

# Acceleration of steady-state lattice Boltzmann simulations on non-uniform mesh using local time step method

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## GILBM and ISLBM

Extend **Interpolation-Supplemented LBM (ISLBM)** to general curvilinear coordinates through **conformal mapping**, without changing the lattice system. But the point of mapping is How can I deal with discrete particle velocity set.

### Key Features:

- Cartesian  $\rightarrow$  Curvilinear via coordinate mapping
- Curved particle paths in computational domain
- Lattice structure remains **unchanged**
- Pull-back interpolation for streaming

$$f_{\alpha}(\vec{\xi}, t + \Delta t) = f_{\alpha}^*(\vec{\xi} - \Delta \vec{\xi}_{\alpha}, t) \quad (1)$$

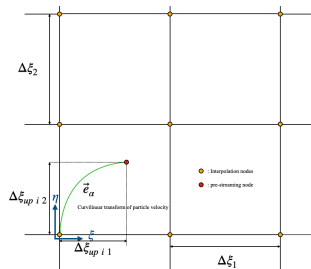


Figure: GILBM: curved paths in  $\xi$ -space

## Jacobian Transformation Matrix:

$$\begin{bmatrix} \xi_x & \xi_y \\ \eta_x & \eta_y \end{bmatrix} = \frac{1}{J} \begin{bmatrix} y_\eta & -x_\eta \\ -y_\xi & x_\xi \end{bmatrix}, \quad J = x_\xi y_\eta - x_\eta y_\xi$$

## Lamé Coefficient & Unit Vector:

$$h_1 \equiv \left| \frac{\partial \vec{r}}{\partial q_1} \right|, \quad \vec{e}_1 \equiv \frac{1}{h_1} \frac{\partial \vec{r}}{\partial q_1}$$

Position vector differentials:

$$\frac{\partial \vec{r}}{\partial \xi} = h_\xi \vec{e}_\xi = x_\xi \vec{e}_x + y_\xi \vec{e}_y$$

$$\frac{\partial \vec{r}}{\partial \eta} = h_\eta \vec{e}_\eta = x_\eta \vec{e}_x + y_\eta \vec{e}_y$$

## Physical Meaning:

- $h_i$ : Scale factor (metric coefficient)
- $\vec{e}_i$ : Local tangent direction
- $J$ : Jacobian determinant (area scaling)
- Transforms derivatives between coordinates

## Standard LBE (BGK Collision Operator):

$$f_{\alpha}(\vec{x} + \vec{c}_{\alpha}\Delta t, t + \Delta t) = f_{\alpha}(\vec{x}, t) + \omega(f_{\alpha} - f_{\alpha}^{eq})$$

## LBE with MRT Collision Operator:

$$M\vec{f}(\vec{x} + \vec{c}_{\alpha}\Delta t, t + \Delta t) = M\vec{f}(\vec{x}, t) + SM(\vec{f} - \vec{f}^{eq})$$

### Collision Step:

Position appears only at grid nodes; collision has **no spatial derivatives**.

⇒ Direct substitution:  $\vec{x} \rightarrow \vec{\xi}$

$$f_i^*(\vec{\xi}, t) = f_i + \omega(f_i^{eq} - f_i)$$

### Streaming Step:

Requires **path integration** of particle velocity in curvilinear space.

$$f_{\alpha}(\vec{\xi}, t) = f_{\alpha}^*(\vec{\xi} - \Delta\xi_{\alpha}, t)$$

(Pull-back from pre-streaming position via interpolation)

## Definition

Transform Cartesian lattice velocity to curvilinear coordinates:

$$e_{\alpha}^j = c_{\alpha}^i \frac{\partial \xi_j}{\partial x_i} \dots (\text{assume lattice speed} = 1)$$

- $c_{\alpha}^i$ : Dimensionless discrete velocity (e.g., D2Q9:  $0, \pm 1$ )
- $\frac{\partial \xi_j}{\partial x_i}$ : Coordinate transformation (from Jacobian)
- $\vec{e}_{\alpha}^j$ : Shows **velocity distortion** due to curvature

**Volumetric Lattice Boltzmann in Curvilinear Coordinates:**

$$\vec{e}_{\alpha} = \underbrace{c_{\alpha}^i}_{\text{an integer}} \cdot \underbrace{\vec{g}_i(\vec{\xi})}_{\text{tangent vector}} \cdot \underbrace{\frac{\Delta x}{\Delta t}}_{\text{lattice speed} \approx 1}$$

Redefine the particle's discrete velocity: Enforce the direction of velocity to be the same as the tangent vector.

From streaming step :

$$f_{\alpha}(\vec{\xi}, t + \Delta t) = f_{\alpha}^*(\vec{\xi} - \delta \vec{\xi}_{\alpha}, t)$$

In curvilinear coordinate, we have to calculate the position of the pre-streaming particles.

**Streaming Length:**

$$\delta \vec{\xi}_{\alpha} = \int_0^{\Delta t} \vec{e}_{\alpha}(\vec{\xi}(t)) dt$$

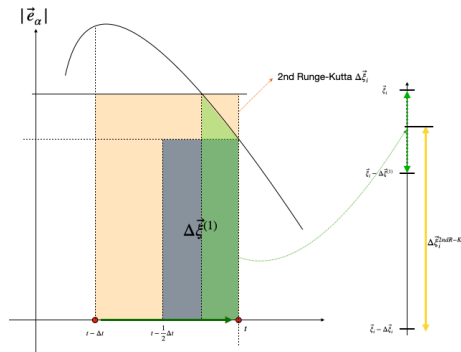
**2nd Order Runge-Kutta:**

$$\text{Step 1: } \Delta \vec{\xi}_{\alpha}^{(1)} = \frac{1}{2} \Delta t \vec{e}_{\alpha}(\vec{\xi})$$

$$\text{Step 2: } \Delta \vec{\xi}_{\alpha} = \Delta t \vec{e}_{\alpha}(\vec{\xi} - \Delta \vec{\xi}_{\alpha}^{(1)})$$

**Why not 1st order Euler?**

- Euler:  $O(\Delta t)$  error  $\rightarrow$  insufficient
- Need  $O(\Delta t^2)$  to recover Navier-Stokes
- Stress term requires 2nd order accuracy



**material derivative for the discrete-velocity Boltzmann equation:**

$$\mathcal{D}_t = \partial_t + \frac{\delta \vec{\xi}_\alpha}{\delta t} \cdot \vec{\nabla}_\xi$$

and using Taylor expansion on lattice Boltzmann equation :

$$\left( \partial_t + \frac{\delta \vec{\xi}_\alpha}{\delta t} \cdot \vec{\nabla}_\xi \right) f_\alpha + \frac{1}{2} \left( \partial_t + \frac{\delta \vec{\xi}_\alpha}{\delta t} \cdot \vec{\nabla}_\xi \right)^2 f_\alpha \Delta t \bigg|_{(\vec{\xi} - \Delta \vec{\xi}_\alpha, t)} + O(\Delta t^2) = \omega(f_\alpha(\vec{\xi} - \Delta \vec{\xi}_\alpha, t) - f_\alpha^{eq}(\rho, \vec{u}, t))$$

Therefore, we must use a method that provides higher-order temporal accuracy for the path integration, ensuring that the differential term of the velocity-discrete Boltzmann equation has at least second-order temporal accuracy.



## Three Time Scales:

- $K^{(0)}$ : Collision & streaming (mesoscopic)
- $K^{(1)}$ : Convection / advection (macroscopic)
- $K^{(2)}$ : Diffusion (macroscopic)

For three types of time scales, we can define three time variables and two types of position vector :

## Scale Operators:

$$\begin{aligned}\partial_t &= K\partial_t^{(1)} + K^2\partial_t^{(2)} \\ \vec{\nabla} &= K\vec{\nabla}^{(1)}\end{aligned}$$

## Distribution Expansion:

$$f_\alpha = f_\alpha^{eq} + Kf_\alpha^{(1)} + K^2f_\alpha^{(2)} + \dots$$

## Order $K^1$ Equation:

$$\left(\partial_t^{(1)} + \vec{e}_\alpha \cdot \vec{\nabla}^{(1)}\right)f_\alpha^{eq} = -\frac{1}{\tau}f_\alpha^{(1)}$$

## Order $K^2$ Equation:

$$\begin{aligned}\left(\partial_t^{(2)} + \vec{e}_\alpha \cdot \vec{\nabla}^{(2)}\right)f_\alpha^{eq} + \left(1 - \frac{\delta t}{2\tau}\right) \\ \times \left(\partial_t^{(1)} + \vec{e}_\alpha \cdot \vec{\nabla}^{(1)}\right)f_\alpha^{(1)} = -\frac{1}{\tau}f_\alpha^{(2)}\end{aligned}$$

### Maxwell-Boltzmann Equilibrium (Hermite Expansion):

$$f_{\alpha}^{eq} = w_{\alpha} \rho \left( 1 + \frac{e_{\alpha}^i u_i}{c_s^2} + \frac{(e_{\alpha}^i e_{\alpha}^j - c_s^2 \delta^{ij}) u_i u_j}{2c_s^4} \right)$$

### Derivatives of $f_{\alpha}^{eq}$ :

$$\frac{\partial f_{\alpha}^{eq}}{\partial u_i} \approx \frac{e_{\alpha}^i - u_i}{c_s^2} f_{\alpha}^{eq}, \quad \frac{\partial f_{\alpha}^{eq}}{\partial \rho} = \frac{f_{\alpha}^{eq}}{\rho}$$

### Conservation Laws (1st order scale):

$$\begin{aligned} \partial_t^{(1)} \rho &= -\vec{\nabla}^{(1)} \cdot (\rho \vec{u}) \\ \partial_t^{(1)} \vec{u} &= -\vec{u} \cdot \vec{\nabla}^{(1)} \vec{u} - \frac{1}{\rho} \vec{\nabla}^{(1)} p \end{aligned}$$

## Assumptions at Boundary:

- ① Constant pressure:  $\nabla p = 0$
- ② Incompressible:  $\nabla \rho = 0$

## Distribution Function at Boundary:

$$f_\alpha|_{bc} = f_\alpha^q + \omega \delta t \left( \frac{(e_\alpha^i - u_i)(e_\alpha^\beta - u_\beta)}{c_s^2} \frac{\partial u_i}{\partial x_\beta} - \frac{\partial u_\beta}{\partial x_\beta} \right) f_\alpha^q$$

## Velocity Gradient in Curvilinear Coordinates:

$$\frac{\partial u_i}{\partial x_\beta} = \frac{\partial u_i}{\partial \xi_j} \cdot \frac{\partial \xi_j}{\partial x_\beta}$$

## 2nd Order One-Side Finite Difference:

$$\left. \frac{\partial u}{\partial \xi} \right|_{i+\frac{1}{2}} = \frac{3u_i - 4u_{i-1} + u_{i-2}}{2\Delta\xi} + O(\Delta\xi^2)$$

**GILBM Initialization:**

- ❶ Set  $Re$ , relaxation factor  $\omega$
- ❷ Contravariant velocity:

$$e_{\alpha}^i = c_{\alpha}^{\beta} \frac{\partial \xi_i}{\partial x_{\beta}}$$

- ❸ Global time step (CFL):

$$\Delta t = \text{CFL} \cdot \min \left| \frac{1}{e_{\alpha}^i} \right|$$

- ❹ Relaxation time:  $\tau = \Delta t / \omega$
- ❺ Viscosity:  $\nu = (\tau - 0.5\Delta t)c_s^2$

**Runtime Loop:**

- ❶ **Collision:**  $f_i^* = f_i + \omega(f_i^{eq} - f_i)$
- ❷ **Streaming:**  $f_i(\vec{\xi}) = f_i^*(\vec{\xi} - \Delta \vec{\xi}_i)$  (with interpolation)
- ❸ **Boundary:** Apply  $f_{\alpha}|_{bc}$
- ❹ **Macroscopic:**  $\rho = \sum_i f_i, \vec{u} = \frac{1}{\rho} \sum_i f_i \vec{c}_i$

Pre-calculation reduces runtime by  $\sim 50\%$

### GILBM: Key Points

- ① **Coordinate Transform:** Jacobian relation maps Cartesian  $\leftrightarrow$  curvilinear
- ② **Collision:** Direct substitution  $\vec{x} \rightarrow \vec{\xi}$  (no spatial derivatives)
- ③ **Streaming:** Path integration with contravariant velocity  $e_{\alpha}^j$
- ④ **Accuracy:** 2nd order RK required for N-S recovery
- ⑤ **Boundary:** Distribution from Chapman-Enskog with  $\nabla p = 0$ ,  $\nabla \rho = 0$
- ⑥ **Efficiency:** Pre-calculated contravariant velocity saves  $\sim 50\%$  runtime

**Limitation:** MRT operator extension to curvilinear coordinates not yet developed.