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EE 521: Analysis of Power Systems

Lecture 5 *Equivalent Networks*

Fall 2009

Mondays & Wednesdays 5:45-7:00

August 24 – December 18

Test 216

Topics

- Recap of Power Flow and Matrix Operations
- Matrix Inversion Update
- Gaussian Elimination (Kron Reduction)
- Ward Equivalent
- Ward Equivalent – PV

Recap of Power Flow and Matrix Operations

- Power Flow Equations
- Power Flow Solutions
 - Newton-Raphson Method
 - Decoupled Power Flow
 - DC Power Flow
- Matrix LU Decomposition
 - Crout's Method
 - Dolittle's Method

$$I = YV$$

$$E^* I = E^* YV$$

$$\begin{bmatrix} \theta^{n+1} \\ V^{n+1} \end{bmatrix} = \begin{bmatrix} \theta^n \\ V^n \end{bmatrix} - [J(x^n)]^{-1} \begin{bmatrix} \Delta P(x^n) \\ \Delta Q(x^n) \end{bmatrix}$$

$$Ax = b$$

$$LUx = b$$

$$\begin{cases} Lz = b \\ Ux = z \end{cases}$$

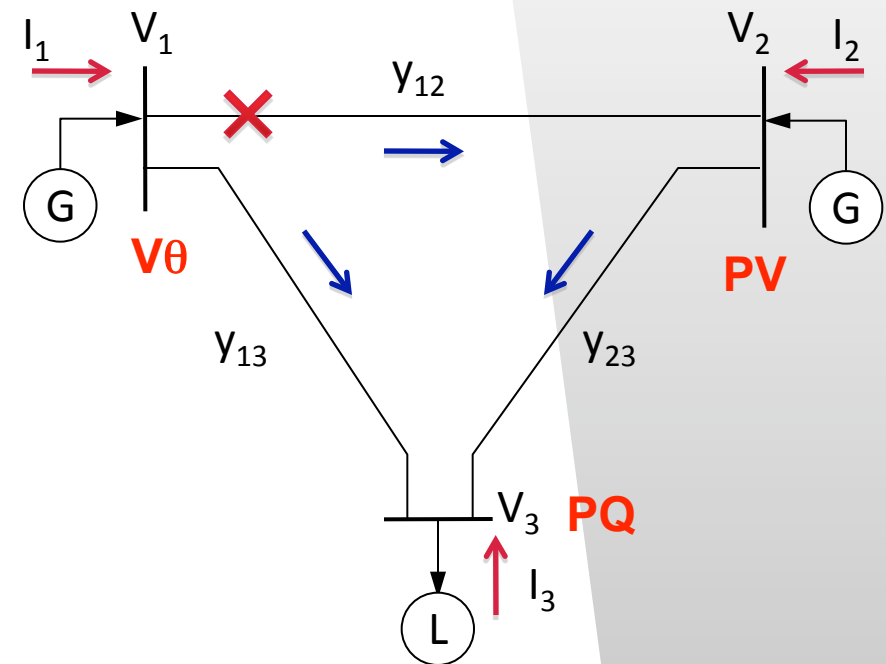
Matrix Update for Contingency Analysis

$$\begin{aligned}
 Y_{new} &= A^T \begin{bmatrix} y_{12} - y_{12} & 0 & 0 \\ 0 & y_{23} & 0 \\ 0 & 0 & y_{13} \end{bmatrix} A \\
 &= A^T \begin{bmatrix} y_{12} & 0 & 0 \\ 0 & y_{23} & 0 \\ 0 & 0 & y_{13} \end{bmatrix} A + A^T \begin{bmatrix} -y_{12} & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} A \\
 &= Y + A^T y A
 \end{aligned}$$

$$Y_{new}^{-1} ?$$

A more general problem:

$$\text{Known } A^{-1}, A_{new} = A + \Delta A, A_{new}^{-1} ?$$



Sherman-Morrison-Woodbury

- When a network is changed the calculated inverse is no longer valid, e.g. topology reconfiguration
- Methods exist for the “updating” of a matrix inversion when there are changes to the source matrix without performing the matrix inversion again

$$(A + uv)^{-1} = A^{-1} - \frac{A^{-1}uvA^{-1}}{1 + vA^{-1}u}$$

Simplification for a symmetric matrix

$$(A + uaa^T)^{-1} = A^{-1} - \gamma bb^T$$

$$b = A^{-1}a$$

$$\gamma = (u^{-1} + a^T b)^{-1}$$

Example: Sherman-Morrison-Woodbury

Problem: find A_{new}^{-1}

$$A = \begin{bmatrix} 2 & 1 & 0 \\ 1 & 2 & 1 \\ 0 & 1 & 1 \end{bmatrix} \quad A^{-1} = \begin{bmatrix} 1 & -1 & 1 \\ -1 & 2 & -2 \\ 1 & -2 & 3 \end{bmatrix}$$

$$A_{\text{new}} = \begin{bmatrix} 2 & 1 & 0 \\ 1 & 4 & 1 \\ 0 & 1 & 1 \end{bmatrix} = A + 2 \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} \begin{bmatrix} 0 & 1 & 0 \end{bmatrix}$$

Solution:

$$b = A^{-1}a = \begin{bmatrix} -1 & 2 & -1 \end{bmatrix} \quad \gamma = (u^{-1} + a^T b)^{-1} = 0.4$$

$$A_{\text{new}}^{-1} = \begin{bmatrix} 1 & -1 & 1 \\ -1 & 2 & -2 \\ 1 & -2 & 3 \end{bmatrix} - 0.4 \begin{bmatrix} -1 \\ 2 \\ -2 \end{bmatrix} \begin{bmatrix} -1 & 2 & -2 \end{bmatrix} = \begin{bmatrix} 0.6 & -0.2 & 0.2 \\ -0.2 & 0.4 & -0.4 \\ 0.2 & -0.4 & 1.4 \end{bmatrix}$$

Equivalent Networks

- Solving the power flow problem for the entire electrical network is not always practical
- In general, an individual balancing authority has authority over only a small portion of the electrical network
- Individual nodes can be “collapsed” to form an equivalent network
- Large portions of a system can be represented as an equivalent network

Gaussian Elimination (Kron Reduction)

- For an arbitrary 4 node system the equations are

$$Y_{11}V_1 + Y_{12}V_2 + Y_{13}V_3 + Y_{14}V_4 = I_1 \quad 1.1$$

$$Y_{21}V_1 + Y_{22}V_2 + Y_{23}V_3 + Y_{24}V_4 = I_2 \quad 1.2$$

$$Y_{31}V_1 + Y_{32}V_2 + Y_{33}V_3 + Y_{34}V_4 = I_3 \quad 1.3$$

$$Y_{41}V_1 + Y_{42}V_2 + Y_{43}V_3 + Y_{44}V_4 = I_4 \quad 1.4$$

- The first step is to pivot about the node to be reduced

$$V_1 + \frac{Y_{12}}{Y_{11}}V_2 + \frac{Y_{13}}{Y_{11}}V_3 + \frac{Y_{14}}{Y_{11}}V_4 = \frac{1}{Y_{11}}I_1 \quad 1.5$$

Gaussian Elimination (Kron Reduction) *cont'd*

- Multiply (1.5) by Y_{21} , Y_{31} , Y_{41} and subtract from (1.2) to (1.4), respectively

$$\left(Y_{22} - \frac{Y_{21}Y_{12}}{Y_{11}}\right)V_2 + \left(Y_{23} - \frac{Y_{21}Y_{13}}{Y_{11}}\right)V_3 + \left(Y_{24} - \frac{Y_{21}Y_{14}}{Y_{11}}\right)V_4 = I_2 - \frac{Y_{21}}{Y_{11}}I_1$$

$$\left(Y_{32} - \frac{Y_{31}Y_{12}}{Y_{11}}\right)V_2 + \left(Y_{33} - \frac{Y_{31}Y_{13}}{Y_{11}}\right)V_3 + \left(Y_{34} - \frac{Y_{31}Y_{14}}{Y_{11}}\right)V_4 = I_3 - \frac{Y_{31}}{Y_{11}}I_1$$

$$\left(Y_{42} - \frac{Y_{41}Y_{12}}{Y_{11}}\right)V_2 + \left(Y_{43} - \frac{Y_{41}Y_{13}}{Y_{11}}\right)V_3 + \left(Y_{44} - \frac{Y_{41}Y_{14}}{Y_{11}}\right)V_4 = I_4 - \frac{Y_{41}}{Y_{11}}I_1$$

$$Y_{22}^{(1)}V_2 + Y_{23}^{(1)}V_3 + Y_{24}^{(1)}V_4 = I_2^{(1)}$$

$$Y_{32}^{(1)}V_2 + Y_{33}^{(1)}V_3 + Y_{34}^{(1)}V_4 = I_3^{(1)}$$

$$Y_{42}^{(1)}V_2 + Y_{43}^{(1)}V_3 + Y_{44}^{(1)}V_4 = I_4^{(1)}$$

$$Y_{ij}^{(1)} = \left(Y_{ij} - \frac{Y_{ik}Y_{kj}}{Y_{kk}}\right)$$

$$I_i^{(1)} = I_i - \frac{Y_{ik}}{Y_{kk}}I_k$$

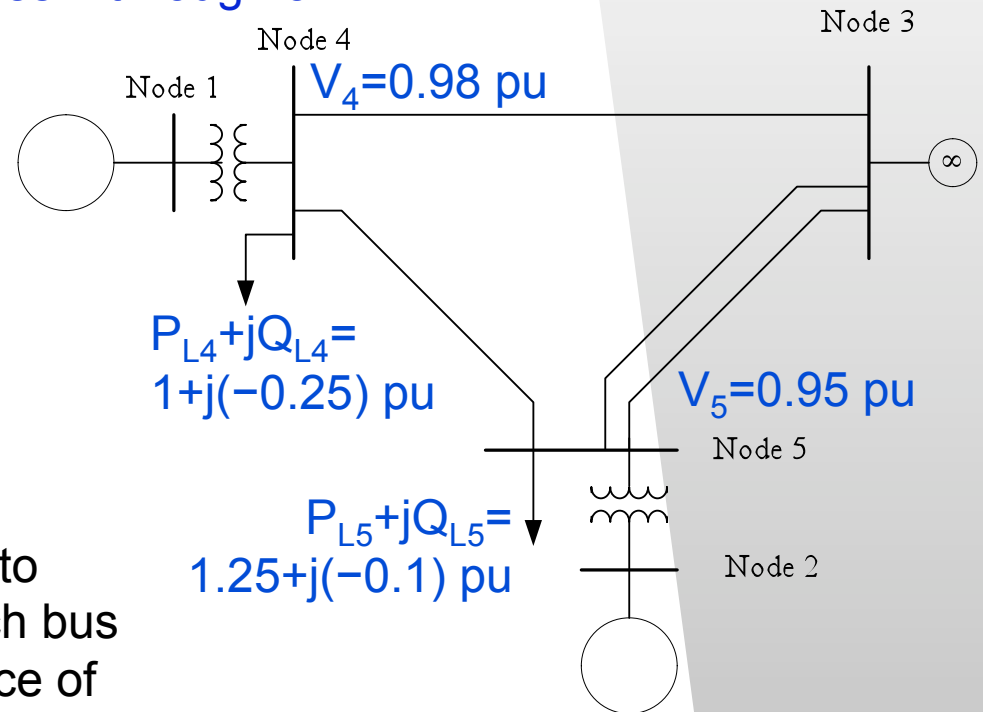
Gaussian Elimination (Kron Reduction) *cont'd*

- By pivoting around multiple nodes, the system can be reduced significantly
- For a large system, the model can be reduced to only the generator buses and their interconnections
 - Especially useful when studying dynamic stability of a power system (*a topic will be addressed later*)
- This requires the conversion of loads from constant power to constant impedance

Example: Gaussian Elimination (Kron Reduction)

Problem: Bus admittance matrix and power flow solution are given. Reduce the network to retain only generator buses 1 through 3

$$Y_{bus} = \begin{bmatrix} -j12.5 & 0 & 0 & j12.5 & 0 \\ 0 & -j12.5 & 0 & 0 & j12.5 \\ 0 & 0 & -j14 & j4 & j10 \\ j12.5 & 0 & j4 & -j21.5 & j5 \\ 0 & j12.5 & j10 & j5 & -j27.5 \end{bmatrix}$$



Solution:

Step 1: Perform a complete power flow to determine the voltage magnitude at each bus

Step 2: Calculate the effective impedance of the loads based on the voltage magnitude

Step 3: Perform a Gaussian elimination to remove bus 4 and 5

Example: Gaussian Elimination (Kron Reduction) *cont'd*

Effective load impedance:

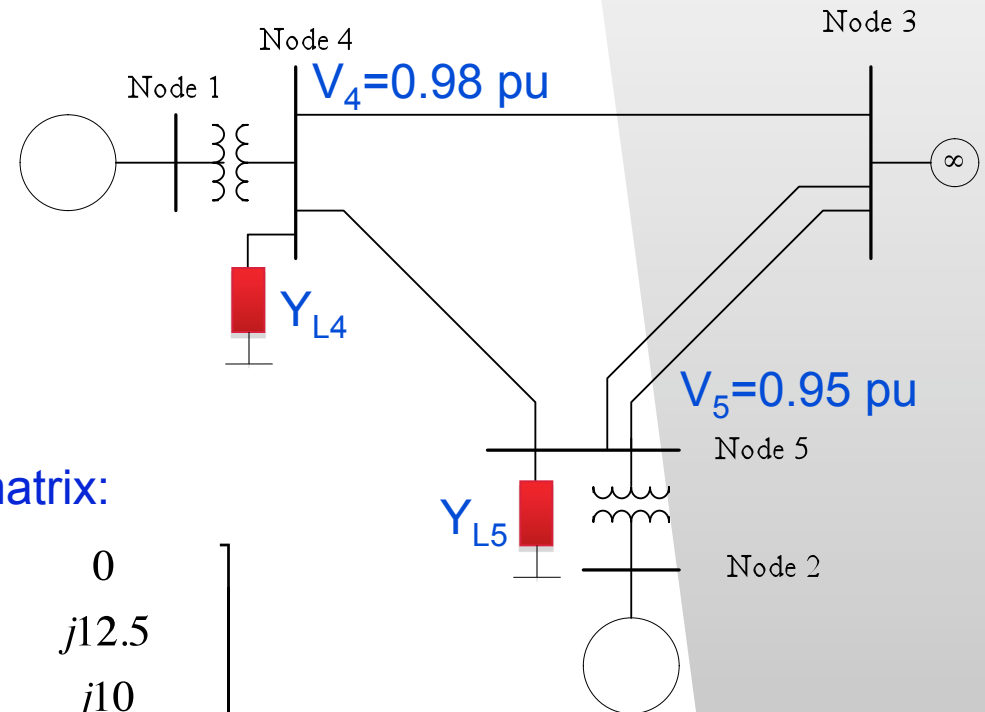
$$Y_L = \frac{P_L - jQ_L}{|V_L|^2}$$

$$Y_{L4} = \frac{P_{L4} - jQ_{L4}}{|V_4|^2} = \frac{1 + j0.25}{0.98^2} = 1.04 + j0.26$$

$$Y_{L5} = \frac{P_{L5} - jQ_{L5}}{|V_5|^2} = \frac{1.25 + j0.1}{0.95^2} = 1.39 + j0.11$$

Include effective load impedance in Y matrix:

$$Y_{bus}^{(1)} = \begin{bmatrix} -j12.5 & 0 & 0 & j12.5 & 0 \\ 0 & -j12.5 & 0 & 0 & j12.5 \\ 0 & 0 & -j14 & j4 & j10 \\ j12.5 & 0 & j4 & 1.04 - j21.24 & j5 \\ 0 & j12.5 & j10 & j5 & 1.39 - j27.39 \end{bmatrix}$$



Example: Gaussian Elimination (Kron Reduction) *cont'd*

Formulate new network equations:

$$\begin{bmatrix} -j12.5 & 0 & 0 & j12.5 & 0 \\ 0 & -j12.5 & 0 & 0 & j12.5 \\ 0 & 0 & -j14 & j4 & j10 \\ j12.5 & 0 & j4 & 1.04 - j21.24 & j5 \\ 0 & j12.5 & j10 & j5 & 1.39 - j27.39 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \\ V_5 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ 0 \\ 0 \end{bmatrix}$$

Pivot around node 4:

$$\begin{bmatrix} 0.36 - j5.16 & 0 & 0.11 + j2.35 & 0 & 0.14 + j2.94 \\ 0 & -j12.5 & 0 & 0 & j12.5 \\ 0.12 + j2.35 & 0 & 0.04 - j13.25 & 0 & 0.05 + j10.94 \\ 0 & 0 & 0 & 0 & 0 \\ 0.14 + j2.94 & j12.5 & 0.05 + j10.94 & 0 & 1.45 - j26.22 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \\ V_5 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ 0 \\ 0 \end{bmatrix}$$

$$Y_{ij}^{(1)} = \left(Y_{ij} - \frac{Y_{ik} Y_{kj}}{Y_{kk}} \right)$$

$$I_i^{(1)} = I_i - \frac{Y_{ik}}{Y_{kk}} I_k$$

Example: Gaussian Elimination (Kron Reduction) *cont'd*

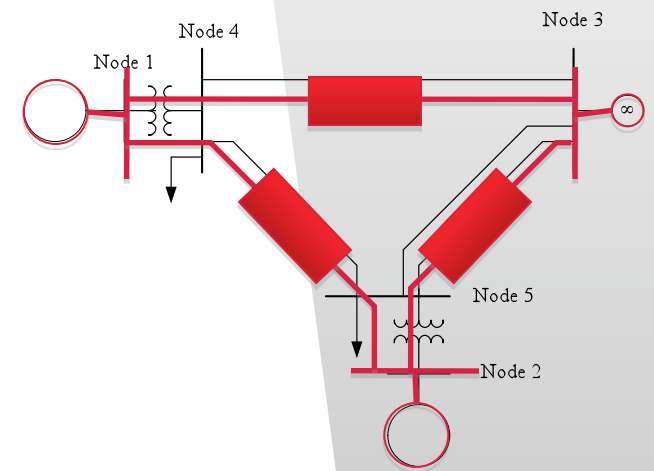
Pivot around node 5:

$$\begin{bmatrix} 0.41 - j4.83 & 0.14 + j1.39 & 0.24 + j3.57 & 0 \\ 0.14 + j1.39 & 0.33 - j6.56 & 0.31 + j5.20 & 0 \\ 0.25 + j3.57 & 0.31 + j5.20 & 0.33 - j8.70 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_5 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ 0 \end{bmatrix}$$

The resulting reduced equations:

$$\begin{bmatrix} 0.41 - j4.83 & 0.14 + j1.39 & 0.24 + j3.57 \\ 0.14 + j1.39 & 0.33 - j6.56 & 0.31 + j5.20 \\ 0.25 + j3.57 & 0.31 + j5.20 & 0.33 - j8.70 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix}$$

Tip: the resulting matrix should be symmetrical as the original matrix.



Elimination of a Group of Nodes

- Matrix form of Gaussian Elimination (Kron reduction)

$$\begin{bmatrix} Y_{ee} & Y_{er} \\ Y_{re} & Y_{rr} \end{bmatrix} \begin{bmatrix} V_e \\ V_r \end{bmatrix} = \begin{bmatrix} I_e \\ I_r \end{bmatrix}$$

“e” = eliminated nodes
“r” = retained nodes

$$Y_{ee}V_e + Y_{er}V_r = I_e$$

$$\Rightarrow V_e = Y_{ee}^{-1}I_e - Y_{ee}^{-1}Y_{er}V_r$$

$$(Y_{rr} - Y_{re}Y_{ee}^{-1}Y_{er})V_r = I_r - Y_{re}Y_{ee}^{-1}I_e$$

Example: Elimination of a Group of Nodes

$$(Y_{rr} - Y_{re}Y_{ee}^{-1}Y_{er})V_r = I_r - Y_{re}Y_{ee}^{-1}I_e$$

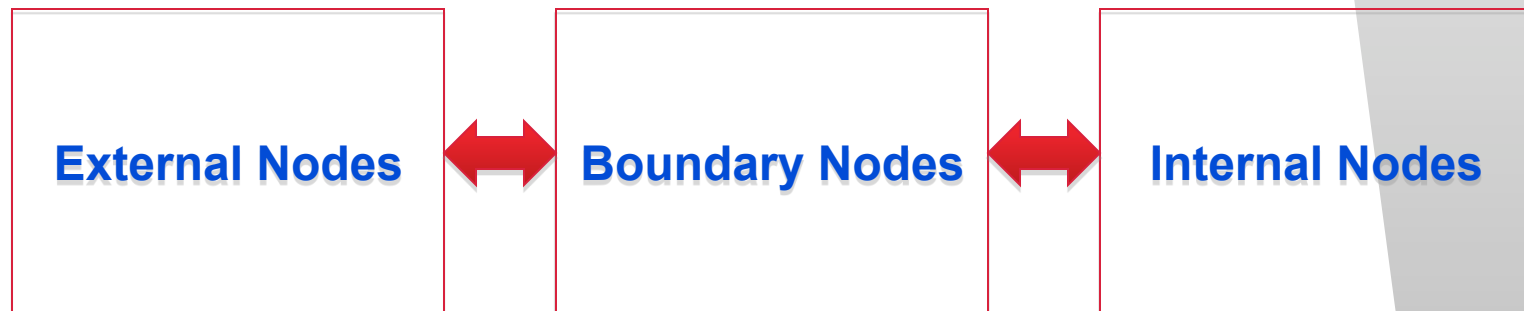
$$\begin{array}{ccc|ccc} -j12.5 & 0 & 0 & j12.5 & 0 & \\ 0 & Y_{rr} & 0 & 0 & Y_{re} & j12.5 \\ 0 & 0 & -j14 & j4 & Y_{re} & j10 \\ \hline j12.5 & 0 & j4 & 1.04 - j21.24 & Y_{ee} & j5 \\ 0 & Y_{er} & j10 & j5 & Y_{ee} & 0.69 - j27.39 \end{array} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \\ V_5 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ 0 \\ 0 \end{bmatrix}$$

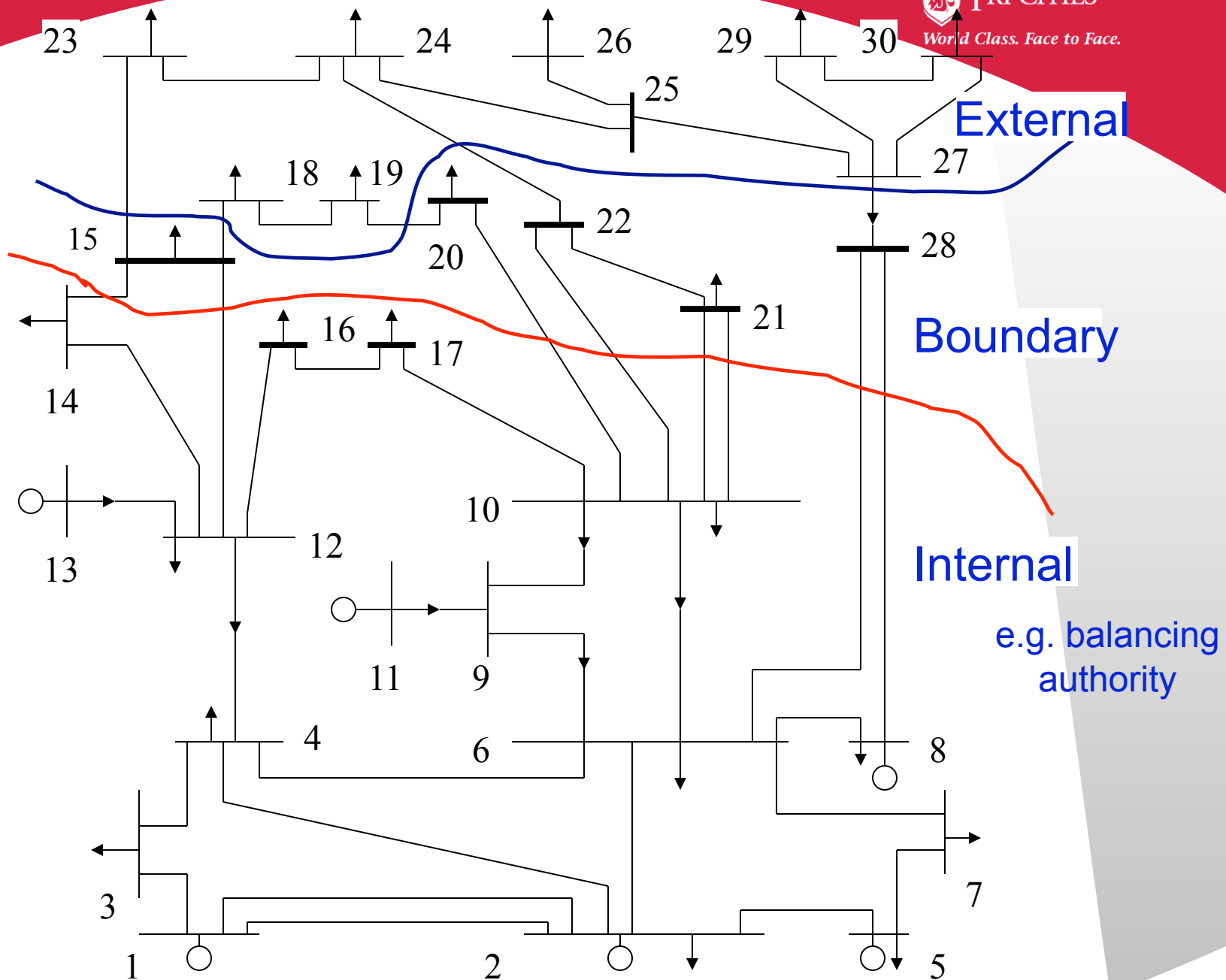
Elimination of a Group of Nodes – A Special Case

- External-Boundary-Internal System – Ward Equivalent

$$\begin{bmatrix} Y_{ee} & Y_{eb} & 0 \\ Y_{be} & Y_{bb}^{(e)} + Y_{bb}^{(i)} & Y_{bi} \\ 0 & Y_{ib} & Y_{ii} \end{bmatrix} \begin{bmatrix} V_e \\ V_b \\ V_i \end{bmatrix} = \begin{bmatrix} I_e \\ I_b \\ I_i \end{bmatrix}$$

“e” = external nodes
“b” = boundary nodes
“i” = internal nodes





Ward Equivalent

Objective: eliminate external nodes

$$\begin{bmatrix} Y_{ee} & Y_{eb} & 0 \\ Y_{be} & Y_{bb}^{(e)} + Y_{bb}^{(i)} & Y_{bi} \\ 0 & Y_{ib} & Y_{ii} \end{bmatrix} \begin{bmatrix} V_e \\ V_b \\ V_i \end{bmatrix} = \begin{bmatrix} I_e \\ I_b \\ I_i \end{bmatrix}$$

Expand the equations:

$$Y_{ee} V_e + Y_{eb} V_b = I_e$$

$$Y_{be} V_e + (Y_{bb}^{(e)} + Y_{bb}^{(i)}) V_b + Y_{bi} V_i = I_b$$

$$Y_{ib} V_b + Y_{ii} V_i = I_i$$

Express V_e by V_b from the 1st equation:

$$V_e = -Y_{ee}^{-1} Y_{eb} V_b + Y_{ee}^{-1} I_e$$

Substitute V_e into the 2nd equation:

$$-Y_{be} Y_{ee}^{-1} Y_{eb} V_b + Y_{be} Y_{ee}^{-1} I_e + (Y_{bb}^{(e)} + Y_{bb}^{(i)}) V_b + Y_{bi} V_i = I_b$$

Re-arrange:

$$(Y_{bb}^{(e)} + Y_{bb}^{(i)} - Y_{be} Y_{ee}^{-1} Y_{eb}) V_b + Y_{bi} V_i = I_b - Y_{be} Y_{ee}^{-1} I_e$$

Define equivalent Y matrix and current injection:

$$Y_{eq} = Y_{bb}^{(e)} - Y_{be} Y_{ee}^{-1} Y_{eb}$$

$$I_{eq} = -Y_{be} Y_{ee}^{-1} I_e$$

Ward equivalent:

$$\begin{bmatrix} Y_{bb}^{(i)} + Y_{eq} & Y_{bi} \\ Y_{ib} & Y_{ii} \end{bmatrix} \begin{bmatrix} V_b \\ V_i \end{bmatrix} = \begin{bmatrix} I_b + I_{eq} \\ I_i \end{bmatrix}$$

Ward Equivalent Procedure

- Determine the model of the whole network
- Solve power flow
- Convert constant power load to constant current load
- Determine the equivalent admittance matrix and current injection
- Derive Ward equivalent model based on the equations on the previous slide

Ward Equivalent

- Ward Equivalent gives reasonably accurate results for real power flows, whereas the accuracy for reactive power flow is relatively poor
- This is due to the fact that the change in reactive power injection to maintain constant voltage at external PV buses is not accounted for

Ward-PV Equivalent

- The Ward reduction process is applied only to external PQ buses
- The external PV buses are retained
- The external buses are separated into Q and V buses
- The Ward-PV equivalents give excellent results for contingency evaluation

Ward-PV Equivalent

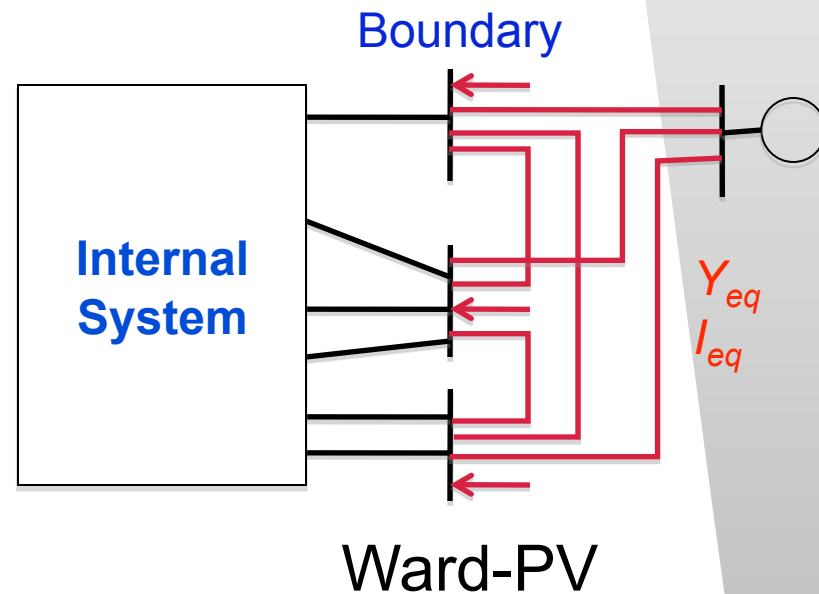
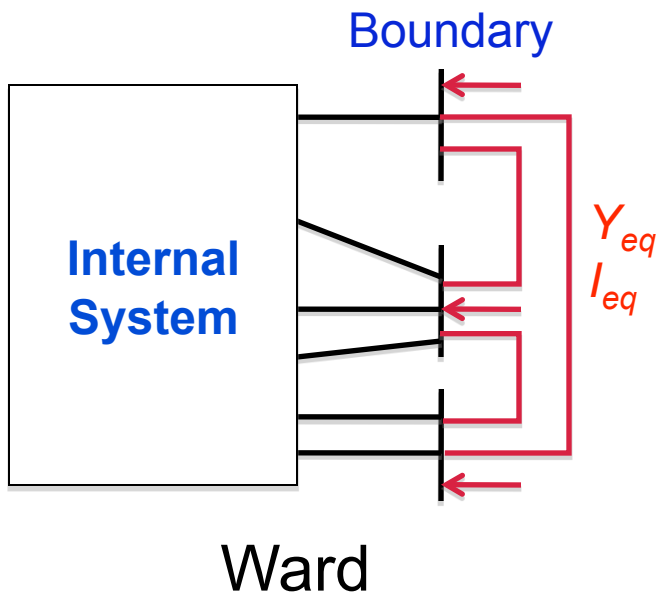
- Gaussian elimination is used to remove terms involving Q buses only

$$\begin{bmatrix} Y_{QQ} & Y_{QV} & Y_{Qb} & 0 \\ Y_{VQ} & Y_{VV} & Y_{Vb} & 0 \\ Y_{bQ} & Y_{bV} & Y_{bb}^{(e)} + Y_{bb}^{(i)} & Y_{bi} \\ 0 & 0 & Y_{ib} & Y_{ii} \end{bmatrix} \begin{bmatrix} V_Q \\ V_V \\ V_b \\ V_i \end{bmatrix} = \begin{bmatrix} I_Q \\ I_V \\ I_b \\ I_i \end{bmatrix}$$

$$\begin{bmatrix} Y_{VV}^{(1)} & Y_{Vb}^{(1)} & 0 \\ Y_{bV}^{(1)} & Y_{eq}^{(1)} + Y_{bb}^{(i)} & Y_{bi} \\ 0 & Y_{ib} & Y_{ii} \end{bmatrix} \begin{bmatrix} V_V \\ V_b \\ V_i \end{bmatrix} = \begin{bmatrix} I_V^{(1)} \\ I_b + I_{eq}^{(1)} \\ I_i \end{bmatrix}$$

Ward Equivalent Summary

- Ward: Pseudo injections at the boundary buses
- Ward-PV: PV buses of the external network are retained



Reading Assignment

Network Reduction and Equivalent Networks

- Chapter 7.6
- Chapter 7.7
- Chapter 14.6

State Estimation (next class's topic)

- Chapter 15

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Questions?

