Assignment 6

Due time : 10:15, Oct 30, 2020 (Friday) Grade :

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Problem 1 (Noise in DSB-SC Receiver, 30pts) Score: ______. A DSB-SC modulated signal in transmitted over a noisy channel. The power spectral density of the noise is shown in Figure 1. The message bandwidth is 3 kHz and the carrier frequency is 200 kHz. Assuming that the average power of the modulated signal is 12 watts, determine the input signal-to-noise ratio (predetection SNR), output signal-to-noise ratio (postdetection SNR) and the detection gain (output SNR / input SNR).

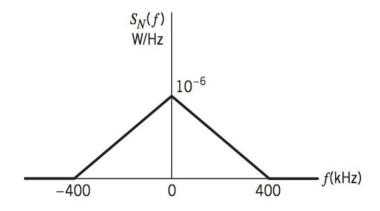


Figure 1:

Solution: The received signal is the sum of the DSB-SC modulated signal and the noise:

$$x_r(t) = x_c(t) + n(t) = A_c m(t) \cos(2\pi f_c t + \theta) + n(t) = A_c \cos(2\pi \cdot 200000t + \theta) + n(t). \tag{1}$$

After passing the bandpass filter, the received signal becomes

$$e_2(t) = x_c(t) + n'(t) = A_c \cos(2\pi f_c t + \theta) + n_c \cos(2\pi f_c t + \theta) - n_s \sin(2\pi f_c t + \theta)$$
$$= A_c \cos(2\pi \cdot 200000t + \theta) + n_c \cos(2\pi \cdot 200000t) - n_s \sin(2\pi \cdot 200000t). \tag{2}$$

The average power of the modulated signal $x_c(t)$ is

$$P_T = \frac{A_c^2}{2} \overline{m^2(t)} = 12 \text{W}.$$
 (3)

According to figure 1, the power spectral density of the noise is

$$S_N(f) = 10^{-6} \Lambda(400000f). \tag{4}$$

After passing the narrowband filter, the average power of the noise component is

$$P_{n'} = \int_{-f_c - W}^{-f_c + W} S_N(f) \, \mathrm{d}f + \int_{f_c - W}^{f_c + W} S_N(f) \, \mathrm{d}f$$

$$= 2 \int_{f_c - W}^{f_c + W} S_N(f) \, \mathrm{d}f$$

$$= 2 \int_{200000 + 3000}^{200000 + 3000} 10^{-6} \Lambda(400000f) \, \mathrm{d}f$$

$$= 0.006(W). \tag{5}$$

The input SNR is

$$SNR_T = \frac{P_T}{P_{n'}} = \frac{12}{0.006} = 2000. \tag{6}$$

After demodulation, the output is

$$y_D(t) = \text{LP}[e_2(t) \cdot 2\cos(2\pi f_c t + \theta)]$$

=\text{LP}\{A_c m(t)[1 + \cos(4\pi f_c t + 2\theta)] + n_c(t)[1 + \cos(4\pi f_c t + 2\theta)] - n_s(t)\sin(2\pi f_c t + 2\theta)\}
=A_c m(t) + n_c(t).

The average power of the demodulated signal component is

$$A_c^2 \overline{m^2(t)} = 2P_T = 24W. (7)$$

The average power of the noise component is

$$P_{n_c} = P_{n'} = 0.006 \text{W}.$$
 (8)

The output SNR is

$$SNR_D = \frac{2P_T}{P_{n_c}} = \frac{24}{0.006} = 4000. \tag{9}$$

The detection gain is

$$\frac{\text{SNR}_D}{\text{SNR}_T} = 2. \tag{10}$$

Problem 2 (Noise in SSB Receiver, 25pts) Score: ______. Derive the equation for $y_D(t)$ for an USB-SSB system assuming that the noise is expanded about the frequency $f_c + \frac{W}{2}$. Derive the output SNR (postdetection SNR), detection gain and the figure of merit. Determine and plot the power spectral density of the in-phase component $n_c(t)$ and the quadrature component $n_s(t)$ of the narrowband noise.

Solution: The USB-SSB modulated signal is

$$x_c(t) = A_c[m(t)\cos(2\pi f_c t + \theta) - \hat{m}(t)\sin(2\pi f_c t + \theta)]. \tag{11}$$

The received signal is

$$x_r(t) = x_c(t) + w(t) = A_c[m(t)\cos(2\pi f_c t + \theta) - \hat{m}(t)\sin(2\pi f_c t + \theta)] + w(t). \tag{12}$$

After passing the band filter whose center frequency is $f_c + \frac{W}{2}$ and bandwidth is W, the signal becomes

$$e_2(t) = A_c[m(t)\cos(2\pi f_c t + \theta) - \hat{m}(t)\sin(2\pi f_c t + \theta)] + n(t)$$

$$= A_c[m(t)\cos(2\pi f_c t + \theta) - \hat{m}(t)\sin(2\pi f_c t + \theta)]$$

$$+ n_c(t)\cos\left[2\pi \left(f_c + \frac{W}{2}\right)t + \theta\right] - n_s(t)\sin\left[2\pi \left(f_c + \frac{W}{2}\right)t + \theta\right].$$
(13)

The average power of the modulated signal is

$$P_T = A_c^2 \overline{m^2(t)} \tag{14}$$

The average power of the filtered noise is $N_0 \cdot W$. Therefore, the input SNR is

$$SNR_T = \frac{P_T}{N_0 W} = \frac{A_c^2 \overline{m^2(t)}}{N_0 W}.$$
 (15)

After passing demodulator (i.e., multiplying with a local oscillator $2\cos(2\pi f_c t + \theta)$ and passing a lowpass filter), the output signal is

$$y_D(t) = A_c m(t) + n_{c,\text{expanded about } f_c}(t). \tag{16}$$

The average power of the demodulated signal is

$$P_D = A_c \overline{m^2(t)}. (17)$$

The average power of the noise in output signal is $N_0 \cdot W$. Therefore, the output SNR is

$$SNR_D = \frac{P_D}{N_0 W} = \frac{A_c^2 \overline{m^2(t)}}{N_0 W}.$$
 (18)

The detection gain is

$$\frac{\text{SNR}_D}{\text{SNR}_T} = 1. \tag{19}$$

The channel SNR is

$$SNR_c = \frac{P_T}{N_0 W} = \frac{A_c^2 \overline{m^2(t)}}{N_0 W}.$$
 (20)

The figure of merit is

$$\frac{\text{SNR}_D}{\text{SNR}_c} = 1. \tag{21}$$

The power spectral density of the narrowband noise is

$$S_n(f) = \frac{N_0}{2} \left[\Pi\left(\frac{f - \left(f_c + \frac{W}{2}\right)}{W}\right) + \Pi\left(\frac{f + \left(f_c + \frac{W}{2}\right)}{W}\right) \right]. \tag{22}$$

Expanded about the frequency $f_c + \frac{W}{2}$, the power spectral density of the in-phase component $n_c(t)$ and the quadrature component $n_s(t)$ are both

$$S_{n_c}(f) = S_{n_s}(f) = \operatorname{LP}\left[S_n\left(f - f_c - \frac{W}{2}\right) + S_n\left(f + f_c + \frac{W}{2}\right)\right] = N_0 \Pi\left(\frac{f}{W}\right),\tag{23}$$

as shown in figure 2.

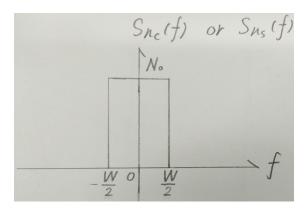


Figure 2: The power spectral density of the in-phase component $n_c(t)$ and the quadrature component $n_s(t)$

Problem 3 (Noise in AM Receiver, 25pts) Score: ______. Assume an AM system operates with a modulation index a = 0.4. The message signal is $m(t) = 5\cos(10\pi t)$.

- 1) Compute the transmission efficiency.
- 2) Assume the envelope detector operates above the threshold. Compute the output SNR (postdetection SNR) in decibel relative to the input SNR.
- 3) Compute the output SNR in decibels relative to the baseband SNR (P_T/N_0W) .
- 4) Keep P_T (the average power of modulated signal) unchanged, determine the improvement (in decibels) in the output SNR if the modulation index is increased from 0.4 to 0.8. (Hint: Since the input SNR and baseband SNR are unchanged, we can calculate the improvement of output SNR based on its relationship with the input SNR and baseband SNR.)

Solution: 1) In AM modulation,

$$m_n(t) = \frac{m(t)}{|\min[m(t)]|} = \cos(10\pi t).$$
 (24)

The transmission efficiency is

$$\mu = \frac{a^2 \overline{m_n^2(t)}}{a^2 \overline{m_n^2(t)} + 1} = \frac{a^2/2}{a^2/2 + 1} = \frac{2}{27} = 7.41\%.$$
 (25)

2) The AM modulated signal is

$$x_c(t) = A_c[1 + am_n(t)]\cos(2\pi f_c t + \theta).$$
 (26)

The received signal is

$$x_c(t) = x_c(t) + w(t). (27)$$

After passing the bandpass filter, the signal becomes

$$e_2(t) = A_c[1 + am_n(t)]\cos(2\pi f_c t + \theta) + n_c(t)\cos(2\pi f_c t + \theta) - n_s(t)\sin(2\pi f_c t + \theta) = r(t)\cos[2\pi f_c t + \phi(t)],$$
(28)

where the envelope of the signal is

$$r(t) = \sqrt{\{A_c[1 + am_n(t)] + n_c(t)\}^2 + n_s^2(t)}.$$
(29)

The average power of the modulated signal is

$$P_t = \overline{\{A_c[1 + am_n(t)]\cos(2\pi f_c t + \theta)\}^2} = \frac{A_c^2}{2} \left[1 + a^2 \overline{m_n(t)}\right]. \tag{30}$$

The average power of the narrowband noise is $2N_0W$. Therefore, the input SNR is

$$SNR_T = \frac{P_T}{2N_0W} = \frac{A_c^2 \left[1 + a^2 \overline{m_n(t)} \right]}{4N_0W}.$$
 (31)

After the envelope detector, the output signal is the envelope

$$y_D(t) = r(t) = \sqrt{\{A_c[1 + am_n(t)] + n_c(t)\}^2 + n_s^2(t)}.$$
(32)

Since the envelope detector operates above the threshold, i.e., SNR_T is large and thus $|A_c[1 + am_n(t)] + n_c(t)| \gg |n_s(t)|$,

$$y_D(t) \approx A_c[1 + am_n(t)] + n_c(t). \tag{33}$$

The average of the modulated signal after removal of DC component is

$$P_D = \overline{[A_c a m_n(t)]^2} = A_c^2 a^2 \overline{m_n^2(t)}. \tag{34}$$

The average power of the noise in the output signal is $2N_0W$. Therefore, the output SNR is

$$SNR_D = \frac{P_D}{2N_0W} = \frac{A_c^2 a^2 \overline{m_n^2(t)}}{2N_0W}.$$
 (35)

The output SNR in decibels relative to the input SNR is

$$10 \lg \frac{\text{SNR}_D}{\text{SNR}_T} = 10 \lg \frac{2a^2 \overline{m_n^2(t)}}{1 + a^2 \overline{m_n^2(t)}} = 10 \lg 2\mu = -8.29 \text{(dB)}.$$
 (36)

3) The average power of the modulated signal is $P_T = \frac{A_c^2}{2} [1 + a^2 \overline{m_n^2(t)}]$ and the average power of the noise in the message bandwidth is $N_0 W$, so the baseband SNR is

$$SNR_c = \frac{P_T}{N_0 W} = \frac{A_c^2 [1 + a^2 \overline{m_n^2(t)}]}{2N_0 W}.$$
 (37)

The output SNR in decibels relative to the baseband SNR is

$$10 \lg \frac{\text{SNR}_D}{\text{SNR}_c} = 10 \lg \frac{a^2 \overline{m_n^2(t)}}{1 + a^2 \overline{m_n^2(t)}} = 10 \lg \mu = -11.30(\text{dB}).$$
 (38)

4) Since the baseband SNR is unchanged, we can calculate the improvement of output SNR based on its relation with the baseband SNR:

$$10 \lg \frac{\text{SNR}_D(a=0.8)}{\text{SNR}_D(a=0.4)} = 10 \lg \frac{\text{SNR}_D(a=0.8)/\text{SNR}_c}{\text{SNR}_D(a=0.4)/\text{SNR}_c} = 10 \lg \frac{\text{SNR}_D(a=0.8)}{\text{SNR}_c} - 10 \lg \frac{\text{SNR}_D(a=0.4)}{\text{SNR}_c}$$
$$= 10 \lg \mu(a=0.8) - 10 \lg(a=0.4) = 5.15 \text{dB}. \tag{39}$$

The output SNR improves by 5.15 dB.

Problem 4 (Noise in FM Receiver and FDM, 20pts) Score: ______. An FDM system uses single-sideband modulation to from the baseband, and FM modulation for transmission of the baseband. Assume that there are eight channels and that all eight message signal have equal power P_0 and equal bandwidth W. For each signal, only the upper sideband is transmitted. The sub-carrier waves used for the first stage of modulation are defined by $c_k(t) = A_k \cos(2\pi k f_0 t), 0 \le k \le 7$. The width of the guardbands is 3W. The received signal consists of the transmitted FM signal plus white Gaussian noise of zero mean and two-sided power spectral density $N_0/2$. Assume the frequency discriminator at the receiver operates above the threshold.

- 1) Sketch the power spectral density of the signal produced at the frequency discriminator output, showing both the signal and the noise components.
- 2) Find the relationship between the subcarrier amplitudes A_k such that the SSB modulated signals corresponding to different channels have equal output SNRs at the frequency discriminator output.

Solution: 1) Since each message signal have equal bandwidth W and the width of the guardbands is 3W, we have

$$f_1 = \frac{54}{4}W,$$
 (40)

and the kth channel occupies the frequency range

$$5kW = kf_1 \le f \le W + kf_1 = (5k+1)W, \quad (1+5k)W = -W - kf_1 \le f \le -kf_1 = -5kW. \tag{41}$$

$$4kW = kf_1 < f < W + kf_1 = (4k+1)W, \quad -(1+4k)W = -W - kf_1 < f < -kf_1 = -4kW. \tag{42}$$

Since received signal includes the white Gaussian noise of two-sided power spectral density $N_0/2$, the power spectral density of the noise component is

$$S_n(f) = \frac{K_D^2}{A_c^2} N_0 f^2. (43)$$

The power spectral density of the signal and the noise components are shown in figure 3.

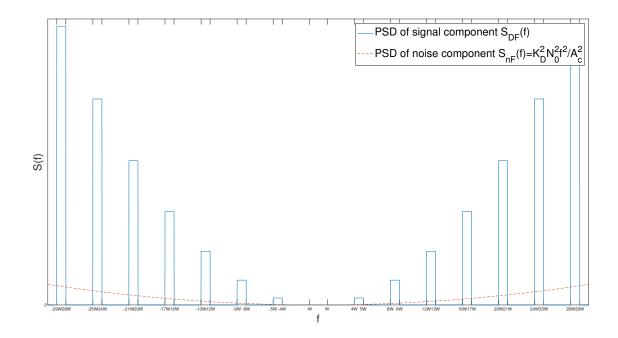


Figure 3: The power spectral density of the signal and the noise components

2) The noise power in the kth channel is

$$P_{nk} = 2 \int_{5kW}^{(5k+1)W} S_n(f) df = 2 \int_{5kW}^{(5k+1)W} \frac{K_D^2}{A_c^2} N_0 f^2 df = \frac{2}{3} \frac{K_D^2}{A_c^2} N_0 (75k^2 + 15k + 1) W^3.$$
 (44)

$$P_{nk} = 2 \int_{4kW}^{(4k+1)W} S_n(f) \, \mathrm{d}f = 2 \int_{4kW}^{(4k+1)W} \frac{K_D^2}{A_c^2} N_0 f^2 \, \mathrm{d}f = \frac{2}{3} \frac{K_D^2}{A_c^2} N_0 (75k^2 + 15k + 1)W^3. \tag{45}$$

The signal power of each channel is

$$P_T = \begin{cases} \frac{K_D^2 f_d^2 A_k^2}{2}, & k = 0\\ \frac{K_D^2 f_d^2 A_k^2}{4}, & 1 \le k \le 7. \end{cases} \quad P_T = \frac{K_D^2 f_d^2 A_k^2}{4}. \tag{46}$$

The output of the kth channel is

$$SNR_{D} = \frac{P_{T}}{P_{nk}} = \begin{cases} \frac{3 \int_{d}^{2} A_{c}^{2} W^{3}}{4 N_{0}} \frac{A_{k}^{2}}{75k^{2} + 15k + 1} = \frac{3 \int_{d}^{2} A_{c}^{2} W^{3}}{4 N_{0}} A_{0}^{2}, & k = 0, \\ \frac{3 \int_{d}^{2} A_{c}^{2} W^{3}}{8 N_{0}} \frac{A_{k}^{2}}{75k^{2} + 15k + 1}, & 1 \le k \le 7. \end{cases} \frac{3}{8} \frac{\int_{d}^{2} A_{c}^{2} W^{3}}{N_{0}} \frac{A_{k}^{2}}{48k^{2} + 12k + 1}.$$
(47)

To make that the SSB modulated signals corresponding to different channels have equal output SNRs at the frequency dicriminator output,

$$2A_0^2 = \frac{A_k^2}{75k^2 + 15k + 1} \frac{A_k^2}{48k^2 + 12k + 1} = \text{constant}, \quad \forall 10 \le k \le 7.$$
 (48)