

Simple Doppler Estimation for MIMO Radar with Co-Located Antennas

I. PROBLEM FORMULATION

Consider a MIMO radar system in which there are N_T transmit antennas and N_R receive antennas, with interelement spacing d and transmission wavelength λ . The received signal at antenna p and time index n due to a moving target located at angle θ with complex reflection coefficient $\beta(\theta)$ can be written as

$$y_p(n) = \beta(\theta) e^{j \frac{2(p-1)\pi d}{\lambda} \sin(\theta)} e^{j 2\pi f_D n} \sum_{q=1}^{N_T} x_q(n) e^{j \frac{2(q-1)\pi d}{\lambda} \sin(\theta)} + w_p(n), \quad (1)$$

where f_D represents the resulting doppler shift caused by the moving target, $x_q(n)$ represents the baseband signal transmitted from antenna q , and $w_p(n)$ is circularly symmetric white Gaussian noise. Assuming the transmitted probing signals are narrowband and that the propagation is nondispersive, the received baseband data vector due to a target at location θ can be described by

$$\mathbf{y}(n) = \beta(\theta) \mathbf{a}_R(\theta) \mathbf{a}_T^T(\theta) \mathbf{x}(n) e^{j 2\pi f_D n} + \mathbf{w}(n), \quad (2)$$

where

$$\mathbf{y}(n) = \begin{bmatrix} y_1(n) & y_2(n) & \dots & y_{N_R}(n) \end{bmatrix}^T, \quad (3)$$

$$\mathbf{x}(n) = \begin{bmatrix} x_1(n) & x_2(n) & \dots & x_{N_T}(n) \end{bmatrix}^T, \quad (4)$$

and

$$\mathbf{w}(n) = \begin{bmatrix} w_1(n) & w_2(n) & \dots & w_{N_R}(n) \end{bmatrix}^T, \quad (5)$$

while

$$\mathbf{a}_T(\theta) = \begin{bmatrix} 1 & e^{j \frac{2\pi d}{\lambda} \sin(\theta)} & \dots & e^{j \frac{2(N_T-1)\pi d}{\lambda} \sin(\theta)} \end{bmatrix}^T \quad (6)$$

and

$$\mathbf{a}_R(\theta) = \begin{bmatrix} 1 & e^{j \frac{2\pi d}{\lambda} \sin(\theta)} & \dots & e^{j \frac{2(N_R-1)\pi d}{\lambda} \sin(\theta)} \end{bmatrix}^T \quad (7)$$

represent the transmit and receive steering vectors, and $(\cdot)^T$ denotes the transpose. The total N samples can be collected into a single matrix

$$\mathbf{Y} = \beta(\theta) \mathbf{A}(\theta) \mathbf{X} \mathbf{D}(f_D) + \mathbf{W}, \quad (8)$$

where

$$\mathbf{A}(\theta) = \mathbf{a}_R(\theta) \mathbf{a}_T^T(\theta), \quad (9)$$

$$\mathbf{X} = \begin{bmatrix} \mathbf{x}(0) & \mathbf{x}(1) & \dots & \mathbf{x}(N-1) \end{bmatrix}, \quad (10)$$

$\mathbf{D}(f_D)$ is the $N \times N$ diagonal matrix whose main diagonal elements consist of the doppler shifts $e^{j2\pi f_D(0:N-1)}$, and \mathbf{W} is the $N_R \times N$ noise matrix. Let the vector of unknown variables be $\psi = [\theta \ f_D]^T$. We vectorize \mathbf{Y} by stacking its columns on top of one another in order to create the received data vector \mathbf{y} . Assuming \mathbf{W} has covariance matrix $\mathbf{C}_\mathbf{W} = \sigma_w^2 \mathbf{I}$, where \mathbf{I} denotes the identity matrix of corresponding dimension, the received signal follows a Gaussian probability density function (pdf) with mean $\mu(\psi) = \text{vec}(\beta(\theta)\mathbf{A}(\theta)\mathbf{X}\mathbf{D}(f_D))$ and covariance matrix $\mathbf{C}_\mathbf{y} = \sigma_w^2 \mathbf{I}$. Let

$$\mathbf{v}(\psi) = \text{vec}(\beta(\theta)\mathbf{A}(\theta)\mathbf{X}\mathbf{D}(f_D)). \quad (11)$$

The log-likelihood function can then be written as

$$\Lambda(\psi) = C - \frac{\sigma_w^2}{2} (\mathbf{y}^H \mathbf{y} - \mathbf{y}^H \mathbf{v}(\theta, f_D) - \mathbf{v}(\theta, f_D)^H \mathbf{y} + \mathbf{v}(\theta, f_D)^H \mathbf{v}(\theta, f_D)), \quad (12)$$

where C is some constant that does not depend on ψ . To find the maximum likelihood (ML) estimate, the log-likelihood function must be maximized with respect to ψ .

$$\hat{\psi} = \arg \max_{\psi} \Lambda(\psi) = \arg \min_{\psi} \mathbf{y}^H \mathbf{y} - \mathbf{y}^H \mathbf{v}(\theta, f_D) - \mathbf{v}(\theta, f_D)^H \mathbf{y} + \mathbf{v}(\theta, f_D)^H \mathbf{v}(\theta, f_D). \quad (13)$$

The first term in the equation does not depend on ψ . The final term is constant with respect to f_D and θ (see Appendix 1 for proof). Thus the estimation simplifies to

$$\hat{\psi} = \arg \max_{\psi} \mathbf{y}^H \mathbf{v}(\theta, f_D) + \mathbf{v}(\theta, f_D)^H \mathbf{y}. \quad (14)$$

The above estimator requires a two-dimensional search over θ and f_D .

II. SIMULATION RESULTS

Simulation results are shown for a uniform linear array with $N_T = N_R = 10$ antennas and half-wavelength interelement spacing at both the transmit and receive side. The angular search is performed over a linear meshgrid of 181 points and the frequency search is performed over a linear meshgrid of 101 points. The frequency is normalized to be between -0.5 and 0.5. Two targets with reflection coefficients equal to unity are placed at 30° and -55° , with $f_D = -0.1$ and $f_D = 0.3$, respectively. Zero-mean circularly symmetric white Gaussian noise with variance $\sigma_w^2 = 0.1$ is added to the received signal. Fig. 1 shows a mesh plot of the magnitude of the resulting location and frequency estimates with data markers placed at the local maxima, where X corresponds to frequency and Y corresponds to location angle. In both cases, the estimator performs perfectly.

III. APPENDIX 1

Proof of independence of f_D, θ for $\mathbf{v}(\theta, f_D)^H \mathbf{v}(\theta, f_D)$.

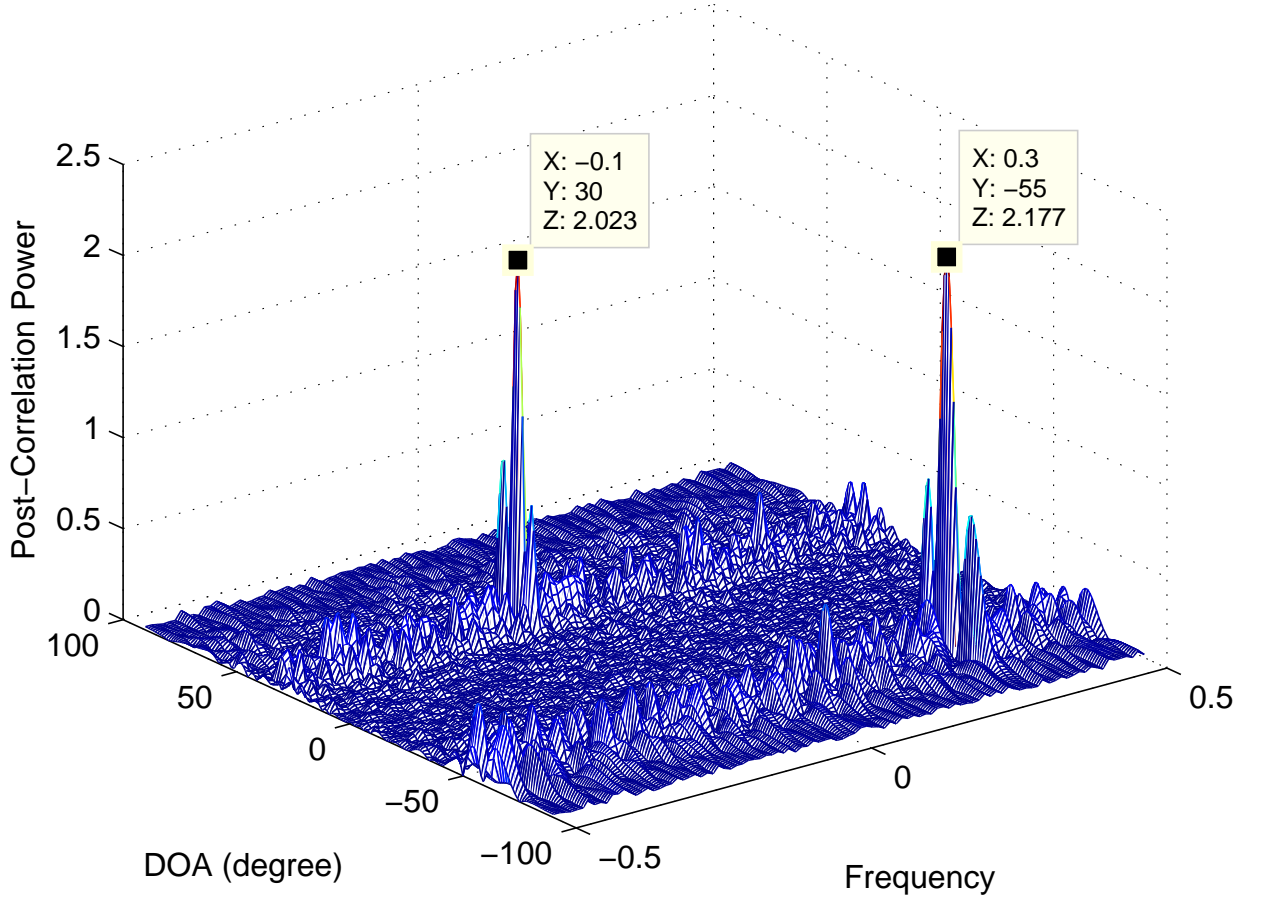


Fig. 1. Location and frequency estimates for two targets where X corresponds to the doppler frequency and Y corresponds to the location angle.

Without any loss of generality, $\beta(\theta)$ is assumed to be unity for compactness. We begin by using the property $\text{vec}(\mathbf{AXB}) = (\mathbf{B}^T \otimes \mathbf{A})\text{vec}(\mathbf{X})$ to rewrite the term as

$$\mathbf{v}(\theta, f_D)^H \mathbf{v}(\theta, f_D) = \text{vec}(\beta(\theta) \mathbf{A}(\theta) \mathbf{X} \mathbf{D}(f_D))^H \text{vec}(\beta(\theta) \mathbf{A}(\theta) \mathbf{X} \mathbf{D}(f_D)) \quad (15)$$

$$= [(\mathbf{D}(f_D) \otimes \mathbf{A}(\theta)) \text{vec}(\mathbf{X})]^H [(\mathbf{D}(f_D) \otimes \mathbf{A}(\theta)) \text{vec}(\mathbf{X})] \quad (16)$$

$$= \text{vec}(\mathbf{X})^H (\mathbf{D}^*(f_D) \otimes \mathbf{A}^H(\theta)) (\mathbf{D}^T(f_D) \otimes \mathbf{A}(\theta)) \text{vec}(\mathbf{X}) \quad (17)$$

$$= \text{vec}(\mathbf{X})^H [(\mathbf{D}^*(f_D) \mathbf{D}^T(f_D)) \otimes (\mathbf{A}^H(\theta) \mathbf{A}(\theta))] \text{vec}(\mathbf{X}) \quad (18)$$

$$= \text{vec}(\mathbf{X})^H [I_{N \times N} \otimes (\mathbf{A}^H(\theta) \mathbf{A}(\theta))] \text{vec}(\mathbf{X}). \quad (19)$$

As seen above, the frequency term cancels out completely. Let $\tilde{\mathbf{A}}(\theta) = \mathbf{A}^H(\theta) \mathbf{A}(\theta)$. It can be easily shown that the diagonal elements of $\tilde{\mathbf{A}}(\theta)$ are constants equal to N_T . Note that due to the orthogonal signaling, we have

$\mathbf{E} \{x_{ij}^* x_{kl}\} = 1$ for $i = k$ and $j = l$, and zero otherwise. Expansion of the above product under expectation yields zeros everywhere except at the diagonal elements of $\tilde{\mathbf{A}}(\theta)$. The resulting product is therefore a constant equal to $N_T^2 \times N$.