# **Robotics : Assignment 2**

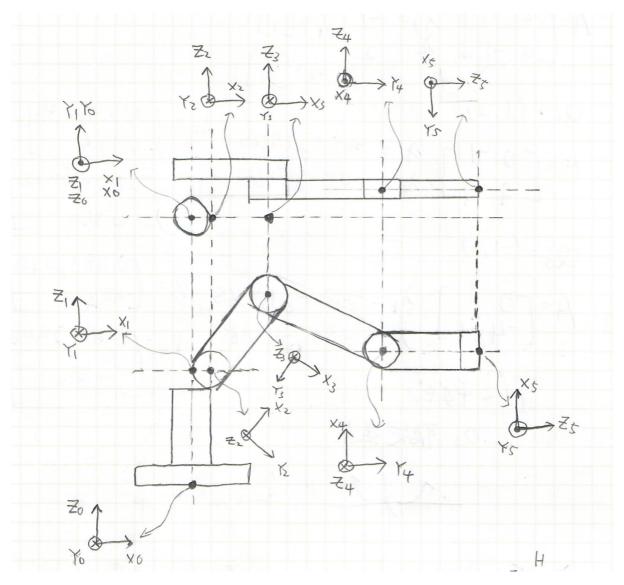


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## Part A

(1)



(2)

Joint	$lpha_{i-1}(^\circ)$	$a_{i-1}(mm)$	$d_i(mm)$	$ heta_i$
1	0	0	358.5	$\theta_1$
2	$-90^{\circ}$	50	0	$\theta_2$
3	0	300	0	$\theta_3$
4	0	350	35.3	$\theta_4$
5	$-90^{\circ}$	0	251	$\theta_5$

### **PART B**

Use the follower formula

$${}^{i-1}{}_{i}T = R_x(\alpha_{i-1})D_x(a_{i-1})R_z(\theta_i)D_z(d_i)$$

Among them,  $R_x$  is the rotation of the x axis.  $D_x$  is the displacement in the x direction, and so on. Regarding the base as joint 0, the following sets of matrices can be obtained, where s=sin,c=cos

$$^{\mathrm{BASE}}_{\phantom{0}1}T = egin{bmatrix} c_1 & -s_1 & 0 & 0 \ s_1 & c_1 & 0 & 0 \ 0 & 0 & 1 & 358.5 \ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$egin{array}{ll} rac{1}{2}T = egin{bmatrix} c_2 & -s_2 & 0 & 50 \ 0 & 0 & 1 & 0 \ -s_2 & -c_2 & 0 & 0 \ 0 & 0 & 0 & 1 \ \end{bmatrix}$$

$${}^2_3T = egin{bmatrix} c_3 & -s_3 & 0 & 300 \ s_3 & c_3 & 0 & 0 \ 0 & 0 & 1 & 0 \ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$egin{array}{lll} egin{array}{lll} egin{array}{lll} egin{array}{lll} egin{array}{lll} c_4 & -s_4 & 0 & 350 \ s_4 & c_4 & 0 & 0 \ 0 & 0 & 1 & 35.3 \ 0 & 0 & 0 & 1 \end{array} \end{array} 
ight] \end{array}$$

$${}^4_5T = egin{bmatrix} c_5 & -s_5 & 0 & 0 \ 0 & 0 & 1 & 251 \ -s_5 & -c_5 & 0 & 0 \ 0 & 0 & 0 & 1 \end{bmatrix}$$

So combine

$$\begin{split} ^{\mathrm{BASE}}{}_5T = & ^{\mathrm{BASE}}{}_1 \ T \ _2^1 T \ _3^2 T \ _4^3 T \ _5^4 T \\ = & \begin{bmatrix} s_1 s_5 + c_{234} c_1 c_5 & s_1 c_5 - c_{234} c_1 s_5 & -s_{234} c_1 & p_x \\ -c_1 s_5 + c_{234} s_1 c_5 & -c_1 c_5 - c_{234} s_1 s_5 & -s_{234} s_1 & p_y \\ -s_{234} c_5 & s_{234} s_5 & -c_{234} & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ = & \begin{bmatrix} r_{11} & r_{12} & r_{13} & p_x \\ r_{21} & r_{22} & r_{23} & p_y \\ r_{31} & r_{32} & r_{33} & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix} \end{split}$$

$$\begin{bmatrix} p_x \\ p_y \\ p_z \end{bmatrix} = \begin{bmatrix} a_1c_1 - d_5(c_4(c_1c_2s_3 + c_1s_2c_3) - s_4(c_1s_2s_3 - c_1c_2c_3)) - a_3(c_1s_2s_3 - c_1c_2c_3) - d_4s_1 + a_2c_1c_2 \\ a_1s_1 - d_5(c_4(s_1c_2s_3 + s_1s_2c_3) - s_4(s_1s_2s_3 - s_1c_2c_3)) - a_3(s_1s_2s_3 - s_1c_2c_3) - d_4c_1 + a_2s_1c_2 \\ d_1 - a_3s_{23} - a_2s_2 - d_5c_{234} \end{bmatrix}$$

$$egin{aligned} {}^5T =_{ ext{BASE}} {}^5T = ({}^{ ext{BASE}}{}^5T)^{-1} = egin{bmatrix} {}^5T_{11} & {}^5T_{12} & {}^5T_{13} & {}^5T_{14} \ {}^5T_{21} & {}^5T_{22} & {}^5T_{23} & {}^5T_{24} \ {}^5T_{31} & {}^5T_{32} & {}^5T_{33} & {}^5T_{34} \ 0 & 0 & 0 & 1 \end{bmatrix} \end{aligned}$$

$$\begin{array}{l} {}^5_0T_{11} = s_1s_5 + c_1c_2c_3c_4c_5 - c_1c_2c_5s_3s_4 - c_1c_3c_5s_2s_4 - c_1c_4c_5s_2s_3 \\ {}^5_0T_{12} = c_2c_3c_4c_5s_1 - c_1s_5 - c_2c_5s_1s_3s_4 - c_3c_5s_1s_2s_4 - c_4c_5s_1s_2s_3 \\ {}^5_0T_{13} = -s_{234-5}/2 - s_{2345}/2 \\ {}^5_0T_{14} = (d_1s_{2345})/2 - (a_1c_{2345})/2 - (a_2c_{34-5})/2 - (a_3c_{45})/2 \\ + d_4s_5 - (a_1c_{234-5})/2 + (d_1s_{234-5})/2 - (a_3c_{4-5})/2 - (a_2c_{345})/2 \\ {}^5_0T_{21} = c_5s_1 - c_1c_2c_3c_4s_5 + c_1c_2s_3s_4s_5 + c_1c_3s_2s_4s_5 + c_1c_4s_2s_3s_5 \\ {}^5_0T_{22} = c_2s_1s_3s_4s_5 - c_2c_3c_4s_1s_5 - c_1c_5 + c_3s_1s_2s_4s_5 + c_4s_1s_2s_3s_5 \\ {}^5_0T_{23} = c_{234-5}/2 - c_{2345}/2 \\ {}^5_0T_{24} = (d_1c_{2345})/2 - (a_2s_{34-5})/2 + (a_1s_{2345})/2 + (a_3s_{45})/2 \\ + d_4c_5 - (d_1c_{234-5})/2 - (a_1s_{234-5})/2 - (a_3s_{4-5})/2 + (a_2s_{345})/2 \\ {}^5_0T_{31} = -s_{234-1}/2 - s_{1234}/2 \\ {}^5_0T_{32} = c_{1234}/2 - c_{234-1}/2 \\ {}^5_0T_{33} = -c_{234} \\ {}^5_0T_{34} = a_2s_{34} - d_5 + a_3s_4 + d_1c_{234} + a_1s_{234} \\ \end{array}$$

#### PART C

#### (1)

To observe the matrix  ${}_5^0T$ 

$$\begin{split} ^{\mathrm{BASE}}{}_5T = & ^{\mathrm{BASE}}{}_1 \ T \, _2^1 T \, _3^2 T \, _4^3 T \, _5^4 T \\ = & \begin{bmatrix} s_1 s_5 + c_{234} c_1 c_5 & s_1 c_5 - c_{234} c_1 s_5 & -s_{234} c_1 & p_x \\ -c_1 s_5 + c_{234} s_1 c_5 & -c_1 c_5 - c_{234} s_1 s_5 & -s_{234} s_1 & p_y \\ -s_{234} c_5 & s_{234} s_5 & -c_{234} & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ = & \begin{bmatrix} r_{11} & r_{12} & r_{13} & p_x \\ r_{21} & r_{22} & r_{23} & p_y \\ r_{31} & r_{32} & r_{33} & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix} \end{split}$$

Can find that througglt  $r_{13}$ ,  $r_{23}$  and  $r_{33}$  can get angle of  $( heta_2+ heta_3+ heta_4)$ 

$$egin{aligned} r_{13}^2 + r_{23}^2 &= s_{234}^2 c_2^2 + s_{234}^2 s_1^2 = s_{234}^2 \ &s_{234} = \pm \sqrt{r_{13}^2 + r_{23}^2} \ &c_{234} = -r_{33} \ & heta_{234} = rctan \, 2(s_{234}, c_{234}) \end{aligned}$$

There exist 2 possible solution

And than  $heta_1$  and  $heta_5$  can be get

$$egin{align} heta_1 &= rctan \, 2(rac{-r_{23}}{s_{234}},rac{-r_{13}}{s_{234}}) \ heta_5 &= rctan \, 2(rac{r_{32}}{s_{234}},rac{-r_{31}}{s_{234}}) \ \end{align*}$$

Since  $heta_1$  and  $heta_5$  have been found, separate them from the original  $^0_5T$ 

$$\begin{split} & \overset{1}{}_{4}T = & \overset{1}{}_{0} T \overset{0}{}_{5}T \overset{5}{}_{4}T \\ & = (\overset{0}{}_{1}T)^{-1} \overset{0}{}_{5}T (\overset{4}{}_{5}T)^{-1} \\ & = \begin{bmatrix} c_{234} & -s_{234} & 0 & a_{1} + a_{3}c_{23} + a_{2}c_{2} \\ 0 & 0 & 1 & d_{4} \\ -s_{234} & -c_{234} & 0 & -a_{3}s_{23} - a_{2}s_{2} \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ & = \begin{bmatrix} r'_{11} & r'_{12} & r'_{13} & p'_{x} \\ r'_{21} & r'_{22} & r'_{23} & p'_{y} \\ r'_{31} & r'_{32} & r'_{33} & p'_{z} \\ 0 & 0 & 0 & 1 \end{bmatrix} \end{aligned}$$

Throunglt  $\,p_x'\,$  and  $\,p_z'\,$  can get  $\cos( heta_3)\,$ 

$$\begin{split} (p_x'-a_1)^2 + (p_z')^2 - a_2^2 - a_3^2 &= (a_3c_{23} + a_2c_2)^2 + (-a_3s_{23} - a_2s_2)^2 - a_2^2 - a_3^2 \\ &= a_3^2c_{23}^2 + 2a_2a_3c_{23}c_2 + a_2^2c_2^2 \\ &+ a_3^2s_{23}^2 + 2a_2a_3s_{23}s_2 + a_2^2s_s^2 - a_2^2 - a_3^2 \\ &= 2a_2a_3(c_{23}c_2 + s_{23}s_2) \\ &= 2a_2a_3c_3 \end{split}$$
 
$$c_3 = \frac{(p_x' - a_1)^2 + (p_z')^2 - a_2^2 - a_3^2}{2a_2a_3}$$
 
$$\theta_3 = \arctan 2(\pm \sqrt{1 - c_3^2}, c_3)$$

There exist 2 possible solution

ThroungIt  $p_x', p_z'$  and  $heta_3$  can get  $heta_2$ 

$$egin{aligned} p_x' - a_1 &= a_3c_{23} + a_2c_2 \ &= a_3(c_2c_3 - s_2s_3) + a_2c_2 \ &= (-a_3s_3)s_2 + (a_3c_3 + a_2)c_2 \ p_z' &= -a_3s_{23} - a_2s_2 \ &= -a_3(s_2c_3 + c_2s_3) - a_2s_2 \ &= (-a_2 - a_3c_3)s_2 + (-a_3s_3)c_2 \end{aligned}$$
 $egin{aligned} \left[ \sin( heta_2) \\ \cos( heta_2) \egin{aligned} &= \left[ -a_3s_3 & a_3c_3 + a_2 \\ -a_2 - a_3c_3 & -a_3s_3 \egin{aligned} &= a_3s_3 \\ -a_2 - a_3c_3 & -a_3s_3 \egin{aligned} &= a_3s_3 \\ -a_2 - a_3c_3 & -a_3s_3 \egin{aligned} &= a_3s_3 \\ -a_3s_3 & -a_3s_3 \egin{aligned} &= a_3s_3 \\ -a_3s_3 & -a_3s_3 \egin{aligned} &= a_3s_3 \\ -a_2 - a_3c_3 & -a_3s_3 \egin{aligned} &= a_3s_3 \\ -a_3s_3 & -a_3s_3 \egin{aligned} &= a$ 

We have  $\theta_2, \theta_3$  and  $(\theta_2 + \theta_3 + \theta_4)$  so that can get  $\theta_4$ 

$$\theta_4 = \theta_{234} - \theta_2 - \theta_3$$

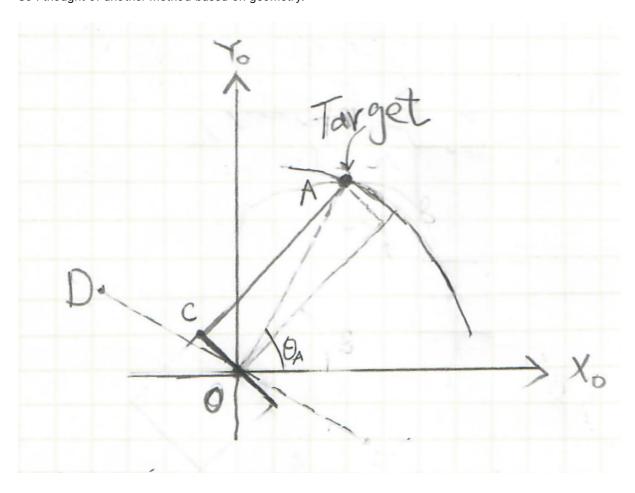
So that all the theta have been found!

BUT! When the  $heta_2+ heta_3+ heta_4=0$  than solve  $heta_1, heta_5$  a Huge problems will happen, it have a Zero denominator. On the other hand, the pose designed for this problem always puts the end down, causing the 234-axis angle sum to be 0.

So that the previous methods are not applicable in this problem.



So I thought of another method based on geometry.



First, by observing the xy plane, we can find that by rotating the first axis to align the  $x_1$  axis with the target, we will get  $heta_A$ 

$$heta_A = rctan 2(p_x, p_y)$$

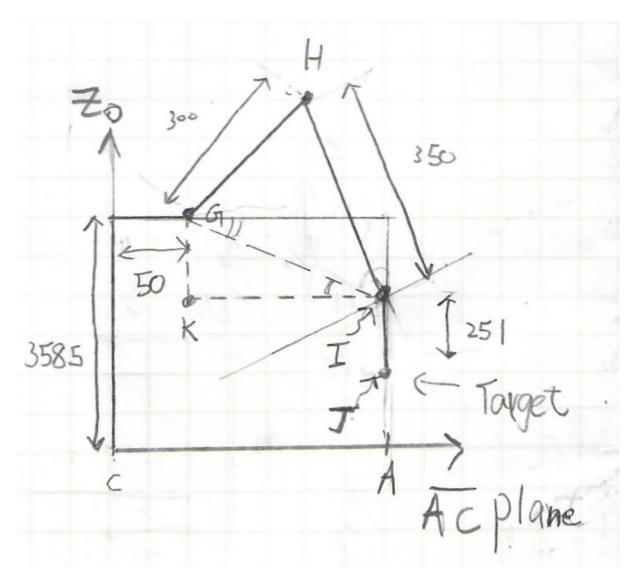
Then you can know that the coordinate system of the first axis and the fourth axis has a known offset in the  $y_1$  direction (35.3mm)  $\overline{OC}$  and the distance to the target  $\overline{AO}$  can get the distance of  $\overline{AC}$ 

$$egin{aligned} \overline{CO} &= 35.3 \ \overline{AO} &= \sqrt{p_x^2 + p_y^2} \ \overline{AC} &= \sqrt{\overline{AO}^2 - \overline{CO}^2} \end{aligned}$$

In the triangle  $\triangle ACO$ , the length of the three sides is known. Through the law of cosines, three angles and the angle of the first axis can be obtained.

$$heta_1 = heta_A - \angle CAO = heta_A - rccos(rac{\overline{AO}^2 + \overline{AC}^2 - \overline{CO}^2}{2\overline{AO}\,\overline{AC}})$$

Robotics: Assignment 2



After observing the AC plane and the  $z_{\mathrm{0}}$  axis, you can intuitively get many side lengths

$$\begin{split} \overline{GK} &= 358.5 - p_z - 251 \\ \overline{IK} &= \overline{AC} - 50 \\ \overline{GH} &= 300 \\ \overline{HI} &= 350 \\ \overline{GI} &= \sqrt{\overline{GK}^2 + \overline{IK}^2} \end{split}$$

From the upper half of the triangle  $\triangle IGH$  , the angle of the third axis after  $\angle GHI$  can be obtained

$$heta_3 = \pi - \angle GHI = \pi - \arccos(rac{\overline{GH}^2 + \overline{HI}^2 - \overline{GI}^2}{2\overline{GH}\ \overline{HI}})$$

$$\angle IGH = \arccos(rac{\overline{GH}^2 + \overline{GI}^2 - \overline{HI}^2}{2\overline{GH}\ \overline{GI}})$$

From the lower half triangle cna get

$$\angle GIK = \arccos(\frac{\overline{GI}^2 + \overline{IK}^2 - \overline{GK}^2}{2\overline{GI} \overline{IK}})$$

$$\theta_2 = -\angle IGH + \angle GIK$$

$$\angle GIH = \arccos(\frac{\overline{GI}^2 + \overline{HI}^2 - \overline{GH}^2}{2\overline{GI} \overline{HI}})$$

$$\theta_3 = -(\angle GIK + \angle GIH)$$

Finally, consider the fifth axis. Since the problem is limited to the gripper facing downwards,  $(\phi, \theta, \psi)$  only needs to consider one rotation  $\phi$ , which can be found when written as a rotation matrix

$$_{5}^{0}R=egin{bmatrix}\cos(\phi)&-\sin(\phi)&0\-\sin(\phi)&-\cos(\phi)&0\0&0&-1\end{bmatrix}$$

The overall rotation angle can be obtained. In this posture, only the first and fifth axis can rotate in the  $z_0$  axis direction, and the angle of the first axis has been calculated so

$$heta_5 = rctan 2(-rac{0}{5}R_{21}, rac{0}{5}R_{11}) + heta_1$$

All angles have been found.

(2.a)

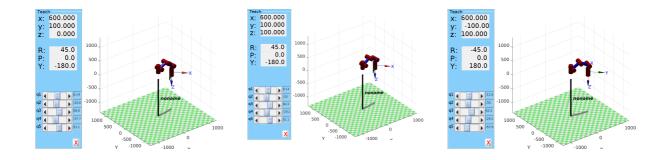
$$(\theta_1,\theta_2,\theta_3,\theta_4,\theta_5) = (6.1354^\circ, -20.8224^\circ, 58.5447^\circ, -37.7222^\circ, 51.1354^\circ)$$

(2.b)

$$(\theta_1, \theta_2, \theta_3, \theta_4, \theta_5) = (6.1354^{\circ}, -32.9612^{\circ}, 62.1556^{\circ}, -29.1944^{\circ}, 51.1354^{\circ})$$

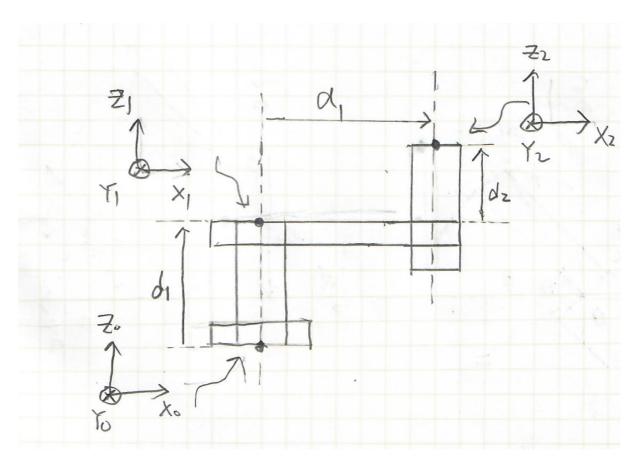
(2.c)

$$(\theta_1,\theta_2,\theta_3,\theta_4,\theta_5) = (-12.7892^\circ, -32.9612^\circ, 62.1556^\circ, -29.1944^\circ, -57.7892^\circ)$$



#### PART D

(1)



Joint	$lpha_{i-1}(^\circ)$	$a_{i-1}(mm)$	$d_i(mm)$	$ heta_i$
1	0	0	$d_1$	$\theta_1$
2	0	$a_1$	$d_2$	0

(2)

 $heta_1,d_2$