

Review of  
SEMICONDUCTOR DEVICES

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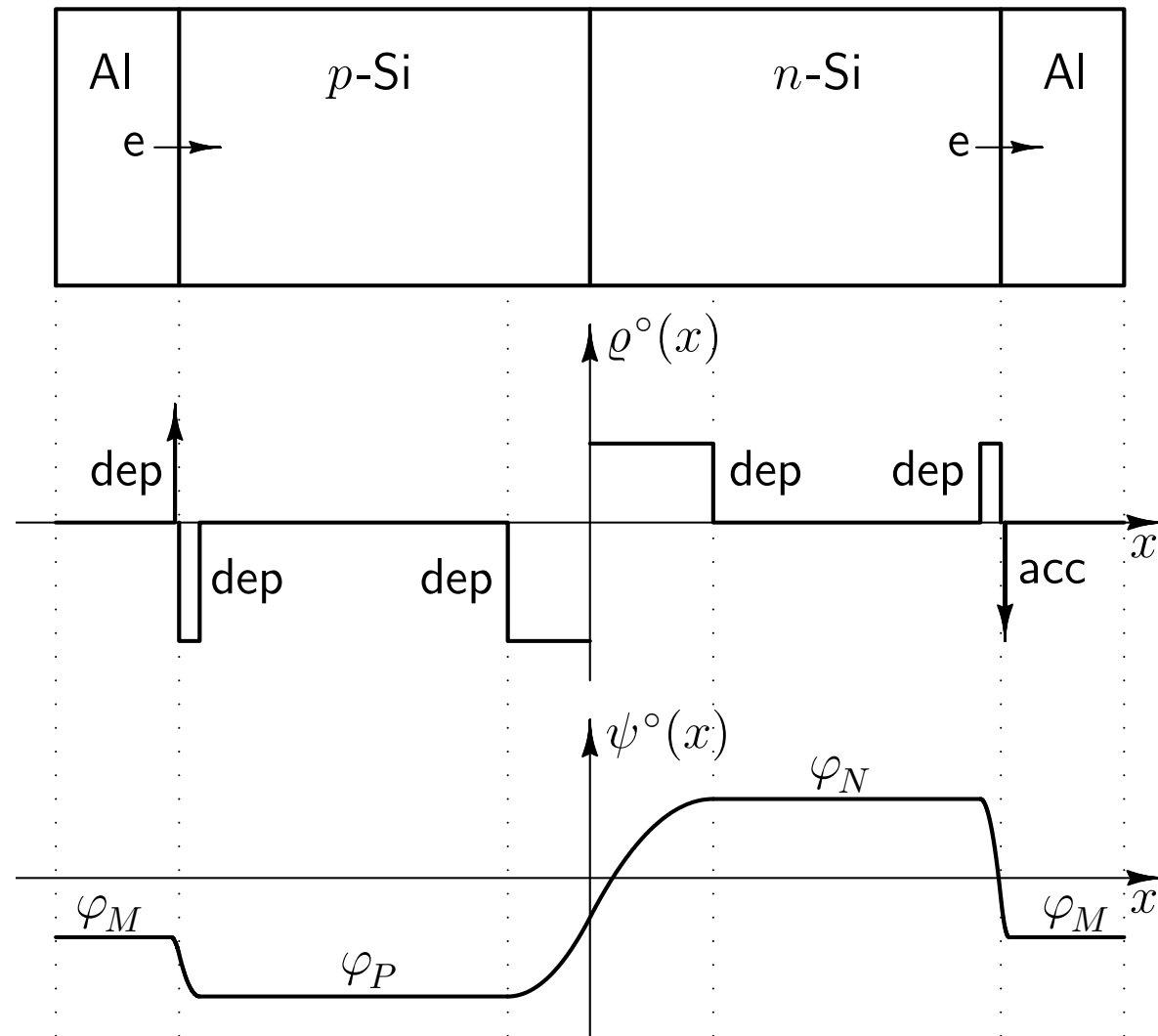
## FORMATION OF THE DEPLETION REGION IN PN-JUNCTION DIODES

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- The depletion region is formed because holes from the  $p$ -side diffuse to the  $n$ -side where they recombine with electrons, and electrons from the  $n$ -side diffuse to the  $p$ -side where they recombine with holes.
- The concentrations of electrons and holes in the depletion region are much smaller than  $N_a$  in the  $p$ -side and  $N_d$  in the  $n$ -side.
- In the depletion region, there is a built-in electric field and non-zero carrier-concentration gradients:
  - Hole diffusion  $\rightarrow$  is cancelled by hole drift  $\leftarrow$ , and
  - Electron diffusion  $\leftarrow$  is cancelled by electron drift  $\rightarrow$ .
- The net recombination or generation rate distributions are zero the depletion region and the quasi neutral regions.
- Charge conservation requires that

$$N_a^- W_{d,P}^\circ = N_d^+ W_{d,N}^\circ .$$

# PN-JUNCTION DIODE AT THERMAL EQUILIBRIUM



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# PN-JUNCTION DIODE AT THERMAL EQUILIBRIUM

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- The built-in potential  $V_{bi}$  is given by

$$V_{bi} = \frac{k_B T}{q} \ln \left( \frac{N_a^- N_d^+}{n_i^2} \right) .$$

- The depletion-region width  $W_d^\circ$  at thermal equilibrium is given by

$$W_d^\circ = \sqrt{\frac{2 \epsilon_{Si}}{q} \cdot \frac{(N_a^- + N_d^+)}{N_a^- N_d^+} V_{bi}} .$$

# PN-JUNCTION DIODE AT THERMAL EQUILIBRIUM

- The  $p$ -side depletion-region width  $W_{d,P}^{\circ}$  at thermal equilibrium is

$$W_{d,P}^{\circ} = \frac{N_d^{+}}{(N_a^{-} + N_d^{+})} W_d^{\circ} = \sqrt{\frac{2 \epsilon_{Si}}{q} \cdot \frac{N_d^{+}}{N_a^{-} (N_a^{-} + N_d^{+})} V_{bi}} .$$

- The  $n$ -side depletion-region width  $W_{d,N}^{\circ}$  at thermal equilibrium is

$$W_{d,N}^{\circ} = \frac{N_a^{-}}{(N_a^{-} + N_d^{+})} W_d^{\circ} = \sqrt{\frac{2 \epsilon_{Si}}{q} \cdot \frac{N_a^{-}}{N_d^{+} (N_a^{-} + N_d^{+})} V_{bi}} .$$

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## BIAS-VOLTAGE EFFECTS IN A PN-JUNCTION DIODE

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- For  $V_{PN} > 0$ :
  - $W_d(V_{PN}) \downarrow$ ,
  - The barrier becomes  $(V_{bi} - V_{PN}) \downarrow$ ,
  - The magnitude of the field in the depletion region  $\downarrow$ , and
  - The depletion-region carrier gradients  $dp/dx \uparrow$  and  $dn/dx \uparrow$ .
- For  $V_{PN} < 0$ :
  - $W_d(V_{PN}) \uparrow$ ,
  - The barrier becomes  $(V_{bi} - V_{PN}) \uparrow$ ,
  - The magnitude of the field in the depletion region  $\uparrow$ , and
  - The depletion-region carrier gradients  $dp/dx \downarrow$  and  $dn/dx \downarrow$ .

## BIAS-VOLTAGE EFFECTS IN A PN-JUNCTION DIODE

- The width of the depletion region  $W_d(V_{PN})$  is given by

$$W_d(V_{PN}) = \sqrt{\frac{2 \epsilon_{Si}}{q} \cdot \frac{(N_a^- + N_d^+)}{N_a^- N_d^+} (V_{bi} - V_{PN})}.$$

- The  $p$ -side depletion-region width is

$$W_{d,P}(V_{PN}) = \sqrt{\frac{2 \epsilon_{Si}}{q} \cdot \frac{N_d^+}{N_a^- (N_a^- + N_d^+)} (V_{bi} - V_{PN})}.$$

- The  $n$ -side depletion-region width is

$$W_{d,N}(V_{PN}) = \sqrt{\frac{2 \epsilon_{Si}}{q} \cdot \frac{N_a^-}{N_d^+ (N_a^- + N_d^+)} (V_{bi} - V_{PN})}.$$

## BIAS-VOLTAGE EFFECTS IN A PN-JUNCTION DIODE

- The field at  $x = 0$  is given by

$$\begin{aligned}\mathcal{E}_{x \cdot max}(V_{PN}) &\equiv \mathcal{E}_x(0, V_{PN}), \\ &= - \frac{q N_a^- W_{d,P}(V_{PN})}{\epsilon_{Si}} = - \frac{q N_d^+ W_{d,N}(V_{PN})}{\epsilon_{Si}}, \\ &= - \sqrt{\frac{2q}{\epsilon_{Si}} \cdot \frac{N_a^- N_d^+}{(N_a^- + N_d^+)} (V_{bi} - V_{PN})}.\end{aligned}$$



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## BIAS-VOLTAGE EFFECTS IN A PN-JUNCTION DIODE

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- The minority-carrier concentrations at the depletion-region edges under bias conditions are given by

$$p_N(W_{d,N}, V_{PN}) = p_N^{\circ} \exp \left( \frac{q V_{PN}}{k_B T} \right) ,$$

and

$$n_P(-W_{d,P}, V_{PN}) = n_P^{\circ} \exp \left( \frac{q V_{PN}}{k_B T} \right) .$$

These important relationships are called the **law of the junction**.

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## BIAS-VOLTAGE EFFECTS IN A PN-JUNCTION DIODE

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- Under forward-bias static conditions, holes are transported in the positive  $x$  direction by drift and diffusion in the  $p$ -side quasi-neutral region where they also recombine with electrons injected from the  $n$ -side of the junction.
- Holes and electrons recombine throughout the depletion region. Under the assumption of a uniform net recombination rate throughout this region, the hole current density decreases linearly from the  $p$ -side depletion-region edge to the  $n$ -side depletion-region edge.
- Holes are transported in the positive  $x$  direction mainly by diffusion in the  $n$ -side quasi-neutral region where they also recombine with the majority electrons.

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## STATIC $I_D(V_{PN})$ CHARACTERISTICS

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- Under forward-bias static conditions, electrons are transported in the negative  $x$  direction by drift and diffusion in the  $n$ -side quasi-neutral region where they also recombine with holes injected from the  $p$ -side of the junction.
- Electrons and holes recombine throughout the depletion region. Under the assumption of a uniform net recombination rate throughout this region, the electron current density decreases linearly from the  $n$ -side depletion-region edge to the  $p$ -side depletion-region edge.
- Electrons are transported in the negative  $x$  direction mainly by diffusion in the  $p$ -side quasi-neutral region where they also recombine with the majority holes.

## STATIC $I_D(V_{PN})$ CHARACTERISTICS

- The PN-junction diode current density is then given by

$$J_D(V_{PN}) = J_{S.diff} \left[ \exp \left( \frac{q V_{PN}}{k_B T} \right) - 1 \right] + J_{S.scr}(V_{PN}) \left[ \exp \left( \frac{q V_{PN}}{2 k_B T} \right) - 1 \right],$$

where

$$J_{S.diff} = \frac{q D_{n,P} n_i^2}{L_{n,P} N_a^-} + \frac{q D_{p,N} n_i^2}{L_{p,N} N_d^+},$$

$$J_{S.scr}(V_{PN}) = \frac{q n_i W_d(V_{PN})}{2 \tau_{rec,SCR}},$$

and

$$\tau_{rec,SCR} \approx \frac{\tau_{rec,P} + \tau_{rec,N}}{2}.$$

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## STATIC $I_D(V_{PN})$ CHARACTERISTICS

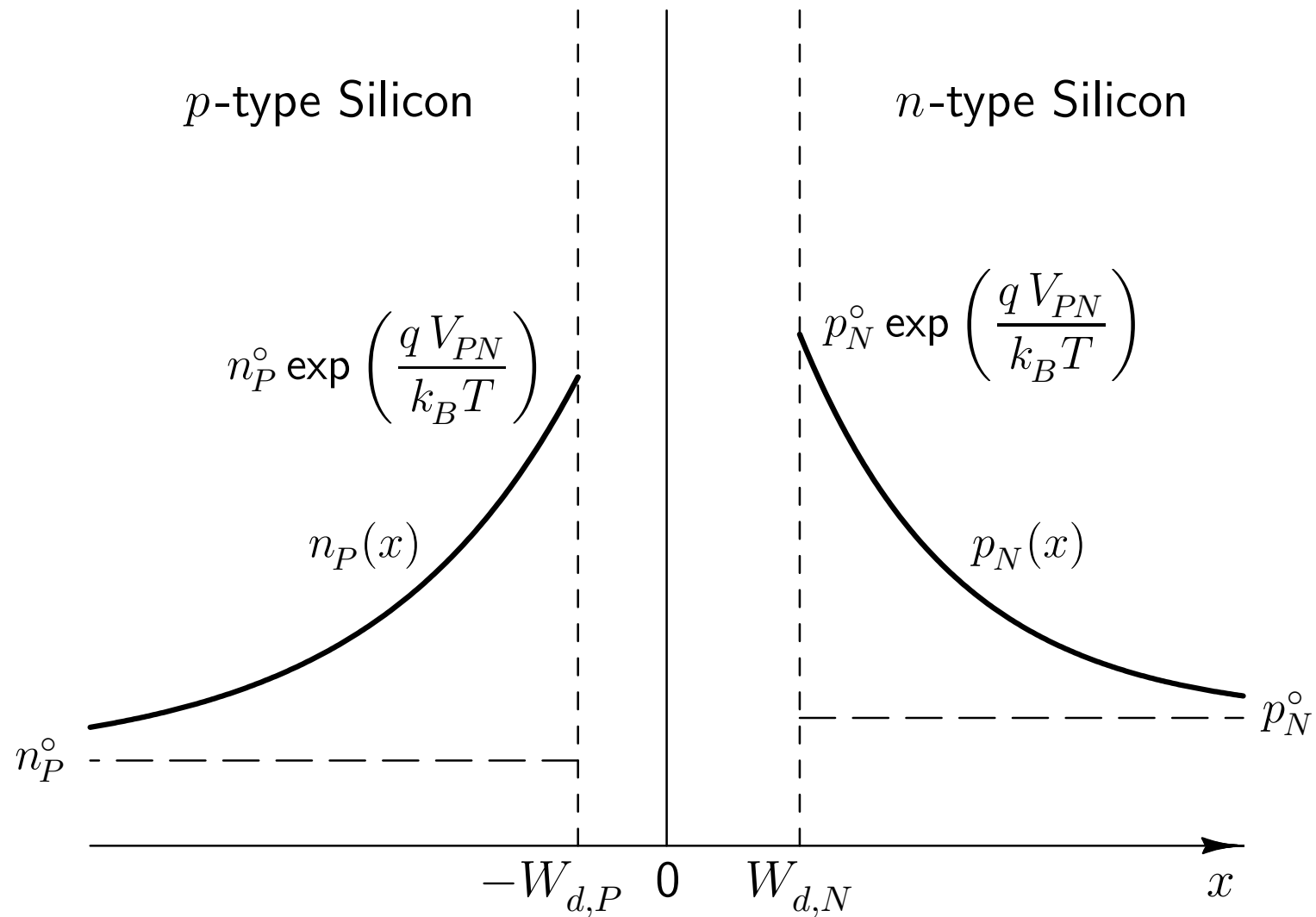
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- The PN-junction diode current  $I_D(V_{PN})$  is then given by

$$\begin{aligned} I_D(V_{PN}) &= A_d J_D(V_{PN}) , \\ &= I_{S.diff} \left[ \exp \left( \frac{q V_{PN}}{k_B T} \right) - 1 \right] + I_{S.scr}(V_{PN}) \left[ \exp \left( \frac{q V_{PN}}{2 k_B T} \right) - 1 \right] , \end{aligned}$$

where  $A_d$  is the diode area.

# STATIC $I_D(V_{PN})$ CHARACTERISTICS



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## STATIC $I_D(V_{PN})$ CHARACTERISTICS

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- When the applied bias voltage  $V_{PN}$  is negative, the PN-junction diode is reverse-biased. Under such conditions
  - $W_d(V_{PN}) \uparrow$ ,
  - $|\mathcal{E}_x| \uparrow$  in the depletion region,
  - $(V_{bi} - V_{PN}) \uparrow$  across the junction because  $V_{PN} < 0$ ,
  - $p_N(W_{d,N}) \downarrow < p_N^\circ$  because  $V_{PN} < 0$  and  $\exp(qV_{PN}/k_B T) < 1$ ,
  - Holes in the  $n$ -side quasi-neutral region diffuse towards the junction,
  - $n_P(-W_{d,P}) \downarrow < n_P^\circ$  because  $V_{PN} < 0$  and  $\exp(qV_{PN}/k_B T) < 1$ ,
  - Electrons in the  $p$ -side quasi-neutral region diffuse towards the junction, and
  - There is net electron-hole-pair generation throughout the diode.

## STATIC $I_D(V_{PN})$ CHARACTERISTICS

- The minority-carrier lifetimes and diffusion lengths used in calculating the carrier-concentration distributions are minority-carrier generation lifetimes and diffusion lengths. In other words:

$$\tau_{rec \cdot p, N} \longrightarrow \tau_{gen \cdot p, N} ,$$

$$L_{p, N} = \sqrt{\tau_{rec \cdot p, N} D_{p, N}} \longrightarrow L_{p, N} = \sqrt{\tau_{gen \cdot p, N} D_{p, N}} ,$$

$$\tau_{rec \cdot n, P} \longrightarrow \tau_{gen \cdot n, P} ,$$

$$L_{n, P} = \sqrt{\tau_{rec \cdot n, P} D_{n, P}} \longrightarrow L_{n, P} = \sqrt{\tau_{gen \cdot n, P} D_{n, P}} ,$$

$$\tau_{rec, SCR} \longrightarrow \tau_{gen, SCR} .$$



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## STATIC $I_D(V_{PN})$ CHARACTERISTICS

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- Holes generated in the  $n$ -side quasi-neutral region diffuse towards the depletion region where they join holes generated there. These holes are swept by the electric field in the depletion region towards the  $p$ -side depletion-region edge. More holes are generated in the  $p$ -side quasi-neutral region, and all holes are transported there by drift and diffusion towards the metal contact at  $x = -W_P$ , and
- Electrons generated in the  $p$ -side quasi-neutral region diffuse towards the depletion region where they join electrons generated there. These electrons are swept by the electric field in the depletion region towards the  $n$ -side depletion-region edge. More electrons are generated in the  $n$ -side quasi-neutral region, and all electrons are transported there by drift and diffusion towards the metal contact at  $x = W_N$ .

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## STATIC $I_D(V_{PN})$ CHARACTERISTICS

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- Under reverse-bias conditions, the space-charge-generation current density is given by

$$J_{D.scg}(V_{PN}) = \frac{q n_i W_d(V_{PN})}{2 \tau_{gen,SCR}} \left[ \exp \left( \frac{q V_{PN}}{2 k_B T} \right) - 1 \right] ,$$
$$\approx - \frac{q n_i W_d(V_{PN})}{2 \tau_{gen,SCR}} \quad \text{for } V_{PN} \leq -6 k_B T / q .$$

It is evident that the reverse-bias space-charge-generation current density has a weak bias-voltage dependence.

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## REVERSE-BIAS BREAKDOWN IN A PN-JUNCTION DIODE

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- At large enough reverse-bias voltages, the reverse-bias diode current  $I_D$  increases substantially due to **avalanche multiplication**, a process that results directly from carrier impact ionization.
- Breakdown can also occur due to carrier tunneling at low bias voltages in heavily doped PN-junction diodes. As the dopant concentrations in both sides of a PN-junction diode are increased, the depletion width decreases.
- For depletion widths near 50 Å, carriers can tunnel through the potential barrier between valence and conduction bands. This lower voltage breakdown in heavily doped PN-junction diodes is called **tunneling breakdown** or **Zener breakdown**.

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## SMALL-SIGNAL $C_{pn}(V_{PN})$ CHARACTERISTICS

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- The small-signal capacitance per unit area  $C_{pn}(V_{PN})$  of a PN-junction diode is given by :

$$\begin{aligned} C_{pn}(V_{PN}) &\equiv \left| \frac{dQ_{pn}(V_{PN})}{dV_{PN}} \right| , \\ &= \left| \frac{dQ_{pn\cdot dep}(V_{PN})}{dV_{PN}} \right| + \left| \frac{dQ_{pn\cdot diff,P}(V_{PN})}{dV_{PN}} \right| + \left| \frac{dQ_{pn\cdot diff,N}(V_{PN})}{dV_{PN}} \right| , \\ &= C_{pn\cdot dep}(V_{PN}) + C_{pn\cdot diff,P}(V_{PN}) + C_{pn\cdot diff,N}(V_{PN}) . \end{aligned}$$

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## SMALL-SIGNAL $C_{pn}(V_{PN})$ CHARACTERISTICS

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- The small-signal PN-junction diode depletion capacitance  $C_{pn\cdot dep}(V_{PN})$  per unit area is given by

$$C_{pn\cdot dep}(V_{PN}) = \sqrt{\frac{q \epsilon_{Si}}{2} \cdot \frac{N_a^- N_d^+}{(N_a^- + N_d^+)} \cdot \frac{1}{(V_{bi} - V_{PN})}}.$$

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## SMALL-SIGNAL $C_{pn}(V_{PN})$ CHARACTERISTICS

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- The small-signal diffusion capacitance  $C_{pn\cdot diff,N}(V_{PN})$  per unit area on the  $n$ -side of the junction for a long-base  $n$ -side quasi-neutral region is given by

$$C_{pn\cdot diff,N}(V_{PN}) = \frac{q^2 n_i^2 L_{p,N}}{k_B T N_d^+} \exp\left(\frac{q V_{PN}}{k_B T}\right) .$$

- The small-signal diffusion capacitance  $C_{pn\cdot diff,P}(V_{PN})$  per unit area on the  $p$ -side of the junction for a long-base  $p$ -side quasi-neutral region is given by

$$C_{pn\cdot diff,P}(V_{PN}) = \frac{q^2 n_i^2 L_{n,P}}{k_B T N_a^-} \exp\left(\frac{q V_{PN}}{k_B T}\right) .$$

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## SMALL-SIGNAL $C_{pn}(V_{PN})$ CHARACTERISTICS

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- The PN-junction diffusion capacitance per unit area can be expressed as

$$\begin{aligned} C_{pn\cdot diff}(V_{PN}) &= \left[ C_{pn\cdot diff,P}(0) + C_{pn\cdot diff,N}(0) \right] \exp \left( \frac{q V_{PN}}{k_B T} \right) , \\ &= C_{pn\cdot diff}(0) \exp \left( \frac{q V_{PN}}{k_B T} \right) , \end{aligned}$$

where

$$C_{pn\cdot diff}(0) = C_{pn\cdot diff,P}(0) + C_{pn\cdot diff,N}(0) .$$

## SMALL-SIGNAL $C_{pn}(V_{PN})$ CHARACTERISTICS

- The small-signal PN-junction diode capacitance per unit area is given by

$$C_{pn}(V_{PN}) = C_{pn\cdot dep}(0) \sqrt{\frac{V_{bi}}{(V_{bi} - V_{PN})}} + C_{pn\cdot diff}(0) \exp\left(\frac{q V_{PN}}{k_B T}\right),$$

where

$$C_{pn\cdot dep}(0) = \sqrt{\frac{q \epsilon_{Si}}{2} \cdot \frac{N_a^- N_d^+}{(N_a^- + N_d^+)} \cdot \frac{1}{V_{bi}}},$$

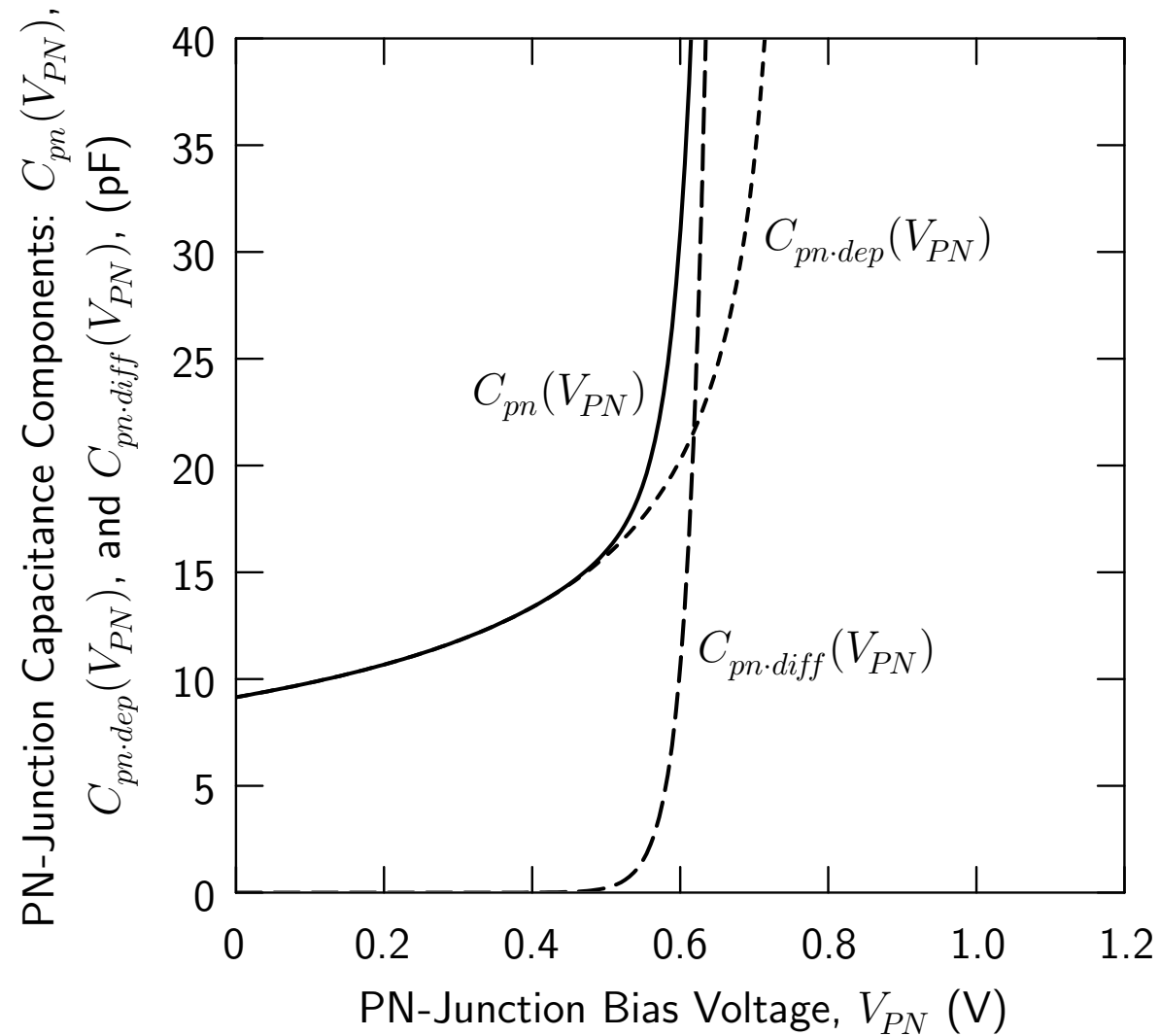
$$C_{pn\cdot diff,P}(0) = \frac{q^2 n_i^2 L_{n,P}}{k_B T N_a^-},$$

and

$$C_{pn\cdot diff,N}(0) = \frac{q^2 n_i^2 L_{p,N}}{k_B T N_d^+}.$$



## SMALL-SIGNAL $C_{pn}(V_{PN})$ CHARACTERISTICS



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## MOSCAP PARAMETERS, VARIABLES, AND DISTRIBUTIONS

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- $N_{a,B}^-$  Ionized-acceptor concentration in the substrate region,
- $X_{ox}$  Gate-oxide thickness,
- $Q_f$  Fixed-oxide charge density ( $Q_f = q N_f$ ),
- $Q_{it}(V_{GB})$  Interface-trap charge density ( $Q_{it}(V_{GB}) = q N_{it}(V_{GB})$ ), and
- $\varphi_{PM}$  Contact-potential difference between the  $p$ -type substrate and the backside metal contact.
- $Q_G(V_{GB})$  Charge density in the metal-gate region,
- $\mathcal{E}_{x,OX}(V_{GB})$  Electric field in the  $x$ -direction in a charge-free gate-oxide layer,
- $V_{OX}(V_{GB})$  Voltage across the gate-oxide layer,
- $Q_{SC,B}(V_{GB})$  Charge density in the substrate space-charge region, and
- $V_{SC,B}(V_{GB})$  Voltage across the substrate space-charge region.

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# MOSCAP PARAMETERS, VARIABLES, AND DISTRIBUTIONS

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- The charge density  $Q_{SC,B}(V_{GB})$  (C/cm<sup>2</sup>) in the substrate space-charge region is defined as

$$Q_{SC,B}(V_{GB}) \equiv \int_{0^+}^{\text{neutral bulk}} \varrho_B(x, V_{GB}) \, dx .$$

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## BASIC RELATIONSHIPS

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- The electrostatic-potential-distribution relationship

$$V_{GB} = V_{OX}(V_{GB}) + V_{SC,B}(V_{GB}) + \varphi_{PM} ,$$

- The charge-density-conservation relationship

$$Q_G(V_{GB}) + Q_f + Q_{it}(V_{GB}) + Q_{SC,B}(V_{GB}) = 0 .$$

- The electric-displacement-vector continuity at the metal/gate-oxide interface

$$\begin{aligned} \epsilon_{ox} \mathcal{E}_{x,OX}(V_{GB}) + Q_f + Q_{it}(V_{GB}) &= \epsilon_{Si} \mathcal{E}_{x,B}(0^+, V_{GB}) , \\ &= -Q_{SC,B}(V_{GB}) . \end{aligned}$$

- The electric-displacement-vector continuity at the gate-oxide/substrate interface

$$Q_G(V_{GB}) = \epsilon_{ox} \mathcal{E}_{x,OX}(V_{GB}) .$$

## BASIC RELATIONSHIPS

- The voltage  $V_{OX}(V_{GB})$  across a charge-free gate-oxide layer and the electric field  $\mathcal{E}_{x,OX}(V_{GB})$  in it are related by :

$$V_{OX}(V_{GB}) = X_{ox} \mathcal{E}_{x,OX}(V_{GB}) , \quad \text{or} \quad \mathcal{E}_{x,OX}(V_{GB}) = \frac{V_{OX}(V_{GB})}{X_{ox}} .$$

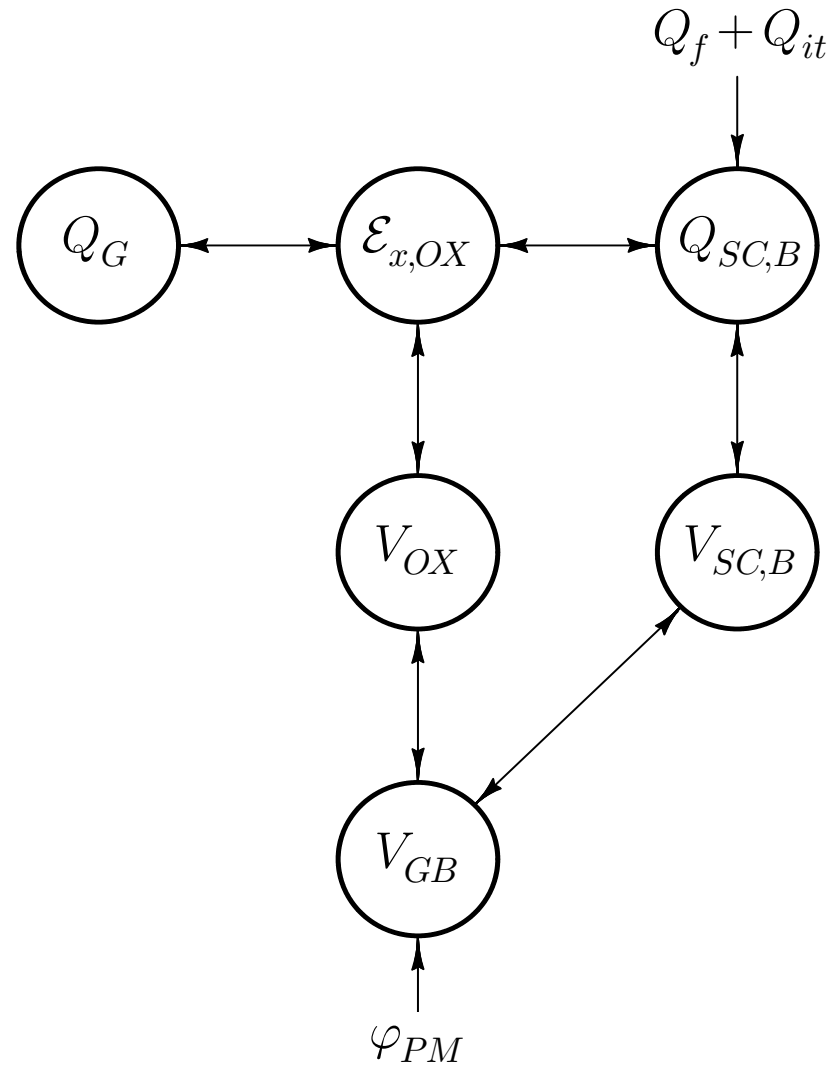
- The electron and hole concentration distributions are related to the electrostatic-potential distribution by

$$n_B(x, V_{GB}) = n_B^{\circ} \exp \left( \frac{q [\psi_B(x, V_{GB}) - \psi_B(\text{neutral bulk})]}{k_B T} \right) ,$$

and

$$p_B(x, V_{GB}) = p_B^{\circ} \exp \left( - \frac{q [\psi_B(x, V_{GB}) - \psi_B(\text{neutral bulk})]}{k_B T} \right) .$$

# BASIC RELATIONSHIPS



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## MOSCAP AT THERMAL EQUILIBRIUM

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- A metal-gate MOS capacitor is at thermal equilibrium at  $V_{GB} = 0$ . At thermal equilibrium,

$$V_{OX}^{\circ} + V_{SC,B}^{\circ} + \varphi_{PM} = 0.$$

- At thermal equilibrium, the charge-density-conservation relationship at thermal equilibrium is expressed as

$$Q_G^{\circ} + Q_f + Q_{it}^{\circ} + Q_{SC,B}^{\circ} = 0.$$

- The values of the flat-band and threshold voltages will determine the condition of the substrate space-charge region at thermal equilibrium. The approximate analysis can be then applied to find  $V_{SC,B}^{\circ}$  and  $Q_{SC,B}^{\circ}$ .

## MOSCAP AT THERMAL EQUILIBRIUM

- The oxide electric field  $\mathcal{E}_{x,OX}^\circ$  at thermal equilibrium is given by

$$\mathcal{E}_{x,OX}^\circ = \frac{Q_G^\circ}{\epsilon_{ox}} = - \frac{Q_f + Q_{it}^\circ + Q_{SC,B}^\circ}{\epsilon_{ox}} ,$$

and the thermal-equilibrium oxide voltage  $V_{OX}^\circ$  is given by

$$\begin{aligned} V_{OX}^\circ &= X_{ox} \mathcal{E}_{x,OX}^\circ , \\ &= - X_{ox} \frac{Q_f + Q_{it}^\circ + Q_{SC,B}^\circ}{\epsilon_{ox}} , \\ &= - \frac{Q_f + Q_{it}^\circ + Q_{SC,B}^\circ}{C_{ox}} = - \left( V_{SC,B}^\circ + \varphi_{PM} \right) . \end{aligned}$$

which can be rearranged to read

$$Q_{SC,B}^\circ(V_{SC,B}^\circ) = C_{ox} V_{SC,B}^\circ + C_{ox} \varphi_{PM} - \left( Q_f + Q_{it}^\circ \right) .$$



## The Accumulation Bias Range:

- $V_{GB} \leq V_{FB.N}$ .
- $p_B(0, V_{GB}) \geq p_B^\circ$ .
- $n_B(0, V_{GB}) \leq n_B^\circ$ .

In the approximate analysis:

- $V_{SC,B}^{acc}(V_{GB}) \ll V_{OX}^{acc}(V_{GB}) + \varphi_{PM}$ ,
- $V_{GB} \approx V_{OX}^{acc}(V_{GB}) + \varphi_{PM}$ .
- $V_{OX}^{acc}(V_{GB}) \approx V_{GB} - \varphi_{PM}$ .
- $\mathcal{E}_{x,OX}^{acc}(V_{GB}) \approx \frac{V_{GB} - \varphi_{PM}}{X_{ox}}$ .
- $Q_G^{acc}(V_{GB}) \approx C_{ox}(V_{GB} - \varphi_{PM})$ .
- $Q_{SC,B}^{acc}(V_{GB}) \approx -C_{ox}(V_{GB} - V_{FB.N})$ .

# BIAS RANGES AND IMPORTANT BIAS VOLTAGES

## The Flat-Band Voltage:

- $Q_{SC,B}(V_{FB,N}) \equiv 0$ .
- $V_{SC,B}(V_{FB,N}) \equiv 0$ .
- $V_{FB,N} = V_{OX}(V_{FB,N}) + \varphi_{PM}$ .
- $Q_G(V_{FB,N}) = -(Q_f + Q_{it}(V_{FB,N}))$ .
- $\mathcal{E}_{x,OX}(V_{FB,N}) = \frac{Q_G(V_{FB,N})}{\epsilon_{ox}} = -\frac{(Q_f + Q_{it}(V_{FB,N}))}{\epsilon_{ox}}$ .
- $V_{OX}(V_{FB,N}) = X_{ox} \mathcal{E}_{x,OX}(V_{FB,N}) = -\frac{(Q_f + Q_{it}(V_{FB,N}))}{C_{ox}}$ .
- $V_{FB,N} = \varphi_{PM} - \frac{(Q_f + Q_{it}(V_{FB,N}))}{C_{ox}}$ .

### The Flat-Band Voltage:

- The flat-band voltage  $V_{FB.N}$  can be negative, zero, or positive.
- At the flat-band voltage:

$$n_B(x, V_{FB.N}) = n_B^{\circ} = \frac{n_i^2}{N_{a,B}^-},$$

$$p_B(x, V_{FB.N}) = p_B^{\circ} = N_{a,B}^-,$$

$$\rho_B(x, V_{FB.N}) = 0,$$

and

$$\mathcal{E}_{x,B}(x, V_{FB.N}) = 0.$$

# BIAS RANGES AND IMPORTANT BIAS VOLTAGES

## The Depletion Bias Range:

- $V_{T.N} \geq V_{GB} \geq V_{FB.N}$ .
- $p_B^{\circ} \geq p_B(0, V_{GB}) \geq n_B^{\circ}$ .
- $n_B^{\circ} \leq n_B(0, V_{GB}) \leq p_B^{\circ}$ .
- $W_{d,B}^{dep}(V_{GB})$  increases from 0 to  $W_{d,B}^{dep}(V_{T.N})$ .
- $V_{SC,B}^{dep}(V_{GB})$  increases from 0 to  $2\varphi_{F,B}$ .

In the approximate analysis:

- $W_{d,B}^{dep}(V_{GB}) \approx \sqrt{\frac{2\epsilon_{Si}}{q N_{a,B}^-} V_{SC,B}^{dep}(V_{GB})}$ .
- $Q_{SC,B}^{dep}(V_{GB}) \approx -\sqrt{2q\epsilon_{Si} N_{a,B}^- V_{SC,B}^{dep}(V_{GB})}$ .

# BIAS RANGES AND IMPORTANT BIAS VOLTAGES

## The Depletion Bias Range:

- $Q_G^{dep}(V_{GB}) \approx \sqrt{2 q \epsilon_{Si} N_{a,B}^- V_{SC,B}^{dep}(V_{GB})} - \left[ Q_f + Q_{it}^{dep}(V_{GB}) \right] .$
- $\mathcal{E}_{x,OX}^{dep}(V_{GB}) \approx \frac{\sqrt{2 q \epsilon_{Si} N_{a,B}^- V_{SC,B}^{dep}(V_{GB})}}{\epsilon_{ox}} - \frac{\left[ Q_f + Q_{it}^{dep}(V_{GB}) \right]}{\epsilon_{ox}} .$
- $V_{OX}^{dep}(V_{GB}) \approx \frac{\sqrt{2 q \epsilon_{Si} N_{a,B}^- V_{SC,B}^{dep}(V_{GB})}}{C_{ox}} - \frac{\left[ Q_f + Q_{it}^{dep}(V_{GB}) \right]}{C_{ox}} .$
- $V_{GB} \approx \frac{\sqrt{2 q \epsilon_{Si} N_{a,B}^- V_{SC,B}^{dep}(V_{GB})}}{C_{ox}} + V_{SC,B}^{dep}(V_{GB}) + V_{FB,N} .$

# BIAS RANGES AND IMPORTANT BIAS VOLTAGES

## The Depletion Bias Range:

- $V_{SC,B}^{dep}(V_{GB}) \approx V_{GB} - V_{FB,N}$   
$$+ \frac{q \epsilon_{Si} N_{a,B}^-}{C_{ox}^2} \left[ 1 - \sqrt{1 + \frac{2 C_{ox}^2}{q \epsilon_{Si} N_{a,B}^-} (V_{GB} - V_{FB,N})} \right] .$$
- From this approximate relationship, we can calculate  $V_{SC,B}^{dep}(V_{GB})$  for a certain value of  $V_{GB}$ . It is then possible to calculate all other MOS variables which depend only on  $V_{SC,B}^{dep}(V_{GB})$ .

### The Threshold Voltage:

- $n_B(0, V_{T.N}) = p_B^{\circ} ,$
- $p_B(0, V_{T.N}) = n_B^{\circ} ,$
- $V_{T.N} = V_{OX}(V_{T.N}) + V_{SC,B}(V_{T.N}) + \varphi_{PM} ,$
- $Q_G(V_{T.N}) + Q_f + Q_{it}(V_{T.N}) + Q_{SC,B}(V_{T.N}) = 0 .$
- $V_{SC,B}(V_{T.N}) = \frac{2 k_B T}{q} \ln \left( \frac{N_{a,B}^-}{n_i} \right) = 2 \varphi_{F,B} ,$
- $\varphi_{F,B} = \frac{k_B T}{q} \ln \left( \frac{N_{a,B}^-}{n_i} \right) .$

# BIAS RANGES AND IMPORTANT BIAS VOLTAGES

## The Threshold Voltage:

- $W_{d,B}(V_{T.N}) = \sqrt{\frac{2 \epsilon_{Si}}{q N_{a,B}^-} V_{SC,B}(V_{T.N})} = \sqrt{\frac{4 \epsilon_{Si} \varphi_{F,B}}{q N_{a,B}^-}} .$
- $Q_{SC,B}(V_{T.N}) = -q N_{a,B}^- W_{d,B}(V_{T.N}) = -\sqrt{4 q \epsilon_{Si} N_{a,B}^- \varphi_{F,B}} .$
- $Q_G(V_{T.N}) = \sqrt{4 q \epsilon_{Si} N_{a,B}^- \varphi_{F,B}} - [Q_f + Q_{it}(V_{T.N})] .$
- $\mathcal{E}_{x,OX}(V_{T.N}) = \frac{Q_G(V_{T.N})}{\epsilon_{ox}} = \frac{\sqrt{4 q \epsilon_{Si} N_{a,B}^- \varphi_{F,B}} - [Q_f + Q_{it}(V_{T.N})]}{\epsilon_{ox}} .$
- $V_{OX}(V_{T.N}) = \frac{\sqrt{4 q \epsilon_{Si} N_{a,B}^- \varphi_{F,B}}}{C_{ox}} - \frac{Q_f + Q_{it}(V_{T.N})}{C_{ox}} .$



## The Threshold Voltage:

- $V_{T.N} = V_{FB.N} + 2\varphi_{F,B} + \frac{\sqrt{4q\epsilon_{Si}N_{a,B}^-\varphi_{F,B}}}{C_{ox}}.$
- $\varphi_{PM} = -0.51165 - \frac{k_B T}{q} \ln \left( \frac{N_{a,B}^-}{n_i} \right).$

# BIAS RANGES AND IMPORTANT BIAS VOLTAGES

## The Inversion Bias Range:

- $V_{GB} \geq V_{T.N}$ ,
- $n_B(0, V_{GB}) \geq p_B^\circ$ ,
- $p_B(0, V_{GB}) \leq n_B^\circ$ .

In the approximate analysis:

- $Q_{SC,B}^{inv}(V_{GB}) = Q_{DEP,B}^{inv}(V_{GB}) + Q_{INV,B}^{inv}(V_{GB})$ .
- $W_{d,B}^{inv}(V_{GB}) = W_{d,B}^{max} \approx W_{d,B}^{dep}(V_{T.N}) \approx \sqrt{\frac{4 \epsilon_{Si} \varphi_{F,B}}{q N_{a,B}^-}}$ .
- $V_{SC,B}^{inv}(V_{GB}) \approx V_{SC,B}^{inv}(V_{T.N}) \approx 2 \varphi_{F,B}$ .
- The inversion-layer charge is assumed to be a charge sheet located at the gate-oxide/substrate interface.

## The Inversion Bias Range:

- $Q_{DEP,B}^{inv}(V_{GB}) \approx -q N_{a,B}^- W_{d,B}^{max} \approx -\sqrt{4 q \epsilon_{Si} N_{a,B}^- \varphi_{F,B}} \cdot$
- $Q_{INV,B}^{inv}(V_{GB}) \approx Q_{SC,B}^{inv}(V_{GB}) + \sqrt{4 q \epsilon_{Si} N_{a,B}^- \varphi_{F,B}} \cdot$
- $V_{GB} \approx V_{OX}^{inv}(V_{GB}) + 2 \varphi_{F,B} + \varphi_{PM} \cdot$
- $V_{OX}^{inv}(V_{GB}) \approx V_{GB} - 2 \varphi_{F,B} - \varphi_{PM} \cdot$
- $\mathcal{E}_{x,OX}^{inv}(V_{GB}) \approx \frac{V_{GB} - 2 \varphi_{F,B} - \varphi_{PM}}{X_{ox}} \cdot$
- $Q_G^{inv}(V_{GB}) \approx C_{ox} (V_{GB} - 2 \varphi_{F,B} - \varphi_{PM}) \cdot$
- $Q_{SC,B}^{inv}(V_{GB}) \approx -C_{ox} (V_{GB} - 2 \varphi_{F,B} - V_{FB,N}) \cdot$
- $Q_{INV,B}^{inv}(V_{GB}) \approx -C_{ox} (V_{GB} - V_{T,N}) \cdot$

# SMALL-SIGNAL CAPACITANCE-VOLTAGE CHARACTERISTICS

- $C_{gb}(V_{GB}) = \frac{C_{ox} C_{sc,B}(V_{GB})}{C_{ox} + C_{sc,B}(V_{GB})} .$
- $C_{gb}^{acc}(V_{GB}) \approx C_{ox} .$
- $C_{sc,B}^{dep}(V_{GB}) \approx \frac{\epsilon_{Si}}{W_{d,B}^{dep}(V_{GB})} \approx \frac{\epsilon_{Si}}{\sqrt{2 \epsilon_{Si} V_{SC,B}^{dep}(V_{GB}) / q N_{a,B}^-}} .$
- $W_{d,B}^{inv}(V_{GB}) = W_{d,B}^{dep}(V_{T.N}) = W_{d,B}^{max} = \sqrt{\frac{4 \epsilon_{Si} \varphi_{F,B}}{q N_{a,B}^-}} .$
- $C_{sc,B.HF}^{inv}(V_{GB}) = \frac{\epsilon_{Si}}{W_{d,B}^{max}} = \sqrt{\frac{q \epsilon_{Si} N_{a,B}^-}{4 \varphi_{F,B}}} .$

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## SMALL-SIGNAL CAPACITANCE-VOLTAGE CHARACTERISTICS

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- $C_{gb\cdot HF}^{inv}(V_{GB}) = \frac{C_{ox} C_{sc,B\cdot HF}^{inv}(V_{GB})}{C_{ox} + C_{sc,B\cdot HF}^{inv}(V_{GB})} = \frac{1}{\left(\frac{X_{ox}}{\epsilon_{ox}} + \frac{W_{d,B}^{max}}{\epsilon_{Si}}\right)} \neq f(V_{GB}) .$
- $C_{gb\cdot LF}^{inv}(V_{GB}) \approx C_{ox} .$

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## MOSFET TYPES

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- N-Channel and P-Channel MOSFETs
- Enhancement-Mode and Depletion-Mode MOSFETs
- Surface-channel and Buried-channel MOSFETs
- Bulk and Silicon-on-Insulator (SOI) MOSFETs

## STATIC DRAIN-CURRENT CHARACTERISTICS

- $V_{T.N}(V_{BS}) = V_{FB.N0} + 2\varphi_{F,B} + \frac{1}{C_{ox}} \sqrt{2q\epsilon_{Si} N_{a,B}^- (2\varphi_{F,B} - V_{BS})}$ .
- $V_{T.N0} \equiv V_{T.N}(V_{BS} = 0) = V_{FB.N0} + 2\varphi_{F,B} + \gamma_{B.N} \sqrt{2\varphi_{F,B}}$ .
- $\gamma_{B.N} \equiv \frac{\sqrt{2q\epsilon_{Si} N_{a,B}^-}}{C_{ox}}$ .
- $V_{DSat} = V_{GS} - V_{T.N}(V_{BS})$ .
- $K_N = \mu_{n.ch} C_{ox} \frac{W_{ch}}{L_{ch}}$ .
- For  $V_{GS} \leq V_{T.N}(V_{BS})$ , the NMOSFET is off and

$$I_D^{off} = 0.$$

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## STATIC DRAIN-CURRENT CHARACTERISTICS

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- For  $V_{GS} \geq V_{T.N}(V_{BS})$  and  $V_{DS} \leq V_{DSat}$ , the NMOSFET is in the linear bias range and

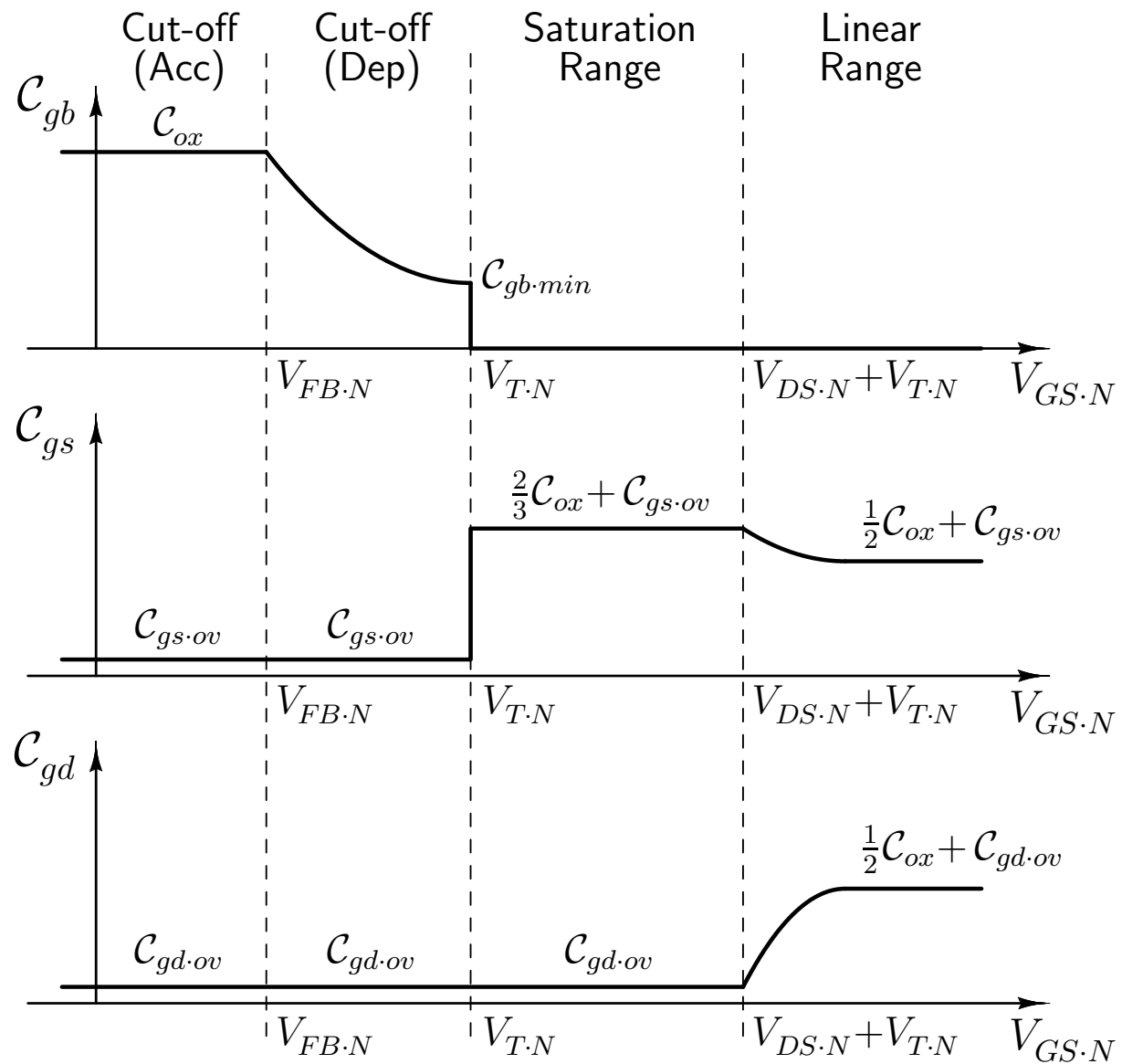
$$I_D^{lin} = K_N \left[ \left( V_{GS} - V_{T.N}(V_{BS}) \right) V_{DS} - \frac{1}{2} V_{DS}^2 \right].$$

- For  $V_{GS} \geq V_{T.N}(V_{BS})$  and  $V_{DS} \geq V_{DSat}$ , the NMOSFET is in the saturation bias range and

$$I_D^{sat} = \frac{K_N}{2} \left( V_{GS} - V_{T.N}(V_{BS}) \right)^2 \left[ 1 + \lambda_N (V_{DS} - V_{DSat}) \right].$$



# MOSFET CAPACITANCES



## SMALL-SIGNAL MOSFET MODEL

- $i_d = g_m v_{gs} + g_{mb} v_{bs} + g_o v_{ds} .$
- $g_m^{sat} = K_N \left( V_{GS} - V_{T.N}(V_{BS}) \right) \left[ 1 + \lambda_N (V_{DS} - V_{DSat}) \right] .$
- $g_{mb}^{sat} = \frac{\gamma_{B.N}}{2 \sqrt{2 \varphi_{F,B} - V_{BS}}} g_m^{sat} .$
- $g_o^{sat} = \frac{\lambda_N K_N}{2} \left( V_{GS} - V_{T.N}(V_{BS}) \right)^2 = \frac{1}{r_o^{sat}} ,$
- $f_T = \frac{g_m^{sat}}{2 \pi (C_{gs} + C_{gd})} = \frac{3 \mu_{n.ch}}{4 \pi L_{ch}^2} \left( V_{GS} - V_{T.N}(V_{BS}) \right) .$