

RAYLEIGH-SOMMERFELD DIFFRACTION INTEGRAL OF THE FIRST KIND FRESNEL ZONE PLATE

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op_rs_zones.m

Calculation of the irradiance in a plane perpendicular to the optical axis for uniformly illuminated zone plates. It uses Method 3 – one-dimensional form of Simpson's rule for the integration of the diffraction integral.

op_rs_zones_z.m

Calculation of the irradiance along the optical axis for uniformly illuminated zone plates. It uses Method 3 – one-dimensional form of Simpson's rule for the integration of the diffraction integral.

Function calls to:

simpson1d.m (integration)

fn_distancePQ.m (calculates the distance between points P and Q)
turningPoints.m (finds the location of zeros, min and max of function)

Background documents



Scalar Diffraction theory: Diffraction Integrals



Numerical Integration Methods for the Rayleigh-Sommerfeld Diffraction Integral of the First Kind

Warning: The results of the integration may look OK but they may not be accurate if you have used insufficient number of partitions for the aperture space and observation space. It is best to check the convergence of the results as the number partitions is increased. Note: as the number of partitions increases, the calculation time **rapidly** increases.

RAYLEIGH-SOMMERFELD DIFFRACTION INTEGRAL OF THE FIRST KIND

FRESNEL ZONE PLATES

The Rayleigh-Sommerfeld diffraction integral of the first kind states that the electric field at an observation point P can be expressed as

(1)
$$E(P) = \frac{1}{2\pi} \iint_{S_A} E(\vec{r}) \frac{e^{jkr}}{r^3} z_p (jkr - 1) dS$$

It is assumed that the Rayleigh-Sommerfeld diffraction integral of the first kind is valid throughout the space in front of the aperture, right down to the aperture itself. There are no limitations on the maximum size of either the aperture or observation region, relative to the observation distance, because **no approximations have been made**.

The **irradiance** or more generally the term **intensity** has S.I. units of W.m⁻². Another way of thinking about the irradiance is to use the term **energy density** as an alternative. The use of the letter I can be misleading, therefore, we will often use the symbol u to represent the irradiance or energy density.

The irradiance or energy density u of a monochromatic light wave in matter is given in terms of its electric field E by

$$(2) u = \frac{c n \varepsilon_0}{2} |E|^2$$

where n is the refractive index of the medium, c is the speed of light in vacuum and ε_0 is the permittivity of free space. This formula assumes that the magnetic susceptibility is negligible, i.e. $\mu_r \approx 1$ where μ_r is the magnetic permeability of the light transmitting media. This assumption is typically valid in transparent media in the optical frequency range.

The integration can be done accurately using any of the numerical procedures based upon Simpson's rule to compute the energy density in the whole space in front of the aperture.



Numerical Integration Methods for the Rayleigh-Sommerfeld Diffraction Integral of the First Kind

FRESNEL ZONE PLATE

A circular aperture in which alternate rings are transparent and opaque is called a **Fresnel zone plate**. For a plane wave normally incident upon a zone plate, the diffracted light will be concentrated at the focal points along the optical axis. The zone plate acts just like a lens (figure 1).

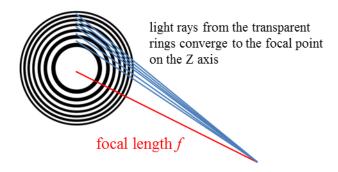


Fig. 1. Fresnel zone plate acts like a lens.

Complementary zone plates as shown in figure (2) give the same diffraction pattern. This is an example of **Babinet's Principle**.

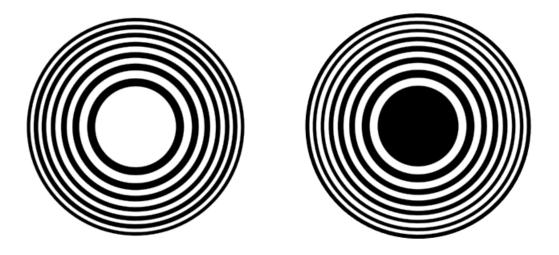


Fig. 2. Fresnel zone plates. Both zones plates give the same diffraction pattern (Babinet's Principle). **op_rs_zones.m**

The zone radii required to make the half-period zones relative to the focal point f_1 are given by equation (1)

(1)
$$R_N = \sqrt{\left(f_1 + \frac{N\lambda}{2}\right)^2 - f_1^2} \qquad \text{radius of the } N^{\text{th}} \text{ zone}$$

There are other maximum irradiance points along the optical axis and these focal points are found at

(2)
$$f_m = \left(\frac{1}{2m-1}\right) \frac{R_1^2}{\lambda} = \left(\frac{1}{2m-1}\right) f_1 \qquad m = 1, 2, 3, \dots \qquad f_1 = \frac{R_1^2}{\lambda}$$

Hence, these focal points occur along the optical axis at $z_P = f_1, f_1 / 3, f_1 / 5, \dots$

The Matlab code below shows how the zone plate and aperture grid was constructed.

```
% ZONE PLATE SETUP -----
 rz = zeros(Nzones,1);
 for nc = 1 : Nzones
 rz(nc) = sqrt((fzone + nc * wL / 2)^2 - fzone^2);
 end
 rMax = rz(end);
 rMin = eps;
 r = linspace(rMin, rMax, nR);
 dr = r(2)-r(1);
 m = (n2-n1) / (nR-1);
 b = n2 - m * nR;
 for c = 1 : nR
   n(c) = 2*round(0.5*(m*c+b))+1;
 end
 nQ = sum(n);
 flag = zeros(nR,1); flags = 1;
 for nc = 2 : Nzones
   if flags == 1; flag(r > rz(nc)) = 1; end;
   if flags \sim= 1; flag(r > rz(nc)) = 0; end;
   flags = (-1)^{(nc-1)};
 end
 EQ = sqrt(2*uQmax/(cL*nRI*eps0)).*EQ;
                             % bright centre
 %EQ = EQ .* ~flag;
 EQ = EQ .* flag;
                                % dark centre
```

Energy density variation along the optical axis

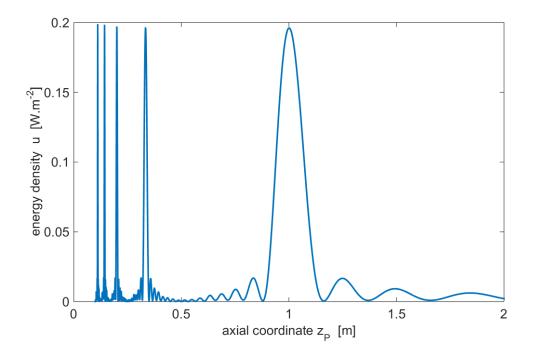
The mscript op_rs_zones_z.m was used to model the variation in the energy density along the optical axis (Z axis) for a Fresnel zone plate. A summary of the parameters used is given in the Matlab Command Window:

```
wavelength [m] = 6.328e-07
nQ = 562002
nP = 5309

Aperture Space
Number of zones = 16
radius of zone plate [m] = 3.182e-03

Observation Space
max radius rP [m] = 2.000
focal length of zone plate [m] f1 = 1.000
```

Figure 3 shows the variation in the energy density along the optical axis. The peaks show the location of the focal points. Table 1 gives the location z_P of the peaks and their strengths. The results are in excellent agreement with the predictions of equation (2). The execution time for running the mscript **op_rs_zones_z.m** was about 15 minutes. The Data Cursor function in the Figure Window for figure (3) was used for the location and strengths of the peaks.



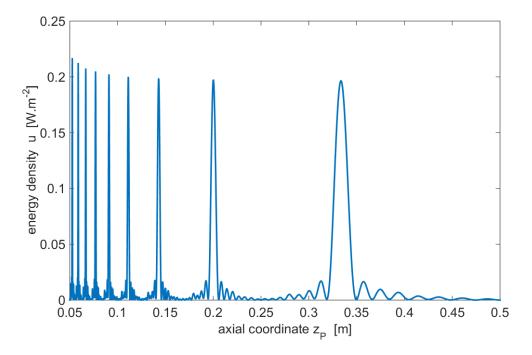


Fig. 3. Energy density along the optical axis.

Table 1. Location z_P of the peaks and their strengths along the optical axis.

m	1/(2m-1)	z_P [m]	$u_P(\text{peak}) \text{ [W.m}^{-2}]$
1	1.0000	1.000	1.000
2	0.3333	0.333	0.196
3	0.2000	0.200	0.197
4	0.1429	0.143	0.198
5	0.1111	0.111	0.200
6	0.0909	0.0910	0.202
7	0.0769	0.0770	0.205
8	0.0667	0.0667	0.207
9	0.0588	0.0588	0.212
10	0.0526	0.0526	0.217

Energy density variation in XY observation planes

The mscript **op_rs_zones.m** was used to model the variation in the energy density in various XY planes for a Fresnel zone plate. A summary of the parameters used is given in the Matlab Command Window:

```
wavelength [m] = 6.328e-07
nQ = 701000
nP = 1309

Aperture Space
Number of zones = 16
radius of zone plate [m] = 3.182e-03

Observation Space
max radius rP [m] = 1.999e-04
```

focal length of zone plate [m] f1 = 1.000

Energy density at the focal point $z_P = f_1$

The energy density in the focal plane (XY plane) is shown in figure (4) as a function of the perpendicular distance from the optical axis (Z axis) and figure (5) shows scaled images of the diffraction pattern where $z_P = f_1 = 1.00$ m.

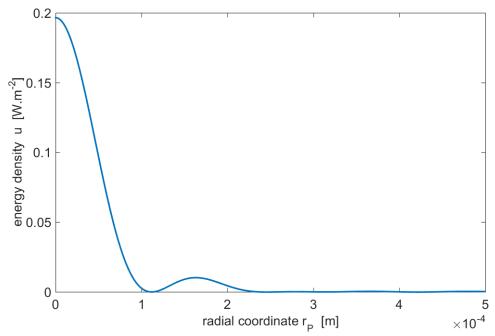


Fig. 4. Energy density variation in a radial direction for the focal plane when $z_P = f_1 = 1.00$ m.

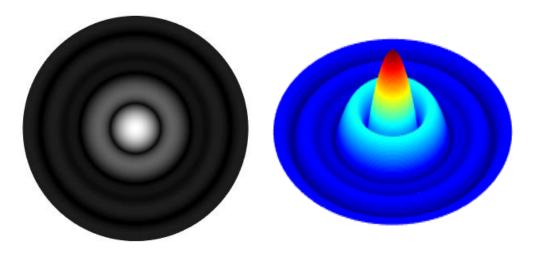


Fig.5. Scaled energy density images of the diffraction pattern in the focal plane when $z_P = f_1 = 1.00$ m.

The energy density in a XY plane where $z_P > f_1$ is shown in figure (6) as a function of the perpendicular distance from the optical axis (Z axis) and figure (7) show scaled images of the diffraction pattern where $f_1 = 1.00$ m and $z_P = 1.10$ m.

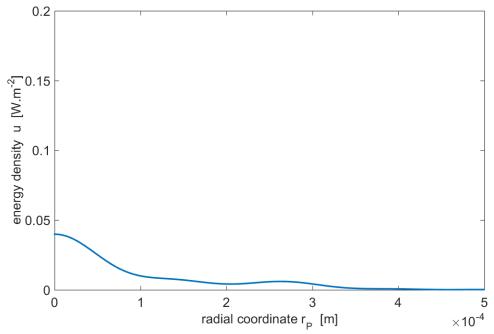


Fig. 6. Energy density variation in a radial direction when $z_P > f_1$, $f_1 = 1.00$ m and $z_P = 1.10$ m.

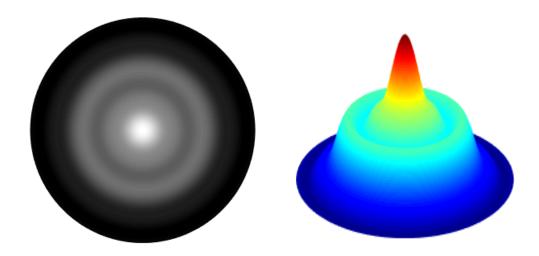


Fig. 7. Scaled energy density images of the diffraction pattern in the focal plane when $z_P > f_1$, $f_1 = 1.00$ m and $z_P = 1.10$ m.

The energy density in a XY plane where $z_P < f_1$ is shown in figure (8) as a function of the perpendicular distance from the optical axis (Z axis) and figure (9) show scaled images of the diffraction pattern where $f_1 = 1.00$ m and $z_P = 0.80$ m.

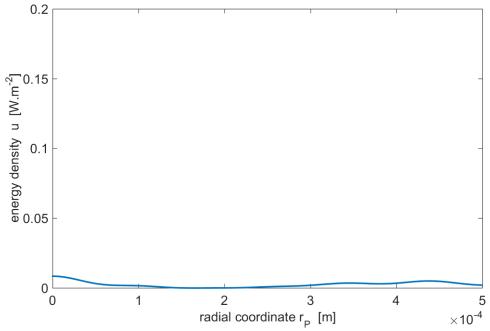


Fig. 8. Energy density variation in a radial direction when $z_P < f_1$, $f_1 = 1.00$ m and $z_P = 0.80$ m.

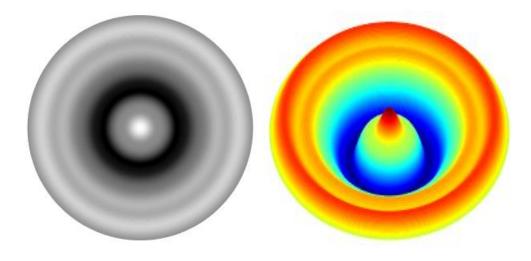


Fig. 9. Scaled energy density images of the diffraction pattern in the focal plane when $z_P < f_1$, $f_1 = 1.00$ m and $z_P = 0.80$ m.

Examination of the above figures clearly demonstrates how the Fresnel zone plate acts as lens. The concentration of the light at the focal point is much greater compared with just a circular aperture without the transparent and opaque zones.

Energy density at the focal point $z_P = f_3 = f_1 / 5$

The energy density in the focal plane (XY plane) is shown in figure (10) as a function of the perpendicular distance from the optical axis (Z axis) and figure (11 shows scaled images of the diffraction pattern where $z_P = f_3 = (1.00 / 5) \text{ m} = 0.200 \text{ m}$.

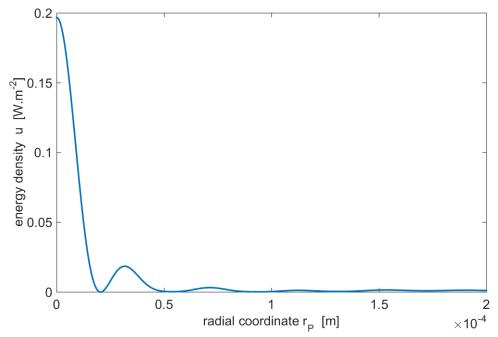


Fig. 10. Energy density variation in a radial direction for the focal plane when $z_P = f_3 = 0.200$ m.

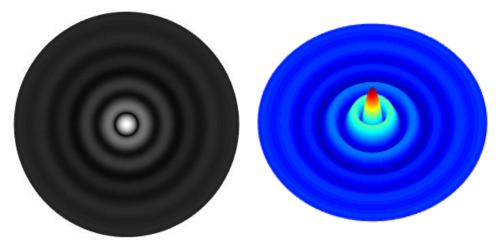


Fig. 11. Scaled energy density images of the diffraction pattern in the focal plane when $z_P = 0.200$ m.

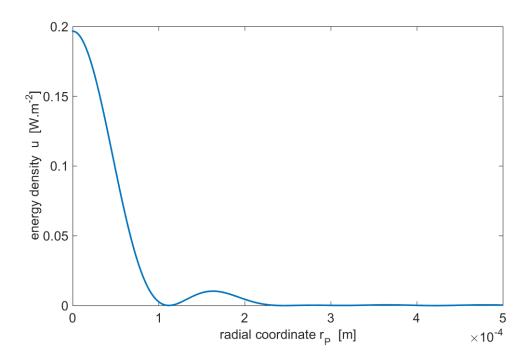


Fig. 4. Energy density variation in a radial direction for the focal plane when $z_P = f_1 = 1.000$ m.

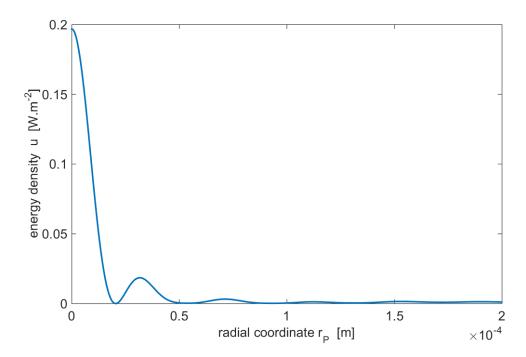


Fig. 10. Energy density variation in a radial direction for the focal plane when $z_P = f_3 = 0.200$ m.

Examination of figures (3), (4) and (10) clearly show that the peaks become narrower as m becomes larger, that is, the closer the peaks are to the aperture the narrow they are.