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| **Transmission Line Impedance Estimation** |
| OpenECA Analytic Design Document |
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| **Chen Wang** |
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# **Statement of Work**

The analytic of transmission line impedance calibration is aiming to use linear Least Squares Estimation method to estimate the true line impedance of the whole power system given measurement error of the transducers. The alpha version of the program of this analytic firstly takes PSS\E simulated PMU measurements as input; then, analyzes the topology of the aimed power network; thirdly starting from one of the buses taken as the calibration starting bus that equipped with revenue PT and the corresponding line that equipped with revenue CT, conducts single transmission line impedance calibration; finally propagate the accuracy to the whole system based on its tree topology. The alpha version program is designed to be operating without openECA platform.

# **Introduction**

One of the ways to get the knowledge of the transmission lines’ impedances is to use the voltage and current measurements one get from the PMUs to conduct the Ohm Law. But as is shown in the previous analytic of CT/PT Calibration, such measurement would have ratio errors from the instrument transformers (CT/PTs) and the errors added by PMUs brought by the digitalization process. Both the errors brought by CT/PTs and PMUs is going to influence the accuracy of the calculation of the line. Therefore, one need to first know the components of the errors, then utilize estimation methods to find out the exact error to find the true impedances within the system.

# **CT/PT Calibration Methodology**

## *Measurement Data Flow*

The actual voltages and currents of each single transmission line will firstly detected by the CT/PTs, and those values should be complex numbers and three-phase separately. Such transducers will inevitably add ratio errors which are also three-phases to those true values and send them to the PMUs. PMUs then are going to quantize each phase’s data and provide the positive sequence measurements to the energy management system after computation. The whole process is shown in Figure III‑



Figure III‑1. Voltage and Current Measurement Data Flow

The ratio errors, both three-phase separately and positive sequence, aforementioned are also complex values. For each single transmission line, the relationship among true values, measurements, and ratio errors is shown as in Figure III‑2 and equation .



Figure III‑2. CT/PT Measurements Demonstration



where,  and  are the measurement of and true voltage on bus , respectively;  and  are the measurement of and true current flowing from bus  to bus , respectively;  and  are the ratio errors of voltage and currents on or flowing out of bus , respectively. The values on bus  are similar. All the values aforementioned are of positive sequence.

Accordingly, one can find the ratio correction factors , , , and  as follow



Such factors are equivalent to the ratio errors and will be used in the following calibration methodology.

However, for various phases, the ratio errors should be different. According to the IEEE C57.13-2016 standard, the ratio errors are as follows:



where  is the ratio error of phase A voltage measurement;  is the error magnitude, which should be within ;  is the error angle, which should be within . The ratio errors of the other two phases are respectively similar.

The CT/PTs will integrate ratio errors to the three-phase measurements separately. But the PMUs will provide positive sequence values. Therefore, taking voltage as example, the positive sequence voltage measurements would be as follow



where,  is the measured positive sequence voltage value; , , and  are the true values of three-phase voltages respectively;  is .

If the three-phase voltage measurements are balanced, namely



then,



Therefore, the positive sequence ratio error is



For the field data, the differences between three-phase measurements are less than 1%. Thus, as the three phases’ ratio errors keep constant, there is a constant positive sequence ratio error for each PMU measurements.

## *PMU Quantization and Error*

The PMUs installed on each 500KV buses within the system would provide time-stamped voltage and current measurements. According to the IEEE Std. C37.118, the digital signals output by PMUs are firstly quantized and then transferred to the positive sequence values. The quantization scale of the three-phase voltage measurements is 20V and that of the three-phase current measurements is 0.65A. Such results are based on the real PMU data

With the plot, some conclusions could be reached. Firstly, both the real and imaginary parts of the three single phases’ measurements are perfectly and separately quantized by the PMU because of its own characteristics.

Then the positive sequence measurements are thus approximately quantized. Take  as the quantization scale. The quantization error of the positive sequence values, i.e. , is uniformly distributed within  according to Theorem III‑1.

**Theorem III‑1**. If  is uniformly distributed in  then  is uniformly distributed in  for any  and .

Since the PMU quantization error is also uniformly distributed within a known range, the expectation of such error is 0 and therefore unbiased. During the estimation process, such 3-phase to positive sequence transfer error could be eliminated by conducting multiple times calibration and averaging the estimation results.

## *Single Transmission Line Impedance Calibration Methodology*

The single transmission line impedance calibration method is similar to the instrument transformer calibration method. We are also going to use the measured voltages and currents from both sides of the line to conduct the LSE algorithm. The estimation result is going to be the estimated impedance matrix .

However, the impedance and susceptance here is unknown and to be calculated. To simplify the calculation, two new variables are introduced as shown in equation .



With the entries of , we can calculate the estimated impedance and susceptance by compute estimated  firstly.



If we know the correction factors of the voltage and current measurements of the bus , the correction factors on bus  can then be calibrated as follow.



Then the estimated susceptance can be calculated as follow.



The single transmission line impedance can be calibrated as follow.



## *System Propagation Methodology*

The single line impedance calibration method can not only estimate the impedance and susceptance of the concerned transmission line, but also calibrate the correction factors of the instrument transformers on the other side of the line. However, this is based on the fact that both the  and  are known.

Since the voltage on one bus will always remain the same no matter measured from which line that connects to it, the bus voltage correction factor is chosen as the propagation media. Based on the aforementioned fact, we can find that if there are  lines that connected to the concerned bus  as in Figure III‑3, the voltages measured by different PTs on those  lines should be as follow.



Figure III‑3. Bus Voltage Injections



where,  is the true value of the voltage on bus ;  is the voltage correction factor of the PT measuring the voltage of bus  on line ;  is the voltage measurement of bus  on line  and .

Therefore, if we know one of the correction factors from the calibration of the previous line, we will be able to reach the true value of the voltage on the concerned bus. Thus we can calculate all the other ones and acquire enough information to calibrate the following lines.



In order to calculate all the ’s of current injections on the bus , we firstly need to know all the current injection measurements. A typical bus injection that has  lines connected to it can be shown as Figure III‑4.



Figure III‑4 Bus Current Injections Demonstration



If one of the correction factors, for example , is known, this equation can be written as



With the LSE method and the current injections measurements, the correction factors of all the other lines connected to the concerned bus can be estimated.

With such propagation method, if we can form the whole system into a tree topology, then all the CTs and PTs within such tree can be calibrated, given that the impedance as well as the susceptances are known and the existence of a redundant PT. The graphical searching method could be Breadth First Search(BFS) which is shown in Figure III‑5. The numbers are the order based on which the nodes are visited.



Figure III‑5. Breadth First Search Method

# **Program Architecture (Alpha Version)**

## *Data Structure*

The data structure of the alpha version controller is shown as follows:





## *Data Flow*



# **Program Details (Alpha Version)**

## *Program Process*

1. PSS\E power system operation simulation

Use PSS\E to conduct power flow based on the DVP power system and the morning load pick-up curve to generate the voltages of the buses and currents flowing though concerned transmission lines.

1. Raw data processing

Read in CSV file generated by Python and PSS\E.

1. Building error model (For test plan)

Add CT/PT measurement errors and PMU errors to the raw data of voltages and currents based on the derived error model; record the positive sequence errors and the true line impedance and susceptance.

1. System topology analysis

Analyze the system topology based on the from-bus and to-bus information of the concerned lines; find the order of calibration propagation.

1. Transmission line impedance calibration

Conduct the transmission line impedance calibration starting from the bus and corresponding line that equipped with revenue transducers; use the injection propagation method aforementioned to calibrate the whole concerned system.