

Heating Process

① Total Mass Balance:

$$\frac{dM}{dt} = \dot{m}_{in} - \dot{m}_{out} ; \quad M = \rho \cdot V$$

$$\dot{m} = \rho \cdot F$$

$$\frac{d(\rho V)}{dt} = \frac{\rho dV}{dt} = \rho F_{in} - \rho F_{out}$$

$$\frac{dV}{dt} = F_{in} - F_{out} ; \text{ Volume is controlled}$$

$\Rightarrow V \text{ is constant}$

$$0 = F_{in} - F_{out} \Rightarrow F_{in} = F_{out}$$

Energy Balance: $H = m C_p T = \rho V C_p T$

$$\frac{dH}{dt} = \dot{H}_{in} - \dot{H}_{out} + Q$$

$$\frac{d(m C_p T)}{dt} = \dot{m}_{in} C_p T_{in} - \dot{m}_{out} C_p T_{out} + Q$$

$$m C_p \frac{dT_{out}}{dt} = \rho F_{in} C_p T_{in} - \rho F_{out} C_p T_{out} + Q ; F_{in} = F_{out}$$

$$\rho V C_p \frac{dT_{out}}{dt} = \rho C_p F_{in} (T_{in} - T_{out}) + Q ; m = \rho V$$

$$V \frac{dT_{out}}{dt} = F_{in} (T_{in} - T_{out}) + \frac{Q}{\rho C_p}$$

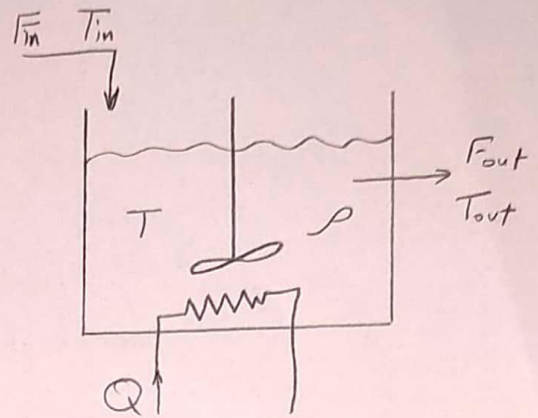
$$V \frac{dT_{out}}{dt} + F_{in} T_{out} = F_{in} T_{in} + \frac{Q}{\rho C_p}$$

$$\underbrace{\left(\frac{V}{F_{in}} \right)}_T \frac{dT_{out}}{dt} + T_{out} = \underbrace{\frac{1 \cdot T_{in}}{K_{P1}}}_{K_{P1}} + \underbrace{\left(\frac{1}{F_{in} \rho C_p} \right)}_{K_{P2}} Q$$

$$T \frac{dT_{out}}{dt} + T_{out} = K_{P1} T_{in} + K_{P2} Q$$

Time
constant

State
constant



F_{in} : Input flow rate

F_{out} : Output flow rate

T_{in} : Input Temperature

T_{out} : Output Temperature

C_p : Heat Capacity Factor, const

Q : Manipulated Heat Rate

The system is isolated

\Rightarrow No heat losses

$$T = \frac{V}{F_{in}} , K_{P1} = 1$$

$$K_{P2} = \frac{1}{F_{in} \rho C_p}$$

$$V \frac{dT}{dt} = \bar{F}_{in} (\bar{T}_{in} - \bar{T}_{out}) + \frac{Q}{\rho C_p} \text{ Manipulated}$$

steady state

$$0 = \bar{F}_{in} (\bar{T}_{in} - \bar{T}_{out}) + \frac{\bar{Q}}{\rho C_p}$$

$$\bar{F}_{in} (\bar{T}_{out} - \bar{T}_{in}) = \frac{\bar{Q}}{\rho C_p}$$

$$\bar{T}_{out} = \frac{\bar{Q}}{\bar{F}_{in} \rho C_p} + \bar{T}_{in}$$

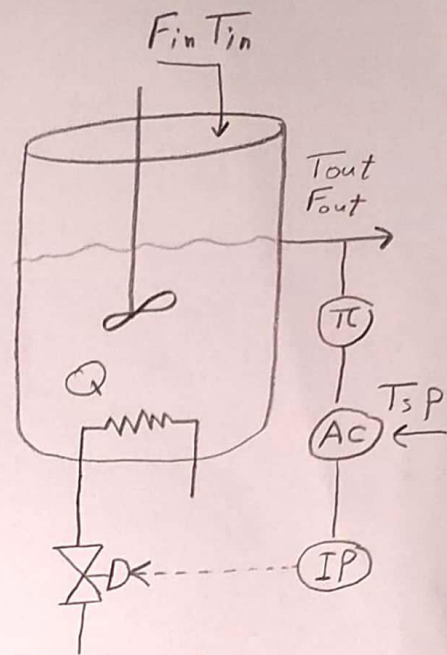
$$\frac{1}{\bar{F}_{in} \rho C_p} = 0.05 \frac{^\circ\text{C}}{\text{min}} \frac{\text{min}}{\text{Kcal}}$$

$$\bar{Q} = 1200 \frac{\text{Kcal}}{\text{min}}$$

$$\bar{T}_{in} = 30^\circ\text{C}$$

$$\bar{T}_{out} = 1200 \frac{\text{Kcal}}{\text{min}} \cdot 0.05 \frac{^\circ\text{C}}{\text{min}} \frac{\text{min}}{\text{Kcal}} + 30^\circ\text{C}$$

$$\bar{T}_{out} = 90^\circ\text{C}$$



Q manipulated variable

T controlled variable

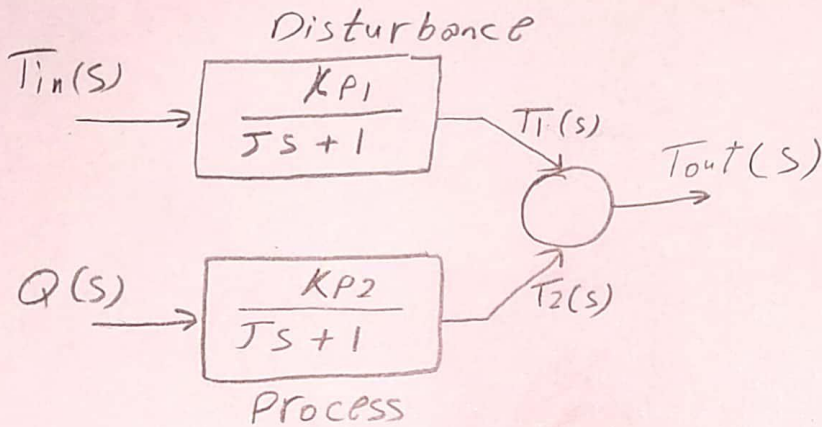
Laplace initial condition 'zero'

$$\tau S T_{out}(s) + T_{out}(s) = K_{P1} T_{in}(s) + K_{P2} Q(s)$$

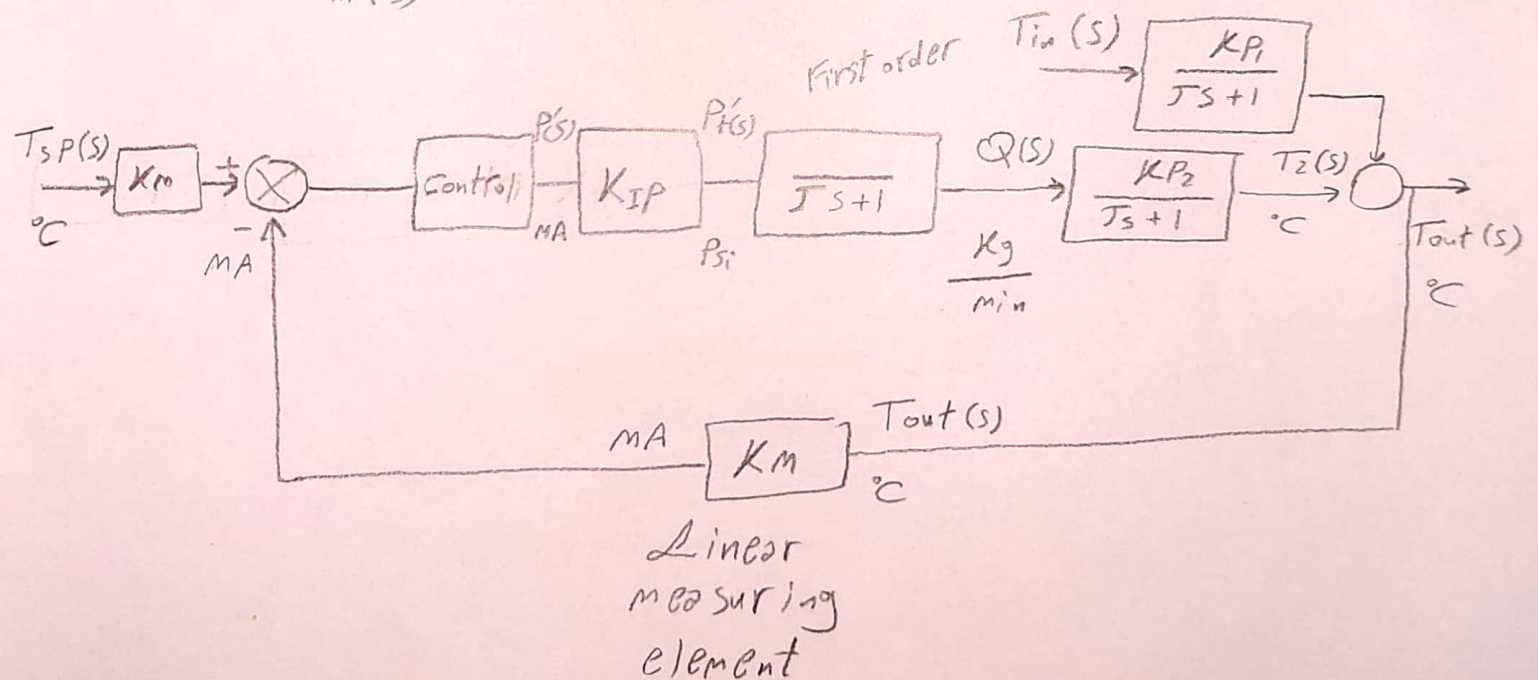
$$(\tau S + 1) T_{out}(s) = K_{P1} T_{in}(s) + K_{P2} Q(s)$$

$$T_{out}(s) = \frac{K_{P1}}{\tau S + 1} T_{in}(s) + \frac{K_{P2}}{\tau S + 1} Q(s) \rightarrow \text{manipulated}$$

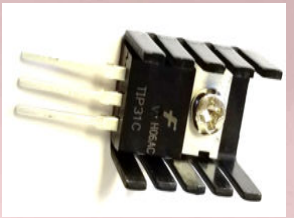
Super Position



$$G_d(s) = \frac{T_1(s)}{T_{in}(s)} = \frac{K_{P1}}{\tau S + 1}, \quad G_P(s) = \frac{T_2(s)}{Q(s)} = \frac{K_{P2}}{\tau S + 1}$$



Enthalpy $H = m C_p T$



Total Energy Balance = $\dot{H}_{in} - \dot{H}_{out} + Q$

$$m C_p \frac{dT}{dt} = \underbrace{UA(T_{\infty} - T)}_{\text{Convection}} + \underbrace{E \sigma (T_{\infty}^4 - T^4)}_{\text{Radiation}} + \underbrace{Q}_{\text{Heater}}$$

if we ignore Radiation:

$$m C_p \frac{dT}{dt} = UA(T_{\infty} - T) + Q \quad \text{First order differential equation}$$

$$m C_p \frac{dT}{dt} + UA T = UA T_{\infty} + Q$$

$$\frac{m C_p}{UA} \frac{dT}{dt} + T = T_{\infty} + \frac{1}{UA} Q \rightarrow$$

$$T_P \frac{dT}{dt} + T = T_{\infty} + K_P Q$$

$$T_P: \text{Time Constant} = \frac{m C_p}{UA}$$

$$K_P: \text{Process gain} = \frac{1}{UA}$$

Place, initial condition 'zero'

$$T_P S T(s) = T_{\infty}(s) + K_P Q(s)$$

$$T(s) = \frac{1}{T_P S + 1} T_{\infty}(s) + \frac{K_P}{T_P S + 1} Q(s) \quad \text{Linear model}$$

$$T(s) = T_{\infty} + \frac{K_P}{T_P S + 1} Q(s)$$

$$\text{using } * \frac{dT}{dt} = \frac{UA(T_{\infty} - T) + Q}{m C_p} \quad \text{first order differential equation}$$

H: Enthalpy M: mass of transistor

Cp: Heat Capacity factor

T: Temperature of transistor

T_∞: ambient temperature

E: Emissivity

σ: Stefan Boltzman constant

A: surface area

U: overall heat transfer coefficient

Q: Heat output

α: factor of the heater

(0-100%)

(0-1)

$$M = 0,001 \text{ Kg}$$

$$C_p = 4900 \frac{\text{J}}{\text{Kg} \cdot \text{K}}$$

$$u = 200 \frac{\text{W}}{\text{m}^2 \cdot \text{K}}$$

$$A = \frac{2}{100^2} \text{ m}^2$$

$$T_p = \frac{(0,001 \text{ Kg}) (4900 \frac{\text{J}}{\text{Kg} \cdot \text{K}})}{(200 \frac{\text{W}}{\text{m}^2 \cdot \text{K}}) (0,0002 \text{ m}^2)}$$

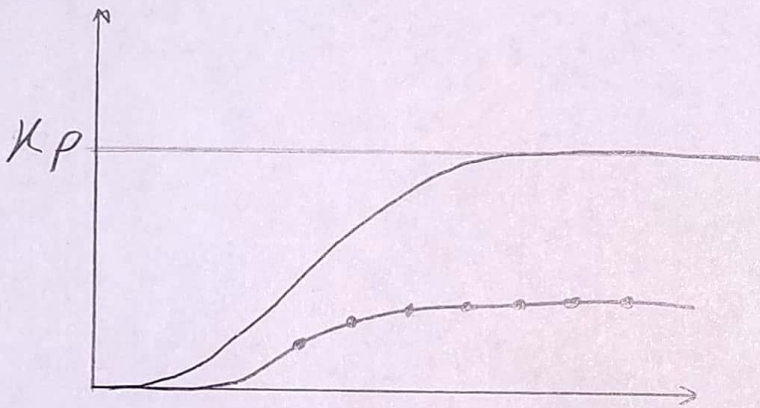
$$T_p = 122,5 \frac{\text{J}}{\text{W}}$$

$$T_p = 122,5 \text{ s} ; [W] = \left[\frac{\text{J}}{\text{s}} \right]$$

FO PDT to an SKP input

$$T(s) = \frac{K_p e^{-\theta_p s}}{T_p s + 1}$$

θ_p Process dead time



The method approximate high order models to first order model + dead time.

→ Comparing measured response and the interpolated answer.