

UNIVERSITY OF TÜBINGEN

Thermionic Emission

BLOCKPRAKTIKUM 2021

First English Version

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1 Introduction

In this experiment we analyse the behavior of a glowing diode emitting electrons which is the so called thermionic emission. At first we start with the theoretical fundamentals by describing the problem with the laws of physics. Then we hand over by describing the experiment and it's implementation. Further we evaluate our measurements and present our result.

2 Theoretical Fundamentals

A part of the electrons in the reverse-bias domain have enough energy to overcome the work function potential and aswell the small reverse bias voltage

$$U_{AK} = \varphi_A - \varphi_K = -U_G(\varphi_A, \varphi_K) \quad (1)$$

where φ_K is the cathode potential and φ_A is the anode potential. ($U_G > 0$) The starting current is given by

$$I_A(U_G, T) = I_S(T) \cdot \exp\left(-\frac{eU_G}{k_B T}\right) \quad (2)$$

where $I_S(T) = I_A(0, T)$ is the saturation current, e the elementary charge, k_B the Boltzmann-constant, T cathode temperature. Due to Sommerfeld and Nordheim we have an expression of the saturation current in dependence of the cathode temperature T and the cathode work function W_K . Without an external field it yields to

$$I_S(T) = A_0 F T^2 \exp\left(-\frac{W_K}{k_B T}\right) \quad (3)$$

with a constant A_0 and the surface area of the cathode F . The tube in the experiment has the radii ratio of anode radii and cathode radii $\frac{R}{r} \approx 1,5$, which is important for the homogeneous surface with temperature independent work function. It guarantees us the validity of equation (3). For cathodes which are not fulfilling this condition, it is possible to calculate with the Richardson-equation

$$I_S(T) = A_R F T^2 \exp\left(-\frac{W_K}{k_B T}\right) \quad (4)$$

When we are taking the natural logarithm of I_A and also plotting this versus U_G , it is possible to calculate the cathode temperature out of the slope of the resulting line. But the applied reverse voltage needs to be corrected cause of two effects. First, the space charge between cathode and anode forms a potential barrier in the near of the

cathode. Second, the difference between the work functions of cathode and anode is resulting in a contact voltage between cathode and anode.

For small current densities is the spacecharge minor and can be neglected. The effective reverse bias voltage is in due consideration of the contact potential given by

$$U_{AK}^{\text{eff}} = -U_G + \frac{1}{e}(W_K - W_A) \quad (5)$$

with the work functions of cathode W_K and anode W_A . With this we obtain then

$$I_A(U_G, T) = A_0 F T^2 \exp\left(-\frac{W_A + eU_G}{k_B T}\right) \quad (6)$$

When the influence of the cathode temperature T on the work function W_A is minor, it is then possible to calculate T out of (6). For the anode work function W_A we find

$$W_A = k_B T \cdot \ln\left(\frac{A_0 F T^2}{I_A(0, T)}\right) \quad (7)$$

The calculation of the cathode work function is in our case redundant.

3 Experiment Execution

The experimental setup is clarified by following picture.

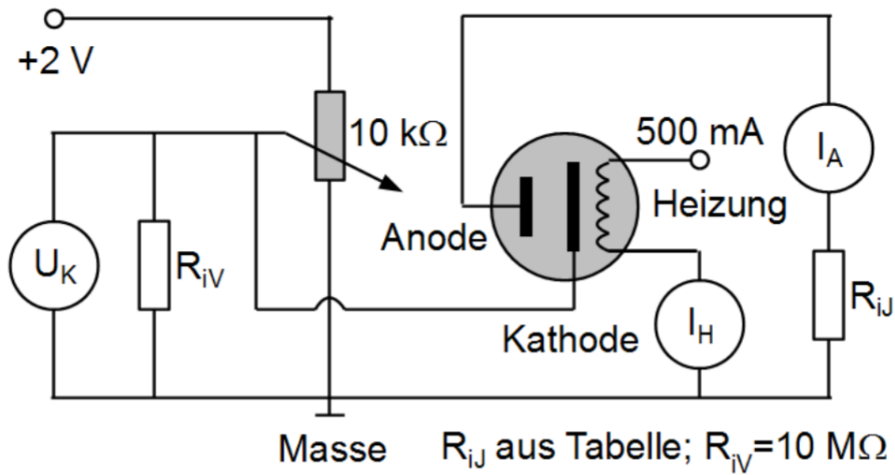


Abbildung TE.2: Schematic of the measurement setup. (Heizung = heating).

Figure 1: circuit design for our experiment from the instructions

We build this setup and let it check from the assistant. Then we measured for different heating currents ($I_H = 450, 500, 550 \text{ mA}$) the measurement series $I_A = I_A(U_G)$. Further

we increased the reverse bias Voltage from 0V in 20 equidistant steps until we measured a starting current $I_A \leq 2\text{nA}$. Each time we measured the starting current I_A we also note the measurement range of the digital multimeter. This is important for the evaluation of our measurements. The dependence of the internal resistance of our measuring device from the measurement range is depicted in the following table.

measurement range	intenal resistance
1A	0,1 Ω
100mA	0,1 Ω
10mA	1 Ω
1mA	10 Ω
100 μA	100 Ω
10 μA	1k Ω
1 μA	10k Ω
100nA	100k Ω

Figure 2: internal resistance for each measurement range; source: instruction paper of this experiment

4 Analysis of the measurement results

We determined the dependence of the starting current I_A from the reverse bias voltage for three different heating currents.

U_{tot} in V	0	0.098	0.2	0.3	0.398	0.5	0.599	0.65	0.7	0.751
I_A in A	142	147	120	116	84	62.5	34.9	24.1	15.5	8.4
m. r.	1mA	1mA	1mA	1mA	1mA	100 μ A	100 μ A	100 μ A	100 μ A	10 μ A

U_{tot} in V	0.801	0.85	0.901	0.951	1.001	1.05	1.098	1.149	1.199	1.25	1.349	1.4
I_A in A	5.15	2.94	1.66	0.845	0.498	0.276	0.159	0.0939	0.049	0.027	0.0053	0.0011
m. r.	10 μ A	10 μ A	10 μ A	1 μ A	1 μ A	1 μ A	1 μ A	1 μ A	1 μ A	100nA	100nA	100nA

Table 1: measurement with $I_H = 450 \text{ mA}$ heating current (m.r. stands for the used measurement range)

U_{tot} in V	0	0.065	0.131	0.194	0.259	0.324	0.39	0.454	0.521	0.585
I_A in A	361	286	221	162.9	109.8	68.5	40.3	22.9	12.36	6.61
m. r.	1mA	1mA	1mA	100 μ A	100 μ A	100 μ A	100 μ A	100 μ A	10 μ A	10 μ A

U_{tot} in V	0.65	0.714	0.77	0.786	0.845	0.91	0.974	1.04	1.102	1.165
I_A in A	3.35	1.69	0.9	0.759	0.389	0.184	0.087	0.0405	0.0194	0.0094
m. r.	10 μ A	1 μ A	1 μ A	1 μ A	1 μ A	100nA	100nA	100nA	100nA	100nA

U_{tot} in V	1.23	1.294
I_A in A	0.0042	0.0018
m. r.	100nA	100nA

Table 2: measurement data with a heating current of $I_H = 500 \text{ mA}$

U_{tot} in V	0	0.101	0.201	0.301	0.402	0.5	0.599	0.701	0.8	0.9
I_A in μA	1250	1080	896	748	609	481	362	253	161	82.2
m. r.	10mA	10mA	1mA	1mA	1mA	1mA	1mA	1mA	1mA	100 μ A

U_{tot} in V	1.001	1.101	1.2	1.299	1.399	1.499	1.6	1.65	1.701	1.75	1.801
I_A in μA	36.1	13.7	4.71	1.72	0.575	0.0207	0.0743	0.0404	0.0212	0.0085	0.0012
m. r.	100 μ A	100 μ A	10 μ A	10 μ A	1 μ A	1 μ A	100nA	100nA	100nA	100nA	100nA

Table 3: measurement data from the heating with $I_H = 550 \text{ mA}$

In Order to use the right Voltage U_G we have to take into consideration, that the voltage, we measured, (U_{tot}) was the voltage, which was applied to both, cathode and

anode as well as our measuring device for the starting current. It holds

$$U_{\text{tot}} = U_G + U_{\text{MC}} = I (R_G + R_{\text{MC}}),$$

where $I = I_A$ and the index MC denotes the current measuring device. Thus we get our real U_G by applying the correction

$$U_G = U_{\text{tot}} - I_A \cdot R_{\text{MC}}$$

After doing this we can now evaluate our data further. From Equation (6) we can derive the following expression by taking the logarithm.

$$\ln(I_A) = -\frac{e}{k_B T} U_G + \ln(A_0 F T^2) - \frac{W_A}{k_B T}$$

From this we can determine the temperature of the heating diode by fitting a linear regression to our data, what was done in the following.

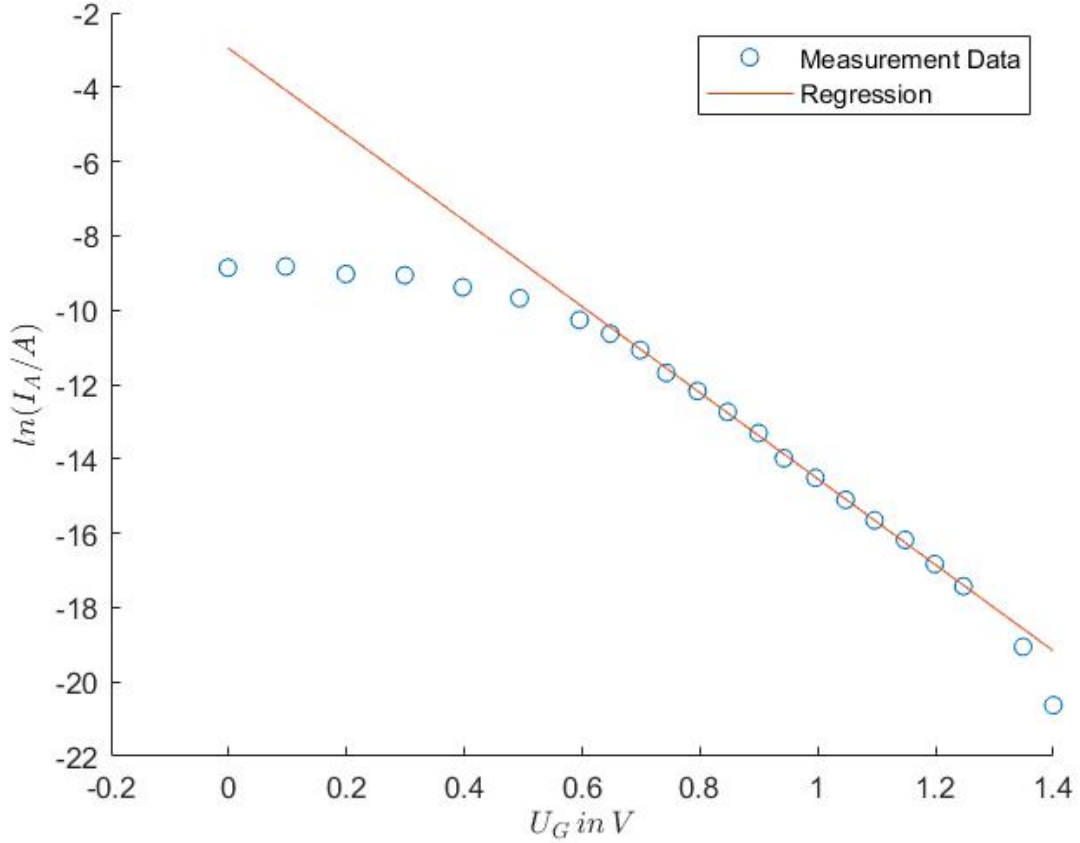


Figure 3: experiment data with regression in an appropriate part with heating of $I_H = 450 \text{ mA}$

We approximated a function of the form $\ln(I_A) = m \cdot U_G + b$, where m was determined to

$$m = -11.5769 \pm 0.1198 \text{ (stat.)} \pm 0.0179 \text{ (sys.)}$$

$$b = -2.9619 \pm 0.1236 \text{ (stat.)} \pm 0.0153 \text{ (sys.)}.$$

The calculated temperature of this result is

$$T = 1.0024 \cdot 10^3 \pm 10.3739 \text{ (stat.)} \pm 1.5519 \text{ (sys.) K.}$$

For the next heating current we proceeded the same way.

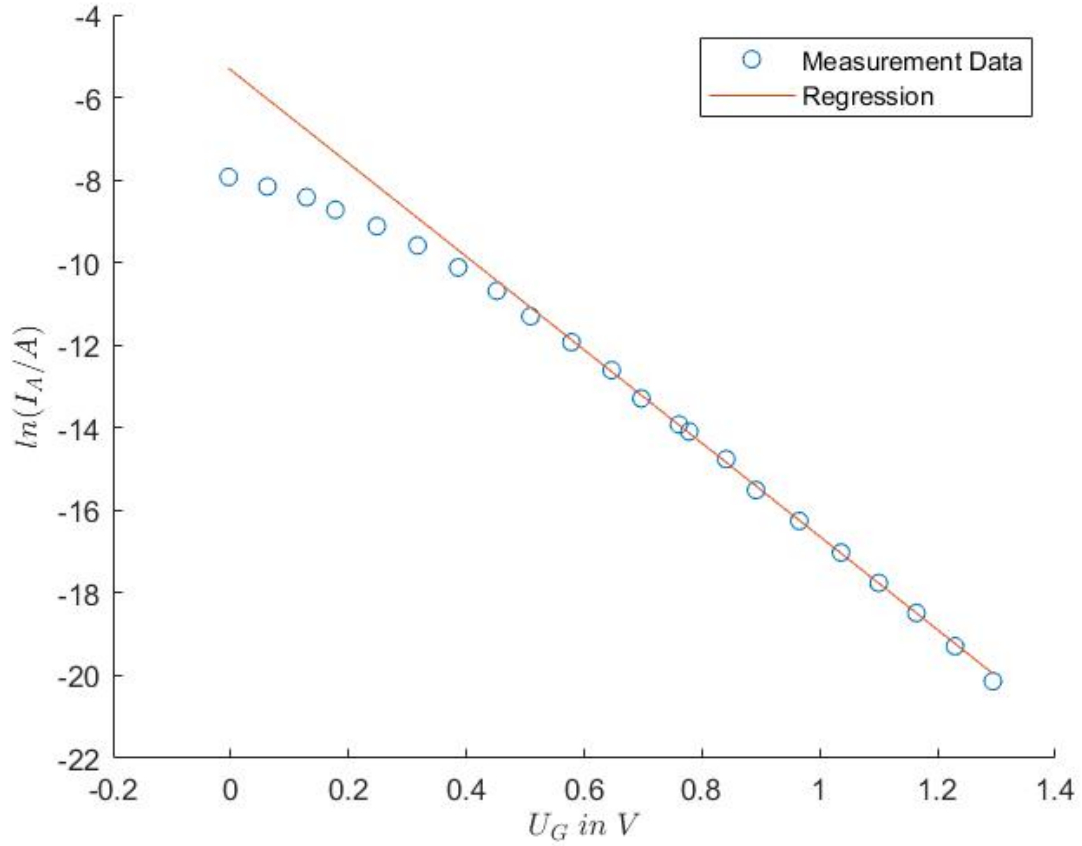


Figure 4: experiment data with regression in an appropriate part with heating of $I_H = 500 \text{ mA}$

Out of the regression of the form $\ln(I_A) = m \cdot U_G + b$ with

$$m = -11.2951 \pm 0.1087 \text{ (stat.)} \pm 0.0214 \text{ (sys.)}$$

$$b = -5.3383 \pm 0.0982 \text{ (stat.)} \pm 0.0127 \text{ (sys.)}$$

we calculated the temperature of the heating diode as

$$T = 1027.38 \pm 9.88 \text{ (stat.)} \pm 1.95 \text{ (sys.) } K.$$

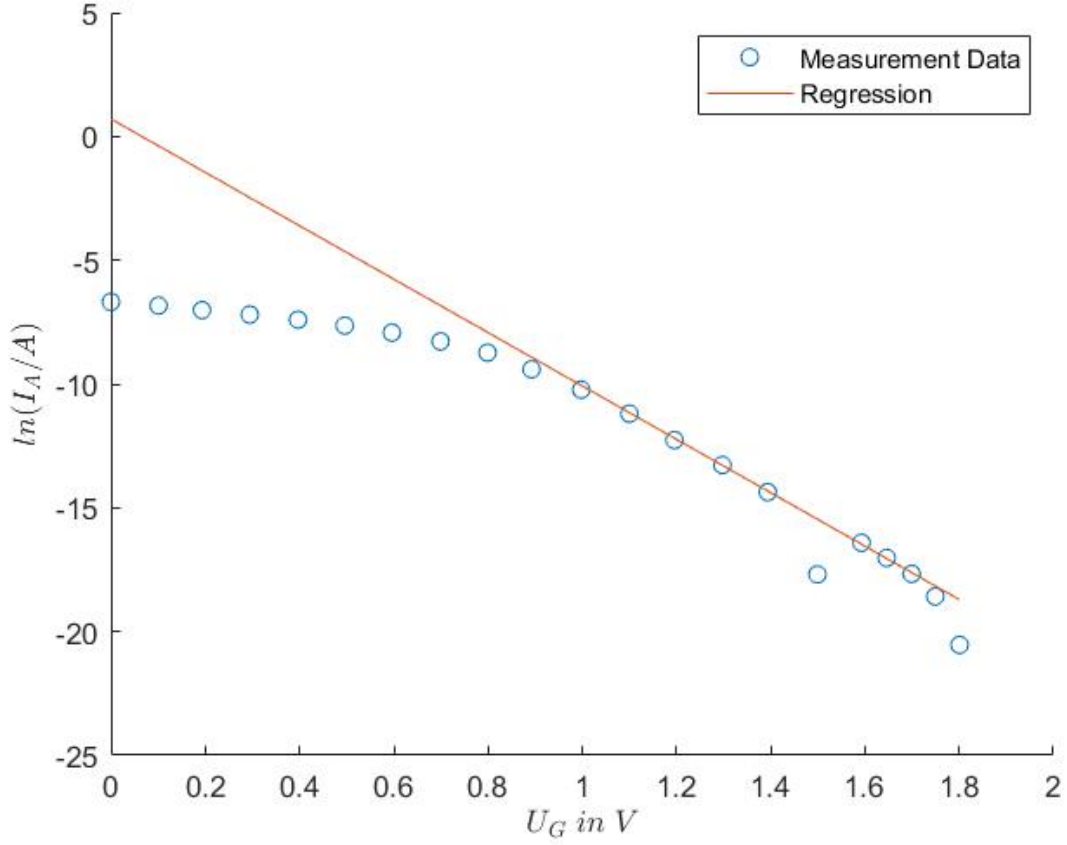


Figure 5: experiment data with regression in an appropriate part with heating of $I_H = 550 \text{ mA}$

With the same calculation as before we calculated from the regression $\ln(I_A) = m \cdot U_G + b$ with

$$m = -10.7785 \pm 0.1564 \text{ (stat.)} \pm 0.0101 \text{ (sys.)}$$

$$b = 0.6933 \pm 0.2399 \text{ (stat.)} \pm 0.0158 \text{ (sys.)}$$

the temperature of the heating diode as

$$T = 1076.64 \pm 15.63 \text{ (stat.)} \pm 1.00 \text{ (sys.) } K.$$

In the next step we want to determine the anode work function W_A from the equation

$$W_A = k_B T \ln \left(\frac{A_0 F T^2}{I_A(0, T)} \right).$$

The constants are given as $A_0 = 0.1 \frac{A}{cm^2 K^2}$; $F = 1.26 cm^2$. For $I_A(0, T)$ we take the y-axis intercept b , because our model, from which we get this formula, demands a linear course and doesn't account the effects, that lead to the deviation of the linear course. Thus we use $I_A(0, T) = \exp(b)$.

From this we get the result for the anode escape work from our first execution of the experiment with a heating current of $I_H = 450 mA$

$$W_{A,1} = 1.2707 \pm 0.0175 \text{ (stat.)} \pm 0.0034 \text{ (sys.) } eV$$

From a heating current of $I_H = 500 mA$ we get

$$W_{A,2} = 1.5172 \pm 0.017 \text{ (stat.)} \pm 0.004 \text{ (sys.) } eV$$

and from a heating current of $I_H = 550 mA$ we get

$$W_{A,3} = 1.0390 \pm 0.0620 \text{ (stat.)} \pm 0.0052 \text{ (sys.) } eV.$$

We calculated the statistical deviation always according to Gauß' law of error propagation

$$\Delta f(x_1, \dots, x_n)_{\text{stat}} = \sqrt{\sum_{i=1}^n \left(\frac{\partial f}{\partial x_i}(x_1, \dots, x_n) \cdot \Delta x_i \right)^2}$$

and the executed the systematic error propagation over

$$\Delta f(x_1, \dots, x_n)_{\text{sys}} = \sum_{i=1}^n \left| \frac{\partial f}{\partial x_i}(x_1, \dots, x_n) \cdot \Delta x_i \right|$$

As it can be seen in our results, the anode escape work is not constant, but depends slightly on the temperature of the heating diode.

At this point I want to calculate, which degree of emission efficiency a diode of two different materials can get at a distinct emission current. The emitting diode shall deliver an emission current density of $j_S = 0.5 \frac{A}{cm^2}$. We consider two different cathode materials. At the one hand an tungsten cathode with the values $A_R = 60 \frac{A}{cm^2 K^2}$, $W_K = 4.53 eV$, and at other hand an oxide cathode with parameters $A_R = 0.046 \frac{A}{cm^2 K^2}$, $W_K = 1.2 eV$. In order to get the needed temperature for a current density of $j_S = 0.5 \frac{A}{cm^2}$, I solved the equation

$$j_S = A_R T^2 e^{-\frac{W_K}{k_B T}}$$

numerically and obtained the values

$$T_t = 2565.8 K$$

$$T_o = 1183.5 K$$

The power, which is applied by the diode can be calculated, according to the Stefan-Boltzmann law with emissivities $\epsilon_t = 0.29$ and $\epsilon_o = 0.19$

$$\frac{P_H}{F} = \sigma \epsilon T^4$$

where F is the surface of the cathode. We obtain

$$\frac{P_{H,t}}{F} = 71.276 \frac{W}{cm^2}$$

$$\frac{P_{H,o}}{F} = 2.114 \frac{W}{cm^2}$$

This results in a emission efficiency of

$$\eta_t = \frac{I_{S,t}}{P_{H,t}} = \frac{j_{S,t}}{P_{H,t}/F} = 0.007 \frac{1}{V}$$

$$\eta_o = 0.237 \frac{1}{V}$$

It becomes clear that the oxide cathode is much more efficient than the tungsten one.

4.1 Schottky-Effect

At the end of our Analysis I want to make a quick digression and explain the Schottky-Effect. A electron outside a metal experiences an attractive force from this metal due to electric influence. This can be described by a mirroring charge. The force on this electron in distance r is expressed by

$$F(r) = -\frac{e^2}{4\pi\epsilon_0 (2r)^2}$$

In order to obtain the work, that has to be performed to remove an electron from the metal, we have to integrate this force after following rule

$$W = - \int_0^\infty F \, dr$$

The electrons already got an energy in the metal due to Pauli's principle, the Fermi energy. Therefore they don't have to muster the whole escape work i.e. from thermal energy. To account this fact I start the integration from particular point R_F , which depends on the Fermi energy, and is therefore material dependent.

$$W = - \int_{R_F}^\infty F \, dr$$

When in this situation an additional constant electric field is applied, which supports the escaping movement of the electron by its polarization, then the force turns at some point r_0 from an attractive to a repulsive force. The potential has a maximum at this point and the work, which brings the electron to this point, has to be performed in order to remove the electron from the metal. To determine the position of r_0 we solve the equation

$$0 = -\frac{e^2}{16\pi\epsilon_0 r_0^2} - e E$$

We find

$$r_0 = \sqrt{-\frac{e}{16\pi\epsilon_0 E}}$$

We also see that the sign of the electric field has to be negative in order to be able to notice this effect. Further we can say, that the larger the electric field is the closer comes the maximum of the potential to the surface of the metal. We notice a difference in the escape work of the electron with this additional electric field in form of

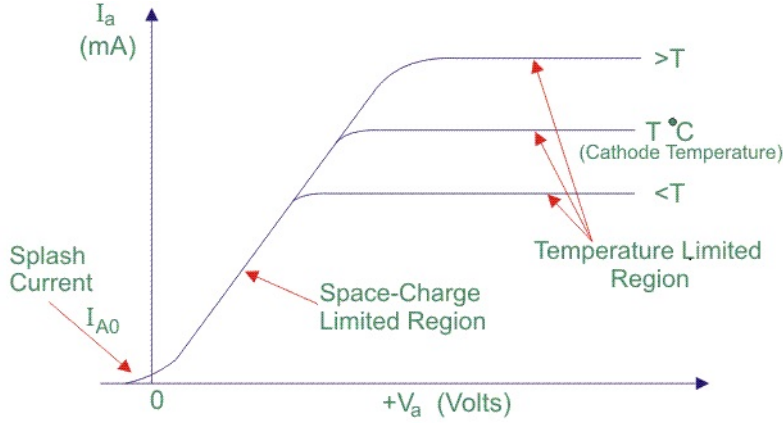
$$\begin{aligned} \Delta W &= - \int_0^\infty F(r, E=0) \, dr + \int_0^{r_0} F(r, E) \, dr \\ &= - \int_{r_0}^\infty \frac{e^2}{16\pi\epsilon_0 r^2} \, dr - \int_0^{r_0} e E \, dr \\ &= \frac{e^2}{16\pi\epsilon_0 r_0} - e E r_0 \\ &= \sqrt{\frac{-E e^3}{4\pi\epsilon_0}} \end{aligned}$$

Having dealt with this phenomena we can now predict, that when the reverse bias voltage changes it's sign and supports the escape movement, the emission current raises. Thus the thermionic emission shows a dependence from the applied voltage in the form of

$$I_A = A_0 F T^2 e^{-\frac{W_K - \Delta W}{k_B T}}$$

$$= A_0 F T^2 \exp \left(-\frac{1}{k_B T} \left(W_K - \sqrt{\frac{U e^2}{4\pi\epsilon_0 d}} \right) \right),$$

where we used $-eE = U/d$, d is the distance between cathode and anode. The course of the characteristic curve of a thermionic diode is shown in the following picture



I-V Characteristics of Vacuum Diode under forward bias

Figure 6: characteristic curve of thermionic emission

5 Conclusion

Finally it can be said, that the result for the escape work was in the right order of magnitude and therefore quite good. The temperature dependence of the work can be explained among others by the mistake of the used model, which didn't account the influence of the space charge density at all, arising when charges leave the metal. This effect is especially notable at low reverse bias voltage and explains the deviation of our measurement data from the linear course in the $U_b - \ln(I_A)$ diagram at low voltages. We can also understand now the course of emission current, when the reverse bias voltage changes it's sign, which can be explained by the Schottky-Effect in combination with the space charge density. At even higher voltages the emission current get into saturation. Through this experiment we achieved a greater understanding of the physics of thermionic emission and even understood, why in old television devices oxide cathode diodes were used, because of it's high efficiency.