

A Doublet-Lattice Method for Calculating Lift Distributions on Oscillating Surfaces in Subsonic Flows

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Approximate solutions from the linearized formulation are obtained by idealizing the surface as a set of lifting elements which are short line segments of acceleration-potential doublets. The normal velocity induced by an element of unit strength is given by an integral of the subsonic kernel function. The load on each element is determined by satisfying normal velocity boundary conditions at a set of points on the surface. It is seen a posteriori that the lifting elements and collocation stations can be located such that the Kutta condition is satisfied. The method obviates the prescription of singularities in lift distribution along lines where normal velocity is discontinuous, and is readily adapted for problems of complex geometries. Results compare closely with those from methods that prescribe lifting pressure modal series, and from pressure measurements. The technique constitutes an extension of a method developed by S. G. Hedman for steady flow.†

Nomenclature

AR	= aspect ratio
b	= semichord
c	= chord
K	= kernel function
\mathcal{K}	= numerator of singular kernel
k	= reduced frequency, $k = \omega b/U$
M	= freestream Mach number
NC	= number of boxes on chord
NS	= number of boxes on semispan
P	= lifting pressure
p	= dimensionless lifting pressure coefficient, $p = P/\frac{1}{2}\rho U^2$
W	= normal velocity at surface
w	= dimensionless normal velocity (normalwash), $w = W/U$
t	= time
s, σ	= curvilinear spanwise coordinates on the surface; s also denotes span of planar surface
U	= freestream velocity
x, y, z	= Cartesian coordinates
ξ, η, ζ	= Cartesian coordinates
γ	= dihedral angle
ω	= frequency of oscillation
ρ	= freestream density
$(-)$	= complex amplitude

Introduction

THE linearized formulation of the oscillatory, subsonic, lifting surface theory relates the normal velocity at the surface

$$W(x, s, t) = URl[\bar{w}(x, s) \exp(i\omega t)]$$

to the pressure difference across the surface

$$P(x, s, t) = \frac{1}{2}\rho U^2 Rl[\bar{p}(x, s) \exp(i\omega t)]$$

by a singular integral equation and the Kutta condition at

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‡ At the time of writing, the authors learned that a similar extension had been developed independently by Stark,²² which has been reported in Ref. 23.

the trailing edge (TE):

$$\bar{w}(x, s) = \frac{1}{8} \pi \oint_s K(x, \xi; s, \sigma; \omega, M) \bar{p}(\xi, \sigma) d\xi d\sigma \quad (1)$$

$$\bar{p}[x_{TE}(s), s] = 0$$

where (x, s) are orthogonal coordinates on the surface S such that the undisturbed stream is directed parallel to the x axis.

Rodemich¹ has derived an expression for the kernel function for a nonplanar surface in the form

$$K = e^{-(i\omega x_0/U)} (K_1 T_1 + K_2 T_2) / r_1^2 \quad (2)$$

where

$$T_1 = \cos[\gamma(s) - \gamma(\sigma)]$$

$$T_2 = \left\{ \frac{z_0}{r_1} \cos[\gamma(s)] - \frac{y_0}{r_1} \sin[\gamma(s)] \right\} \times$$

$$\left\{ \frac{z_0}{r_1} \cos[\gamma(\sigma)] - \frac{y_0}{r_1} \sin[\gamma(\sigma)] \right\}$$

$$r_1 = (y_0^2 + z_0^2)^{1/2}$$

$$x_0 = x - \xi \quad y_0 = y - \eta \quad z_0 = z - \zeta$$

and Landahl² has simplified the forms of K_1 and K_2 to read

$$K_1 = I_1 + [Mr_1/R][e^{-ik_1 u_1}/(1 + u_1^2)^{1/2}]$$

$$K_2 = -3I_2 - \frac{ik_1 M^2 r_1^2}{R^2} \frac{e^{-ik_1 u_1}}{(1 + u_1^2)^{1/2}} -$$

$$\frac{Mr_1}{R} \left[(1 + u_1^2) \frac{\beta^2 r_1^2}{R^2} + 2 + \frac{Mr_1 u_1}{R} \right] \frac{e^{-ik_1 u_1}}{(1 + u_1^2)^{3/2}}$$

where

$$I_1 = \int_{u_1}^{\infty} \frac{e^{-ik_1 u}}{(1 + u^2)^{3/2}} du \quad (3)$$

$$I_2 = \int_{u_1}^{\infty} \frac{e^{-ik_1 u}}{(1 + u^2)^{5/2}} du \quad (4)$$

$$u_1 = (MR - x_0)/\beta^2 r_1$$

$$k_1 = \omega r_1/U \quad \beta = (1 - M^2)^{1/2}$$

$$R = (x_0^2 + \beta^2 r_1^2)^{1/2}$$

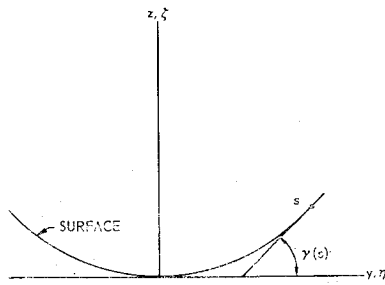


Fig. 1 Coordinate system.

The coordinate system is illustrated in Fig. 1. The symbol \oint means that the integral in Eq. (1) is defined in the "finite part" sense.⁸

The traditional method for obtaining approximate solutions for \bar{p} when \bar{w} is given is to assume a series approximation

$$\bar{p} \approx \sum_i \sum_j a_{ij} f_i(x) g_j(s)$$

and to determine the coefficients a_{ij} by satisfying normal-velocity conditions on the surface. Known properties of the lifting pressure distribution \bar{p} such as the behavior near surface edges are built into the approximation by appropriate choice of the functions in the series. This technique has been used successfully for many years, although most applications have been for planar wings without control surfaces.

Consideration of the efforts needed to develop a single computer program to handle a fairly general class of non-planar problems has led the authors to seek a technique that would obviate the prescription of the behavior of \bar{p} along edges and corners and, in fact, would remove a priori restrictions on the global behavior of the force distribution. The "box methods" for the supersonic problem provide examples of the method sought.

Doublet-Lattice Method

We describe a method which is an extension of the one developed for steady subsonic flow by Hedman⁴ in 1965. The elements of the technique are to be found in the vortex-lattice method of Falkner.⁵ The present study may be regarded as an extension of the method of Hedman in an analogous manner to the procedure by which Runyan and Woolston⁶ extended the method of Falkner to the oscillatory case. Since it appears at the present time that a rigorous analytical basis for the method is not available, we present an operational description as follows.

It is assumed that the surface can be approximated by segments of planes. The surface is divided into small trapezoidal panels ("boxes") in a manner such that the boxes are

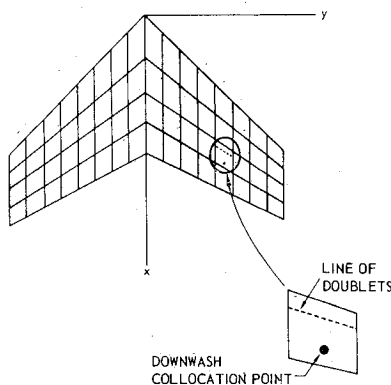


Fig. 2 Surface and panel geometry.

arranged in columns parallel to the freestream (Fig. 2), and surface edges and fold lines lie on box boundaries. The $\frac{1}{4}$ -chord line of each box is taken to contain a distribution of acceleration potential doublets⁸ of uniform but unknown strength. In steady flow, each doublet line segment is equivalent to a horseshoe vortex whose "bound" segment coincides with the doublet line.

Let n be the number of boxes and f be the constant force per unit length of the $\frac{1}{4}$ -chord line of a box. The amplitude of the doublet strength of the j th line segment is

$$(\bar{f}_j/4\pi\rho) \int_{l_j} d\mu$$

where $d\mu$ is the incremental length and l_j is the length of the line segment, and the amplitude of the normal velocity (normalwash) induced at a point (x_i, s_i) on the surface by the j th doublet line is

$$\bar{w}_j(x_i, s_i) = \left(\frac{\bar{f}_j}{4\pi\rho} U^2 \right) \oint_{l_j} K[x_i, s_i; x_j(\mu), s_j(\mu)] d\mu$$

The total normal wash induced at point (x_i, s_i) is the sum of the normal washes induced by the n doublet lines

$$\bar{w}(x_i, s_i) = \sum_{j=1}^n \left(\frac{\bar{f}_j}{4\pi\rho} U^2 \right) \oint_{l_j} K[x_i, s_i; x_j(\mu), s_j(\mu)] d\mu \quad (5)$$

If Eq. (5) is applied at n downwash points on the surface, the \bar{f}_j are determined. The force on the doublet line is taken as the force on the box and the pressure difference across the surface is approximated by

$$\begin{aligned} \bar{P}_j &= \text{force}/(\text{box area}) = \bar{f}_j l_j / (\text{box area}) \\ &= \bar{f}_j / \Delta x_j \cos \lambda_j \end{aligned}$$

where Δx_j is the box average chord and λ_j the sweep angle of the doublet line, so that

$$\bar{f}_j / 4\pi\rho U^2 = \frac{1}{8} \pi \bar{p}_j \Delta x_j \cos \lambda_j$$

We note that the induced downwash calculated by Eq. (5) will be infinite if the downwash point lies on a doublet line segment or downstream from its end points. Furthermore, the Kutta condition has not been imposed. However, from numerical experimentation with this technique, it has become apparent that the Kutta condition will be satisfied when each downwash point is the $\frac{3}{4}$ -chord point at midspan of a box.

Equation (5) may finally be written

$$\bar{w}_i = \sum_{j=1}^n D_{ij} \bar{p}_j$$

where

$$D_{ij} = \left(\frac{1}{8} \pi \right) \Delta x_j \cos \lambda_j \oint_{l_j} K[x_i, s_i; x_j(\mu), s_j(\mu)] d\mu \quad (6)$$

If A_{ij} are the elements of the matrix whose inverse is the matrix of D_{ij} , then

$$\bar{p}_i = \sum_{j=1}^n A_{ij} \bar{w}_j$$

provides the approximate solution for the lifting pressure coefficients.

Generalized force coefficients are computed approximately by

$$\bar{Q}_{ij} = \frac{1}{b_r^2 s_r} \sum_{k=1}^n h_k^{(i)} \bar{p}_k^{(j)} S_k$$

⁸ See, e.g., Ref. 7, pp. 189 and 198, or Ref. 8, pp. 19, 130, and 211 for a discussion of Prandtl's acceleration potential.

where

- S_k = area of box k
 $h_k^{(i)}$ = deflection in mode i of $\frac{1}{4}$ -chord, midspan point of box k
 $\bar{p}_k^{(j)}$ = pressure coefficient in mode j at box k
 b_r = reference semichord
 s_r = reference semispan

Working Forms

Approximate evaluation of the integral in Eq. (6) is achieved by approximating the integrand by a simple function. We consider the downwash induced at a receiving point $R = (x_R, y_R, z_R)$ by a doublet line segment whose midpoint is S_m and whose inboard and outboard end points are S_i and S_o , respectively. Let

$$\mathcal{K} = r_1^2 K$$

Denote

$$\mathcal{K}_m = \mathcal{K}(R, S_m) = \mathcal{K}(x_R, y_R, z_R; x_{S_m}, y_{S_m}, z_{S_m}; \omega, M)$$

$$\mathcal{K}_i = \mathcal{K}(R, S_i) \quad \mathcal{K}_o = \mathcal{K}(R, S_o)$$

Define the coordinate system (Fig. 3)

$$\eta = y \cos \gamma_s + z \sin \gamma_s$$

$$\zeta = -y \sin \gamma_s + z \cos \gamma_s$$

If the length of the doublet segment is small, it may be anticipated that a parabolic approximation for \mathcal{K} along the segment would be sufficiently accurate for evaluating the integral;

$$I_{ij} = \oint_{-e}^e K[x_i, s_i; x_j(\eta), s_j(\eta); \omega, M] \cos \lambda_j d\eta \quad (7)$$

$$\approx \oint_{-e}^e \frac{A\eta^2 + B\eta + C}{(\eta_0 - \eta)^2 + \zeta_0^2} d\eta$$

where

$$e = \frac{1}{2} l_j \cos \lambda_j$$

$$\eta_0 = (y_R - y_{S_m}) \cos \gamma_s + (z_R - z_{S_m}) \sin \gamma_s$$

$$\zeta_0 = -(y_R - y_{S_m}) \sin \gamma_s + (z_R - z_{S_m}) \cos \gamma_s$$

$$A = (\mathcal{K}_i - 2\mathcal{K}_m + \mathcal{K}_o)/2e^2$$

$$B = (\mathcal{K}_o - \mathcal{K}_i)/2e \quad C = \mathcal{K}_m$$

The result of the integration is

$$I_{ij} \approx [(\eta_0^2 - \zeta_0^2)A + \eta_0 B + C] |\zeta_0|^{-1} \tan^{-1} \left(\frac{2e|\zeta_0|}{r_1^2 - e^2} \right) + \left(\frac{1}{2} B + \eta_0 A \right) \log \frac{r_1^2 - 2\eta_0 e + e^2}{r_1^2 + 2\eta_0 e + e^2} + 2eA$$

where $r_1^2 = \eta_0^2 + \zeta_0^2$. For the planar case ($\zeta_0 \rightarrow 0$),

$$I_{ij} = (\eta_0^2 A + \eta_0 B + C) \left(\frac{1}{\eta_0 - e} - \frac{1}{\eta_0 + e} \right) + \left(\frac{1}{2} B + \eta_0 A \right) \log \left(\frac{\eta_0 - e}{\eta_0 + e} \right)^2 + 2eA$$

In order to converge to Hedman's vortex-lattice results for steady flow and to improve the approximation of Eq. (7), the authors have found it necessary to subtract the steady part ($\omega = 0$) from \mathcal{K} before applying the preceding formulas, and then to add the effect of a horseshoe vortex. The error in the parabolic approximation appears to be small if the division of the surface into boxes is such that the boxes have aspect ratios of order unity. The steady values of K_1 and K_2 are

$$K_1(\omega = 0) = 1 + x_o/R$$

$$K_2(\omega = 0) = -2 - (x_o/R)(2 + \beta^2 r_1^2/R^2)$$

In any event, it is necessary to evaluate numerically the kernel function, Eq. (2), at a number of points, and hence to evaluate the integrals I_1 and I_2 , Eqs. (3) and (4), respectively. Approximate evaluation of these integrals may be accomplished in many ways. L. Schwarz⁹ has given an ex-

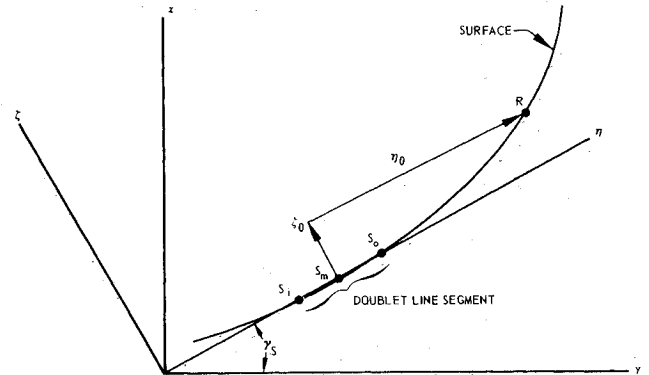


Fig. 3 Sending panel coordinate system.

pression for I_1 in terms of infinite series. However, we prefer to approximate the integrands by simple functions. It is sufficient to consider nonnegative arguments because of symmetry properties of the integrand. Integrating Eq. (3) by parts gives

$$I_1(u_1; k_1) = \left[1 - \frac{u_1}{(1 + u_1^2)^{1/2}} \right] e^{-ik_1 u_1} - ik_1 \int_{u_1}^{\infty} \left[1 - \frac{u}{(1 + u^2)^{1/2}} \right] e^{-ik_1 u} du$$

Watkins, Runyan, and Cunningham¹⁰ have given the formula

$$t/(1 + t^2)^{1/2} \approx 1 - 0.101 \exp(-0.329t) - 0.899 \exp(-1.4067t) - 0.09480933 \exp(-2.90t) \sin \pi t \quad (t \geq 0)$$

which when substituted in the foregoing yields a simple expression for I_1 . The integral I_2 is evaluated in similar fashion, requiring integration of Eq. (4) by parts twice.

In view of the lack of a rigorous basis for the foregoing assumptions, it is necessary to demonstrate the adequacy of the doublet-lattice method by comparison of results with solutions obtained by other means, and with experimental data.

Results for Two-Dimensional Flow

For planar flow, the integral equation (1) becomes the one-dimensional integral equation of Possio (see, e.g., Sec. 6-4 of Ref. 7) and the doublet line segments become two-dimensional doublets on the chord. The results of the doublet-lattice method presented here have been obtained by dividing the airfoil chord into equal intervals and locating each sending and receiving point at the $\frac{1}{4}$ -chord and $\frac{3}{4}$ -chord, respectively, of each interval.

For graphical presentation of results, the values of the lifting pressure coefficient \bar{p} are plotted at the sending points and smooth curves are drawn going to zero at the trailing edge. In describing results, we use the term "boxes" to mean intervals in two-dimensional flow or small panels in three-dimensional flow, and

NC = number of boxes per surface chord

NS = number of boxes per semispan (planar surfaces)

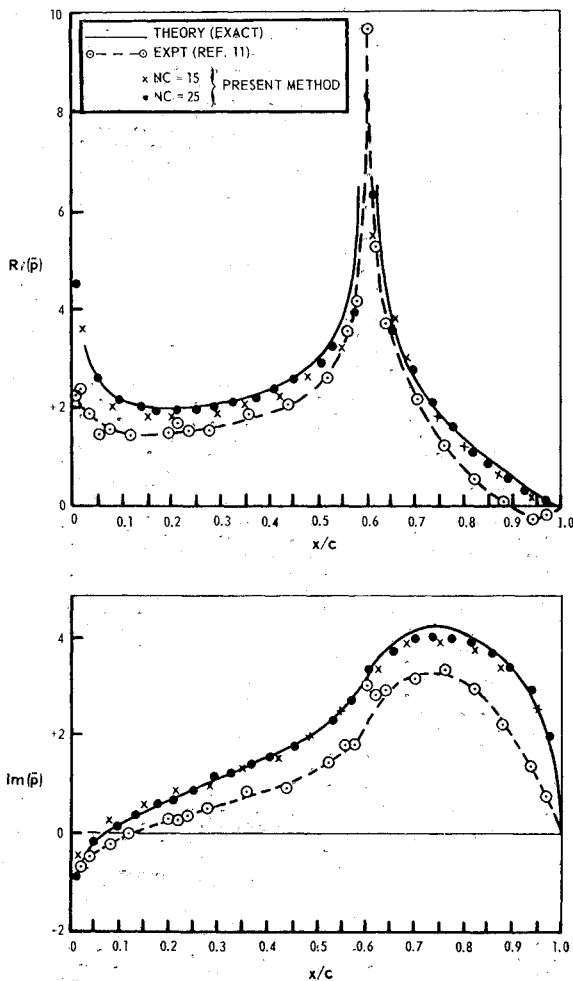


Fig. 4 Lifting pressure distribution on airfoil with oscillating flap in two-dimensional flow, $M = 0$, $k = 1.0$.

For incompressible flow, exact solutions are available. Solutions for an airfoil with oscillating flap are compared in Fig. 4, where measurements reported by Bergh¹¹ are included.

For compressible flow, Table 1 presents a comparison of generalized forces for a flapped airfoil from the present method and from the tables of Ref. 12. The coefficients are defined by

$$L = \pi \rho U^2 b^2 e^{ikt} (A k_a + B k_b + C k_c)$$

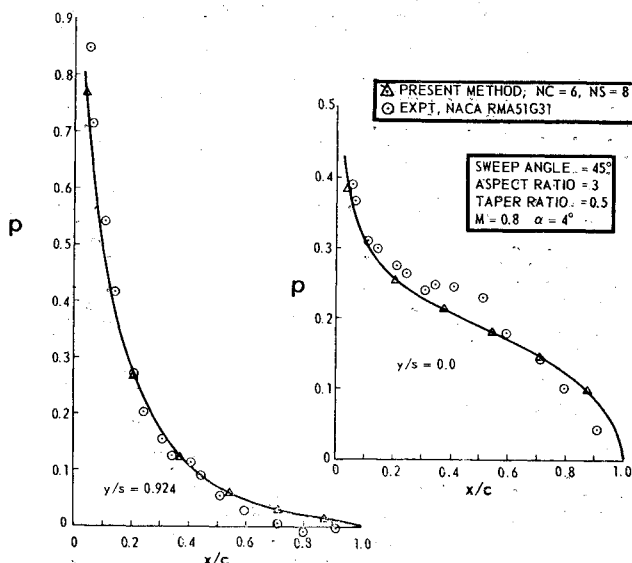


Fig. 5 Lift distribution on swept wing in steady flow.

$$M = \pi \rho U^2 b^2 e^{ikt} (A m_a + B m_b + C m_c)$$

$$N = \pi \rho U^2 b^2 e^{ikt} (A n_a + B n_b + C n_c)$$

where

L = force of airfoil and flap, positive downward

M = moment of wing and flap about midchord, positive tail heavy

N = moment of flap about hinge axis, positive tail heavy

Ab = translation amplitude, positive downward

B = amplitude of airfoil rotation about midchord, positive trailing edge down

C = amplitude of flap rotation, positive trailing edge down

Results shown in Table 1 are for the case $M = 0.8$, $k = 0.9$, $\tau = (\text{flap chord})/(\text{airfoil chord}) = 0.3$. The tabulated results indicate that the doublet-lattice approximation is valid for high subsonic Mach numbers and reduced frequencies of order unity.

Results for Three-Dimensional Flows

Figure 5 compares calculated lift distributions with measurements reported by Kolbe and Boltz¹³ for a swept, tapered wing at incidence in steady flow. For this problem, the semiwing was divided into 48 boxes, each containing a horseshoe vortex as in Hedman's method. Results for the wing stations shown were obtained by interpolation.

Calculations and measurements for a wing with partial-span flap are presented in Fig. 6. The curves labeled "experiment" were obtained by reduction of graphical data of Hammond and Keffer,¹⁴ and, for this reason, are rather imprecise. Calculations were made with 80 horseshoe vortices on the semiwing, eight vortices being on the flap. Landahl¹⁵ has shown that both the form and strength of the pressure singularity at the hinge line can be determined analytically. The expression for the lift distribution for unit flap angle is

$$p = (-2/\pi \beta_n) \cos \lambda_c \log |(x - x_c)/c| + O(1) \quad (8)$$

where x_c = streamwise coordinate of hinge, λ_c = hingeline sweep angle, $\beta_n = (1 - M^2 \cos^2 \lambda_c)^{1/2}$, and c = local chord. For the wing considered here, $\lambda_c \approx 30^\circ$ and $M = 0.6$; the singular part of Eq. (8) becomes

$$p \approx -0.645 \log |(x - x_c)/c| \quad (9)$$

The graph of this expression is labeled "local solution" in Fig. 6a. Figure 6b shows the distribution of lift on the semiwing calculated by the Hedman vortex-lattice technique.

Both kernel function calculations and measurements of lift distribution reported by Lessing, Troutman, and Menees¹⁶ are compared in Fig. 7 with results from the doublet-lattice method. The rectangular wing (aspect ratio = 3) considered is oscillating in a bending mode described approximately by

$$\bar{h} \approx 0.18043 |(y/s)| + 1.70255 (y/s)^2 - 1.13688 |(y/s)^3| + 0.25387 (y/s)^4$$

where \bar{h} is the nondimensional deflection amplitude. In Fig. 7, α_h denotes the magnitude of the effective oscillatory angle of attack at the wing tip due to bending.

Table 1 Coefficients for oscillating flapped airfoil

	20 "boxes"	30 "boxes"	Ref. 12
k_a	-0.0075 - 1.118i	-0.0197 - 1.119i	-0.0444 - 1.1201i
b_b	-1.571 - 0.0291i	-1.574 - 0.0795i	-1.5755 - 0.0267i
k_c	-0.4835 + 0.0789i	-0.4824 + 0.0823i	-0.4803 + 0.0868i
m_a	0.3293 + 0.1005i	0.3303 + 0.0924i	0.3309 + 0.0760i
m_b	-0.0391 - 0.8604i	-0.0572 - 0.8623i	-0.0946 - 0.8619i
m_c	-0.4075 + 0.0021i	-0.4105 + 0.0058i	-0.4147 + 0.0248i
n_a	0.0584 - 0.0626i	0.0591 - 0.0638i	0.0601 - 0.0661i
n_b	-0.0745 - 0.1456i	-0.0762 - 0.1474i	-0.0798 - 0.1504i
n_c	-0.0912 - 0.0696i	-0.0919 - 0.0712i	-0.0931 - 0.0739i

Results of computations for another rectangular wing (aspect ratio = 2) with full-span, 40% chord, oscillating flap are shown in Fig. 8. These are compared with kernel function calculations (with built-in hingeline singularity) given by Curtis, Gikas, and Hassig¹⁷ and experimental data of Beals and Targoff.¹⁸ The doublet-lattice calculations were made with 99 boxes on the semiwing and, of these, 45 boxes were on the flap.

The rolling moment of the horizontal stabilizer of a rectangular T-tail configuration is shown in Fig. 9,[†] where measurements by Clevenson and Leadbetter¹⁹ are repro-

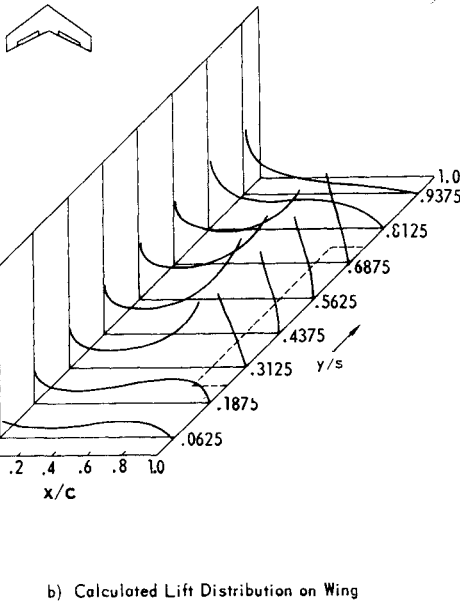
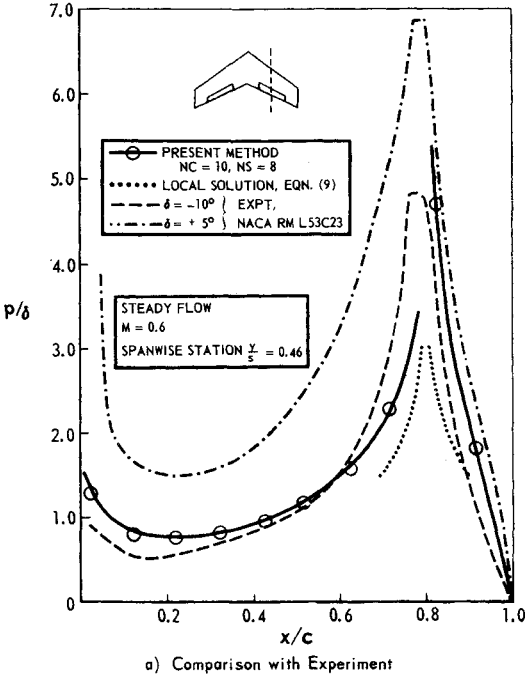


Fig. 6 Lift distribution induced by deflected partial-span flap.

[†] Note that the side force results presented in Fig. 9 of AIAA Paper 68-73 were incorrect because of a mistake in the computer program. The rolling moment of the horizontal stabilizer is presented here in place of the side force since it is a more critical measure of the accuracy of an interference theory. The complete solution is given in Ref. 21.

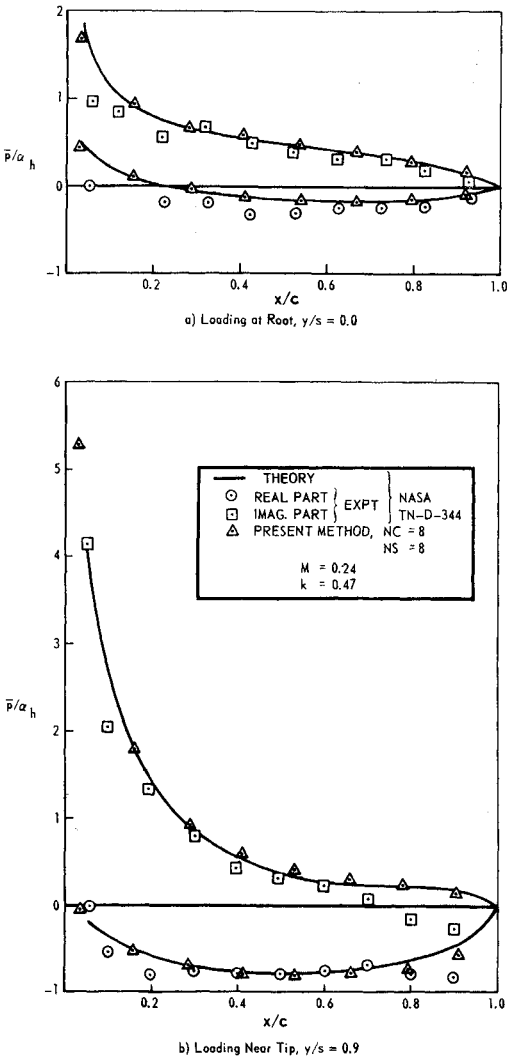


Fig. 7 Lift distribution on rectangular wing oscillating in bending mode.

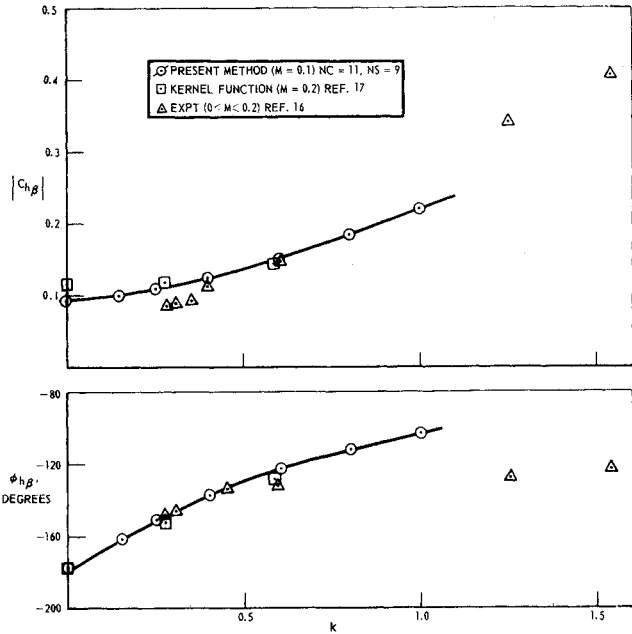


Fig. 8 Flap hinge moment coefficient due to flap oscillation for a 40% chord, full-span flap on a rectangular wing with aspect ratio 2.

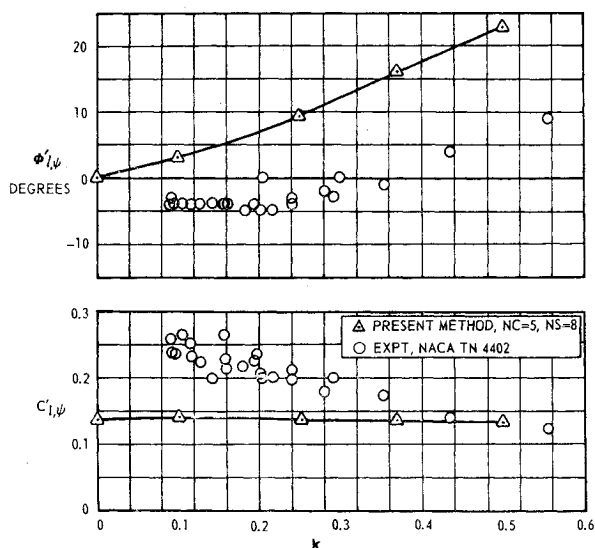


Fig. 9 Rolling moment coefficient of horizontal stabilizer for simplified T-tail oscillating in yaw about fin midchord, $M = 0$.

duced. To account in part for the tunnel wall, the image system of the fin was included in the calculations; the image of the horizontal stabilizer was neglected. Forty boxes were placed on the fin and 40 on the horizontal stabilizer semispan. The discrepancy between calculations and experimental data for increasing reduced frequency might be due to the relatively small number of boxes used or to the incomplete modelling of the effect of the tunnel wall.** The T-tail results illustrate that nonplanar interference problems are easily approached by the doublet-lattice technique.

Concluding Remarks

Within the context of the linearized, subsonic, lifting surface theory, two types of approximations are involved in the doublet-lattice method. The assumption that for purposes of calculating lift distributions the surface can be represented by a system of line segments of acceleration potential doublets is seen to be a valid approximation in view of the results obtained. As far as the authors are aware, an analytical basis for this approximation has not been established and warrants further study so that its full implications may be brought out. Such an investigation would also determine the extent to which the box chord-lengths on a strip and strip-widths across the span may be unequal. However, until a rigorous basis is found, further numerical experiments will be necessary to define the limitations of the method. The second kind of approximation is associated with the evaluation of the integrals in the kernel, Eqs. (3) and (4), and in the normalwash-pressure influence coefficients, Eq. (6). These procedures may be improved and optimized according to standard techniques of numerical quadrature.

The advantages of the doublet-lattice method arise from being able to disregard the special behavior of the lift distribution where the normalwash is discontinuous. So long as edges do not intersect boxes, a computer program based on this technique does not need to discriminate among side edges, fold lines, hinge lines, etc., and this fact is important when problems of intersecting surfaces are considered. Furthermore, since the influence coefficients D_{ij} are independent of the properties of the normalwash distribution, the same matrix computed for a given wing will yield solu-

tions for a large class of normalwash distributions; e.g., generalized forces for many different control surface configurations may be obtained from the same influence coefficient matrix.

For applications in aeroelastic analyses, aerodynamic influence coefficients that relate control point forces to deflections have been defined by Rodden and Revell.²⁰ The doublet-lattice method leads immediately to this definition of influence coefficients since the control point force is given by the product of lifting pressure and box area, and the normalwash is the substantial derivative in the streamwise direction of the deflection. (The substantial derivative requires curve fitting "in-the-small" along the surface strip; e.g., a parabola may be passed through the control point and the points upstream and downstream of it.) If a reduced number of degrees of freedom is desired for the aeroelastic analysis over the number of boxes employed in the aerodynamic analysis, the number of control point forces and deflections may be reduced by a streamwise curve fit and the method of virtual work as discussed in Ref. 20.

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Aerodynamic Shattering of Liquid Drops

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New experimental and analytical results are reported for the problem of liquid drop shattering. Breakup is observed to occur as a result of the interaction between a drop and the convective flowfield established by the passage of a shock wave over it. The purpose of this investigation, which supplements and extends previous experimental and theoretical studies, is to establish the influence of various parameters on the rate of disintegration and on the time required for breakup to occur. Photographic, drop displacement, and break-up time information is presented for a range of conditions which involve shock waves moving at Mach numbers $M_s = 1.5-3.5$ in air over water drops having diameters of $750-4000\mu$. A model is formulated for the breakup phenomenon by considering that it results from a boundary-layer stripping mechanism. The experimental determination of the variation of drop shape and of drop velocity with time is used together with the analytical results to compute the disintegration rate.

Nomenclature

A	= dimensionless interface velocity
a	= drop acceleration (dW/dt)
C_D	= drag coefficient
D	= drop diameter
M, m	= droplet mass
M_s	= shock Mach number
P, p	= static pressure
q	= dynamic pressure
R	= drop radius
Re	= Reynolds number
S	= drop frontal area ($\pi D^2/4$)
t	= time after collision
\bar{T}	= dimensionless time [$t(U_2/D_0)(\beta)^{1/2}$]
U	= fluid velocity
u	= boundary-layer velocity
W	= drop velocity
x	= drop displacement
\bar{X}	= dimensionless displacement (x/D_0)
α	= boundary-layer shape factor
β	= gas-to-liquid density ratio (ρ_g/ρ_l)
μ	= fluid viscosity (also implies micro and micron)

ν	= kinematic viscosity
ρ	= fluid density

Subscripts

1	= initial conditions
2	= shock conditions
b	= breakup
g	= gas
l	= liquid
0	= $t = 0$
r	= relative velocity
∞	= freestream velocity

I. Introduction

THE fragmentation of liquid drops, resulting from their sudden exposure to a high-velocity gas stream, has many important applications in the fields of aerodynamics and propulsion. For example, the phenomenon of supersonic rain erosion, which is caused by the impingement of rain droplets at high relative speeds on exterior missile and aircraft surfaces, can be greatly alleviated through proper aerodynamic design. A reduction in the damage sustained from impacting drops is achieved by designing a body whose detached shock is sufficiently far removed to allow for drop shattering in the region separating the shock from the body surface. With regard to propulsion, the rate of mixing and combustion of liquid fuel droplets can be greatly enhanced by virtue of the fragmentation process. As a result of droplet breakup, burning rates are obtainable which are higher than

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