

Ejercicio 1

$$\eta = \frac{W_{\text{neto}}}{Q_{\text{abs}}} \quad \text{--- para a ---}$$

A

$$a) \quad \eta_a = \frac{W_{\text{neto a}}}{Q_{\text{abs a}}}$$

Tenemos ciclo así que para cada ciclo reversible

$$\Delta E = \Delta S = 0$$

$$\Delta E = Q_{\text{neto}} - W_{\text{neto}} \Rightarrow Q_{\text{neto}} = W_{\text{neto}}$$

$$\Rightarrow \eta_a = \frac{Q_{AB} + Q_{BC} + Q_{CA}}{Q_{AB}}$$

Como nuestro gráfico, obtenemos el calor por tramo como el área debajo de la curva

$$\Rightarrow Q_{AB} = (S_2 - S_1) \cdot T_2 \quad (\text{rectángulo})$$

$$Q_{BC} = -(S_2 - S_1)T_1 - \frac{(T_2 - T_1)(S_2 - S_1)}{2} \quad (\text{rectángulo} + \text{triángulo})$$

$$Q_{CA} = 0; \quad dS = 0 = \frac{dQ_{\text{rev}}}{T} \Rightarrow dQ_{\text{rev}} = 0 \Rightarrow Q_{CA} = 0$$

$$\text{así } \eta_a = \frac{(S_2 - S_1)T_2 + [-(S_2 - S_1)T_1 - \frac{(T_2 - T_1)(S_2 - S_1)}{2}]}{(S_2 - S_1)T_2}$$

$$\Rightarrow \eta_a = 1 - \frac{(S_2 - S_1) \left[T_1 + \frac{T_2 + T_1}{2} \right]}{(S_2 - S_1)T_2} = 1 - \frac{(T_1 + T_2)}{2T_2} \quad \checkmark$$

$$b) \quad \eta_b = \frac{Q_{AB} + Q_{BC} + Q_{CA}}{Q_{AB}}$$

$$Q_{AB} = (S_2 - S_1)T_1 + \frac{(S_2 - S_1)(T_2 - T_1)}{2}$$

$$Q_{BC} = -(S_2 - S_1)T_1$$

$$Q_{CA} = 0 \quad \text{como antes}$$

$$\text{así } \eta_b = \frac{(S_2 - S_1)T_1 + (S_2 - S_1)\frac{(T_2 - T_1)}{2} - (S_2 - S_1)T_1}{(S_2 - S_1)T_1 + (S_2 - S_1)\frac{(T_2 - T_1)}{2}}$$

$$\Rightarrow \eta_b = 1 - \frac{(S_2 - S_1)T_1}{(S_2 - S_1) \left[T_1 + \frac{T_2 - T_1}{2} \right]} = 1 - \frac{T_1}{T_1 + T_2} \quad \checkmark$$

$$\Rightarrow \eta_A = 1 - \left(\frac{T_1 + T_2}{2T_2} \right)$$

$$\eta_B = 1 - \left(\frac{2T_1}{T_1 + T_2} \right)$$

¿Cuál es la más eficiente?

Vemos

$$\eta_A > \eta_B ? \Leftrightarrow - \left(\frac{T_1 + T_2}{2T_2} \right) > - \left(\frac{2T_1}{T_1 + T_2} \right)$$

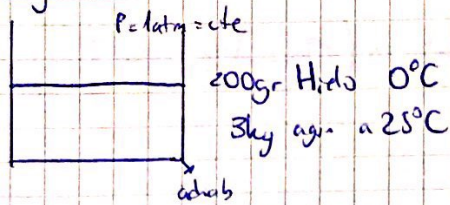
$$\Leftrightarrow (T_1 + T_2)^2 \leq 4T_1T_2 \Leftrightarrow T_1^2 + 2T_1T_2 + T_2^2 - 4T_1T_2 \leq 0$$

$$\Leftrightarrow T_1^2 - 2T_1T_2 + T_2^2 \leq 0$$

$$\Leftrightarrow (T_1 - T_2)^2 \leq 0 \text{ absurdo (pues } T_2 > T_1 \text{ no puede ser cero, y al cuadrado no negativo)}$$

$$\Rightarrow \boxed{\eta_B > \eta_A}$$

Ejercicio 2



$$a) H = E + PV$$

$$dH = dQ + VdP \Rightarrow dH_{P=\text{cte}} = dQ$$

$$\Rightarrow \left. \frac{dH}{dT} \right|_P = \left. \frac{dQ}{dT} \right|_P = C_p \Rightarrow \Delta H = Q \Delta T$$

$$H_{\text{tot}} = H_{\text{sol}} + H_{\text{liq}}$$

Como nuestro recipiente es adiabático, no hay intercambio de calor con el exterior

$$\Rightarrow dH_{\text{tot}} = dQ = 0 \Rightarrow \Delta H_{\text{tot}} = Q = 0$$

como

$$\Rightarrow \Delta H_{\text{tot}} = \Delta H_{\text{sol}} + \Delta H_{\text{liq}} = 0$$

es C_p (destruyete hielo y se calienta agua)

$$b) T_{\text{eq}}? \quad 0 = \Delta H_{\text{sol}} + \Delta H_{\text{liq}} = L_f m_{\text{hielo}} + C_{\text{hielo}} (T_{\text{eq}} - 273K) + C_{\text{agua}} (T_{\text{eq}} - 298K)$$

hielo agua

$$\Rightarrow \frac{80 \text{ cal}}{\text{gr}} \cdot 200 \text{ gr} + 200 \text{ gr} \cdot \frac{0.5 \text{ cal}}{\text{gK}} (T_{\text{eq}} - 273K) + 3000 \text{ gr} \cdot \frac{1 \text{ cal}}{\text{gK}} (T_{\text{eq}} - 298K) = 0$$

$$\Rightarrow 16000 \text{ cal} + 100 \frac{\text{cal}}{\text{K}} T_{\text{eq}} + 3000 \frac{\text{cal}}{\text{K}} T_{\text{eq}} = 100 \frac{\text{cal}}{\text{K}} 273K + 3000 \frac{\text{cal}}{\text{K}} 298K$$

$$\Rightarrow T_{\text{eq}} \approx 292.03K$$

c)

$$\Delta S_{\text{tot}} = \Delta S_{\text{sol}} + \Delta S_{\text{liq}} =$$

$$\Delta S_{\text{liq}} = \int_{298K}^{292.03K} \frac{1 \text{ cal}}{\text{gK}} \frac{dT}{T} = \frac{1 \text{ cal}}{\text{gK}} \ln \left(\frac{292.03K}{298K} \right)$$

me olvide la masa

$$\Rightarrow \Delta S_{\text{liq}} \approx -0.02 \frac{\text{cal}}{\text{gK}}$$

$$\Delta S_{liq} = dS_{liq}|_p = \frac{C_p m \ln q}{T} \quad (dQ_p = C_p dT)$$

$$\Rightarrow \Delta S_{liq}|_p = \int_{298K}^{292.03K} \frac{1 \text{ cal}}{9K} \cdot 3000g \cdot \frac{dT}{T} = 3000 \frac{\text{cal}}{K} \cdot \ln\left(\frac{292.03}{298}\right) \approx -60.71 \frac{\text{cal}}{K}$$

another error

$$\Delta S_{sol}|_p = \Delta S_{sol}|_{\text{fusion } p} + \Delta S_{sol}|_{\Delta T} = \frac{mHL_f}{T} + \int_{273K}^{292.03K} \frac{mC_p dT}{T} = \frac{16000 \text{ cal}}{273K} + \frac{100 \text{ cal}}{K} \cdot \ln\left(\frac{292.03}{273}\right)$$

$dQ_p = L_f \checkmark$

$$\Rightarrow \Delta S_{sol}|_p \approx 65.33 \frac{\text{cal}}{K} \times$$

$$\Delta S = \Delta S_{liq} + \Delta S_{sol} \approx 4.6 \frac{\text{cal}}{K} > 0 \text{ proceso irreversible concuerda } \checkmark$$

$$\Delta S_{sol} \approx 65.33 \frac{\text{cal}}{K} \quad \Delta S_{liq} \approx -60.71 \frac{\text{cal}}{K}$$

¿Por qué pedís usar $dS = \frac{dQ_{rev}}{T}$ si el proceso es irrever-? ¡alta intensidad irre

Ejercicio 4

$$f(v) = C v^2 e^{-\frac{m}{2k_B T} v^2} \quad \text{velocidades escalares}$$

a) Halle C

$$\frac{dn}{dv} = f(v) dv \quad \text{probabilidad de una velocidad entre } v \text{ y } v+dv$$

⇒ integrando todas las posibilidades

$$1 = \int_0^{+\infty} f(v) dv = C \int_0^{+\infty} v^2 e^{-\frac{m v^2}{2k_B T}} dv$$

Por ende $\int_0^{+\infty} x^2 e^{-x^2} dx = \frac{\sqrt{\pi}}{4} \Rightarrow \text{sea } r = \sqrt{\frac{m}{2k_B T}} v$

$$1 = C \int_0^{+\infty} \frac{2k_B T}{m} r^2 e^{-r^2} \sqrt{\frac{2k_B T}{m}} dr$$

$$1 = C \left(\frac{2k_B T}{m} \right)^{3/2} \cdot \frac{\sqrt{\pi}}{4} \Rightarrow C = \frac{4}{\sqrt{\pi}} \left(\frac{m}{2k_B T} \right)^{3/2} \quad \checkmark$$

$$b) \langle v \rangle = \int \text{Prob. } v \cdot v = \int_0^{+\infty} \frac{4}{\sqrt{\pi}} \left(\frac{m}{2k_B T} \right)^{3/2} \cdot v^3 e^{-\frac{m}{2k_B T} v^2} dv$$

análogo $\langle v \rangle = \frac{4}{\sqrt{\pi}} \left(\frac{m}{2k_B T} \right)^{3/2} \left(\frac{2k_B T}{m} \right)^2 \int_0^{+\infty} r^3 e^{-r^2} dr$

$$\Rightarrow \langle v \rangle = \frac{4}{\sqrt{\pi}} \left(\frac{2k_B T}{m} \right)^{1/2} \cdot \frac{1}{2} = \frac{2}{\sqrt{\pi}} \left(\frac{2k_B T}{m} \right)^{1/2} \quad \checkmark$$

$$\langle v^2 \rangle = \frac{4}{\sqrt{\pi}} \left(\frac{m}{2k_B T} \right)^{3/2} \int_0^{+\infty} v^4 e^{-\frac{m}{2k_B T} v^2} dv$$

dos caminos: a) usando la fórmula que nos dan

b) usando $\int_0^{+\infty} v^4 e^{-\frac{m}{2k_B T} v^2} dv = \frac{1}{2} \left(\frac{m}{2k_B T} \right) \left(\int_0^{+\infty} v^2 e^{-\frac{m}{2k_B T} v^2} dv \right) \cdot \frac{1}{C}$

$$\Rightarrow \langle v^2 \rangle = \frac{4}{\sqrt{\pi}} \left(\frac{m}{2k_B T} \right)^{3/2} \left[\frac{\sqrt{\pi}}{4} \left(\frac{2k_B T}{m} \right)^{3/2} \right] \cdot \frac{1}{C} \left(\frac{m}{2k_B T} \right) = \frac{4}{\sqrt{\pi}} \left(\frac{m}{2k_B T} \right)^{3/2} \cdot \frac{3}{2} \frac{\sqrt{\pi}}{4} \left(\frac{2k_B T}{m} \right)^{3/2}$$

$$\Rightarrow \langle v^2 \rangle = \frac{3k_B T}{m} = 3k_B T$$

$$c) \langle v \rangle = 11.2 \frac{\text{km}}{\text{s}} = \frac{2}{\sqrt{\pi}} \cdot \left(\frac{2k_B T_e}{m} \right)^{1/2}$$

$$\Rightarrow (11.2)^2 \frac{\text{km}^2}{\text{s}^2} = \frac{4}{\pi} \cdot \frac{2k_B T_e}{m} \Rightarrow T_e = \frac{(11.2)^2 \frac{\text{km}^2}{\text{s}^2}}{8} \cdot \frac{\pi \cdot 10^{-3} \text{ kg}}{k_B}$$

$T_e = 11916.77409 \text{ K}$ *¡¡¡ ¡¡¡ ¡¡¡*

d) \Rightarrow seguimos con 3 de traslación, + 2 de rotación, + 1 vibración

$$\Rightarrow \langle E \rangle = \frac{m}{2} \langle v^2 \rangle = \frac{1}{2} k_B T \left[\underbrace{\frac{3}{2}}_{\text{3 d.o.f. de traslación de centros}} + \underbrace{1}_{\text{2 d.o.f. de rotación de centros}} + \underbrace{\frac{1}{2}}_{\text{1 d.o.f. de vibración}} \right]$$

Por teorema de equipartición

$$c_v = \frac{2}{\partial T} \langle E \rangle = 3k_B T$$

$$\gamma = \frac{c_p}{c_v} =$$

¡¡¡ la vibración aporta 2 términos cuadráticos

$$\frac{1}{2} m v^2 + \frac{1}{2} k r^2$$

vibración

Ejercicio 3

$$\alpha_{\text{coex}} = \frac{1}{V} \left. \frac{\partial V}{\partial T} \right|_{\text{coex}}$$

$$CC = \left. \frac{\partial P}{\partial T} \right|_{\text{coex}} = \frac{L}{T(v_g - v_l)} \quad \text{que sale de } dg_l(T, P) = dg_g(T, P)$$

$$P_v = RT$$

en coexistencia de fases

~~$$T_l = T_g \Rightarrow dT_l = dT_g$$

$$dT_l = \left. \frac{\partial T}{\partial P} \right|_{\text{coex}} dP + \left. \frac{\partial T}{\partial v} \right|_{\text{coex}} dv \quad \text{nore.}$$~~

$$\begin{aligned} dg(T, v) &= -s(T, v)dT + v dP(T, v) \\ &= -s(T, v)dT + v \left[\left. \frac{\partial P}{\partial T} \right|_{\text{coex}} dT + \left. \frac{\partial P}{\partial v} \right|_{\text{coex}} dv \right] \\ &= -s dT + v \left[\frac{L}{T(v_g - v_l)} dT + \left(-\frac{RT}{v^2} \right) dv \right] \end{aligned}$$

esto es
 $\left. \frac{\partial P}{\partial T} \right|_v dT + \left. \frac{\partial P}{\partial v} \right|_T dv$
 No se sabe el camino de coexistencia, ni se sabe el dv

Pero

esto

se justifica

LA

EC

de

CLASICO

CLAMPON

$$\Rightarrow \left[-s_g + \frac{v_g L}{T(v_g - v_l)} \right] dT - \frac{RT}{v_g} dv = \left[-s_l + \frac{v_l L}{T(v_g - v_l)} \right] dT - \frac{RT}{v_l} dv$$

$$\Rightarrow \left[(s_l - s_g) + \frac{(v_g - v_l)L}{T(v_g - v_l)} \right] dT = RT \left[\frac{1}{v_g} - \frac{1}{v_l} \right] dv$$

$$\Rightarrow \left. \frac{dv}{dT} \right|_{\text{coex}} = \frac{(s_l - s_g) + \frac{(v_g - v_l)L}{T(v_g - v_l)}}{RT \left[\frac{1}{v_g} - \frac{1}{v_l} \right]} \quad \text{utilizando } \left. \frac{dP}{dT} \right|_{\text{coex}} = \frac{L}{T(v_g - v_l)} = \frac{s_g - s_l}{v_g - v_l}$$

$$\Rightarrow \left. \frac{dv}{dT} \right|_{\text{coex}} = \frac{2L v_g v_l}{RT^2 (v_l - v_g)}$$

$$\Rightarrow \alpha_{\text{coex}} = \frac{1}{V} \cdot \frac{2L v_g v_l}{RT^2 (v_l - v_g)}$$