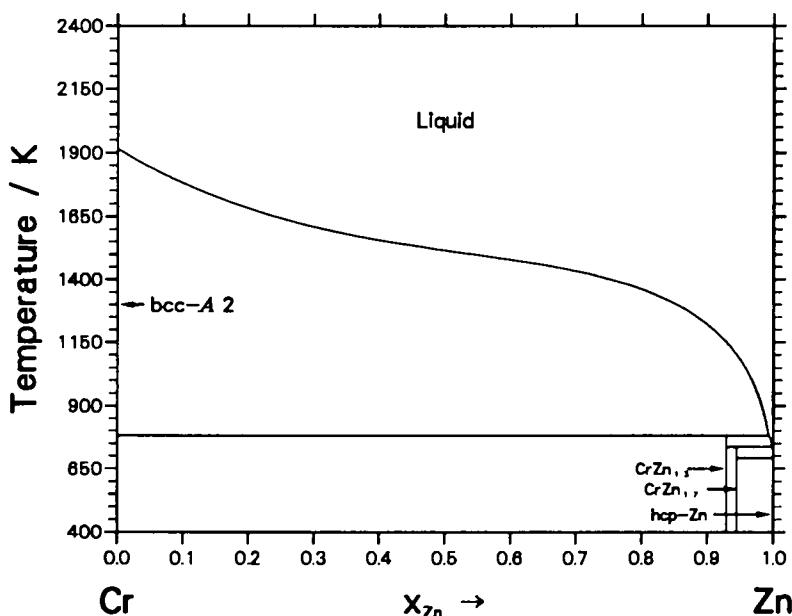
$\text{CrZn}_{13}$ ,  $\text{CrZn}_{17}$

**Modelling:**

bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister
Liquid	:	Substitutional, Redlich-Kister
$\text{CrZn}_{13}$	:	Stoichiometric, $(\text{Cr})(\text{Zn})_{13}$
$\text{CrZn}_{17}$	:	Stoichiometric, $(\text{Cr})(\text{Zn})_{17}$

**Assessor and Date:**

I. Ansara, 1992



Thermodynamic properties of the solution and compound phases ( $\text{J}\cdot\text{mol}^{-1}$ )**Phase bcc-A2**

$$L_{\text{Cr,Zn}:□}^{0,\text{bcc}-\text{A2}} = 80 \text{ } T$$

**Phase fcc-A1**

$$L_{\text{Cr,Zn}:□}^{0,\text{fcc}-\text{A1}} = 80 \text{ } T$$

**Phase hcp-Zn**

$$L_{\text{Cr,Zn}:□}^{0,\text{hcp}-\text{Zn}} = 80 \text{ } T$$

**Phase liquid**

$$L_{\text{Cr,Zn}}^{0,\text{liquid}} = 19000$$

$$L_{\text{Cr,Zn}}^{1,\text{liquid}} = -1000$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Zn}}$			$T / \text{K}$
Liquid + bcc-A2 $\rightleftharpoons$ CrZn <sub>13</sub> <sup>*</sup>	Peritectic	0.996	0.000	0.928	761.4
Liquid + CrZn <sub>13</sub> $\rightleftharpoons$ CrZn <sub>17</sub>	Peritectic	0.998	0.928	0.944	736.5
Liquid $\rightleftharpoons$ CrZn <sub>17</sub> + hcp-Zn	Degenerate	0.999	0.944	0.999	692.5

\* Reaction uncertain

**Phase CrZn<sub>13</sub>**

$$\begin{aligned} G^\circ(T) - H_{\text{Cr}}^{\circ,\text{bcc}-\text{A2},\text{para}}(298.15 \text{ K}) - 13.0 \text{ } H_{\text{Zn}}^{\circ,\text{hcp}-\text{A3}}(298.15 \text{ K}) \\ - 9800.0 + \text{GHSER}_{\text{Cr}} + 13.0 \text{ } \text{GHSER}_{\text{Zn}} \end{aligned}$$

**Phase CrZn<sub>17</sub>**

$$\begin{aligned} G^\circ(T) - H_{\text{Cr}}^{\circ,\text{bcc}-\text{A2},\text{para}}(298.15 \text{ K}) - 17.0 \text{ } H_{\text{Zn}}^{\circ,\text{hcp}-\text{A3}}(298.15 \text{ K}) \\ - 11700.0 + \text{GHSER}_{\text{Cr}} + 17.0 \text{ } \text{GHSER}_{\text{Zn}} \end{aligned}$$

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group
Cr-Zn	(Cr)	W	<i>cI2</i> <i>Im3m</i>
	(Zn)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>
	CrZn <sub>13</sub>	CoZn <sub>13</sub>	
	CrZn <sub>17</sub>		

# System Cr-Zr

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, hcp- <i>A</i> 3
(metastable)	fcc- <i>A</i> 1

**Compounds:**

Laves-*C*14, Laves-*C*15, Laves-*C*36

**Modelling:**

bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Liquid	:	Substitutional, Redlich-Kister
Laves- <i>C</i> 14	:	Sublattice model, $(\text{Cr}, \text{Zr})_2(\text{Cr}, \text{Zr})$
Laves- <i>C</i> 15	:	Sublattice model, $(\text{Cr}, \text{Zr})_2(\text{Cr}, \text{Zr})$
Laves- <i>C</i> 36	:	Sublattice model, $(\text{Cr}, \text{Zr})_2(\text{Cr}, \text{Zr})$

**Assessor and Date:**

K. Zeng, M. Hämäläinen, and I. Ansara (1993)

**Thermodynamic properties of the solution and compound phases ( $\text{J} \cdot \text{mol}^{-1}$ )**

**Phase Laves-*C*14**

$$G^\circ(T) - 3.0 \ H_{\text{Cr}}^{\circ, \text{bcc}-\text{A}2, \text{para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = \\ 15000.0 + 3.0 \ \text{GHSER}_{\text{Cr}}$$

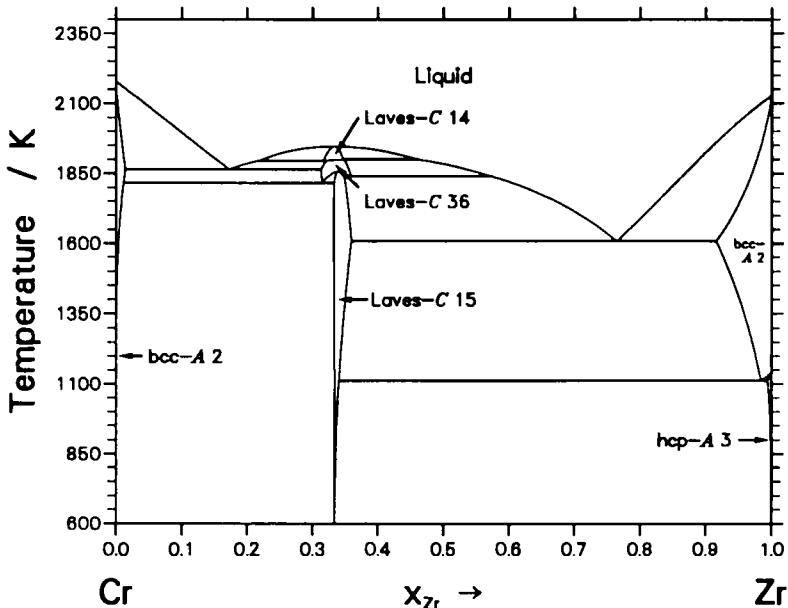
$$G^\circ(T) - 2.0 \ H_{\text{Cr}}^{\circ, \text{bcc}-\text{A}2, \text{para}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Cr:Zr}) = \\ -8114 - 11.652 \ T + 2.0 \ \text{GHSER}_{\text{Cr}} + \text{GHSER}_{\text{Zr}}$$

$$G^\circ(T) - H_{\text{Cr}}^{\circ, \text{bcc}-\text{A}2, \text{para}}(298.15 \text{ K}) - 2.0 \ H_{\text{Zr}}^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Zr:Cr}) = \\ 38114 + 11.652 \ T + \text{GHSER}_{\text{Cr}} + 2.0 \ \text{GHSER}_{\text{Zr}}$$

$$G^\circ(T) - 3.0 \ H_{\text{Zr}}^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Zr:Zr}) = \\ 15000.0 + 3.0 \ \text{GHSER}_{\text{Zr}}$$

$$L_{\text{Cr}, \text{Zr}: \text{Cr}}^{0, \text{Laves}-\text{C}14} = L_{\text{Cr}, \text{Zr}: \text{Zr}}^{0, \text{Laves}-\text{C}14} = 52300$$

$$L_{\text{Cr}: \text{Cr}, \text{Zr}}^{0, \text{Laves}-\text{C}14} = L_{\text{Zr}: \text{Cr}, \text{Zr}}^{0, \text{Laves}-\text{C}14} = 26060$$



### Phase Laves-C15

$$G^\circ(T) - 3.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = 15000.0 + 3.0 \ \text{GHSER}_{\text{Cr}}$$

$$G^\circ(T) - 2.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cr:Zr}) = -87273 + 29.915 \ T + 2.0 \ \text{GHSER}_{\text{Cr}} + \text{GHSER}_{\text{Zr}}$$

$$G^\circ(T) - H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 2.0 \ H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Zr:Cr}) = 387273 - 29.915 \ T + \text{GHSER}_{\text{Cr}} + 2.0 \ \text{GHSER}_{\text{Zr}}$$

$$G^\circ(T) - 3.0 \ H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Zr:Zr}) = 15000.0 + 3.0 \ \text{GHSER}_{\text{Zr}}$$

$$L_{\text{Cr},\text{Zr:Cr}}^{0,\text{Laves-C15}} = 70328$$

$$L_{\text{Cr},\text{Zr:Zr}}^{0,\text{Laves-C15}} = 70328$$

$$L_{\text{Cr:Cr},\text{Zr}}^{0,\text{Laves-C15}} = 62910$$

$$L_{\text{Zr:Cr},\text{Zr}}^{0,\text{Laves-C15}} = 62910$$

**Phase Laves-C36**

$$G^\circ(T) - 3.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) = G(\text{Cr:Cr}) = \\ 15000.0 + 3.0 \ \text{GHSER}_{\text{Cr}}$$

$$G^\circ(T) - 2.0 \ H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cr:Zr}) = \\ - 70026 + 20.901 \ T + 2.0 \ \text{GHSER}_{\text{Cr}} + \text{GHSER}_{\text{Zr}}$$

$$G^\circ(T) - H_{\text{Cr}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 2.0 \ H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Zr:Cr}) = \\ 100026.08 - 20.901 \ T + \text{GHSER}_{\text{Cr}} + 2.0 \ \text{GHSER}_{\text{Zr}}$$

$$G^\circ(T) - 3.0 \ H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Zr:Zr}) = \\ 15000.0 + 3.0 \ \text{GHSER}_{\text{Zr}}$$

$$I_{\text{Cr,Zr:Cr}}^{0,\text{Laves-C36}} = 52614$$

$$I_{\text{Cr,Zr:Zr}}^{0,\text{Laves-C36}} = 52614$$

$$I_{\text{Cr:Cr,Zr}}^{0,\text{Laves-C36}} = 29400$$

$$I_{\text{Zr:Cr,Zr}}^{0,\text{Laves-C36}} = 2940$$

**Phase liquid**

$$I_{\text{Cr,Zr}}^{0,\text{liquid}} = - 12971.34 + 1.20015 \ T$$

$$I_{\text{Cr,Zr}}^{1,\text{liquid}} = 8025.96 - 0.74259 \ T$$

$$I_{\text{Cr,Zr}}^{2,\text{Liquid}} = - 9984.87 + 0.92383 \ T$$

**Phase bcc-A2**

$$I_{\text{Cr,Zr:}\square}^{0,\text{bcc}-A2} = 16555.47 + 4.92028 \ T$$

$$I_{\text{Cr,Zr:}\square}^{1,\text{bcc}-A2} = 11365.57$$

**Phase fcc-A1**

$$I_{\text{Cr,Zr:}\square}^{0,\text{fcc}-A1} = 20000$$

**Phase hcp-A3**

$$I_{\text{Cr,Zr:}\square}^{0,\text{hcp}-A3} = 15800$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{Zr}$			$T / K$
Liquid $\rightleftharpoons$ Laves-C15 + bcc-A2	Eutectic	.765	.359	.916	1607.9
Laves-C36 $\rightleftharpoons$ Laves-C15 + Liquid	Metatectic	.359	.348	.573	1839.6
Liquid + Laves-C14 $\rightleftharpoons$ Laves-C36	Peritectic	.461	.346	.348	1900.0
Laves-C36 $\rightleftharpoons$ Liquid + Laves-C14	Metatectic	.316	.218	.321	1895.9
Liquid $\rightleftharpoons$ bcc-A2 + Laves-C36	Eutectic	.173	.014	.313	1864.6
Laves-C36 $\rightleftharpoons$ bcc-A2 + Laves-C15	Eutectoid	.314	.012	.333	1816.1
bcc-A2 $\rightleftharpoons$ Laves-C15 + hcp-A3	Eutectoid	.984	.340	.994	1112.3
Laves-C14 $\rightleftharpoons$ Liquid	Congruent	.333	.333	....	1946.5
Laves-C15 $\rightleftharpoons$ Laves-C36	Congruent	.340	.340	....	1858.0

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Cr-Zr	(Cr)	W	<i>cI2</i> <i>Im3m</i>	M 2	Laves-C15
	(Zr)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	(Zr)	W	<i>cI2</i> <i>Im3m</i>	M 4	Laves-C36
	$\alpha$ -Cr <sub>2</sub> Zr	Cu <sub>2</sub> Mg	<i>cF24</i> <i>Fd3m</i>	M <sub>1</sub> 8 M <sub>2</sub> 16	
	$\beta$ -Cr <sub>2</sub> Zr	MgNi <sub>2</sub>	<i>hP24</i> <i>P6<sub>3</sub>/mmc</i>	Cr <sub>1</sub> 6 Cr <sub>2</sub> 6 Zr <sub>1</sub> 3 Zr <sub>2</sub> 3	Laves-C14
	$\gamma$ -Cr <sub>2</sub> Zr	MgZn <sub>2</sub>	<i>hP12</i> <i>P6<sub>3</sub>/mmc</i>	Cr 2 Cr 6 Zr 4	

# System Cu–Fe

**Solution Phases:**

(stable)	:	Liquid, fcc- <i>A</i> 1, bcc- <i>A</i> 2
(metastable)	:	hcp- <i>A</i> 3

**Modelling:**

Liquid	:	Substitutional, Redlich–Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich–Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich–Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich–Kister

**Assessor and Date:**

I. Ansara, and Å. Jansson

**Publication:**

Trita-Mac-0533, Dec. 1993, Materials Research Center,  
The Royal Institute of Technology, Stockholm (Sweden)

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A*2**

$$I_{\text{Cu}, \text{Fe}: \square}^{0, \text{bcc}-A2} = 39258.0 - 4.14983 T$$

**Phase fcc-*A*1**

$$I_{\text{Cu}, \text{Fe}: \square}^{0, \text{fcc}-A1} = 48232.5 - 8.60954 T$$

$$I_{\text{Cu}, \text{Fe}: \square}^{1, \text{fcc}-A1} = 8861.88 - 5.28975 T$$

**Phase hcp-*A*3**

$$I_{\text{Cu}, \text{Fe}: \square}^{0, \text{hcp}-A3} = 48232.5 - 8.60954 T$$

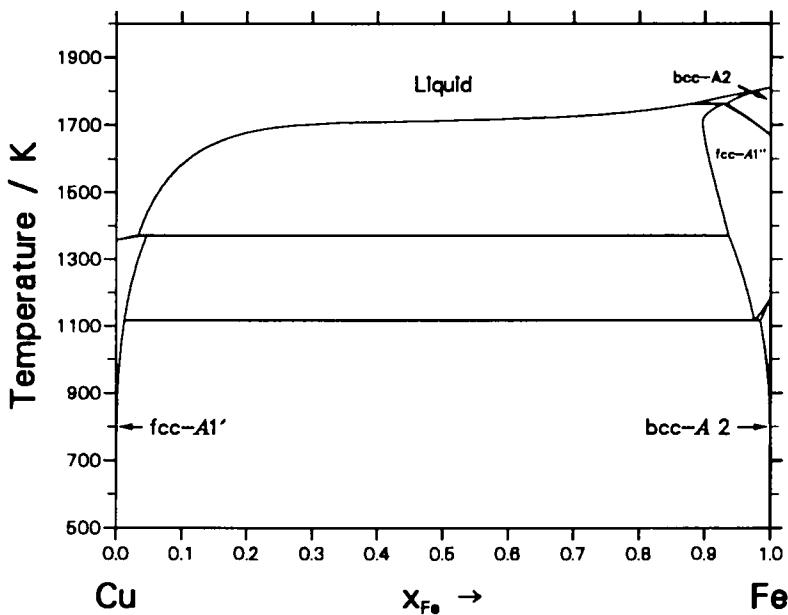
$$I_{\text{Cu}, \text{Fe}: \square}^{1, \text{hcp}-A3} = 8861.88 - 5.28975 T$$

**Phase liquid**

$$L_{\text{Cu},\text{Fe}}^{0,\text{liquid}} = 36088.0 - 2.32968 \ T$$

$$L_{\text{Cu},\text{Fe}}^{1,\text{liquid}} = 324.53 - 0.03270 \ T$$

$$L_{\text{Cu},\text{Fe}}^{2,\text{liquid}} = 10355.40 - 3.60297 \ T$$



**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Fe}}$				$T / \text{K}$
Liquid + bcc-A2 $\rightleftharpoons$ fcc-A1''	Peritectic	.880	.933	.927	1762.4	
Liquid + fcc-A1'' $\rightleftharpoons$ fcc-A1'	Peritectic	.034	.936	.047	1371.4	
fcc-A1'' $\rightleftharpoons$ fcc-A1' + bcc-A2	Eutectoid	.975	.012	.984	1115.9	

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group
Cu-Fe	(Cu)	Cu	$cF\bar{4}$ $Fm\bar{3}m$
	(Fe)	Cu	$cF\bar{4}$ $Fm\bar{3}m$
	(Fe)	W	$cl2$ $Im\bar{3}m$

# System Cu–Li

**Solution Phases:**

(stable)                      Liquid, bcc-*A*2, fcc-*A*1

**Solution Phases:**

(metastable)                hcp-*A*3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister

**Assessor and Date:**

N. Saunders, 1991

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A*2**

$$L_{\text{Cu},\text{Li};\square}^{0,\text{bcc-}A2} = 50000$$

**Phase fcc-*A*1**

$$L_{\text{Cu},\text{Li};\square}^{0,\text{fcc-}A1} = 2750 + 13.0 \cdot T$$

$$L_{\text{Cu},\text{Li};\square}^{1,\text{fcc-}A1} = -1000$$

**Phase hcp-*A*3**

$$L_{\text{Cu},\text{Li};\square}^{0,\text{hcp-}A3} = 2042 + 10.9617 \cdot T$$

**Phase liquid**

$$L_{\text{Cu},\text{Li}}^{0,\text{liquid}} = 66000 - 44.723 \cdot T$$

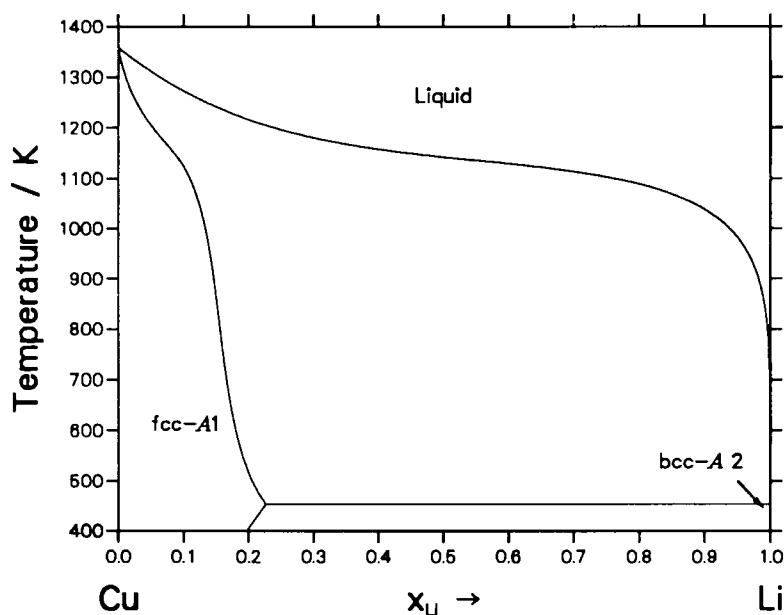


Table I – Invariant Reactions.

Reaction	Type	Compositions \$x_{\text{Li}}	\$T / \text{K}
$\text{Liquid} \rightleftharpoons \text{fcc}-A1 + \text{bcc}-A2$	Degenerate	1.000    0.228    1.000	453.6

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pears. Space Group	Symb. Group
Cu-Li	(Cu)	Cu	<i>cF</i> 4 <i>Fm</i> $\bar{3}m$	
	(Li)	W	<i>cI</i> 2 <i>Im</i> $\bar{3}m$	

# System Cu–Mg

**Solution Phases:**

(stable)	:	Liquid, fcc- <i>A</i> 1, hcp- <i>A</i> 3
(metastable)	:	bcc- <i>B</i> 2, hcp-Zn

**Compound:**

(stable)	Laves- <i>C</i> 15, CuMg <sub>2</sub>
(metastable)	Laves- <i>C</i> 14, Laves- <i>C</i> 36, CuZn- $\gamma$ MgZn, Mg <sub>2</sub> Zn <sub>3</sub> , Mg <sub>2</sub> Zn <sub>11</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Laves- <i>C</i> 15	:	Sublattice-model, Cu,Mg) <sub>0.5</sub> (Cu,Mg) <sub>0.5</sub> (□) <sub>3</sub>
CuMg <sub>2</sub>	:	Stoichiometric, CuMg <sub>2</sub>
bcc- <i>A</i> 2	:	see below
bcc- <i>B</i> 2	:	Sublattice model, (Cu,Mg) <sub>0.5</sub> (Cu,Mg) <sub>0.5</sub> Two descriptions of the bcc- <i>A</i> 2:bcc- <i>B</i> 2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.
hcp-Zn	:	Substitutional, Redlich-Kister
CuZn- $\gamma$	:	Stoichiometric, (Cu) <sub>2</sub> (Cu) <sub>2</sub> (Cu) <sub>3</sub> (Mg) <sub>6</sub>
Mg <sub>2</sub> Zn <sub>11</sub>	:	Stoichiometric, (Cu) <sub>11</sub> (Mg) <sub>2</sub>
Mg <sub>2</sub> Zn <sub>3</sub>	:	Stoichiometric, (Cu) <sub>3</sub> (Mg) <sub>2</sub>
MgZn	:	Stoichiometric, (Cu) <sub>13</sub> (Mg) <sub>12</sub>
Laves- <i>C</i> 14	:	Sublattice-model, (Cu,Mg) <sub>2</sub> (Cu,Mg)
Laves- <i>C</i> 36	:	Sublattice-model, (Cu,Mg) <sub>2</sub> (Cu,Mg)

**Assessor and Date:**

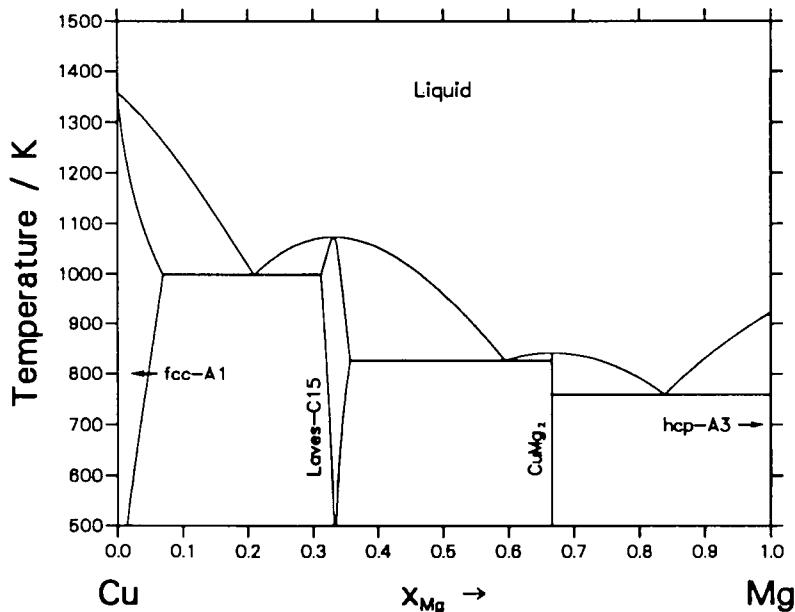
C.A. Coughnanowr, I. Ansara, R. Luoma,  
M. Hämäläinen, and H.L. Lukas

**Publication:**

Z. für Metallkde., 82, 7, 574-581 (1991).

**Comments:**

A new assessment was performed where the lattice stabilities of Cu and Mg in the Laves-*C*15 structure were taken equal to 15kJ/formula unit, in order to ensure consistency in the database.



Thermodynamic properties of the solution and compound phases ( $\text{J} \cdot \text{mol}^{-1}$ )

#### Phase liquid

$$L_{\text{Cu,Mg}}^{0,\text{liquid}} = -36962.71 + 4.74394 T$$

$$L_{\text{Cu,Mg}}^{\text{t,liquid}} = -8182.19$$

#### Phase fcc-A1

$$L_{\text{Cu,Mg}:□}^{0,\text{fcc-A1}} = -22059.61 + 5.63232 T$$

#### Phase hcp-A3

$$L_{\text{Cu,Mg}:□}^{0,\text{hcp-A3}} = 22500.0 - 3.0 T$$

### Phase hcp-Zn

$$L_{\text{Cu,Mg;}\square}^{0,\text{hcp-Zn}} = 22500.0 - 3.0 \cdot T$$

### Phase Laves-C14

$$G^\circ(T) - 3.0 \cdot H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 15000.0 + 3.0 \cdot \text{GHSER}_{\text{Cu}}$$

$$\begin{aligned} G^\circ(T) - 2.0 \cdot H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) &= G(\text{Cu:Mg}) = \\ &- 24691.0 + 364.73085 \cdot T - 69.276417 \cdot T \cdot \ln T - 5.19246E-04 \cdot T^2 \\ &+ 143502 \cdot T^{-1} - 5.65953E-6 \cdot T^3 \end{aligned}$$

$$\begin{aligned} G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) &= G(\text{Mg:Cu}) = \\ &74970.96 - 16.46448 \cdot T + \text{GHSER}_{\text{Cu}} + 2.0 \cdot \text{GHSER}_{\text{Mg}} \end{aligned}$$

$$G^\circ(T) - 3.0 \cdot H_{\text{Mg}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000.0 + 3.0 \cdot \text{GHSER}_{\text{Mg}}$$

$$L_{\text{Cu,Mg;Cu}}^{0,\text{Laves-C14}} = L_{\text{Cu,Mg;Mg}}^{0,\text{Laves-C14}} = 13011.35$$

$$L_{\text{Cu,Cu,Mg}}^{0,\text{Laves-C14}} = L_{\text{Mg,Cu,Mg}}^{0,\text{Laves-C14}} = 6599.45$$

### Phase Laves-C15

$$G^\circ(T) - 3.0 \cdot H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 15000.0 + 3.0 \cdot \text{GHSER}_{\text{Cu}}$$

$$\begin{aligned} G^\circ(T) - 2.0 \cdot H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) &= G(\text{Cu:Mg}) = \\ &- 54691.0 + 364.73085 \cdot T - 69.276417 \cdot T \cdot \ln T - 5.19246E-04 \cdot T^2 \\ &+ 143502 \cdot T^{-1} - 5.65953E-6 \cdot T^3 \end{aligned}$$

$$\begin{aligned} G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - 2.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) &= G(\text{Mg:Cu}) = \\ &104970.96 - 16.46448 \cdot T + \text{GHSER}_{\text{Cu}} + 2.0 \cdot \text{GHSER}_{\text{Mg}} \end{aligned}$$

$$G^\circ(T) - 3.0 \cdot H_{\text{Mg}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000.0 + 3.0 \cdot \text{GHSER}_{\text{Mg}}$$

$$L_{\text{Cu,Mg;Cu}}^{0,\text{Laves-C15}} = L_{\text{Cu,Mg;Mg}}^{0,\text{Laves-C15}} = 13011.35$$

$$L_{\text{Cu,Cu,Mg}}^{0,\text{Laves-C15}} = L_{\text{Mg,Cu,Mg}}^{0,\text{Laves-C15}} = 6599.45$$

### Phase Laves-C36

$$G^\circ(T) - 3.0 \cdot H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 15000.0 + 3.0 \cdot \text{GHSER}_{\text{Cu}}$$

$$\begin{aligned} G^\circ(T) - 2.0 \cdot H_{\text{Cu}}^{\circ,\text{fcc-A1}}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) &= G(\text{Cu:Mg}) = \\ &- 34691.0 + 364.73085 \cdot T - 69.276417 \cdot T \cdot \ln T - 5.19246E-04 \cdot T^2 \\ &+ 143502 \cdot T^{-1} - 5.65953E-6 \cdot T^3 \end{aligned}$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = \\ 84970.96 - 16.46448 T + \text{GHSER}_{\text{Cu}} + 2.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Mg}}$$

$$L_{\text{Cu},\text{Mg:Cu}}^{0,\text{Laves-C36}} = L_{\text{Cu},\text{Mg:Mg}}^{0,\text{Laves-C36}} = 13011.35$$

$$L_{\text{Cu:Cu,Mg}}^{0,\text{Laves-C36}} = L_{\text{Mg:Cu,Mg}}^{0,\text{Laves-C36}} = 6599.45$$

### Phase CuMg<sub>2</sub>

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 28620.0 + 1.86456 T + \text{GHSER}_{\text{Cu}} + 2.0 \text{ GHSER}_{\text{Mg}}$$

### Phase CuZn- $\gamma$

$$K4 = -11552.71 - 1.67824 T$$

$$K5 = 15732.3 - 10.26575 T$$

$$K7 = 9000.0 - 1.5 T$$

$$G^\circ(T) - 7.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 6.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Cu:Cu:Mg}) = \\ 13.0 K4 + 2.0 K5 + 6.0 K7 + 7.0 \text{ GHSER}_{\text{Cu}} + 6.0 \text{ GHSER}_{\text{Mg}}$$

### Phase Mg<sub>2</sub>Zn<sub>11</sub>

$$G^\circ(T) - 11.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = \\ 0.0 + 11.0 \text{ GHSER}_{\text{Cu}} + 2.0 \text{ GHSER}_{\text{Mg}}$$

### Phase Mg<sub>2</sub>Zn<sub>3</sub>

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = \\ 0.0 + 3.0 \text{ GHSER}_{\text{Cu}} + 2.0 \text{ GHSER}_{\text{Mg}}$$

### Phase MgZn

$$G^\circ(T) - 13.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 12.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = \\ 0.0 + 13.0 \text{ GHSER}_{\text{Cu}} + 12.0 \text{ GHSER}_{\text{Mg}}$$

### Phase bcc-B2

$$G^\circ\text{Cu : Mg} = 0.0$$

$$L^0\text{Cu, Mg} = -2500$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = \text{GBCC}_{\text{Cu}}$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Mg}) = \\ G^\circ\text{Cu : Mg} + 0.5 L_{\text{Cu},\text{Mg}}^0 + 0.5 \text{ GBCC}_{\text{Cu}} + 0.5 \text{ GBCC}_{\text{Mg}}$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = \\ G^*\text{Cu : Mg} + L_{\text{Cu,Mg}}^0 + 0.5 \text{ GBCC}_{\text{Cu}} + 0.5 \text{ GBCC}_{\text{Mg}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = \text{GBCC}_{\text{Mg}}$$

$$L_{\text{Cu,Mg:Cu:\square}}^{0,\text{bcc}-B2} = L_{\text{Cu,Mg:Mg:\square}}^{0,\text{bcc}-B2} = -G^*\text{Cu : Mg} + L^0\text{Cu, Mg}$$

$$L_{\text{Cu:Cu,Mg:\square}}^{0,\text{bcc}-B2} = L_{\text{Mg:Cu,Mg:\square}}^{0,\text{bcc}-B2} = -G^*\text{Cu : Mg} + L^0\text{Cu, Mg}$$

### Phase bcc-B2

$$G_{\text{Cu:Mg}}^* = 0.0$$

$$L_{\text{Cu,Mg}}^0 = -2500$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Mg}) = 2.0 G^*\text{Cu : Mg}$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Cu}) = 2.0 G^*\text{Cu : Mg}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 0.0$$

### Phase bcc-A2

$$L_{\text{Cu,Mg:\square}}^{0,\text{bcc}-A2} = 4.0 L^0\text{Cu, Mg}$$

**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Mg}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ fcc-A1 + Laves-C15	Eutectic	.209	.069	.313	998.6
Liquid $\rightleftharpoons$ Laves-C15 + CuMg <sub>2</sub>	Eutectic	.595	.356	.667	825.5
Liquid $\rightleftharpoons$ CuMg <sub>2</sub> + hcp-A3	Eutectic	.839	.667	1.000	759.7
CuMg <sub>2</sub> $\rightleftharpoons$ Liquid	Congruent	0.666	0.666	...	841.0
Laves-C15 $\rightleftharpoons$ Liquid	Congruent	0.333	0.333	...	1073.5

# System Cu-Ni

**Solution Phases:**

(stable)	Liquid, fcc-A1
(metastable)	bcc-A2, hcp-A3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
fcc-A1	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister

**Assessor and Date:**

S. an Mey

**Publication:**

Calphad, **16**, (3), 255-260 (1992).

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

$$L_{\text{Cu},\text{Ni};\square}^{0,\text{bcc}-A2} = 8047.72 + 3.42217 \cdot T$$

$$L_{\text{Cu},\text{Ni};\square}^{1,\text{bcc}-A2} = -2041.3 + 0.99714 \cdot T$$

**Phase fcc-A1**

$$L_{\text{Cu},\text{Ni};\square}^{0,\text{fcc}-A1} = 8047.72 + 3.42217 \cdot T$$

$$L_{\text{Cu},\text{Ni};\square}^{1,\text{fcc}-A1} = -2041.3 + 0.99714 \cdot T$$

$$T_{\text{c,Cu},\text{Ni};\square}^{0,\text{fcc}-A1} = -935.5$$

$$T_{\text{c,Cu},\text{Ni};\square}^{1,\text{fcc}-A1} = -594.9$$

$$\beta_{\text{Cu},\text{Ni};\square}^{0,\text{mag,fcc}-A1} = -0.7316$$

$$\beta_{\text{Cu},\text{Ni};\square}^{1,\text{mag,fcc}-A1} = -0.3174$$

**Phase hcp-A3**

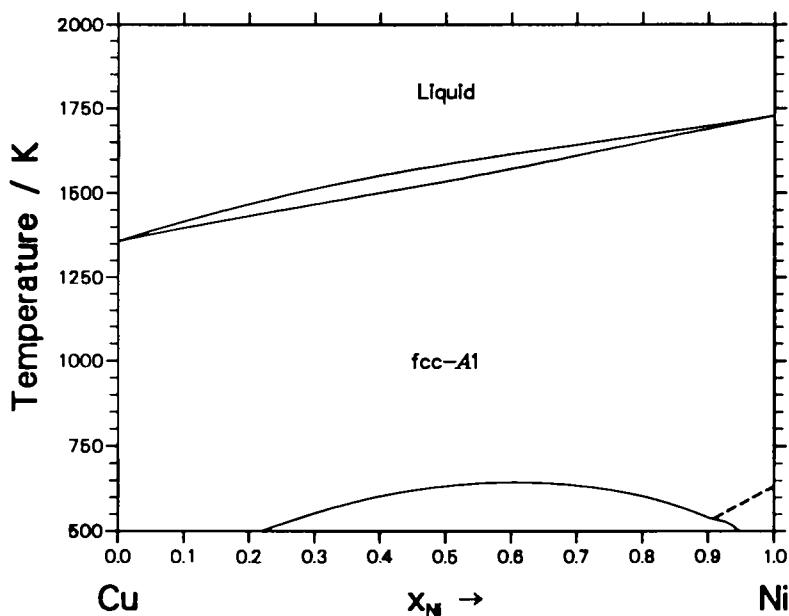
$$L_{\text{Cu},\text{Ni};\square}^{0,\text{hcp}-A3} = 8047.72 + 3.42217 \ T$$

$$L_{\text{Cu},\text{Ni};\square}^{1,\text{hcp}-A3} = -2041.3 + 0.99714 \ T$$

**Phase liquid**

$$L_{\text{Cu},\text{Ni}}^{0,\text{liquid}} = 12048.61 + 1.29893 \ T$$

$$L_{\text{Cu},\text{Ni}}^{1,\text{liquid}} = -1861.61 + 0.94201 \ T$$

**Table I – Invariant Reaction.**

Reaction	Type	Compositions $x_{\text{Ni}}$	$T / \text{K}$
$\text{fcc}-A1' \rightleftharpoons \text{fcc}-A1''$	Critical Temp.	0.600    0.600    .....	641.0

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group
Cu–Ni	(Cu)	Cu	$cF\bar{4}$ $Fm\bar{3}m$
	(Ni)	Cu	$cF\bar{4}$ $Fm\bar{3}m$

# System Cu–Si

**Solution Phases:**

(stable)	Liquid, bcc- <i>A2</i> , fcc- <i>A1</i>
(metastable)	hcp- <i>A3</i>

**Compounds:**

(stable)	Cu <sub>56</sub> Si <sub>11</sub> - $\gamma$ , Cu <sub>4</sub> Si- $\epsilon$ , Cu <sub>19</sub> Si <sub>6</sub> - $\eta$ , Cu <sub>33</sub> Si <sub>7</sub> - $\delta$
(metastable)	Laves- <i>C15</i>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A2</i>	:	Substitutional, Redlich-Kister
fcc- <i>A1</i>	:	Substitutional, Redlich-Kister
hcp- <i>A3</i>	:	Substitutional, Redlich-Kister
Cu <sub>56</sub> Si <sub>11</sub> - $\gamma$	:	Stoichiometric, (Cu) <sub>56</sub> (Si)
Cu <sub>4</sub> Si- $\epsilon$	:	Stoichiometric, (Cu) <sub>4</sub> (Si)
Cu <sub>19</sub> Si <sub>6</sub> - $\eta$	:	Stoichiometric, (Cu) <sub>19</sub> (Si) <sub>6</sub>
Cu <sub>33</sub> Si <sub>7</sub> - $\delta$	:	Stoichiometric, (Cu) <sub>33</sub> (Si) <sub>7</sub>
Laves- <i>C15</i>	:	Sublattice model, (Cu,Si) <sub>2</sub> (Cu,Si)

**Assessor and Date:**

M. Jacobs, 1991. Revised by T. Bühler et al. 1997

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A2***

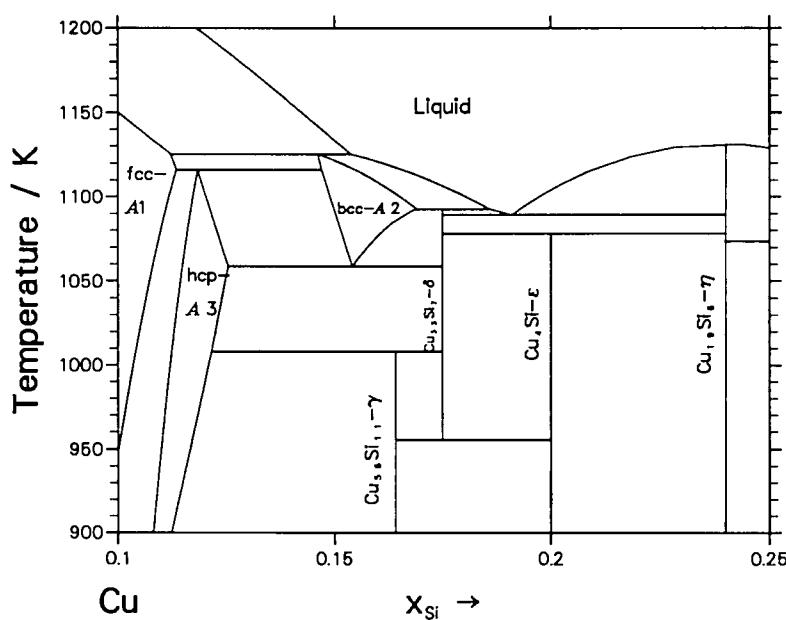
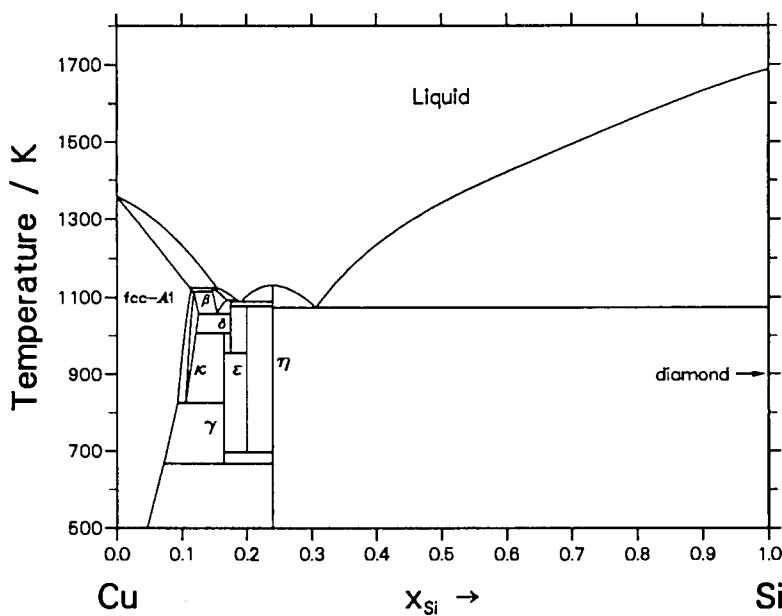
$$L_{\text{Cu},\text{Si}:0}^{0,\text{bcc}-\text{A}2} = -21740 + 3.9 \cdot T$$

$$L_{\text{Cu},\text{Si}:0}^{1,\text{bcc}-\text{A}2} = -40000 - 4.39 \cdot T$$

$$L_{\text{Cu},\text{Si}:0}^{2,\text{bcc}-\text{A}2} = -100$$

**Phase fcc-*A1***

$$L_{\text{Cu},\text{Si}:0}^{0,\text{fcc}-\text{A}1} = -34105.96 - 1.908 \cdot T$$



**Phase hcp-A3**

$$L_{\text{Cu},\text{Si}: \square}^{0,\text{hcp}-\text{A}3} = -19948 - 2.356 T$$

$$L_{\text{Cu},\text{Si}: \square}^{1,\text{hcp}-\text{A}3} = -23800 - 1.97 T$$

$$L_{\text{Cu},\text{Si}: \square}^{2,\text{hcp}-\text{A}3} = -20$$

**Phase liquid**

$$L_{\text{Cu},\text{Si}}^{0,\text{liquid}} = -39688.86 + 14.27467 T$$

$$L_{\text{Cu},\text{Si}}^{1,\text{liquid}} = -49937.13 + 29.78960 T$$

$$L_{\text{Cu},\text{Si}}^{2,\text{liquid}} = -31810.16 + 18.00804 T$$

**Phase Cu<sub>33</sub>Si<sub>7</sub>-δ**

$$\begin{aligned} G^\circ(T) - 33.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 7.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ -200372.4 + 4985.675 T - 955.5312 T \cdot \ln T - 0.101066 T^2 \\ + 4.2396E-06 T^3 + 2968440 T^{-1} \end{aligned}$$

**Phase Cu<sub>56</sub>Si<sub>11</sub>-γ**

$$\begin{aligned} G^\circ(T) - 56.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 11.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ 69000 + 405 T - 107.73 T \cdot \ln T + 46.0 \text{ GIISER}_{\text{Cu}} \\ + 11.0 \text{ GIISER}_{\text{Si}} \end{aligned}$$

**Phase Cu<sub>4</sub>Si-ε**

$$\begin{aligned} G^\circ(T) - 4.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ -39974.35 + 858.5047 T - 154.6764 T \cdot \ln T \\ + 0.01074864 T^2 + 5.1335E-07 T^3 + 386580 T^{-1} \end{aligned}$$

**Phase Cu<sub>19</sub>Si<sub>6</sub>-η**

$$\begin{aligned} G^\circ(T) - 19.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 6.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ -137488.5 + 3119.537 T - 595.1259 T \cdot \ln T - 0.0619575 T^2 \\ + 2.434E-06 T^3 + 2057075 T^{-1} \end{aligned}$$

**Phase Laves-C15**

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = \\ 15000.0 + 3.0 \text{ GIISER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Cu:Si}) \\ 15000.0 + 2.0 \text{ GIISER}_{\text{Cu}} + \text{GIISER}_{\text{Si}}$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 2.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Cu}) \\ 15000.0 + \text{GIISER}_{\text{Cu}} + 2.0 \text{ GIISER}_{\text{Si}}$$

$$G^\circ(T) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si}) \\ 15000.0 + 3.0 \text{ GHSER}_{\text{Si}}$$

$$L_{\text{Cu},\text{Si:Cu}}^{0,\text{Laves}-\text{C}15} = L_{\text{Cu},\text{Si:Si}}^{0,\text{Laves}-\text{C}15} = 15305 + 20.69 T$$

Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Si}}$			$T / \text{K}$
Liquid + fcc-A1 $\rightleftharpoons$ $\beta^*$	Peritectic	.154	.112	.146	1125.4
fcc-A1 + $\beta^*$ $\rightleftharpoons$ $\beta^{**}$	Peritectoid	.113	.147	.118	1115.9
$\beta^* \rightleftharpoons \beta^{**} + \delta$	Eutectoid	.154	.125	.175	1058.6
Liquid + $\beta^*$ $\rightleftharpoons$ $\delta$	Peritectic	.186	.169	.175	1092.7
Liquid $\rightleftharpoons$ $\delta + \eta$	Eutectic	.191	.175	.240	1089.2
$\eta + \delta \rightleftharpoons \epsilon$	Peritectoid	.175	.240	.200	1077.9
$\delta \rightleftharpoons \beta^{***} + \epsilon$	Eutectoid	.175	.164	.200	955.6
$\beta^{**} + \delta \rightleftharpoons \beta^{***}$	Peritectoid	.121	.175	.164	1008.3
$\epsilon \rightleftharpoons \beta^{***} + \eta$	Eutectoid	.200	.164	.240	696.5
$\beta^{**} \rightleftharpoons$ fcc-A1 + $\beta^{***}$	Eutectoid	.105	.093	.164	825.5
$\beta^{***} \rightleftharpoons$ fcc-A1 + $\eta$	Eutectoid	.164	.072	.240	667.8
Liquid $\rightleftharpoons$ $\eta + \text{diamond}$	Eutectic	.306	.240	1.000	1073.7
$\eta \rightleftharpoons$ Liquid	Congruent	.240	.240	....	1132.0

\*  $\beta \equiv$  bcc-A2, \*\*  $\kappa \equiv$  hcp-A3, \*\*\*  $\gamma \equiv$  cub-A13

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Cu-Si	(Cu)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Si)	diamond	$cF8$ $Fd\bar{3}m$	M 8	
	$\kappa$	Mg	$hP2$ $P6_3/mmc$	M 2	hcp-A3 $\text{Cu}_7\text{Si}$ in [91Vii]
	$\text{Cu}_3\text{Si}$		$t^{**}$		$\eta, \eta', \eta''$ in $\text{M}_{23}$ denoted $\text{Cu}_4\text{Si}-\epsilon$
	$\delta$		$hP72$		
	$\gamma$	$\beta$ -Mn	$cP20$ $P4_{1}32$	$M_1$ 8 $M_2$ 12	
	$\beta$	W	$cI2$ $Im\bar{3}m$	M 2	bcc-A2

## System Cu-Y

**Solution Phases:**

Liquid, bcc-A2, hcp-A3, Cu<sub>6</sub>Y

**Compound:**

Cu<sub>4</sub>Y, Cu<sub>6</sub>Y, Cu<sub>7</sub>Y<sub>2</sub>, Cu<sub>2</sub>Y-R, Cu<sub>2</sub>Y-H, CuY

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Cu <sub>6</sub> Y	:	Sublattice model, (Cu) <sub>5</sub> (Cu <sub>2</sub> ,Y)
Cu <sub>4</sub> Y	:	Stoichiometric, (Cu) <sub>4</sub> (Y)
Cu <sub>7</sub> Y <sub>2</sub>	:	Stoichiometric, (Cu) <sub>7</sub> (Y) <sub>2</sub>
Cu <sub>2</sub> Y-R	:	Stoichiometric, (Cu) <sub>2</sub> (Y)
Cu <sub>2</sub> Y-H	:	Stoichiometric, (Cu) <sub>2</sub> (Y)
CuY	:	Stoichiometric, (Cu)(Y)

**Assessor and Date:**

T. Jantzen, 1997.

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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase bcc-A2**

$$L_{\text{Cu},\text{Y}:0}^{0,\text{bcc}-\text{A}2} = 80.0 \ T$$

**Phase hcp-A3**

$$L_{\text{Cu},\text{Y}:0}^{0,\text{hcp}-\text{A}3} = 80.0 \ T$$

**Phase liquid**

$$L_{\text{Cu},\text{Y}}^{0,\text{liquid}} = -88958.06 + 21.5667 \ T$$

$$L_{\text{Cu},\text{Y}}^{1,\text{liquid}} = -33607.31 + 3.10462 \ T$$

$$L_{\text{Cu},\text{Y}}^{2,\text{liquid}} = 8083.16 - 0.74669 \ T$$

**Phase fcc-A1**

$$L_{\text{Cu,Y}}^{0,\text{fcc}-A1} = 80.0 \text{ } T$$

**Phase Cu<sub>2</sub>Y-R**

$$G^\circ(T) - 2.0 \text{ } H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 65324.22 + 6.03462 \text{ } T + 2.0 \text{ } \text{GHSER}_{\text{Cu}} + \text{GHSER}_Y$$

**Phase Cu<sub>2</sub>Y-H**

$$G^\circ(T) - 2.0 \text{ } H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 51788.22 - 5.96538 \text{ } T + 2.0 \text{ } \text{GHSER}_{\text{Cu}} + \text{GHSER}_Y$$

**Phase Cu<sub>4</sub>Y**

$$G^\circ(T) - 4.0 \text{ } H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 89328.5 + 8.25205 \text{ } T + 4.0 \text{ } \text{GHSER}_{\text{Cu}} + \text{GHSER}_Y$$

**Phase Cu<sub>6</sub>Y**

$$G^\circ(T) - 7.0 \text{ } H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu:Cu}_2) = \\ 35000.0 + 7.0 \text{ } \text{GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 5.0 \text{ } H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 89797.58 + 8.2954 \text{ } T + 5.0 \text{ } \text{GHSER}_{\text{Cu}} + \text{GHSER}_Y$$

$$L_{\text{Cu:Cu}_2,Y}^{0,\text{Cu}_6\text{Y}} = - 34386.27 + 3.17656 \text{ } T$$

**Phase Cu<sub>7</sub>Y<sub>2</sub>**

$$G^\circ(T) - 7.0 \text{ } H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 \text{ } H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 168519.6 + 15.56757 \text{ } T + 7.0 \text{ } \text{GHSER}_{\text{Cu}} + 2.0 \text{ } \text{GHSER}_Y$$

**Phase CuY**

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Cu:Y}) = \\ - 44616.68 + 4.12162 \text{ } T + \text{GHSER}_{\text{Cu}} + \text{GHSER}_Y$$

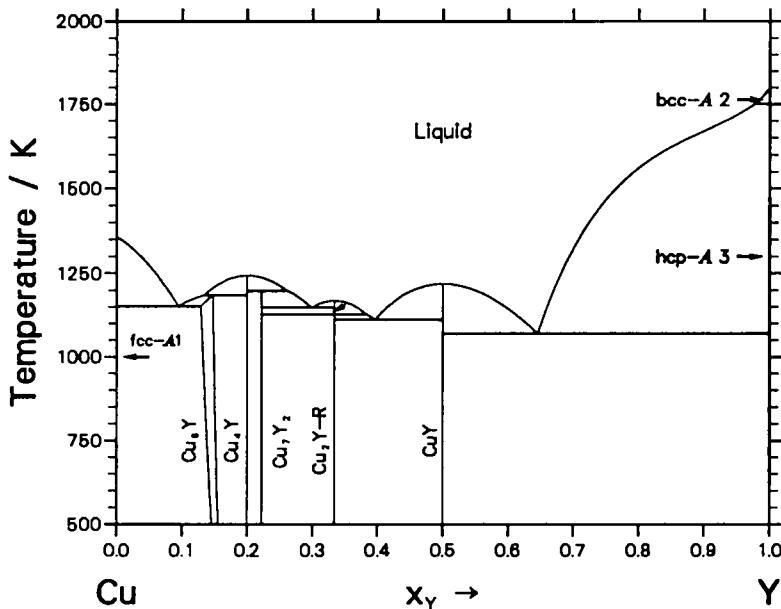


Table I - Invariant Reactions.

Reaction	Type	Compositions $xy$			$T / K$
$Liquid \rightleftharpoons CuY + hcp-A3$	Eutectic	.646	.646	1.000	1070.0
$Liquid \rightleftharpoons Cu_2Y-R + CuY$	Eutectic	.396	.333	.500	1113.0
$Liquid \rightleftharpoons Cu_2Y-H + Cu_7Y_2$	Eutectic	.299	.222	.333	1148.6
$Liquid \rightleftharpoons Cu_4Y + Cu_7Y_2$	Peritectic	.262	.200	.222	1198.0
$Liquid + Cu_4Y \rightleftharpoons Cu_6Y$	Peritectic	.133	.200	.147	1184.0
$Liquid \rightleftharpoons fcc-A1 + Cu_6Y$	Eutectic	.094	.000	.129	1153.0
$hcp-A3 \rightleftharpoons bcc-A2$	Polymorphic	1.000	1.000	....	1752.0
$Cu_2Y-R \rightleftharpoons Cu_2Y-H$	Polymorphic	.333	.333	....	1128.0
$Liquid \rightleftharpoons Cu_4Y$	Congruent	.200	.200	....	1224.0
$Liquid \rightleftharpoons Cu_2Y-H$	Congruent	.333	.333	....	1149.0
$Liquid \rightleftharpoons CuY$	Congruent	.500	.500	....	1220.0

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Cu-Y	(Cu)	Cu	<i>cF</i> 4 <i>Fm</i> 3 <i>m</i>	M 4	
	(Y)	W	<i>cI</i> 2 <i>Im</i> 3 <i>m</i>	M 4	
	(Y)	Mg	<i>hP</i> 2 <i>P</i> 63/ <i>mmc</i>	M 2	
	Cu <sub>6</sub> Y				not in [91Vil]
	Cu <sub>5</sub> Y	CaCu <sub>5</sub>	<i>hP</i> 6 <i>P</i> 6/ <i>mmm</i>	Y 1 Cu <sub>1</sub> 2 Cu <sub>2</sub> 3	quoted as metastable in 90Mas]
	Cu <sub>4</sub> Y	CaCu <sub>5</sub> ?	<i>hP</i> 6 <i>P</i> 6/ <i>mmm</i>		not quoted in [91Vil]
	Cu <sub>7</sub> Y <sub>2</sub>				not in [91Vil]
	Cu <sub>2</sub> Y	CeCu <sub>2</sub>	<i>oI</i> 12 <i>Imma</i>	Y 4 Cu 8	
	CuY	CsCl	<i>cP</i> 2 <i>Pm</i> 3 <i>m</i>	Cu 1 Y 1	bcc-B2

## System Cu-Zn

**Solution Phases:**

(stable) : Liquid, bcc-*A*2, bcc-*B*2, fcc-*A*1, hcp-*A*3(CuZn- $\epsilon$ ), hcp-Zn  
 :  
 :

**Solution Phases:**

(stable) : CuZn- $\gamma$   
 (metastable) : Laves-*C*14, Laves-*C*15, Laves-*C*36

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3(CuZn- $\epsilon$ )	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister
CuZn- $\gamma$	:	Sublattice, $(\text{Cu}, \text{Zn})_2(\text{Cu}, \text{Zn})_2(\text{Cu})_3(\text{Zn})_6$
bcc- <i>A</i> 2	:	see below
bcc- <i>B</i> 2	:	Sublattice model, $(\text{Cu}, \text{Zn})_{0.5}(\text{Cu}, \text{Zn})_{0.5}(\square)_3$ Two descriptions of the bcc- <i>A</i> 2:bcc- <i>B</i> 2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame. Two descriptions of the bcc- <i>A</i> 2:bcc- <i>B</i> 2 order-disorder
Laves- <i>C</i> 14	:	Sublattice model, $(\text{Cu}, \text{Zn})_2(\text{Cu}, \text{Zn})$
Laves- <i>C</i> 15	:	Sublattice model, $(\text{Cu}, \text{Zn})_2(\text{Cu}, \text{Zn})$
Laves- <i>C</i> 36	:	Sublattice model, $(\text{Cu}, \text{Zn})_2(\text{Cu}, \text{Zn})$

**Assessor and Date:**

M. Kowalski, and P.J. Spencer,

**Publication:**

J. Phase Equil., 14, 4, 432-438 (1993).

**Comments:**

Based on Kowalski's data, a new assessment was performed to differentiate the two hexagonal forms of Zn.

**Thermodynamic properties of the solution and compound phases(J.mol<sup>-1</sup>)****Phase fcc-A1**

$$L_{\text{Cu},\text{Zn}:□}^{0,\text{fcc}-\text{A1}} = -42803.75 + 10.02258 \ T$$

$$L_{\text{Cu},\text{Zn}:□}^{1,\text{fcc}-\text{A1}} = 2936.39 - 3.05323 \ T$$

$$L_{\text{Cu},\text{Zn}:□}^{2,\text{fcc}-\text{A1}} = 9034.2 - 5.39314 \ T$$

**Phase hcp-A3**

$$L_{\text{Cu},\text{Zn}:□}^{0,\text{hcp}-\text{A3}} = -36475 + 4.896 \ T$$

$$L_{\text{Cu},\text{Zn}:□}^{1,\text{hcp}-\text{A3}} = 24790.0 - 10.135 \ T$$

**Phase hcp-Zn**

$$L_{\text{Cu},\text{Zn}}^{0,\text{hcp}-\text{Zn}} = -14432.17 - 10.7814 \ T$$

**Phase liquid**

$$L_{\text{Cu},\text{Zn}}^{0,\text{liquid}} = -40695.54 + 12.65269 \ T$$

$$L_{\text{Cu},\text{Zn}}^{1,\text{liquid}} = 4402.72 - 6.55425 \ T$$

$$L_{\text{Cu},\text{Zn}}^{2,\text{liquid}} = 7818.1 - 3.25416 \ T$$

**Phase bcc-B2**

$$G_{\text{Cu},\text{Zn}:□}^* = -3085.0$$

$$L_{\text{Cu},\text{Zn}}^0 = -12898.97 + 3.26598 \ T$$

$$L_{\text{Cu},\text{Zn}}^1 = 945.265 - 0.80679 \ T$$

$$L_{\text{Cu},\text{Zn}}^2 = 1921.485 - 1.86969 \ T$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) = G(\text{Cu:Cu:□}) = \text{GBCC}_{\text{Cu}}$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-\text{A1}}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu:Zn:□}) = \\ G_{\text{Cu:Zn}}^* + L_{\text{Cu},\text{Zn}}^0 + 0.5 \text{GBCC}_{\text{Cu}} + 0.5 \text{GBCC}_{\text{Zn}}$$

$$\begin{aligned}
G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) &= G(\text{Zn}: \text{Cu}: \square) = \\
G_{\text{Cu}: \text{Zn}: \square}^* + L_{\text{Cu}, \text{Zn}}^0 + 0.5 \text{ GBCC}_{\text{Cu}} + 0.5 \text{ GBCC}_{\text{Zn}} \\
G^\circ(T) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) &= G(\text{Zn}: \text{Zn}: \square) = \text{GBCC}_{\text{Zn}} \\
L_{\text{Cu}, \text{Zn}: \text{Cu}: \square}^{0, \text{bcc}-B2} &= L_{\text{Cu}: \text{Cu}, \text{Zn}: \square}^{0, \text{bcc}-B2} = -G_{\text{Cu}: \text{Zn}: \square}^* + L_{\text{Cu}, \text{Zn}}^0 + 3.0 L_{\text{Cu}, \text{Zn}}^1 + 3.0 L_{\text{Cu}, \text{Zn}}^2 \\
L_{\text{Cu}, \text{Zn}: \text{Cu}: \square}^{1, \text{bcc}-B2} &= L_{\text{Cu}: \text{Cu}, \text{Zn}: \square}^{1, \text{bcc}-B2} = L_{\text{Cu}, \text{Zn}}^1 + 4.0 L_{\text{Cu}, \text{Zn}}^2 \\
L_{\text{Cu}, \text{Zn}: \text{Cu}: \square}^{2, \text{bcc}-B2} &= L_{\text{Cu}: \text{Cu}, \text{Zn}: \square}^{2, \text{bcc}-B2} = L_{\text{Cu}, \text{Zn}}^2 \\
L_{\text{Cu}, \text{Zn}: \text{Zn}: \square}^{0, \text{bcc}-B2} &= L_{\text{Zn}: \text{Cu}, \text{Zn}: \square}^{0, \text{bcc}-B2} = -G_{\text{Cu}: \text{Zn}: \square}^* + L_{\text{Cu}, \text{Zn}}^0 - 3.0 L_{\text{Cu}, \text{Zn}}^1 + 3.0 L_{\text{Cu}, \text{Zn}}^2 \\
L_{\text{Cu}, \text{Zn}: \text{Zn}: \square}^{1, \text{bcc}-B2} &= L_{\text{Zn}: \text{Cu}, \text{Zn}: \square}^{1, \text{bcc}-B2} = L_{\text{Cu}, \text{Zn}}^1 - 4.0 L_{\text{Cu}, \text{Zn}}^2 \\
L_{\text{Cu}, \text{Zn}: \text{Zn}: \square}^{2, \text{bcc}-B2} &= L_{\text{Zn}: \text{Cu}, \text{Zn}: \square}^{2, \text{bcc}-B2} = L_{\text{Cu}, \text{Zn}}^2 \\
L_{\text{Cu}, \text{Zn}: \text{Cu}, \text{Zn}: \square}^{0, \text{bcc}-B2} &= -24.0 L_{\text{Cu}, \text{Zn}}^2
\end{aligned}$$

### Phase bcc-B2

$$\begin{aligned}
G_{\text{Cu}: \text{Zn}: \square}^* &= -3085.0 \\
L_{\text{Cu}, \text{Zn}}^0 &= -12898.97 + 3.26598 T \\
L_{\text{Cu}, \text{Zn}}^1 &= 945.265 - 0.80679 T \\
L_{\text{Cu}, \text{Zn}}^2 &= 1921.485 - 1.86969 T
\end{aligned}$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu}: \text{Cu}: \square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu}: \text{Zn}: \square) = 2.0 G_{\text{Cu}: \text{Zn}: \square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}: \text{Cu}: \square) = 2.0 G_{\text{Cu}: \text{Zn}: \square}^*$$

$$G^\circ(T) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}: \text{Zn}: \square) = 0.0$$

### Phase bcc-A2

$$\begin{aligned}
L_{\text{Cu}, \text{Zn}: \square}^{0, \text{bcc}-A2} &= 4.0 L_{\text{Cu}, \text{Zn}}^0 \\
L_{\text{Cu}, \text{Zn}: \square}^{1, \text{bcc}-A2} &= 8.0 L_{\text{Cu}, \text{Zn}}^1 \\
L_{\text{Cu}, \text{Zn}: \square}^{2, \text{bcc}-A2} &= 16.0 L_{\text{Cu}, \text{Zn}}^2
\end{aligned}$$

### Phase CuZn- $\gamma$

$$K4 = -11552.71 - 1.67824 T$$

$$K5 = 15732.3 - 10.26575 T$$

$$K6 = 37289.2 - 13.05259 T$$

$$G^\circ(T) - 7.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 6.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu}:\text{Cu}:\text{Zn}) = \\ 13.0 K4 + 2.0 K5 + 7.0 \text{ GHSER}_{\text{Cu}} + 6.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 5.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 8.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Cu}:\text{Zn}) = \\ 13.0 K4 + 2.0 K5 + 2.0 K6 + 5.0 \text{ GHSER}_{\text{Cu}} + 8.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 5.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 8.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu}:\text{Zn}:\text{Cu}:\text{Zn}) = \\ 13.0 K4 + 5.0 \text{ GHSER}_{\text{Cu}} + 8.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 10.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Zn}:\text{Cu}:\text{Zn}) = \\ 13.0 K4 + 2.0 K6 + 3.0 \text{ GHSER}_{\text{Cu}} + 10.0 \text{ GHSER}_{\text{Zn}}$$

### Phase Laves-C14

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu}:\text{Cu}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu}:\text{Zn}) = \\ 15000.0 + 2.0 \text{ GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Cu}) = \\ 15000.0 + \text{GHSER}_{\text{Cu}} + 2.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Zn}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Cu},\text{Zn}:\text{Cu}}^{0,\text{Laves}-\text{C}14} = L_{\text{Cu},\text{Zn}:\text{Zn}}^{0,\text{Laves}-\text{C}14} = -75305.48$$

### Phase Laves-C15

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu}:\text{Cu}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu}:\text{Zn}) = \\ 15000.0 + 2.0 \text{ GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Cu}) = \\ 15000.0 + \text{GHSER}_{\text{Cu}} + 2.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn}:\text{Zn}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Cu},\text{Zn}:\text{Cu}}^{0,\text{Laves}-\text{C}15} = L_{\text{Cu},\text{Zn}:\text{Zn}}^{0,\text{Laves}-\text{C}15} = -78824.62$$

$$L_{\text{Cu},\text{Zn}:\text{Cu}}^{1,\text{Laves}-\text{C}15} = L_{\text{Cu},\text{Zn}:\text{Zn}}^{1,\text{Laves}-\text{C}15} = 25529.06$$

### Phase Laves-C36

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) = G(\text{Cu:Cu}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Cu}}$$

$$G^\circ(T) - 2.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Cu:Zn}) = \\ 15000.0 + 2.0 \text{ GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Cu}) = \\ 15000.0 + \text{GHSER}_{\text{Cu}} + 2.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Zn}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Cu},\text{Zn:Cu}}^{0,\text{Laves-C36}} = L_{\text{Cu},\text{Zn:Zn}}^{0,\text{Laves-C36}} = -90226.26$$

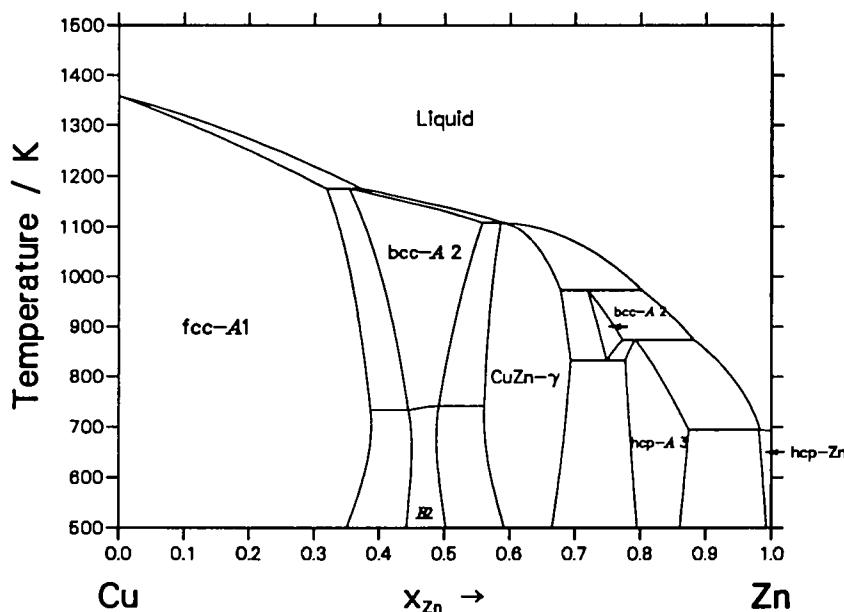


Table I – Invariant Reactions.

Reaction	Type	Compositions \$x_{\text{Zn}}			\$T / \text{K}
Liquid + fcc-A1 \$\rightleftharpoons\$ bcc-A2	Peritectic	.373	.319	.353	1175.3
Liquid + bcc-A2 \$\rightleftharpoons\$ CuZn-\$\gamma\$	Peritectic	.592	.558	.586	1108.3
Liquid + CuZn-\$\gamma\$ \$\rightleftharpoons\$ bcc-A2	Peritectic	.802	.678	.719	972.5
Liquid + bcc-A2 \$\rightleftharpoons\$ hcp-A3	Peritectic	.882	.773	.792	873.4
bcc-A2 \$\rightleftharpoons\$ CuZn-\$\gamma\$ + hcp-A3	Eutectoid	.748	.693	.777	831.9
Liquid + hcp-A3 \$\rightleftharpoons\$ hcp-Zn	Peritectic	.983	.874	.981	694.4

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
Cu-Zn	(Cu)	Cu	$cF\bar{4}$ $Pm\bar{3}m$	M 4	
	(Zn)	Mg	$hP2$ $P\bar{6}_3/mmc$	M 2	
	$\beta$	W	$cI2$ $I\bar{m}\bar{3}m$	M 2	bcc-A2
	$\beta'$	CsCl	$cP2$ $Pm\bar{3}m$	Cu 1 Zn 1	bcc-B2
	$\delta$	$CuZn_2$	$hP9$ $P\bar{6}$	Cu 1 Zn <sub>1</sub> 1 Zn <sub>2</sub> 1	assumed as bcc-A2
	$\epsilon$	Mg	$hP2$ $P\bar{6}_3mmc$	M 2	CuZn-A3
	$\gamma$	$Cu_5Zn_8$	$cI52$ $I\bar{4}\bar{3}m$	Cu <sub>1</sub> 8 Cu <sub>2</sub> 12 Zn <sub>1</sub> 8 Zn <sub>2</sub> 24	Cu <sub>5</sub> Zn

# System Cu-Zr

**Solution Phases:**

Liquid, bcc-*A*2, hcp-*A*3

**Compounds:**

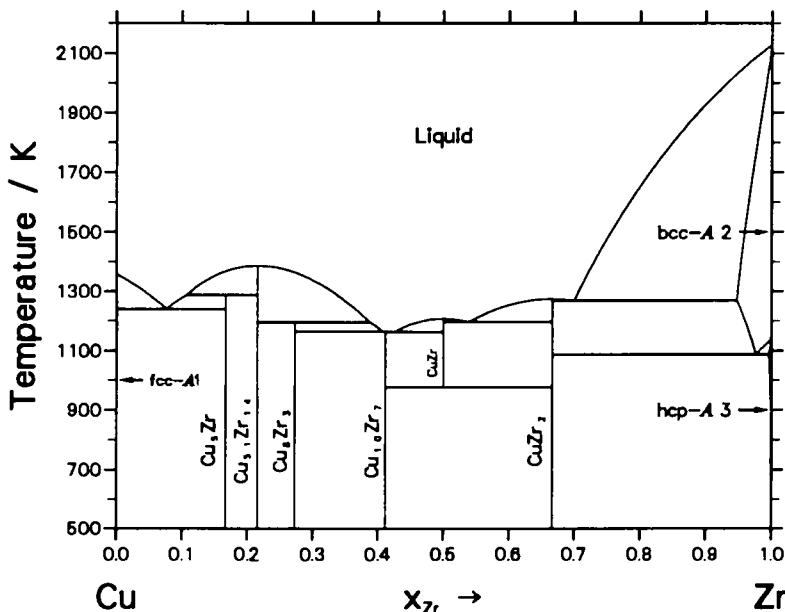
$\text{Cu}_5\text{Zr}$ ,  $\text{Cu}_{51}\text{Zr}_{14}$ ,  $\text{Cu}_{10}\text{Zr}_7$ ,  $\text{CuZr}$ ,  $\text{CuZr}_2$ ,  $\text{Cu}_8\text{Zr}_3$

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
$\text{Cu}_5\text{Zr}$	:	Stoichiometric, $(\text{Cu})_5(\text{Zr})$
$\text{Cu}_{51}\text{Zr}_{14}$	:	Stoichiometric, $(\text{Cu})_{51}(\text{Zr})_{14}$
$\text{Cu}_{10}\text{Zr}_7$	:	Stoichiometric, $(\text{Cu})_{10}(\text{Zr})_7$
$\text{Cu}_8\text{Zr}_3$	:	Stoichiometric, $(\text{Cu})_8(\text{Zr})_3$
$\text{CuZr}$	:	Stoichiometric, $(\text{Cu})(\text{Zr})$
$\text{CuZr}_2$	:	Stoichiometric, $(\text{Cu})(\text{Zr})_2$

**Assessor and Date:**

K. Zeng, and M. Hämäläinen 1993



**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)****Phase bcc-A2**

$$I_{\text{Cu},\text{Zr}:0}^{0,\text{bcc}-A2} = -7381.13$$

**Phase fcc-A1**

$$I_{\text{Cu},\text{Zr}:0}^{0,\text{fcc}-A1} = 2233$$

**Phase hcp-A3**

$$I_{\text{Cu},\text{Zr}:0}^{0,\text{hcp}-A3} = 11336.85$$

**Phase liquid**

$$I_{\text{Cu},\text{Zr}}^{0,\text{liquid}} = -61685.53 + 11.29235 T$$

$$I_{\text{Cu},\text{Zr}}^{1,\text{liquid}} = -8830.66 + 5.04565 T$$

**Phase Cu<sub>10</sub>Zr<sub>7</sub>**

$$\begin{aligned} G^\circ(T) - 10.0 & H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 7.0 & H_{\text{Zr}}^{\circ,\text{hcp}-A1}(298.15 \text{ K}) = \\ & -241750.0 + 10.0 & \text{GHSER}_{\text{Cu}} + 7.0 & \text{GHSER}_{\text{Zr}} \end{aligned}$$

**Phase Cu<sub>51</sub>Zr<sub>14</sub>**

$$\begin{aligned} G^\circ(T) - 51.0 & H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 14.0 & H_{\text{Zr}}^{\circ,\text{hcp}-A1}(298.15 \text{ K}) = \\ & -843412.7 + 51.0 & \text{GHSER}_{\text{Cu}} + 14.0 & \text{GHSER}_{\text{Zr}} \end{aligned}$$

**Phase Cu<sub>5</sub>Zr**

$$\begin{aligned} G^\circ(T) - 5.0 & H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - & H_{\text{Zr}}^{\circ,\text{hcp}-A1}(298.15 \text{ K}) = \\ & -61794 + 5.0 & \text{GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Zr}} \end{aligned}$$

**Phase Cu<sub>8</sub>Zr<sub>3</sub>**

$$\begin{aligned} G^\circ(T) - 8.0 & H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 & H_{\text{Zr}}^{\circ,\text{hcp}-A1}(298.15 \text{ K}) = \\ & -148063.1 + 8.0 & \text{GHSER}_{\text{Cu}} + 3.0 & \text{GHSER}_{\text{Zr}} \end{aligned}$$

**Phase CuZr**

$$\begin{aligned} G^\circ(T) - & H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - & H_{\text{Zr}}^{\circ,\text{hcp}-A1}(298.15 \text{ K}) = \\ & -20104.24 - 7.63196 T + \text{GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Zr}} \end{aligned}$$

**Phase CuZr<sub>2</sub>**

$$\begin{aligned} G^\circ(T) - & H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 & H_{\text{Zr}}^{\circ,\text{hcp}-A1}(298.15 \text{ K}) = \\ & -43904.01 + 5.19051 T + \text{GHSER}_{\text{Cu}} + 2.0 & \text{GHSER}_{\text{Zr}} \end{aligned}$$

Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Zr}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ fcc-A1 + Cu <sub>5</sub> Zr	Eutectic	.078	.001	.167	1240.8
Liquid + Cu <sub>51</sub> Zr <sub>14</sub> $\rightleftharpoons$ Cu <sub>5</sub> Zr	Peritectic	.107	.215	.167	1287.5
Cu <sub>51</sub> Zr <sub>14</sub> $\rightleftharpoons$ Liquid	Congruent	.215	.215	....	1386.0
Liquid + Cu <sub>51</sub> Zr <sub>14</sub> $\rightleftharpoons$ Cu <sub>8</sub> Zr <sub>3</sub>	Peritectic	.388	.273	.215	1195.3
Liquid $\rightleftharpoons$ Cu <sub>8</sub> Zr <sub>3</sub> + Cu <sub>10</sub> Zr <sub>7</sub>	Eutectic	.408	.273	.412	1164.2
Cu <sub>10</sub> Zr <sub>7</sub> $\rightleftharpoons$ Liquid	Congruent	.412	.412	....	1164.2
Liquid $\rightleftharpoons$ Cu <sub>10</sub> Zr <sub>7</sub> + CuZr	Eutectic	.425	.412	.500	1163.2
CuZr $\rightleftharpoons$ Cu <sub>10</sub> Zr <sub>7</sub> + CuZr <sub>2</sub>	Eutectoid	.500	.412	.667	976.7
Liquid $\rightleftharpoons$ CuZr + CuZr <sub>2</sub>	Eutectic	.538	.500	.667	1196.7
CuZr $\rightleftharpoons$ Liquid	Congruent	.500	.500	....	1208.5
Liquid $\rightleftharpoons$ CuZr <sub>2</sub> + bcc-A2	Eutectic	.700	.666	.947	1269.5
CuZr <sub>2</sub> $\rightleftharpoons$ Liquid	Congruent	.666	.666	....	1275.0
bcc-A2 $\rightleftharpoons$ CuZr <sub>2</sub> + hcp-A3	Eutectoid	.975	.667	.992	1095.2

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Cu-Zr	(Cu)	Cu	cF4 Fm $\bar{3}m$	M 4	
	(Zr)	Mg	hP2 P6 <sub>3</sub> /mmc	M 2	
	(Zr)	W	cI2 Im $\bar{3}m$	M 4	
	CuZr	ClCs	cP2 Pm $\bar{3}m$	M <sub>1</sub> 1 M <sub>2</sub> 1	bcc-B2
	CuZr <sub>2</sub>	MoSi <sub>2</sub>	tI6 I4/mmm	Cu 2 Zr 4	
	Cu <sub>10</sub> Zr <sub>7</sub>	Ni <sub>10</sub> Zr <sub>7</sub>	oC68 Aba2		
	Cu <sub>9</sub> Zr <sub>2</sub>		tP24 P4/m		o** in [91Vii]
	Cu <sub>5</sub> Zr	AuBe <sub>5</sub>	Cf24 F43m	Cu <sub>1</sub> 4 Cu <sub>2</sub> 16 Zr 4	
	Cu <sub>51</sub> Zr <sub>14</sub>	Ag <sub>51</sub> Gd <sub>14</sub>	hP65 P6/m		hP68 in [91Vii]
	Cu <sub>8</sub> Zr <sub>3</sub>	Cu <sub>8</sub> Hf <sub>3</sub>	oP44 Pnma		

# System Fe-Mg

**Solution Phases:**

Liquid, fcc-*A*1, bcc-*A*2, hcp-*A*3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister

**Assessor and Date:**

J. Tibballs (1991)

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A*2**

$$L_{\text{Fe,Mg};\square}^{0,\text{bcc-}A2} = 65700.0$$

**Phase fcc-*A*1**

$$L_{\text{Fe,Mg};\square}^{0,\text{fcc-}A1} = 65200.0$$

**Phase hcp-*A*3**

$$L_{\text{Fe,Mg};\square}^{0,\text{hcp-}A3} = 92400.0$$

**Phase liquid**

$$L_{\text{Fe,Mg}}^{0,\text{liquid}} = 61343.0 + 1.5 \cdot T$$

$$L_{\text{Fe,Mg}}^{1,\text{liquid}} = -2700.0$$

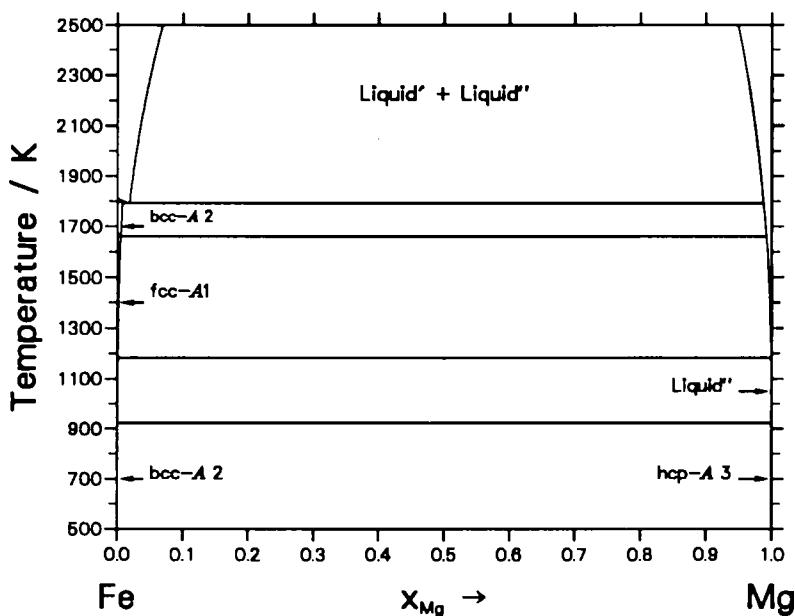


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{Mg}$	$T / K$
$\text{Liquid}' \rightleftharpoons \text{bcc}-\text{A}2 + \text{Liquid}''$	Monotectic	.018 .008 .987	1791.4
$\text{Liquid}'' + \text{bcc}-\text{A}2 \rightleftharpoons \text{fcc}-\text{A}1$	Degenerate	.992 .005 .005	1661.6
$\text{Liquid}'' + \text{bcc}-\text{A}2 \rightleftharpoons \text{fcc}-\text{A}1$	Degenerate	.999 .001 .001	1183.4
$\text{Liquid}'' + \text{bcc}-\text{A}2 \rightleftharpoons \text{hcp}-\text{A}3$	Degenerate	1.000 .000 1.000	922.9

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol]
Fe-Mg	(Fe)	Cu	$cF4$ $Pm\bar{3}m$
	(Fe)	W	$cI2$ $I\bar{m}\bar{3}m$
	(Mg)	Mg	$hP2$ $P6_3/mmc$

## System Fe-Mn

**Solution Phases:**

(stable) Liquid, bcc-*A*2, cbcc-*A*12, cub-*A*13, fcc-*A*1

**Solution Phases:**

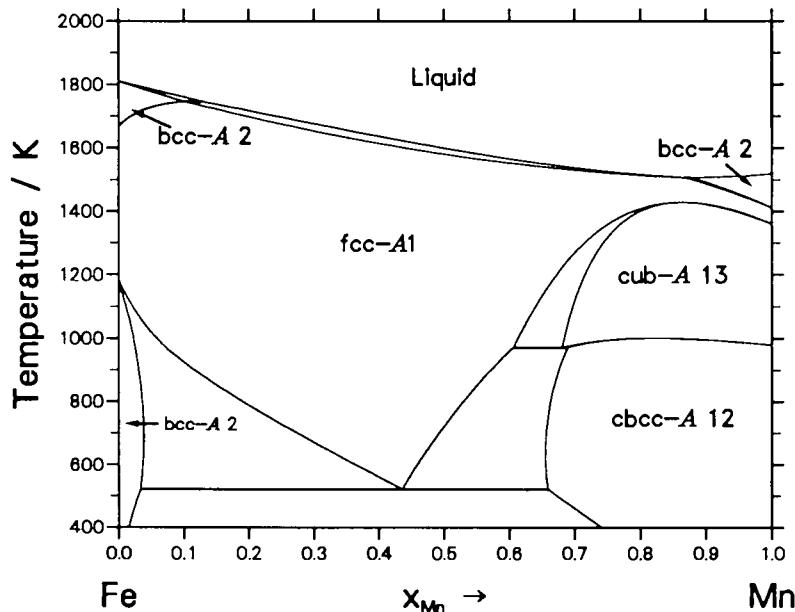
(metastable) hcp-*A*3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 12	:	Substitutional, Redlich-Kister
cub- <i>A</i> 13	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister

**Assessor and Date:**

Scientific Group Thermodata Europe Database



Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**Phase bcc-A2**

$$L_{\text{Fe,Mn}:□}^{0,\text{bcc}-A2} = - 2759 + 1.237 \text{ T}$$

$$T_{\text{c,Fe,Mn}:□}^{0,\text{bcc}-A2} = 123$$

$$\beta_{\text{Fe,Mn}:□}^{0,\text{mag,bcc}-A2} = 0$$

**Phase cbcc-A12**

$$L_{\text{Fe,Mn}:□}^{0,\text{cbcc}-A12} = - 10184$$

**Phase cub-A13**

$$L_{\text{Fe,Mn}:□}^{0,\text{cub}-A13} = - 11518 + 2.819 \text{ T}$$

**Phase fcc-A1**

$$L_{\text{Fe,Mn}:□}^{0,\text{fcc}-A1} = - 7762 + 3.865 \text{ T}$$

$$L_{\text{Fe,Mn}:□}^{1,\text{fcc}-A1} = - 259$$

$$T_{\text{c,Fe,Mn}:□}^{0,\text{fcc}-A1} = - 2282$$

$$T_{\text{c,Fe,Mn}:□}^{1,\text{fcc}-A1} = - 2068$$

$$\beta_{\text{Fe,Mn}:□}^{0,\text{mag,fcc}-A1} = 0$$

**Phase liquid**

$$L_{\text{Fe,Mn}}^{0,\text{liquid}} = - 3950 + 0.489 \text{ T}$$

$$L_{\text{Fe,Mn}}^{1,\text{liquid}} = 1145$$

**Phase hcp-A3**

$$L_{\text{Fe,Mn}}^{0,\text{hcp}-A3} = - 5582 + 3.865 \text{ T}$$

$$L_{\text{Fe,Mn}}^{1,\text{hcp}-A3} = 273$$

**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Mn}}$			$T / \text{K}$
$\text{cub}-A13 \rightleftharpoons \text{fcc}-A1 + \text{cbcc}-A12$	Eutectoid	.681	.606	.690	973.2
$\text{fcc}-A1 \rightleftharpoons \text{bcc}-A2 + \text{cbcc}-A12$	Eutectoid	.436	.033	.659	521.3
$\text{Liquid} + \text{bcc}-A2 \rightleftharpoons \text{fcc}-A1$	Peritectic	.100	.129	.129	1746.8
$\text{Liquid} + \text{bcc}-A2 \rightleftharpoons \text{fcc}-A1$	Peritectic	.867	.877	.875	1507.2

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Fe-Mn	(Fe)	Cu	$cF4$ $Pm\bar{3}m$	
	(Fe)	W	$cI2$ $Im\bar{3}m$	
	$\alpha$ -Mn	$\alpha$ -Mn	$c58$ $I\bar{4}3m$	cbcc-A12
	$\beta$ -Mn	$\beta$ -Mn	$cP20$ $P4_132$	cub-A13
	$\gamma$ -Mn	Cu	$cF4$ $Fm\bar{3}m$	
	$\delta$ -Mn	W	$cI2$ $Im\bar{3}m$	

# System Fe–Si

**Solution Phases:**

Liquid, bcc-*A*2, bcc-*B*2, fcc-*A*1

**Compounds:**

Fe<sub>5</sub>Si<sub>3</sub>, FeSi, Fe<sub>2</sub>Si, FeSi<sub>2</sub>-L, FeSi<sub>2</sub>-H

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
bcc- <i>B</i> 2	:	Sublattice model , (Fe,Si) <sub>0.5</sub> (Fe,Si) <sub>0.5</sub> (□) <sub>3</sub> Two descriptions of the bcc- <i>A</i> 2:bcc- <i>B</i> 2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.
bcc- <i>A</i> 2	:	see bcc- <i>B</i> 2
Fe <sub>2</sub> Si	:	Stoichiometric, (Fe) <sub>2</sub> (Si)
Fe <sub>5</sub> Si <sub>3</sub>	:	Stoichiometric, (Fe) <sub>5</sub> (Si) <sub>3</sub>
FeSi <sub>2</sub> -L	:	Stoichiometric, (Fe)(Si) <sub>2</sub>
FeSi <sub>2</sub> -II	:	Stoichiometric, (Fe) <sub>3</sub> (Si) <sub>7</sub>
FeSi	:	Stoichiometric, (Fe)(Si)

**Assessor and Date:**

J. Lacaze, and B. Sundman

**Publication:**

Met. Trans., **22A**, (10), 2211-2223 (1991).

## Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)

### Phase Fe<sub>2</sub>Si

$$G^\circ(T) - 2.0 \ H_{\text{Fe}}^{\circ,\text{bcc-}A2,\text{para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 71256.6 - 10.62 \ T + 2.0 \ \text{GHSER}_{\text{Fe}} + \text{GIISER}_{\text{Si}}$$

### Phase $\text{Fe}_5\text{Si}_3$

$$G^\circ(T) - 5.0 H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 241144 + 2.16 T + 5.0 \text{ GHSER}_{\text{Fe}} + 3.0 \text{ GHSER}_{\text{Si}}$$

### Phase $\text{FeSi}_2\text{-L}$

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) - 2.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 82149.0 + 10.44 T + \text{GHSER}_{\text{Fe}} + 2.0 \text{ GHSER}_{\text{Si}}$$

### Phase $\text{FeSi}_2\text{-H}$

$$G^\circ(T) - 3.0 H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) - 7.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 196490 - 9.2 T + 3.0 \text{ GHSER}_{\text{Fe}} + 7.0 \text{ GHSER}_{\text{Si}}$$

### Phase $\text{FeSi}$

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 72761.2 + 4.44 T + \text{GHSER}_{\text{Fe}} + \text{GHSER}_{\text{Si}}$$

### Phase liquid

$$L_{\text{Fe},\text{Si}}^{0,\text{liquid}} = - 164434.6 + 41.9773 T$$

$$L_{\text{Fe},\text{Si}}^{1,\text{liquid}} = - 21.523 T$$

$$L_{\text{Fe},\text{Si}}^{2,\text{liquid}} = - 18821.542 + 22.07 T$$

$$L_{\text{Fe},\text{Si}}^{3,\text{liquid}} = 9695.8$$

### Phase fcc-A1

$$L_{\text{Fe},\text{Si}:□}^{0,\text{fcc-A}1} = - 125247.7 + 41.166 T$$

$$L_{\text{Fe},\text{Si}:□}^{1,\text{fcc-A}1} = - 142707.6$$

$$L_{\text{Fe},\text{Si}:□}^{2,\text{fcc-A}1} = 89907.3$$

### Phase bcc-B2

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) = G(\text{Fe:Fe:}□) = \text{GHSER}_{\text{Fe}}$$

$$T_{\text{c},\text{Fe:Fe}□}^{\text{bcc-B}2} = 1043 \quad \beta_{\text{c},\text{Fe:Fe}□}^{\text{bcc-B}2} = 2.22$$

$$G^\circ(T) - 0.5 H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) - 0.5 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Fe:Si:}□) = \\ - 48761.565 + 11.62 T + 0.5 \text{ GHSER}_{\text{Fe}} + 0.5 \text{ GBCC}_{\text{Si}}$$

$$T_{\text{c},\text{Fe:Si}□}^{0,\text{bcc-B}2} = 521.5 \quad \beta_{\text{c},\text{Si:Fe}□}^{0,\text{bcc-B}2} = 1.11$$

$$G^\circ(T) - 0.5 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 0.5 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Fe:}\square) = \\ - 48761.565 + 11.62 T + 0.5 \text{ GHSER}_{\text{Fe}} + 0.5 \text{ GBCC}_{\text{Si}}$$

$$T_{c,\text{Si:Fe}\square}^{0,\text{bcc}-B2} = 521.5 \quad \beta_{c,\text{Si:Fe}\square}^{0,\text{bcc}-B2} = 1.11$$

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si:}\square) = \text{GBCC}_{\text{Si}}$$

$$L_{\text{Fe},\text{Si:Fe}\square}^{0,\text{bcc}-B2} = L_{\text{Fe:Fe},\text{Si}\square}^{0,\text{bcc}-B2} = - 50771 + 11.62 T$$

$$L_{\text{Fe},\text{Si:Fe}\square}^{1,\text{bcc}-B2} = L_{\text{Fe:Fe},\text{Si}\square}^{1,\text{bcc}-B2} = 4016$$

$$L_{\text{Fe},\text{Si:Fe}\square}^{2,\text{bcc}-B2} = L_{\text{Fe:Fe},\text{Si}\square}^{2,\text{bcc}-B2} = 3890$$

$$L_{\text{Fe},\text{Si:Si}\square}^{0,\text{bcc}-B2} = L_{\text{Si:Fe},\text{Si}\square}^{0,\text{bcc}-B2} = 18493 + 11.62 T$$

$$L_{\text{Fe},\text{Si:Si}\square}^{1,\text{bcc}-B2} = L_{\text{Si:Fe},\text{Si}\square}^{1,\text{bcc}-B2} = - 27104$$

$$L_{\text{Fe},\text{Si:Si}\square}^{2,\text{bcc}-B2} = L_{\text{Si:Fe},\text{Si}\square}^{2,\text{bcc}-B2} = 3890$$

$$L_{\text{Fe},\text{Si:Fe},\text{Si}\square}^{0,\text{bcc}-B2} = - 93360$$

$$T_{c,\text{Fe},\text{Si:Fe}\square}^{0,\text{bcc}-B2} = T_{c,\text{Fe:Fe},\text{Si}\square}^{0,\text{bcc}-B2} = 189$$

$$T_{c,\text{Fe},\text{Si:Fe}\square}^{1,\text{bcc}-B2} = T_{c,\text{Fe:Fe},\text{Si}\square}^{1,\text{bcc}-B2} = 63$$

$$T_{c,\text{Fe},\text{Si:Si}\square}^{0,\text{bcc}-B2} = T_{c,\text{Si:Fe},\text{Si}\square}^{0,\text{bcc}-B2} = - 189$$

$$T_{c,\text{Fe},\text{Si:Si}\square}^{1,\text{bcc}-B2} = T_{c,\text{Si:Fe},\text{Si}\square}^{1,\text{bcc}-B2} = 63$$

$$G_{\text{Fe:Si}\square}^* = - 1260 R \quad (R = 8.31451)$$

$$L_{\text{Fe},\text{Si}}^0 = - 27809 + 11.62 T$$

$$L_{\text{Fe},\text{Si}}^1 = - 11544$$

$$L_{\text{Fe},\text{Si}}^2 = 3890$$

### Phase bcc-B2

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) = G(\text{Fe:Fe:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 0.5 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Fe:Si:}\square) = 2.0 G_{\text{Fe:Si}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) - 0.5 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Fe:}\square) = 2.0 G_{\text{Fe:Si}\square}^*$$

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si:}\square) = 0.0$$

### Phase bcc-A2

$$L_{\text{Fe},\text{Si}\square}^{0,\text{bcc}-A2} = 4.0 L_{\text{Fe},\text{Si}}^0$$

$$L_{\text{Fe},\text{Si}\square}^{1,\text{bcc}-A2} = 8.0 L_{\text{Fe},\text{Si}}^1$$

$$T_{c,\text{Fe},\text{Si}\square}^{1,\text{bcc}-A2} = 63$$

$$L_{\text{Fe},\text{Si}\square}^{2,\text{bcc}-A2} = 16.0 L_{\text{Fe},\text{Si}}^2$$

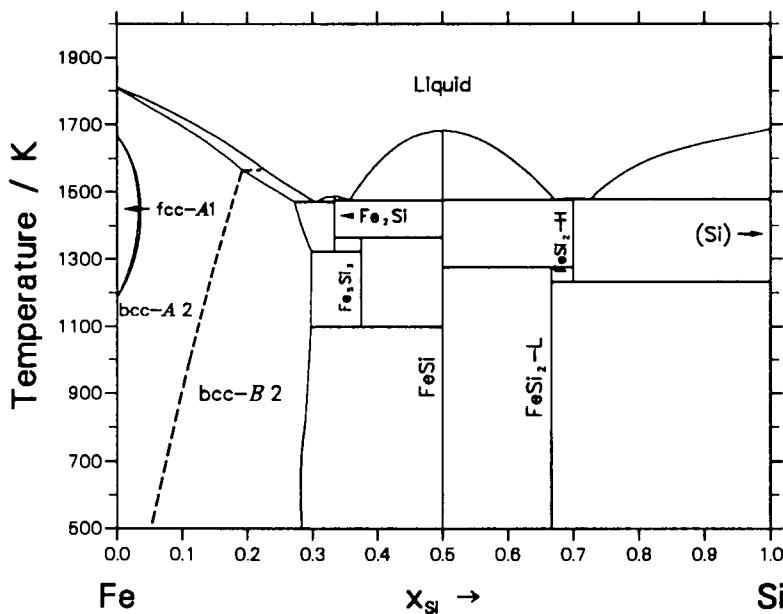


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Si}}$	Temp. / K
Liquid $\rightleftharpoons$ bcc-B2 + Fe <sub>2</sub> Si	Eutectic	.273 .267 .333	1470.6
Fe <sub>2</sub> Si $\rightleftharpoons$ bcc-B2 + Fe <sub>5</sub> Si <sub>3</sub>	Eutectoid	.333 .299 .375	1322.8
Fe <sub>5</sub> Si <sub>3</sub> $\rightleftharpoons$ bcc-B2 + FeSi	Eutectoid	.375 .298 .500	1097.8
Fe <sub>2</sub> Si + FeSi $\rightleftharpoons$ Fe <sub>5</sub> Si <sub>3</sub>	Peritectoid	.333 .500 .375	1364.4
Liquid $\rightleftharpoons$ Fe <sub>2</sub> Si + FeSi	Eutectic	.357 .333 .500	1475.8
Liquid $\rightleftharpoons$ FeSi + FeSi <sub>2</sub> -H	Eutectic	.672 .500 .700	1477.2
FeSi + FeSi <sub>2</sub> -H $\rightleftharpoons$ FeSi <sub>2</sub> -L	Peritectoid	.500 .700 .666	1275.7
FeSi <sub>2</sub> -H $\rightleftharpoons$ FeSi <sub>2</sub> -L + (Si)	Eutectoid	.700 .667 1.000	1232.9
Liquid $\rightleftharpoons$ FeSi <sub>2</sub> -H + (Si)	Eutectic	.725 .700 1.000	1478.3
Fe <sub>2</sub> Si $\rightleftharpoons$ Liquid	Congruent	.333 .333 ....	1488.0
FeSi $\rightleftharpoons$ Liquid	Congruent	.500 .500 ....	1683.0
FeSi <sub>2</sub> -H $\rightleftharpoons$ Liquid	Congruent	.700 .700 ....	1482.0

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Symbol Group	Sub- lattices	Comments
Fe–Si	(Fe)	Cu	<i>cF</i> 4 <i>Pm</i> 3 <i>m</i>		
	(Fe)	W	<i>cI</i> 2 <i>Im</i> 3 <i>m</i>		
	(Si)	diamond	<i>cF</i> 8 <i>Fd</i> 3 <i>m</i>		
	FeSi <sub>2</sub> -L		<i>tP</i> 3 <i>P</i> 4/ <i>mmm</i>	Fe Si	1 2
	FeSi <sub>2</sub> -H		<i>oC</i> 48 <i>Cmca</i>	Fe <sub>1</sub> Fe <sub>2</sub> Si <sub>1</sub> Si <sub>2</sub>	8 8 8 16
	Fe <sub>2</sub> Si		<i>hP</i> 6 <i>P</i> 3 <i>m</i> 1	Fe <sub>1</sub> Fe <sub>2</sub> Fe <sub>3</sub> Si	1 1 2 2
	FeSi		<i>cP</i> 8 <i>P</i> 2 <sub>1</sub> 3	Fe Si	4 4
	Fe <sub>5</sub> Si <sub>3</sub>		<i>hP</i> 16 <i>P</i> 6 <sub>3</sub> / <i>mmc</i>	Fe <sub>1</sub> Fe <sub>2</sub> Si	4 6 6
	bcc-B2	CsCl	<i>cP</i> 2 <i>Fm</i> 3 <i>m</i>		α2 in [90Mas]

# System Fe-Ti

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1, hcp-*A*3

**Compounds:**

FeTi, Laves-*C*14

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Laves- <i>C</i> 14	:	Sublattice model, (Fe,Ti) <sub>2</sub> (Fe,Ti)
FeTi	:	Sublattice model, (Fe,Ti)(Fe,Ti)

**Assessor and Date:**

M.II. Rand 1995

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase FeTi**

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ - 51584.05 + 238.686 T - 44.858 T \cdot \ln T - 0.008493 T^2 + 100500 T^{-1}$$

**Phase Laves-*C*14**

$$G^\circ(T) - 3.0 H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}3,\text{para}}(298.15 \text{ K}) = G(\text{Fe:Fe}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Fe}}$$

$$G^\circ(T) - 2.0 H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}3,\text{para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Fe:Ti}) = \\ - 1440.0 - 6.75 T + 2.0 \text{ GHSER}_{\text{Fe}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Fe}}^{\circ,\text{bcc}-\text{A}3,\text{para}}(298.15 \text{ K}) - 2.0 H_{\text{Ti}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Ti:Fe}) = \\ 15000.0 + \text{GHSER}_{\text{Fe}} + 2.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = \\ 15000 + 3.0 \text{ GHSER}_{\text{Ti}}$$

$$L_{\text{Fe:Fe,Ti}}^{0,\text{Laves}-\text{C}14} = L_{\text{Ti:Fe,Ti}}^{0,\text{Laves}-\text{C}14} = 60000$$

$$L_{\text{Fe,Ti:Fe}}^{0,\text{Laves}-\text{C}14} = L_{\text{Fe,Ti:Ti}}^{0,\text{Laves}-\text{C}14} = 60000$$

**Phase liquid**

$$L_{\text{Fe,Ti}}^{0,\text{liquid}} = -62273.8 + 5.6939 \ T$$

$$L_{\text{Fe,Ti}}^{1,\text{liquid}} = -5491.468$$

**Phase fcc-*A*1**

$$L_{\text{Fe,Ti:}\square}^{0,\text{fcc-}A1} = -42000$$

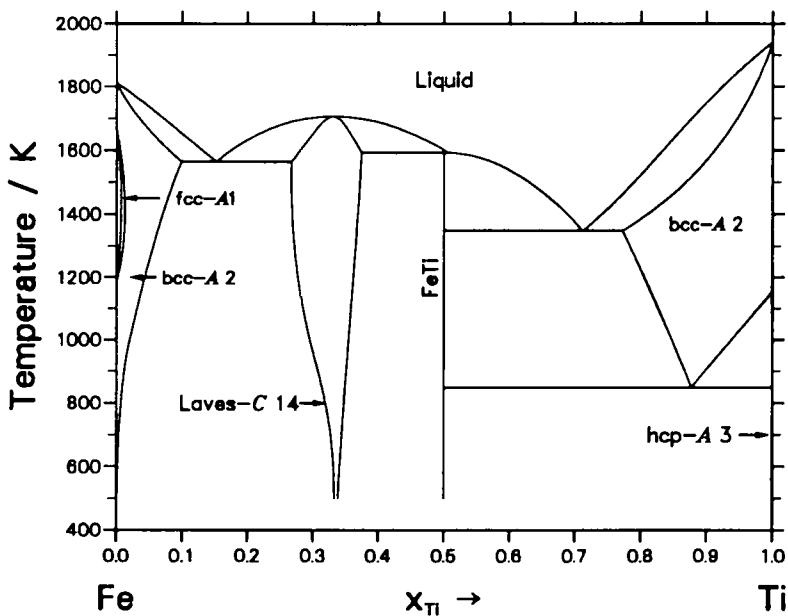
**Phase hcp-*A*3**

$$L_{\text{Fe,Ti:}\square}^{0,\text{hcp-}A3} = 18500 - 15 \ T$$

**Phase bcc-*A*2**

$$L_{\text{Fe,Ti:}\square}^{0,\text{bcc-}A2} = -52400.65 + 10.7268 \ T$$

$$L_{\text{Fe,Ti:}\square}^{1,\text{bcc-}A2} = -7442 + 0.41968 \ T$$



**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Ti}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ FeTi* + bcc-A2	Eutectic	.712	.500	.772	1349.3
bcc-A2 $\rightleftharpoons$ FeTi* + hcp-A3	Eutectoid	.877	.500	.999	849.4
Liquid + Laves-C14 $\rightleftharpoons$ FeTi*	Peritectic	.506	.334	.500	1593.4
Laves-C14 $\rightleftharpoons$ bcc-A2	Congruent	.333	.333	....	1707.0
Liquid $\rightleftharpoons$ bcc-A2 + Laves-C14	Eutectic	.152	.099	0.267	1564.4

\*  $\text{FeTi} \equiv \text{bcc-}B2$ **Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Fe-Ti	(Fe)	Cu	$cF\bar{4}$ $Pm\bar{3}m$	
	(Fe)	W	$c\bar{I}2$ $Im\bar{3}m$	
	(Ti)	Mg	$hP\bar{2}$ $P\bar{6}_3/mmc$	
	(Ti)	W	$c\bar{I}2$ $Im\bar{3}m$	
	FeTi	CsCl	$cP\bar{2}$ $Pm\bar{3}m$	bcc- $B2$
	$\beta$ Fe <sub>2</sub> Ti	MgZn <sub>2</sub>	$hPI\bar{2}$ $P\bar{6}_3/mmc$	Laves-C14

# System Hf–Ti

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, hcp- <i>A</i> 3
(metastable)	fcc- <i>A</i> 1

**Modelling:**

Liquid	:	Substitutional, Redlich–Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich–Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich–Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich–Kister

**Assessor and Date:**

H. Bitterman, Univ. Wien, Austria, 1997

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase liquid**

$$L_{\text{Hf,Ti}}^{0,\text{liquid}} = -4993.5 - 7.10316 \cdot T$$

**Phase fcc-*A*1**

$$L_{\text{Hf,Ti:\square}}^{0,\text{fcc-}A1} = 1.0\text{E-}4$$

**Phase hcp-*A*3**

$$L_{\text{Hf,Ti:\square}}^{0,\text{hcp-}A3} = 13644 - 10.6383 \cdot T$$

**Phase bcc-*A*2**

$$L_{\text{Hf,Ti:\square}}^{0,\text{bcc-}A2} = 3003.24 - 7.4114 \cdot T$$

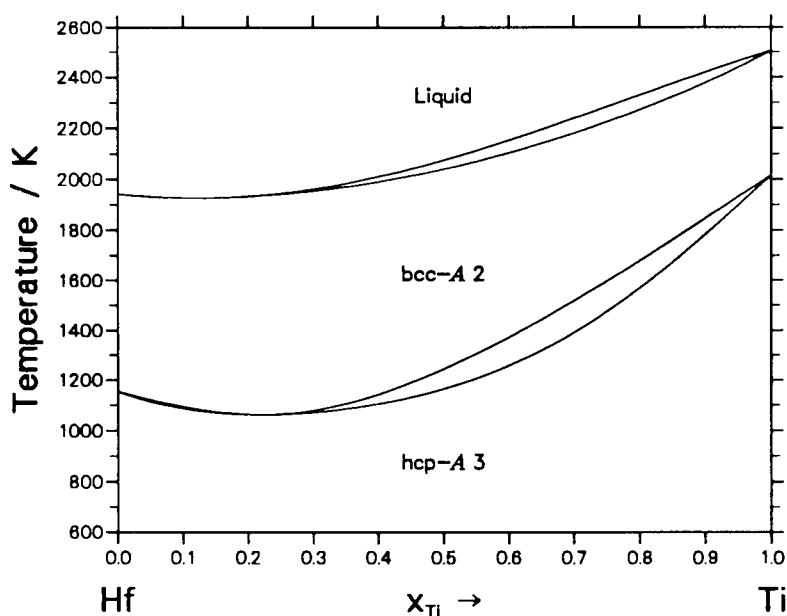


Table I – Invariant Reactions.

Reaction	Type	Compositions \$x_{\text{Ti}}	\$T / \text{K}
$\text{hcp-A3} \rightleftharpoons \text{bcc-A2}$	Congruent	.224 .224 ....	1063.3
$\text{bcc-A2} \rightleftharpoons \text{Liquid}$	Congruent	.120 .120 ....	1296.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Hf-Ti	(Hf)	Mg	$hP2$ $P6_3/mmc$	
	(Hf)	W	$cI2$ $Im\bar{3}m$	
	(Ti)	Mg	$hP2$ $P6_3/mmc$	
	(Ti)	W	$cI2$ $Im\bar{3}m$	

# System Li-Mg

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, hcp- <i>A</i> 3
(metastable)	fcc- <i>A</i> 1

**Compounds:**

(metastable)	Al <sub>12</sub> Mg <sub>17</sub> , AlLi
--------------	--

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Al <sub>12</sub> Mg <sub>17</sub>	:	Sublattice model, (Li,Mg) <sub>24</sub> (Li,Mg) <sub>10</sub> (Mg) <sub>24</sub>
AlLi	:	Sublattice model,(Li,Mg)(Li,Mg, $\square$ )

**Assessor and Date:**

N. Saunders, 1991

**Comments:**

The models describing the metastable phases are compatible with the ones used in the Al-Mg system (Version I).

Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)

**Phase bcc-*A*2**

$$L_{\text{Li}, \text{Mg}; \square}^{0, \text{bcc}-\text{A}2} = -18335 + 8.49 \cdot T$$

$$L_{\text{Li}, \text{Mg}; \square}^{1, \text{bcc}-\text{A}2} = 3481$$

$$L_{\text{Li}, \text{Mg}; \square}^{2, \text{bcc}-\text{A}2} = 2658 - 0.114 \cdot T$$

**Phase fcc-A1**

$$L_{\text{Li,Mg};\square}^{0,\text{fcc}-A1} = -6856.0$$

**Phase hcp-A3**

$$L_{\text{Li,Mg};\square}^{0,\text{hcp}-A3} = -6856.0$$

$$L_{\text{Li,Mg};\square}^{1,\text{hcp}-A3} = 4000.0$$

$$L_{\text{Li,Mg};\square}^{2,\text{hcp}-A3} = 4000.0$$

**Phase liquid**

$$L_{\text{Li,Mg}}^{0,\text{liquid}} = -14935 + 10.371 T$$

$$L_{\text{Li,Mg}}^{1,\text{liquid}} = -1789 + 1.143 T$$

$$L_{\text{Li,Mg}}^{2,\text{liquid}} = 6533 - 6.6915 T$$

**Phase Al<sub>12</sub>Mg<sub>17</sub>**

$$G^\circ(T) - 34.0 H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 24.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Li:Li:Mg}) = \\ 290000 + 34.0 \text{ GHSER}_{\text{Li}} + 24.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 10.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 48.0 H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Li:Li:Mg}) = \\ 290000 + 10.0 \text{ GHSER}_{\text{Li}} + 48.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 24.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 34.0 H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Li:Li:Mg}) = \\ 290000 + 24.0 \text{ GHSER}_{\text{Li}} + 34.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 58.0 H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mg:Mg:Mg}) = 0.0$$

**Phase AlLi**

$$G^\circ(T) - 2.0 H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Li:Li}) = \\ 2.0 \text{ GHSER}_{\text{Li}}$$

$$G^\circ(T) - H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Li:Mg}) = \\ -9168 + 4.2 T + \text{GHSER}_{\text{Li}} + \text{GBCC}_{\text{Mg}}$$

$$G^\circ(T) - H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Li}) = \\ -9168 + 4.2 T + \text{GHSER}_{\text{Li}} + \text{GBCC}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 0.0$$

$$G^\circ(T) - H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Li:}\square) = \\ 50000 + \text{GHSER}_{\text{Li}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:}\square) = 0.0$$

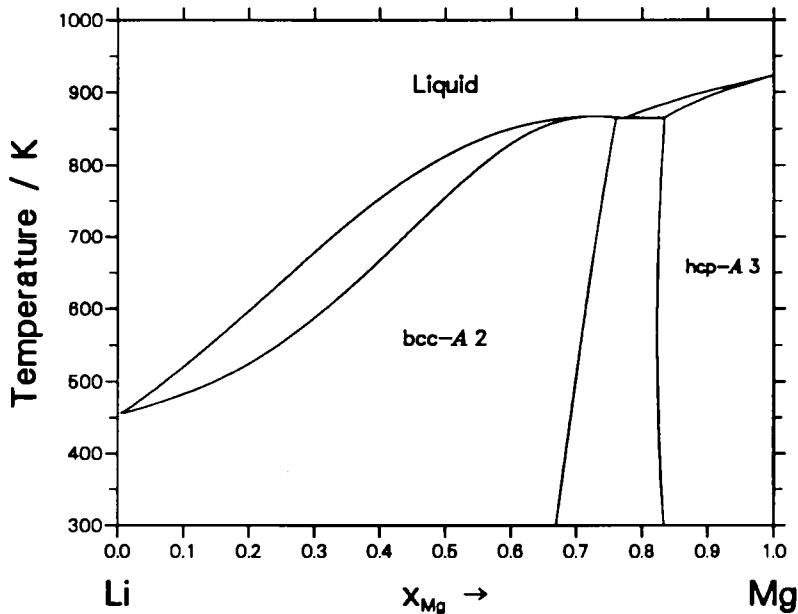


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Mg}}$	$T / \text{K}$
Liquid $\rightleftharpoons$ bcc-A2 + hcp-A3	Eutectic	.774 .760 .834	865.2
Liquid $\rightleftharpoons$ bcc-A2	Congruent	.727 .727 ....	867.4

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol Group
Li-Mg	(Li)	W	$c\bar{I}2$ $I\bar{m}\bar{3}m$
	(Mg)	Mg	$hP2$ $P\bar{6}_3/mmc$

# System Li-Zr

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, hcp- <i>A</i> 3
(metastable)	fcc- <i>A</i> 1

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister

**Assessor and Date:**

N. Saunders, 1991

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A*2**

$$L_{\text{Li,Zr};\square}^{0,\text{bcc-}A2} = 100000$$

**Phase fcc-*A*1**

$$L_{\text{Li,Zr};\square}^{0,\text{fcc-}A1} = 100000$$

**Phase hcp-*A*3**

$$L_{\text{Li,Zr};\square}^{0,\text{hcp-}A3} = 100000$$

**Phase liquid**

$$L_{\text{Li,Zr}}^{0,\text{liquid}} = 100000$$

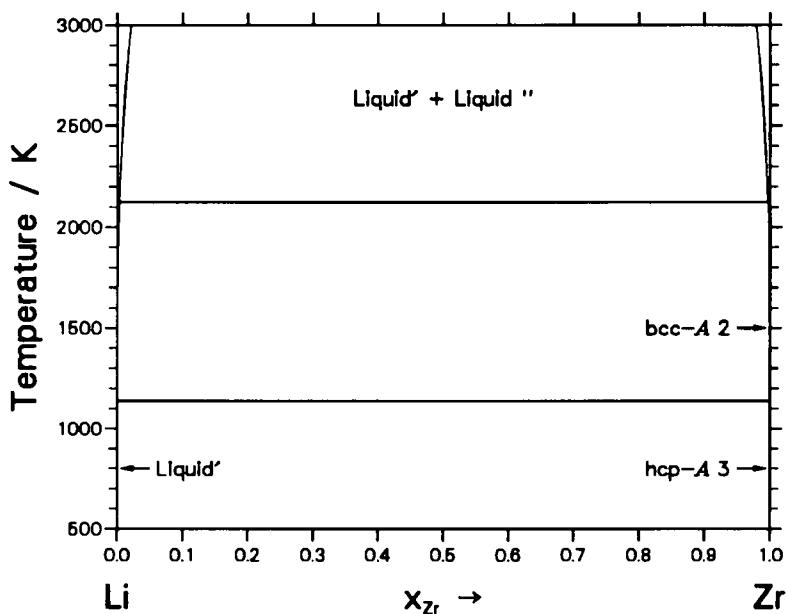


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{Zr}$	$T / K$
$hcp-A3 \rightleftharpoons bcc-A2$	Allotropic	1.000    1.000    ....	1139.45
$Liquid'' \rightleftharpoons Liquid' + bcc-A2$	Monotectic	.996    .003    .998	2124.9
$Liquid' \rightleftharpoons bcc-A2 + hcp-A3$	Degenerate	.000    .000    1.000	453.6

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Li-Zr	(Li)	W	$c\bar{I}2$ $I\bar{m}\bar{3}m$
	(Zr)	Mg	$hP2$ $P6_3/mmc$
	(Zr)	W	$c\bar{I}2$ $I\bar{m}\bar{3}m$

## System Mg-Mn

Solution Phases:

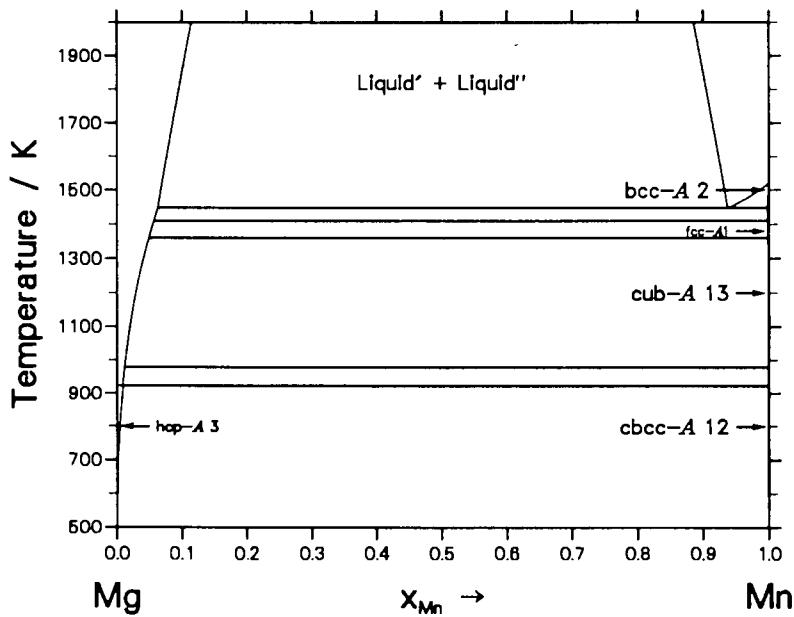
Liquid, bcc-*A*2, hcp-*A*3, cbcc-*A*12, cub-*A*13, fcc-*A*1

Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 12	:	Substitutional, Redlich-Kister
cub- <i>A</i> 13	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister

Assessor and Date:

J. Tibballs 1991



**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)****Phase bcc-*A*2**

$$L_{\text{Mg,Mn:}\square}^{0,\text{bcc-}A2} = 70000.0$$

**Phase cbcc-*A*12**

$$L_{\text{Mg,Mn:Vn}}^{0,\text{cbcc-}A12} = 70000.0$$

**Phase cub-*A*13**

$$L_{\text{Mg,Mn:Vn}}^{0,\text{cub-}A13} = 70000.0$$

**Phase fcc-*A*1**

$$L_{\text{Mg,Mn}}^{0,\text{fcc-}A1} = 70000.0$$

**Phase hcp-*A*3**

$$L_{\text{Mg,Mn:Vn}}^{0,\text{hcp-}A3} = 32985.0 + 2.5 \ T$$

**Phase liquid**

$$L_{\text{Mg,Mn}}^{0,\text{liquid}} = 19125.0 + 12.5 \ T$$

Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Mn}}$			$T / \text{K}$
Liquid' + cbcc-A12 $\rightleftharpoons$ hcp-A3	Peritectic	.008	1.000	.009	923.8
cub-A13 $\rightleftharpoons$ Liquid' + cbcc-A12	Metatactic	.999	.012	1.000	980.5
fcc-A1 $\rightleftharpoons$ Liquid' + cub-A13	Metatactic	.999	.048	1.000	1351.7
bcc-A2 $\rightleftharpoons$ Liquid' + fcc-A1	Metatactic	.998	.057	.999	1409.6
Liquid" $\rightleftharpoons$ Liquid' + bcc-A2	Monotectic	.937	.063	.998	1447.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Mg-Mn	(Mg)	Mg	$hP2$ $P6_3/mmc$	
	$\alpha$ -Mn	$\alpha$ -Mn	$c58$ $I\bar{4}3m$	cbcc-A12
	$\beta$ -Mn	$\beta$ -Mn	$cP20$ $P4_1323m$	cub-A13
	$\gamma$ -Mn	Cu	$cF4$ $Fm\bar{3}m$	
	$\delta$ -Mn	W	$cI2$ $I\bar{m}\bar{3}m$	

## System Mg–Ni

**Solution Phases:**

Liquid, fcc-*A1*

**Compounds:**

Mg<sub>2</sub>Ni, Laves-*C36*

**Modelling:**

Liquid	:	Substitutional, Redlich–Kister
fcc- <i>A1</i>	:	Substitutional, Redlich–Kister
Mg <sub>2</sub> Ni	:	Stoichiometric, (Mg) <sub>2</sub> (Ni)
Laves- <i>C36</i>	:	Sublattice model, (Mg,Ni) <sub>2</sub> (Mg,Ni)

**Comments:**

M. Jacobs assumed the Laves-*C36* phase to be stoichiometric. The thermodynamic description of that phase was modified and is now consistent with the one in the database.

**Assessor and Date:**

M. Jacobs September 1991 (Laves-*C36* modified by I. Ansara December 1997).

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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A2***

$$L_{\text{Mg},\text{Ni}: \square}^{0,\text{bcc}-\text{A}2} = 80 \text{ } T$$

**Phase fcc-*A1***

$$L_{\text{Mg},\text{Ni}: \square}^{0,\text{fcc}-\text{A}1} = 80 \text{ } T$$

**Phase hcp-*A3***

$$L_{\text{Mg},\text{Ni}: \square}^{0,\text{hcp}-\text{A}3} = 80 \text{ } T$$

**Phase liquid**

$$L_{\text{Mg},\text{Ni}}^{0,\text{liquid}} = -42304.49 + 7.45704 T$$

$$L_{\text{Mg},\text{Ni}}^{1,\text{liquid}} = -15611.66 + 9.11885 T$$

**Phase Laves-C36**

$$\begin{aligned} G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = \\ 15000.0 + \text{GHSER}_{\text{Mg}} \\ G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 2.0 H_{\text{Ni}}^{\circ,\text{fcc}-A1,\text{para}}(298.15 \text{ K}) = \\ -74136.0 + 293.9216 T - 54.35385 T \cdot \ln T - 0.03329235 T^2 \\ + 5.14203E-06 T^3 - 99.0 T^{-1} \\ G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - H_{\text{Ni}}^{\circ,\text{fcc}-A1,\text{para}}(298.15 \text{ K}) = \\ 104136.0 - 293.9216 T + 54.35385 T \cdot \ln T + 0.03329235 T^2 \\ - 5.14203E-06 T^3 + 99.0 T^{-1} \\ G^\circ(T) - 3.0 H_{\text{Ni}}^{\circ,\text{fcc}-A1,\text{para}}(298.15 \text{ K}) = G(\text{Ni:Ni}) = \\ 15000.0 + \text{GHSER}_{\text{Ni}} \\ L_{\text{Mg},\text{Ni};\text{Mg}}^{0,\text{Laves}-C36} = L_{\text{Mg},\text{Ni};\text{Ni}}^{0,\text{Laves}-C36} = 50000 \\ L_{\text{Mg};\text{Mg},\text{Ni}}^{0,\text{Laves}-C36} = L_{\text{Ni};\text{Mg},\text{Ni}}^{0,\text{Laves}-C36} = 50000 \end{aligned}$$

**Phase Mg<sub>2</sub>Ni**

$$\begin{aligned} G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - H_{\text{Ni}}^{\circ,\text{fcc}-A1,\text{para}}(298.15 \text{ K}) = \\ -82211.0 + 571.0183 T - 95.992 T \cdot \ln T \end{aligned}$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Ni}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ Laves-C36 + fcc-A1	Eutectic	.802	.666	1.000	1366.6
Liquid $\rightleftharpoons$ MgNi <sub>2</sub>	Congruent	.666	.666	....	1420.0
Liquid + Mg <sub>2</sub> Ni $\rightleftharpoons$ Laves-C36	Peritectic	.278	.666	.333	1032.2
Liquid $\rightleftharpoons$ + hcp-A3 Mg <sub>2</sub> Ni	Eutectic	.101	.000	.333	780.0

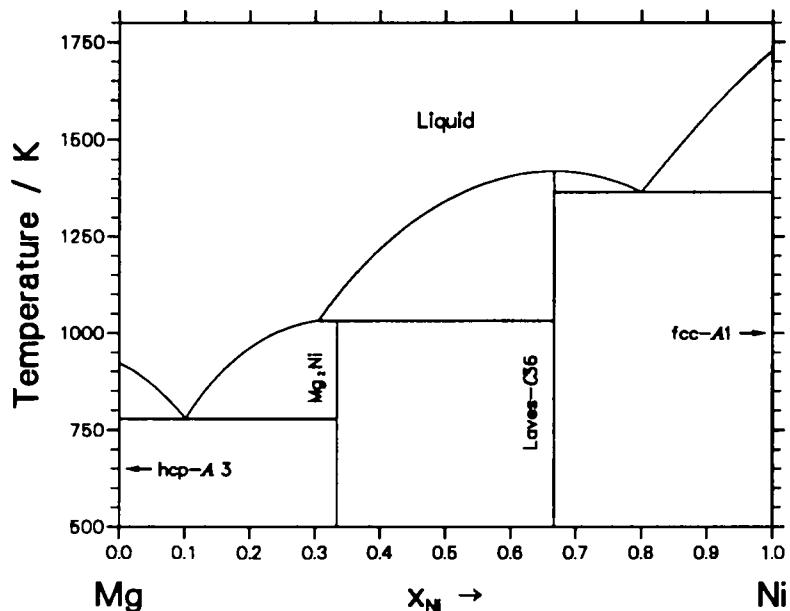


Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Mg-Ni	(Mg)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	(Ni)	Cu	<i>cF4</i> <i>Fm<bar>3</bar></i> m	M 4	
	MgNi <sub>2</sub>	MgNi <sub>2</sub>	<i>hP24</i> <i>P6<sub>3</sub>/mmc</i>	Mg <sub>1</sub> 4 Mg <sub>2</sub> 4 Ni <sub>1</sub> 4 Ni <sub>2</sub> 6 Ni <sub>3</sub> 6	
	Mg <sub>2</sub> Ni	Mg <sub>2</sub> Ni	<i>hP18</i> <i>P6<sub>2</sub>22</i>	Mg <sub>1</sub> 6 Mg <sub>2</sub> 6 Ni <sub>1</sub> 3 Ni <sub>2</sub> 3	in Mas2, Mg <sub>2</sub> Ni related to Al <sub>2</sub> Cu-C16 type according to [90Mas]

# System Mg-Si

**Solution Phases:**

(stable)	Liquid, hcp- <i>A3</i>
(metastable)	fcc- <i>A1</i>

**Compound:**

(stable)	Mg <sub>2</sub> Si
(metastable)	Laves- <i>C15</i>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
hcp- <i>A3</i>	:	Substitutional, Redlich-Kister
fcc- <i>A1</i>	:	Substitutional, Redlich-Kister
Mg <sub>2</sub> Si	:	Stoichiometric, (Mg) <sub>2</sub> (Si)
Laves- <i>C15</i>	:	Sublattice model, (Mg,Si) <sub>2</sub> (Mg,Si)

**Publication:**

H. Heufel, T. Gödecke, H.-L. Lukas, and F. Sommer,  
J. Alloys and Comp., **247**, (1-2), 31-42 (1997).

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase liquid**

$$L_{\text{Mg},\text{Si}}^{0,\text{liquid}} = -83864.26 + 32.44438 \cdot T$$

$$L_{\text{Mg},\text{Si}}^{1,\text{liquid}} = 18027.41 - 19.61202 \cdot T$$

$$L_{\text{Mg},\text{Si}}^{2,\text{liquid}} = 2486.67 - 0.31084 \cdot T$$

$$L_{\text{Mg},\text{Si}}^{3,\text{liquid}} = 18541.17 - 2.317664 \cdot T$$

$$L_{\text{Mg},\text{Si}}^{4,\text{liquid}} = -12338.84 + 1.54236 \cdot T$$

**Phase hcp-*A3***

$$L_{\text{Mg},\text{Si}:□}^{0,\text{hcp-}A3} = -7148.79 + 0.89361 \cdot T$$

**Phase fcc-A1**

$$L_{\text{Mg}, \text{Si}: \square}^{0, \text{fcc}-\text{A}1} = -7148.79 + 0.89361 T$$

**Phase Mg<sub>2</sub>Si**

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = \\ - 92250.0 + 440.4 T - 75.9 T \cdot \ln T - 0.0018 T^2 + 630000 T^{-1}$$

**Phase Laves-C15**

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Mg:Si}) = \\ 104970.96 - 16.46448 T + 2.0 \text{ GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Si}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) - 2.0 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Si:Mg}) = \\ 41039.0 + 6.25 T + \text{GHSER}_{\text{Mg}} + 2.0 \text{ GHSER}_{\text{Si}}$$

$$L_{\text{Mg}, \text{Si}: \text{Mg}}^{0, \text{LavesC}15} = 15000.0$$

=

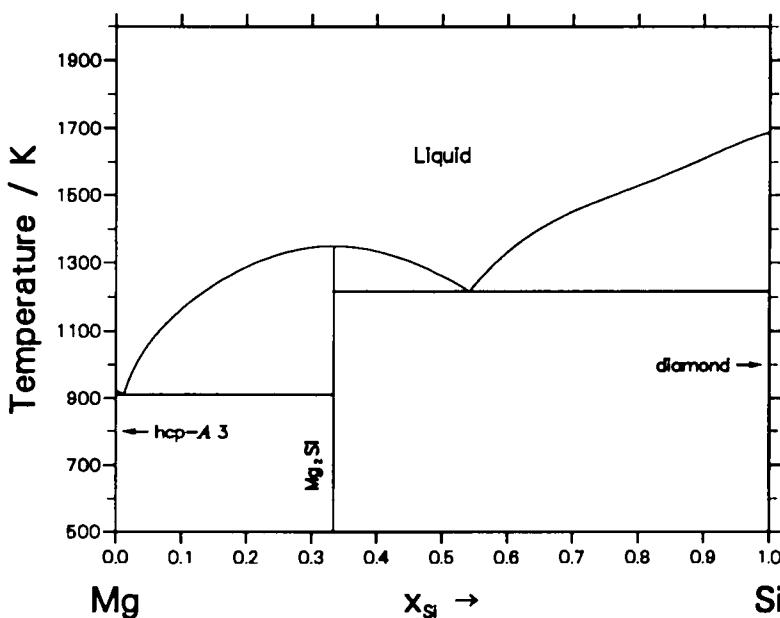
$$L_{\text{Mg}, \text{Si}: \text{Si}}^{0, \text{LavesC}15} = 15000.0$$

=

$$L_{\text{Mg}: \text{Mg}, \text{Si}}^{0, \text{LavesC}15} = 8000.0$$

=

$$L_{\text{Si}: \text{Mg}, \text{Si}}^{0, \text{LavesC}15} = 8000.0$$



**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Si}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ hcp-A3 + Mg <sub>2</sub> Si	Eutectic	.013	.000	.333	911.8
Liquid $\rightleftharpoons$ Mg <sub>2</sub> Si + diamond	Eutectic	.530	.333	1.000	1214.4
Mg <sub>2</sub> Si $\rightleftharpoons$ Liquid	Congruent	.333	.333	...	1350.0

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices
Mg-Si	(Mg)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2
	(Si)	diamond	<i>cF8</i> <i>Fd<sub>3</sub>m</i>	M 8
	Mg <sub>2</sub> Si	CaF <sub>2</sub>	<i>cFl2</i> <i>Fm<sub>3</sub>m</i>	Mg 8 Si 4

# System Mg–Y

**Solution Phases:**

Liquid, bcc-*A*2, hcp-*A*3

**Compounds:**

MgY, Mg<sub>24</sub>Y<sub>5</sub>, Mg<sub>2</sub>Y

**Modelling:**

Liquid	:	Substitutional, Redlich–Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich–Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich–Kister
MgY	:	Stoichiometric, (Mg)(Y)
Mg <sub>2</sub> Y	:	Stoichiometric, (Mg) <sub>2</sub> (Y)
Mg <sub>24</sub> Y <sub>5</sub>	:	Sublattice model, (Mg) <sub>24</sub> (Mg,Y) <sub>5</sub>

**Assessor and Date:**

H.L. Lukas, 1991

**Thermodynamic properties of the solution and compound phases (J·mol<sup>-1</sup>)**

**Phase bcc-*A*2**

$$L_{\text{Mg},\text{Y}:□}^{0,\text{bcc-}A2} = - 38570.0 + 15.0 \ T$$

$$L_{\text{Mg},\text{Y}:□}^{1,\text{bcc-}A2} = - 8204.21$$

**Phase hcp-*A*3**

$$L_{\text{Mg},\text{Y}:□}^{0,\text{hcp-}A3} = - 16582.94 + 4.77482 \ T$$

$$L_{\text{Mg},\text{Y}:□}^{1,\text{hcp-}A3} = - 7077.87$$

**Phase liquid**

$$L_{\text{Mg},\text{Y}}^{0,\text{liquid}} = - 25802.51 + 4.30042 \ T$$

$$L_{\text{Mg},\text{Y}}^{1,\text{liquid}} = - 19229.76 + 3.20497 \ T$$

**Phase fcc-A1**

$$L_{\text{Mg},\text{Y}}^{0,\text{fcc}-\text{A}1} = 0.0001$$

**Phase  $\text{Mg}_{24}\text{Y}_5$** 

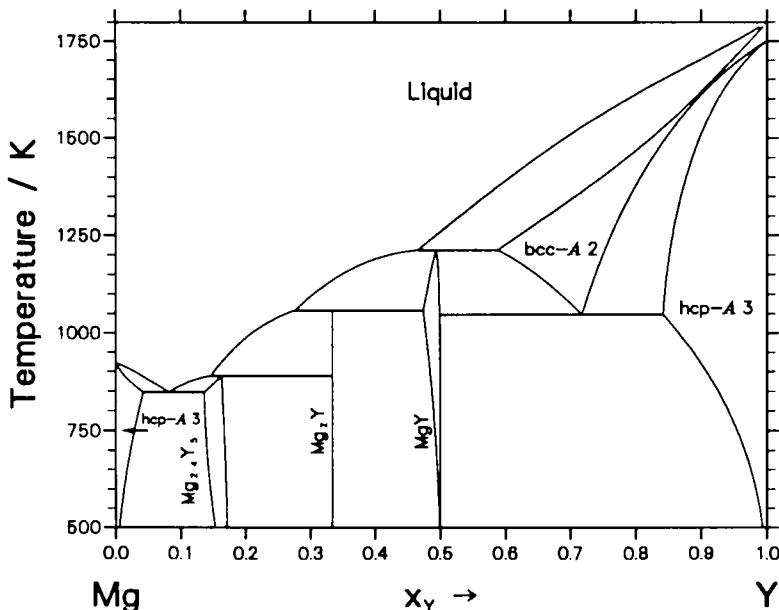
$$G^\circ(T) - 24.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) - 5.0 \ H_{\text{Y}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Mg:Y}) = \\ - 227282.28 + 36.52985 \ T + 24.0 \ \text{GHSER}_{\text{Mg}} + 5.0 \ \text{GHSER}_{\text{Y}}$$

**Phase  $\text{Mg}_2\text{Y}$** 

$$G^\circ(T) - 2.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) - H_{\text{Y}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Mg:Y}) = \\ - 39075.78 + 6.51258 \ T + 2.0 \ \text{GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Y}}$$

**Phase MgY**

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) - H_{\text{Y}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Mg:Y}) = \\ - 32162.76 + 8.0 \ T + \text{GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Y}}$$



**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_Y$			$T / K$
Liquid + bcc-A2 $\rightleftharpoons$ MgY	Peritectic	.466	.588	.494	1213.3
Liquid + MgY $\rightleftharpoons$ Mg <sub>2</sub> Y	Peritectic	.276	.474	.333	1058.5
Liquid+ Mg <sub>2</sub> Y $\rightleftharpoons$ Mg <sub>24</sub> Y <sub>5</sub>	Peritectic	.146	.333	.163	889.4
Liquid $\rightleftharpoons$ hcp-A3 + Mg <sub>24</sub> Y <sub>5</sub>	Eutectic	.082	.042	.136	847.6
bcc-A2 $\rightleftharpoons$ MgY + hcp-A3	Eutectoid	.717	.499	.841	1048.0

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Mg-Y	(Mg)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	(Y)	W	<i>cI2</i> <i>Im<math>\bar{3}</math>m</i>	M 4	
	(Y)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	Mg <sub>24+x</sub> Y <sub>5</sub>	$\alpha$ -Mn	<i>cI58</i> <i>I43m</i>	M 2 Mg <sub>1</sub> 24 Mg <sub>2</sub> 24 Y 8	cbcc-A12 designated as Mg <sub>24</sub> Y <sub>5</sub>
	Mg <sub>2</sub> Y	MgZn <sub>2</sub>	<i>hP12</i> <i>P6<sub>3</sub>/mmc</i>	Mg <sub>1</sub> 2 Mg <sub>2</sub> 6	
	Mg <sub>1+x</sub> Y	CsCl	<i>cP2</i> <i>Pm<math>\bar{3}</math>m</i>	Mg 1 Y 1	bcc-B2 designated as MgY

## System Mg-Zn

**Solution Phases:**

- (stable) : Liquid, hcp-Zn, Laves-C14  
 (metastable) : bcc-A2, bcc-B2, fcc-A1, hcp-A3

**Compounds:**

- (stable) :  $\text{Mg}_2\text{Zn}_{11}$ ,  $\text{MgZn}$ ,  $\text{Mg}_2\text{Zn}_3$ ,  $\text{Mg}_{51}\text{Zn}_{20}$   
 (metastable) :  $\text{AlMg}-\beta$ ,  $\text{AlMg}-\epsilon$ ,  $\text{AlMg}-\gamma$ ,  $\text{AlMgZn}-\phi$   
 (metastable) : Laves-C15, Laves-C36

**Modelling:**

- Liquid : Substitutional, Redlich-Kister  
 hcp-Zn : Substitutional, Redlich-Kister  
 bcc-A2 : see below  
 bcc-B2 : Sublattice model,  $(\text{Mg},\text{Zn})_{0.5}(\text{Mg},\text{Zn})_{0.5}(\square)_3$   
           Two descriptions of the bcc-A2:bcc-B2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.  
 fcc-A1 : Substitutional, Redlich-Kister  
 hcp-A3 : Substitutional, Redlich-Kister  
 $\text{Mg}_2\text{Zn}_{11}$  : Stoichiometric,  $(\text{Mg})_2(\text{Zn})_{11}$   
 $\text{MgZn}$  : Stoichiometric,  $(\text{Mg})_{12}(\text{Zn})_{13}$   
 $\text{Mg}_2\text{Zn}_3$  : Stoichiometric,  $(\text{Mg})_2(\text{Zn})_3$   
 $\text{Mg}_{51}\text{Zn}_{20}$  : Stoichiometric,  $(\text{Mg})_{51}(\text{Zn})_{20}$   
 $\text{AlMgZn}-\phi$  : Stoichiometric,  $(\text{Mg})_6(\text{Zn})_5$   
 $\text{AlMg}-\beta$  : Stoichiometric,  $(\text{Mg})_{89}(\text{Zn})_{104}$   
 $\text{AlMg}-\epsilon$  : Stoichiometric,  $(\text{Mg})_{23}(\text{Zn})_{30}$   
 $\text{AlMg}-\gamma$  : Sublattice model,  $(\text{Mg})_5(\text{Mg},\text{Zn})_{12}(\text{Mg},\text{Zn})_{12}$   
 Laves-C14 : Sublattice model,  $(\text{Mg},\text{Zn})_2(\text{Mg},\text{Zn})$   
 Laves-C15 : Sublattice model,  $(\text{Mg},\text{Zn})_2(\text{Mg},\text{Zn})$   
 Laves-C36 : Sublattice model,  $(\text{Mg},\text{Zn})_2(\text{Mg},\text{Zn})$

Assessor and Date:

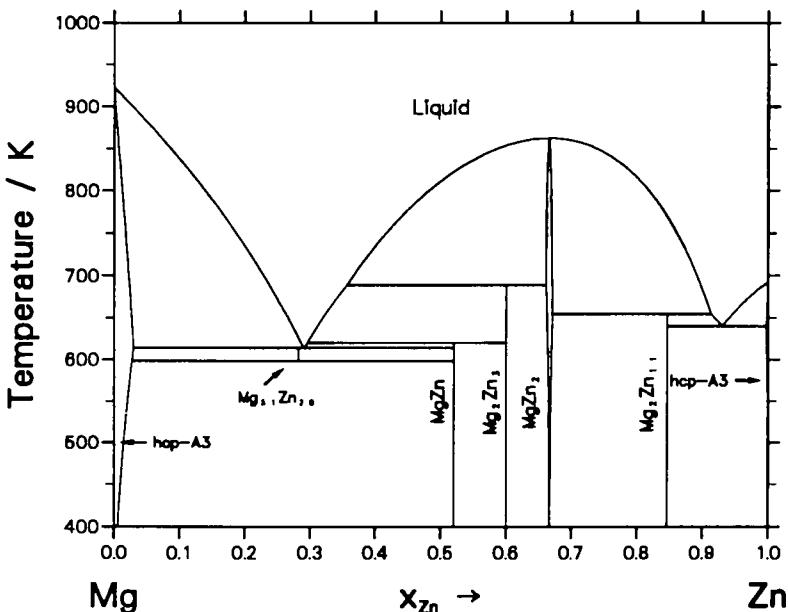
R. Agarwal, S.G. Fries, H.L. Lukas, G. Petzow,  
F. Sommer, T.G. Chart, G. Effenberg

Publication:

Z. für Metallkde., 83, 4, 216–223 (1992).

Comments:

A reevaluation was performed in order to take into account the non-stoichiometry of the Laves-C14 phase.

Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**Phase fcc-A1**

$$L_{\text{Mg}, \text{Zn}:0}^{0,\text{fcc}-\text{A}1} = -3056.82 + 5.63801 \cdot T$$

$$L_{\text{Mg}, \text{Zn}:0}^{1,\text{fcc}-\text{A}1} = -3127.26 + 5.65563 \cdot T$$

### Phase hcp-Zn

$$L_{\text{Mg},\text{Zn}:0}^{0,\text{hcp-Zn}} = -3056.82 + 5.63801 T$$

$$L_{\text{Mg},\text{Zn}:0}^{1,\text{hcp-Zn}} = -3127.26 + 5.65563 T$$

### Phase hcp-A3

$$L_{\text{Mg},\text{Zn}:0}^{0,\text{hcp-A3}} = -3056.82 + 5.63801 T$$

$$L_{\text{Mg},\text{Zn}:0}^{1,\text{hcp-A3}} = -3127.26 + 5.65563 T$$

### Phase liquid

$$L_{\text{Mg},\text{Zn}}^{0,\text{liquid}} = -77729.24 + 680.52266 T - 95.0 T \cdot \ln T + 0.04 T^2$$

$$L_{\text{Mg},\text{Zn}}^{1,\text{liquid}} = 3674.72 + 0.57139 T$$

$$L_{\text{Mg},\text{Zn}}^{2,\text{liquid}} = -1588.15$$

### Phase AlMg- $\beta$

$$G^\circ(T) - 89.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 104.0 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = \\ 206100 + 89.0 \text{ GHSER}_{\text{Mg}} + 104.0 \text{ GHSER}_{\text{Zn}}$$

### Phase AlMg- $\epsilon$

$$G^\circ(T) - 23.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 30.0 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = \\ -318000 + 63.6 T + 23.0 \text{ GHSER}_{\text{Mg}} + 30.0 \text{ GHSER}_{\text{Zn}}$$

### Phase AlMg- $\gamma$

$$G^\circ(T) - 17.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 12.0 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Mg:Mg:Zn}) = \\ -145000 + 58 T + 17.0 \text{ GHSER}_{\text{Mg}} + 12.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 17.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 12.0 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Mg:Zn:Mg}) = \\ 87000 + 29 T + 17.0 \text{ GHSER}_{\text{Mg}} + 12.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 5.0 H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) - 24.0 H_{\text{Zn}}^{\circ,\text{hcp-Zn}}(298.15 \text{ K}) = G(\text{Mg:Zn:Zn}) = \\ 290000.0 + 5.0 \text{ GHSER}_{\text{Mg}} + 24.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Mg:Mg,Zn:Mg}}^{0,\text{AlMg-}\gamma} = L_{\text{Mg:Mg,Zn:Zn}}^{0,\text{AlMg-}\gamma} = -116000 + 58 T$$

**Phase Mg<sub>51</sub>Zn<sub>20</sub>**

$$G^\circ(T) - 51.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 20.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = \\ - 335741.54 + 35.5 T + 51.0 \text{ GHSER}_{\text{Mg}} + 20.0 \text{ GHSER}_{\text{Zn}}$$

**Phase MgZn**

$$G^\circ(T) - 12.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 13.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = \\ - 236980.84 + 59.24524 T + 12.0 \text{ GHSER}_{\text{Mg}} + 13.0 \text{ GHSER}_{\text{Zn}}$$

**Phase Mg<sub>2</sub>Zn<sub>3</sub>**

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = \\ - 54406.20 + 13.60156 T + 2.0 \text{ GHSER}_{\text{Mg}} + 3.0 \text{ GHSER}_{\text{Zn}}$$

**Phase Mg<sub>2</sub>Zn<sub>11</sub>**

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 11.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = \\ - 73818.32 + 18.45457 T + 2.0 \text{ GHSER}_{\text{Mg}} + 11.0 \text{ GHSER}_{\text{Zn}}$$

**Phase AlMgZn- $\phi$** 

$$G^\circ(T) - 6.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 5.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = \\ - 79530 + 20.9 T + 6.0 \text{ GHSER}_{\text{Mg}} + 5.0 \text{ GHSER}_{\text{Zn}}$$

**Phase Laves-C14**

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Mg:Zn}) = \\ 65355.45 - 8.83886 T + 2.0 \text{ GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Zn:Mg}) = \\ - 35355.45 + 8.83886 T + \text{GHSER}_{\text{Mg}} + 2.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Zn:Zn}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Mg},\text{Zn:Mg}}^{0,\text{Laves-C14}} = L_{\text{Mg},\text{Zn:Zn}}^{0,\text{Laves-C14}} = 35000.0$$

$$L_{\text{Mg:Mg},\text{Zn}}^{0,\text{Laves-C14}} = L_{\text{Zn:Mg},\text{Zn}}^{0,\text{Laves-C14}} = 8000.0$$

### Phase Laves-C15

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Mg:Zn}) = \\ 55355.45 - 8.83886 T + 2.0 \text{ GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Zn:Mg}) = \\ - 25355.45 + 8.83886 T + \text{GHSER}_{\text{Mg}} + 2.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Zn:Zn}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Mg},\text{Zn}: \text{Mg}}^{0,\text{Laves}-C15} = L_{\text{Mg},\text{Zn}: \text{Zn}}^{0,\text{Laves}-C15} = 35000.0$$

$$L_{\text{Mg}: \text{Mg}, \text{Zn}}^{0,\text{Laves}-C15} = L_{\text{Zn}: \text{Mg}, \text{Zn}}^{0,\text{Laves}-C15} = 8000.0$$

### Phase Laves-C36

$$G^\circ(T) - 3.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Mg}}$$

$$G^\circ(T) - 2.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Mg:Zn}) = \\ 65355.45 - 8.83886 T + 2.0 \text{ GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Zn:Mg}) = \\ - 35355.45 + 8.83886 T + \text{GHSER}_{\text{Mg}} + 2.0 \text{ GHSER}_{\text{Zn}}$$

$$G^\circ(T) - 3.0 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Zn:Zn}) = 15000.0 + 3.0 \text{ GHSER}_{\text{Zn}}$$

$$L_{\text{Mg},\text{Zn}: \text{Mg}}^{0,\text{Laves}-C36} = L_{\text{Mg},\text{Zn}: \text{Zn}}^{0,\text{Laves}-C36} = 35000.0$$

$$L_{\text{Mg}: \text{Mg}, \text{Zn}}^{0,\text{Laves}-C36} = L_{\text{Zn}: \text{Mg}, \text{Zn}}^{0,\text{Laves}-C36} = 8000.0$$

### Phase bcc-B2

$$G_{\text{Mg}: \text{Zn}: \square}^* = 0.0$$

$$L_{\text{Mg}, \text{Zn}}^0 = - 2500.0$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg:}\square) = \text{GBCC}_{\text{Mg}}$$

$$G^\circ(T) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Mg:Zn:}\square) = \\ G_{\text{Mg}: \text{Zn}: \square}^* + L_{\text{Mg}, \text{Zn}}^0 + 0.5 \text{ GBCC}_{\text{Mg}} + 0.5 \text{ GBCC}_{\text{Zn}}$$

$$G^\circ(T) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Zn:Mg:}\square) = \\ G_{\text{Mg}: \text{Zn}: \square}^* + L_{\text{Mg}, \text{Zn}}^0 + 0.5 \text{ GBCC}_{\text{Mg}} + 0.5 \text{ GBCC}_{\text{Zn}}$$

$$G^\circ(T) - H_{\text{Zn}}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) = G(\text{Zn:Zn:}\square) = \text{GBCC}_{\text{Zn}}$$

$$L_{\text{Mg}, \text{Zn}: \text{Mg}: \square}^{0,\text{bcc}-B2} = L_{\text{Mg}, \text{Zn}: \text{Zn}: \square}^{0,\text{bcc}-B2} = - G_{\text{Mg}: \text{Zn}: \square}^* + L_{\text{Mg}, \text{Zn}}^0$$

$$L_{\text{Mg}, \text{Zn}: \text{Zn}: \square}^{0,\text{bcc}-B2} = L_{\text{Zn}: \text{Mg}, \text{Zn}: \square}^{0,\text{bcc}-B2} = - G_{\text{Mg}: \text{Zn}: \square}^* + L_{\text{Mg}, \text{Zn}}^0$$

## Phase bcc-B2

$$G_{\text{Mg:Zn:}\square}^* = 0.0$$

$$L_{\text{Mg,Zn}}^0 = -2500.0$$

$$G^\circ(T) - H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Mg:Zn:}\square) = 2.0 G_{\text{Mg:Zn:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 0.5 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Mg:}\square) = 2.0 G_{\text{Mg:Zn:}\square}^*$$

$$G^\circ(T) - H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Zn:Zn:}\square) = 0.0$$

## Phase bcc-A2

$$L_{\text{Mg,Zn:}\square}^{0,\text{bcc}-A2} = 4.0 L_{\text{Mg,Zn}}^0$$

Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Zn}}$			$T / \text{K}$
Liquid + hcp-A3 $\rightleftharpoons$ Mg <sub>51</sub> Zn <sub>20</sub>	Peritectic	.295	.029	.289	614.1
Liquid $\rightleftharpoons$ Mg <sub>51</sub> Zn <sub>20</sub> + MgZn	Eutectic	.281	.290	.520	614.1
Liquid + Mg <sub>2</sub> Zn <sub>3</sub> $\rightleftharpoons$ MgZn	Peritectic	.196	.600	.520	620.1
Liquid + Laves-C14 $\rightleftharpoons$ Mg <sub>2</sub> Zn <sub>3</sub>	Peritectic	.356	.661	.600	688.9
Liquid $\rightleftharpoons$ MgZn <sub>2</sub>	Congruent	.667	.667	....	864.0
Liquid + Laves-C14 $\rightleftharpoons$ Mg <sub>2</sub> Zn <sub>11</sub>	Peritectic	.913	.661	.846	654.4
Liquid $\rightleftharpoons$ Mg <sub>2</sub> Zn <sub>11</sub> $\rightleftharpoons$ hcp-A3	Eutectic	.926	.846	.997	637.3
Mg <sub>51</sub> Zn <sub>20</sub> $\rightleftharpoons$ hcp-A3 + MgZn	Eutectoid	.282	.027	.520	598.1

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub- Model	Comments
Mg-Zn	(Mg)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	(Zn)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	MgZn <sub>2</sub>	MgZn <sub>2</sub>	<i>hP12</i> <i>P6<sub>3</sub>/mmc</i>	Mg 4 Zn <sub>1</sub> 2 Zn <sub>3</sub> 6	Laves-C14
	Mg <sub>2</sub> Zn <sub>11</sub>	Mg <sub>2</sub> Zn <sub>11</sub>	<i>cP39</i> <i>Pm<math>\bar{3}</math></i>		
	MgZn				
	Mg <sub>2</sub> Zn <sub>3</sub>		<i>mC110</i> <i>B2/m</i>		
	Mg <sub>7</sub> Zn <sub>3</sub>	Ta <sub>3</sub> B <sub>4</sub>	<i>oI142</i> <i>Immm</i>		designated as Mg <sub>51</sub> Zn <sub>20</sub>

# System Mg-Zr

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, hcp- <i>A</i> 3
(metastable)	fcc- <i>A</i> 1

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister

**Assessor and Date:**

M. Hämäläinen 1991

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A*2**

$$I_{\text{Mg,Zr:\square}}^{0,\text{bcc-}A^2} = 5720.44 + 50.11642 \ T$$

**Phase fcc-*A*1**

$$I_{\text{Mg,Zr:\square}}^{0,\text{fcc-}A^1} = 42063.55 + 1.01789 \ T$$

$$I_{\text{Mg,Zr:\square}}^{1,\text{fcc-}A^1} = -2885.9$$

**Phase hcp-*A*3**

$$I_{\text{Mg,Zr:\square}}^{0,\text{hcp-}A^3} = 42063.55 + 1.01789 \ T$$

$$I_{\text{Mg,Zr:\square}}^{1,\text{hcp-}A^3} = -2885.9$$

**Phase liquid**

$$I_{\text{Mg,Zr}}^{0,\text{liquid}} = 14003.84 + 29.34205 \ T$$

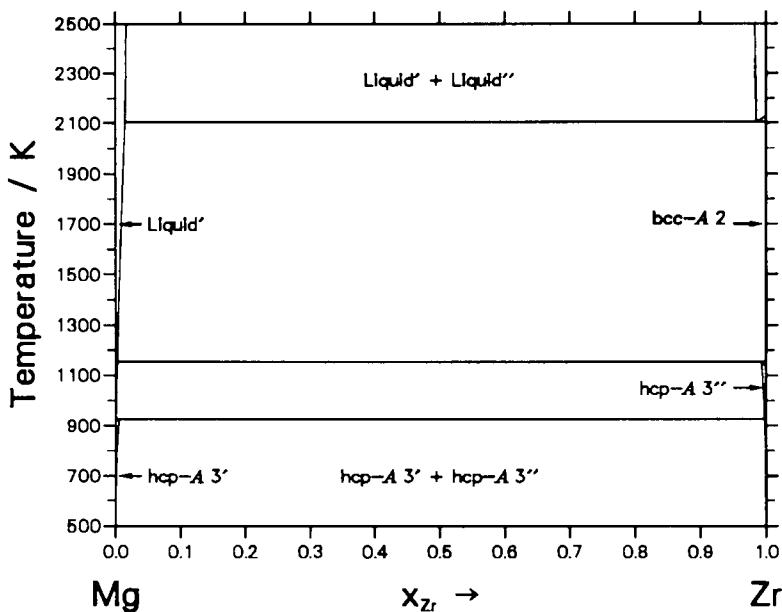


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Zr}}$	$T / \text{K}$
$\text{Liquid}' + \text{bcc}-A2 \rightleftharpoons \text{hcp}-A3$	Peritectic	.003    1.000    .993	1154.6
$\text{Liquid}'' \rightleftharpoons \text{Liquid}' + \text{bcc}-A2$	Monotectic	.985    .015    .999	2104.8
$\text{Liquid}' + \text{hcp}-A3'' \rightleftharpoons \text{hcp}-A3'$	Peritectic	.001    .997    .006	926.6

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Mg-Zr	(Mg)	Mg	$hP2$ $P6_3/mmc$
	(Zr)	Mg	$hP2$ $P6_3/mmc$
	(Zr)	W	$cI2$ $Im\bar{3}m$

# System Mn–Si

**Solution Phases:**

Liquid, bcc-*A*2, cbcc-*A*12, cub-*A*13, fcc-*A*1

**Compounds:**

(stable)	Mn <sub>6</sub> Si, Mn <sub>9</sub> Si <sub>2</sub> , Mn <sub>3</sub> Si, Mn <sub>5</sub> Si <sub>3</sub> , MnSi, Mn <sub>11</sub> Si <sub>19</sub>
(metastable)	Al <sub>8</sub> Mn <sub>5</sub> -D8 <sub>10</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
cbcc- <i>A</i> 12	:	Substitutional, Redlich-Kister
cub- <i>A</i> 13	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
Mn <sub>6</sub> Si	:	Stoichiometric, (Mn) <sub>17</sub> (Si) <sub>3</sub>
Mn <sub>9</sub> Si <sub>2</sub>	:	Stoichiometric, (Mn) <sub>33</sub> (Si) <sub>7</sub>
Mn <sub>3</sub> Si	:	Stoichiometric, (Mn) <sub>3</sub> (Si)
Mn <sub>5</sub> Si <sub>3</sub>	:	Stoichiometric, (Mn) <sub>5</sub> (Si) <sub>3</sub>
MnSi	:	Stoichiometric, (Mn)(Si)
Mn <sub>11</sub> Si <sub>19</sub>	:	Stoichiometric, (Mn) <sub>11</sub> (Si) <sub>19</sub>
Al <sub>8</sub> Mn <sub>5</sub> -D8 <sub>10</sub>	:	Sublattice model, (Si) <sub>12</sub> (Mn) <sub>4</sub> (Mn) <sub>10</sub>

**Assessor and Date:**

J.E. Tibballs, 1991

**Publication:**

SI-report, 890221-5, 1991

## Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)

**Phase Mn<sub>3</sub>Si**

$$\begin{aligned}
 G^\circ(T) - 3.0 \ H_{\text{Mn}}^{\circ, \text{cbcc-}A12, \text{para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = \\
 298.15 < T < 950.00 : -124189.87 + 782.4373 \ T - 131.682 \ T \cdot \ln T \\
 &\quad - 0.00777 \ T^2 + 1657200 \ T^{-1} \\
 950.00 < T < 2000.00 : -119740.6 + 777.7538 \ T - 131.682 \ T \cdot \ln T \\
 &\quad - 0.00777 \ T^2 + 1657200 \ T^{-1}
 \end{aligned}$$

### Phase MnSi

$$G^\circ(T) = H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$- 78135.144 + 308.2488 T - 52.42121 T \cdot \ln T - 0.006903355 T^2$$

$$+ 876442.9 T^{-1}$$

### Phase $\text{Mn}_{11}\text{Si}_{19}$

$$G^\circ(T) = 11.0 H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) - 19.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$- 636300.0 + 1624.93 T - 378.694 T \cdot \ln T - 0.16391 T^2$$

$$- 15432618 T^{-1}$$

### Phase $\text{Mn}_6\text{Si}$

$$G^\circ(T) = 17.0 H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 1519.00 : & - 250180.6 + 84.8444 T - 12.07755 T \cdot \ln T \\ & - 0.02850984 T^2 + 7514 T^{-1} \\ & + 17.0 \text{ GHSER}_{\text{Mn}} + 3.0 \text{ GHSER}_{\text{Si}} \\ 1519.00 < T < 3000.00 : & - 282008.6 - 32.58304 T + 12.06754 T \cdot \ln T \\ & - 0.05879165 T^2 + 3.928228E+31 T^{-9} \\ & + 17.0 \text{ GHSER}_{\text{Mn}} + 3.0 \text{ GHSER}_{\text{Si}} \end{aligned}$$

### Phase $\text{Mn}_9\text{Si}_2$

$$G^\circ(T) = 33.0 H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) - 7.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 1519.00 : & - 578208.4 + 381.294 T - 56.86988 T \cdot \ln T \\ & - 0.0500355 T^2 + 1458600 T^{-1} \\ & + 33.0 \text{ GHSER}_{\text{Mn}} + 7.0 \text{ GHSER}_{\text{Si}} \\ 298.15 < T < 1519.00 : & - 639992.0 + 153.3464 T - 10.0 T \cdot \ln T \\ & - 0.1 T^2 + 7.625384E+31 T^{-9} \\ & + 33.0 \text{ GHSER}_{\text{Mn}} + 7.0 \text{ GHSER}_{\text{Si}} \end{aligned}$$

### Phase $\text{Mn}_5\text{Si}_3$

$$G^\circ(T) = 5.0 H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$- 261930.32 + 1170.778 T - 211.150 T \cdot \ln T - 0.015293 T^2$$

$$- 149263.11 T^{-1}$$

### Phase $\text{Al}_8\text{Mn}_5-D8_{10}$

$$G^\circ(T) = 14.0 H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) - 12.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) =$$

$$+ 14.0 \text{ GHSER}_{\text{Mn}} + 12.0 \text{ GHSER}_{\text{Si}}$$

### Phase bcc-A2

$$L_{\text{Mn},\text{Si};\square}^{0,\text{bcc}-A2} = - 89620.7 + 2.94097 T$$

$$L_{\text{Mn},\text{Si};\square}^{1,\text{bcc}-A2} = - 7500.0$$

**Phase cbcc-A12**

$$L_{\text{Mn},\text{Si}:0}^{0,\text{cbcc}-\text{A12}} = -142743.62 + 22.3961 \cdot T$$

$$L_{\text{Mn},\text{Si}:0}^{1,\text{cbcc}-\text{A12}} = 16440.608 - 3.5300332 \cdot T$$

**Phase cub-A13**

$$L_{\text{Mn},\text{Si}:0}^{0,\text{cub}-\text{A13}} = -142343.62 + 21.892610 \cdot T$$

$$L_{\text{Mn},\text{Si}:0}^{1,\text{cub}-\text{A13}} = 16440.608 - 3.5300332 \cdot T$$

**Phase fcc-A1**

$$L_{\text{Mn},\text{Si}:0}^{0,\text{fcc}-\text{A1}} = -95600 + 2.94097 \cdot T$$

$$L_{\text{Mn},\text{Si}:0}^{1,\text{fcc}-\text{A1}} = -7500$$

**Phase liquid**

$$L_{\text{Mn},\text{Si}}^{\text{liquid}} = -139817 + 29.86137 \cdot T$$

$$L_{\text{Mn},\text{Si}}^{\text{1,liquid}} = -34917.2 + 3.20488 \cdot T$$

$$L_{\text{Mn},\text{Si}}^{\text{2,liquid}} = 46782.4 - 1.8 \cdot 1.1897 \cdot T$$

$$L_{\text{Mn},\text{Si}}^{\text{3,liquid}} = 16168.2$$

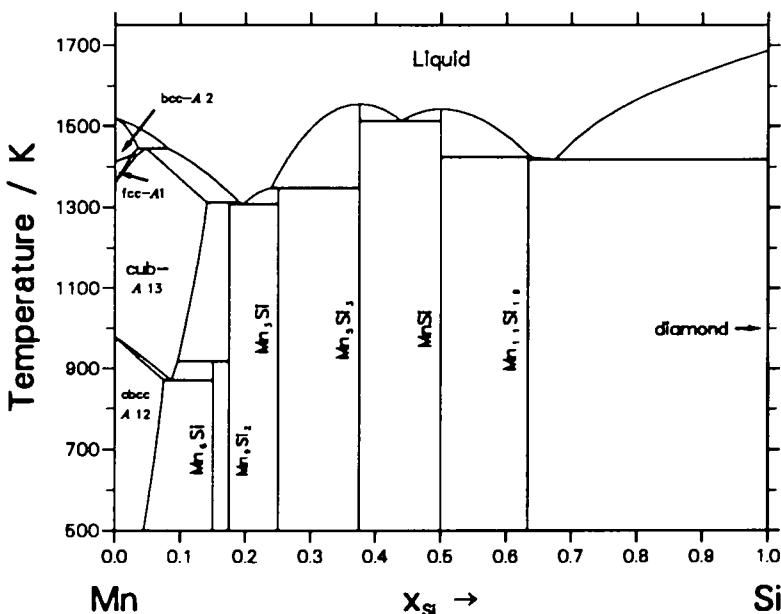


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Si}}$			$T / \text{K}$
Liquid + bcc-A2 $\rightleftharpoons$ cub-A13	Peritectic	.080	.035	.046	1445.3
bcc-A2 + cub-A13 $\rightleftharpoons$ fcc-A1	Peritectic	.024	.024	.033	1426.6
Liquid + cub-A13 $\rightleftharpoons$ Mn <sub>9</sub> Si <sub>2</sub>	Peritectic	.191	.140	.175	1312.7
Liquid $\rightleftharpoons$ Mn <sub>9</sub> Si <sub>2</sub> + Mn <sub>3</sub> Si	Eutectic	.197	.175	.250	1309.3
Liquid + Mn <sub>5</sub> Si <sub>3</sub> $\rightleftharpoons$ Mn <sub>3</sub> Si	Peritectic	.239	.375	.250	1348.0
Mn <sub>5</sub> Si <sub>3</sub> $\rightleftharpoons$ Liquid	Congruent	.375	.375	.....	1556.0
Liquid $\rightleftharpoons$ Mn <sub>5</sub> Si <sub>3</sub> + MnSi	Eutectic	.439	.375	.500	1513.4
MnSi $\rightleftharpoons$ Liquid	Congruent	.500	.500	.....	1544.0
Liquid + MnSi $\rightleftharpoons$ Mn <sub>11</sub> Si <sub>19</sub>	Peritectic	.639	.500	.633	1423.4
Liquid $\rightleftharpoons$ diamond + Mn <sub>11</sub> Si <sub>19</sub>	Eutectic	.674	.633	1.000	1417.1
cub-A13 + Mn <sub>9</sub> Si <sub>2</sub> $\rightleftharpoons$ Mn <sub>6</sub> Si	Peritectoid	.096	.170	.150	918.0
cbcc-A12 $\rightleftharpoons$ cub-A13 + Mn <sub>6</sub> Si	Eutectoid	.086	.075	.150	870.6

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Mn-Si	$\alpha$ -Mn	$\alpha$ -Mn	$c58$ $I\bar{4}3m$		cbcc-A12
	$\beta$ -Mn	$\beta$ -Mn	$cP20$ $P4_1323m$		cub-A13
	$\gamma$ -Mn	Cu	$cF4$ $Fm\bar{3}m$		
	$\delta$ -Mn	W	$cI2$ $I\bar{m}\bar{3}m$		
	(Si)	diamond	$cF8$ $Fd\bar{3}m$	M 8	
	MnSi	FeSi	$cP8$ $P2_13$	Mn 4 Si 4	
	Mn <sub>3</sub> Si- $\alpha$			M <sub>1</sub> 4	transformation not considered
	Mn <sub>3</sub> Si- $\beta$	BiF <sub>3</sub>	$cF16$ $Fm\bar{3}m$	M <sub>1</sub> 4 M <sub>2</sub> 4 M <sub>3</sub> 8	
	Mn <sub>5</sub> Si <sub>2</sub>	Mn <sub>5</sub> Si <sub>2</sub>	$tP56$ $P4_12_12$		

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
	$\text{Mn}_{11}\text{Si}_{19}$	$\text{Mn}_{11}\text{Si}_{19}$	$tP120$ $P\bar{4}n2$		$\text{MnSi}_{1.75-\epsilon}$ in [90Mas]
	$\text{Mn}_{44}\text{Si}_9$	Mo	$hR53$ $R\bar{3}$	$M_1$ 1 $M_2$ 2 $M_3$ 6 $M_5$ 6 $M_6$ 6 $M_{n1}$ 2 $M_{n2}$ 6 $M_{n3}$ 6 $M_{n4}$ 6 $M_{n5}$ 6	approximated as $\text{Mn}_6\text{Si}$
	$\text{Mn}_5\text{Si}_3$	$\text{Mn}_5\text{Si}_3$	$hP16$ $P6_3/mcm$	$M_{n1}$ 4 $M_{n2}$ 6 Si 6	

# System Mn-Ti

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1, hcp-*A*3, cbcc-*A*12, cub-*A*13

**Compounds:**

Mn<sub>4</sub>Ti, Mn<sub>3</sub>Ti, MnTi- $\alpha$ , MnTi- $\beta$ , Laves-*C*14

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
cbcc- <i>A</i> 12	:	Substitutional, Redlich-Kister
cub- <i>A</i> 13	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Laves- <i>C</i> 14	:	Sublattice model: (Mn,Ti) <sub>2</sub> (Mn,Ti)
Mn <sub>4</sub> Ti	:	Stoichiometric, (Mn) <sub>0.815</sub> (Ti) <sub>0.185</sub>
MnTi- $\alpha$	:	Stoichiometric, (Mn)(Ti)
MnTi- $\beta$	:	Stoichiometric, (Mn) <sub>0.515</sub> (Ti) <sub>0.485</sub>

**Assessor and Date:**

N. Saunders, 1993

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A*2**

$$L_{\text{Mn,Ti:\square}}^{0,\text{bcc-}A2} = -23200 + 20 \ T$$

$$L_{\text{Mn,Ti:\square}}^{1,\text{bcc-}A2} = -1000$$

**Phase cbcc-*A*12**

$$L_{\text{Mn,Ti:\square}}^{0,\text{cbcc-}A12} = -29500 + 20 \ T$$

$$L_{\text{Mn,Ti:\square}}^{1,\text{cbcc-}A12} = -3635 - 5 \ T$$

**Phase cub-*A*13**

$$L_{\text{Mn,Ti:\square}}^{0,\text{cub-}A13} = -34000 + 20 \ T$$

**Phase fcc-A1**

$$L_{\text{Mn,Ti:\square}}^{0,\text{fcc}-A1} = -26200 + 20 T$$

**Phase hcp-A3**

$$L_{\text{Mn,Ti:\square}}^{0,\text{hcp}-A3} = 22100$$

**Phase liquid**

$$L_{\text{Mn,Ti}}^{0,\text{liquid}} = -34000 + 21.5 T$$

$$L_{\text{Mn,Ti}}^{1,\text{liquid}} = 1400$$

**Phase Mn<sub>4</sub>Ti**

$$G^\circ(T) - 0.815 H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) - 0.185 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 2445.0 - 2.9 T + 0.815 \text{ GHSER}_{\text{Mn}} + 0.185 \text{ GHSER}_{\text{Ti}}$$

**Phase Mn<sub>3</sub>Ti**

$$G^\circ(T) - 3.0 H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 18552.0 - 9.12 T + 3.0 \text{ GHSER}_{\text{Mn}} + \text{GIISER}_{\text{Ti}}$$

**Phase MnTi- $\alpha$** 

$$G^\circ(T) - H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 11478.0 + \text{GHSER}_{\text{Mn}} + \text{GHSER}_{\text{Ti}}$$

**Phase MnTi- $\beta$** 

$$G^\circ(T) - 0.515 H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) - 0.485 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 5540.0 - 2.29 T + 0.515 \text{ GHSER}_{\text{Mn}} + 0.485 \text{ GHSER}_{\text{Ti}}$$

**Phase Laves-C14**

$$G^\circ(T) - 3.0 H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) = G(\text{Mn:Mn}) = 3000.0 + 3.0 \text{ GIISER}_{\text{Mn}}$$

$$G^\circ(T) - 2.0 H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mn:Ti}) = \\ - 26400.0 + 2.0 \text{ GHSER}_{\text{Mn}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Mn}}^{\circ,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) - 2.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Mn}) = \\ 3000.0 + \text{GIISER}_{\text{Mn}} + 2.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = \\ 15000.0 + 3.0 \text{ GHSER}_{\text{Ti}}$$

$$L_{\text{Mn:Mn,Ti}}^{0,\text{Laves}-C14} = L_{\text{Ti:Mn,Ti}}^{0,\text{Laves}-C14} = 15000$$

$$L_{\text{Mn,Ti:Mn}}^{0,\text{Laves}-C14} = L_{\text{Mn,Ti:Ti}}^{0,\text{Laves}-C14} = 27000$$

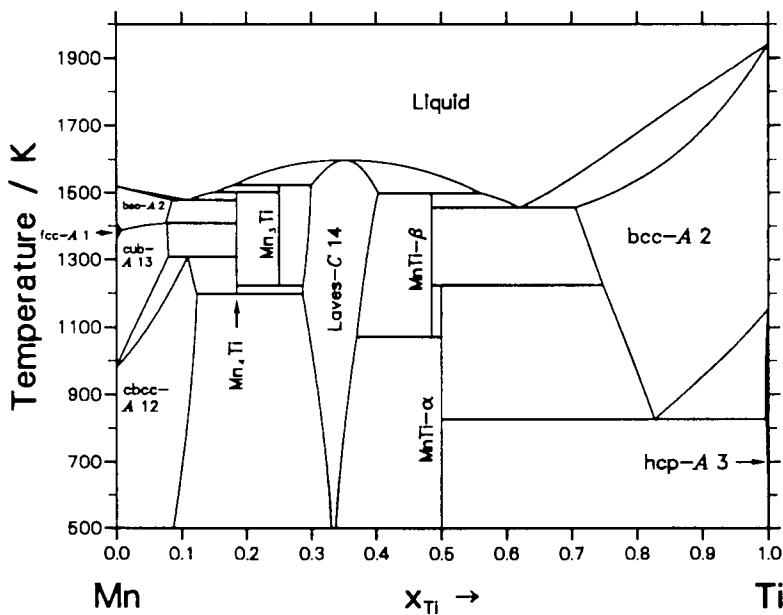


Table I – Invariant Reactions.

Reaction	Type	Compositions \$x_{Ti}\$	\$T / K\$
Liquid \$\rightleftharpoons\$ bcc-A2 + Mn <sub>4</sub> Ti	Eutectic	.111 .086 .185	1478.0
Liquid + Mn <sub>3</sub> Ti \$\rightleftharpoons\$ Mn <sub>4</sub> Ti	Peritectic	.153 .250 .185	1502.8
Liquid + Laves-C14 \$\rightleftharpoons\$ Mn <sub>3</sub> Ti	Peritectic	.180 .300 .250	1523.5
Mn <sub>3</sub> Ti \$\rightleftharpoons\$ Mn <sub>4</sub> Ti + Laves-C14	Eutectoid	.250 .185 .287	1222.3
Mn <sub>4</sub> Ti \$\rightleftharpoons\$ cbcc-A12 + Laves-C14	Eutectoid	.185 .124 .286	1198.4
cbcc-A12 + Mn <sub>4</sub> Ti \$\rightleftharpoons\$ cub-A13	Peritectoid	.080 .185 .110	1309.3
bcc-A2 + Mn <sub>4</sub> Ti \$\rightleftharpoons\$ cub-A13	Peritectoid	.076 .185 .078	1408.6
bcc-A2 \$\rightleftharpoons\$ fcc-A1 + cub-A13	Eutectoid	.008 .005 .009	1387.6
Laves-C14 \$\rightleftharpoons\$ Liquid	Congruent	.344 .344 ....	1598.0
Liquid + Laves-C14 \$\rightleftharpoons\$ MnTi-\$\beta\$	Peritectic	.560 .485 .403	1500.2
MnTi-\$\beta\$ \$\rightleftharpoons\$ Laves-C14 + MnTi-\$\alpha\$	Eutectoid	.485 .369 .500	1071.3
MnTi-\$\beta\$ + bcc-A2 \$\rightleftharpoons\$ MnTi-\$\alpha\$	Peritectoid	.485 .748 .500	1224.0
bcc-A2 \$\rightleftharpoons\$ MnTi-\$\alpha\$ + hcp-A3	Eutectoid	.827 .500 .996	827.6
Liquid \$\rightleftharpoons\$ MnTi-\$\beta\$ + bcc-A2	Eutectic	.620 .485 .706	1455.5

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Group	Sub-lattice	Comments
Mn-Ti	$\alpha$ -Mn	$\alpha$ -Mn	$c584$ $I43m$		cbcc- <i>A</i> 12
	$\beta$ -Mn	$\beta$ -Mn	$cP20$ $P4_1323m$		cub- <i>A</i> 13
	$\gamma$ -Mn	Cu	$cF4$ $Fm3m$	M 4	fcc- <i>A</i> 1
	$\delta$ -Mn	W	$cI2$ $Im\bar{3}m$	M 2	bcc- <i>A</i> 2
	(Ti)	Mg	$hP2$ $P6_3/mmc$	M 2	
	(Ti)	W	$cI2$ $Im\bar{3}m$	M 2	
	MnTi- $\alpha$		$t \star 58$		
	MnTi- $\beta$				
	Mn <sub>3</sub> Ti				
	Mn <sub>2</sub> Ti	MgZn <sub>2</sub>	$hP12$ $P6_3/mmc$	Mn <sub>1</sub> 2 Mn <sub>2</sub> 6 Ti 4	Laves- <i>C</i> 14
	Mn <sub>4</sub> Ti	$\sim \delta$ (Mo,Ni)	$hR53$ $R\bar{3}$		

# System Mn-Zr

**Solution Phases:**

Liquid, bcc-*A*2, cbcc-*A*12, cub-*A*13, fcc-*A*1, hcp-*A*3

**Compound:**

Mn<sub>2</sub>Zr

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
cbcc- <i>A</i> 12	:	Substitutional, Redlich-Kister
cub- <i>A</i> 13	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Mn <sub>2</sub> Zr	:	Stoichiometric, (Mn) <sub>2</sub> (Zr)

**Assessor and Date:**

K. Hack, GTT, Germany (1997).

## Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)

### Phase Mn<sub>2</sub>Zr

$$G^\circ(T) - 3.0 \ H_{\text{Mn}}^{\circ, \text{cbcc}-\text{A}12, \text{para}}(298.15 \text{ K}) = G(\text{Mn: Mn}) = \\ 298.15 < T < 1519.00 : -021345.84 + 390.177 \ T - 70.3746 \ T \cdot \ln T \\ - 0.02204304 \ T^2 + 209481.3 \ T^{-1}$$

$$1519.00 < T < 2000.00 : -83200.23 + 936.7944 \ T - 144 \ T \cdot \ln T \\ + 4.970541E+30 \ T^{-9}$$

$$G^\circ(T) - 2.0 \ H_{\text{Mn}}^{\circ, \text{cbcc}-\text{A}12, \text{para}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) = G(\text{Mn: Zr}) = \\ 298.15 < T < 1900.00 : -79282.375 + 386.94271 \ T - 71.0782 \ T \cdot \ln T \\ - 0.01907327 \ T^2 + 174625.2 \ T^{-1}$$

$$1900.00 < T < 2000.00 : -119446.65 + 750.75589 \ T - 120.1618 \ T \cdot \ln T \\ - 0.00437791 \ T^2 + 34971 \ T^{-1} \\ + 3.313694E+30 \ T^{-9}$$

$$G^\circ(T) - H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) - 2.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Zr:Mn}) = \\ 298.15 < T < 1519.00 : - 8770.8146 + 381.3571 T - 71.7818 T \cdot \ln T \\ - 0.0161035 T^2 + 139769.1 T^{-1}$$

$$1519.00 < T < 2000.00 : - 29388.945 + 563.56289 T - 96.3236 T \cdot \ln T \\ - 0.00875582 T^2 + 69942 T^{-1} \\ + 1.656847E+30 T^{-9}$$

$$G^\circ(T) - 3.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Zr:Zr}) = \\ 298.15 < T < 2128.00 : - 8482.785 + 376.94715 T - 72.4854 T \cdot \ln T \\ - 0.01313373 T^2 + 104913 T^{-1} \\ 2128.00 < T < 6000.00 : - 63257.763 + 788.17255 T - 126.432 T \cdot \ln T \\ - 4.028685E+31 T^{-9}$$

$$L_{\text{Mn},\text{Zr:Mn}}^{0,\text{Mn}_2\text{Zr}} = 18442.56 + 14.090471 T$$

$$L_{\text{Zr},\text{Mn},\text{Zr}}^{0,\text{Mn}_2\text{Zr}} = 18442.56 + 14.090471 T$$

$$L_{\text{Mn},\text{Mn},\text{Zr}}^{0,\text{Mn}_2\text{Zr}} = 1066.4675 + 10.504933 T$$

$$L_{\text{Mn},\text{Zr:Zr}}^{0,\text{Mn}_2\text{Zr}} = 1066.4675 + 10.504933 T$$

#### Phase bcc-A2

$$L_{\text{Mn},\text{Zr:}\square}^{0,\text{bcc}-A2} = - 2135.3475 - 0.13258 T$$

$$L_{\text{Mn},\text{Zr:}\square}^{1,\text{bcc}-A2} = - 4084$$

#### Phase cbcc-A12

$$L_{\text{Mn},\text{Zr:}\square}^{0,\text{cbcc}-A12} = 20000$$

#### Phase cub-A13

$$L_{\text{Mn},\text{Zr:}\square}^{0,\text{cub}-A13} = 24000$$

#### Phase fcc-A1

$$L_{\text{Mn},\text{Zr:}\square}^{0,\text{fcc}-A1} = 20000$$

#### Phase hcp-A3

$$L_{\text{Mn},\text{Zr:}\square}^{0,\text{hcp}-A3} = 25000$$

#### Phase liquid

$$L_{\text{Mn},\text{Zr}}^{0,\text{liquid}} = - 35187.553 + 2.6983563 T$$

$$L_{\text{Mn},\text{Zr}}^{1,\text{liquid}} = - 1305.986$$

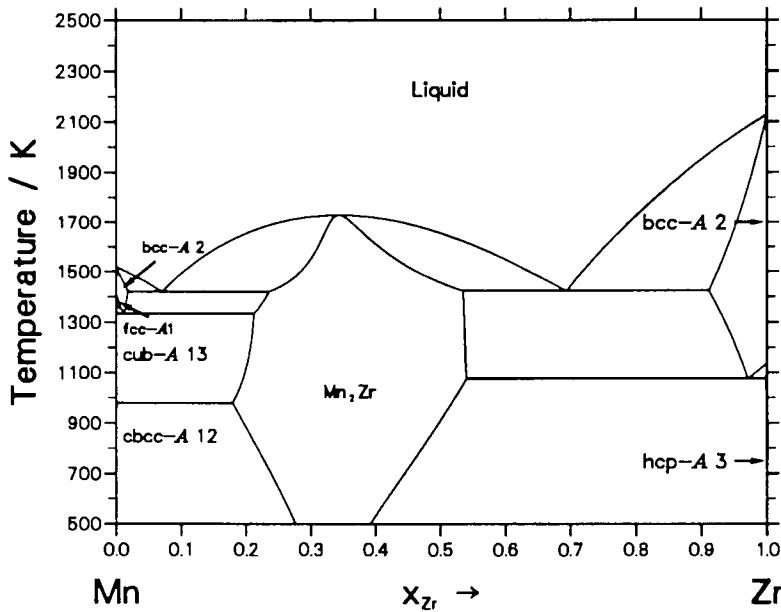


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Zr}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ bcc-A2 + Mn <sub>2</sub> Zr	Eutectic	.071	.018	.236	1421.9
bcc-A2 $\rightleftharpoons$ + cub-A13 + Mn <sub>2</sub> Zr	Eutectoid	.012	.000	.213	1334.5
fcc-A1 $\rightleftharpoons$ bcc-A2 + cub-A13	Metaeutectic	.0003	.0002	.0062	1359.1
cub-A13 $\rightleftharpoons$ cbcc-A12 + Mn <sub>2</sub> Zr	Degenerate	.000	.000	.179	980.1
Liquid $\rightleftharpoons$ Mn <sub>2</sub> Zr + bcc-A2	Eutectic	.694	.535	.911	1424.1
bcc-A2 $\rightleftharpoons$ Mn <sub>2</sub> Zr + hcp-A3	Eutectoid	.971	.540	.998	1075.4
Mn <sub>2</sub> Zr $\rightleftharpoons$ Liquid	Congruent	.345	.345	.....	1730.0

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
<b>Mn-Zr</b>	$\alpha$ -Mn	$\alpha$ -Mn	$c58$ $I\bar{4}9m$		cbcc- <i>A12</i>
	$\beta$ -Mn	$\beta$ -Mn	$cP20$ $P\bar{4}_132\bar{3}m$		cub- <i>A13</i>
	$\gamma$ -Mn	Cu	$cF4$ $Fm\bar{3}m$		
	$\delta$ -Mn	W	$cl2$ $I\bar{m}\bar{3}m$		
	(Zr)	Mg	$hP2$ $P6_3/mmc$	M 2	
	(Zr)	W	$cl2$ $I\bar{m}\bar{3}m$	M 4	
	$Mn_2Zr$	$MgZn_2$	$hP12$ $P6_3/mmc$	Mn 2 Mn 6 Zr 4	Laves- <i>C14</i>

# System Mo-Ti

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, hcp- <i>A</i> 3
(metastable)	bcc- <i>B</i> 2, fcc- <i>A</i> 1

**Compounds:**

(metastable)	AlM- <i>D</i> 0 <sub>19</sub> , AlM- <i>D</i> 0 <sub>22</sub> , AlTi- <i>L</i> 1 <sub>0</sub>
--------------	---

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
bcc- <i>B</i> 2	:	Sublattice model, (Mo,Ti) <sub>0.5</sub> (Mo,Ti) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc- <i>A</i> 2 ⇌ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Mo,Ti)(Mo,Ti) <sub>3</sub>
AlM- <i>D</i> 0 <sub>22</sub>	:	Sublattice model, (Mo,Ti) <sub>3</sub> (Mo,Ti)
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Mo,Ti)(Mo,Ti)

**Assessor and Date:**

N. Saunders, 1995

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase liquid**

$$\nu_{\text{Mo,Ti}}^{0,\text{liquid}} = -9000 + 2T$$

**Phase fcc-*A*1**

$$\nu_{\text{Mo,Ti:}\square}^{0,\text{fcc-}\mathcal{A}1} = 16500$$

**Phase hcp-A3**

$$L_{\text{Mo,Ti:\square}}^{0,\text{hcp}-A3} = 22760 - 6 \cdot T$$

**Phase bcc-A2**

$$L_{\text{Mo,Ti:\square}}^{0,\text{bcc}-A2} = 2000$$

$$L_{\text{Mo,Ti:\square}}^{1,\text{bcc}-A2} = -2000$$

**Phase bcc-B2**

$$\begin{aligned} G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Mo:Mo}) = 0.0 \\ G^\circ(T) - 0.5 \cdot H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 \cdot H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Mo:Ti}) = \\ &\quad 5000 \\ G^\circ(T) - 0.5 \cdot H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 \cdot H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Mo}) = \\ &\quad 5000 \\ G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ti}) = \\ &\quad 0 \\ L_{\text{Mo,Ti:Mo:\square}}^{0,\text{bcc}-B2} &= L_{\text{Mo,Ti:Ti:\square}}^{0,\text{bcc}-B2} = -5000 \\ L_{\text{Mo:Mo,Ti:\square}}^{0,\text{bcc}-B2} &= L_{\text{Ti:Mo,Ti:\square}}^{0,\text{bcc}-B2} = -5000 \end{aligned}$$

**Phase bcc-B2**

$$G_{\text{Mo,Ti:\square}}^* = 5000$$

$$G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Mo:\square}) = 0.0$$

$$G^\circ(T) - 0.5 \cdot H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 \cdot H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mo:Ti:\square}) = 2.0 \cdot G_{\text{Mo,Ti:\square}}^*$$

$$G^\circ(T) - 0.5 \cdot H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 \cdot H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Mo:\square}) = 2.0 \cdot G_{\text{Mo,Ti:\square}}^*$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti:\square}) = 0.0$$

**Phase bcc-A2**

$$L_{\text{Mo,Ti:\square}}^{0,\text{bcc}-A2} = 2000$$

$$L_{\text{Mo,Ti:\square}}^{1,\text{bcc}-A2} = -2000$$

**Phase AlM-D0<sub>19</sub>**

$$\begin{aligned}
 G^\circ(T) - 4.0 & H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Mo}) = 4.0 \text{ GHCP}_{\text{Mo}} \\
 G^\circ(T) - 3.0 & H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mo:Ti}) = \\
 & 17072 - 4.5 T + 3.0 \text{ GHCP}_{\text{Mo}} + \text{GHSER}_{\text{Ti}} \\
 G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 3.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Mo}) = \\
 & 17072 - 4.5 T + \text{GHCP}_{\text{Mo}} + 3.0 \text{ GHSER}_{\text{Ti}} \\
 G^\circ(T) - 4.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 4.0 + 4.0 \text{ GHSER}_{\text{Ti}}
 \end{aligned}$$

**Phase AlM-D0<sub>22</sub>**

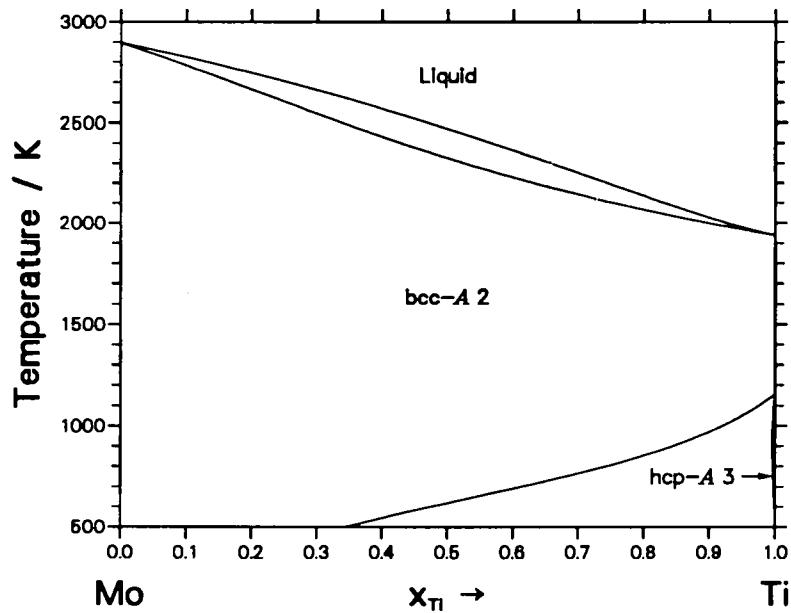
$$\begin{aligned}
 G^\circ(T) - 4.0 & H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Mo}) = 4.0 \text{ GFCC}_{\text{Mo}} \\
 G^\circ(T) - 3.0 & H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mo:Ti}) = \\
 & 3.0 \text{ GFCC}_{\text{Mo}} + \text{GFCC}_{\text{Ti}} \\
 G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 3.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Mo}) = \\
 & \text{GFCC}_{\text{Mo}} + 3.0 \text{ GFCC}_{\text{Ti}} \\
 G^\circ(T) - 4.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 4.0 \text{ GFCC}_{\text{Ti}}
 \end{aligned}$$

**Phase AlTi-L1<sub>0</sub>**

$$\begin{aligned}
 G^\circ(T) - 2.0 & H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Mo:Mo}) = 2.0 \text{ GFCC}_{\text{Mo}} \\
 G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mo:Ti}) = \\
 & 8250 + \text{GFCC}_{\text{Mo}} + \text{GFCC}_{\text{Ti}} \\
 G^\circ(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Mo}) = \\
 & 8250 + \text{GFCC}_{\text{Mo}} + \text{GFCC}_{\text{Ti}} \\
 G^\circ(T) - 2.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 2.0 \text{ GFCC}_{\text{Ti}} \\
 L_{\text{Mo,Ti:Mo}}^{0,\text{AlTi}-L1_0} & = L_{\text{Mo:Mo,Ti}}^{0,\text{AlTi}-L1_0} = 8250 \\
 L_{\text{Mo,Ti:Ti}}^{0,\text{AlTi}-L1_0} & = L_{\text{Ti:Mo,Ti}}^{0,\text{AlTi}-L1_0} = 8250
 \end{aligned}$$

**Table I – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Group	Comments
Mo-Ti	(Mo)	W	<i>cI2</i> <i>Im3m</i>	
	(Ti)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	
	(Ti)	W	<i>cI2</i> <i>Im3m</i>	



# System N-Ti

**Solution Phases:**

Liquid, hcp-A3, bcc-A2, fcc-A1 ( $Ti_xN_{1-x}$ )

**Compound:**

$Ti_2N$ ,  $Ti_3N_2$ ,  $Ti_4N_3$

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Sub-lattice, $(Ti)(N,\square)$
hcp-A3	:	Sub-lattice, $(Ti)(N,\square)$
fcc-A1	:	Sub-lattice, $(Ti)(N,\square)$
$Ti_2N$	:	Stoichiometric, $(Ti)_2(N)$
$Ti_3N_2$	:	Stoichiometric, $(Ti)_{0.29}(N)_{0.71}$
$Ti_4N_3$	:	Stoichiometric, $(Ti)_{0.315}(N)_{0.685}$

**Assessor and Date:**

K. Zeng and R. Schmid-Fetzer, Univ. Clausthal,  
Germany, 1997

**Comments:**

The value of  $GHSER_{TiN}$  is taken from S. Jonsson,  
Thesis, Royal Institute of Technology, Stockholm,  
Sweden (1993)

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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

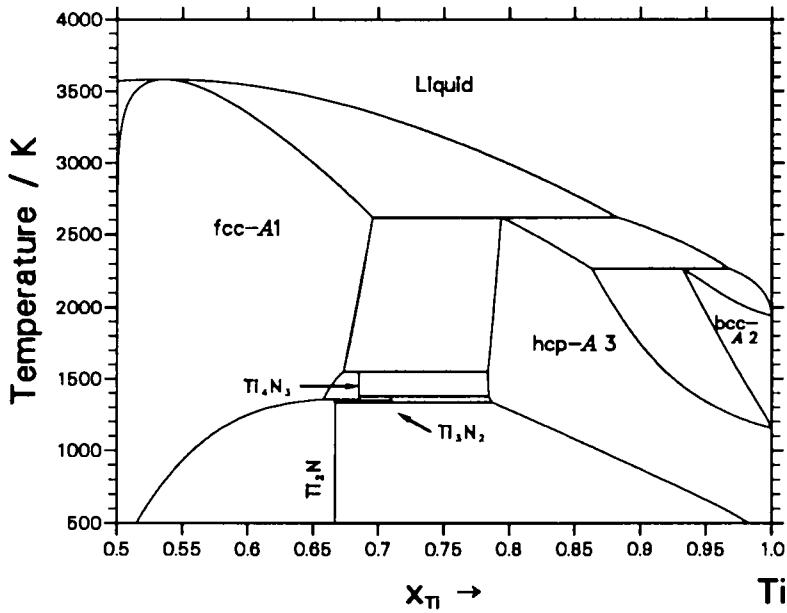
**Phase fcc-A1**

$$\begin{aligned}
 G^\circ(T) - H_{0.5N_2}^{\circ,gas}(298.15\text{ K}) - H_{Ti}^{\circ,hcp-A3}(298.15\text{ K}) &= GHSER_{TiN} = \\
 &- 357905.0 + 330.498 T - 52.4587 T \cdot \ln T - 9.28E-04 T^2 \\
 &- 2.41E+09 T^{-3} + 871000.0 T^{-1} \\
 L_{Ti:\square}^{0,fcc-A1} &= - 42704.41
 \end{aligned}$$

$$L_{Ti:\square}^{1,fcc-A1} = - 13989.34$$

**Phase  $Ti_4N_3$**

$$\begin{aligned}
 G^\circ(T) - 0.315 H_{0.5N_2}^{\circ,gas}(298.15\text{ K}) - 0.685 H_{Ti}^{\circ,hcp-A3}(298.15\text{ K}) &= \\
 &- 5956.8633 - 3.2749 T + 0.37 GHSER_{Ti} + 0.315 GHSER_{TiN}
 \end{aligned}$$



### Phase bcc-A2

$$\begin{aligned}
 G^\circ(T) - 3.0 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:N}) = \\
 2604201.62 + 118.04 T + \text{GHSER}_{\text{Ti:N}} + 2.0 \text{ GHSER}_N \\
 L_{\text{Ti:N},\square}^{0,\text{bcc}-A2} = -3215338.17
 \end{aligned}$$

### Phase hcp-A3

$$\begin{aligned}
 G^\circ(T) - 0.5 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:N}) = \\
 -6046.53 - 2.653 T + 0.5 \text{ GHSER}_{\text{Ti:N}} + 0.5 \text{ GHSER}_{\text{Ti}} \\
 L_{\text{Ti:N},\square}^{0,\text{hcp}-A3} = -13501
 \end{aligned}$$

### Phase Ti<sub>2</sub>N

$$\begin{aligned}
 G^\circ(T) - H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) - 2.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\
 -67116 + 26.5395533 T + \text{GHSER}_{\text{Ti}} + \text{GHSER}_{\text{Ti:N}}
 \end{aligned}$$

### Phase Ti<sub>3</sub>N<sub>2</sub>

$$\begin{aligned}
 G^\circ(T) - 0.29 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) - 0.71 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\
 -8190.34 - 1.54816 T + 0.42 \text{ GHSER}_{\text{Ti}} + 0.29 \text{ GHSER}_{\text{Ti:N}}
 \end{aligned}$$

**Phase liquid**

$$L_{N,Ti}^{0,\text{liquid}} = -376354.145$$

$$L_{N,Ti}^{1,\text{liquid}} = -98242.2945$$

**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{Ti}$			$T / K$
$fcc\text{-}A1 + hcp\text{-}A3 \rightleftharpoons Ti_4N_3$	Peritectoid	.673	.784	.685	1551.1
$Ti_4N_3 + hcp\text{-}A3 \rightleftharpoons Ti_3N_2$	Peritectoid	.685	.784	.710	1376.8
$Ti_3N_2 \rightleftharpoons Ti_2N + hcp\text{-}A3$	Eutectoid	.710	.667	.787	1336.2
$Ti_4N_3 \rightleftharpoons Ti_2N + Ti_3N_2$	Eutectoid	.685	.667	.710	1348.5
$fcc\text{-}A1^* + Ti_3N_2 \rightleftharpoons Ti_2N$	Peritectoid	.658	.685	.667	1354.8
Liquid + fcc-A1* $\rightleftharpoons$ hcp-A3	Peritectic	.882	.695	.793	2618.0
Liquid + hcp-A3 $\rightleftharpoons$ bcc-A2	Peritectic	.967	.863	.932	2268.6
$fcc\text{-}A1 \rightleftharpoons$ Liquid	Congruent	.533	.541	....	3585.0

\*  $fcc\text{-}A1 \equiv Ti_xN_{1-x}$

**Table II - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattice	Comments
N-Ti	$0.5N_2$	gas			
	(Ti)	Mg	$hP2$ $P6_3/mmc$	M 2	
	(Ti)	W	$cI2$ $I\bar{m}\bar{3}m$	M 2	
	TiN	ClNa	$cF8$ $Fm\bar{3}m$	N 4 Ti 4	modelled as fcc-A1
	Ti <sub>2</sub> N	anti-O <sub>2</sub> Ti (rutile)	$tP6$ $P4_2/mnm$	N 2 Ti 4	
	Ti <sub>4</sub> N <sub>3</sub>	Ti <sub>7</sub> S <sub>12</sub>	$hR8$ $R\bar{3}m$	N <sub>1</sub> 3 N <sub>2</sub> 3 N <sub>3</sub> 6 Ti <sub>1</sub> 6 Ti <sub>2</sub> 6	
	Ti <sub>3</sub> N <sub>2</sub>				not indicated in [91Vil] nor in [90Mas]

## System Nb–Ti

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, hcp- <i>A</i> 3
(metastable)	bcc- <i>B</i> 2, fcc- <i>A</i> 1

**Compounds:**

(metastable)	AlM- <i>D</i> 0 <sub>19</sub> , AlM- <i>D</i> 0 <sub>22</sub> , AlTi- <i>L</i> 1 <sub>0</sub> , Cr <sub>3</sub> Si- <i>A</i> 15
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**Modelling:**

Liquid	:	Substitutional, Redlich–Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich–Kister
bcc- <i>B</i> 2	:	Sublattice model, (Nb,Ti) <sub>0.5</sub> (Nb,Ti) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc- <i>B</i> 2 takes into account the ordering reaction bcc- <i>A</i> 2 ⇌ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
fcc- <i>A</i> 1	:	Substitutional, Redlich–Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich–Kister
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Nb,Ti)(Nb,Ti) <sub>3</sub>
AlM- <i>D</i> 0 <sub>22</sub>	:	Sublattice model, (Ti) <sub>3</sub> (Nb,Ti)
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Nb,Ti)(Nb,Ti)
Cr <sub>3</sub> Si- <i>A</i> 15	:	Sublattice model, (Nb,Ti) <sub>3</sub> (Nb)

**Assessor and Date:**

N. Saunders, 1995

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase liquid**

$$L_{\text{Nb},\text{Ti}}^{0,\text{liquid}} = 8500$$

**Phase fcc-A1**

$$L_{\text{Nb,Ti:\square}}^{0,\text{fcc-A1}} = 13600$$

$$L_{\text{Nb,Ti:\square}}^{1,\text{fcc-A1}} = 1\text{E-}04$$

$$L_{\text{Nb,Ti:\square}}^{2,\text{fcc-A1}} = 2500$$

**Phase hcp-A3**

$$L_{\text{Nb,Ti:\square}}^{0,\text{hcp-A3}} = 13600$$

$$L_{\text{Nb,Ti:\square}}^{1,\text{hcp-A3}} = 1\text{E-}04$$

$$L_{\text{Nb,Ti:\square}}^{2,\text{hcp-A3}} = 2500$$

**Phase Cr<sub>3</sub>Si-A15**

$$\begin{aligned} G^\circ(T) - 4.0 \ H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) &= G(\text{Nb:Nb}) = \\ &20000 + 10 \ T + 4.0 \ \text{GFCC}_{\text{Nb}} \\ G^\circ(T) - H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - 3.0 \ H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) &= G(\text{Ti:Nb}) = \\ &20000 + 10 \ T + 3.0 \ \text{GFCC}_{\text{Nb}} + \text{GFCC}_{\text{Ti}} \end{aligned}$$

**Phase bcc-A2**

$$L_{\text{Nb,Ti:\square}}^{0,\text{bcc-A2}} = 14000$$

$$L_{\text{Nb,Ti:\square}}^{1,\text{bcc-A2}} = 1.0\text{E-}4$$

$$L_{\text{Nb,Ti:\square}}^{2,\text{bcc-A2}} = 2500$$

**Phase bcc-B2**

$$\begin{aligned} G_{\text{Nb,Ti:\square}}^* &= 5500 \\ G^\circ(T) - H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) &= G(\text{Nb:Nb\square}) = 0.0 \\ G^\circ(T) - 0.5 \ H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - 0.5 \ H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) &= \\ &G(\text{Nb:Ti:\square}) = G_{\text{Nb,Ti:\square}}^* \\ G^\circ(T) - 0.5 \ H_{\text{Nb}}^{\circ,\text{bcc-A2}}(298.15 \text{ K}) - 0.5 \ H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) &= \\ &G(\text{Ti:Nb:\square}) = G_{\text{Nb,Ti:\square}}^* \\ G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) &= G(\text{Ti:Ti\square}) = 0.0 \\ L_{\text{Nb,Ti:Nb:\square}}^{0,\text{bcc-B2}} &= L_{\text{Nb,Ti:Ti:\square}}^{0,\text{bcc-B2}} = -5500 \\ L_{\text{Nb:Nb,Ti:\square}}^{0,\text{bcc-B2}} &= L_{\text{Ti:Nb,Ti:\square}}^{0,\text{bcc-B2}} = -5500 \end{aligned}$$

**Phase bcc-B2**

$$G_{\text{Nb}: \text{Ti}: \square}^* = 5500$$

$$G^\circ(T) - H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) = G(\text{Nb:Nb:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Nb:Ti:}\square) = 2.0 \text{ } G_{\text{Nb}: \text{Ti}: \square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Nb:}\square) = 2.0 \text{ } G_{\text{Nb}: \text{Ti}: \square}^*$$

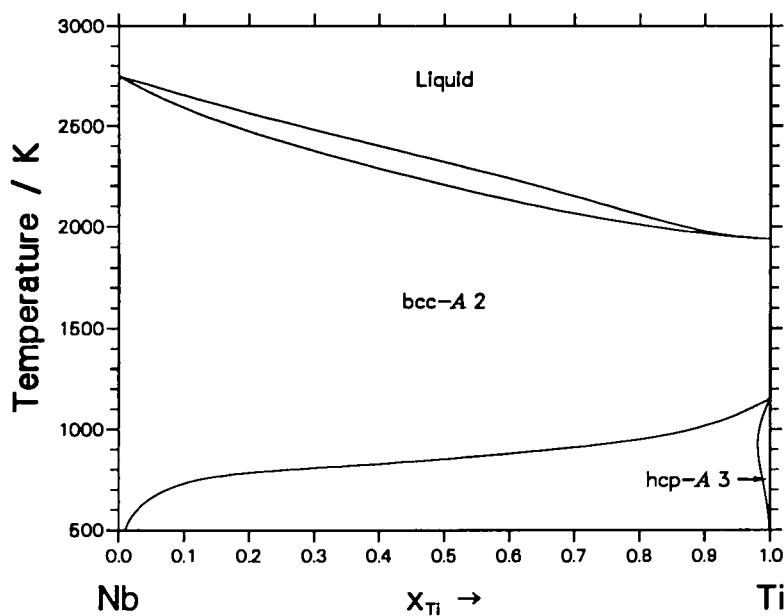
$$G^\circ(T) - H_{\text{Ti}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 0.0$$

**Phase bcc-A2**

$$L_{\text{Nb}, \text{Ti}: \square}^{0, \text{bcc}-A2} = 14000$$

$$L_{\text{Nb}, \text{Ti}: \square}^{1, \text{bcc}-A2} = 1.0E-4$$

$$L_{\text{Nb}, \text{Ti}: \square}^{2, \text{bcc}-A2} = 2500$$



**Phase AlM-D0<sub>19</sub>**

$$G^\circ(T) - 4.0 H_{Nb}^{\circ,bcc-A2}(298.15 \text{ K}) = G(\text{Nb:Nb}) = 4.0 \text{ GHCP}_{Nb}$$

$$G^\circ(T) - 3.0 H_{Nb}^{\circ,bcc-A2}(298.15 \text{ K}) - H_{Ti}^{\circ,hcp-A3}(298.15 \text{ K}) = G(\text{Nb:Ti}) =$$

$$10668 + 3.0 \text{ GHCP}_{Nb} + \text{GHSER}_{Ti}$$

$$G^\circ(T) - H_{Nb}^{\circ,bcc-A2}(298.15 \text{ K}) - 3.0 H_{Ti}^{\circ,hcp-A3}(298.15 \text{ K}) = G(\text{Ti:Nb}) =$$

$$10668 + \text{GHCP}_{Nb} + 3.0 \text{ GHSER}_{Ti}$$

$$G^\circ(T) - 4.0 H_{Ti}^{\circ,hcp-A3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 4.0 + 4.0 \text{ GHSER}_{Ti}$$

$$L_{Nb,Ti:Nb}^{0,AlM-D0_{19}} = 30248$$

$$L_{Nb,Ti:Nb}^{1,AlM-D0_{19}} = 4220$$

$$L_{Nb,Ti:Nb}^{2,AlM-D0_{19}} = 3164$$

$$L_{Nb,Ti:Ti}^{0,AlM-D0_{19}} = 30248$$

$$L_{Nb,Ti:Ti}^{1,AlM-D0_{19}} = -4220$$

$$L_{Nb,Ti:Ti}^{2,AlM-D0_{19}} = 3164$$

$$L_{Nb:Nb,Ti}^{0,AlM-D0_{19}} = 4924$$

$$L_{Nb:Nb,Ti}^{1,AlM-D0_{19}} = 468$$

$$L_{Nb:Nb,Ti}^{2,AlM-D0_{19}} = 40$$

$$L_{Ti:Nb,Ti}^{0,AlM-D0_{19}} = 4924$$

$$L_{Ti:Nb,Ti}^{1,AlM-D0_{19}} = -468$$

$$L_{Ti:Nb,Ti}^{2,AlM-D0_{19}} = 40$$

**Phase AlM-D0<sub>22</sub>**

$$G^\circ(T) - H_{Nb}^{\circ,bcc-A2}(298.15 \text{ K}) - 3.0 H_{Ti}^{\circ,hcp-A3}(298.15 \text{ K}) = G(\text{Ti:Nb}) =$$

$$\text{GFCC}_{Nb} + 3.0 \text{ GFCC}_{Ti}$$

$$G^\circ(T) - 4.0 H_{Ti}^{\circ,hcp-A3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = 4.0 \text{ GFCC}_{Ti}$$

**Phase AlTi-L1<sub>0</sub>**

$$G^\circ(T) - 2.0 H_{Nb}^{\circ,bcc-A2}(298.15 \text{ K}) = G(\text{Nb:Nb}) = 2.0 \text{ GFCC}_{Nb}$$

$$G^\circ(T) - H_{Nb}^{\circ,bcc-A2}(298.15 \text{ K}) - H_{Ti}^{\circ,hcp-A3}(298.15 \text{ K}) = G(\text{Nb:Ti}) =$$

$$13600 + \text{GFCC}_{Nb} + \text{GFCC}_{Ti}$$

$$\begin{aligned}
 G^\circ(T) - H_{\text{Nb}}^{\text{o}, \text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\text{o}, \text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Nb}) = \\
 &\quad 6800 + \text{GFCC}_{\text{Nb}} + \text{GFCC}_{\text{Ti}} \\
 G^\circ(T) - 2.0 \quad H_{\text{Ti}}^{\text{o}, \text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ti}) = 2.0 \quad \text{GFCC}_{\text{Ti}} \\
 L_{\text{Nb}, \text{Ti:Nb}}^{0, \text{AlTi}-L1_0} &= 7738 \\
 L_{\text{Nb}, \text{Ti:Nb}}^{1, \text{AlTi}-L1_0} &= 1250 \\
 L_{\text{Nb}, \text{Ti:Nb}}^{2, \text{AlTi}-L1_0} &= 312 \\
 L_{\text{Nb}, \text{Ti:Ti}}^{0, \text{AlTi}-L1_0} &= 7738 \\
 L_{\text{Nb}, \text{Ti:Ti}}^{1, \text{AlTi}-L1_0} &= -1250 \\
 L_{\text{Nb}, \text{Ti:Ti}}^{2, \text{AlTi}-L1_0} &= 312 \\
 L_{\text{Nb:Nb}, \text{Ti}}^{0, \text{AlTi}-L1_0} &= 7738 \\
 L_{\text{Nb:Nb}, \text{Ti}}^{1, \text{AlTi}-L1_0} &= 1250 \\
 L_{\text{Nb:Nb}, \text{Ti}}^{2, \text{AlTi}-L1_0} &= 312 \\
 L_{\text{Ti:Nb}, \text{Ti}}^{0, \text{AlTi}-L1_0} &= 7738 \\
 L_{\text{Ti:Nb}, \text{Ti}}^{1, \text{AlTi}-L1_0} &= -1250 \\
 L_{\text{Ti:Nb}, \text{Ti}}^{2, \text{AlTi}-L1_0} &= 312 \\
 L_{\text{Nb}, \text{Ti:Nb}, \text{Ti}}^{0, \text{AlTi}-L1_0} &= -7500
 \end{aligned}$$

Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Comments
Nb-Ti	(Nb)	W	<i>cI2</i> <i>I</i> <i>m</i> <i>3m</i>	
	(Ti)	Mg	<i>hP2</i> <i>P</i> <i>6</i> <sub>3</sub> / <i>mmc</i>	
	(Ti)	W	<i>cI2</i> <i>I</i> <i>m</i> <i>3m</i>	

# System Ni-V

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1,  $\sigma$

**Compounds:**

Ni<sub>2</sub>V, Ni<sub>3</sub>V, Ni<sub>2</sub>V<sub>7</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
Ni <sub>2</sub> V	:	Stoichiometric, (Ni) <sub>2</sub> (V)
Ni <sub>3</sub> V	:	Stoichiometric, (Ni) <sub>3</sub> (V)
Ni <sub>2</sub> V <sub>7</sub>	:	Stoichiometric, (Ni) <sub>2</sub> (V) <sub>7</sub>
$\sigma$	:	Sublattice model, (Ni) <sub>8</sub> (V) <sub>4</sub> (Ni,V) <sub>18</sub>

**Publication:**

J. Korb, and K. Hack, GTT, Germany (1997).

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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**


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**Phase bcc-*A*2**

$$L_{\text{Ni},\text{V};\square}^{0,\text{bcc-}A2} = -30513.8 + 12.6138 \ T$$

**Phase fcc-*A*1**

$$L_{\text{Ni},\text{V};\square}^{0,\text{fcc-}A1} = -36365.6 + 3.75677 \ T$$

$$L_{\text{Ni},\text{V};\square}^{1,\text{fcc-}A1} = 11860.7 - 9.0302 \ T$$

$$L_{\text{Ni},\text{V};\square}^{2,\text{fcc-}A1} = -10617.5 + 7.00954 \ T$$

**Phase liquid**

$$L_{\text{Ni},\text{V}}^{0,\text{liquid}} = -51927 + 14.99 \ T$$

**Phase Ni<sub>2</sub>V**

$$G^\circ(T) - 2.0 \ H_{\text{Ni}}^{\text{o,fcc-A1,para}}(298.15 \text{ K}) - H_{\text{V}}^{\text{o,bcc-A2}}(298.15 \text{ K}) = \\ - 38032.065 + 337.2614 \ T - 64.6973 \ T \cdot \ln T - 0.01512 \ T^2 \\ - 13.75326 \ T^{-1}$$

**Phase Ni<sub>3</sub>V**

$$G^\circ(T) - 3.0 \ H_{\text{Ni}}^{\text{o,fcc-A1,para}}(298.15 \text{ K}) - H_{\text{V}}^{\text{o,bcc-A2}}(298.15 \text{ K}) = \\ - 45524.96 + 529.01852 \ T - 99.74166 \ T \cdot \ln T - 0.00824 \ T^2 \\ - 13753.332 \ T^{-1}$$

**Phase Ni<sub>2</sub>V<sub>7</sub>**

$$G^\circ(T) - 2.0 \ H_{\text{Ni}}^{\text{o,fcc-A1,para}}(298.15 \text{ K}) - 7.0 \ H_{\text{V}}^{\text{o,bcc-A2}}(298.15 \text{ K}) = \\ - 190634.14 + 1333.90548 \ T - 233.55668 \ T \cdot \ln T - 0.00482 \ T^2 \\ - 5.196308E-06 \ T^3 + 844557.21 \ T^{-1}$$

**Phase σ**

$$G^\circ(T) - 26.0 \ H_{\text{Ni}}^{\text{o,fcc-A1,para}}(298.15 \text{ K}) - 4.0 \ H_{\text{V}}^{\text{o,bcc-A2}}(298.15 \text{ K}) = G(\text{Ni:V:Ni}) = \\ 298.15 < T < 790.00 : - 161645.05 + 3532.8443 \ T - 671.032 \ T \cdot \ln T \\ - 0.1382502 \ T^2 + 4.87E-07 \ T^3 + 277840 \ T^{-1} \\ 790.00 < T < 1728.00 : - 161794.7 + 3572.6245 \ T - 678.096 \ T \cdot \ln T \\ - 0.1256082 \ T^2 - 2.72E-06 \ T^3$$

$$G^\circ(T) - 8.0 \ H_{\text{Ni}}^{\text{o,fcc-A1,para}}(298.15 \text{ K}) - 22.0 \ H_{\text{V}}^{\text{o,bcc-A2}}(298.15 \text{ K}) = G(\text{Ni:V:V}) = \\ 298.15 < T < 790.00 : - 663330.65 + 4012.7719 \ T - 707.716 \ T \cdot \ln T \\ - 0.1068816 \ T^2 + 2.6785E-06 \ T^3 + 1528120 \ T^{-1} \\ 790.00 < T < 1728.00 : - 664153.72 + 4231.5628 \ T - 746.568 \ T \cdot \ln T \\ - 0.0373506 \ T^2 - 1.496E-05 \ T^3$$

**Table I – Invariant Reactions.**

Reaction	Type	Compositions $\pi_{\text{Zr}}$			$T / \text{K}$
Liquid + bcc-A2 $\rightleftharpoons$ σ	Peritectic	.626	.769	.662	1552.3
σ + bcc-A2 $\rightleftharpoons$ Ni <sub>2</sub> V <sub>7</sub>	Peritectoid	.727	.922	.778	1171.9
Liquid $\rightleftharpoons$ fcc-A1 + σ	Eutectic	.501	.443	.578	1485.7
fcc-A1 $\rightleftharpoons$ Ni <sub>2</sub> V + σ	Eutectoid	.368	.333	.554	1150.9
fcc-A1 $\rightleftharpoons$ Ni <sub>3</sub> V + Ni <sub>2</sub> V	Eutectoid	.313	.250	.333	1175.5
Ni <sub>3</sub> V $\rightleftharpoons$ fcc-A1	Congruent	.250	.250	....	1324.0
Ni <sub>2</sub> V $\rightleftharpoons$ fcc-A1	Congruent	.333	.333	....	1190.0

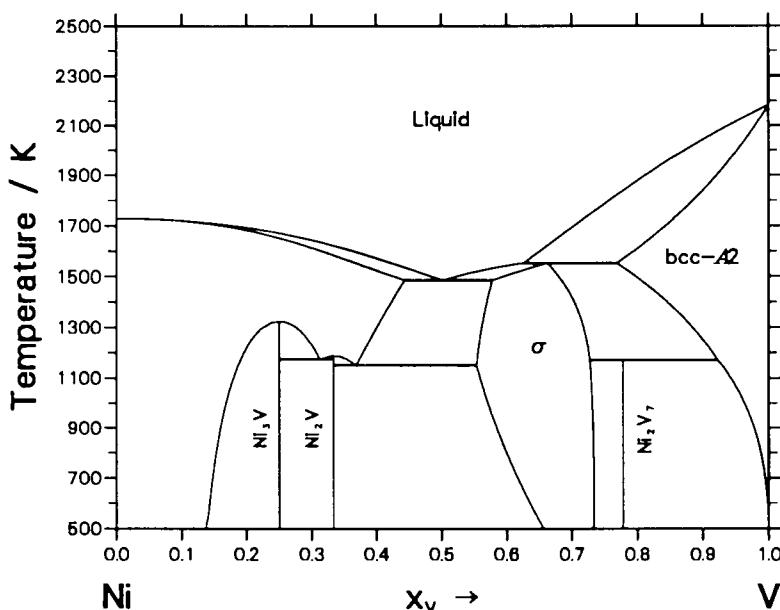


Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Ni-V	(Ni)	Cu	$cF_4$ $Fm\bar{3}m$	M 4	High and low forms given in [90Mas] assumed to be $\text{Ni}_2\text{V}_7$ by the assessors
	(V)	W	$cI2$ $Im\bar{3}m$		
	$\text{Ni}_8\text{V}$	$\text{NbNi}_8$	$tI18$		
	$\text{Ni}_3\text{V}$	$\text{Al}_3\text{Ti}$	$tI8$ $I4/mmm$	$\text{Ni}_1$ 2 $\text{Ni}_2$ 4 V 2	
	$\text{Ni}_2\text{V}$	$\text{MoPt}_2$	$oI6$ $tP30$		
	$\sigma$	$\sigma$ CrFe	$P4_2/mnm$		
	$\text{NiV}_3$	$\text{Cr}_3\text{Si}$	$cP8$ $Pm\bar{3}n$	$\text{Cr}$ 6 $\text{Si}$ 2	

## System Si–Sn

### Solution Phases:

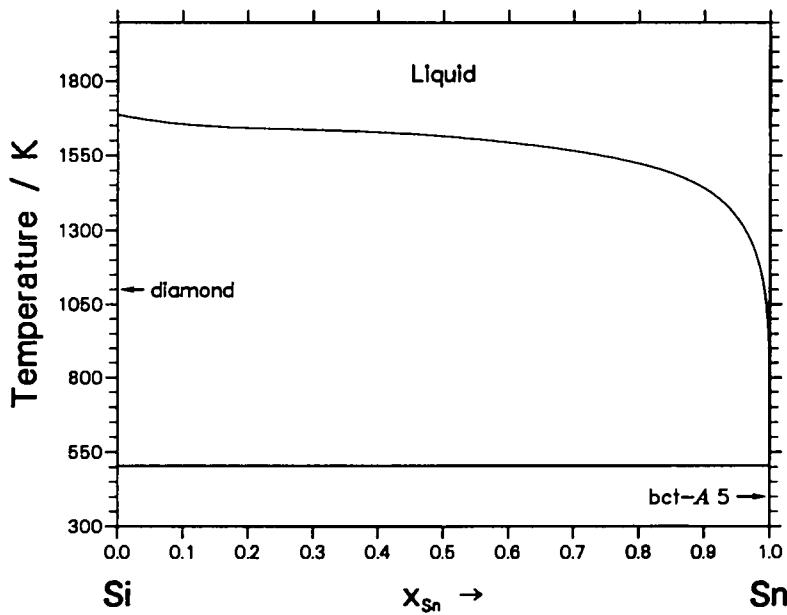
Liquid, diamond

### Modelling:

Liquid : Substitutional, Redlich–Kister  
diamond : Substitutional, Redlich–Kister

### Assessor and Date:

H.L. Lukas 1993



Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**Phase diamond**

$$L_{\text{Si},\text{Sn}}^{\text{0,diamond}} = 25265.65 + 23.84 \ T$$

**Phase liquid**

$$L_{\text{Si},\text{Sn}}^{\text{0,liquid}} = 25364.6$$

$$L_{\text{Si},\text{Sn}}^{\text{1,liquid}} = 3148.8$$

$$L_{\text{Si},\text{Sn}}^{\text{2,liquid}} = 4460.9$$

**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Sn}}$	$T / \text{K}$
Liquid $\rightleftharpoons$ bct-A5 + diamond	Degenerate	.000 .000 1.000	505.1

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group
Si-Sn	(Si)	diamond	<i>cF8</i> <i>Fd3m</i>
	(Sn)	$\beta$ -Sn	<i>lI4</i> <i>I4<sub>1</sub>/amd</i>

# System Si-Ti

**Solution Phases:**

Liquid, bcc-A2, hcp-A3

**Compounds:**

Si<sub>2</sub>Ti, Si<sub>4</sub>Ti<sub>5</sub>, SiTi, SiTi<sub>3</sub>, Si<sub>3</sub>Ti<sub>5</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Si <sub>2</sub> Ti	:	Stoichiometric (Si) <sub>2</sub> (Ti)
Si <sub>4</sub> Ti <sub>5</sub>	:	Stoichiometric (Si) <sub>4</sub> (Ti) <sub>5</sub>
SiTi	:	Stoichiometric, (Si)(Ti)
SiTi <sub>3</sub>	:	Stoichiometric, (Si)(Ti) <sub>3</sub>
Si <sub>3</sub> Ti <sub>5</sub>	:	Sublattice model, (Si,Ti) <sub>2</sub> (Si,Ti) <sub>3</sub> (Ti) <sub>3</sub>
	:	

**Assessor and Date:**

H. Seifert

**Publication:**

Thesis, Univ. Stuttgart, Germany (1994)

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Si<sub>2</sub>Ti**

$$G^\circ(T) - 2.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 175038.5 + 4.54 \ T + 2.0 \ \text{GHSER}_{\text{Si}} + \text{GHSER}_{\text{Ti}}$$

**Phase Si<sub>4</sub>Ti<sub>5</sub>**

$$G^\circ(T) - 4.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 \ H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 711000.0 + 22.37355 \ T + 4.0 \ \text{GHSER}_{\text{Si}} + 5.0 \ \text{GHSER}_{\text{Ti}}$$

**Phase SiTi**

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 155061.7 + 7.6345 \ T + \text{GHSER}_{\text{Si}} + \text{GHSER}_{\text{Ti}}$$

### Phase $\text{Si}_3\text{Ti}_5$

$$\begin{aligned}
 G^\circ(T) - 5.0 & H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Si}: \text{Si}: \text{Ti}) = \\
 & - 206191.45 + 16.4953 & T + 5.0 & \text{GHSER}_{\text{Si}} + 3.0 & \text{GHSER}_{\text{Ti}} \\
 G^\circ(T) - 3.0 & H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Si}: \text{Ti}) = \\
 & - 583564.31 + 2.68514 & T + 3.0 & \text{GHSER}_{\text{Si}} + 5.0 & \text{GHSER}_{\text{Ti}} \\
 G^\circ(T) - 2.0 & H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 6.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Si}: \text{Ti}: \text{Ti}) = \\
 & 417372.85 + 33.81017 & T + 2.0 & \text{GHSER}_{\text{Si}} + 6.0 & \text{GHSER}_{\text{Ti}} \\
 G^\circ(T) - 8.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Ti}: \text{Ti}) = \\
 & 40000.0 + 20.0 & T + 8.0 & \text{GHSER}_{\text{Ti}} \\
 L_{\text{Si}, \text{Ti}: \text{Si}: \text{Ti}}^{0, \text{Si}_3\text{Ti}_5} & = -500000 + 40.0 & T \\
 L_{\text{Si}, \text{Ti}: \text{Ti}: \text{Ti}}^{0, \text{Si}_3\text{Ti}_5} & = -500000 + 40.0 & T \\
 L_{\text{Si}: \text{Si}, \text{Ti}: \text{Ti}}^{0, \text{Si}_3\text{Ti}_5} & = 43024.29 - 3.44194 & T \\
 L_{\text{Ti}: \text{Si}, \text{Ti}: \text{Ti}}^{0, \text{Si}_3\text{Ti}_5} & = 43024.29 - 3.44194 & T
 \end{aligned}$$

### Phase $\text{SiTi}_3$

$$\begin{aligned}
 G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 & H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\
 & - 200000.0 + 3.19924 & T + \text{GHSER}_{\text{Si}} + 3.0 & \text{GHSER}_{\text{Ti}}
 \end{aligned}$$

### Phase bcc-A2

$$\begin{aligned}
 L_{\text{Si}, \text{Ti}: \square}^{0, \text{bcc}-A2} & = -275629.1 + 42.5094 & T \\
 L_{\text{Si}, \text{Ti}: \square}^{1, \text{bcc}-A2} & = 25025.35 - 2.00203 & T \\
 L_{\text{Si}, \text{Ti}: \square}^{2, \text{bcc}-A2} & = 83940.65 - 6.71526 & T
 \end{aligned}$$

### Phase diamond

$$L_{\text{Si}, \text{Ti}}^{0, \text{diamond}} = 80 & T$$

### Phase hcp-A3

$$\begin{aligned}
 L_{\text{Si}, \text{Ti}: \square}^{0, \text{hcp}-A3} & = -302731.04 + 69.08469 & T \\
 L_{\text{Si}, \text{Ti}: \square}^{1, \text{hcp}-A3} & = 25025.35 - 2.00203 & T \\
 L_{\text{Si}, \text{Ti}: \square}^{2, \text{hcp}-A3} & = 83940.65 - 6.71526 & T
 \end{aligned}$$

## Phase liquid

$$L_{\text{Si,Ti}}^{0,\text{liquid}} = -255852.17 + 21.87411 \cdot T$$

$$L_{\text{Si,Ti}}^{1,\text{liquid}} = 25025.35 - 2.00203 \cdot T$$

$$L_{\text{Si,Ti}}^{2,\text{liquid}} = 83940.65 - 6.71526 \cdot T$$

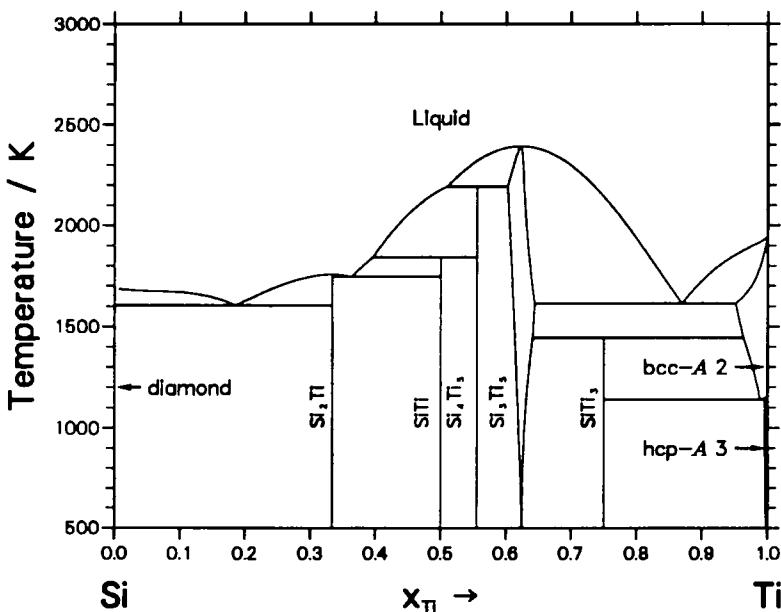


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Ti}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ diamond + $\text{Si}_2\text{Ti}$	Eutectic	.185	.000	.333	1604.3
Liquid $\rightleftharpoons$ $\text{Si}_2\text{Ti}$ + $\text{SiTi}$	Eutectic	.363	.333	.500	1747.4
$\text{Si}_2\text{Ti} \rightleftharpoons$ Liquid	Congruent	.333	.333	....	1757.0
Liquid + $\text{Si}_4\text{Ti}_5 \rightleftharpoons$ $\text{SiTi}$	Peritectic	.396	.556	.500	1842.8
Liquid + $\text{Si}_3\text{Ti}_5 \rightleftharpoons$ $\text{Si}_4\text{Ti}_5$	Peritectic	.509	.602	.555	2192.6
$\text{Si}_3\text{Ti}_5 \rightleftharpoons$ Liquid	Congruent	.625	.625	....	2394.0
Liquid $\rightleftharpoons$ $\text{Si}_3\text{Ti}_5$ + bcc-A2	Eutectic	.869	.644	.951	1613.0
$\text{Si}_3\text{Ti}_5$ + bcc-A2 $\rightleftharpoons$ $\text{SiTi}_3$	Peritectoid	.641	.963	.750	1443.2
bcc-A2 $\rightleftharpoons$ $\text{SiTi}_3$ + hcp-A3	Eutectoid	.988	.750	.995	1139.4

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol Group	Sub-lattices	Comments
Si-Ti	(Si)	diamond	$cF8$ $Fd\bar{3}m$		
	(Ti)	Mg	$hP2$ $P6_3/mmc$		
	(Ti)	W	$cI2$ $Im\bar{3}m$		
	TiSi <sub>2</sub>	TiSi <sub>2</sub>	$oF24$ $Fddd$		
	TiSi	TiSi	$oP8$ $Pmm2$	$Si_1$ $Si_2$ $Ti_1$ $Ti_2$ $Ti_3$ $Ti_4$	2 2 1 1 1 1
	TiSi	FeB	$oP8$ $Pnma$		also given in [90Mas]
	Ti <sub>3</sub> Si	PTi <sub>3</sub>	$tP32$ $P4_2/n$		
	Ti <sub>5</sub> Si <sub>3</sub>	Mn <sub>5</sub> Si <sub>3</sub>	$hP16$ $P6_3/mcm$	$Si$ $Ti_1$ $Ti_2$	6 4 6
	Ti <sub>5</sub> Si <sub>4</sub>	Si <sub>4</sub> Zr <sub>5</sub>	$tP36$ $P4_{12}12$		

# System Si–V

**Solution Phases:**

Liquid, bcc-A2

**Compounds:**

Si<sub>2</sub>V, Si<sub>3</sub>V<sub>5</sub>, Si<sub>5</sub>V<sub>6</sub>, SiV<sub>3</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
SiV <sub>3</sub>	:	Sublattice model, (Si,V)(Si,V) <sub>3</sub>
Si <sub>2</sub> V	:	Stoichiometric (Si) <sub>2</sub> (V)
Si <sub>3</sub> V <sub>5</sub>	:	Stoichiometric (Si) <sub>3</sub> (V) <sub>5</sub>
Si <sub>5</sub> V <sub>6</sub>	:	Stoichiometric (Si) <sub>5</sub> (V) <sub>6</sub>

**Assessor and Date:**

M.H. Rand, and N. Saunders 1994

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Si<sub>2</sub>V**

$$\begin{aligned} G^\circ(T) - 2.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{V}}^{\circ,\text{bcc}-\text{A2}}(298.15 \text{ K}) = \\ - 143160.0 + 401.98 \ T - 67.8 \ T \cdot \ln T - 0.0075 \ T^2 \\ + 330000.0 \ T^{-1} \end{aligned}$$

**Phase Si<sub>3</sub>V<sub>5</sub>**

$$\begin{aligned} G^\circ(T) - 3.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 \ H_{\text{V}}^{\circ,\text{bcc}-\text{A2}}(298.15 \text{ K}) = \\ - 504000.0 + 1259.03 \ T - 211.04 \ T \cdot \ln T - 0.00748 \ T^2 \\ + 1680000.0 \ T^{-1} \end{aligned}$$

**Phase Si<sub>5</sub>V<sub>6</sub>**

$$\begin{aligned} G^\circ(T) - 5.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 6.0 \ H_{\text{V}}^{\circ,\text{bcc}-\text{A2}}(298.15 \text{ K}) = \\ - 641675.0 + 1665.98 \ T - 280.28 \ T \cdot \ln T - 0.013915 \ T^2 \\ + 2310000.0 \ T^{-1} \end{aligned}$$

### Phase **SiV<sub>3</sub>**

$$G^\circ(T) - 4.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Si:Si}) = \\ 208000.0 - 80.0 \ T + 4.0 \ \text{GHSER}_{\text{Si}}$$

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 \ H_{\text{V}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Si:V}) = \\ - 216397.0 + 516.532 \ T - 90.44 \ T \cdot \ln T - 0.008346 \ T^2 \\ + 358000 \ T^{-1}$$

$$G^\circ(T) - 3.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{V}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{V:Si}) = \\ 166000.0 - 60.0 \ T + 3.0 \ \text{GHSER}_{\text{Si}} + \text{GHSER}_{\text{V}}$$

$$G^\circ(T) - 4.0 \ H_{\text{V}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{V:V}) = \\ + 18000.0 + 10.0 \ T + 4.0 \ \text{GHSER}_{\text{V}}$$

$$L_{\text{Si},\text{V:Si}}^{0,\text{SiV}_3} = 9794.5 - 21.8 \ T$$

$$L_{\text{Si},\text{V:V}}^{0,\text{SiV}_3} = 9794.5 - 21.8 \ T$$

$$L_{\text{Si:Si},\text{V}}^{0,\text{SiV}_3} = - 150000$$

$$L_{\text{V:Si},\text{V}}^{0,\text{SiV}_3} = 0.0$$

### Phase **bcc-A2**

$$L_{\text{Si},\text{V:}\square}^{0,\text{bcc}-A2} = - 164505 + 30.1 \ T$$

$$L_{\text{Si},\text{V:}\square}^{1,\text{bcc}-A2} = 37000$$

$$L_{\text{Si},\text{V:}\square}^{2,\text{bcc}-A2} = 20000$$

### Phase liquid

$$L_{\text{Si},\text{V}}^{0,\text{liquid}} = - 180900 + 40 \ T$$

$$L_{\text{Si},\text{V}}^{1,\text{liquid}} = 37000$$

$$L_{\text{Si},\text{V}}^{2,\text{liquid}} = 20000$$

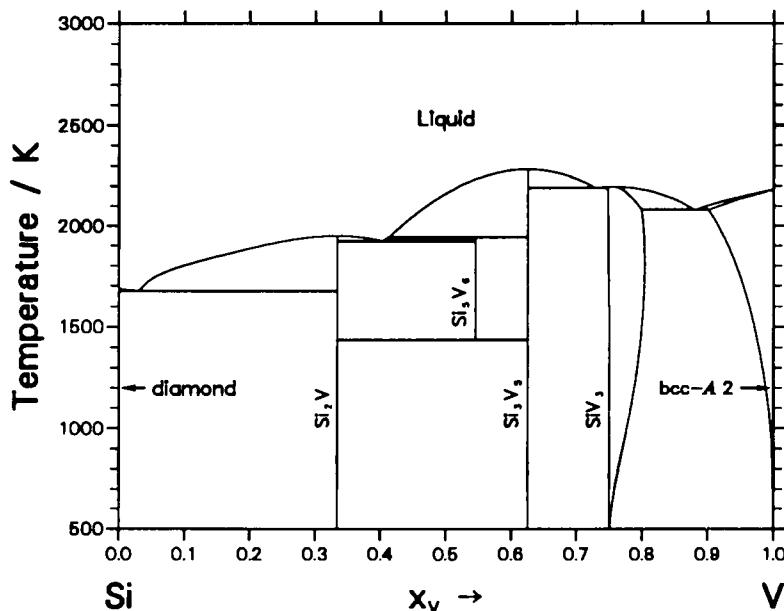


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_V$			$T / K$
$Liquid \rightleftharpoons diamond + Si_2V$	Eutectic	.031	.000	.333	1675.1
$Si_2V \rightleftharpoons Liquid$	Congruent	.333	.333	....	1952.0
$Liquid \rightleftharpoons Si_2V + Si_5V_6$	Eutectic	.403	.333	.545	1923.9
$Liquid + Si_3V_5 \rightleftharpoons Si_5V_6$	Peritectic	.412	.625	.545	1943.1
$Si_3V_5 \rightleftharpoons Liquid$	Congruent	.625	.625	....	2284.0
$Liquid \rightleftharpoons Si_3V_5 + SiV_3$	Eutectic	.727	.625	.748	2190.8
$SiV_3 \rightleftharpoons Liquid$	Congruent	.750	.750	....	2196.0
$Liquid \rightleftharpoons SiV_3 + bcc-A2$	Eutectic	.879	.799	.901	2081.1
$Si_5V_6 \rightleftharpoons Si_2V + Si_3V_5$	Eutectoid	.545	.333	.625	1434.7

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Symbol Group	Sub-lattices	Comments
Si-V	(Si)	diamond	<i>cF8</i> <i>Fd3m</i>	M 8	
	(V)	W	<i>cI2</i> <i>Im3m</i>	M 2	
	Si <sub>3</sub> V <sub>3</sub>	Cr <sub>3</sub> Si	<i>cP8</i> <i>Pm3n</i>	Si 2 V 6	
	Si <sub>2</sub> V	CrSi <sub>2</sub>	<i>hP9</i> <i>P6<sub>2</sub>22</i>	Si 6 V 4	
	Si <sub>3</sub> V <sub>5</sub>	Si <sub>3</sub> W <sub>5</sub>	<i>tI32</i> <i>I4/mcm</i>		
	Si <sub>5</sub> V <sub>6</sub>	Nb <sub>6</sub> Sn <sub>5</sub>	<i>oI44</i> <i>Imm</i>	Si <sub>1</sub> 4 Si <sub>2</sub> 8 Si <sub>3</sub> 8 V <sub>1</sub> 8 V <sub>2</sub> 8 V <sub>3</sub> 8	Ge <sub>5</sub> Ti <sub>6</sub> , <i>Ibam</i> in [91Vil]

# System Si-Y

**Solution Phases:**

Liquid, bcc-A2, hcp-A3

**Compounds:**

Si<sub>2</sub>Y-R, Si<sub>2</sub>Y-H, Si<sub>5</sub>Y<sub>3</sub>-R, Si<sub>5</sub>Y<sub>3</sub>-H, SiY,  
Si<sub>3</sub>Y<sub>5</sub>, Si<sub>4</sub>Y<sub>5</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
Si <sub>2</sub> Y-H	:	Stoichiometric, (Si) <sub>2</sub> (Y)-H
Si <sub>2</sub> Y-R	:	Stoichiometric, (Si) <sub>2</sub> (Y)-R
Si <sub>5</sub> Y <sub>3</sub> -H	:	Stoichiometric (Si) <sub>5</sub> (Y) <sub>3</sub> -H
Si <sub>5</sub> Y <sub>3</sub> -R	:	Stoichiometric (Si) <sub>5</sub> (Y) <sub>3</sub> -R
SiY	:	Stoichiometric, (Si)(Y)
Si <sub>3</sub> Y <sub>5</sub>	:	Stoichiometric, (Si) <sub>3</sub> (Y) <sub>5</sub>
Si <sub>4</sub> Y <sub>5</sub>	:	Stoichiometric, (Si) <sub>4</sub> (Y) <sub>5</sub>

**Assessor and Date:**

H.L. Lukas 1991

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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

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**Phase Si<sub>2</sub>Y-H**

$$G^\circ(T) - 2.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 21463.0 + 28.5 \ T + 2.0 \ \text{GHSER}_{\text{Si}} + \text{GHSER}_Y$$

**Phase Si<sub>2</sub>Y-R**

$$G^\circ(T) - 2.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 219201.0 + 31.5 \ T + 2.0 \ \text{GHSER}_{\text{Si}} + \text{GHSER}_Y$$

**Phase  $\text{Si}_3\text{Y}_5$** 

$$G^\circ(T) - 3.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 \ H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 588000.0 + 76.0 \ T + 3.0 \ \text{GHSER}_{\text{Si}} + 5.0 \ \text{GHSER}_Y$$

**Phase  $\text{Si}_4\text{Y}_5$** 

$$G^\circ(T) - 4.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 \ H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 697950.0 + 86.72688 \ T + 4.0 \ \text{GHSER}_{\text{Si}} + 5.0 \ \text{GHSER}_Y$$

**Phase  $\text{SiY}$** 

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 160700.0 + 19.8 \ T + \text{GHSER}_{\text{Si}} + \text{GHSER}_Y$$

**Phase  $\text{Si}_5\text{Y}_3\text{-H}$** 

$$G^\circ(T) - 5.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 \ H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 601572.0 + 76.0 \ T + 5.0 \ \text{GHSER}_{\text{Si}} + 3.0 \ \text{GHSER}_Y$$

**Phase  $\text{Si}_5\text{Y}_3\text{-R}$** 

$$G^\circ(T) - 5.0 \ H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 \ H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ - 607356.0 + 84.0 \ T + 5.0 \ \text{GHSER}_{\text{Si}} + 3.0 \ \text{GHSER}_Y$$

**Phase bcc-A2**

$$L_{\text{Si},\text{Y}:□}^{0,\text{bcc}-A2} = 80 \ T$$

**Phase hcp-A3**

$$L_{\text{Si},\text{Y}:□}^{0,\text{hcp}-A3} = 80 \ T$$

**Phase liquid**

$$L_{\text{Si},\text{Y}}^{0,\text{liquid}} = - 212656.12 + 25.83471 \ T$$

$$L_{\text{Si},\text{Y}}^{1,\text{liquid}} = 13977.08 - 31.08941 \ T$$

$$L_{\text{Si},\text{Y}}^{2,\text{liquid}} = 62049.23 - 50.31476 \ T$$

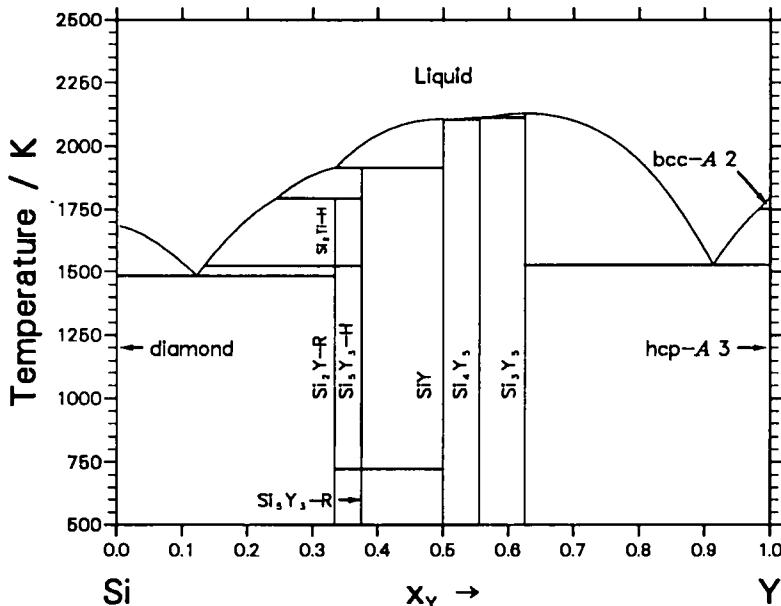


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_Y$			$T / K$
Liquid $\rightleftharpoons$ diamond + Si <sub>2</sub> Y-R	Eutectic	.122	.000	.333	1485.3
Si <sub>2</sub> Y-R $\rightleftharpoons$ Si <sub>2</sub> Y-H	Polymorphic	.333	.333	....	1523.0
Liquid + Si <sub>5</sub> Y <sub>3</sub> -H $\rightleftharpoons$ Si <sub>2</sub> Y-H	Peritectic	.244	.375	.333	1793.2
Liquid + SiY $\rightleftharpoons$ Si <sub>5</sub> Y <sub>3</sub> -H	Peritectic	.335	.500	.375	1915.3
SiY $\rightleftharpoons$ Liquid	Congruent	.500	.500	....	2108.0
Liquid $\rightleftharpoons$ SiY + Si <sub>4</sub> Y <sub>5</sub>	Eutectic	.518	.500	.556	2107.0
Si <sub>4</sub> Y <sub>5</sub> $\rightleftharpoons$ Liquid	Congruent	.556	.556	....	2114.5
Liquid $\rightleftharpoons$ Si <sub>4</sub> Y <sub>5</sub> + Si <sub>3</sub> Y <sub>5</sub>	Eutectic	.567	.556	.625	2113.9
Si <sub>3</sub> Y <sub>5</sub> $\rightleftharpoons$ Liquid	Congruent	.625	.625	....	2132.0
Liquid $\rightleftharpoons$ Si <sub>3</sub> Y <sub>5</sub> + hcp-A3	Eutectic	.913	.625	1.000	1527.9
hcp-A3 $\rightleftharpoons$ bcc-A2	Allotropic	1.000	1.000	....	1752.0
Si <sub>5</sub> Y <sub>3</sub> -R $\rightleftharpoons$ Si <sub>5</sub> Y <sub>3</sub> -H	Polymorphic	.375	.375	....	723.0

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
Si-Y	(Si)	C(diamond)	<i>cF8</i> <i>Fd3m</i>	M 8	
	(Y)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	(Y)	W	<i>cI2</i> <i>Im3m</i>	M 2	
	Si <sub>2</sub> Y- $\alpha$	AlB <sub>2</sub>	<i>hP3</i> <i>P6/mmm</i>		designated as Si <sub>2</sub> Y-R
	Si <sub>2</sub> Y- $\beta$	Si <sub>2</sub> Th	<i>oI12</i> <i>Imma</i>		designated as Si <sub>2</sub> Y-H Gd <sub>2</sub> Si <sub>3</sub> -type in [91Vil]
	Si <sub>3</sub> Y <sub>5</sub>	Mn <sub>5</sub> Si <sub>3</sub>	<i>hP16</i> <i>P6<sub>3</sub>/mc</i>	Si 6 Y <sub>1</sub> 4 Y <sub>2</sub> 6	
	Si <sub>4</sub> Y <sub>5</sub>	Si <sub>4</sub> Y <sub>5</sub>	<i>tP36</i> <i>P4<sub>1</sub>2<sub>1</sub>2</i>	Si <sub>1</sub> 8 Si <sub>2</sub> 8 Zr <sub>1</sub> 4 Zr <sub>2</sub> 8 Zr <sub>3</sub> 8	
	Si <sub>5</sub> Y <sub>3</sub> - $\alpha$	AlB <sub>2</sub>	<i>hP3</i> <i>P6/mmm</i>	Si 2 Y 1	designated as Si <sub>5</sub> Y <sub>3</sub> -R
	Si <sub>5</sub> Y <sub>3</sub> - $\beta$	ThSi <sub>2</sub>			designated as Si <sub>5</sub> Y <sub>3</sub> -H
	SiY	CrB	<i>oC8</i> <i>Cmcm</i>	Si 4 Y 4	

# System Si-Zn

**Solution Phases:**

Liquid, diamond, hcp-Zn

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
diamond	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister

**Assessor and Date:**

M. Jacobs 1993

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase diamond**

$$L_{\text{Si}, \text{Zn}}^{0, \text{diamond}} = 100 \ T$$

**Phase hcp-Zn**

$$L_{\text{Si}, \text{Zn}}^{0, \text{hcp-Zn}} = 80 \ T$$

**Phase liquid**

$$L_{\text{Si}, \text{Zn}}^{0, \text{liquid}} = 7829.25$$

$$L_{\text{Si}, \text{Zn}}^{1, \text{liquid}} = -3338.18$$

$$L_{\text{Si}, \text{Zn}}^{2, \text{liquid}} = -891.33$$

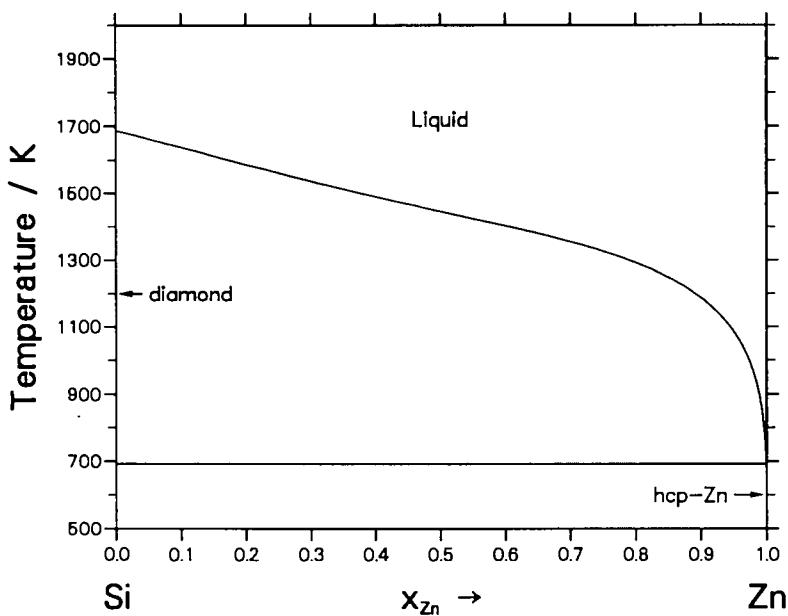


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Zn}}$	$T / \text{K}$
$\text{Liquid} \rightleftharpoons \text{diamond} + \text{hcp-Zn}$	Degenerate	1.000 .000 1.000	692.1

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Si-Zn	(Si)	diamond	$cF8$ $Fd\bar{3}m$
	(Zn)	Mg	$hP2$ $P\bar{6}_3/mmc$

# System Si-Zr

**Solution Phases:**

Liquid

**Compounds:**

Si<sub>2</sub>Zr, Si<sub>2</sub>Zr<sub>3</sub>, Si<sub>3</sub>Zr<sub>5</sub>, Si<sub>4</sub>Zr<sub>5</sub>, SiZr, SiZr<sub>2</sub>, SiZr<sub>3</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
Si <sub>2</sub> Zr	:	Stoichiometric (Si) <sub>2</sub> (Zr)
Si <sub>2</sub> Zr <sub>3</sub>	:	Stoichiometric (Si) <sub>2</sub> (Zr) <sub>3</sub>
Si <sub>3</sub> Zr <sub>5</sub>	:	Stoichiometric (Si) <sub>3</sub> (Zr) <sub>5</sub>
Si <sub>4</sub> Zr <sub>5</sub>	:	Stoichiometric (Si) <sub>4</sub> (Zr) <sub>5</sub>
SiZr	:	Stoichiometric (Si)(Zr)
SiZr <sub>2</sub>	:	Stoichiometric, (Si)(Zr) <sub>2</sub>
SiZr <sub>3</sub>	:	Stoichiometric (Si)(Zr) <sub>3</sub>

**Assessor and Date:**

C. Gueneau, C. Servant, I. Ansara, and N. Dupin

**Publication:**

Calphad, 18, 3, 319-327 (1994)

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase liquid**

$$L_{\text{Si},\text{Zr}}^{0,\text{liquid}} = -190000.0 + 16.8955 T$$

$$L_{\text{Si},\text{Zr}}^{1,\text{liquid}} = 14.52575 T$$

**Phase Si<sub>2</sub>Zr**

$$\begin{aligned} G^\circ(T) - 2.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp}-A^3}(298.15 \text{ K}) = \\ -189332.0 + 354.937 T - 63.16867 T \cdot \ln T - 7.67745E-03 T^2 \\ - 1.972048E-11 T^3 + 139751.1 T^{-1} \end{aligned}$$

**Phase SiZr**

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) =$$

$$- 182203.4 + 258.514 T - 45.18631 T \cdot \ln T - 4.393865 \times 10^{-3} T^2$$

$$+ 5.49699 \times 10^{-11} T^3 + 148517.5 T^{-1}$$

**Phase Si<sub>4</sub>Zr<sub>5</sub>**

$$G^\circ(T) - 4.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) =$$

$$- 880743.11 + 1433.658 T - 240.256 T \cdot \ln T - 0.0109481 T^2$$

$$+ 6.591183 \times 10^{-7} T^3 + 2006425 T^{-1}$$

**Phase Si<sub>2</sub>Zr<sub>3</sub>**

$$G^\circ(T) - 2.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) =$$

$$- 493990.62 + 844.448 T - 140.103 T \cdot \ln T - 0.003701 T^2$$

$$+ 1.028333 \times 10^{-7} T^3 + 1167755 T^{-1}$$

**Phase Si<sub>3</sub>Zr<sub>5</sub>**

$$G^\circ(T) - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 5.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) =$$

$$- 685146.78 + 1044.78 T - 187 T \cdot \ln T - 0.0161754 T^2$$

$$+ 5.22283 \times 10^{-8} T^3 + 381210 T^{-1}$$

**Phase SiZr<sub>2</sub>**

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 2.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) =$$

$$- 255317.83 + 411.767 T - 72.43244 T \cdot \ln T - 5.46177 \times 10^{-3} T^2$$

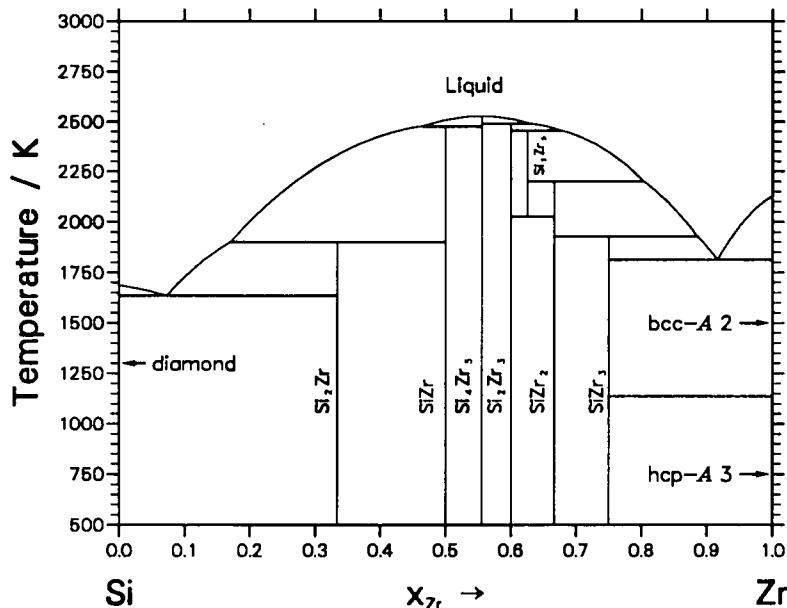
$$- 4.0442633 \times 10^{-9} T^3 + 306730.45 T^{-1}$$

**Phase SiZr<sub>3</sub>**

$$G^\circ(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) - 3.0 H_{\text{Zr}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) =$$

$$- 270398.16 + 457.33 T - 82.328 T \cdot \ln T - 0.0263963 T^2$$

$$+ 1.54326 \times 10^{-6} T^3 - 34700 T^{-1}$$



**Table I - Invariant Reactions.**

Reaction	Type	Compositions $x_{Zr}$			$T / K$
$Liquid \rightleftharpoons diamond + Si_2Zr$	Eutectic	.073	.000	.333	1634.6
$Liquid + SiZr \rightleftharpoons Si_2Zr$	Peritectic	.170	.500	.333	1900.3
$Liquid + Si_4Zr_5 \rightleftharpoons Si_2Zr$	Peritectic	.463	.555	.500	2477.0
$Liquid + Si_4Zr_5 \rightleftharpoons Si_2Zr_3$	Peritectic	.629	.555	.600	2491.5
$Liquid + Si_2Zr_3 \rightleftharpoons Si_3Zr_5$	Peritectic	.677	.600	.675	2455.4
$Liquid + Si_3Zr_5 \rightleftharpoons Si_2Zr_2$	Peritectic	.803	.625	.666	2200.0
$Liquid + Si_2Zr_2 \rightleftharpoons Si_2Zr_3$	Peritectic	.886	.666	.750	1927.4
$Liquid \rightleftharpoons Si_2Zr_3 + bcc-A2$	Eutectic	.916	.750	1.000	1814.2
$hcp-A3 \rightleftharpoons bcc-A2$	Allotropic	1.000	1.000	....	1139.4
$Si_3Zr_5 \rightleftharpoons Si_2Zr_3 + Si_2Zr_2$	Eutectoid	.625	.600	.666	2025.2
$Liquid \rightleftharpoons Si_4Zr_5$	Congruent	.556	.556	....	2527.0

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
Si-Zr	(Si)	diamond	<i>cF8</i> <i>Fd3m</i>	M 8	
	(Zr)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	(Zr)	W	<i>cI2</i> <i>Im3m</i>	M 4	
	SiZr- $\alpha$	BFe	<i>oP8</i>	Si 4	transformation not considered
	SiZr- $\beta$	BCr	<i>oC8</i> <i>Cmcm</i>	Zr 4	
	SiZr <sub>2</sub>	Al <sub>2</sub> Cu	<i>tI12</i> <i>I4/mcm</i>	Si 8 Zr 4	
	SiZr <sub>3</sub>	PTi <sub>3</sub>	<i>tP32</i> <i>P4<sub>2</sub>/n</i>		
	Si <sub>2</sub> Zr	Si <sub>2</sub> Zr	<i>oCl2</i> <i>Cmcm</i>	Si <sub>1</sub> 4 Si <sub>2</sub> 4 Zr 4	
	Si <sub>2</sub> Zr <sub>3</sub>	Si <sub>2</sub> U <sub>3</sub>	<i>tP10</i> <i>P4/mbm</i>		
	Si <sub>3</sub> Zr <sub>5</sub>	Mn <sub>5</sub> Si <sub>3</sub>	<i>hP16</i> <i>P6<sub>3</sub>/mcm</i>	Si 6 Zr <sub>1</sub> 4 Zr <sub>2</sub> 6	
Si <sub>4</sub> Zr <sub>5</sub> - $\alpha$	Si <sub>4</sub> Zr <sub>5</sub>		<i>tP36</i> <i>P4<sub>1</sub>2<sub>1</sub>2</i>	Si <sub>1</sub> 8 Si <sub>2</sub> 8 Zr <sub>1</sub> 4 Zr <sub>2</sub> 8 Zr <sub>3</sub> 8	transformation not considered
	Si <sub>4</sub> Zr <sub>5</sub> - $\beta$	Si <sub>4</sub> Zr <sub>5</sub>			

# System Sn-Ti

**Solution Phases:**

Liquid, bcc-A2, hcp-A3, bct-A5

**Compounds:**

Sn<sub>5</sub>Ti<sub>6</sub>, Sn<sub>3</sub>Ti<sub>5</sub>, SnTi<sub>2</sub>, SnTi<sub>3</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc-A2	:	Substitutional, Redlich-Kister
bct-A5	:	Substitutional, Redlich-Kister
hcp-A3	:	Substitutional, Redlich-Kister
SnTi <sub>3</sub>	:	Sublattice model: (Sn,Ti)(Sn,Ti) <sub>3</sub>
Sn <sub>5</sub> Ti <sub>6</sub>	:	Stoichiometric, (Sn) <sub>5</sub> (Ti) <sub>6</sub>
Sn <sub>3</sub> Ti <sub>5</sub>	:	Stoichiometric, (Sn) <sub>3</sub> (Ti) <sub>5</sub>
SnTi <sub>2</sub>	:	Stoichiometric, (Sn)(Ti) <sub>2</sub>

**Assessor and Date:**

F. Hayes, 1992

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase bcc-A2**

$$L_{\text{Sn}, \text{Ti}: \square}^{0, \text{bcc}-A2} = -115000.00 + 6.77583 T$$

$$L_{\text{Sn}, \text{Ti}: \square}^{1, \text{bcc}-A2} = 45000.00 + 1.58018 T$$

**Phase bct-A5**

$$L_{\text{Sn}, \text{Ti}: \square}^{0, \text{bct}-A5} = 50000.0$$

**Phase hcp-A3**

$$L_{\text{Sn}, \text{Ti}: \square}^{0, \text{hcp}-A3} = -111502.08 + 1.8068 T$$

$$L_{\text{Sn}, \text{Ti}: \square}^{1, \text{hcp}-A3} = 43871.41 + 2.08175 T$$

### Phase liquid

$$L_{\text{Sn,Ti}}^{0,\text{liquid}} = -90206.13 - 5.55089 T$$

$$L_{\text{Sn,Ti}}^{1,\text{liquid}} = 44395.59 - 6.09746 T$$

### Phase $\text{SnTi}_3$

$$G^\circ(T) - 4.0 H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) = G(\text{Sn:Sn}) = \\ 4.0 \text{ GHSER}_{\text{Sn}}$$

$$G^\circ(T) - H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Sn:Ti}) = \\ -193466.8 + 35.74052 T + \text{GLIQ}_{\text{Sn}} + 3.0 \text{ GLIQ}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Sn}) = \\ 300000 - 200 T + 3.0 \text{ GLIQ}_{\text{Sn}} + \text{GLIQ}_{\text{Ti}}$$

$$G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti}) = \\ 4.0 \text{ GHSER}_{\text{Ti}}$$

$$L_{\text{Sn:Sn,Ti}}^{0,\text{SnTi}_3} = 400000 - 40.0 T$$

$$L_{\text{Ti:Sn,Ti}}^{0,\text{SnTi}_3} = 600000 + 40.0 T$$

$$L_{\text{Sn,Ti:Sn}}^{0,\text{SnTi}_3} = 400000$$

$$L_{\text{Sn,Ti:Ti}}^{0,\text{SnTi}_3} = 200000 - 108.000 T$$

### Phase $\text{SnTi}_2$

$$G^\circ(T) - H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) - 2.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ -152700.00 + 26.80539 T + \text{GLIQ}_{\text{Sn}} + 2.0 \text{ GLIQ}_{\text{Ti}}$$

### Phase $\text{Sn}_3\text{Ti}_5$

$$G^\circ(T) - 3.0 H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) - 5.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ -398000.00 + 64.8 T + 3.0 \text{ GLIQ}_{\text{Sn}} + 5.0 \text{ GLIQ}_{\text{Ti}}$$

### Phase $\text{Sn}_5\text{Ti}_6$

$$G^\circ(T) - 5.0 H_{\text{Sn}}^{\circ,\text{bct}-A5}(298.15 \text{ K}) - 6.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = \\ -525800.00 + 77.0 T + 5.0 \text{ GLIQ}_{\text{Sn}} + 6.0 \text{ GLIQ}_{\text{Ti}}$$

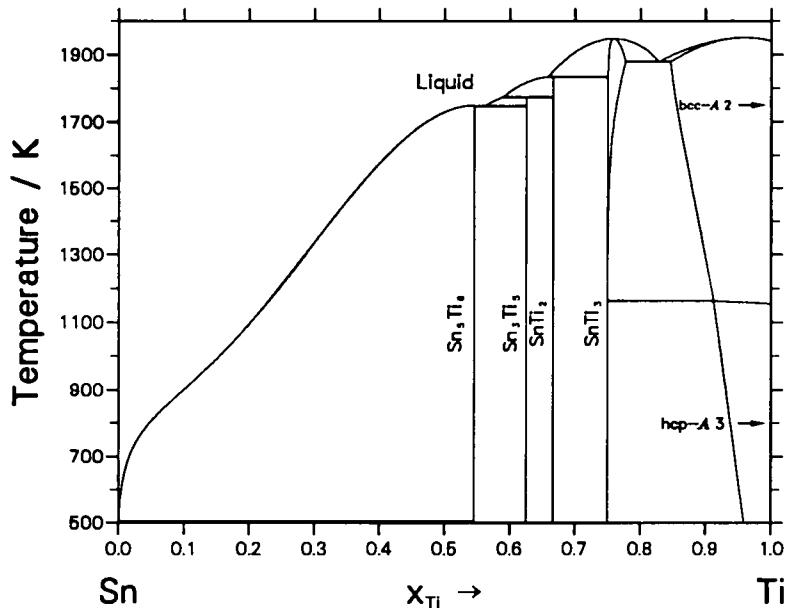


Table I – Invariant Reactions.

Reaction	Type	Compositions x <sub>Ti</sub>			T / K
bcc-A2 + SnTi <sub>3</sub> ⇌ hcp-A3	Peritectic	.913	.750	.912	1163.3
Liquid ⇌ SnTi <sub>3</sub> + bcc-A2	Eutectic	.828	.777	.846	1879.8
SnTi <sub>3</sub> ⇌ Liquid	Congruent	.750	.750	....	1947.0
Liquid + SnTi <sub>3</sub> ⇌ SnTi <sub>2</sub>	Peritectic	.659	.750	.667	1835.9
Liquid + SnTi <sub>2</sub> ⇌ + Sn <sub>3</sub> Ti <sub>5</sub>	Peritectic	.589	.667	.625	1774.7
Liquid ⇌ Sn <sub>5</sub> Ti <sub>6</sub> + Sn <sub>3</sub> Ti <sub>5</sub>	Eutectic	.561	.545	.625	1746.9
Sn <sub>5</sub> Ti <sub>6</sub> ⇌ Liquid	Congruent	.545	.545	....	1750.0
Liquid ⇌ bct-A5 + Sn <sub>5</sub> Ti <sub>6</sub>	Degenerate	.001	.000	.545	504.8

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Sn-Ti	(Sn)	$\beta$ -Sn	$tI\bar{4}$ $I\bar{4}_1/amd$	M 2	transformation not considered
	(Ti)	Mg	$hP2$ $P\bar{6}_3/mmc$	M 2	
	(Ti)	W	$cI\bar{2}$ $I\bar{m}\bar{3}m$	M 2	
	$Sn_5Ti_6-\alpha$	$Nb_6Sn_5$	$oI\bar{4}\bar{4}$ $Immm\bar{3}$		
	$Sn_5Ti_6-\beta$	.....	$hP22$ $P\bar{6}_3/mmc$	Sn 3 Ti 6	
	$Sn_3Ti_5$	$Mn_5Si_3$	$hP16$ $P\bar{6}_3/mcm$	Sn 6 Ti 4	
	$SnTi_2$	$InNi_2$	$hP6$ $P\bar{6}_3/mmc$		
	$SnTi_3$	$Ni_3Sn$	$hP8$ $P\bar{6}_3/mmc$	Sn 2 Ti 6 $Si_1$ 4 $Si_2$ 8	

# System Sn-Zn

**Solution Phases:**

(stable)	Liquid, bct- <i>A5</i> , hcp-Zn
(metastable)	bcc- <i>A2</i>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A2</i>	:	Substitutional, Redlich-Kister
bct- <i>A5</i>	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister

**Assessor and Date:**

S. Fries, and H.L. Lukas

**Publication:**

"Cost507 New Light Alloys", Leuven Proceedings,  
Ed. G. Effenberg (1991)

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase bct-*A5***

$$L_{\text{Sn}, \text{Zn}: \square}^{0, \text{bct}-\text{A5}} = 6514.76 + 25.70957 \ T$$

**Phase bcc-*A2***

$$L_{\text{Sn}, \text{Zn}: \square}^{0, \text{bcc}-\text{A2}} = 6514.76 + 25.70957 \ T$$

**Phase hcp-Zn**

$$L_{\text{Sn}, \text{Zn}: \square}^{0, \text{hcp}-\text{Zn}} = 33433.94 - 11.14466 \ T$$

**Phase liquid**

$$L_{\text{Sn}, \text{Zn}}^{0, \text{liquid}} = 19314.64 - 75.89939 \ T + 8.751396 \ T \cdot \ln T$$

$$L_{\text{Sn}, \text{Zn}}^{1, \text{liquid}} = -5696.28 + 4.20198 \ T$$

$$L_{\text{Sn}, \text{Zn}}^{2, \text{liquid}} = 1037.22 + 0.98362 \ T$$

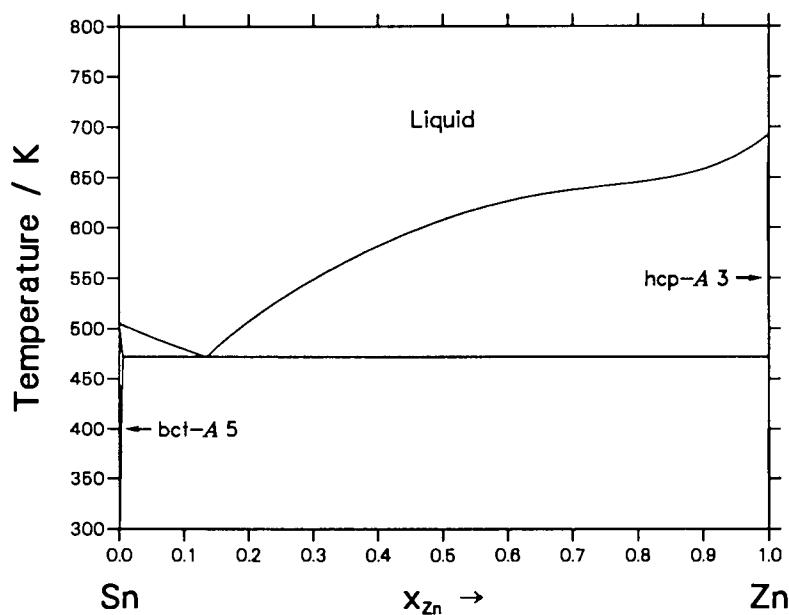


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Zn}}$	$T / \text{K}$
Liquid $\rightleftharpoons$ bct-A5 + hcp-Zn	Eutectic	0.135 .006 1.000	471.7

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Sn-Zn	(Sn)	$\beta$ -Sn	$tI_4$ $I_{41}/amd$
	(Zn)	Mg	$hP2$ $P6_3/mmc$

# System Sn – Zr

**Solution Phases**

Liquid, bcc-*A*2, bct-*A*5, hcp-*A*3

**Compounds:**

SnZr4, Sn3Zr5, Sn2Zr

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
<chem>SnZr4</chem>	:	Stoichiometric, <chem>(Sn)(Zr)4</chem>
<chem>Sn3Zr5</chem>	:	Stoichiometric, <chem>(Sn)3(Zr)5</chem>
<chem>Sn2Zr</chem>	:	Stoichiometric, <chem>(Sn)2(Zr)</chem>

**Assessor and date:**

J. Korb, and K. Hack, GTT, Germany (1996).

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase liquid**

$$L_{\text{Sn}, \text{Zr}}^{0, \text{liquid}} = -45520 - 95.46 T$$

$$L_{\text{Sn}, \text{Zr}}^{1, \text{Liquid}} = -80000 + 82.115 T$$

$$L_{\text{Sn}, \text{Zr}}^{2, \text{Liquid}} = -120000 + 80.0273 T$$

**Phase bcc-*A*2**

$$L_{\text{Sn}, \text{Zr}: \square}^{0, \text{bcc-}A2} = -101200 - 71.13 T$$

$$L_{\text{Sn}, \text{Zr}: \square}^{1, \text{bcc-}A2} = 55000$$

$$L_{\text{Sn}, \text{Zr}: \square}^{2, \text{bcc-}A2} = 26102.3$$

**Phase hcp-A3**

$$L_{\text{Sn}, \text{Zr}: \square}^{0, \text{hcp}-A3} = -160000 - 31 T$$

$$L_{\text{Sn}, \text{Zr}: \square}^{1, \text{hcp}-A3} = 151800$$

$$L_{\text{Sn}, \text{Zr}: \square}^{2, \text{hcp}-A3} = 129900$$

**Phase SnZr<sub>4</sub>**

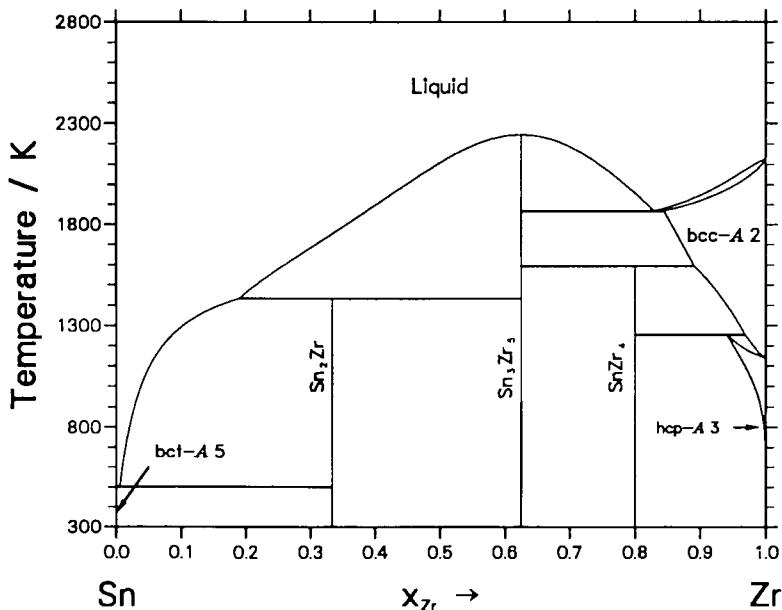
$$G^\circ(T) - H_{\text{Sn}}^{\circ, \text{bct}-A5}(298.15 \text{ K}) - 4.0 H_{\text{Zr}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \\ - 270456.8 + 602.125 T - 123.0 T \cdot \ln T - 0.00883 T^2$$

**Phase Sn<sub>3</sub>Zr<sub>5</sub>**

$$G^\circ(T) - 3.0 H_{\text{Sn}}^{\circ, \text{bct}-A5}(298.15 \text{ K}) - 5.0 H_{\text{Zr}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \\ - 769380 + 1131.86 T - 217.118 T \cdot \ln T - 0.02404 T^2 \\ + 1648000 T^{-1}$$

**Phase Sn<sub>2</sub>Zr**

$$G^\circ(T) - 2.0 H_{\text{Sn}}^{\circ, \text{bct}-A5}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = \\ - 267104.8 + 492.1 T - 86.404 T \cdot \ln T - 0.002226 T^2 \\ + 618000 T^{-1}$$



**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{\text{Zr}}$			$T / \text{K}$
Liquid $\rightleftharpoons$ bcc-A2 + Sn <sub>3</sub> Zr <sub>5</sub>	Eutectic	.892	.844	.625	1868.5
bcc-A2 + Sn <sub>3</sub> Zr <sub>5</sub> $\rightleftharpoons$ SnZr <sub>4</sub>	Peritectoid	.891	.625	.800	1595.5
bcc-A2 + SnZr <sub>4</sub> $\rightleftharpoons$ hcp-A3	Peritectoid	.968	.800	.941	1254.0
Liquid + Sn <sub>3</sub> Zr <sub>5</sub> $\rightleftharpoons$ Sn <sub>2</sub> Zr	Peritectoid	.189	.625	.333	1433.3
Liquid $\rightleftharpoons$ Sn <sub>2</sub> Zr + bct-A5	Eutectic	.0056	.333	.000	502.0
Liquid $\rightleftharpoons$ Sn <sub>3</sub> Zr <sub>5</sub>	Congruent	.625	.625	....	2245.0

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices
Sn-Zr	(Sn)	$\beta$ -Sn	$tI_4$ $I\bar{4}_1/AMD$	M 2
	(Zr)	Mg	$hP2$ $P\bar{6}_3/mmc$	M 2
	(Zr)	W	$cI2$ $I\bar{m}\bar{3}m$	M 2
	SnZr <sub>4</sub>	Cr <sub>3</sub> Si	$cP8$ $Pm\bar{3}n$	
	Sn <sub>3</sub> Zr <sub>5</sub>	Mn <sub>5</sub> Si <sub>3</sub>	$hP16$ $P\bar{6}_3/mcm$	
	Sn <sub>2</sub> Zr	SiTi <sub>2</sub>	$oF24$ $Fddd$	

# System Ta-Ti

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, hcp- <i>A</i> 3
(metastable)	bcc- <i>B</i> 2, fcc- <i>A</i> 1

**Compounds:**

(metastable)	AlM- <i>D</i> 0 <sub>19</sub> , AlM- <i>D</i> 0 <sub>22</sub> , AlTi- <i>L</i> 1 <sub>0</sub>
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**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	see below
bcc- <i>B</i> 2	:	Sublattice model, (Ta,Ti) <sub>0.5</sub> (Ta,Ti) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc- <i>A</i> 2 ⇌ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Ta,Ti)(Ta,Ti) <sub>3</sub>
AlM- <i>D</i> 0 <sub>22</sub>	:	Sublattice model, (Ti) <sub>3</sub> (Ta,Ti)
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Ta,Ti)(Ta,Ti)

**Assessor and Date:**

N. Saunders, 1997.

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase fcc-*A*1**

$$L_{\text{Ta,Ti:}\square}^{0,\text{fcc-}A1} = 8500$$

**Phase hcp-*A*3**

$$L_{\text{Ta,Ti:}\square}^{0,\text{hcp-}A3} = 8500$$

### Phase liquid

$$L_{\text{Ta,Ti}}^{0,\text{liquid}} = 1000$$

$$L_{\text{Ta,Ti}}^{1,\text{liquid}} = -7000$$

### Phase AlM-D0<sub>19</sub>

$$\begin{aligned} G^\circ(T) - 4.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Ta:Ta}) = 4.0 \text{ GHCP}_{\text{Ta}} \\ G^\circ(T) - 3.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ta:Ti}) = \\ &\quad 6376 + 3.0 \text{ GHCP}_{\text{Ta}} + \text{GHSER}_{\text{Ti}} \\ G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ta}) = \\ &\quad 6376 + \text{GHCP}_{\text{Ta}} + 3.0 \text{ GHSER}_{\text{Ti}} \\ G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ti}) = 4.0 + 4.0 \text{ GHSER}_{\text{Ti}} \\ L_{\text{Ta,Ti:Ta}}^{0,\text{AlM}-D0_{19}} &= L_{\text{Ta,Ti:Ti}}^{0,\text{AlM}-D0_{19}} = 19128 \\ L_{\text{Ta:Ta,Ti}}^{0,\text{AlM}-D0_{19}} &= L_{\text{Ti:Ta,Ti}}^{0,\text{AlM}-D0_{19}} = 2128 \end{aligned}$$

### Phase AlM-D0<sub>22</sub>

$$\begin{aligned} G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ta}) = \\ &\quad \text{GFCC}_{\text{Ta}} + 3.0 \text{ GFCC}_{\text{Ti}} \\ G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ti}) = 4.0 \text{ GFCC}_{\text{Ti}} \end{aligned}$$

### Phase AlTi-L1<sub>0</sub>

$$\begin{aligned} G^\circ(T) - 2.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) &= G(\text{Ta:Ta}) = 2.0 \text{ GFCC}_{\text{Ta}} \\ G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ta:Ti}) = \\ &\quad 4250 + \text{GFCC}_{\text{Ta}} + \text{GFCC}_{\text{Ti}} \\ G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ta}) = \\ &\quad 4250 + \text{GFCC}_{\text{Ta}} + \text{GFCC}_{\text{Ti}} \\ G^\circ(T) - 2.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) &= G(\text{Ti:Ti}) = 2.0 \text{ GFCC}_{\text{Ti}} \\ L_{\text{Ta,Ti:Ta}}^{0,\text{AlTi}-L1_0} &= L_{\text{Ta:Ta,Ti}}^{0,\text{AlTi}-L1_0} = 4250 \\ L_{\text{Ta,Ti:Ti}}^{0,\text{AlTi}-L1_0} &= L_{\text{Ti:Ta,Ti}}^{0,\text{AlTi}-L1_0} = 4250 \end{aligned}$$

### Phase bcc-A2

$$L_{\text{Ta,Ti:O}}^{0,\text{bcc}-A2} = 12000$$

$$L_{\text{Ta,Ti:O}}^{1,\text{bcc}-A2} = -2500$$

## Phase bcc-B2

$$G_{\text{Ta:Ta:}\square}^* = -2500$$

$$G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Ta:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ta:Ti:}\square) = G_{\text{Ta:Ti:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ta:Ti:}\square) = G_{\text{Ti:Ta:}\square}^*$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 0.0$$

$$L_{\text{Ta,Ti:Ta:}\square}^{0,\text{bcc}-B2} = L_{\text{Ta,Ti:Ti:}\square}^{0,\text{bcc}-B2} = -G_{\text{Ti:Ta:}\square}^*$$

$$L_{\text{Ta:Ta,Ti:}\square}^{0,\text{bcc}-B2} = L_{\text{Ti:Ta,Ti:}\square}^{0,\text{bcc}-B2} = -G_{\text{Ti:Ta:}\square}^*$$

## Phase bcc-B2

$$G_{\text{Ti:Ta:}\square}^* = 2500$$

$$G^\circ(T) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ta:Ta:}\square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ta:Ti:}\square) = 2.0 G_{\text{Ti:Ta:}\square}^*$$

$$G^\circ(T) - 0.5 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ta:}\square) = 2.0 G_{\text{Ti:Ta:}\square}^*$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 0.0$$

## Phase bcc-A2

$$L_{\text{Ta,Ti:}\square}^{0,\text{bcc}-A2} = 12000$$

$$L_{\text{Ta,Ti:}\square}^{1,\text{bcc}-A2} = -2500$$

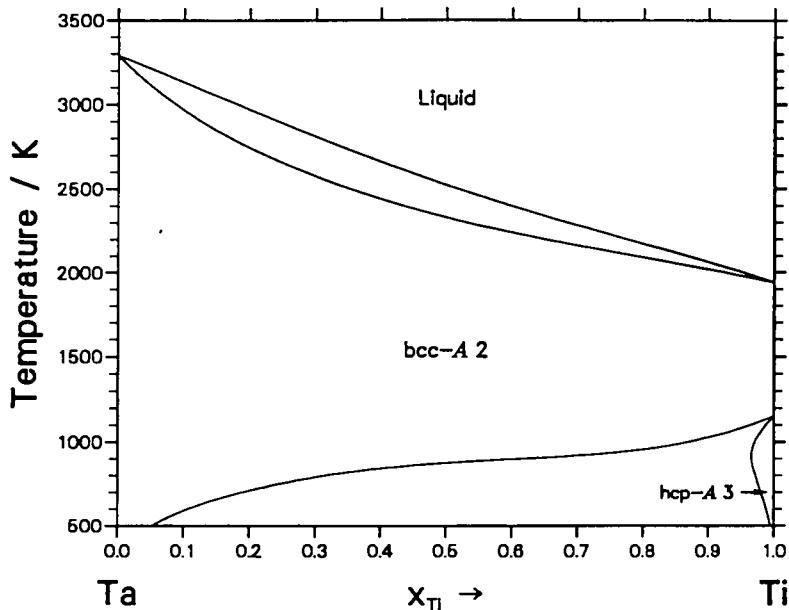


Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Ta-Ti	(V)	W	<i>cI2</i> <i>Im3m</i>
	(Ti)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>
	(Ti)	W	<i>cI2</i> <i>Im3m</i>

# System Ti-V

**Solution Phases:**

Liquid, bcc-*A*2, hcp-*A*3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
	:	

**Assessor and Date:**

N. Saunders (1990)

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A*2**

$$L_{\text{Ti,V}:□}^{0,\text{bcc-}A2} = 10500 - 1.5 \cdot T$$

$$L_{\text{Ti,V}:□}^{1,\text{bcc-}A2} = 2000$$

$$L_{\text{Ti,V}:□}^{2,\text{bcc-}A2} = 1000$$

**Phase hcp-*A*3**

$$L_{\text{Ti,V}:□}^{0,\text{hcp-}A3} = 20000$$

**Phase liquid**

$$L_{\text{Ti,V}}^{0,\text{liquid}} = 1400$$

$$L_{\text{Ti,V}}^{1,\text{liquid}} = 4100$$

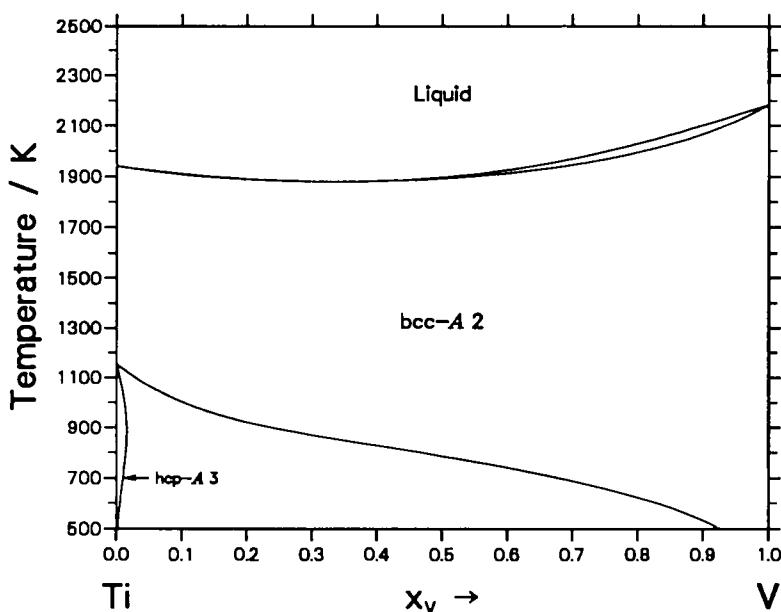


Table I – Invariant Reactions.

Reaction	Type	Compositions $x_V$	$T / K$
$bcc\text{-}A2 \rightleftharpoons \text{Liquid}$	Congruent	0.333    0.333    ....	1881.0

Table II – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group
Ti-V	(Ti)	Mg	$hP2$ $P6_3/mmc$
	(Ti)	W	$cI2$ $I\bar{m}\bar{3}m$
	(V)	W	$cI2$ $I\bar{m}\bar{3}m$

# System Ti-W

**Solution Phases:**

(stable)	Liquid, bcc- <i>A</i> 2, hcp- <i>A</i> 3
(metastable) :	bcc- <i>B</i> 2, fcc- <i>A</i> 1

**Compounds:**

(metastable) :	AlM- <i>D</i> 0 <sub>19</sub> , AlTi- <i>L</i> 1 <sub>0</sub>
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**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	see above
bcc- <i>B</i> 2	:	Sublattice model, (Ti,W) <sub>0.5</sub> (Ti,W) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc- <i>B</i> 2 takes into account the ordering reaction bcc- <i>A</i> 2 ⇌ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Ti,W)(Ti,W) <sub>3</sub>
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Ti,W)(Ti,W)

**Assessor and Date:**

N. Saunders, 1997.

**Thermodynamic properties of the solution phases (J.mol<sup>-1</sup>)**

**Phase fcc-*A*1**

$$L_{\text{Ti}, \text{W}: \square}^{0, \text{fcc}-\text{A}1} = 33825$$

**Phase hcp-*A*3**

$$L_{\text{Ti}, \text{W}: \square}^{0, \text{hcp}-\text{A}3} = 35774$$

### Phase liquid

$$L_{\text{Ti},\text{W}}^{0,\text{liquid}} = 28392$$

$$L_{\text{Ti},\text{W}}^{1,\text{liquid}} = -4282$$

### Phase AlM-D0<sub>19</sub>

$$G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Ti}) = 4.0 + 4.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ti}: \text{W}) = 26832 + 3.0 \text{ GHCP}_{\text{W}} + \text{GHSER}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 3.0 H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{W}: \text{Ti}) = 26832 + \text{GHCP}_{\text{W}} + 3.0 \text{ GHSER}_{\text{Ti}}$$

$$G^\circ(T) - 4.0 H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{W}: \text{W}) = 4.0 \text{ GHCP}_{\text{W}}$$

$$L_{\text{Ti},\text{W}: \text{Ti}}^{0,\text{AlM}-D0_{19}} = L_{\text{Ti},\text{W}: \text{Wi}}^{0,\text{AlM}-D0_{19}} = 80492$$

$$L_{\text{Ti}: \text{Ti}, \text{W}}^{0,\text{AlM}-D0_{19}} = L_{\text{W}: \text{Ti}, \text{W}}^{0,\text{AlM}-D0_{19}} = 8944$$

### Phase AlTi-L1<sub>0</sub>

$$G^\circ(T) - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Ti}) = 2.0 \text{ GFCC}_{\text{Ti}}$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ti}: \text{W}) = 4250 + \text{GFCC}_{\text{Ti}} + \text{GFCC}_{\text{W}}$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{W}: \text{Ti}) = 4250 + \text{GFCC}_{\text{Ti}} + \text{GFCC}_{\text{W}}$$

$$G^\circ(T) - 2.0 H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{W}: \text{W}) = 2.0 \text{ GFCC}_{\text{W}}$$

$$L_{\text{Ti},\text{W}: \text{Ti}}^{0,\text{AlTi}-L1_0} = L_{\text{Ti}: \text{Ti}, \text{W}}^{0,\text{AlTi}-L1_0} = 16914$$

$$L_{\text{Ti},\text{W}: \text{W}}^{0,\text{AlTi}-L1_0} = L_{\text{W}: \text{Ti}, \text{W}}^{0,\text{AlTi}-L1_0} = 16914$$

### Phase bcc-A2

$$L_{\text{Ti},\text{W}: \square}^{0,\text{bcc}-A2} = 3957 + 13.033 \text{ } T$$

$$L_{\text{Ti},\text{W}: \square}^{1,\text{bcc}-A2} = 10640 - 4.464 \text{ } T$$

### Phase bcc-B2

$$G_{\text{Ti}: \text{W}: \square}^* = 0$$

$$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti}: \text{Ti}: \square) = 0.0$$

$$G^\circ(T) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 0.5 H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Ti}: \text{W}: \square) = G_{\text{Ti}: \text{W}: \square}^*$$

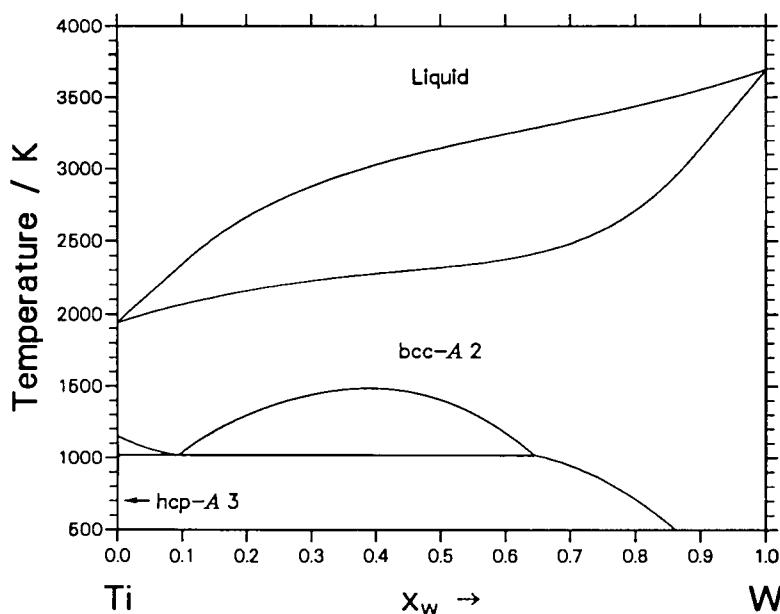
$$G^\circ(T) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) - 0.5 H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{W}: \text{Ti}: \square) = G_{\text{Ti}: \text{W}: \square}^*$$

$$G^\circ(T) - H_{\text{W}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{W}: \text{W}: \square) = 0.0$$

$$L_{\text{Ti},\text{W}: \text{W}: \square}^{0,\text{bcc}-B2} = L_{\text{Ti},\text{W}: \text{Ti}: \square}^{0,\text{bcc}-B2} = -G_{\text{Ti}: \text{W}: \square}^*$$

$$L_{\text{W}: \text{Ti}, \text{W}: \square}^{0,\text{bcc}-B2} = L_{\text{Ti}: \text{Ti}, \text{W}: \square}^{0,\text{bcc}-B2} = -G_{\text{Ti}: \text{W}: \square}^*$$

Phase bcc-B2	
$G_{\text{Ti:W:}\square}^* = 0$	
$G^\circ(T) - H_W^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{W:W:}\square) = 0.0$	
$G^\circ(T) - 0.5 H_W^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{W:Ti:}\square) = 2.0$	$G_{\text{Ti:W:}\square}^*$
$G^\circ(T) - 0.5 H_W^{\circ,\text{bcc}-A2}(298.15 \text{ K}) - 0.5 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:W:}\square) = 2.0$	$G_{\text{Ti:W:}\square}^*$
$G^\circ(T) - H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Ti:Ti:}\square) = 0.0$	
Phase bcc-A2	
$L_{\text{Ti,W:}\square}^{0,\text{bcc}-A2} = 3957 + 13.033 T$	
$L_{\text{Ti,W:}\square}^{1,\text{bcc}-A2} = 10640 - 4.464 T$	



**Table I – Invariant Reactions.**

Reaction	Type	Compositions $x_{W_i}$	$T / K$
hcp-A3 bcc-A2' $\rightleftharpoons$ bcc-A2''	Monotectoid	.002 .645 .095	1019.5

**Table II – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group
Ti-W	(V)	W	<i>cI2</i> <i>Im3m</i>
	(Ti)	Mg	<i>hP2</i> <i>P63/mmc</i>
	(Ti)	W	<i>cI2</i> <i>Im3m</i>

# System V-Zr

**Solution Phases:**

Liquid, bcc-*A*2, hcp-*A*3

**Compound:**

V<sub>2</sub>Zr

**Modelling:**

bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
Liquid	:	Substitutional, Redlich-Kister
V <sub>2</sub> Zr	:	Sublattice model, (V) <sub>2</sub> (Zr)

**Assessor and Date:**

J. Korb, and K. Hack, GTT, Germany (1995).

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**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

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**Phase V<sub>2</sub>Zr**

$$G^\circ(T) - 2.0 \ H_V^{\circ,\text{bcc-}A2}(298.15 \text{ K}) - H_{\text{Zr}}^{\circ,\text{hcp-}A3}(298.15 \text{ K}) = \\ - 63100 + 26.83 \ T + 2.0 \ \text{GLIQ}_V + \text{GLIQ}_{\text{Zr}}$$

**Phase liquid**

$$L_{\text{V},\text{Zr}}^{0,\text{liquid}} = - 23986 + 19.338 \ T$$

$$L_{\text{V},\text{Zr}}^{1,\text{liquid}} = - 2058.35 + 3.289 \ T$$

**Phase bcc-*A*2**

$$L_{\text{V},\text{Zr}:□}^{0,\text{bcc-}A2} = 21876 + 7.76081 \ T$$

$$L_{\text{V},\text{Zr}:□}^{1,\text{bcc-}A2} = 8995.72 - 0.8968 \ T$$

**Phase hcp-*A*3**

$$L_{\text{V},\text{Zr}:□}^{0,\text{hcp-}A3} = 29007 - 7.2944 \ T$$

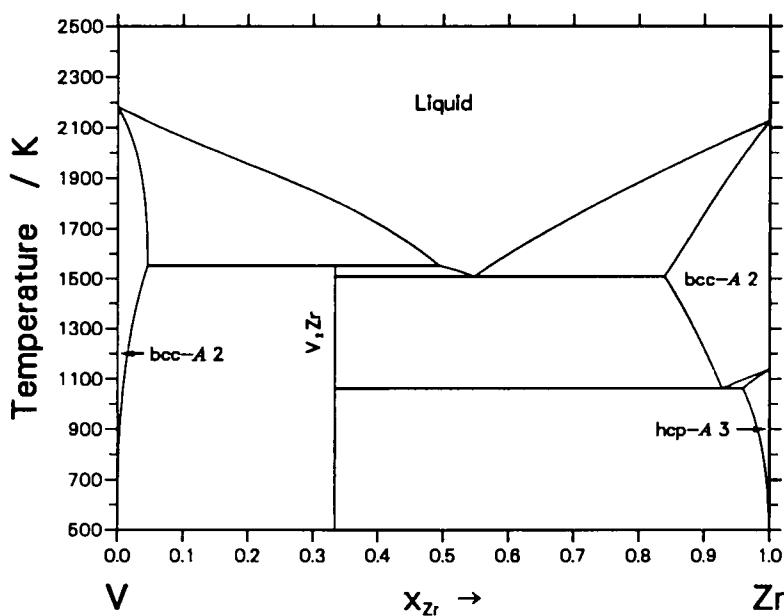


Table I - Invariant Reactions.

Reaction	Type	Compositions $x_{\text{Zr}}$	$T / \text{K}$
bcc-A2 + Liquid $\rightleftharpoons$ V <sub>2</sub> Zr	Peritectic	.046	1552.7
Liquid $\rightleftharpoons$ V <sub>2</sub> Zr + bcc-A2	Eutectic	.548	1510.2
bcc-A2 $\rightleftharpoons$ V <sub>2</sub> Zr + hcp-A3	Eutectoid	.927	1062.9

Table II - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
V-Zr	(V)	W	cI2 Im $\bar{3}m$	M 2	Laves-C15
	(Zr)	Mg	hP2 P6 $_3/mmc$	M 2	
	(Zr)	W	cI2 Im $\bar{3}m$	M 4	
	V <sub>2</sub> Zr	Cu <sub>2</sub> Mg	cF24 Fd $\bar{3}m$	M <sub>1</sub> 8 M <sub>2</sub> 16	

# **TERNARY SYSTEMS**



# System Al-C-Si

Ternary Solution Phases:

Liquid, fcc-Al

Ternary Compounds:

$\text{Al}_4\text{SiC}_4$ ,  $\text{Al}_8\text{SiC}_7$

Quasi-binary phase:

$(\text{Al},\text{Si})_4\text{C}_3$

Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc-Al	:	Substitutional, Redlich-Kister
$\text{Al}_4\text{C}_3$	:	Quasi-binary, $(\text{Al},\text{Si})_4(\text{C})_3$
$\text{Al}_4\text{SiC}_4$	:	$(\text{Al})_4(\text{Si})_1(\text{C})_4$
$\text{Al}_8\text{SiC}_7$	:	$(\text{Al})_8(\text{Si})_1(\text{C})_7$

Comments:

Liquid and fcc-Al phases assumed to be ideal  
 Al and Si behave ideally in the  $\text{Al}_4\text{C}_3$  phase  
 No ternary compounds

Assessor and Date:

J. Gröbner, H. L. Lukas, and F. Aldinger.

Publication:

Calphad **20**, 2 (1996) 247-254.

Thermodynamic properties of the solution and compound phases ( $\text{J}\cdot\text{mol}^{-1}$ )

**Phase  $\text{Al}_4\text{SiC}_4$**

$$\begin{aligned} G^\circ(T) - 4.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - 4.0 \ H_C^{\circ,\text{graphite}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 380700.0 + 1233 \ T - 193.902723 \ T \cdot \ln T - 0.017517573 \ T^2 \\ + 3240000 \ T^{-1} + 9\text{E-}07 \ T^3 \end{aligned}$$

**Phase  $\text{Al}_8\text{SiC}_7$**

$$\begin{aligned} G^\circ(T) - 8.0 \ H_{\text{Al}}^{\circ,\text{fcc}-\text{Al}}(298.15 \text{ K}) - 7.0 \ H_C^{\circ,\text{graphite}}(298.15 \text{ K}) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ - 686400.0 + 2212.8 \ T - 344.434112 \ T \cdot \ln T - 0.04544832 \ T^2 \\ + 5680000 \ T^{-1} + 3.2\text{E-}06 \ T^3 \end{aligned}$$

**Table I - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Al-C-Si	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M 4
	(C)	graphite		
	(Si)	diamond	<i>cF8</i> <i>Fd</i> $\bar{3}m$	
	$\text{Al}_4\text{SiC}_4$	$\text{Al}_5\text{C}_3\text{N}$	<i>hP18</i> <i>P</i> $\bar{6}_3mc$	
	$\text{Al}_8\text{SiC}_7$		<i>hP16</i>	
	$(\text{Al},\text{Si})_4\text{C}_3$	$\text{Al}_4\text{C}_3$	<i>hP7</i> <i>R</i> $\bar{3}m$	

# System Al-Cu-Li

**Ternary Solution Phases:**

Liquid, fcc-*A1*, bcc-*A2*

**Ternary Compounds:**

AlCuLi-R, AlCuLi-T1, AlCuLi-T2, AlCuLi-TB

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A2</i>	:	Substitutional, Redlich-Kister
fcc- <i>A1</i>	:	Substitutional, Redlich-Kister
AlCuLi-R	:	Stoichiometric, (Al) <sub>0.55</sub> (Cu) <sub>0.117</sub> (Li) <sub>0.333</sub>
AlCuLi-T1	:	Stoichiometric, (Al) <sub>0.5</sub> (Cu) <sub>0.25</sub> (Li) <sub>0.25</sub>
AlCuLi-T2	:	Stoichiometric, (Al) <sub>0.57</sub> (Cu) <sub>0.11</sub> (Li) <sub>0.32</sub>
AlCuLi-TB	:	Stoichiometric, (Al) <sub>0.60</sub> (Cu) <sub>0.32</sub> (Li) <sub>0.08</sub>

**Assessor and Date:**

N. Saunders, 1994.

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase AlCuLi-R**

$$\begin{aligned}
 G^\circ(T) - 0.55 & H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.117 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) \\
 - 0.333 & H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Cu:Li}) = \\
 & - 20983.0 + 6.0 T + 0.55 \text{ GHSER}_{\text{Al}} + 0.117 \text{ GHSER}_{\text{Cu}} \\
 & + 0.333 \text{ GHSER}_{\text{Li}}
 \end{aligned}$$

**Phase AlCuLi-T1**

$$\begin{aligned}
 G^\circ(T) - 0.5 & H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.25 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) \\
 - 0.25 & H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = G(\text{Al:Cu:Li}) = \\
 & - 24560.0 + 6.0 T + 0.25 \text{ GHSER}_{\text{Al}} + 0.25 \text{ GHSER}_{\text{Cu}} \\
 & + 0.25 \text{ GHSER}_{\text{Li}}
 \end{aligned}$$

**Phase AlCuLi-T2**

$$\begin{aligned}
 G^\circ(T) = & 0.57 H_{\text{Al}}^{\text{o},\text{fcc}-\text{A}1}(298.15 \text{ K}) - 0.11 H_{\text{Cu}}^{\text{o},\text{fcc}-\text{A}1}(298.15 \text{ K}) \\
 & - 0.32 H_{\text{Li}}^{\text{o},\text{bcc}-\text{A}2}(298.15 \text{ K}) = G(\text{Al:Cu:Li}) = \\
 & - 20000.0 + 5.497 T + 0.57 \text{ GHSER}_{\text{Al}} + 0.11 \text{ GHSER}_{\text{Cu}} \\
 & + 0.32 \text{ GHSER}_{\text{Li}}
 \end{aligned}$$

**Phase AlCuLi-TB**

$$\begin{aligned}
 G^\circ(T) = & 0.60 H_{\text{Al}}^{\text{o},\text{fcc}-\text{A}1}(298.15 \text{ K}) - 0.32 H_{\text{Cu}}^{\text{o},\text{fcc}-\text{A}1}(298.15 \text{ K}) \\
 & - 0.08 H_{\text{Li}}^{\text{o},\text{bcc}-\text{A}2}(298.15 \text{ K}) = G(\text{Al:Cu:Li}) = \\
 & - 19918.0 + 4.0 T + 0.60 \text{ GHSER}_{\text{Al}} + 0.32 \text{ GHSER}_{\text{Cu}} \\
 & + 0.08 \text{ GHSER}_{\text{Li}}
 \end{aligned}$$

**Table I – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Cu-Li	(Al)	Cu	cF4 Fm $\bar{3}m$	M 4	
	(Cu)	Cu	cF4	M 4	
	(Li)	W	cl2 Im $\bar{3}m$	M 2	
	Al <sub>7.5</sub> Cu <sub>4</sub> Li	CaF <sub>2</sub>	cF12 Fm $\bar{3}m$		AlCuLi-TB
	Al <sub>2</sub> CuLi	Al <sub>2</sub> CuLi	hP12 P6/mmm		AlCuLi-T1
	Al <sub>6</sub> CuLi <sub>3</sub>				AlCuLi-T2 quasicrystal
	Al <sub>5</sub> CuLi <sub>3</sub>	Mg <sub>23</sub> (Zn,Al <sub>49</sub> )	cI162 Im $\bar{3}$		AlCuLi-TR

# System Al-Cu-Mg

**Ternary Solution Phases:**

Liquid, fcc-*A1*, hcp-*A3*

**Ternary Compounds:**

Laves-*C14*, Laves-*C15*, Laves-*C36*, Q-Phase,  
S-Phase,  $\tau$ , V-Phase

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A1</i>	:	Substitutional, Redlich-Kister
hcp- <i>A3</i>	:	Substitutional, Redlich-Kister
Laves- <i>C14</i>	:	Sublattice model, (Al,Cu,Mg)(Al,CuMg) <sub>2</sub>
Laves- <i>C15</i>	:	Sublattice model, (Al,Cu,Mg)(Al,Cu,Mg) <sub>2</sub>
Laves- <i>C36</i>	:	Sublattice model, (Al,Cu,Mg)(Al,Cu,Mg) <sub>2</sub>
$\tau$	:	Sublattice model, (Mg) <sub>26</sub> (Al, Mg) <sub>6</sub> (Al,Cu,Mg) <sub>48</sub> (Al)
Q-Phase	:	Stoichiometric, (Al) <sub>7</sub> (Cu) <sub>3</sub> (Mg) <sub>6</sub>
S-Phase	:	Stoichiometric, (Al) <sub>2</sub> (Cu)(Mg)
V-Phase	:	Stoichiometric, (Al) <sub>5</sub> (Cu) <sub>6</sub> (Mg) <sub>2</sub>

**Assessor and Date:**

T. Bühler, RWTH, Germany, (1997).

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Q-Phase**

$$\begin{aligned}
 G^\circ(T) - 7.0 & H_{\text{Al}}^{\circ,\text{fcc-}A1}(298.15 \text{ K}) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc-}A1}(298.15 \text{ K}) \\
 - 6.0 & H_{\text{Mg}}^{\circ,\text{hcp-}A3}(298.15 \text{ K}) = G(\text{Al:Cu:Mg}) = \\
 & - 221500 + 18.46 T + 7.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Cu}} \\
 & + 6.0 \text{ GHSER}_{\text{Mg}}
 \end{aligned}$$

**Phase Laves-C14**

$$L_{\text{Cu,Mg:Al}}^{0,\text{Laves-C14}} = 13011.35$$

$$L_{\text{Cu:Al,Mg}}^{0,\text{Laves-C14}} = 8000$$

$$L_{\text{Al,Mg:Cu}}^{0,\text{Laves-C14}} = 15000$$

$$L_{\text{Al:Cu,Mg}}^{0,\text{Laves-C14}} = 6599.45$$

$$L_{\text{Al,Cu:Mg}}^{0,\text{Laves-C14}} = -224000 + 2.44 \ T$$

**Phase Laves-C15**

$$L_{\text{Cu,Mg:Al}}^{0,\text{Laves-C15}} = 13011.35$$

$$L_{\text{Cu:Al,Mg}}^{0,\text{Laves-C15}} = 8000$$

$$L_{\text{Al,Mg:Cu}}^{0,\text{Laves-C15}} = 15000$$

$$L_{\text{Al:Cu,Mg}}^{0,\text{Laves-C15}} = 6599.45$$

$$L_{\text{Al,Cu:Mg}}^{0,\text{Laves-C15}} = -180000 - 1.615 \ T$$

**Phase Laves-C36**

$$L_{\text{Cu,Mg:Al}}^{0,\text{Laves-C36}} = 13011.35$$

$$L_{\text{Cu:Al,Mg}}^{0,\text{Laves-C36}} = 8000$$

$$L_{\text{Al,Mg:Cu}}^{0,\text{Laves-C36}} = 15000$$

$$L_{\text{Al:Cu,Mg}}^{0,\text{Laves-C36}} = 6599.45$$

$$L_{\text{Al,Cu:Mg}}^{0,\text{Laves-C36}} = -227442 + 14.61 \ T$$

**Phase S-Phase**

$$\begin{aligned} G^\circ(T) - 2.0 & H_{\text{Al}}^{\circ,\text{fcc-Al}}(298.15 \text{ K}) - H_{\text{Cu}}^{\circ,\text{fcc-Al}}(298.15 \text{ K}) \\ - H_{\text{Mg}}^{\circ,\text{hcp-A3}}(298.15 \text{ K}) & = G(\text{Al:Cu:Mg}) = \\ & - 63200 + 4.13 \ T + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Cu}} + \text{GHSER}_{\text{Mg}} \end{aligned}$$

**Phase V-Phase**

$$\begin{aligned}
 G^\circ(T) - 5.0 & H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 6.0 & H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) \\
 - 2.0 & H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al:Cu:Mg}) = \\
 & - 274527.45 + 13.0 & T + 5.0 \text{ GHSER}_{\text{Al}} + 6.0 \text{ GHSER}_{\text{Cu}} + 2.0 \\
 & \text{GHSER}_{\text{Mg}}
 \end{aligned}$$

**Phase  $\tau$** 

$$\begin{aligned}
 G^\circ(T) - 7.0 & H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 48.0 & H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) \\
 - 26.0 & H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Al:Cu:Al}) = \\
 & - 23000 + 440 & T + 7.0 \text{ GHSER}_{\text{Al}} + 48.0 \text{ GHSER}_{\text{Cu}} \\
 & + 26.0 \text{ GHSER}_{\text{Mg}}
 \end{aligned}$$

$$\begin{aligned}
 G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 48.0 & H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) \\
 - 32.0 & H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Mg:Cu:Al}) = \\
 & - 220000 + 440 & T + \text{GHSER}_{\text{Al}} + 48.0 \text{ GHSER}_{\text{Cu}} \\
 & + 32.0 \text{ GHSER}_{\text{Mg}}
 \end{aligned}$$

$$L_{\text{Mg:Al:Al,Cu:Al}}^{0,\tau} = - 4649190 + 2261.86 & T$$

$$L_{\text{Mg:Mg:Al,Cu:Al}}^{0,\tau} = - 4649190 + 2261.86 & T$$

$$L_{\text{Mg:Mg:Cu,Mg:Al}}^{0,\tau} = - 220000$$

**Table I – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
Al–Cu–Mg	(Al)	Cu	<i>cF</i> 4 <i>Fm</i> 3 <i>m</i>	M 4	
	(Cu)	Cu	<i>cF</i> 4 <i>Fm</i> 3 <i>m</i>	M 4	
	(Mg)	Mg	<i>hP</i> 2 <i>P</i> 63/ <i>mmc</i>	M 2	
	Laves-C14	MgZn <sub>2</sub>	<i>hP</i> 12 <i>P</i> 63/ <i>mmc</i>	Cu 2 Cu 6 Mg 4	
	Laves-C15	Cu <sub>2</sub> Mg	<i>cF</i> 24 <i>Fd</i> 3 <i>m</i>	Mg <sub>1</sub> 8 Cu <sub>2</sub> 16	
	Laves-C36	MgNi <sub>2</sub>	<i>hP</i> 24 <i>P</i> 63/ <i>mmc</i>	Cu <sub>1</sub> 6 Cu <sub>2</sub> 6 Mg <sub>1</sub> 3 Mg <sub>2</sub> 3	
	Al <sub>11</sub> Cu <sub>11</sub> Mg <sub>4</sub>	Mg <sub>2</sub> Zn <sub>11</sub>	<i>cP</i> 39 <i>Pm</i> 3		V-phase
	Al <sub>7</sub> Cu <sub>3</sub> Mg <sub>6</sub>		<i>cI</i> 96 <i>Pm</i> 3		Q-phase
	Al <sub>2</sub> CuMg	BRe <sub>3</sub>	<i>oC</i> 16 <i>Cmcm</i>	Cu 4 Mg 4 Al 8	S-phase
	(Al <sub>x</sub> Cu <sub>1-x</sub> ) <sub>49</sub> Mg <sub>32</sub>	Mg <sub>32</sub> (Al,Zn) <sub>49</sub>	<i>cI</i> 163	Al <sub>1</sub> 1 Cu <sub>1</sub> 1 Mg 6 Al <sub>2</sub> 6 Al <sub>3</sub> 8 Cu <sub>2</sub> 12	

# System Al–Cu–Si

**Ternary Solution Phases:**

Liquid, fcc-*A*1, bcc-*A*2, hcp-*A*3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister

**Assessor and Date:**

T. Bühler, RWTH, Aachen, Germany, (1997).

**Comments:**

No coefficients for the ternary solution phases.  
No ternary compounds.

**Table I – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Al-Cu-Mg	(Al)	Cu	<i>cF</i> 4 <i>Fm</i> $\bar{3}m$	M 4
	(Cu)	Cu	<i>cF</i> 4 <i>Fm</i> $\bar{3}m$	M 4
	(Si)	diamond	<i>cF</i> 8 <i>Fd</i> $\bar{3}m$	M 8

# System Al–Fe–Mn

**Ternary Solution Phases:**

Liquid, fcc-*A1*, Al<sub>8</sub>Mn<sub>5</sub>-*D8<sub>10</sub>*

**Quasi-binary phases:**

Al<sub>13</sub>Fe<sub>4</sub>, Al<sub>2</sub>Fe, Al<sub>5</sub>Fe<sub>2</sub>, Al<sub>6</sub>Mn, Al<sub>4</sub>Mn, Al<sub>12</sub>Mn

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
Al <sub>5</sub> Fe <sub>4</sub>	:	Substitutional, Redlich-Kister
fcc- <i>A1</i>	:	Substitutional, Redlich-Kister
Al <sub>8</sub> Mn <sub>5</sub> - <i>D8<sub>10</sub></i>	:	Sublattice model, (Al) <sub>12</sub> (Mn) <sub>4</sub> (Al,Fe,Mn) <sub>10</sub>
Al <sub>2</sub> Fe	:	Quasi-binary, (Al) <sub>2</sub> (Fe,Mn)
Al <sub>5</sub> Fe <sub>2</sub>	:	Quasi-binary, (Al) <sub>5</sub> (Fe,Mn) <sub>2</sub>
Al <sub>13</sub> Fe <sub>4</sub>	:	Quasi-binary, (Al) <sub>.6275</sub> (Fe,Mn) <sub>.235</sub> (Al, $\square$ ) <sub>.1375</sub>
Al <sub>4</sub> Mn	:	Quasi-binary, (Al) <sub>4</sub> (Fe,Mn)
Al <sub>6</sub> Mn	:	Quasi-binary, (Al) <sub>6</sub> (Fe,Mn)
Al <sub>12</sub> Mn	:	Quasi-binary, (Al) <sub>12</sub> Mn

**Comments:**

The data below are valid in the composition range  $x_{\text{Mn}} < 0.25$  (wt%<sub>Mn</sub> < 40.0) and  $x_{\text{Fe}} < 0.25$  (wt%<sub>Fe</sub> < 40.0)

No ternary interaction coefficients for the liquid phase. Interactions between Fe and Mn in Al<sub>12</sub>Mn, Al<sub>2</sub>Fe and Al<sub>5</sub>Fe<sub>2</sub> assumed to be ideal.

**Assessor and Date:**

Å. Jansson, and T.G. Chart (August 1997)

**Thermodynamic properties of the solution and compound phases (J·mol<sup>-1</sup>)**

**Phase fcc-*A1***

$$\begin{aligned}
 L_{\text{Al},\text{Fe},\text{Mn}:\square}^{0,\text{fcc}-\text{A1}} &= 0.000 \\
 &= \\
 L_{\text{Al},\text{Fe},\text{Mn}:\square}^{1,\text{fcc}-\text{A1}} &= -63652 \\
 &= \\
 L_{\text{Al},\text{Fe},\text{Mn}:\square}^{2,\text{fcc}-\text{A1}} &= -26753
 \end{aligned}$$

**Phase  $\text{Al}_{13}\text{Fe}_4$** 

$$L_{\text{Al:Fe,Mn:Al}}^{0,\text{Al}_{13}\text{Fe}_4} = -11987 + 6 T$$

=

$$L_{\text{Al:Fe,Mn:}\square}^{0,\text{Al}_{13}\text{Fe}_4} = -11987 + 6 T$$

**Phase  $\text{Al}_4\text{Mn}$** 

$$L_{\text{Al:Fe,Mn}}^{0,\text{Al}_4\text{Mn}} = -10000$$

**Phase  $\text{Al}_6\text{Mn}$** 

$$L_{\text{Al:Fe,Mn}}^{0,\text{Al}_6\text{Mn}} = -32753 + 21 T$$

**Phase  $\text{Al}_8\text{Mn}_5-D8_{10}$** 

$$\begin{aligned} G^\circ(T) &= 12.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 10.0 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ &\quad - 4.0 H_{\text{Mn}}^{\circ,\text{bcc}-A12,\text{para}}(298.15 \text{ K}) = \\ &\quad - 632544.85 + 12.0 \text{ GHSER}_{\text{Al}} + 10.0 \text{ GHSER}_{\text{Fe}} \\ &\quad + 4.0 \text{ GHSER}_{\text{Mn}} \\ L_{\text{Al:Mn:Al,Fe}}^{0,\text{Al}_8\text{Mn}_5-D8_{10}} &= -457832.778 \end{aligned}$$

$$L_{\text{Al:Mn:Fe,Mn}}^{0,\text{Al}_8\text{Mn}_5-D8_{10}} = -11169.158$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
Al-Fe-Mn	(Al)	Cu	<i>cF</i> 4 <i>Fm</i> $\bar{3}$ <i>m</i>	M 4	
	(Fe)	Cu	<i>cF</i> 4 <i>Fm</i> $\bar{3}$ <i>m</i>	M 4	
	(Fe)	W	<i>cI</i> 2 <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	$\alpha$ -Mn	$\alpha$ -Mn	<i>c</i> 58 <i>I</i> $\bar{4}$ <i>3m</i>		cbcc-Al
	$\beta$ -Mn	$\beta$ -Mn	<i>cP</i> 20 <i>P</i> $\bar{4}$ <i>32</i>		cub-Al3
	AlFe	CsCl	<i>cP</i> 2 <i>Pm</i> $\bar{3}$ <i>m</i>	M <sub>1</sub> 1 M <sub>2</sub> 1	
	AlFe <sub>3</sub>	BiF <sub>3</sub>	<i>cF</i> 16 <i>Fm</i> $\bar{3}$ <i>m</i>	Al 4 Fe <sub>1</sub> 4 Fe <sub>2</sub> 8	not considered
	Al <sub>2</sub> Fe	Al <sub>2</sub> Fe	<i>aP</i> 18 <i>P</i> 1		
	Al <sub>3</sub> Fe		<i>mC</i> 102 <i>C</i> 2/ <i>m</i>		designated by Al <sub>13</sub> Fe <sub>4</sub>
	Al <sub>5</sub> Fe <sub>2</sub>		<i>oC</i> * <i>Cmcm</i>		
	Al <sub>4</sub> Mn	Al <sub>4</sub> Mn	<i>oP</i> 60 <i>Pnnn</i>		
	Al <sub>6</sub> Mn	Al <sub>6</sub> Mn	<i>oC</i> 28		
	Al <sub>12</sub> Mn	Al <sub>12</sub> W	<i>cI</i> 26 <i>Im</i> $\bar{3}$		not quoted in [90Mas] metast.
	Al <sub>8</sub> Mn <sub>5</sub>	Al <sub>8</sub> Cr <sub>5</sub>	<i>hR</i> 26 <i>R</i> 3 <i>m</i>		Al <sub>8</sub> Mn <sub>5</sub> -D0 <sub>8</sub>

# System Al-Fe-Si

**Ternary Solution Phases:**

Liquid, fcc-*A*1, bcc-*A*2, bcc-*B*2

**Quasi-binary phases:**

AlFeSi- $\alpha$ , AlFeSi- $\beta$ , AlFeSi- $\gamma$ , AlFeSi- $\tau_1$ , Al<sub>13</sub>Fe<sub>4</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
Al <sub>5</sub> Fe <sub>4</sub>	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
bcc- <i>B</i> 2	:	Sublattice model, (Al,Fe,Si) <sub>0.5</sub> (Al,Fe,Si) <sub>0.5</sub> (□) <sub>3</sub>
Al <sub>13</sub> Fe <sub>4</sub>	:	Quasi-binary, (Al) <sub>0.6275</sub> (Fe) <sub>0.235</sub> (Al, Si, □) <sub>0.1375</sub>
AlFeSi- $\alpha$	:	Quasi-binary, (Al) <sub>0.6612</sub> (Fe) <sub>0.19</sub> (Si) <sub>0.0496</sub> (Al, Si) <sub>0.0992</sub>
AlFeSi- $\beta$	:	Stoichiometric, (Al) <sub>14</sub> (Fe) <sub>3</sub> (Si) <sub>3</sub>
AlFeSi- $\delta$	:	Stoichiometric, (Al) <sub>55</sub> (Fe) <sub>15</sub> (Si) <sub>30</sub>
AlFeSi- $\gamma$	:	Stoichiometric, (Al) <sub>3</sub> (Fe)(Si)
AlFeSi- $\tau_1$	:	Stoichiometric, (Al) <sub>2</sub> (Fe) <sub>2</sub> (Si)
AlFeSi- $\tau_3$	:	Stoichiometric, (Al) <sub>2</sub> (Fe)(Si)

**Comments:**

No ternary interaction coefficients for the substitutional solutions.

**Assessor and Date:**

P. Kolby, 1997.

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Al<sub>13</sub>Fe<sub>4</sub>**

$$\begin{aligned}
 G^\circ(T) = & 0.6275 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 0.235 H_{\text{Fe}}^{\circ, \text{bcc}-A2, \text{para}}(298.15 \text{ K}) \\
 & - 0.1375 H_{\text{Si}}^{\circ, \text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\
 & - 22013.336 + 0.6275 \text{ GHSER}_{\text{Al}} + 0.235 \text{ GHSER}_{\text{Fe}} + 0.1375 \text{ GHSER}_{\text{Si}}
 \end{aligned}$$

### Phase AlFeSi- $\alpha$

$$\begin{aligned} G^\circ(T) = & 0.7604 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.19 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ & - 0.0496 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si:Al}) = \\ & - 24920.609 + 5.4894 T + 0.7604 \text{ GHSER}_{\text{Al}} + 0.19 \text{ GHSER}_{\text{Fe}} + 0.0496 \text{ GHSER}_{\text{Si}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) = & 0.6612 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.19 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ & - 0.1488 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si:Si}) = \\ & - 25340.922 + 5.4894 T + 0.6612 \text{ GHSER}_{\text{Al}} + 0.19 \text{ GHSER}_{\text{Fe}} \\ & + 0.1488 \text{ GHSER}_{\text{Si}} \end{aligned}$$

### Phase AlFeSi- $\beta$

$$\begin{aligned} G^\circ(T) = & 14.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 3.0 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ & - 3.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\ & - 391310.9 + 55.84756 T + 14.0 \text{ GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Fe}} \\ & + 3.0 \text{ GHSER}_{\text{Si}} \end{aligned}$$

### Phase AlFeSi- $\delta$

$$\begin{aligned} G^\circ(T) = & 0.55 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.15 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ & - 0.3 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\ & - 14431.105 - 2.90062 T + 0.55 \text{ GHSER}_{\text{Al}} + 0.15 \text{ GHSER}_{\text{Fe}} \\ & + 0.3 \text{ GHSER}_{\text{Si}} \end{aligned}$$

### Phase AlFeSi- $\gamma$

$$\begin{aligned} G^\circ(T) = & 3.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ & - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\ & - 116929.6 + 8.399833 T + 3.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Fe}} + \text{GHSER}_{\text{Si}} \end{aligned}$$

### Phase AlFeSi- $\tau_1$

$$\begin{aligned} G^\circ(T) = & 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ & - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\ & - 153000 + 2.0 \text{ GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Fe}} + \text{GHSER}_{\text{Si}} \end{aligned}$$

### Phase AlFeSi- $\tau_3$

$$\begin{aligned} G^\circ(T) = & 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - H_{\text{Fe}}^{\circ,\text{bcc}-A2,\text{para}}(298.15 \text{ K}) \\ & - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Al:Fe:Si}) = \\ & - 99325.65 + 2.0 \text{ GHSER}_{\text{Al}} + \text{GHSER}_{\text{Fe}} + \text{GHSER}_{\text{Si}} \end{aligned}$$

**Table I - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Symbol Group	Sub-lattices	Comments
Al-Fe-Si	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Fe)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Fe)	W	$cP2$ $Im\bar{3}m$	M 2	
	(Si)	diamond	$cF8$ $Fd3m$		
	$Al_3Fe$		$mCl02$ $C2/m$		designated by $Al_{13}Fe_4$
Al-Fe-Si	$AlFeSi-\alpha$	$Fe_2Al_7Si$	$hP246$		$hP246$ and $Fe_2Al_{7.4}Si$ in [92Pet]
	$AlFeSi-\beta$	$Fe_2Al_9Si_2$	$m^{**}$		
	$AlFeSi-\gamma$		$c^{**}$		
	$AlFeSi-\delta$	$PdGa_5$	$tI24$		$FeAl_4Si_2$ in [91Vil] $FeAl_4Si_3$ in [92Pet]
	$AlFeSi-\tau_1$				$Fe_3Al_3Si_2$
	$AlFeSi-\tau_3$				$Fe_5Al_9Si_5$

# System Al-Li-Mg

**Ternary Solution Phases:**

Liquid, fcc-*A*1, bcc-*A*2, hcp-*A*3

**Ternary Compounds:**

AlLi, AlLiMg- $\tau$ , AlMg- $\beta$ , Al<sub>12</sub>Mg<sub>17</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
AlLi	:	Sublattice model, (Al,Li,Mg)(Li,Mg, $\square$ )
AlLiMg- $\tau$	:	Stoichiometric, (Al) <sub>0.53</sub> (Li) <sub>0.33</sub> (Mg) <sub>0.14</sub>
AlMg- $\beta$	:	Sublattice model, (Al) <sub>0.615</sub> (Li,Mg) <sub>0.385</sub>
Al <sub>12</sub> Mg <sub>17</sub>	:	Sublattice model, (Li,Mg) <sub>24</sub> (Al,Li,Mg) <sub>10</sub> (Al,Mg) <sub>24</sub>

**Assessor and Date:**

N. Saunders, (1994).

**Comments:**

The data below are compatible with Version I  
of the Al-Mg system.

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Liquid**

$$L_{\text{Al,Li,Mg}}^{\text{0,liquid}} = -20000$$

$$L_{\text{Al,Li,Mg}}^{\text{1,liquid}} = -15000$$

$$L_{\text{Al,Li,Mg}}^{\text{2,liquid}} = -20000$$

**Phase bcc-A2**

$$L_{\text{Al,Li,Mg};\square}^{0,\text{bcc}-A2} = -71200.0 + 50.0 \cdot T$$

**Phase fcc-A1**

$$L_{\text{Al,Li,Mg};\square}^{0,\text{fcc}-A1} = -63650.0 + 50.0 \cdot T$$

**Phase hcp-A3**

$$L_{\text{Al,Li,Mg};\square}^{0,\text{hcp}-A3} = 1.0E-4$$

$$L_{\text{Al,Li,Mg};\square}^{1,\text{hcp}-A3} = 1.0E-4$$

$$L_{\text{Al,Li,Mg};\square}^{2,\text{hcp}-A3} = -80000 + 50.0 \cdot T$$

**Phase AlLi**

$$L_{\text{Al,Mg;Li}}^{0,\text{AlLi}} = 3300.0 - 2.0 \cdot T$$

$$L_{\text{Al,Mg;Li,Mg}}^{0,\text{AlLi}} = -43460.0 + 60.0 \cdot T$$

$$L_{\text{Al;Li,Mg}}^{0,\text{AlLi}} = -25000.0 + 10.0 \cdot T$$

**Phase AlMg- $\beta$** 

$$L_{\text{Al;Li,Mg}}^{0,\text{AlMg-}\beta} = -4250$$

**Phase AlLiMg- $\tau$** 

$$\begin{aligned} G^\circ(T) - 0.53 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.33 \cdot H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) \\ - 0.14 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al:Li:Mg}) = \\ - 15500 + 23.93 \cdot T - 3.0 \cdot T \cdot \ln T + 0.53 \cdot \text{GHSER}_{\text{Al}} \\ + 0.33 \cdot \text{GHSER}_{\text{Li}} + 0.14 \cdot \text{GHSER}_{\text{Mg}} \end{aligned}$$

**Phase Al<sub>12</sub>Mg<sub>17</sub>**

$$\begin{aligned} G^\circ(T) - 24.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 10.0 \cdot H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) \\ - 24.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Mg:Li:Al}) = \\ - 610000 + 125 \cdot T + 24.0 \cdot \text{GHSER}_{\text{Al}} + 10.0 \cdot \text{GHSER}_{\text{Li}} \\ + 24.0 \cdot \text{GHSER}_{\text{Mg}} \\ G^\circ(T) - 24.0 \cdot H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 24.0 \cdot H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) \\ - 10.0 \cdot H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Li:Mg:Al}) = \\ - 625000 + 269 \cdot T + 24.0 \cdot \text{GHSER}_{\text{Al}} + 24.0 \cdot \text{GHSER}_{\text{Li}} \\ + 10.0 \cdot \text{GHSER}_{\text{Mg}} \end{aligned}$$

$$\begin{aligned}
 G^\circ(T) = & 24.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 10.0 H_{\text{Li}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) \\
 - & 24.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Li:Al:Mg}) = \\
 & 1.0E-4 + 24.0 \text{ GHSER}_{\text{Al}} + 10.0 \text{ GHSER}_{\text{Li}} + 24.0 \text{ GHSER}_{\text{Mg}} \\
 L_{\text{Li,Mg:Al:Al}}^{0,\text{Al}_1\text{Mg}_{17}} & = -220000 \\
 L_{\text{Mg:Al,Li:Al}}^{0,\text{Al}_1\text{Mg}_{17}} & = -50000
 \end{aligned}$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Li-Mg	(Al)	Cu	<i>cF</i> 4 <i>Fm</i> 3 <i>m</i>	M 4	designated as Al <sub>12</sub> Mg <sub>17</sub>
	(Li)	W	<i>cI</i> 2 <i>Im</i> 3 <i>m</i>	M 2	
	(Mg)	Mg	<i>hP</i> 2 <i>P</i> 6 <sub>3</sub> / <i>mmc</i>	M 2	
	AlLi	NaTl	<i>cF</i> 16 <i>Fd</i> 3 <i>m</i>	M <sub>1</sub> 8 M <sub>2</sub> 8	
	AlMg- $\gamma$	$\alpha$ -Mn cbcc-A12	<i>cI</i> 58 <i>I</i> 43 <i>m</i>	Al 24 Mg <sub>1</sub> 2 Mg <sub>2</sub> 8 Mg <sub>3</sub> 24	
	Al <sub>3</sub> Mg <sub>2</sub>	Cd <sub>2</sub> Na	<i>cF</i> 112 <i>Fd</i> 3 <i>m</i>		<i>cF</i> 1832 in [91Vil] designated as AlMg- $\beta$
	Al <sub>2</sub> LiMg		<i>c</i> * 456		AlLiMg- $\tau$

# System Al-Mg-Mn

**Ternary Solution Phases:**

Liquid, fcc-*A*1

**Ternary Compound:**

AlMgMn-T

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
AlMgMn-T	:	Stoichiometric, (Al) <sub>18</sub> (Mg) <sub>3</sub> (Mn) <sub>2</sub>

**Assessor and Date:**

I. Ansara (1994).

**Comments:**

The data are valid only in the Al-rich corner.  
Very little information on the phase relationships  
is known

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase AlMgMn-T**

$$\begin{aligned}
 G^\circ(T) = & 18.0 \ H_{\text{Al}}^{\circ, \text{fcc}-\text{A}1}(298.15 \text{ K}) - 3.0 \ H_{\text{Mg}}^{\circ, \text{hcp}-\text{A}3}(298.15 \text{ K}) \\
 & - 2.0 \ H_{\text{Mn}}^{\circ, \text{bcc}-\text{A}12, \text{para}}(298.15 \text{ K}) = G(\text{Al:Mg:Mn}) = \\
 & - 206402.0 + 11.85 \ T + 18.0 \ \text{GHSER}_{\text{Al}} + 3.0 \ \text{GHSER}_{\text{Mg}} \\
 & + 2.0 \ \text{GHSER}_{\text{Mn}}
 \end{aligned}$$

**Table I - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
Al-Mg-Mn	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M 4	
	(Mg)	Mg	<i>hP2</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>	M 2	
	$\alpha$ -Mn	$\alpha$ -Mn	<i>c58</i> <i>I</i> $\bar{4}3m$		cbcc-Al
	$\beta$ -Mn	$\beta$ -Mn	<i>cP20</i> <i>P</i> <sub>4</sub> $\bar{3}2$		cub-A13
	$\gamma$ -Mn	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M 4	
	$\delta$ -Mn	W	<i>cI2</i> <i>I</i> $m\bar{3}m$	M 2	
	$\text{Al}_{18}\text{Mg}_3\text{Mn}_2$	$\text{Al}_{18}\text{Cr}_2\text{Mg}_3$	<i>cF184</i> <i>Fd</i> $\bar{3}m$		designated as AlMgMn-T

# System Al–Mg–Si

**Ternary Solution Phases:**

Liquid, fcc-*A*1, hcp-*A*3, diamond

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
diamond	:	Substitutional, Redlich-Kister

**Assessor and Date:**

H. L. Lukas (1996)

**Comments:**

No ternary compounds or quasi-binary phases

**Publication:**

H. Feufel, T. Gödecke, H. L. Lukas, and F. Sommer,  
J. Alloys Comp. **247**, 31–42 (1997).

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Liquid**

$$L_{\text{Al,Mg,Si}}^{0,\text{liquid}} = 4125.86 - 0.51573 \ T$$

$$L_{\text{Al,Mg,Si}}^{1,\text{liquid}} = -47961.64 + 5.9952 \ T$$

$$L_{\text{Al,Mg,Si}}^{2,\text{liquid}} = 25813.8 - 3.22672 \ T$$

**Table I - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Mg-Si	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>	M 4	
	(Mg)	Mg	<i>hP2</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>	M 2	
	(Si)	diamond	<i>cF8</i> <i>Fd</i> $\bar{3}$ <i>m</i>		

# System Al-Mg-Zn

**Ternary Solution Phases:**

Liquid, fcc-*A1*, hcp-*A3*, hcp-*Zn*,  $\tau$ ,  $\varphi$

**Compounds:**

AlMg- $\beta$ , AlMg- $\gamma$ , Laves-*C14*

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A1</i>	:	Substitutional, Redlich-Kister
hcp- <i>A3</i>	:	Substitutional, Redlich-Kister
hcp- <i>Zn</i>	:	Substitutional, Redlich-Kister
AlMg- $\beta$	:	Sublattice model, $(\text{Mg})_{89}(\text{Al}, \text{Zn})_{140}$
AlMg- $\gamma$	:	Sublattice model, $(\text{Al}, \text{Mg}, \text{Zn})_{12}(\text{Al}, \text{Mg}, \text{Zn})_{12}(\text{Mg})_5$
Laves- <i>C14</i>	:	Sublattice model, $(\text{Al}, \text{Mg}, \text{Zn})(\text{Al}, \text{Mg}, \text{Zn})_2$
$\tau$	:	Sublattice model, $(\text{Mg})_{26}(\text{Al}, \text{Mg})_6(\text{Al}, \text{Mg}, \text{Zn})_{48}(\text{Al})$
$\varphi$	:	Sublattice model, $(\text{Mg})_6(\text{Al}, \text{Zn})_5$

**Assessor and Date:**

P. Liang, H. L. Lukas (1967)

**Publication:**

P. Liang, T. Tarfa, J. A. Robinson, S. Wagner, P. Ochin, M. G. Harmelin, H. J. Seifert, H. L. Lukas, G. Effenberg, F. Aldinger

Thermochimica Acta, **314**, 1-2, 87-110 (1998).

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)****Phase Liquid**

$$L_{\text{Al,Mg,Zn}}^{0,\text{liquid}} = -11475 + 11 T$$

$$L_{\text{Al,Mg,Zn}}^{1,\text{liquid}} = -11475 + 11 T$$

$$L_{\text{Al,Mg,Zn}}^{2,\text{liquid}} = -11475 + 11 T$$

**Phase hcp-A3**

$$L_{\text{Al,Mg,Zn}}^{0,\text{hcp-A3}} = 1.0\text{E-}4$$

$$L_{\text{Al,Mg,Zn}}^{1,\text{hcp-A3}} = 1.0\text{E-}4$$

$$L_{\text{Al,Mg,Zn}}^{2,\text{hcp-A3}} = 1.0\text{E-}4$$

**Phase hcp-Zn**

$$L_{\text{Al,Mg,Zn}}^{0,\text{hcp-Zn}} = 1.0\text{E-}4$$

$$L_{\text{Al,Mg,Zn}}^{1,\text{hcp-Zn}} = 1.0\text{E-}4$$

$$L_{\text{Al,Mg,Zn}}^{2,\text{hcp-Zn}} = 1.0\text{E-}4$$

**Phase Laves-C14**

$$L_{\text{Mg,Zn:Al}}^{0,\text{Laves-C14}} = 35000$$

$$L_{\text{Zn:Al,Mg}}^{0,\text{Laves-C14}} = 15000$$

$$L_{\text{Al,Zn:Mg}}^{0,\text{Laves-C14}} = -7500 - 18 T$$

$$L_{\text{Al:Mg,Zn}}^{0,\text{Laves-C14}} = 8000$$

$$L_{\text{Al,Mg:Zn}}^{0,\text{Laves-C14}} = 8000$$

**Phase AlMg- $\beta$** 

$$L_{\text{Al,Mg,Zn}}^{0,\text{AlMg-}\beta} = -1717500 + 343.5 T$$

**Phase AlMg- $\gamma$** 

$$L_{\text{Mg:Mg:Al:Zn}}^{0,\text{AlMg-}\gamma} = -116000 + 58 T$$

$$L_{\text{Mg:Zn:Al:Mg}}^{0,\text{AlMg-}\gamma} = 113100 - 14.5 T$$

**Phase  $\varphi$** 

$$L_{\text{Mg:Mg:Al,Zn}}^{0,\varphi} = -23100 + 11 T$$

**Phase  $\tau$** 

$$\begin{aligned} G^\circ(T) - 7.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 26.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) \\ - 48.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Mg:Al:Zn:Al}) = \\ - 832680 + 162 T + 7.0 \text{ GHSER}_{\text{Al}} + 26.0 \text{ GHSER}_{\text{Mg}} \\ + 48.0 \text{ GHSER}_{\text{Zn}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 32.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) \\ - 48.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) = G(\text{Mg:Mg:Zn:Al}) = \\ - 811620 + 162 T + \text{GHSER}_{\text{Al}} + 32.0 \text{ GHSER}_{\text{Mg}} + 48.0 \text{ GHSER}_{\text{Zn}} \end{aligned}$$

$$L_{\text{Mg:Al:Al,Zn:Al}}^{0,\tau} = -16200 + 243 T$$

$$L_{\text{Mg:Mg:Al,Zn:Al}}^{0,\tau} = -105300 + 243 T$$

$$L_{\text{Mg:Al:Mg,Zn:Al}}^{0,\tau} = 243000 + 81 T$$

$$L_{\text{Mg:Mg:Mg,Zn:Al}}^{0,\tau} = 243000 + 81 T$$

**Table I – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Cu-Mg	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M 4	
	(Mg)	Mg	<i>hP2</i> <i>P6</i> $_3/mmc$	M 2	
	Laves- <i>C14</i>	MgZn <sub>2</sub>	<i>hP12</i> <i>P6</i> $_3/mmc$	Cu 2 Cu 6 Mg 4	
	Al <sub>3</sub> Mg <sub>2</sub>	Cd <sub>2</sub> Na	<i>cF112</i> <i>Fd</i> $\bar{3}m$		<i>cF1832</i> in [91Vil] designated as AlMg- $\beta$
	AlMg- $\gamma$	$\alpha$ -Mn	<i>cI58</i> <i>I</i> $\bar{4}3m$	Al 24 Mg <sub>1</sub> 2	designated as Al <sub>12</sub> Mg <sub>17</sub>
	$\Phi$		o*		
	$\tau$	Mg <sub>32</sub> (Al,Zn) <sub>49</sub>	<i>cI162</i> <i>Im</i> $\bar{3}$		

# System Al–Mn–Si

**Ternary Solution Phases:**

Liquid, fcc-*A*1, Al<sub>8</sub>Mn<sub>5</sub>-*D*8<sub>10</sub>

**Quasi-binary phases:**

AlMnSi- $\alpha$ , AlMnSi- $\beta$

**Compounds:**

AlMnSi- $\delta$

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
Al <sub>8</sub> Mn <sub>5</sub> - <i>D</i> 8 <sub>10</sub>	:	Sublattice model, (Al,Si) <sub>12</sub> (Mn) <sub>4</sub> (Al,Mn) <sub>10</sub>
AlMnSi- $\alpha$	:	Quasi-binary, (Al) <sub>16</sub> (Mn) <sub>4</sub> (Si)(Al,Si) <sub>2</sub>
AlMnSi- $\beta$	:	Quasi-binary, (Al) <sub>15</sub> (Si)(Al,Si) <sub>4</sub> (Mn) <sub>6</sub>
AlMnSi- $\delta$	:	Stoichiometric, (Al) <sub>2</sub> (Mn)(Si) <sub>3</sub>

**Comments:**

The data below are valid in the composition range x<sub>Si</sub> < 0.2 and x<sub>Mn</sub> < 0.05

The fcc-*A*1 phase is assumed to be ideal

**Assessor and Date:**

P. Kolby, M.H. Rand, and T.G. Chart, 1997.

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Liquid**

$$L_{\text{Al},\text{Mn},\text{Si}}^{0,\text{Liquid}} = -37000$$

**Phase Al<sub>8</sub>Mn<sub>5</sub>-*D*8<sub>10</sub>**

$$\begin{aligned} G^\circ(T) - 10.0 & H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 4.0 H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A}12,\text{para}}(298.15 \text{ K}) \\ - 12.0 & H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ & 10.0 \text{ GHSER}_{\text{Al}} + 4.0 \text{ GHSER}_{\text{Mn}} + 12.0 \text{ GHSER}_{\text{Si}} \end{aligned}$$

### Phase AlMnSi- $\alpha$

$$\begin{aligned}
 G^\circ(T) - 18.0 & H_{\text{Al}}^{\text{o},\text{fcc}-\text{A}1}(298.15 \text{ K}) - 4.0 & H_{\text{Mn}}^{\text{o},\text{cbcc}-\text{A}12,\text{para}}(298.15 \text{ K}) \\
 - H_{\text{Si}}^{\text{o},\text{diamond}}(298.15 \text{ K}) = & - 755772 + 3544.43 & T - 573.95 & T \cdot \ln T \\
 & - 0.114419 & T^2 + 9.70013\text{E-}06 & T^3 + 3716760 & T^{-1} \\
 G^\circ(T) - 16.0 & H_{\text{Al}}^{\text{o},\text{fcc}-\text{A}1}(298.15 \text{ K}) - 4.0 & H_{\text{Mn}}^{\text{o},\text{cbcc}-\text{A}12,\text{para}}(298.15 \text{ K}) \\
 - 3.0 & H_{\text{Si}}^{\text{o},\text{diamond}}(298.15 \text{ K}) = & - 698911 + 2958.7 & T - 493.78 & T \cdot \ln T \\
 & - 0.17905 & T^2 + 1.87237\text{E-}05 & T^3 + 1822810 & T^{-1} \\
 L_{\text{Al:Mn:Si:Al,Si}}^{0,\text{AlMnSi-}\alpha} & = 0.0001
 \end{aligned}$$

### Phase AlMnSi- $\beta$

$$\begin{aligned}
 G^\circ(T) - 19.0 & H_{\text{Al}}^{\text{o},\text{fcc}-\text{A}1}(298.15 \text{ K}) - 6.0 & H_{\text{Mn}}^{\text{o},\text{cbcc}-\text{A}12,\text{para}}(298.15 \text{ K}) \\
 - H_{\text{Si}}^{\text{o},\text{diamond}}(298.15 \text{ K}) = & - 880648 + 3451.04 & T - 572.75 & T \cdot \ln T \\
 & - 0.201935 & T^2 + 2.0\text{E-}05 & T^3 + 2184750 & T^{-1} \\
 G^\circ(T) - 15.0 & H_{\text{Al}}^{\text{o},\text{fcc}-\text{A}1}(298.15 \text{ K}) - 6.0 & H_{\text{Mn}}^{\text{o},\text{cbcc}-\text{A}12,\text{para}}(298.15 \text{ K}) \\
 - 5.0 & H_{\text{Si}}^{\text{o},\text{diamond}}(298.15 \text{ K}) = & - 779980 + 3451.04 & T - 593.657 & T \cdot \ln T \\
 & - 0.16164 & T^2 + 1.35092\text{E-}05 & T^3 + 2946120 & T^{-1} \\
 L_{\text{Al:Si:Al,Si:Mn}}^{0,\text{AlMnSi-}\beta} & = 0.0001
 \end{aligned}$$

### Phase AlMnSi- $\delta$

$$\begin{aligned}
 G^\circ(T) - 2.0 & H_{\text{Al}}^{\text{o},\text{fcc}-\text{A}1}(298.15 \text{ K}) - 3.0 & H_{\text{Mn}}^{\text{o},\text{cbcc}-\text{A}12,\text{para}}(298.15 \text{ K}) \\
 - H_{\text{Si}}^{\text{o},\text{diamond}}(298.15 \text{ K}) = & - 70000 - 2 & T + 2.0 & \text{GHSER}_{\text{Al}} + 3.0 & \text{GHSER}_{\text{Mn}} \\
 & + \text{GHSER}_{\text{Si}}
 \end{aligned}$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol Group	Sub-lattices	Comments
Al-Mn-Si	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Mg)	Mg	$hP2$ $P6_3/mmc$	M 2	
	$\alpha$ -Mn	$\alpha$ -Mn	$c58$ $I\bar{4}3m$		cbcc- <i>A1</i>
	$\beta$ -Mn	$\beta$ -Mn	$cP20$ $P4_132$		cub- <i>A13</i>
	$\gamma$ -Mn	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	$\delta$ -Mn	W	$cI2$ $Im\bar{3}m$	M 2	
	(Si)	diamond	$cF8$ $Fd\bar{3}m$		
	AlMnSi- $\alpha$	Al <sub>9</sub> Mn <sub>2</sub> Si	$cP138$ $Pm\bar{3}$		
	AlMnSi- $\beta$	Al <sub>10</sub> Mn <sub>3</sub>	$hP26$ $P6_3/mmc$		
	AlMnSi- $\delta$		$hP100$		quoted in [93Pet]
	Al <sub>8</sub> Mn <sub>5</sub> -D8 <sub>10</sub>	Al <sub>8</sub> Cr <sub>5</sub>	$hR26$ $R\bar{3}m$		

# System Al–Mo–Ti

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1, bcc-*B*2, hcp-*A*3

**Ternary Compounds:**

AlM-*D*0<sub>19</sub>, AlM-*D*0<sub>22</sub>, AlTi-*L*1<sub>0</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
bcc- <i>B</i> 2	:	Sublattice model, (Al,Mo,Ti) <sub>0.5</sub> (Al,Mo,Ti) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc- <i>B</i> 2 takes into account the ordering reaction bcc- <i>A</i> 2 ⇌ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Al,Mo,Ti) <sub>3</sub> (Al,Mo,Ti)(□) <sub>0.5</sub>
AlM- <i>D</i> 0 <sub>22</sub>	:	Sublattice model, (Al,Mo,Ti) <sub>3</sub> (Al,Mo,Ti)
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Al,Mo,Ti)(Al,Mo,Ti)

**Assessor and Date:**

N. Saunders, 1996

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase AlM-*D*0<sub>19</sub>**

$$L_{\text{Mo:Al,Ti:}\square}^{0,\text{AlM-}D0_{19}} = 10656 - 1.332 \ T$$

$$L_{\text{Al,Ti:Mo:}\square}^{0,\text{AlM-}D0_{19}} = 32000 - 4 \ T$$

**Phase AlM-D0<sub>22</sub>**

$$L_{\text{Al:Mo,Ti}}^{0,\text{AlM}-D0_{22}} = -212000 + 120 \cdot T$$

**Phase AlTi-L1<sub>0</sub>**

$$L_{\text{Mo,Ti:Al}}^{0,\text{AlTi}-L1_0} = L_{\text{Al:Mo,Ti}}^{0,\text{AlTi}-L1_0} = -13000$$

$$L_{\text{Mo,Ti:Al}}^{1,\text{AlTi}-L1_0} = L_{\text{Al:Mo,Ti}}^{1,\text{AlTi}-L1_0} = 1.0E-4$$

$$L_{\text{Mo,Ti:Al}}^{2,\text{AlTi}-L1_0} = L_{\text{Al:Mo,Ti}}^{2,\text{AlTi}-L1_0} = -13000$$

$$L_{\text{Mo:Al,Ti}}^{0,\text{AlTi}-L1_0} = L_{\text{Al,Ti:Mo}}^{0,\text{AlTi}-L1_0} = -15134 - 2.36 \cdot T$$

**Phase bcc-A2**

$$L_{\text{Al,Mo,Ti:}\square}^{1,\text{bcc}-A2} = 0$$

$$L_{\text{Al,Mo,Ti:}\square}^{2,\text{bcc}-A2} = 0$$

$$L_{\text{Al,Mo,Ti:}\square}^{3,\text{bcc}-A2} = 0$$

**Phase bcc-B2**

$$L_{\text{Mo,Ti:}\square}^{0,\text{bcc}-B2} = L_{\text{Al:Mo,Ti:}\square}^{0,\text{bcc}-B2} = -5000$$

$$L_{\text{Mo:Al,Ti:}\square}^{0,\text{bcc}-B2} = L_{\text{Al,Ti:Mo:}\square}^{0,\text{bcc}-B2} = 8750 - 1.25 \cdot T$$

$$L_{\text{Ti:Al,Mo:}\square}^{0,\text{bcc}-B2} = L_{\text{Al,Mo,Ti:}\square}^{0,\text{bcc}-B2} = 14100 - 2 \cdot T$$

**Phase bcc-A2**

$$L_{\text{Al,Mo,Ti:}\square}^{0,\text{bcc}-A2} = 0$$

$$L_{\text{Al,Mo,Ti:}\square}^{1,\text{bcc}-A2} = 0$$

$$L_{\text{Al,Mo,Ti:}\square}^{2,\text{bcc}-A2} = 0$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Mo-Ti	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>	M 4	
	(Mo)	W	<i>cI2</i> <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	bcc- <i>B2</i>	CsCl	<i>cP2</i> <i>Pm</i> $\bar{3}$ <i>m</i>	M <sub>1</sub> 1 M <sub>2</sub> 1	
	(Ti)	Mg	<i>hP2</i> <i>P6</i> <sub>3</sub> /mmc	M 2	
	(Ti)	W	<i>cI2</i> <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	AlTi	AuCu	<i>tP4</i> <i>P</i> <sub>4</sub> /mmm	Al 2 Ti <sub>1</sub> 1 Ti <sub>2</sub> 1	AlTi- <i>L1</i> <sub>0</sub>
	AlTi <sub>3</sub>	Ni <sub>3</sub> Sn	<i>hP8</i> <i>P6</i> <sub>3</sub> /mmc		AlM- <i>D0</i> <sub>19</sub>
	Al <sub>3</sub> Ti	Al <sub>3</sub> Ti	<i>tI8</i> <i>I</i> <sub>4</sub> /mmm	Al <sub>1</sub> 2 Al <sub>2</sub> 4 Ti 2	AlM- <i>D0</i> <sub>22</sub>

# System Al-N-Ti

**Ternary Solution Phases:**

Liquid, bcc-*A2*, hcp-*A3*

**Ternary Compounds:**

AlNTi<sub>2</sub>, AlNTi<sub>3</sub>, Al<sub>2</sub>N<sub>2</sub>Ti<sub>3</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A2</i>	:	Substitutional, Redlich-Kister
hcp- <i>A3</i>	:	Substitutional, Redlich-Kister
AlNTi <sub>2</sub>	:	Stoichiometric, (Al)(Ti) <sub>2</sub> (N) <sub>0.82</sub>
AlNTi <sub>3</sub>	:	Stoichiometric, (Al)(Ti) <sub>3</sub> (N) <sub>0.56</sub>
Al <sub>2</sub> N <sub>2</sub> Ti <sub>3</sub>	:	Stoichiometric, (Al) <sub>2</sub> (Ti) <sub>3</sub> (N) <sub>2</sub>

**Assessor and Date:**

K. Zeng, and R. Schmid-Fetzer, Univ. Clausthal,  
Germany, (1996).

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase bcc-*A2***

$$L_{\text{Al,Ti:N}}^{0,\text{bcc-}A2} = -200000$$

$$L_{\text{Al,Ti:N,O}}^{0,\text{bcc-}A2} = -200000$$

**Phase hcp-*A3***

$$L_{\text{Al,Ti:N}}^{0,\text{hcp-}A3} = -100000$$

$$L_{\text{Al,Ti:N,O}}^{0,\text{hcp-}A3} = -80000$$

$$L_{\text{Al,Ti:N,O}}^{1,\text{hcp-}A3} = -37300 + 100 T$$

**Phase AlNTi<sub>2</sub>**

$$\begin{aligned}
 G^\circ(T) = & H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.82 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) \\
 - 2.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = & -389592 + 104 T + \text{GHSER}_{\text{Al}} + 2.0 \text{ GHSER}_{\text{Ti}} + 0.82 \text{ GHSER}_{0.5\text{N}_2}
 \end{aligned}$$

**Phase AlNTi<sub>3</sub>**

$$\begin{aligned}
 G^\circ(T) = & H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 0.56 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) \\
 - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = & -349502.5 + 92.5 T + \text{GHSER}_{\text{Al}} + 3.0 \text{ GHSER}_{\text{Ti}} + 0.56 \text{ GHSER}_{0.5\text{N}_2}
 \end{aligned}$$

**Phase Al<sub>2</sub>N<sub>2</sub>Ti<sub>3</sub>**

$$\begin{aligned}
 G^\circ(T) = & 2.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 H_{0.5\text{N}_2}^{\circ,\text{gas}}(298.15 \text{ K}) \\
 - 3.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = & 3405331.05 - 5217.37371 T + 1.75061514 T^2 + 2.0 \text{ GHSER}_{\text{Al}} \\
 & + 3.0 \text{ GHSER}_{\text{Ti}} + 2.0 \text{ GHSER}_{0.5\text{N}_2}
 \end{aligned}$$

**Table I:a - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Symbol Group	Sub-lattices
Al-N-Ti	(Al)	Cu	cF4 <i>Fm</i> 3 <i>m</i>	M 4
	(Ti)	Mg	hP2 <i>P</i> 6 <sub>3</sub> / <i>mmc</i>	M 2
	(Ti)	W	cI2 <i>I</i> m3 <i>m</i>	M 2
	AlNTi <sub>2</sub>	AlCr <sub>2</sub>	hP8 <i>P</i> 6 <sub>3</sub> / <i>mmc</i>	
	AlNTi <sub>3</sub>	CaO <sub>3</sub> Ti	cP5 <i>P</i> m3 <i>m</i>	M <sub>1</sub> 1 M <sub>2</sub> 1 Ti 3

**Table I:b - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Group	Sub-lattices
	$\text{Al}_2\text{N}_2\text{Ti}_3$	$\text{Al}_2\text{N}_2\text{Ti}_3$	$hP22$ $P31c$	$\begin{array}{ll}\text{Al}_1 & 2 \\ \text{Ti}_1 & 2 \\ \text{Al}_2 & 2 \\ \text{N}_1 & 2 \\ \text{N}_2 & 2 \\ \text{N}_3 & 2 \\ \text{N}_4 & 2 \\ \text{Ti}_2 & 2 \\ \text{Ti}_3 & 2 \\ \text{Ti}_4 & 2 \\ \text{Ti}_5 & 2\end{array}$

## System Al–Nb–Ti

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1, bcc-*B*2, hcp-*A*3

**Ternary Compounds:**

AlM-*D*0<sub>19</sub>, AlM-*D*0<sub>22</sub>, AlTi-*L*1<sub>0</sub>,  $\sigma$ , AlNb<sub>3</sub>-*A*15

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
bcc- <i>B</i> 2	:	Sublattice model, (Al,Nb,Ti) <sub>0.5</sub> (Al,Nb,Ti) <sub>0.5</sub> (□) <sub>3</sub>
bcc- <i>B</i> 2	:	Sublattice model, (Al,Mo,Ti) <sub>0.5</sub> (Al,Mo,Ti) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc- <i>B</i> 2 takes into account the ordering reaction bcc- <i>A</i> 2 $\rightleftharpoons$ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlNb <sub>3</sub> - <i>A</i> 15	:	Sublattice model, (Al,Nb)(Nb) <sub>3</sub>
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Al,Nb,Ti) <sub>3</sub> (Al,Nb,Ti)(□) <sub>0.5</sub>
AlM- <i>D</i> 0 <sub>22</sub>	:	Sublattice model, (Al,Nb,Ti) <sub>3</sub> (Al,Nb,Ti)
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Al,Nb,Ti)(Al,Nb,Ti)
$\sigma$	:	Sublattice model, (Al) <sub>8</sub> (Nb,Ti) <sub>4</sub> (Al,Nb,Ti) <sub>18</sub>

**Assessor and Date:**

N. Saunders, 1996

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase AlM-*D*0<sub>22</sub>**

$$L_{\text{Al:Nb,Ti}}^{\text{0,AlM-}D\text{022}} = 20000$$

**Phase AlM-D0<sub>19</sub>**

$$L_{\text{Nb:Al,Ti:}\square}^{0,\text{AlM}-D0_{19}} = 10656 - 1.333 T$$

$$L_{\text{Ti:Al,Nb:}\square}^{0,\text{AlM}-D0_{19}} = 4000$$

$$L_{\text{Al,Ti:Nb:}\square}^{0,\text{AlM}-D0_{19}} = 32000 - T$$

$$L_{\text{Al,Nb:Ti:}\square}^{0,\text{AlM}-D0_{19}} = 12000$$

**Phase AlTi-L1<sub>0</sub>**

$$L_{\text{Al,Nb,Ti:Al}}^{0,\text{AlTi}-L1_0} = -45000$$

$$L_{\text{Al:Al,Nb,Ti}}^{0,\text{AlTi}-L1_0} = -45000$$

$$L_{\text{Nb,Ti:Al}}^{0,\text{AlTi}-L1_0} = -18076 + 12 T$$

$$L_{\text{Nb:Al,Ti}}^{0,\text{AlTi}-L1_0} = -15134 - 2.36 T$$

$$L_{\text{Ti:Al,Nb}}^{0,\text{AlTi}-L1_0} = -37600$$

$$L_{\text{Al,Ti:Nb}}^{0,\text{AlTi}-L1_0} = -15134 - 2.36 T$$

$$L_{\text{Al:Nb,Ti}}^{0,\text{AlTi}-L1_0} = -18076 + 12 T$$

$$L_{\text{Al,Nb:Ti}}^{0,\text{AlTi}-L1_0} = -37600$$

**Phase bcc-A2**

$$L_{\text{Al,Nb,Ti:}\square}^{0,\text{bcc}-A2} = 0$$

$$L_{\text{Al,Nb,Ti:}\square}^{1,\text{bcc}-A2} = 0$$

$$L_{\text{Al,Nb,Ti:}\square}^{2,\text{bcc}-A2} = 0$$

**Phase bcc-B2**

$$G_{\text{Al:Nb:}\square}^* = -8650 + T$$

$$G_{\text{Al:Ti:}\square}^* = -8750 + 1.35 T$$

$$G_{\text{Nb,Ti:}\square}^* = 5500$$

$$L_{\text{Nb}, \text{Ti}: \text{Al}: \square}^{0, \text{bcc}-B2} = L_{\text{Al}: \text{Nb}, \text{Ti}: \text{Al}: \square}^{0, \text{bcc}-B2} = -G_{\text{Nb}, \text{Ti}: \square}^*$$

$$L_{\text{Nb}: \text{Al}, \text{Ti}: \square}^{0, \text{bcc}-B2} = L_{\text{Al}, \text{Ti}: \text{Nb}: \square}^{0, \text{bcc}-B2} = -G_{\text{Al}: \text{Ti}: \square}^*$$

$$L_{\text{Ti}: \text{Al}, \text{Nb}: \square}^{0, \text{bcc}-B2} = L_{\text{Al}, \text{Nb}: \text{Ti}: \square}^{0, \text{bcc}-B2} = -G_{\text{Al}: \text{Nb}: \square}^*$$

### Phase bcc-A2

$$L_{\text{Al}, \text{Nb}, \text{Ti}: \square}^{0, \text{bcc}-A2} = 0$$

$$L_{\text{Al}, \text{Nb}, \text{Ti}: \square}^{1, \text{bcc}-A2} = 0$$

$$L_{\text{Al}, \text{Nb}, \text{Ti}: \square}^{2, \text{bcc}-A2} = 0$$

### Phase hcp-A3

$$L_{\text{Al}, \text{Nb}, \text{Ti}: \square}^{0, \text{hcp}-A3} = -10 \ T$$

### Phase $\sigma$

$$\begin{aligned} G^\circ(T) - 8.0 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 18.0 H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) \\ - 4.0 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al}: \text{Ti}: \text{Nb}) = \\ - 660000 + 79.5 \ T + 8.0 \text{ GHSER}_{\text{Al}} + 18.0 \text{ GHSER}_{\text{Nb}} \\ + 4.0 \text{ GHSER}_{\text{Ti}} \end{aligned}$$

$$\begin{aligned} G^\circ(T) - 8.0 H_{\text{Al}}^{\circ, \text{fcc}-A1}(298.15 \text{ K}) - 4.0 H_{\text{Nb}}^{\circ, \text{bcc}-A2}(298.15 \text{ K}) \\ - 18.0 H_{\text{Ti}}^{\circ, \text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al}: \text{Nb}: \text{Ti}) = \\ - 690000 + 148.5 \ T + 8.0 \text{ GHSER}_{\text{Al}} + 4.0 \text{ GHSER}_{\text{Nb}} \\ + 18.0 \text{ GHSER}_{\text{Ti}} \end{aligned}$$

$$L_{\text{Al}: \text{Nb}: \text{Al}, \text{Ti}: \square}^{0, \sigma} = -1680000 + 510 \ T$$

$$L_{\text{Al}: \text{Ti}: \text{Al}, \text{Nb}: \square}^{0, \sigma} = -990000 + 270 \ T$$

$$L_{\text{Al}: \text{Ti}: \text{Al}, \text{Nb}: \square}^{1, \sigma} = 420000$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Symbol Group	Sub-lattices	Comments
Al-Nb-Ti	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>	M 4	
	(Nb)	W	<i>cI2</i> <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	bcc- <i>B2</i>	CsCl	<i>cP2</i> <i>Pm</i> $\bar{3}$ <i>m</i>	M <sub>1</sub> 1 M <sub>2</sub> 1	
	(Ti)	Mg	<i>hP2</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>	M 2	
	(Ti)	W	<i>cI2</i> <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	AlTi	AuCu	<i>tP4</i> <i>P4/mmm</i>	Al 2 Ti <sub>1</sub> 1 Ti <sub>2</sub> 1	AlTi- <i>L1</i> <sub>0</sub>
	AlTi <sub>3</sub>	Ni <sub>3</sub> Sn	<i>hP8</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>		AlM- <i>D0</i> <sub>19</sub>
	Al <sub>3</sub> Ti	Al <sub>3</sub> Ti	<i>tI8</i> <i>I4/mmm</i>	Al <sub>1</sub> 2 Al <sub>2</sub> 4 Ti 2	AlM- <i>D0</i> <sub>22</sub>
	AlNb <sub>3</sub>	Cr <sub>3</sub> Si	<i>cP8</i> <i>Pm</i> $\bar{3}$ <i>n</i>	Al 2 Nb 6	cub- <i>A15</i>
	$\sigma$	$\sigma$ CrFe	<i>tP30</i> <i>P4</i> <sub>2</sub> / <i>mn</i> <i>m</i>		

# System Al-Si-Zn

**Ternary Solution Phases:**

Liquid, fcc-*A*1, hcp-Zn

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister

**Assessor and Date:**

M. Jacobs (1992).

**Comments:**

No ternary interaction coefficients.  
No ternary compounds.

**Table I - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices
Al-Si-Zn	(Al)	Cu	<i>cF</i> <sub>4</sub> <i>Fm</i> <sub>3</sub> <i>m</i>	M 4
	(Si)	diamond	<i>cF</i> <sub>8</sub> <i>Fd</i> <sub>3</sub> <i>m</i>	
	(Zn)	Mg	<i>hP</i> <sub>2</sub> <i>P6</i> <sub>3</sub> / <i>mmc</i>	M 2

# System Al-Sn-Zn

**Ternary Solution Phases:**

Liquid, fcc-*A1*, hcp-*A3*, hcp-Zn

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A1</i>	:	Substitutional, Redlich-Kister
hcp- <i>A3</i>	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister

**Assessor and Date:**

H. L. Lukas (1991)

**Publication:**

N. Chakraborti, G. Effenberg, S. Fries, S. Kuang,  
H.-L. Lukas, and G. Petzow,  
Vortr. Poster Symp. Materialforsch., 1991,  
2nd, 3, 2692-2693 (1991).

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Liquid**

$$L_{\text{Al},\text{Sn},\text{Zn}}^{0,\text{liquid}} = -2777.03 + 0.59427 \ T$$

$$L_{\text{Al},\text{Sn},\text{Zn}}^{1,\text{liquid}} = 15225.63 - 3.25821 \ T$$

$$L_{\text{Al},\text{Sn},\text{Zn}}^{2,\text{liquid}} = -16198.13 + 3.46632 \ T$$

**Phase hcp-*A3***

$$L_{\text{Al},\text{Sn},\text{Zn}}^{0,\text{hcp-}A3} = 1.0\text{E-}4$$

**Phase hcp-Zn**

$$L_{\text{Al},\text{Sn},\text{Zn}}^{0,\text{hcp-Zn}} = 1.0\text{E-}4$$

**Table I - Crystal Structure and Phase Description.**

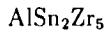
System	Phase	Prototype	Pearson Space Symbol Group	Sub- lattices
Al-Sn-Zn	(Al)	Cu	<i>cF4</i> <i>Fm\bar{3}m</i>	M 4
	(Sn)	$\beta$ -Sn	<i>tI4</i> <i>I41/amd</i>	
	(Zn)	Mg	<i>hP2</i> <i>P63/mmc</i>	M 2

# System Al–Sn–Zr

**Ternary Solution Phases:**

Liquid, bcc-*A*2, bct-*A*5, fcc-*A*1, hcp-*A*3

**Compound:**



**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bct- <i>A</i> 5	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
$\text{AlSn}_2\text{Zr}_5$	:	Stoichiometric, $(\text{Al})(\text{Sn})_2(\text{Zr})_5$

**Assessor and Date:**

J. Korb, and K. Hack, GTT, Germany (1997)

**Thermodynamic properties of the compound phase ( $\text{J} \cdot \text{mol}^{-1}$ )**

**Phase  $\text{AlSn}_2\text{Zr}_5$**

$$\begin{aligned}
 G^\circ(T) - H_{\text{Al}}^{\circ,\text{fcc}-\text{A}1}(298.15 \text{ K}) - 2.0 H_{\text{Sn}}^{\circ,\text{bct}-\text{A}5}(298.15 \text{ K}) - 5.0 H_{\text{Zr}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\
 - 58824.4 + 896.225 T - 177.0982 T \cdot \ln T - 0.0411 T^2 \\
 - 8.4073E-6 T^3 + 261079 T^{-1}
 \end{aligned}$$

**Table I - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol	Sub-lattices	Comments
Al-Sn-Zr	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$		
	(Sn)	$\beta$ -Sn	<i>tI4</i> <i>I4</i> <sub>1</sub> / <i>amd</i>		
	(Zr)	Mg	<i>hP2</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>	M 2	
	(Zr)	W	<i>cI2</i> <i>Im</i> $\bar{3}m$	M 4	
	AlSn <sub>2</sub> Zr <sub>5</sub>				not quoted in [91Vil] nor in [90Mas]

# System Al–Ta–Ti

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1, bcc-*B*2, hcp-*A*3

**Ternary Compounds:**

AlM-*D*0<sub>19</sub>, AlM-*D*0<sub>22</sub>, AlTi-*L*1<sub>0</sub>,  $\sigma$

**Modelling:**

Liquid	:	Substitutional, Redlich–Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich–Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich–Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich–Kister
bcc- <i>B</i> 2	:	Sublattice model, (Al,Ta,Ti) <sub>0.5</sub> (Al,Ta,Ti) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc- <i>B</i> 2 takes into account the ordering reaction bcc- <i>A</i> 2 $\rightleftharpoons$ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Al,Ta,Ti) <sub>3</sub> (Al,Ta,Ti)(□) <sub>0.5</sub>
AlM- <i>D</i> 0 <sub>22</sub>	:	Sublattice model, (Al,Ta,Ti) <sub>3</sub> (Al,Ta,Ti)
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Al,Ta,Ti)(Al,Ta,Ti)
$\sigma$	:	Sublattice model, (Al) <sub>8</sub> (Ta,Ti) <sub>4</sub> (Al,Ta,Ti) <sub>18</sub>

**Assessor and Date:**

N. Saunders, 1996

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase hcp-*A*3**

$$L_{\text{Al,Ta,Ti:}\square}^{0,\text{hcp-}B3} = -40000$$

**Phase AlTi-L1<sub>0</sub>**

$$L_{\text{Ta}, \text{Ti}: \text{Al}}^{0, \text{AlTi}-\text{L}1_0} = L_{\text{Al}: \text{Ta}, \text{Ti}}^{0, \text{AlTi}-\text{L}1_0} = -11000$$

$$L_{\text{Ta}: \text{Al}, \text{Ti}}^{0, \text{AlTi}-\text{L}1_0} = L_{\text{Al}, \text{Ti}: \text{Ta}}^{0, \text{AlTi}-\text{L}1_0} = -15134 - 2.36 T$$

**Phase AlM-D0<sub>19</sub>**

$$L_{\text{Ta}, \text{Ti}: \text{Al}: \text{O}}^{0, \text{AlM}-\text{D}0_{19}} = -24000$$

$$L_{\text{Ta}: \text{Al}, \text{Ti}: \text{O}}^{0, \text{AlM}-\text{D}0_{19}} = 10656 - 1.332 T$$

$$L_{\text{Ti}: \text{Al}, \text{Ta}: \text{O}}^{0, \text{AlM}-\text{D}0_{19}} = 8000$$

$$L_{\text{Al}, \text{Ti}: \text{Ta}: \text{O}}^{0, \text{AlM}-\text{D}0_{19}} = 32000 - T$$

$$L_{\text{Al}: \text{Ta}, \text{Ti}: \text{O}}^{0, \text{AlM}-\text{D}0_{19}} = 2128$$

$$L_{\text{Al}, \text{Ta}: \text{Ti}: \text{O}}^{0, \text{AlM}-\text{D}0_{19}} = 20000$$

**Phase AlM-D0<sub>22</sub>**

$$L_{\text{Al}: \text{Ta}, \text{Ti}}^{0, \text{AlM}-\text{D}0_{22}} = 20000$$

**Phase bcc-A2**

$$L_{\text{Al}, \text{Ta}, \text{Ti}: \text{Box}}^{0, \text{bcc}-\text{A}2} = -10000$$

**Phase bcc-B2**

$$G_{\text{Al}: \text{Ta}}^* = -8250 + T$$

$$G_{\text{Al}: \text{Ti}}^* = -8750 + 1.25 T$$

$$L_{\text{Ti}: \text{Al}, \text{Ta}: \text{O}}^{0, \text{bcc}-\text{B}2} = L_{\text{Al}, \text{Ta}: \text{Ti}: \text{O}}^{0, \text{bcc}-\text{B}2} = -G_{\text{Al}: \text{Ta}}^*$$

$$L_{\text{Ta}: \text{Al}, \text{Ti}: \text{O}}^{0, \text{bcc}-\text{B}2} = L_{\text{Al}, \text{Ti}: \text{Ta}: \text{O}}^{0, \text{bcc}-\text{B}2} = -G_{\text{Al}: \text{Ti}}^*$$

**Phase bcc-A2**

$$L_{\text{Al}, \text{Mo}, \text{Ti}: \text{O}}^{0, \text{bcc}-\text{A}2} = -10000$$

$$L_{\text{Al}, \text{Mo}, \text{Ti}: \text{O}}^{1, \text{bcc}-\text{A}2} = -10000$$

$$L_{\text{Al}, \text{Mo}, \text{Ti}: \text{O}}^{2, \text{bcc}-\text{A}2} = -10000$$

Phase  $\sigma$ 

$$\begin{aligned}
 G^\circ(T) = & 8.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 18.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) \\
 & - 4.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al:Ti:Ta}) = \\
 & - 672000 + 105 T + 8.0 \text{ GHSER}_{\text{Al}} + 18.0 \text{ GHSER}_{\text{Ta}} \\
 & + 4.0 \text{ GHSER}_{\text{Ti}} \\
 G^\circ(T) = & 8.0 H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 4.0 H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) \\
 & - 18.0 H_{\text{Ti}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) = G(\text{Al:Ta:Ti}) = \\
 & - 720000 + 153.9 T + 8.0 \text{ GHSER}_{\text{Al}} + 4.0 \text{ GHSER}_{\text{Ta}} \\
 & + 18.0 \text{ GHSER}_{\text{Ti}} \\
 L_{\text{Al:Ta:Al,Ti:}\square}^{0,\sigma} = & - 1680000 + 510 T \\
 L_{\text{Al:Ti:Al,Ta:}\square}^{0,\sigma} = & - 1230000 + 450 T \\
 L_{\text{Al:Ti:Al,Ta:}\square}^{1,\sigma} = & 1.0E-4 \\
 L_{\text{Al:Ti:Al,Ta:}\square}^{2,\sigma} = & 300000
 \end{aligned}$$

Table I - Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Symbol Space Group	Sub-lattices	Comments
Al-Ta-Ti	(Al)	Cu	$cF4$ $Fm\bar{3}m$	M 4	
	(Ta)	W	$cI2$ $Im\bar{3}m$	M 2	
	bcc-B2	CsCl	$cP2$ $Pm\bar{3}m$	M <sub>1</sub> 1 M <sub>2</sub> 1	
	(Ti)	Mg	$hP2$ $P6_3/mmc$	M 2	
	(Ti)	W	$cI2$ $Im\bar{3}m$	M 2	
	AlTi	AuCu	$tP4$ $P4/mmm$	Al 2 Ti <sub>1</sub> 1 Ti <sub>2</sub> 1	AlTi-L1 <sub>0</sub>
	AlTi <sub>3</sub>	Ni <sub>3</sub> Sn	$hP8$ $P6_3/mmc$		AlM-D0 <sub>19</sub>
	Al <sub>3</sub> Ti	Al <sub>3</sub> Ti	$tI8$ $I4/mmm$	Al <sub>1</sub> 2 Al <sub>2</sub> 4 Ti 2	AlM-D0 <sub>22</sub>
	$\sigma$	$\sigma$ CrFe	$tP30$ $P4_2/mnm$		

# System Al–Ti–W

**Solution Phases:**

Liquid, bcc-*A*2, fcc-*A*1, bcc-*B*2, hcp-*A*3

**Ternary Compounds:**

AlM-*D*0<sub>19</sub>, AlTi-*L*1<sub>0</sub>

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
bcc- <i>B</i> 2	:	Sublattice model, (Al,Ti,W) <sub>0.5</sub> (Al,Ti,W) <sub>0.5</sub> (□) <sub>3</sub> The thermodynamic description of the bcc-B2 takes into account the ordering reaction bcc- <i>A</i> 2 ⇌ bcc- <i>B</i> 2. Two descriptions are given: one using equations 23 and 27, the other using equations 23 and 28. For the latter, the parameters are given in a frame.
AlM- <i>D</i> 0 <sub>19</sub>	:	Sublattice model, (Al,Ti,W) <sub>3</sub> (Al,Ti,W)(□) <sub>0.5</sub>
AlTi- <i>L</i> 1 <sub>0</sub>	:	Sublattice model, (Al,Ti,W)(Al,Ti,W)

**Assessor and Date:**

N. Saunders, 1996

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase AlM-*D*0<sub>19</sub>**

$$L_{\text{Ti},\text{W};\text{Al};\square}^{0,\text{AlM}-\text{D}0_{19}} = 73212$$

$$L_{\text{Ti};\text{Al},\text{W};\square}^{0,\text{AlM}-\text{D}0_{19}} = -2000$$

$$L_{\text{Al},\text{Ti};\text{W};\square}^{0,\text{AlM}-\text{D}0_{19}} = 8000$$

$$L_{\text{Al};\text{Ti},\text{W};\square}^{0,\text{AlM}-\text{D}0_{19}} = 8136$$

**Phase AlTi-L1<sub>0</sub>**

$$\begin{aligned}
 L_{\text{Ti},\text{W};\text{Al}}^{0,\text{AlTi}-L1_0} &= L_{\text{Al};\text{Ti},\text{W}}^{0,\text{AlTi}-L1_0} = 16914 \\
 L_{\text{W};\text{Al},\text{Ti}}^{0,\text{AlTi}-L1_0} &= L_{\text{Al},\text{Ti};\text{W}}^{0,\text{AlTi}-L1_0} = -15134 - 2.36 T \\
 L_{\text{Ti};\text{Al},\text{W}}^{0,\text{AlTi}-L1_0} &= L_{\text{Al},\text{W};\text{Ti}}^{0,\text{AlTi}-L1_0} = -3000
 \end{aligned}$$

**Phase bcc-A2**

$$\begin{aligned}
 L_{\text{Al},\text{Ti},\text{W};\square}^{1,\text{bcc}-A2} &= 0 \\
 L_{\text{Al},\text{Ti},\text{W};\square}^{2,\text{bcc}-A2} &= 0 \\
 L_{\text{Al},\text{Ti},\text{W},\text{Ti};\square}^{3,\text{bcc}-A2} &= 0
 \end{aligned}$$

**Phase bcc-B2**

$$\begin{aligned}
 G_{\text{Al};\text{Ti};\square}^* &= -8750 + 1.25 T \\
 L_{\text{W};\text{Al},\text{Ti};\square}^{0,\text{bcc}-B2} &= L_{\text{Al},\text{Ti};\text{W};\square}^{0,\text{bcc}-B2} = -G_{\text{Al};\text{Ti};\square}^*
 \end{aligned}$$

**Phase bcc-A2**

$$\begin{aligned}
 L_{\text{Al},\text{Ti};\text{W};\square}^{0,\text{bcc}-A2} &= 0 \\
 L_{\text{Al},\text{Ti};\text{W};\square}^{1,\text{bcc}-A2} &= 0 \\
 L_{\text{Al},\text{Ti};\text{W};\square}^{2,\text{bcc}-A2} &= 0
 \end{aligned}$$

**Table I - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Symbol Space Group	Sub- lattices	Comments
Al-Ti-W	(Al)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}$ <i>m</i>	M 4	
	(W)	W	<i>cl2</i> <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	bcc- <i>B2</i>	CsCl	<i>cP2</i> <i>Pm</i> $\bar{3}$ <i>m</i>	M <sub>1</sub> 1	
			<i>hP2</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>	M <sub>2</sub> 1	
	(Ti)	Mg	<i>cl2</i> <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	(Ti)	W	<i>cl2</i> <i>Im</i> $\bar{3}$ <i>m</i>	M 2	
	AlTi	AuCu	<i>tP4</i> <i>P4/mmm</i>	Al 2 Ti <sub>1</sub> 1 Ti <sub>2</sub> 1	AlTi- <i>L1</i> <sub>0</sub>
	AlTi <sub>3</sub>	Ni <sub>3</sub> Sn	<i>hP8</i> <i>P6</i> <sub>3</sub> / <i>mmc</i>		AlM- <i>D0</i> <sub>19</sub>

## System B–Hf–Ti

**Ternary Solution Phases:**

Liquid, bcc-*A*2, hcp-*A*3

**Quasi-binary phases:**

B<sub>2</sub>M, B<sub>4</sub>M<sub>3</sub>, BM

**Modelling:**

Liquid	:	Substitutional, Redlich–Kister
bcc- <i>A</i> 2	:	Sublattice model (Hf,Ti)(B, $\square$ ) <sub>3</sub>
hcp- <i>A</i> 3	:	Sublattice model (Hf,Ti)(B, $\square$ ) <sub>0.5</sub>
B <sub>2</sub> M	:	Quasi-binary, (B) <sub>2</sub> (Hf,Ti)
B <sub>4</sub> M <sub>3</sub>	:	Quasi-binary, (B) <sub>4</sub> (Hf,Ti) <sub>3</sub>
BM	:	Quasi-binary, (B)(Hf,Ti)

**Comments:**

No ternary compounds

**Assessor and Date:**

H. Bittermann, (1997)

**Publication:**

H. Bittermann, and P. Rogl, J. Phase Equil., **18**, 24–47 (1997).

**Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**

**Phase Liquid**

$$L_{\text{B,Hf,Ti}}^{\text{0,liquid}} = 41733.1$$

$$L_{\text{B,Hf,Ti}}^{\text{0,liquid}} = 125.375 \ T$$

$$L_{\text{B,Hf,Ti}}^{\text{0,liquid}} = 93.6697 \ T$$

**Phase B<sub>2</sub>M**

$$L_{\text{B:Hf,Ti}}^{0,\text{B}_2\text{M}} = 7223.32 + 1.75379 \ T$$

**Phase B<sub>4</sub>M<sub>3</sub>**

$$L_{\text{B:Hf,Ti}}^{0,\text{B}_4\text{M}_3} = 115124 - 49.5166 \ T$$

**Phase BM**

$$L_{\text{B:Hf,Ti}}^{0,\text{BM}} = 19396.7 - 6.57772 \ T$$

**Table I - Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Symbol	Symbol Group	Sub- lattices
B-Hf-Ti	(B)	$\beta$ -rhombo-B			
	(Hf)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M	2
	(Hf)	W	<i>cI2</i> <i>Im3m</i>	M	2
	(Ti)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M	2
	(Ti)	W	<i>cI2</i> <i>Im3m</i>	M	2
	BM	BFe	<i>oP8</i> <i>Pnma</i>	B	4
	B <sub>2</sub> M	AlB <sub>2</sub>	<i>hP3</i> <i>P6/mmm</i>	Ti	4
	B <sub>4</sub> M <sub>3</sub>	B <sub>4</sub> Ta <sub>3</sub>	<i>oI14</i> <i>Immm</i>	B	2
				Ti	1

# System Cu-Mg-Y

**Ternary Solution Phases:**

Liquid, fcc-*A*1, bcc-*A*2, hcp-*A*3

**Modelling:**

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister

**Assessor and Date:**

T. Bühler, RWTH, Aachen, Germany, (1997).

**Comments:**

No coefficients for the ternary solution phases.  
No ternary compounds.

**Table I – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Symbol Group	Sub- lattices
Cu-Mg-Si	(Cu)	Cu	<i>cF</i> <sub>4</sub> <i>Fm</i> <sub>3</sub> <i>m</i>	M 4
	(Mg)	Mg	<i>hP</i> <sub>2</sub> <i>P</i> <sub>6</sub> <sub>3</sub> / <i>mmc</i>	M 2
	(Y)	W	<i>cI</i> <sub>2</sub> <i>I</i> <sub>m</sub> <sub>3</sub> <i>m</i>	M 4
	(Y)	Mg	<i>hP</i> <sub>2</sub> <i>P</i> <sub>6</sub> <sub>3</sub> / <i>mmc</i>	M 2

# System Cu–Mg–Si

## Ternary Solution Phases:

(stable)	Liquid, fcc- <i>A</i> 1, bcc- <i>A</i> 2, hcp- <i>A</i> 3
(metastable)	hcp-Zn

## Ternary Compounds:

CuMgSi- $\sigma$ , CuMgSi- $\tau$ , Laves-*C*15

## Modelling:

Liquid	:	Substitutional, Redlich-Kister
bcc- <i>A</i> 2	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister
CuMgSi- $\sigma$	:	Stoichiometric, (Cu) <sub>16</sub> (Mg) <sub>6</sub> (Si) <sub>7</sub>
CuMgSi- $\tau$	:	Stoichiometric, (Cu) <sub>3</sub> (Mg) <sub>2</sub> (Si)
Laves- <i>C</i> 15	:	Sublattice model, (Cu,Mg,Si) <sub>2</sub> (Cu,Mg,Si)

## Assessor and Date:

T. Bühler, RWTH, Aachen, Germany, (1997).

## Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)

### Phase CuMgSi- $\sigma$

$$\begin{aligned}
 G^\circ(T) = & 16.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 6.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) \\
 & - 7.0 H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Cu:Mg:Si}) = \\
 & - 559636 + 110.94 T + 16.0 \text{ GHSER}_{\text{Cu}} + 6.0 \text{ GHSER}_{\text{Mg}} \\
 & + 7.0 \text{ GHSER}_{\text{Si}}
 \end{aligned}$$

**Phase CuMgSi- $\tau$** 

$$G^\circ(T) = 3.0 \ H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 2.0 \ H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K}) \\ - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = G(\text{Cu:Mg:Si}) = \\ - 141720 + 20.26 \ T + 3.0 \ \text{GHSER}_{\text{Cu}} + 2.0 \ \text{GHSER}_{\text{Mg}} + \text{GHSER}_{\text{Si}}$$

**Phase Liquid**

$$L_{\text{Cu,Mg,Si}}^{0,\text{liquid}} = 1\text{E-}04$$

$$L_{\text{Cu,Mg,Si}}^{1,\text{liquid}} = -141736$$

$$L_{\text{Cu,Mg,Si}}^{2,\text{liquid}} = 1\text{E-}04$$

**Phase hcp-Zn**

$$L_{\text{Cu,Mg,Si:}\square}^{0,\text{hcp-Zn}} = 50000$$

$$L_{\text{Cu,Mg,Si:}\square}^{1,\text{hcp-Zn}} = 50000$$

$$L_{\text{Cu,Mg,Si:}\square}^{2,\text{hcp-Zn}} = 50000$$

**Phase Laves-C15**

$$L_{\text{Mg,Si:Cu}}^{0,\text{Laves-C15}} = 15000$$

$$L_{\text{Si:Cu,Mg}}^{0,\text{Laves-C15}} = 6599.45$$

$$L_{\text{Cu,Si:Mg}}^{0,\text{Laves-C15}} = -193131 + 20.69 \ T$$

$$L_{\text{Cu:Mg,Si}}^{0,\text{Laves-C15}} = 8000$$

$$L_{\text{Cu,Mg,Si}}^{0,\text{Laves-C15}} = 13011.35$$

**Table I:a – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Symbol Group	Sub-lattices	Comments
Cu-Mg-Si	(Cu)	Cu	$cF_4$ $Fm\bar{3}m$	M 4	
	(Mg)	Mg	$hP2$ $P6_3/mmc$	M 2	
	(Si)	diamond	$cF8$ $Fd\bar{3}m$	M 8	

**Table I:b – Crystal Structure and Phase Description.**

System	Phase	Prototype	Pearson Space Symbol Group	Sub- lattices	Comments
	$\text{Cu}_2\text{Mg}$	$\text{Cu}_2\text{Mg}$	$cF24$ $Fd\bar{3}m$	Cu 16 Mg 8	Laves-C15
	$\text{Cu}_{16}\text{Mg}_9\text{Si}_7$	$\text{Mn}_{23}\text{Th}_6$	$cF112$ $Fm\bar{3}m$	$\text{Si}_1$ 4 $\text{Si}_1$ 24 Mg 24 $\text{Cu}_1$ 32 $\text{Cu}_2$ 32	$\text{CuMgSi}-\sigma$
	$\text{Cu}_3\text{Mg}_2\text{Si}$	$\text{MgZn}_2$	$hP12$ $P6_3/mmc$	Si 2 Mg 4 Cu 6	$\text{CuMgSi}-\tau$

# System Cu–Mg–Zn

## Ternary Solution Phases:

Liquid, fcc-*A*1, bcc-*A*2, bcc-*B*2, hcp-*A*3, hcp-Zn

## Compounds:

Laves-*C*14, Laves-*C*15, Laves-*C*36, CuZn- $\gamma$ , MgZn,  
Mg<sub>2</sub>Zn<sub>3</sub>, Mg<sub>2</sub>Zn<sub>11</sub>

## Modelling:

Liquid	:	Substitutional, Redlich-Kister
fcc- <i>A</i> 1	:	Substitutional, Redlich-Kister
hcp- <i>A</i> 3	:	Substitutional, Redlich-Kister
hcp-Zn	:	Substitutional, Redlich-Kister
bcc- <i>B</i> 2	:	Sublattice model, (Cu,Mg,Zn) <sub>0.5</sub> (Cu,Mg,Zn) <sub>0.5</sub> Two descriptions of the bcc- <i>A</i> 2:bcc- <i>B</i> 2 order-disorder transformation are given: one which includes the parameters of the order and disordered phases in a single description (equation 21 and 22 in the thermodynamic modelling chapter), and a second one where the order and disorder contributions are expressed by equation 23. For the second case, the parameters are in a frame.
hcp-Zn	:	Substitutional, Redlich-Kister-Muggianu
CuZn- $\gamma$	:	Sublattice model, (Cu,Zn) <sub>2</sub> (Cu,Zn) <sub>2</sub> (Cu) <sub>3</sub> (Mg,Zn) <sub>6</sub>
Laves- <i>C</i> 14	:	Sublattice model, (Cu,Mg,Zn) <sub>2</sub> (Cu,Mg,Zn)
Laves- <i>C</i> 15	:	Sublattice model, (Cu,Mg,Zn) <sub>2</sub> (Cu,Mg,Zn)
Laves- <i>C</i> 36	:	Sublattice model, (Cu,Mg,Zn) <sub>2</sub> (Cu,Mg,Zn)
MgZn	:	Sublattice model, (Mg) <sub>12</sub> (Cu,Zn) <sub>13</sub>
Mg <sub>2</sub> Zn <sub>3</sub>	:	Sublattice model, (Mg) <sub>2</sub> (Cu,Zn) <sub>3</sub>
Mg <sub>2</sub> Zn <sub>11</sub>	:	Sublattice model, (Mg) <sub>2</sub> (Cu,Zn) <sub>11</sub>

## Assessor and Date:

P. Liang, H. L. Lukas (1997)

## Publication:

P. Liang, H. L. Lukas, H. J. Seifert, G. Ghosh, G. Effenberg, F. Aldinger,  
in preparation for *Calphad* (1997)

Thermodynamic properties of the solution and compound phases (J.mol<sup>-1</sup>)**Phase bcc-B2**

$$G_{\text{Cu:Mg}}^* = 0.0$$

$$L_{\text{Cu,Mg}}^0 = - 2500$$

$$G_{\text{Cu:Zn}}^* = 0.0$$

$$L_{\text{Cu,Zn}}^0 = - 12898.97 + 3.26598 \ T$$

$$L_{\text{Cu,Zn}}^1 = 945.265 - 0.80679 \ T$$

$$L_{\text{Cu,Zn}}^2 = 1921.485 - 1.86969 \ T$$

$$G_{\text{Mg:Zn}}^* = 0.0$$

$$L_{\text{Mg,Zn}}^0 = - 2500$$

$$L_{\text{Cu,Mg:Zn:}\square}^{0,\text{bcc-B2}} = L_{\text{Zn:Cu,Mg:}\square}^{0,\text{bcc-B2}} = - G_{\text{Cu:Mg}}^* + L_{\text{Cu,Mg}}^0 - L_{\text{Cu,Zn}}^1 + 0.5 \ L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Mg:Zn:}\square}^{1,\text{bcc-B2}} = L_{\text{Zn:Cu,Mg:}\square}^{1,\text{bcc-B2}} = - 0.5 \ L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Zn:Mg:}\square}^{0,\text{bcc-B2}} = L_{\text{Mg:Cu,Zn:}\square}^{0,\text{bcc-B2}} = - G_{\text{Cu:Zn}}^* + L_{\text{Cu,Zn}}^0$$

$$L_{\text{Cu,Zn:Mg:}\square}^{1,\text{bcc-B2}} = L_{\text{Mg:Cu,Zn:}\square}^{1,\text{bcc-B2}} = L_{\text{Cu,Zn}}^1$$

$$L_{\text{Cu,Zn:Mg:}\square}^{2,\text{bcc-B2}} = L_{\text{Mg:Cu,Zn:}\square}^{2,\text{bcc-B2}} = L_{\text{Cu,Zn}}^2$$

$$L_{\text{Mg,Zn:Cu:}\square}^{0,\text{bcc-B2}} = L_{\text{Cu:Mg,Zn:}\square}^{0,\text{bcc-B2}} = - G_{\text{Mg:Zn}}^* + L_{\text{Mg,Zn}}^0 + L_{\text{Cu,Zn}}^1 + 0.5 \ L_{\text{Cu,Zn}}^2$$

$$L_{\text{Mg,Zn:Cu:}\square}^{1,\text{bcc-B2}} = L_{\text{Cu:Mg,Zn:}\square}^{1,\text{bcc-B2}} = 0.5 \ L_{\text{Cu,Zn}}^2$$

$$L_{\text{Mg,Zn:Cu,Zn:}\square}^{0,\text{bcc-B2}} = L_{\text{Cu,Zn:Mg,Zn:}\square}^{0,\text{bcc-B2}} = - 5 \ L_{\text{Cu,Zn}}^2$$

$$L_{\text{Mg,Zn:Cu,Mg:}\square}^{0,\text{bcc-B2}} = L_{\text{Cu,Mg:Mg,Zn:}\square}^{0,\text{bcc-B2}} = - 2 \ L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Zn:Cu,Mg:}\square}^{0,\text{bcc-B2}} = L_{\text{Cu,Mg:Cu,Zn:}\square}^{0,\text{bcc-B2}} = - 5 \ L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Mg,Zn:Cu:}\square}^{0,\text{bcc-B2}} = L_{\text{Cu,Cu,Mg,Zn:}\square}^{0,\text{bcc-B2}} = 1.5 \ L_{\text{Cu,Zn}}^2$$

$$L_{\text{Cu,Mg,Zn:Zn:}\square}^{0,\text{bcc-B2}} = L_{\text{Zn:Cu,Mg,Zn:}\square}^{0,\text{bcc-B2}} = 1.5 \ L_{\text{Cu,Zn}}^2$$

**Phase bcc-A2**

$$L_{\text{Cu,Mg,Zn:}\square}^{0,\text{bcc-A2}} = 0$$

$$L_{\text{Cu,Mg,Zn:}\square}^{1,\text{bcc-A2}} = 0$$

$$L_{\text{Cu,Mg,Zn:}\square}^{2,\text{bcc-A2}} = 0$$

**Phase Mg<sub>2</sub>Zn<sub>11</sub>**

$$L_{\text{Mg:Cu,Zn}}^{0,\text{Mg}_2\text{Zn}_{11}} = -351000$$

**Phase Laves-C14**

$$L_{\text{Mg,Zn:Cu}}^{0,\text{Laves-C14}} = 35000.00$$

$$L_{\text{Cu:Mg,Zn}}^{0,\text{Laves-C14}} = 35000.00$$

$$L_{\text{Zn:Cu,Mg}}^{0,\text{Laves-C14}} = 6599.45$$

$$L_{\text{Cu,Mg:Zn}}^{0,\text{Laves-C14}} = 13011.35$$

$$L_{\text{Cu,Zn:Mg}}^{0,\text{Laves-C14}} = -75305.48$$

**Phase Laves-C15**

$$L_{\text{Cu,Mg:Zn}}^{0,\text{Laves-C15}} = 13011.35$$

$$L_{\text{Zn:Cu,Mg}}^{0,\text{Laves-C15}} = 6599.45$$

$$L_{\text{Mg,Zn:Cu}}^{0,\text{Laves-C15}} = 35000.00$$

$$L_{\text{Cu:Mg,Zn}}^{0,\text{Laves-C15}} = 8000.00$$

$$L_{\text{Cu,Zn:Mg}}^{0,\text{Laves-C15}} = -78824.62$$

$$L_{\text{Mg:Cu,Zn}}^{0,\text{Laves-C15}} = 25529.06$$

**Phase Laves-C36**

$$L_{\text{Mg},\text{Zn}:Cu}^{0,\text{Laves}-C36} = 35000.00$$

$$L_{\text{Cu}:Mg,Zn}^{0,\text{Laves}-C36} = 8000.00$$

$$L_{Zn:Cu,Mg}^{0,\text{Laves}-C36} = 6599.45$$

$$L_{Cu,Mg:Zn}^{0,\text{Laves}-C36} = 13011.35$$

$$L_{Cu,Zn:Mg}^{0,\text{Laves}-C36} = -90226.26$$

**Phase Mg<sub>2</sub>Zn<sub>3</sub>**

$$L_{Mg:Cu,Zn}^{0,Mg_2Zn_3} = -100000$$

**Phase MgZn**

$$L_{Mg:Cu,Zn}^{0,MgZn} = -575000$$

**Phase CuZn- $\gamma$** 

$$K4 = -11552.71 - 1.67824 T$$

$$K5 = 15732.3 - 10.26575 T$$

$$K6 = 37289.2 - 13.05259 T$$

$$K7 = 9000.0 - 1.50000 T$$

$$13 K4 + 2 K5 + 2 K6 + 6 K7 = 9857.77 - 77.4538 T$$

$$13 K4 + 6 K7 = -96185.23 - 30.81712 T$$

$$13 K4 + 2 K6 + 6 K7 = -21606.83 - 56.9223 T$$

$$G^\circ(T) - 5.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 6.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K})$$

$$\begin{aligned} - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) &= G(\text{Zn:Cu:Cu:Mg}) = \\ &13.0 K4 + 2.0 K5 + 2.0 K6 + 6 K7 + 5.0 \text{ GHSER}_{\text{Cu}} \\ &+ 6.0 \text{ GHSER}_{\text{Mg}} + 2.0 \text{ GHSER}_{\text{Zn}} \end{aligned}$$

$$G^\circ(T) - 5.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 6.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K})$$

$$\begin{aligned} - 2.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) &= G(\text{Cu:Zn:Cu:Mg}) = \\ &13.0 K4 + 6.0 K7 + 5.0 \text{ GHSER}_{\text{Cu}} + 6.0 \text{ GHSER}_{\text{Mg}} \\ &+ 2.0 \text{ GHSER}_{\text{Zn}} \end{aligned}$$

$$G^\circ(T) - 3.0 H_{\text{Cu}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) - 6.0 H_{\text{Mg}}^{\circ,\text{hcp}-A3}(298.15 \text{ K})$$

$$\begin{aligned} - 4.0 H_{\text{Zn}}^{\circ,\text{hcp}-\text{Zn}}(298.15 \text{ K}) &= G(\text{Cu:Zn:Cu:Mg}) = \\ &13.0 K4 + 2.0 K6 + 6.0 K7 + 3.0 \text{ GHSER}_{\text{Cu}} + 6.0 \text{ GHSER}_{\text{Mg}} \\ &+ 4.0 \text{ GHSER}_{\text{Zn}} \end{aligned}$$

Table I – Crystal Structure and Phase Description.

System	Phase	Prototype	Pearson Space Group	Sub-lattices	Comments
Cu-Mg-Zn	(Cu)	Cu	<i>cF4</i> <i>Fm</i> $\bar{3}m$	M 4	
	(Mg)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	(Zn)	Mg	<i>hP2</i> <i>P6<sub>3</sub>/mmc</i>	M 2	
	CuMg <sub>2</sub>	CuMg <sub>2</sub>	<i>oF48</i> <i>Fddd</i>	Cu 16 Mg1 16 Mg2 16	
	Cu <sub>2</sub> Mg	Cu <sub>2</sub> Mg	<i>cF24</i> <i>Fd</i> $\bar{3}m$	Cu 16	Laves-C15
	Laves-C36	MgNi <sub>2</sub>	<i>hP24</i> <i>P6<sub>3</sub>/mmc</i>	Mg 8	Laves-C36
				Cr <sub>1</sub> 6 Cr <sub>2</sub> 6 Zr <sub>1</sub> 3 Zr <sub>2</sub> 3	
	Laves-C14	MgZn <sub>2</sub>	<i>hP12</i> <i>P6<sub>3</sub>/mmc</i>	Cr 2 Cr 6 Zr 4	Laves-C14
	$\gamma$	Cu <sub>5</sub> Zn <sub>8</sub>	<i>cI52</i> <i>I</i> $\bar{4}3m$	Cu <sub>1</sub> 8 Cu <sub>2</sub> 12 Zn <sub>1</sub> 8 Zn <sub>2</sub> 24	Cu <sub>5</sub> Zn
	Mg <sub>2</sub> Zn <sub>11</sub>	Mg <sub>2</sub> Zn <sub>11</sub>	<i>cP39</i> <i>Pm</i> $\bar{3}$		
	MgZn				
	Mg <sub>2</sub> Zn <sub>3</sub>		<i>mC110</i> <i>B2/m</i>		



## **APPENDICES**



**APPENDIX I: THERMODYNAMIC PROPERTIES OF THE ELEMENTS  
(J.mol<sup>-1</sup>)**

NOTE: The Gibbs Energies of Formation at T are relative to the Enthalpy of the Pure Elements in their Reference Phase at 298.15 K<sup>1</sup>

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## ALUMINIUM

### Aluminium fcc-A1

$$GHSER_{Al} = G_{Al}^{fcc-A1}(T) - H_{Al}^{\circ,fcc-A1}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 700.00 : & - 7976.15 + 137.093038 \cdot T - 24.3671976 \cdot T \cdot \ln T \\ & - 1.884662E-3 \cdot T^2 - 0.877664E-6 \cdot T^3 \\ & + 74092 \cdot T^{-1} \\ 700.00 < T < 933.47 : & - 11276.24 + 223.048446 \cdot T - 38.5844296 \cdot T \cdot \ln T \\ & + 18.531982E-3 \cdot T^2 - 5.764227E-6 \cdot T^3 \\ & + 74092 \cdot T^{-1} \\ 933.47 < T < 2900.00 : & - 11278.378 + 188.684153 \cdot T - 31.748192 \cdot T \cdot \ln T \\ & - 1230.524E25 \cdot T^{-9} \end{aligned}$$

### Aluminium bcc-A2

$$GBCC_{Al} = G_{Al}^{bcc-A2}(T) - H_{Al}^{\circ,fcc-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 2900.00 : 10083.00 - 4.813 \cdot T + GHSER_{Al}$$

### Aluminium cbcc-A12

$$G_{Al}^{cbcc-A12}(T) - H_{Al}^{\circ,fcc-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 2900.00 : 10083.40 - 4.813 \cdot T + GHSER_{Al}$$

### Aluminium bcc-B2

$$G_{Al:Al}^{bcc-B2}(T) - H_{Al}^{\circ,fcc-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 2900.00 : GBCC_{Al}$$

### Aluminium bct-A5

$$G_{Al}^{bct-A5}(T) - H_{Al}^{\circ,fcc-A1} =$$

$$298.15 < T < 2900.00 : 10083.0 - 4.813 \cdot T + GHSER_{Al}$$

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<sup>1</sup>Scientific Group Thermodata Europe (S.G.T.E.) Data for Pure Elements, A.T. Dinsdale, CALPHAD, 15, 4, 317 - 425 (1991).

**Aluminium cub-A13**

$$G_{\text{Al}}^{\text{cub}-A13}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1} =$$

$$298.15 < T < 2900.00 : 10920.44 - 4.8116 \cdot T + \text{GHSER}_{\text{Al}}$$

**Aluminium diamond**

$$G_{\text{Al}}^{\text{diamond}}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 2900.00 : 30.0 \cdot T + \text{GHSER}_{\text{Al}}$$

**Aluminium hcp-A3**

$$\text{GHCP}_{\text{Al}} = G_{\text{Al}}^{\text{hcp}-A3}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 2900.00 : 5481.0 - 1.8 \cdot T + \text{GHSER}_{\text{Al}}$$

**Aluminium hcp-Zn**

$$G_{\text{Al}}^{\text{hcp}-Zn}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 5482 - 1.8 \cdot T + \text{GHSER}_{\text{Al}}$$

**Aluminium liquid**

$$\text{GLIQ}_{\text{Al}} = G_{\text{Al}}^{\text{liquid}}(T) - H_{\text{Al}}^{\circ,\text{fcc}-A1}(298.15 \text{ K}) =$$

$$298.15 < T < 933.47 : + 11005.029 - 11.841867 \cdot T + 7.934\text{E-}20 \cdot T^7 \\ + \text{GHSER}_{\text{Al}}$$

$$933.47 < T < 2900.00 : + 10482.382 - 11.253974 \cdot T + 1.231\text{E+}28 \cdot T^{-9} \\ + \text{GHSER}_{\text{Al}}$$


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**BORON****Boron  $\beta$ -rhombo-B**

$$\text{GHSER}_{\text{B}} = G_{\text{B}}^{\beta-\text{rhombo-B}}(T) - H_{\text{B}}^{\circ,\beta-\text{rhombo-B}}(298.15 \text{ K}) =$$

$$298.15 < T < 1100.00 : - 7735.284 + 107.111864 \cdot T - 15.6641 \cdot T \cdot \ln T \\ - 0.006864515 \cdot T^2 + 6.18878\text{E-}07 \cdot T^3 \\ + 370843 \cdot T^{-1}$$

$$1100.00 < T < 2348.00 : - 16649.474 + 184.801744 \cdot T - 26.6047 \cdot T \cdot \ln T \\ - 7.9809\text{E-}04 \cdot T^2 - 2.556\text{E-}08 \cdot T^3 \\ + 1748270 \cdot T^{-1}$$

$$2348.00 < T < 3000.00 : - 36667.582 + 231.336244 \cdot T - 31.5957527 \cdot T \cdot \ln T \\ - 0.00159488 \cdot T^2 + 1.34719\text{E-}07 \cdot T^3 \\ + 11205883 \cdot T^{-1}$$

$$3000.00 < T < 6000.00 : - 21530.653 + 222.396264 \cdot T - 31.4 \cdot T \cdot \ln T$$

$$\text{GBCC}_B = G_B^{\text{bcc}-A2}(T) - H_B^{\circ,\beta-\text{rhombo}-B}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 50208.0 - 13.472 T + \text{GHSER}_B$$

**Boron diamond**

$$G_B^{\text{diamond}}(T) - H_B^{\circ,\beta-\text{rhombo}-B} = \\ 298.15 < T < 6000.00 : 20 + \text{GHSER}_B$$

**Boron fcc-A1**

$$\text{GFCC}_B = G_B^{\text{fcc}-A1}(T) - H_B^{\circ,\beta-\text{rhombo}-B}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 43514.0 - 12.217 T + \text{GHSER}_B$$

**Boron hcp-A3**

$$\text{GHCP}_B = G_B^{\text{hcp}-A3}(T) - H_B^{\circ,\beta-\text{rhombo}-B}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 50208.0 - 9.706 T + \text{GHSER}_B$$

**Boron liquid**

$$\text{GLIQ}_B = G_B^{\text{liquid}}(T) - H_B^{\circ,\beta-\text{rhombo}-B}(298.15 \text{ K}) = \\ 298.15 < T < 500.00 : 40723.275 + 86.843839 T - 15.6641 T \cdot \ln T \\ - 0.006864515 T^2 + 6.18878E-07 T^3 \\ + 370843 T^{-1} \\ 500.00 < T < 2348.00 : 41119.703 + 82.101722 T - 14.9827763 T \cdot \ln T \\ - 0.007095669 T^2 + 5.07347E-07 T^3 \\ + 335484 T^{-1} \\ 2348.00 < T < 6000.00 : + 28842.012 + 200.94731 T - 31.4 T \cdot \ln T$$


---

**CARBON****Carbon graphite**

$$\text{GHSER}_C = G_C^{\text{graphite}}(T) - H_C^{\circ,\text{graphite}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : - 17368.441 + 170.73 T - 24.3 T \cdot \ln T \\ - 4.723E-04 T^2 + 2562600 T^{-1} - 2.643E+08 T^{-2} \\ + 1.2E+10 T^{-3}$$

**Carbon diamond**

$$G_C^{\text{diamond}}(T) - H_C^{\circ,\text{graphite}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : - 16359.441 + 175.61 T - 24.31 T \cdot \ln T \\ - 4.723E-04 T^2 + 2698000 T^{-1} - 2.61E+08 T^{-2} \\ + 1.11E+10 T^{-3}$$

**Carbon liquid**

$$\text{GLIQ}_C = G_C^{\text{liquid}}(T) - H_C^{\text{o,graphite}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 117369 - 24.63 T + \text{GHSER}_C$$


---

**CERIUM****Cerium fcc-A1**

$$\text{GHSER}_{Ce} = G_{Ce}^{\text{fcc-A1}}(T) - H_{Ce}^{\text{o,fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 1000.00 : -7160.519 + 84.23022 T - 22.3664 T \cdot \ln T$$

$$- 0.0067103 T^2 - 3.20773E-07 T^3 - 18117 T^{-1}$$

$$1000.00 < T < 2000.00 : -79678.506 + 659.4604 T - 101.32248 T \cdot \ln T$$

$$+ 0.026046487 T^2 - 1.9302976E-06 T^3 + 11531707 T^{-1}$$

$$2000.00 < T < 4000.00 : -14198.639 + 190.370192 T - 37.6978 T \cdot \ln T$$

**Cerium bcc-A2**

$$\text{GBCC}_{Ce} = G_{Ce}^{\text{bcc-A2}}(T) - H_{Ce}^{\text{o,fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 1000.00 : -1354.69 - 5.21501 T - 7.7305867 T \cdot \ln T$$

$$- 0.029098402 T^2 + 4.784299E-06 T^3 - 196303 T^{-1}$$

$$1000.00 < T < 1072.00 : -12101.106 + 187.449688 T - 37.6142 T \cdot \ln T$$

$$1072.00 < T < 6000.00 : -11950.375 + 186.333811 T - 37.4627992 T \cdot \ln T$$

$$- 5.7145E-05 T^2 + 2.348E-09 T^3 - 25897 T^{-1}$$

**Cerium dhcp**

$$G_{Ce}^{\text{dhcp}}(T) - H_{Ce}^{\text{o,fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 4000.00 : -190.0 + 0.56886 T + \text{GHSER}_{Ce}$$

**Cerium hcp-A3**

$$\text{GHCP}_{Ce} = G_{Ce}^{\text{hcp-A3}}(T) - H_{Ce}^{\text{o,fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 4000.00 : 50000 + \text{GHSER}_{Ce}$$

**Cerium liquid**

$$\text{GLIQ}_{Ce} = G_{Ce}^{\text{liquid}}(T) - H_{Ce}^{\text{o,fcc-A1}}(298.15 \text{ K}) =$$

$$298.15 < T < 1000.00 : 4117.865 - 11.423898 T - 7.5383948 T \cdot \ln T$$

$$- 0.02936407 T^2 + 4.827734E-06 T^3 - 198834 T^{-1}$$

$$1000.00 < T < 4000.00 : -6730.605 + 183.023193 T - 37.6978 T \cdot \ln T$$


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## CHROMIUM

### Chromium bcc-*A*2(paramagnetic)

$$G_{\text{Cr}}^{\text{bcc}-\text{A}2,\text{para}}(T) - H_{\text{Cr}}^{\text{o,bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) =$$

298.15 <  $T$  < 2180.00 :  $-8856.94 + 157.48 T - 26.908 T \cdot \ln T$   
                                   + 1.89435E-3  $T^2 - 1.47721\text{E-}6 T^3 + 139250 T^{-1}$   
 2180.00 <  $T$  < 6000.00 :  $-34869.344 + 344.18 T - 50 T \cdot \ln T$   
                                   - 2885.26E29  $T^{-9}$

### Chromium cbcc-*A*12

$$G_{\text{Cr}}^{\text{bccc}-\text{A}12,\text{para}}(T) - H_{\text{Cr}}^{\text{o,bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) =$$

298.15 <  $T$  < 6000.00 :  $11087.0 + 2.7196 T + \text{GHSER}_{\text{Cr}}$

### Chromium cub-*A*13

$$G_{\text{Cr}}^{\text{cub}-\text{A}13}(T) - H_{\text{Cr}}^{\text{o,bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) =$$

298.15 <  $T$  < 6000.00 :  $15899.0 + 0.6276 T + \text{GHSER}_{\text{Cr}}$

### Chromium fcc-*A*1(paramagnetic)

$$GFCC_{\text{Cr}} = G_{\text{Cr}}^{\text{fcc}-\text{A}1}(T) - H_{\text{Cr}}^{\text{o,bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) =$$

298.15 <  $T$  < 6000.00 :  $7284.0 + 0.163 T + \text{GHSER}_{\text{Cr}} +$

### Chromium hcp-*A*3(paramagnetic)

$$GHCP_{\text{Cr}} = G_{\text{Cr}}^{\text{hcp}-\text{A}3}(T) - H_{\text{Cr}}^{\text{o,bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) =$$

298.15 <  $T$  < 6000.00 :  $4438.00 + \text{GHSER}_{\text{Cr}} +$

### Chromium liquid

$$GLIQ_{\text{Cr}} = G_{\text{Cr}}^{\text{liquid}}(T) - H_{\text{Cr}}^{\text{o,bcc}-\text{A}2,\text{para}}(298.15 \text{ K}) =$$

298.15 <  $T$  < 2180.00 :  $24339.955 - 11.420225 T + 2.37615\text{E-}21 T^7$   
                                   +  $\text{GHSER}_{\text{Cr}}$   
 2180.00 <  $T$  < 6000.00 :  $18409.36 - 8.563683 T + 2.88526\text{E+}32 T^{-9}$   
                                   +  $\text{GHSER}_{\text{Cr}}$

### Chromium Laves-*C*14

$$G_{\text{Cr:Cr}}^{\text{Cr,Laves-C}14} - 3.0 H_{\text{Cr}}^{\text{o,bcc}-\text{A}2}(298.15 \text{ K}) =$$

298.15 <  $T$  < 6000.00 :  $15000.0 + 3.0 \text{ GHSER}_{\text{Cr}}$

### Chromium Laves-*C*15

$$G_{\text{Cr:Cr}}^{\text{Cr,Laves-C}15} - 3.0 H_{\text{Cr}}^{\text{o,bcc}-\text{A}2}(298.15 \text{ K}) =$$

298.15 <  $T$  < 6000.00 :  $15000.0 + 3.0 \text{ GHSER}_{\text{Cr}}$

**Chromium Laves-C36**

$$G_{\text{Cr:Cr}}^{\text{Cr,Laves-C36}} - 3.0 H_{\text{Cr}}^{\text{o,bcc-A2}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 15000.0 + 3.0 \text{ GHSER}_{\text{Cr}}$$


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**COPPER****Copper fcc-A1**

$$\text{GHSER}_{\text{Cu}} = G_{\text{Cu}}^{\text{fcc-A1}}(T) - H_{\text{Cu}}^{\text{o,fcc-A1}}(298.15 \text{ K}) = \\ 298.15 < T < 1357.77 : -7770.458 + 130.485235 T - 24.112392 T \cdot \ln T \\ - 2.65684E-3 T^2 + 0.129223E-6 T^3 + 52478 T^{-1} \\ 1357.77 < T < 3200.00 : -13542.026 + 183.803828 T - 31.38 T \cdot \ln T \\ + 364.167E27 T^{-9}$$

**Copper bcc-A2**

$$\text{GBCC}_{\text{Cu}} = G_{\text{Cu}}^{\text{bcc-A2}}(T) - H_{\text{Cu}}^{\text{o,fcc-A1}}(298.15 \text{ K}) = \\ 298.15 < T < 3200.00 : 4017.00 - 1.255 T + \text{GHSER}_{\text{Cu}}$$

**Copper hcp-A3**

$$\text{GHCP}_{\text{Cu}} = G_{\text{Cu}}^{\text{hcp-A3}}(T) - H_{\text{Cu}}^{\text{o,fcc-A1}}(298.15 \text{ K}) = \\ 298.15 < T < 3200.00 : 600.0 + 0.2 T + \text{GHSER}_{\text{Cu}}$$

**Copper liquid**

$$\text{GLIQ}_{\text{Cu}} = G_{\text{Cu}}^{\text{liquid}}(T) - H_{\text{Cu}}^{\text{o,fcc-A1}}(298.15 \text{ K}) = \\ 298.15 < T < 1357.77 : 12964.736 - 9.511904 T - 5.849E-21 T^7 \\ + \text{GHSER}_{\text{Cu}} \\ 1357.77 < T < 3200.00 : 13495.481 - 9.922344 T - 3.642E+29 T^9 \\ + \text{GHSER}_{\text{Cu}}$$


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**IRON****Iron bcc-A2(paramagnetic)**

$$\text{GHSER}_{\text{Fe}} = G_{\text{Fe}}^{\text{bcc-A2,para}}(T) - H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) = \\ 298.15 < T < 1811.00 : 1225.7 + 124.134 T - 23.5143 T \cdot \ln T \\ - 4.39752E-3 T^2 - 0.058927E-6 T^3 + 77359 T^{-1}$$

$$1811.00 < T < 6000.00 : - 25383.581 + 299.31255 \cdot T - 46 \cdot T \cdot \ln T + 2296.03E28 \cdot T^{-9}$$

**Iron cbcc-A12**

$$G_{\text{Fe}}^{\text{cbcc-A12}}(T) = H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : + 4745 + \text{GHSER}_{\text{Fe}}$$

**Iron cub-A13**

$$G_{\text{Fe}}^{\text{cub-A13}}(T) = H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 3745 + \text{GHSER}_{\text{Fe}}$$

**Iron fcc-A1(paramagnetic)**

$$\text{GFCC}_{\text{Fe}} = G_{\text{Fe}}^{\text{fcc-A1}}(T) = H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) = \\ 298.15 < T < 1811.00 : - 1462.4 + 8.8282 \cdot T - 1.15 \cdot T \cdot \ln T + 0.00064 \cdot T^2 + \text{GHSER}_{\text{Fe}} \\ 1811.00 < T < 6000.00 : - 713.815 + 0.94001 \cdot T + 0.49251 \cdot T^{-9} + \text{GHSER}_{\text{Fe}}$$

**Iron hcp-A3**

$$\text{GHCP}_{\text{Fe}} = G_{\text{Fe}}^{\text{hcp-A3}}(T) = H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) = \\ 298.15 < T < 1811.00 : - 3705.78 + 12.591 \cdot T - 1.15 \cdot T \cdot \ln T + 6.4E-04 \cdot T^2 + \text{GHSER}_{\text{Fe}} \\ 1811.00 < T < 6000.00 : - 3957.199 + 5.24951 \cdot T + 4.9251E+30 \cdot T^{-9} + \text{GHSER}_{\text{Fe}}$$

**Iron liquid**

$$\text{GLIQ}_{\text{Fe}} = G_{\text{Fe}}^{\text{liquid}}(T) = H_{\text{Fe}}^{\text{o,bcc-A2,para}}(298.15 \text{ K}) = \\ 298.15 < T < 1811.00 : + 12040.17 - 6.55843 \cdot T - 3.67516E-21 \cdot T^7 + \text{GHSER}_{\text{Fe}} \\ 1811.00 < T < 6000.00 : + 14544.751 - 8.01055 \cdot T - 2.29603E+31 \cdot T^{-9} + \text{GHSER}_{\text{Fe}}$$

**HAFNIUM****Hafnium hcp-A3**

$$\text{GHSER}_{\text{Hf}} = G_{\text{Hf}}^{\text{hcp-A3}}(T) = H_{\text{Hf}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = \\ 298.15 < T < 2506.00 : - 6987.297 + 110.744026 \cdot T - 22.7075 \cdot T \cdot \ln T - 0.004146145 \cdot T^2 - 4.77E-10 \cdot T^3 - 22590 \cdot T^{-1}$$

$$2506.00 < T < 6000.00 : -1446776.33 + 6193.60999 T - 787.536383 T \cdot \ln T \\ + 0.1735215 T^2 - 7.575759E-06 T^3 \\ + 5.01742495E+08 T^{-1}$$

**Hafnium bcc-A2**

$$\text{GBCC}_{\text{Hf}} = G_{\text{Hf}}^{\text{bcc}-\text{A}2}(T) - H_{\text{Hf}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) =$$

$$298.15 < T < 2506.00 : 5370.703 + 103.836026 T - 22.8995 T \cdot \ln T \\ - 0.004206605 T^2 + 8.71923E-07 T^3 - 22590 T^{-1} \\ - 1.446E-10 T^4$$

$$2506.00 < T < 6000.00 : +1912456.77 - 8624.20573 T + 1087.61412 T \cdot \ln T \\ - 0.286857065 T^2 + 1.3427829E-05 T^3 \\ - 6.10085091E+08 T^{-1}$$

**Hafnium fcc-A1**

$$\text{GFCC}_{\text{Hf}} = G_{\text{Hf}}^{\text{fcc}-\text{A}1}(T) - H_{\text{Hf}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 10000 - 2.2 T + \text{GHSER}_{\text{Hf}}$$

**Hafnium liquid**

$$\text{GLIQ}_{\text{Hf}} = G_{\text{Hf}}^{\text{liquid}}(T) - H_{\text{Hf}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) =$$

$$298.15 < T < 1000.00 : 20414.959 + 99.790933 T - 22.7075 T \cdot \ln T \\ - 0.004146145 T^2 - 4.77E-10 T^3 - 22590 T^{-1}$$

$$1000.00 < T < 2506.00 : 49731.499 - 149.91739 T + 12.116812 T \cdot \ln T \\ - 0.021262021 T^2 + 1.376466E-06 T^3 - 4449699 T^{-1}$$

$$2506.00 < T < 6000.00 : -4247.217 + 265.470523 T - 44 T \cdot \ln T$$


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**LITHIUM****Lithium bcc-A2**

$$\text{GHSER}_{\text{Li}} = G_{\text{Li}}^{\text{bcc}-\text{A}2}(T) - H_{\text{Li}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) =$$

$$200.00 < T < 453.60 : -10583.817 + 217.637482 T - 38.940488 T \cdot \ln T \\ + 35.466931E-3 T^2 - 19.869816E-6 T^3 + 159994 T^{-1}$$

$$453.60 < T < 500.00 : -559579.123 + 10547.879893 T \\ - 1702.8886493 T \cdot \ln T \\ + 2258.329444E-3 T^2 - 571.066077E-6 T^3 \\ + 33885874 T^{-1}$$

$$500.00 < T < 3000.00 : -9062.994 + 179.278285 T - 31.2283718 T \cdot \ln T \\ + 2.633221E-3 T^2 - 0.438058E-6 T^3 - 102387 T^{-1}$$

**Lithium fcc-A1**

$$\text{GFCC}_{\text{Li}} = G_{\text{Li}}^{\text{fcc}-\text{A}1}(T) - H_{\text{Li}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ 200.00 < T < 3000.00 : -108 + 1.3 T + \text{GHSER}_{\text{Li}}$$

**Lithium hcp-A3**

$$\text{GHCP}_{\text{Li}} = G_{\text{Li}}^{\text{hcp}-\text{A}3}(T) - H_{\text{Li}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ 200.00 < T < 3000.00 : -154 + 2 T + \text{GHSER}_{\text{Li}}$$

**Lithium liquid**

$$\text{GLIQ}_{\text{Li}} = G_{\text{Li}}^{\text{liquid}}(T) - H_{\text{Li}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ 200.00 < T < 250.00 : -7883.612 + 211.841861 T - 38.940488 T \cdot \ln T \\ + 35.466931E-3 T^2 - 19.869816E-6 T^3 \\ + 159994 T^{-1} \\ 250.00 < T < 453.60 : 12015.027 - 362.187078 T + 61.6104424 T \cdot \ln T \\ - 182.426463E-3 T^2 + 63.955671E-6 T^3 \\ - 559968 T^{-1} \\ 453.60 < T < 3000.00 : -6057.31 + 172.652183 T - 31.2283718 T \cdot \ln T \\ + 2.633221E-3 T^2 - 0.438058E-6 T^3 \\ - 102387 T^{-1}$$


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**MAGNESIUM****Magnesium hcp-A3**

$$\text{GHSER}_{\text{Mg}} = G_{\text{Mg}}^{\text{hcp}-\text{A}3}(T) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ 298.15 < T < 923.00 : -8367.34 + 143.675547 T - 26.1849782 T \cdot \ln T \\ + 0.4858E-3 T^2 - 1.393669E-6 T^3 + 78950 T^{-1} \\ 923.00 < T < 3000.00 : -14130.185 + 204.716215 T - 34.3088 T \cdot \ln T \\ + 1038.192E25 T^{-9}$$

**Magnesium bcc-A2**

$$\text{GBCC}_{\text{Mg}} = G_{\text{Mg}}^{\text{bcc}-\text{A}2}(T) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ 298.15 < T < 3000.00 : 3100.00 - 2.1 T + \text{GHSER}_{\text{Mg}}$$

**Magnesium cbcc-A12**

$$G_{\text{Mg}}^{\text{cbcc}-\text{A}12}(T) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) = \\ 298.15 < T < 3000.00 : 4602.4 - 3.011 T + \text{GHSER}_{\text{Mg}}$$

**Magnesium cub-A13**

$$G_{\text{Mg}}^{\text{cub}-\text{A}13}(T) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) =$$

$$298.15 < T < 3000.00 : 5000.0 - 3.0 \cdot T + \text{GHSER}_{\text{Mg}}$$

**Magnesium fcc-A1**

$$\text{GFCC}_{\text{Mg}} = G_{\text{Mg}}^{\text{fcc}-\text{A}1}(T) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) =$$

$$298.15 < T < 3000.00 : 2600 - 0.90 \cdot T + \text{GHSER}_{\text{Mg}}$$

**Magnesium liquid**

$$\text{GLIQ}_{\text{Mg}} = G_{\text{Mg}}^{\text{liquid}}(T) - H_{\text{Mg}}^{\circ,\text{hcp}-\text{A}3}(298.15 \text{ K}) =$$

$$298.15 < T < 923.00 : 8202.243 - 8.83693 \cdot T + \text{GHSER}_{\text{Mg}} - 8.0176\text{E-}20 \cdot T^7 \\ + \text{GHSER}_{\text{Mg}}$$

$$923.00 < T < 3000.00 : 8690.316 - 9.392158 \cdot T - 1.038192\text{E+}28 \cdot T^{-9} \\ + \text{GHSER}_{\text{Mg}}$$


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## MANGANESE

**Manganese cbcc-A12(paramagnetic)**

$$\text{GHSER}_{\text{Mn}} = G_{\text{Mn}}^{\text{cbcc}-\text{A}12,\text{para}}(T) - H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A}12,\text{para}}(298.15 \text{ K}) =$$

$$298.15 < T < 1519.00 : -8115.28 + 130.059 \cdot T - 23.4582 \cdot T \cdot \ln T \\ - 7.34768\text{E-}3 \cdot T^2 + 69827 \cdot T^{-1}$$

$$1519.00 < T < 3000.00 : -28733.41 + 312.2648 \cdot T - 48 \cdot T \cdot \ln T \\ + 1656.847\text{E+}27 \cdot T^{-9}$$

**Manganese bcc-A2(paramagnetic)**

$$\text{GBCC}_{\text{Mn}} = G_{\text{Mn}}^{\text{bcc}-\text{A}2,\text{para}}(T) - H_{\text{Mn}}^{\circ,\text{bcc}-\text{A}12,\text{para}}(298.15 \text{ K}) =$$

$$298.15 < T < 1519.00 : -3235.3 + 127.85 \cdot T - 23.7 \cdot T \cdot \ln T \\ - 7.44271\text{E-}3 \cdot T^2 + 60000 \cdot T^{-1}$$

$$1519.00 < T < 3000.00 : -23188.83 + 307.7043 \cdot T - 48 \cdot T \cdot \ln T \\ + 1265.152\text{E27} \cdot T^{-9}$$

**Manganese fcc-A1(paramagnetic)**

$$\text{GFCC}_{\text{Mn}} = G_{\text{Mn}}^{\text{fcc}-\text{A}1,\text{para}}(T) - H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A}12,\text{para}}(298.15 \text{ K}) =$$

$$298.15 < T < 1519.00 : -3439.3 + 131.884 \cdot T - 24.5177 \cdot T \cdot \ln T \\ - 6\text{E-}3 \cdot T^2 + 69600 \cdot T^{-1}$$

$$298.15 < T < 1519.00 : -26070.1 + 309.6664 \cdot T - 48 \cdot T \cdot \ln T \\ + 386.196\text{E28} \cdot T^{-9}$$

**Manganese Laves-C15**

$$G_{\text{Mn}: \text{Mn}}^{\text{Laves-C}15} - 3.0 \cdot H_{\text{Mn}}^{\circ,\text{cbcc}-\text{A}12,\text{para}}(298.15 \text{ K}) =$$

$$298.15 < T < 3000.00 : 3000.0 + 3.0 \cdot \text{GHSER}_{\text{Mn}}$$

**Manganese cub-A13**

$$G_{\text{Mn}}^{\text{cub}-A13}(T) - H_{\text{Mn}}^{o,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 1519.00 : & + 2314.88 + 5.936 T - 1.4203 T \cdot \ln T \\ & + 1.51409E-03 T^2 + 442.0 T^{-1} + \text{GHSER}_{\text{Mn}} \\ 1519.00 & \quad 3000.00 : + 442.65 - 0.9715 T + 2.3107229E+30 T^{-9} \\ & + \text{GHSER}_{\text{Mn}} \end{aligned}$$

**Manganese hcp-A3(paramagnetic)**

$$\text{GHCP}_{\text{Mn}} = G_{\text{Mn}}^{\text{hcp}-A3,\text{para}}(T) - H_{\text{Mn}}^{o,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 1519.00 : & - 4439.3 + 133.007 T - 24.5177 T \cdot \ln T \\ & - 6E-3 T^2 + 69600 T^{-1} \\ 1519.00 < T < 6000.00 : & - 27070.1 + 310.7894 T - 48 T \cdot \ln T \\ & + 386.196E28 T^{-9} \end{aligned}$$

**Manganese liquid**

$$\text{GLIQ}_{\text{Mn}} = G_{\text{Mn}}^{\text{liquid}}(T) - H_{\text{Mn}}^{o,\text{cbcc}-A12,\text{para}}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 1519.00 : & 17859.91 - 12.6208 T - 4.41929E-21 T^7 \\ & + \text{GHSER}_{\text{Mn}} \\ 1519.00 < T < 3000.00 : & 18739.51 - 13.2288 T - 1.656847E+30 T^{-9} \\ & + \text{GHSER}_{\text{Mn}} \end{aligned}$$


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**MOLYBDENUM****Molybdenum bcc-A2**

$$\text{GHSER}_{\text{Mo}} = G_{\text{Mo}}^{\text{bcc}-A2}(T) - H_{\text{Mo}}^{o,\text{bcc}-A2}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 2896.00 : & - 7746.302 + 131.9197 T - 23.56414 T \cdot \ln T \\ & - 0.003443396 T^2 + 5.66283E-07 T^3 + 65812 T^{-1} \\ & - 1.30927E-10 T^4 \\ 2896.00 < T < 5000.00 : & - 30556.41 + 283.559746 T - 42.63829 T \cdot \ln T \\ & - 4.849315E+33 T^{-9} \end{aligned}$$

**Molybdenum fcc-A1**

$$\text{GFCC}_{\text{Mo}} = G_{\text{Mo}}^{\text{fcc}-A1}(T) - H_{\text{Mo}}^{o,\text{bcc}-A2}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 2896.00 : & 7453.698 + 132.5497 T - 23.56414 T \cdot \ln T \\ & - 0.003443396 T^2 + 5.66283E-07 T^3 + 65812 T^{-1} \\ & - 1.30927E-10 T^4 \\ 2896.00 < T < 5000.00 : & - 15356.41 + 284.189746 T - 42.63829 T \cdot \ln T \\ & - 4.849315E+33 T^{-9} \end{aligned}$$

**Molybdenum hcp-A3**

$$\text{GHCP}_{\text{Mo}} = G_{\text{Mo}}^{\text{hcp}-A3}(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) =$$

$$298.15 < T < 5000.00 : 11550 + \text{GHSER}_{\text{Mo}}$$

**Molybdenum liquid**

$$\text{GLIQ}_{\text{Mo}} = G_{\text{Mo}}^{\text{liquid}}(T) - H_{\text{Mo}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) =$$

$$298.15 < T < 2896.00 : 34085.045 + 117.224788 T - 23.56414 T \cdot \ln T \\ - 0.003443396 T^2 + 5.66283E-07 T^3 + 65812 T^{-1} \\ - 1.30927E-10 T^4 + 4.24519E-22 T^7$$

$$2896.00 < T < 5000.00 : 3538.963 + 271.6697 T - 42.63829 T \cdot \ln T$$


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**NITROGEN****Nitrogen gas**

$$\text{GHSER}_{\text{N}} = G_{\text{N}}^{\text{gas}}(T) - H_{0.5\text{N}_2}^{\circ}(298.15 \text{ K}) =$$

$$298.15 < T < 950.00 : - 3750.675 - 9.45425 T - 12.7819 T \cdot \ln T \\ - 0.00176686 T^2 + 2.681E-09 T^3 - 32374 T^{-1}$$

$$950.00 < T < 3350.00 : - 7358.85 + 17.2003 T - 16.3699 T \cdot \ln T \\ - 6.5107E-04 T^2$$

$$+ 3.0097E-08 T^3 + 563070 T^{-1}$$

$$3350.00 < T < 6000.00 : - 16392.8 + 50.26 T - 20.4695 T \cdot \ln T \\ + 2.39754E-04 T^2 - 8.333E-09 T^3 + 4596375 T^{-1}$$

**Nitrogen liquid**

$$\text{GLIQ}_{\text{N}} = G_{\text{N}}^{\text{liquid}}(T) - H_{0.5\text{N}_2}^{\circ}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 29950 + 59.02 T + \text{GHSER}_{\text{N}}$$


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**NEODYMIUM****Neodymium dhcp**

$$\text{GHSER}_{\text{Nd}} = G_{\text{Nd}}^{\text{dhcp}} - H_{\text{Nd}}^{\circ,\text{dhcp}}(298.15 \text{ K}) =$$

$$298.15 < T < 900.00 : - 8402.93 + 111.10239 T - 27.0858 T \cdot \ln T \\ + 5.56125E-04 T^2 - 2.6923E-06 T^3 + 34887 T^{-1}$$

$$900.00 < T < 1128.00 : - 6984.083 + 83.662617 T - 22.7536 T \cdot \ln T \\ - 0.00420402 T^2 - 1.802E-06 T^3$$

$$1128.00 < T < 1799.00 : - 225610.846 + 1673.04075 T - 238.182873 T \cdot \ln T \\ + 0.078615997 T^2 - 6.048207E-06 T^3 + 38810350 T^{-1}$$

$$1799.00 < T < 2000.00 : - 25742.331 + 276.257088 T - 48.7854 T \cdot \ln T$$

**Neodymium bcc-A2**

$$\text{GBCC}_{\text{Nd}} = G_{\text{Nd}}^{\text{bcc}-\text{A}2} - H_{\text{Nd}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) =$$

298.15 <  $T$  < 400.00 :  $-6965.635 + 110.556109 T - 27.0858 T \cdot \ln T$   
 $+ 5.56125E-04 T^2 - 2.6923E-06 T^3 + 34887 T^{-1}$

400.00 <  $T$  < 1128.00 :  $+7312.2 - 153.033976 T + 14.9956777 T \cdot \ln T$   
 $- 0.050479 T^2 + 7.287217E-06 T^3 - 831810 T^{-1}$

1128.00 <  $T$  < 1289.00 :  $-18030.266 + 239.677322 T - 44.5596 T \cdot \ln T$

1289.00 <  $T$  < 1800.00 :  $+334513.017 - 2363.9199 T + 311.409193 T \cdot \ln T$   
 $- 0.156030778 T^2 + 1.2408421E-05 T^3 - 64319604 T^{-1}$

**Neodymium liquid**

$$\text{GLIQ}_{\text{Nd}} = G_{\text{Nd}}^{\text{bcc}-\text{A}2} - H_{\text{Nd}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) =$$

298.15 <  $T$  < 300.00 :  $-3351.187 + 109.517314 T - 27.0858 T \cdot \ln T$   
 $+ 5.56125E-04 T^2 - 2.6923E-06 T^3 + 34887 T^{-1}$

300.00 <  $T$  < 1128.00 :  $+5350.01 - 86.593963 T + 5.357301 T \cdot \ln T$   
 $- 0.046955463 T^2 + 6.860782E-06 T^3 - 374380 T^{-1}$

1128.00 <  $T$  < 1800.00 :  $-16335.232 + 268.625903 T - 48.7854 T \cdot \ln T$

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**NICKEL****Nickel fcc-A1(paramagnetic)**

$$\text{GHSER}_{\text{Ni}} = G_{\text{Ni}}^{\text{fcc}-\text{A}1,\text{para}} - H_{\text{Ni}}^{\circ,\text{fcc}-\text{A}1,\text{para}}(298.15 \text{ K}) =$$

298.15 <  $T$  < 1728.00 :  $-5179.159 + 117.854 T - 22.096 T \cdot \ln T$   
 $- 0.0048407 T^2$

1728.00 <  $T$  < 3000.00 :  $-27840.655 + 279.135 T - 43.1 T \cdot \ln T$   
 $+ 1.12754E+31 T^{-9}$

**Nickel bcc-A2(paramagnetic)**

$$\text{GBCC}_{\text{Ni}} = G_{\text{Ni}}^{\text{bcc}-\text{A}2} - H_{\text{Ni}}^{\circ,\text{bcc}-\text{A}1,\text{para}}(298.15 \text{ K}) =$$

298.15 <  $T$  < 1300.00 :  $+8715.084 - 3.556 T + \text{GHSER}_{\text{Ni}}$

**Nickel hcp-A3(paramagnetic)**

$$\text{GHCP}_{\text{Ni}} = G_{\text{Ni}}^{\text{hcp}-\text{A}3} - H_{\text{Ni}}^{\circ,\text{fcc}-\text{A}1,\text{para}}(298.15 \text{ K}) =$$

298.15 <  $T$  < 3000.00 :  $+1046 + 1.2552 T + \text{GHSER}_{\text{Ni}}$

**Nickel liquid**

$$\text{GLIQ}_{\text{Ni}} = G_{\text{Ni}}^{\text{liquid}} - H_{\text{Ni}}^{\circ,\text{fcc}-\text{A}1,\text{para}}(298.15 \text{ K}) =$$

298.15 <  $T$  < 1300.00 :  $16414.686 - 9.397 T - 3.82318E-21 T^7$   
 $+ \text{GHSER}_{\text{Ni}}$

1728.00 <  $T$  < 3000.00 :  $18290.88 - 10.537 T - 1.127554E+31 T^{-9}$   
 $+ \text{GHSER}_{\text{Ni}}$

## NIOBIUM

### Niobium bcc-A2

$$\begin{aligned} \text{GHSER}_{\text{Nb}} = G_{\text{Nb}}^{\text{bcc}-\text{A}2}(T) - H_{\text{Nb}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ 298.15 < T < 2750.00 : -8519.353 + 142.045475 T - 26.4711 T \cdot \ln T \\ &\quad + 2.03475E-04 T^2 - 3.5012E-07 T^3 + 93399 T^{-1} \\ 2750.00 < T < 1000.00 : -37669.3 + 271.720843 T - 41.77 T \cdot \ln T \\ &\quad + 1.528238E+32 T^{-9} \end{aligned}$$

### Niobium fcc-A1

$$\begin{aligned} \text{GFCC}_{\text{Nb}} = G_{\text{Nb}}^{\text{fcc}-\text{A}1}(T) - H_{\text{Nb}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 13500 + 1.7 T + \text{GHSER}_{\text{Nb}} \end{aligned}$$

### Niobium hcp-A3

$$\begin{aligned} \text{GHCP}_{\text{Nb}} = G_{\text{Nb}}^{\text{hcp}-\text{A}3}(T) - H_{\text{Nb}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ 298.15 < T < 5000.00 : 10000 + 2.4 T + \text{GHSER}_{\text{Nb}} \end{aligned}$$

### Niobium liquid

$$\begin{aligned} \text{GLIQ}_{\text{Nb}} = G_{\text{Nb}}^{\text{liquid}}(T) - H_{\text{Nb}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) = \\ 298.15 < T < 2750.00 : 29781.555 - 10.816417 T \\ &\quad - 3.06098E-23 T^7 \\ + \text{GHSER}_{\text{Nb}} \\ 298.15 < T < 2750.00 : 30169.9 - 10.9647 T - 1.52824E+32 T^{-9} \\ &\quad + \text{GHSER}_{\text{Nb}} \end{aligned}$$


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## SILICON

### Silicon diamond

$$\begin{aligned} \text{GHSER}_{\text{Si}} = G_{\text{Si}}^{\text{diamond}}(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ 298.15 < T < 1687.00 : -8162.609 + 137.236859 T - 22.8317533 T \cdot \ln T \\ &\quad - 1.912904E-3 T^2 - 0.003552E-6 T^3 + 176667 T^{-1} \\ 1687.00 < T < 3600.00 : -9457.642 + 167.281367 T - 27.196 T \cdot \ln T \\ &\quad - 420.369E28 T^{-9} \end{aligned}$$

### Silicon bcc-A2

$$\begin{aligned} \text{GBCC}_{\text{Si}} = G_{\text{Si}}^{\text{bcc}-\text{A}2}(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ 298.15 < T < 1687.00 : 47000.0 - 22.5 T + \text{GHSER}_{\text{Si}} \end{aligned}$$

### Silicon cbcc-A12

$$G_{\text{Si}}^{\text{bcc}-A12}(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 50208.0 - 20.377 T + \text{GHSER}_{\text{Si}}$$

**Silicon cub-A13**

$$G_{\text{Si}}^{\text{cub}-A13}(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 47279.0 - 20.377 T + \text{GHSER}_{\text{Si}}$$

**Silicon fcc-A1**

$$G_{\text{Si}}^{\text{fcc}-A1}(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 51000.00 - 21.8 T + \text{GHSER}_{\text{Si}}$$

**Silicon hcp-A3**

$$G_{\text{Si}}^{\text{hcp}-A3}(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 49200 - 20.8 T + \text{GHSER}_{\text{Si}}$$

**Silicon liquid**

$$G_{\text{Si}}^{\text{liquid}}(T) - H_{\text{Si}}^{\circ,\text{diamond}}(298.15 \text{ K}) = \\ 298.15 < T < 1687.00 : 50696.4 - 30.0994 T + 2.09307E-21 T^7 \\ + \text{GHSER}_{\text{Si}} \\ 1687.00 < T < 6000.00 : 49828.2 - 29.5591 T + 4.20369E+30 T^{-9} \\ + \text{GHSER}_{\text{Si}}$$


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**TANTALUM****Tantalum bcc-A2**

$$\text{GHSER}_{\text{Ta}} = G_{\text{Ta}}^{\text{bcc}-A2}(T) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ 298.15 < T < 1300.00 : -7285.889 + 119.139858 T - 23.7592624 T \cdot \ln T \\ - 0.002623033 T^2 + 1.70109E-07 T^3 - 3293 T^{-1} \\ 1300.00 < T < 2500.00 : -22389.955 + 243.88676 T - 41.137088 T \cdot \ln T \\ + 0.006167572 T^2 - 6.55136E-07 T^3 + 2429586 T^{-1} \\ 2500.00 < T < 3258.00 : +229382.886 - 722.59722 T + 78.5244752 T \cdot \ln T \\ - 0.017983376 T^2 + 1.95033E-07 T^3 - 93813648 T^{-1} \\ 3258.00 < T < 6000.00 : -963392.734 + 2773.7774 T - 337.227976 T \cdot \ln T \\ + 0.039791303 T^2 - 9.74251E-07 T^3 \\ + 5.09949511E+08 T^{-1}$$

**Tantalum fcc-A1**

$$\text{GFCC}_{\text{Ta}} = G_{\text{Ta}}^{\text{fcc}-A1}(T) - H_{\text{Ta}}^{\circ,\text{bcc}-A2}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 16000 + 1.7 T + \text{GHSER}_{\text{Ta}}$$

**Tantalum hcp-A3**

$$\text{GHCP}_{\text{Ta}} = G_{\text{Ta}}^{\text{hcp}-\text{A}3}(T) - H_{\text{Ta}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 12000 + 2.4 T + \text{GHSER}_{\text{Ta}}$$

**Tantalum liquid**

$$\text{GLIQ}_{\text{Ta}} = G_{\text{Ta}}^{\text{liquid}}(T) - H_{\text{Ta}}^{\circ,\text{bcc}-\text{A}2}(298.15 \text{ K}) =$$

$$298.15 < T < 1000.00 : 29160.975 - 7.578729 T$$

$$+ \text{GHSER}_{\text{Ta}}$$

$$1000.00 < T < 1300.00 : 51170.228 - 181.121652 T + 23.7872147 T \cdot \ln T$$

$$- 0.009707033 T^2 + 4.4449E-07 T^3 - 3520045 T^{-1}$$

$$+ \text{GHSER}_{\text{Ta}}$$

$$1300.00 < T < 2500.00 : 66274.294 - 305.868555 T + 41.1650403 T \cdot \ln T$$

$$- 0.018497638 T^2 + 1.269735E-06 T^3 - 5952924 T^{-1}$$

$$+ \text{GHSER}_{\text{Ta}}$$

$$2500.00 < T < 3290.00 : - 185498.547 + 660.615425 T - 78.4965229 T \cdot \ln T$$

$$+ 0.00565331 T^2 + 4.19566E-07 T^3 + 90290310 T^{-1}$$

$$+ \text{GHSER}_{\text{Ta}}$$

$$3290.00 < T < 6000.00 : 1036069.47 - 2727.38037 T + 320.319132 T \cdot \ln T$$

$$- 0.043117795 T^2 + 1.055148E-06 T^3$$

$$- 5.54714342E+08 T^{-1} + \text{GHSER}_{\text{Ta}}$$


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**TIN****Tin bct-A5**

$$\text{GHSER}_{\text{Sn}} = G_{\text{Sn}}^{\text{bct}-\text{A}5}(T) - H_{\text{Sn}}^{\circ,\text{bct}-\text{A}5}(298.15 \text{ K}) =$$

$$100.00 < T < 250.00 : - 7958.517 + 122.765451 T - 25.858 T \cdot \ln T$$

$$+ 0.51185E-3 T^2 - 3.192767E-6 T^3 + 18440 T^{-1}$$

$$250.00 < T < 505.078 : - 5855.135 + 65.443315 T - 15.961 T \cdot \ln T$$

$$- 18.8702E-3 T^2 + 3.121167E-6 T^3 - 61960 T^{-1}$$

$$505.078 < T < 800.00 : 2524.724 + 4.005269 T - 8.2590486 T \cdot \ln T$$

$$- 16.814429E-3 T^2 + 2.623131E-6 T^3 - 1081244 T^{-1}$$

$$- 123.07E23 T^{-9}$$

$$800.00 < T < 3000.00 : - 8256.959 + 138.99688 T - 28.4512 T \cdot \ln T$$

$$- 123.07E23 T^{-9}$$

**Tin bcc-A2**

$$\text{GBCC}_{\text{Sn}} = G_{\text{Sn}}^{\text{bcc}-\text{A}2}(T) - H_{\text{Sn}}^{\circ,\text{bct}-\text{A}5}(298.15 \text{ K}) =$$

$$100.00 < T < 3000.00 : 4400.00 - 6.0 T + \text{GHSER}_{\text{Sn}}$$

**Tin fcc-A1**

$$\text{GFCC}_{\text{Sn}} = G_{\text{Sn}}^{\text{fcc}-A1}(T) - H_{\text{Sn}}^{\text{o,bct}-A5}(298.15 \text{ K}) =$$

$$100.00 < T < 3000.00 : 5510.0 - 8.46 T + \text{GHSER}_{\text{Sn}}$$

**Tin hcp-A3**

$$\text{GHCP}_{\text{Sn}} = G_{\text{Sn}}^{\text{bcc}-A2}(T) - H_{\text{Sn}}^{\text{o,bct}-A5}(298.15 \text{ K}) =$$

$$100.00 < T < 3000.00 : 3900.00 - 4.4 T + \text{GHSER}_{\text{Sn}}$$

**Tin liquid**

$$\text{GLIQ}_{\text{Sn}} = G_{\text{Sn}}^{\text{liquid}}(T) - H_{\text{Sn}}^{\text{o,bct}-A5}(298.15 \text{ K}) =$$

$$100.00 < T < 505.078 : 7103.092 - 14.087767 T + 1.47031E-18 T^7$$

$$+ \text{GHSER}_{\text{Sn}}$$

$$505.078 < T < 3000.00 : 6971.587 - 13.814382 T + 1.2307E+25 T^{-9}$$

$$+ \text{GHSER}_{\text{Sn}}$$


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**TITANIUM****Titanium hcp-A3**

$$\text{GHSER}_{\text{Ti}} = G_{\text{Ti}}^{\text{hcp}-A3}(T) - H_{\text{Ti}}^{\text{o,hcp}-A3}(298.15 \text{ K}) =$$

$$298.15 < T < 900.00 : - 8059.921 + 133.615208 T - 23.9933 T \cdot \ln T$$

$$- 4.777975E-3 T^2 + 0.106716E-6 T^3 + 72636 T^{-1}$$

$$900.00 < T < 1155.00 : - 7811.815 + 132.988068 T - 23.9887 T \cdot \ln T$$

$$- 4.2033E-3 T^2 - 0.090876E-6 T^3 + 42680 T^{-1}$$

$$1155.00 < T < 1941.00 : 908.837 + 66.976538 T - 14.9466 T \cdot \ln T$$

$$- 8.1465E-3 T^2 + 0.202715E-6 T^3 - 1477660 T^{-1}$$

$$1941.00 < T < 4000.00 : - 124526.786 + 638.806871 T - 87.2182461 T \cdot \ln T$$

$$+ 8.204849E-3 T^2 - 0.304747E-6 T^3$$

$$+ 36699805 T^{-1}$$

**Titanium bcc-A2**

$$\text{GBCC}_{\text{Ti}} = G_{\text{Ti}}^{\text{bcc}-A2}(T) - H_{\text{Ti}}^{\text{o,hcp}-A3}(298.15 \text{ K}) =$$

$$298.15 < T < 1155.00 : - 1272.064 + 134.71418 T - 25.5768 T \cdot \ln T$$

$$- 0.663845E-3 T^2 - 0.278803E-6 T^3 + 7208 T^{-1}$$

$$1155.00 < T < 1941.00 : 6667.385 + 105.366379 T - 22.3771 T \cdot \ln T$$

$$+ 1.21707E-3 T^2 - 0.84534E-6 T^3 - 2002750 T^{-1}$$

$$1941.00 < T < 4000.00 : 26483.26 - 182.426471 T + 19.0900905 T \cdot \ln T$$

$$- 22.00832E-3 T^2 + 1.228863E-6 T^3 + 1400501 T^{-1}$$

**Titanium cbcc-A12**

$$G_{\text{Ti}}^{\text{cbcc-A12}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 4602.2 + \text{GHSER}_{\text{Ti}}$$

**Titanium bct-A5**

$$G_{\text{Ti}}^{\text{bct-A5}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 4602.2 + \text{GHSER}_{\text{Ti}}$$

**Titanium cub-A13**

$$G_{\text{Ti}}^{\text{cub-A13}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 7531.2 + \text{GHSER}_{\text{Ti}}$$

**Titanium diamond**

$$G_{\text{Ti}}^{\text{diamond}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 25000.00 + \text{GHSER}_{\text{Ti}}$$

**Titanium fcc-A1**

$$G_{\text{Ti}}^{\text{fcc-A1}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 6000.0 - 0.1 T + \text{GHSER}_{\text{Ti}}$$

**Titanium Laves-C14**

$$G_{\text{Ti:Ti}}^{\text{Laves-C14}}(T) - 3.0 H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 15000.0 + 3.0 \text{ GHSER}_{\text{Ti}}$$

**Titanium Laves-C15**

$$G_{\text{Ti:Ti}}^{\text{Laves-C14}}(T) - 3.0 H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 15000.0 + 3.0 \text{ GHSER}_{\text{Ti}}$$

**Titanium liquid**

$$G_{\text{Ti}}^{\text{liquid}}(T) - H_{\text{Ti}}^{\text{o,hcp-A3}}(298.15 \text{ K}) = \\ 298.15 < T < 1300.00 : + 12194.415 - 6.980938 T + \text{GHSER}_{\text{Ti}} \\ 1300.00 < T < 1941.00 : + 368610.36 - 2620.999038 T + 357.005867 T \cdot \ln T \\ - 155.262855E-03 T^2 + 12.254402E-06 T^3 \\ - 65556856 T^{-1} + \text{GHSER}_{\text{Ti}} \\ 1941.00 < T < 6000.00 : + 104639.72 - 340.070171 T + 40.9282461 T \cdot \ln T \\ - 8.204849E-03 T^2 + 0.304747E-06 T^3 \\ - 36699805 T^{-1} + \text{GHSER}_{\text{Ti}}$$


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## TUNGSTEN

### Tungsten bcc-A2

$$GHSER_W = G_W^{\text{bcc}-A2}(T) - H_W^{\circ,\text{bcc}-A2}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 3695.00 : & -7646.311 + 130.4 T - 24.1 T \cdot \ln T \\ & - 0.001936 T^2 + 2.07E-07 T^3 + 44500 T^{-1} \\ & - 5.33E-11 T^4 \\ 3695.00 < T < 6000.00 : & -82868.801 + 389.362335 T - 54 T \cdot \ln T \\ & + 1.528621E+33 T^{-9} \end{aligned}$$

### Tungsten fcc-A1

$$GFCC_W = G_W^{\text{fcc}-A1}(T) - H_W^{\circ,\text{bcc}-A2}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 3695.00 : & 11653.689 + 131.03 T - 24.1 T \cdot \ln T \\ & - 0.001936 T^2 + 2.07E-07 T^3 + 44500 T^{-1} \\ & - 5.33E-11 T^4 \\ 3695.00 < T < 6000.00 : & -63568.801 + 389.992335 T - 54 T \cdot \ln T \\ & + 1.528621E+33 T^{-9} \end{aligned}$$

### Tungsten hcp-A3

$$GHCP_W = G_W^{\text{hcp}-A3}(T) - H_W^{\circ,\text{bcc}-A2}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 3695.00 : & 7103.689 + 130.4 T - 24.1 T \cdot \ln T \\ & - 0.001936 T^2 + 2.07E-07 T^3 + 44500 T^{-1} \\ & - 5.33E-11 T^4 \\ 3695.00 < T < 6000.00 : & -68118.801 + 389.362335 T - 54 T \cdot \ln T \\ & + 1.528621E+33 T^{-9} \end{aligned}$$

### Tungsten liquid

$$GLIQ_W = G_W^{\text{liquid}}(T) - H_W^{\circ,\text{bcc}-A2}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 3695.00 : & 44514.273 + 116.29001 T - 24.1 T \cdot \ln T \\ & - 0.001936 T^2 + 2.07E-07 T^3 + 44500 T^{-1} \\ & - 5.33E-11 T^4 - 2.713468E-24 T^7 \\ 3695.00 < T < 6000.00 : & -30436.051 + 375.175 T - 54 T \cdot \ln T \end{aligned}$$


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## VANADIUM

### Vanadium bcc-A2

$$GHSER_V = G_V^{\text{bcc}-A2}(T) - H_V^{\circ,\text{bcc}-A2}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 790.00 : & -7930.43 + 133.346053 T - 24.134 T \cdot \ln T \\ & - 3.098E-3 T^2 + 0.12175E-6 T^3 + 69460 T^{-1} \end{aligned}$$

$$\begin{aligned}
 298.15 < T < 2183.00 : & -7967.842 + 143.291093 T - 25.9 T \cdot \ln T \\
 & + 0.0625E-3 T^2 - 0.68E-6 T^3 \\
 2183.00 < T < 4000.00 : & -41689.864 + 321.140783 T - 47.43 T \cdot \ln T \\
 & + 644.389E29 T^{-9}
 \end{aligned}$$

**Vanadium fcc-A1**

$$\begin{aligned}
 \text{GFCC}_V = G_V^{\text{fcc}-A1}(T) - H_V^{\text{o},\text{bcc}-A2}(298.15 \text{ K}) = \\
 298.15 < T < 4000.00 : 7500.0 + 1.7 T + \text{GHSER}_V
 \end{aligned}$$

**Vanadium hcp-A3**

$$\begin{aligned}
 \text{GHCP}_V = G_V^{\text{hcp}-A3}(T) - H_V^{\text{o},\text{bcc}-A2}(298.15 \text{ K}) = \\
 298.15 < T < 4000.00 : 4000.0 + 2.4 T + \text{GHSER}_V
 \end{aligned}$$

**Vanadium liquid**

$$\begin{aligned}
 \text{GLIQ}_V = G_V^{\text{liquid}}(T) - H_V^{\text{o},\text{bcc}-A2}(298.15 \text{ K}) = \\
 298.15 < T < 2183.00 : 20764.117 - 9.455552 T - 5.19136E-22 T^7 \\
 & + \text{GHSER}_V \\
 2183.00 < T < 6000.00 : 22072.353 - 10.0848 T - 6.44389E+31 T^{-9} \\
 & + \text{GHSER}_V
 \end{aligned}$$


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**YTTRIUM****Yttrium hcp-A3**

$$\begin{aligned}
 \text{GHSER}_Y = G_Y^{\text{hcp}-A3}(T) - H_Y^{\text{o},\text{hcp}-A3}(298.15 \text{ K}) = \\
 298.15 < T < 1500.00 : -7347.055 + 117.532124 T - 23.8685 T \cdot \ln T \\
 & - 0.003845475 T^2 + 1.1125E-08 T^3 - 16486 T^{-1} \\
 1500.00 < T < 1799.00 : -15802.62 + 229.831717 T - 40.2851 T \cdot \ln T \\
 & + 0.0068095 T^2 - 1.14182E-06 T^3 \\
 1799.00 < T < 3700.00 : -72946.216 + 393.885821 T - 58.2078433 T \cdot \ln T \\
 & + 0.002436461 T^2 - 7.2627E-08 T^3 + 20866567 T^{-1}
 \end{aligned}$$

**Yttrium bcc-A2**

$$\begin{aligned}
 \text{GBCC}_Y = G_Y^{\text{bcc}-A2}(T) - H_Y^{\text{o},\text{hcp}-A3}(298.15 \text{ K}) = \\
 298.15 < T < 1752.00 : -1861.198 + 97.522398 T - 20.940576 T \cdot \ln T \\
 & - 0.007995833 T^2 + 7.58716E-07 T^3 - 54349 T^{-1} \\
 1752.00 < T < 1799.00 : -10207.724 + 195.741984 T - 35.0201 T \cdot \ln T \\
 1799.00 < T < 3700.00 : +104813.954 - 386.167564 T + 39.8075986 T \cdot \ln T
 \end{aligned}$$

**Yttrium liquid**

$$\text{GLIQ}_Y = G_Y^{\text{liquid}}(T) - H_Y^{\circ,\text{hcp}-A3}(298.15 \text{ K}) =$$

298.15 <  $T$  < 1799.00 :  $3934.121 + 59.921688 T - 14.8146562 T \cdot \ln T$   
                                   - 0.015623487  $T^2 + 1.442946\text{E-}06 T^3$   
                                   - 140695  $T^{-1}$

1799.00 <  $T$  < 3700.00 :  $-13337.609 + 258.004539 T - 43.0952 T \cdot \ln T$   
                                   - 0.019918739  $T^2 + 8.41308\text{E-}07 T^3$   
                                   - 31549963  $T^{-1}$

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**ZINC****Zinc hcp-Zn**

$$\text{GHSER}_{Zn} = G_{Zn}^{\text{hcp}-Zn}(T) - H_{Zn}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) =$$

298.15 <  $T$  < 692.68 :  $-7285.787 + 118.470069 T - 23.701314 T \cdot \ln T$   
                                   - 1.712034E-3  $T^2 - 1.264963\text{E-}6 T^3$

692.68 <  $T$  < 1700.00 :  $-11070.559 + 172.34566 T - 31.38 T \cdot \ln T$   
                                   + 470.514E24  $T^{-9}$

**Zinc hcp-A3**

$$G_{Zn}^{\text{hcp}-A3}(T) - H_{Zn}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) =$$

298.15 <  $T$  < 1700 :  $2970 - 1.57 T + \text{GHSER}_{Zn}$

**Zinc bcc-A2**

$$\text{GBCC}_{Zn} = G_{Zn}^{\text{bcc}-A2}(T) - H_{Zn}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) =$$

298.15 <  $T$  < 6000.00 :  $2886.96 - 2.5104 T + \text{GHSER}_{Zn}$

**Zinc bct-A5**

$$G_{Zn}^{\text{bct}-A5}(T) - H_{Zn}^{\circ,\text{hcp}-Zn} =$$

298.15 <  $T$  < 6000.00 :  $2886.96 - 2.5104 T + \text{GHSER}_{Zn}$

**Zinc fcc-A1**

$$G_{Zn}^{\text{fcc}-A1}(T) - H_{Zn}^{\circ,\text{hcp}-Zn}(298.15 \text{ K}) =$$

298.15 <  $T$  < 6000.00 :  $2969.82 - 1.56968 T + \text{GHSER}_{Zn}$

**Zinc liquid**

$$G_{\text{Zn}}^{\text{liquid}}(T) - H_{\text{Zn}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 692.68 & : 7157.213 - 10.29299 \cdot T - 3.5896\text{E-}19 \cdot T^7 \\ & + \text{GHSER}_{\text{Zn}} \\ 692.68 < T < 1700.00 & : 7450.168 - 10.737066 \cdot T - 4.7051\text{E+}26 \cdot T^{-9} \\ & + \text{GHSER}_{\text{Zn}} \end{aligned}$$


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**ZIRCONIUM****Zirconium hcp-A3**

$$\text{GHSER}_{\text{Zr}} = G_{\text{Zr}}^{\text{T,hcp-A3}}(T) - H_{\text{Zr}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 2128.00 & : -7827.595 + 125.64905 \cdot T - 24.1618 \cdot T \cdot \ln T \\ & - 4.37791\text{E-}3 \cdot T^2 + 34971 \cdot T^{-1} \\ 2128.00 < T < 4000.00 & : -26085.921 + 262.724183 \cdot T - 42.144 \cdot T \cdot \ln T \\ & - 1342.895\text{E}28 \cdot T^{-9} \end{aligned}$$

**Zirconium bcc-A2**

$$\text{GBCC}_{\text{Zr}} = G_{\text{Zr}}^{\text{T,bcc-A2}}(T) - H_{\text{Zr}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$\begin{aligned} 298.15 < T < 2128.00 & : 7302.056 - 0.70335 \cdot T - 1.445606 \cdot T \cdot \ln T \\ & + 4.037826\text{E-}3 \cdot T^2 - 9.7289735\text{E-}9 \cdot T^3 \\ & - 7.6142894\text{E-}11 \cdot T^4 - 9737.0 \cdot T^{-1} + \text{GHSER}_{\text{Zr}} \\ 2128.00 < T < 4000.00 & : -4620.034 + 1.55998 \cdot T + 1.41035\text{E+}32 \cdot T^{-9} \end{aligned}$$

**Zirconium fcc-A1**

$$\text{GFCC}_{\text{Zr}} = G_{\text{Zr}}^{\text{fcc-A1}}(T) - H_{\text{Zr}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$130.00 < T < 4000.00 : 7600.00 - 0.9 \cdot T + \text{GHSER}_{\text{Zr}}$$

**Zirconium liquid**

$$\text{GLIQ}_{\text{Zr}} = G_{\text{Zr}}^{\text{liquid}}(T) - H_{\text{Zr}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$\begin{aligned} 130.00 < T < 2128.00 & : +18147.703 - 9.080762 \cdot T + 1.6275\text{E-}22 \cdot T^7 \\ & + \text{GHSER}_{\text{Zr}} \\ 2128.00 < T < 4000.00 & : +17804.649 - 8.91153 \cdot T + 1.343\text{E+}31 \cdot T^{-9} \\ & + \text{GHSER}_{\text{Zr}} \end{aligned}$$

**Zirconium Laves-C14**

$$G_{\text{Zr:Zr}}^{\text{Zr,Laves-C14}} - 3.0 \cdot H_{\text{Zr}}^{\text{o,hcp-A3}}(298.15 \text{ K}) =$$

$$298.15 < T < 6000.00 : 15000.0 + 3.0 \cdot \text{GHSER}_{\text{Zr}}$$

**Zirconium Laves-C15**

$$G_{\text{Zr:Zr}}^{\text{Zr,Laves-C15}} - 3.0 \ H_{\text{Zr}}^{\text{o,hcp-43}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 15000.0 + 3.0 \ \text{GHSER}_{\text{Zr}}$$

**Zirconium Laves-C36**

$$G_{\text{Zr:Zr}}^{\text{Zr,Laves-C36}} - 3.0 \ H_{\text{Zr}}^{\text{o,hcp-43}}(298.15 \text{ K}) = \\ 298.15 < T < 6000.00 : 15000.0 + 3.0 \ \text{GHSER}_{\text{Zr}}$$

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**APPENDIX II: MAGNETIC CONTRIBUTION TO THE GIBBS ENERGIES OF THE PURE ELEMENTS (S.I. units)<sup>1</sup>**


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$$G^{\text{mag}} = R T \ln (\beta^{\text{mag}} + 1) g(\tau)$$

**Chromium****Chromium bcc-A2**

$$T_{\text{N},\text{(bcc-A2,Cr)}} = 311.5 \quad \beta^{\text{mag}}(\text{bcc-A2,Cr}) = 0.008$$

**Chromium fcc-A1**

$$T_{\text{N},\text{(fcc-A1,Cr)}} = 369.667 \quad \beta^{\text{mag}}(\text{fcc-A1,Cr}) = 0.82$$

**Chromium hcp-A3**

$$T_{\text{N},\text{(hcp-A3,Cr)}} = 369.667 \quad \beta^{\text{mag}}(\text{hcp-A3,Cr}) = 0.82$$

**Iron****Iron bcc-A2**

$$T_{\text{c},\text{(bcc-A2,Fe)}} = 1043.0 \quad \beta^{\text{mag}}(\text{bcc-A2,Fe}) = 2.22$$

**Iron fcc-A1**

$$T_{\text{c},\text{(fcc-A1,Fe)}} = 1043.0 \quad \beta^{\text{mag}}(\text{fcc-A1,Fe}) = 2.22$$

**Manganese****Manganese cbcc-A12**

$$T_{\text{N},\text{(cbcc-A12,Mn)}} = 95.0 \quad \beta^{\text{mag}}(\text{cbcc-A12,Mn}) = 0.22$$

**Manganese bcc-A2**

$$T_{\text{N},\text{(bcc-A2,Mn)}} = 580.0 \quad \beta^{\text{mag}}(\text{bcc-A2,Mn}) = 0.27$$

**Manganese fcc-A1**

$$T_{\text{N},\text{(fcc-A1,Mn)}} = 540.0 \quad \beta^{\text{mag}}(\text{fcc-A1,Mn}) = 0.62$$

**Manganese hcp-A3**

$$T_{\text{N},\text{(hcp-A3,Mn)}} = 540.0 \quad \beta^{\text{mag}}(\text{hcp-A3,Mn}) = 0.62$$

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<sup>1</sup>Scientific Group Thermodata Europe (S.G.T.E.) Data for Pure Elements, A.T. Dinsdale, Calphad, 15, 4, 317 - 425 (1991).

**Nickel****Nickel bcc-A2**

$$T_c(\text{bcc-A2}, \text{Ni}) = 575.0 \quad \beta^{\text{mag}}(\text{bcc-A2}, \text{Ni}) = 0.85$$

**Nickel fcc-A1**

$$T_c(\text{fcc-A1}, \text{Ni}) = 633.0 \quad \beta^{\text{mag}}(\text{fcc-A1}, \text{Ni}) = 0.52$$

**Nickel hcp-A3**

$$T_c(\text{hcp-A3}, \text{Ni}) = 633.0 \quad \beta^{\text{mag}}(\text{hcp-A3}, \text{Ni}) = 0.52$$


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**bcc-A2**

$$\text{for } \tau = T < T_c \quad g(\tau) = 1 - 0.905299383 \tau^{-1} - 0.153008346 \tau^3 \\ - 0.00680037095 \tau^9 - 0.00153008346 \tau^{15}$$

$$\text{for } \tau = T_c < T \quad g(\tau) = - 0.0641731208 \tau^{-5} - 0.00203724193 \tau^{-15} \\ - 4.27820805E-04 \tau^{-25}$$

**cubic-A12**

$$\text{for } \tau = T < T_c \quad g(\tau) = 1 - 0.860338755 \tau^{-1} - 0.17449124 \tau^3 \\ - 0.00775516624 \tau^9 - 0.0017449124 \tau^{15}$$

$$\text{for } \tau = T_c < T \quad g(\tau) = - 0.0426902268 \tau^{-5} - 0.0013552453 \tau^{-15} \\ - 2.84601512E-04 \tau^{-25}$$

**fcc-A1**

$$\text{for } \tau = T < T_c \quad g(\tau) = 1 - 0.860338755 \tau^{-1} - 0.17449124 \tau^3 \\ - 0.00775516624 \tau^9 - 0.0017449124 \tau^{15}$$

$$\text{for } \tau = T_c < T \quad g(\tau) = - 0.0426902268 \tau^{-5} - 0.0013552453 \tau^{-15} \\ - 2.84601512E-04 \tau^{-25}$$

**hcp-A3**

$$\text{for } \tau = T < T_c \quad g(\tau) = 1 - 0.860338755 \tau^{-1} - 0.17449124 \tau^3 \\ - 0.00775516624 \tau^9 - 0.0017449124 \tau^{15}$$

$$\text{for } \tau = T_c < T \quad g(\tau) = - 0.0426902268 \tau^{-5} - 0.0013552453 \tau^{-15} \\ - 2.84601512E-04 \tau^{-25}$$





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