

# **MM-640 Midsem Project**

Preliminary Presentation

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# **Phase field study of grain boundary effects on spinodal decomposition**

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Have developed a phase field model of a **polycrystalline binary alloy** by combining

1. The **Cahn-Hilliard** model for a compositionally inhomogeneous alloy
2. A model of polycrystals (Fan D, Chen L-Q. Acta Mater. 1997;45:3297) which is governed by the **Cahn-Allen** equation for non-conserved variables

Have used this model to study **grain boundary (GB)** effects on **spinodal decomposition (SD)** in two-dimensional (2D) systems.

# **I. Model**

# I.1. Cahn Hilliard Model

Cahn–Hilliard Model for a compositionally inhomogeneous alloy is used. It is developed using the composition field  $\mathbf{c}(\mathbf{r})$  in an alloy.

The local composition  $\mathbf{c}$  used in this model is defined as follows:

$$c = \frac{c' - c'_{\alpha}}{c'_{\beta} - c'_{\alpha}}$$

*where,  $c'$  is the local composition,*

*$c'_{\alpha}$  is the equilibrium composition of A rich  $\alpha$  phase,*

*$c'_{\beta}$  is the equilibrium composition of B rich  $\beta$  phase*

# I.1. Cahn Hilliard Model (contd.)

$$c = \frac{c' - c'_\alpha}{c'_\beta - c'_\alpha}$$

*where,  $c'$  is the local composition,*

*$c'_\alpha$  is the equilibrium composition of A rich  $\alpha$  phase,*

*$c'_\beta$  is the equilibrium composition of B rich  $\beta$  phase*

all the values are expressed in mole fraction of species B. Thus, for  **$\alpha$  phase  $c = 0$**  and for  **$\beta$  phase  $c = 1$**

## I.2. Cahn Allen Model

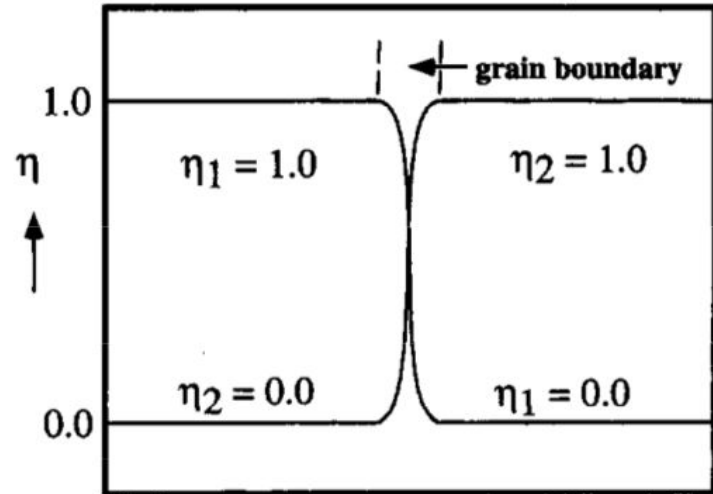
Cahn–Allen theory for non-conserved variables (the model of Fan and Chen (1997) belongs to this category) is used. It is developed using a set of  $n$  ‘orientational’ (and non-conserved) order parameter fields  $\mathbf{n}_i(\mathbf{r})$  ( $i = 1, 2, \dots, n$ ) to represent  $n$  different grain orientations in the microstructure;  $\mathbf{n}_i$  are continuum analogues of Potts variables in the  $n$ -state Potts model



## I.2. Cahn Allen Model (contd.)

Each  $\eta_i$  is taken to be **1** within the  $i^{\text{th}}$  grain and drops to **0** outside it, through a GB region where it varies smoothly.

The schematic profiles of two orientation variables across a flat grain boundary.



## I.3. Conclusion

An instantaneous configuration in our model is described in terms of the  $\mathbf{n}+1$  position-dependent field variables  $(\mathbf{c}; \boldsymbol{\eta}_1, \boldsymbol{\eta}_2, \dots, \boldsymbol{\eta}_n)$ .

## **II. Mathematical Formulation of the Model**

## II.1. Energetics

The Total Free energy,  $\mathbf{F}$ , of a system with inhomogeneities in both  $\mathbf{c}$  and  $\mathbf{\eta}_i$  is written as a volume integral:

$$F = N_V \int \left[ f(c, \eta_i) + \kappa_c (\nabla c)^2 + \sum_i^n \kappa_i (\nabla \eta_i)^2 \right]$$

## II.1. Energetics (contd.)

$$F = N_V \int \left[ f(c, \eta_i) + \kappa_c (\nabla c)^2 + \sum_i^n \kappa_i (\nabla \eta_i)^2 \right]$$

where

$N_V$  is the (constant) number of atoms per unit volume,

$f(\mathbf{c}, \boldsymbol{\eta}_i)$  is the bulk free energy density and,

$\kappa_c$  &  $\kappa_i$  are the (constant) gradient energy coefficients associated with inhomogeneities in  $\mathbf{c}$  and in  $\boldsymbol{\eta}_i$ , respectively.

It is assumed that  $\kappa_i = \kappa_{\boldsymbol{\eta}}$  for all  $i$ .

## II.1. Energetics (contd.)

Thus, the bulk free energy density  $\mathbf{f}(\mathbf{c}, \mathbf{n}_i)$  is chosen such that it exhibits a minimum for these  $2\mathbf{n}$  possibilities. In other words,  $\mathbf{f}$  has  **$2\mathbf{n}$  degenerate minima** (whose value is chosen to be **0**)

These minima are located at  $\mathbf{n}$  grains of  $\mathbf{a}$  with a composition of  $\mathbf{c} = \mathbf{0}$ :

$(\mathbf{0}; \mathbf{1}, \mathbf{0}, \dots, \mathbf{0}), (\mathbf{0}; \mathbf{0}, \mathbf{1}, \dots, \mathbf{0}), \dots, (\mathbf{0}; \mathbf{0}, \mathbf{0}, \dots, \mathbf{1}),$

and  $\mathbf{n}$  grains of  $\mathbf{\beta}$  with a composition of  $\mathbf{c} = \mathbf{1}$ :

$(\mathbf{1}; \mathbf{1}, \mathbf{0}, \dots, \mathbf{0}), (\mathbf{1}; \mathbf{0}, \mathbf{1}, \dots, \mathbf{0}), \dots, (\mathbf{1}; \mathbf{0}, \mathbf{0}, \dots, \mathbf{1}).$

## II.1. Energetics (contd.)

$$f(c, \eta_i) = f(c_o) + m(c) \left\{ 0.25 + \sum_i^n \left[ -\frac{\eta_i^2}{2} + \frac{\eta_i^4}{4} \right] + \epsilon \sum_i^n \sum_{j>i}^n \eta_i^2 \eta_j^2 \right\}$$

**$f_o(\mathbf{c})$**  is the free energy per atom in a bulk single crystal of composition  **$\mathbf{c}$**  given by:

$$f(c_o) = A_c c^2 (1 - c)^2$$

## II.1. Energetics (contd.)

$$f(c_o)=A_c c^2 (1-c)^2$$

The constant  $\mathbf{A_c}$  determines the height of the free energy barrier between the equilibrium phases within a single grain,  $\mathbf{m(c)}$  is a composition dependent factor which couples  $\mathbf{c}$  &  $\mathbf{\eta_i}$  and  $\mathbf{\epsilon}$  is a constant.



## II.1. Energetics (contd.)

$$f(c, \eta_i) = f(c_o) + m(c) \left\{ 0.25 + \sum_i^n \left[ -\frac{\eta_i^2}{2} + \frac{\eta_i^4}{4} \right] + \epsilon \sum_i^n \sum_{j>i}^n \eta_i^2 \eta_j^2 \right\}$$

Note that the terms within the curly braces are even functions of  $\eta_i$ ; therefore,  $\mathbf{f}(\mathbf{c}, \eta_i)$  has additional degenerate minima at  $2n$  more locations with negative values of  $\eta_i$  such as  $\{\mathbf{c}; \eta_i\} = (\mathbf{0}; -1, 0, \dots, 0), \dots$ . In this case, these extra degenerate equilibrium states are excluded by working only with  $\eta_i \geq 0$ .

## II.2. Kinetics

The evolution of the composition field  $\mathbf{c}$  is governed by the **Cahn-Hilliard equation** for conserved variables:

$$\frac{dc}{dt} = M \nabla^2 \left[ \frac{\delta(F/N_V)}{\delta c} \right]$$

where  $\mathbf{d}(F/N_V)/\mathbf{d}\mathbf{c} = \boldsymbol{\mu}$  is the chemical potential whose gradient drives diffusion, and  $\mathbf{M}$  is the atomic mobility.

## II.2. Kinetics (contd.)

The evolution of order parameter fields  $\boldsymbol{\eta}_i$  is governed by the **Cahn-Allen equation** for non-conserved variables:

$$\frac{d\eta_i}{dt} = -L_i \left[ \frac{\delta(F/N_V)}{\delta\eta_i} \right]$$

where  $\partial(F/N_V)/\partial\boldsymbol{\eta}_i$  is the total free energy (per atom) with respect to  $\boldsymbol{\eta}_i$ , and  $\mathbf{L}_i$  are the relaxation coefficients for  $\boldsymbol{\eta}_i$ . Here,  $\mathbf{M}$  and  $\mathbf{L}_i = \mathbf{L}$  ( $i = 1, 2, \dots, n$ ) are assumed to be constants.

## II.3. Numerical Implementation

$$\frac{dc}{dt} = M \nabla^2 [g(c) - 2\kappa_c \nabla^4 c]$$

where  $\mathbf{g}(\mathbf{c}) = \partial \mathbf{f} / \partial \mathbf{c}$

The numerical method used in our simulations is based on the **semi-implicit Fourier spectral method**

$$\tilde{c}(\mathbf{k}, t + \Delta t) = \frac{\tilde{c}(\mathbf{k}, t) - \Delta t M k^2 \tilde{g}(\mathbf{k}, t)}{1 + 2\Delta t M \kappa_c k^4},$$

## II.3. Numerical Implementation (contd.)

Similarly for the **Cahn-Allen equation**

$$\tilde{\eta}_i(\mathbf{k}, t + \Delta t) = \frac{\tilde{\eta}_i(\mathbf{k}, t) - \Delta t L_i \tilde{h}_i(\mathbf{k}, t)}{1 + 2\Delta t L_i \kappa_\eta k^2},$$

where  $\mathbf{h}_i = \partial \mathbf{f} / \partial \mathbf{h}_i$

# **III. Settings for Simulation**

# III.1. The values of the parameters

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Model parameter	Value
$A$	1.0
$\kappa_c$	1.0
$M$	1.0
$\varepsilon$	2.0
$\kappa_i = \kappa_\eta$	1.0
$L_i = L$	1.0
Simulation parameter	Value
$\Delta x = \Delta y$	1.0
$\Delta t$	0.1
$N_x \times N_y$	512 $\times$ 256 (two-grain case)
	512 $\times$ 512 (polycrystalline case)

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## III.2. Variation of $m(c)$ & $\partial_c$ (disturbance)

The Initial Profile is set by  $c_o = 0.5 \pm \partial_c$   
 **$\partial_c$  is varied from 0.01 to 0.04**

System index	$m(c)$	$\kappa_\eta$
Ia	$1 + 0.5c^2$	1.0
Ib	$1 + 0.5c^2 - 2.5c^2(1-c)^2$	1.0
Ic	$2 + c^2$	0.5
IIa	$1 + 0.1c^2$	1.0



## **IV. Pseudo Code**

**Take input from file input.dat**

$n_x$ ,  $\Delta x$ ,  $n_y$ ,  $\Delta y$ ,  $T$ ,  $\Delta t$ ,  $T_{\text{write}}$ (after how many steps do we print the output in a file)

**Declare** composition,  $n_1$ ,  $n_2$ ,  $g$ ,  $h_1$  &  $h_2$  matrix and **Allocate memory**  
**Declare** the **Fourier Transform's** respectively

**Calculate** half\_nx, half\_ny,  $\Delta k_x$  &  $\Delta k_y$

**Make the Initial Profile**

Traverse the matrix

Generate Random Number  $R = [-1, 1]$

composition =  $0.5 \pm R \cdot 0.04$

IF  $i < \text{half\_nx}$

$n_1 = 1$  &  $n_2 = 0$

ELSE

$n_1 = 0$  &  $n_2 = 1$

## **Start time loop**

Traverse Matrix

**Calculate**  $g, h_1, h_2$

**Take** composition,  $n_1, n_2, g, h_1$  &  $h_2$  **to Fourier space**

**Evolve composition**

Traverse Matrix

**Calculate**  $k_x, k_y$

**Calculate** new composition,  $n_1$  &  $n_2$  --

**Take** composition,  $n_1$  &  $n_2$  back **to real space**

Traverse Matrix

**Normalise** the values and **Set** imaginary part to zero for composition,  $n_1$  &  $n_2$

After every  $T_{\text{write}}$  time steps **write** composition profile **to file**  
end time loop

**Free** all memory

**Thank You**