

A Priori Model Order Reduction for Transient Neutron Diffusion

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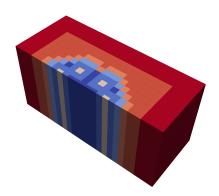
Outline

- 1. Motivation
 - Why reduced order modeling?
- 2. Proper generalized decomposition
- 3. Research Objectives
- 4. Results Transient Neutron Diffusion
 - 1D
 - 2D
- 5. Conclusions and Future Work



Drawbacks of high fidelity computing

- Current methods (FEM) scale exponentially with the number of dimensions and suffer from "curse of dimensionality"
- Consider a transient 3D transport simulation:
 - 2.7 million dof in space
 - 26 energy groups
 - S₈ quadrature in angle
 - 1000 points in time



Leads to $2.7E6 \times 26 \times 80 \times 1000 = 5.616E12 \text{ dof!}$



Need for reduced order models

Intractability increasingly apparent for:

- a) multiscale/multiphysics problems
- b) repeated evaluations (e.g. optimization and uncertainty quantification)

Development of accurate, lower order methods is needed.



Reduced Order Modeling

Main idea - develop efficient, low order models that accurately represent high fidelity, large-scale simulations.

Parametric model reduction:

- generation of a reduced order model (ROM) that approximates the original full-order system with high fidelity over a range of parameters
- Projection methods allow for retainment of underlying physics of original full-scale model



Projection Based Methods

Consider the following first order ODE:

$$\frac{dZ}{dt} = \mathbf{A} \cdot Z \tag{1}$$

We can define Z as the product of a *projection matrix*, ρ and the *reduced solution vector*, Z_r :

$$Z = \rho \cdot Z_r \tag{2}$$

Plugging Equation 2 into Equation 1:

$$\frac{d}{dt}\left(\rho Z_{r}\right) = \mathbf{A} \cdot \left(\rho Z_{r}\right)$$

We can arrive at our reduced order system:

$$ightarrow rac{dZ_r}{dt} =
ho^{-1} \mathbf{A} \cdot
ho Z_r$$



Projection matrix creation

- POD basis vectors are computed a posteriori through the "method of snapshots"
- Assume a set of Q solutions from a series of snapshots are known and defined as:

$$\boldsymbol{X} = [z_i, z_{i+1}, \dots, z_Q]$$

We can find a solution by constructing a correlation matrix and finding it's eigenvalues and eigenvectors:

$$R = \sum_{i=1}^{Q} z_i(z_i^T)$$
 $\rho = [v_1, v_2, ..., v_j]$

The eigenvectors, v_1, v_2, \ldots, v_j , correspond to the largest eigenvalues $\sigma_j > \sigma_1 \times \epsilon$, where $\epsilon = 10^{-8}$



Drawbacks of POD

- Quality of ROM is highly sensitive to snapshot set.
 - What data/solutions are appropriate/useful? Potentially requires ad-hoc/expert knowledge of problem on hand.
- A posteriori methods require an online solution of the full-order system.
 - POD ROM cannot be used without a data set either experimental or simulation. For many problems, this can be difficult or impractical.



A Priori Model Reduction

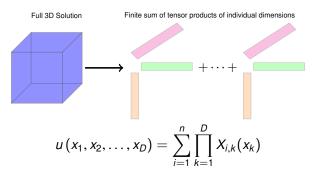
Ideally, one would want to be able to:

- 1. Create a ROM a priori
 - i.e. without having to rely on previous simulation/experimental data or any previous knowledge of the problem
- Assess the accuracy of the ROM on-the-fly and improve accuracy if need be.



Proper Generalized Decomposition (PGD)

PGD seeks a solution that is a series expansion whose components are products of separable functions in each dimension of interest:



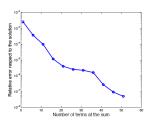
"Curse of dimensionality" is overcome by linear relationship!

F. Chinesta, et al. The Proper Generalized Decomposition for Advanced Numerical Simulations: A Primer. Springer 2014.



Select Applications of PGD

- A. Ammar et. al. applied PGD to multi-bead-spring molecular models of polymer solutions in complex fluids
 - Order reduction from 2.56E6 dof (standard) to 3200 dof (PGD)
- 2. González-Pintor et. al. applied PGD to calculate the dominant mode eigenvalue of a nuclear reactor



- 3. In nearly all works to date, only a few terms have been required in PGD expansions.
- A. Ammar, et. al. A new family of solvers for some classes of multidimensional partial differential equations accountered in kinetic theory modeling of complex fluids. Journal of Non-Newtonian Fluid Mechanics, 139:153-176, 2006.
- S. González-Pintor, et. al.. Using proper generalized decomposition to compute the dominant mode of a nutritiversity
 Mathematical and Computer Modelling 57:1807-1815, 2013.

Potential of PGD in Radiation Transport

Revisiting our 3D transport problem, we can separate the solution into a series of products of 7 1D basis functions:

$$\psi(\mathbf{r}, \mathbf{\Omega}, E, t) = \sum_{i=1}^{n} R(x, y, z) \xi(\theta, \varphi) E(\epsilon) T(t)$$

where:

$$R(x, y, z) = X(x)Y(y)Z(z)$$
, and $\xi(\omega) = A(\theta)P(\varphi)$

"Curse of dimensionality" overcome by linear relationship!

$$n(140 + 140 + 140 + 26 + 80 + 1000) << 5.616E12$$



Research Objectives

Using the diffusion approximation:

- Assess the relationship between model reduction and accuracy of an a priori ROM for two-dimensional, energy dependent transient flux calculations.
 - Theoretically possible to include energy as a "dimension" in the PGD approximation and obtain a continuous energy flux distribution.
- Extend the energy dependent transient flux ROM to include coupled sets of ODEs
 - E.g. reactor kinetics and/or depletion
 - Purpose is to investigate the applicability of a priori ROMs for a select multiscale problem in reactor physics.



Results so far...

- 1. 1D Transient Heat Transfer (FDM) ✓
- 2. 1D Transient Neutron Diffusion ✓
 - Assume constant cross sections, discretize each independent variable with FDM.
 - Expand into spatially dependent cross sections, discretize with FEM.
 - i. Dirichlet BC's, MMS.
 - Reflecting BCs, "real" problem with heterogeneity, reference CFEM solver with backward euler in time.
- 3. 2D Transient Neutron Diffusion
 - Dirichlet BC's, MMS 1/2



Mechanics of PGD - Preliminaries

Consider 1D transient neutron diffusion:

$$\frac{1}{v}\frac{\partial\phi}{\partial t} - \frac{\partial}{\partial x} \cdot D\frac{\partial}{\partial x}\phi + \Sigma_{a}(x)\phi(x,t) = S \tag{4}$$

Assume a solution in space and time:

$$\phi(x,t) \approx \sum_{j=1}^{n} X_j(x) T_j(t)$$
 (5)

where the:

- a) number of enrichment steps, n and
- b) basis functions, $X_j(x)$ and $T_j(t)$ are unknown a-priori.



Mechanics of PGD - Enriching the Solution

Separated representation is built progressively by "enriching".

- At enrichment step n + 1, assume we know the previous n terms.

$$\phi_{n+1}(x,t) = \phi_n(x,t) + X_{n+1}(x)T_{n+1}(t)$$

$$= \sum_{j=1}^n X_j(x)T_j(t) + X(x)T(t)$$
(6)



Mechanics of PGD - Alternating Direction Algorithm

- 1. Solve for X(x) assuming T(t)
- 2. Solve for $\mathcal{T}(t)$ with obtained $\mathcal{X}(x)$
- 3. Check convergence of X(x)T(t)
- 4. Check convergence of ROM



Alternating Direction Algorithm - Step 1

Starting with weighted residual form of the 1D transient neutron diffusion equation

$$\int_{\Omega_x \times \Omega_t} \phi^* \left(\frac{1}{\nu} \frac{\partial \phi}{\partial t} - \nabla \cdot D \nabla \phi + \Sigma_a(x) \phi(x, t) - S \right) dx dt = 0$$
 (7)

where the test function, ϕ^* , defined as:

$$\phi^*(x,t) = u(x)\mathcal{T}(t) \tag{8}$$

- $\mathcal{T}(t)$ is assumed known



Plugging our test function into the weighted residual form, we can obtain a BVP that is solved via CFEM

$$\int_{\Omega_{x}} u(x) \left[\left(\frac{1}{v} t_{2} + t_{1} \Sigma_{a}(x) \right) X(x) - t_{1} \frac{d}{dx} \cdot D(x) \frac{dX(x)}{dx} \right] dx$$

$$= -\sum_{j=1}^{n} \int_{\Omega_{x}} u(x) \left[\left(\frac{1}{v} t_{4,i} + t_{3,i} \Sigma_{a}(x) \right) X_{i}(x) dx - t_{3,i} \frac{d}{dx} \cdot D(x) \frac{dX_{i}(x)}{dx} dx \right]$$

$$+ \int_{\Omega_{x}} \int_{\Omega_{t}} u(x) S(x,t) \tag{9}$$



Alternating Direction Algorithm - Step 2

Revisiting our weighted residual form:

$$\int_{\Omega_x \times \Omega_t} \phi^* \cdot \left(\frac{1}{\nu} \frac{\partial \phi}{\partial t} - \nabla \cdot D \nabla \phi + \Sigma_a(x) \phi(x, t) - S \right) dx dt = 0$$
 (10)

This time, with a new test function, ϕ^* , defined as:

$$\phi^*(x,t) = \mathcal{X}(x)w(t) \tag{11}$$

- X(x) is known from previous step



 Plugging our test function into the weighted residual form, we can obtain an IVP that is solved via DFEM

$$\frac{1}{v}x_{1}\left(w(t)\mathcal{T}(t)\big|_{surf} - \int_{\Omega_{t}} \mathcal{T}(t)\frac{dw}{dt}dt\right) + (x_{2} - x_{3})\int_{\Omega_{t}} w(t)\mathcal{T}(t)dt$$

$$= -\sum_{i=1}^{n} \left[\frac{1}{v}x_{4,i}\left(w(t)\mathcal{T}_{i}(t)\big|_{surf} - \mathcal{T}_{i}\frac{dw}{dt}dt\right) + (x_{6,i} - x_{5,i})\int_{\Omega_{t}} w(t)\mathcal{T}_{i}(t)dt\right]$$

$$+ \int_{\Omega_{t}} \int_{\Omega_{x}} w(t)S(x,t) \tag{12}$$

- Closure obtained by upwinding on surface terms.
- Initial condition in all tests = 0.0.



Alternating Direction Algorithm - Steps 3 & 4

- Solving for X(x) and T(t) involves a nonlinear iteration.
- Convergence criteria, $v = 1 \times 10^{-6}$

$$\nu = \sqrt{(\|X^{p}\| \|\mathcal{T}^{p}\| - \|X^{p-1}\| \|\mathcal{T}^{p-1}\|)^{2}}$$

note,
$$\|\cdot\| = \|\cdot\|_{L_2}^2$$

- ROM convergence criteria, $\epsilon = 1 \times 10^{-6}$

$$\epsilon = \|\phi_{n+1} - \phi_n\|$$

$$= \|\left(\sum_{i=1}^n X_i T_i + X_{n+1} T_{n+1}\right) - \sum_{i=1}^n X_i T_i\|$$

$$\leq \|X_{n+1}\| \|T_{n+1}\|$$



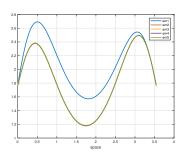
Alternating Direction Algorithm - Review

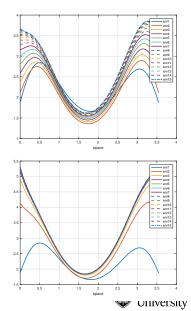
```
for m=1 to m_{max}
define X^{(0)}, T^{(0)} (initialization)
   for k=1 to k_{max}
   compute X^{(k)} = F_m(T^{(k-1)})
   compute T^{(k)} = G_m(X^{(k)})
   normalize, s.t. ||T^{(k)}||_{L^2}^2 = 1
   check convergence, v < X^{(k)}T^{(k)}
   end
normalize X^{(k)} and T^{(k)}
set X^{(k)} = X_m and T^{(k)} = T_m
check convergence, \epsilon < ||X_m||||T_m||
end
```



Importance of Normalizing in Non-linear Iterations

- Not commonly observed in literature
- Crucial to quality and convergence behavior of enrichment steps
- Normalization of time domain enhances convergence behavior and improves solution quality.





Test Problem 1

Using MMS with assumed solution of $\phi_{ref}(x, t) = t \sin(x)$:

Assume v = 1.5, $D = \Sigma_a = x + 1$

 $\Omega_{x} = [0, \pi]$; CFEM; 250 elements

 $\Omega_t = [0, 1; \text{DFEM}; 60 \text{ elements}]$

Both are discretized via 1st order linear polynomials

$$dof = n(251 + 120)$$

Error quantification is defined by the following:

$$ext{error}_i = \sqrt{\int_{\Omega_t} \int_{\Omega_x} \left(\phi_{ref}(x,t) - \sum_{j=1}^i \phi_{pgd,j}(x,t) \right)^2 dx dt}$$

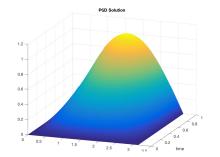
where, i, is the enrichment step of interest

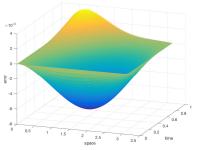


Test Problem 1 - Results

- PGD solution captures reference solution within first enrichment step.
- Higher enrichment steps have negligible effects.

Enr.Step	$ Ref - PGD _{L2}$
1	3.516E-3
2	4.325E-3
3	3.686E-3
4	3.679E-3
5	3.715E-3



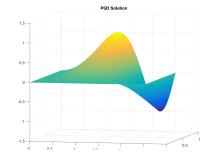


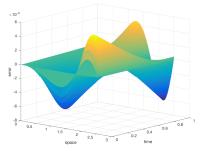


Test Problem 2

- $\phi_{ref} = t \sin(x^2)$
- $\Omega_x \in [0, \sqrt{2}\sqrt{\pi}]$; CFEM; 250 elements.
- $\Omega_t = [0, 1]$; DFEM; 60 elements
- Both are discretized via 1st order linear polynomials
- dofs = n(201+120)
- Again, PGD solution captures reference solution within first enrichment step.

Enr.Step	$ Ref - PGD _{L2}$
1	2.5661E-3
2	2.5693E-3
3	2.5694E-3





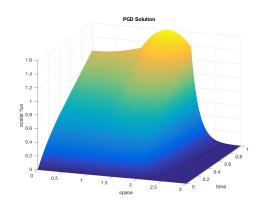


Test Problem 3 - A "real" problem

 Define 3 region heterogeneous problem (v= 1.5):

Region	D	Σ _a	Source
1	5.0	0.001	0.0
2	1.0	0.5	3.0
3	0.1	3.5	0.0

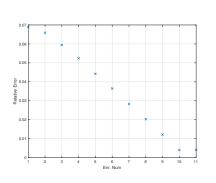
- $\Omega_x = [0,3]$; CFEM; 300 elements
- $\Omega_t = [0, 1]$; DFEM; 100 elements
- 1st order linear polynomials.
- dofs = n(301 + 200)

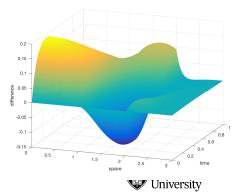




Test Problem 3 - Error Analysis

- Reference solution generated from solver with CFEM in space and Backward Euler in time
- Reference solution has $256 \times 256 = 65,536$ dof.
- PGD with 10 enrichment steps has 10(301 + 200) = 5,010 dof.





Test Problem 4 - 2D Transient

-
$$\phi_{ref} = t \sin(x) \sin(y)$$

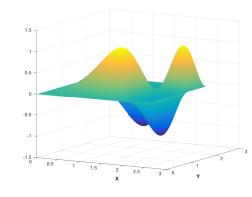
$$\Omega_x = \Omega_y \in [0, \sqrt{2}\sqrt{\pi}]; \text{ CFEM}; 100$$
 elements.

$$\Omega_t = [0, 1]$$
; DFEM; 100 elements.

$$D = (xy) + 1.0$$

$$\Sigma_t = ((x_r - x)(y_r - y)) + 1.0$$

Enr.Step	Ref – PGD _{L2} / _{Ref}	
1	0.0287	
2	0.0221	
3	0.3395	
4	0.2772	
5	0.3184	



- 1st order linear polynomials.
- dofs = n(100+100+100)



Conclusions

- "Curse of dimensionality" is apparent in reactor physics calculations
- More well developed, data driven methods are potentially impractical
- Proper generalized decomposition provides an avenue for a priori model reduction
- 1D Transient results show promise that PGD is a potentially viable solution to dimensionality issues



Moving Forward

- 1. 1D Transient problem
 - Mesh refinement studies.
- 2. 2D Transient problem
 - Improve understanding of normalization process in enrichment process.
 - Non-separable problems.
- 3. Expand to energy dependence
 - 1D transient formulation under construction now
 - Include energy as PGD dimension continuous in energy
- Couple energy dependent PGD ROM to ODEs
 - Reactor kinetics; precursor equations and delayed neutrons

Along the way...

- · Spatial discontinuities
- Increasingly real problems (fission source, etc)



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Questions?

