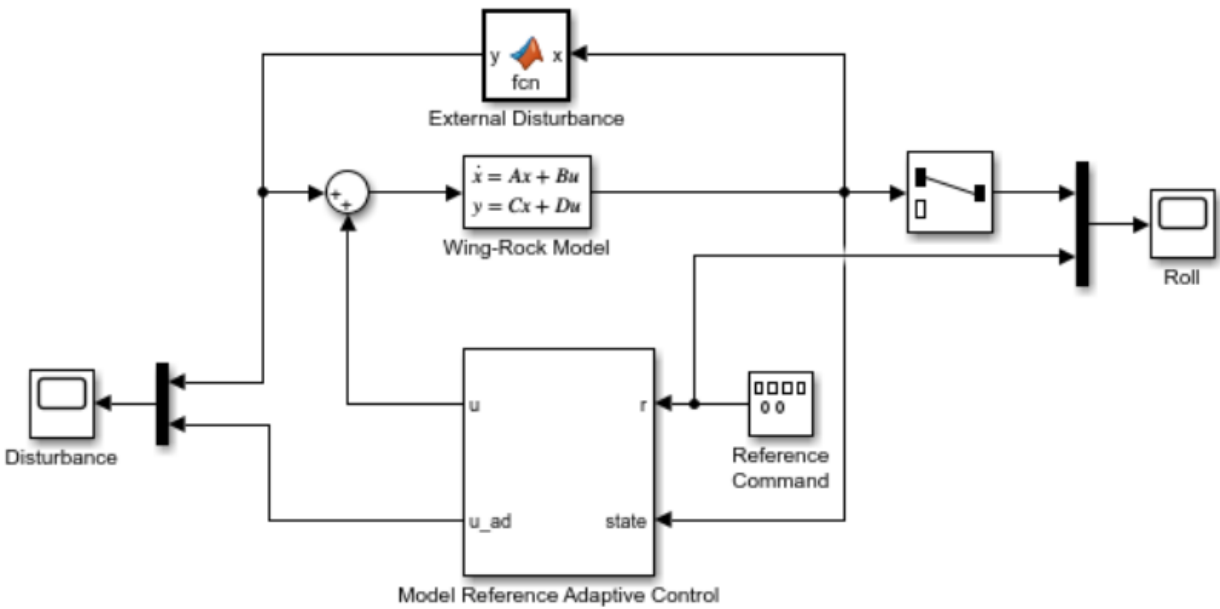
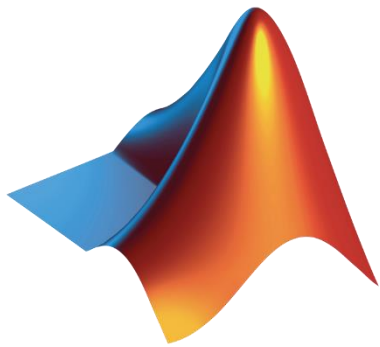
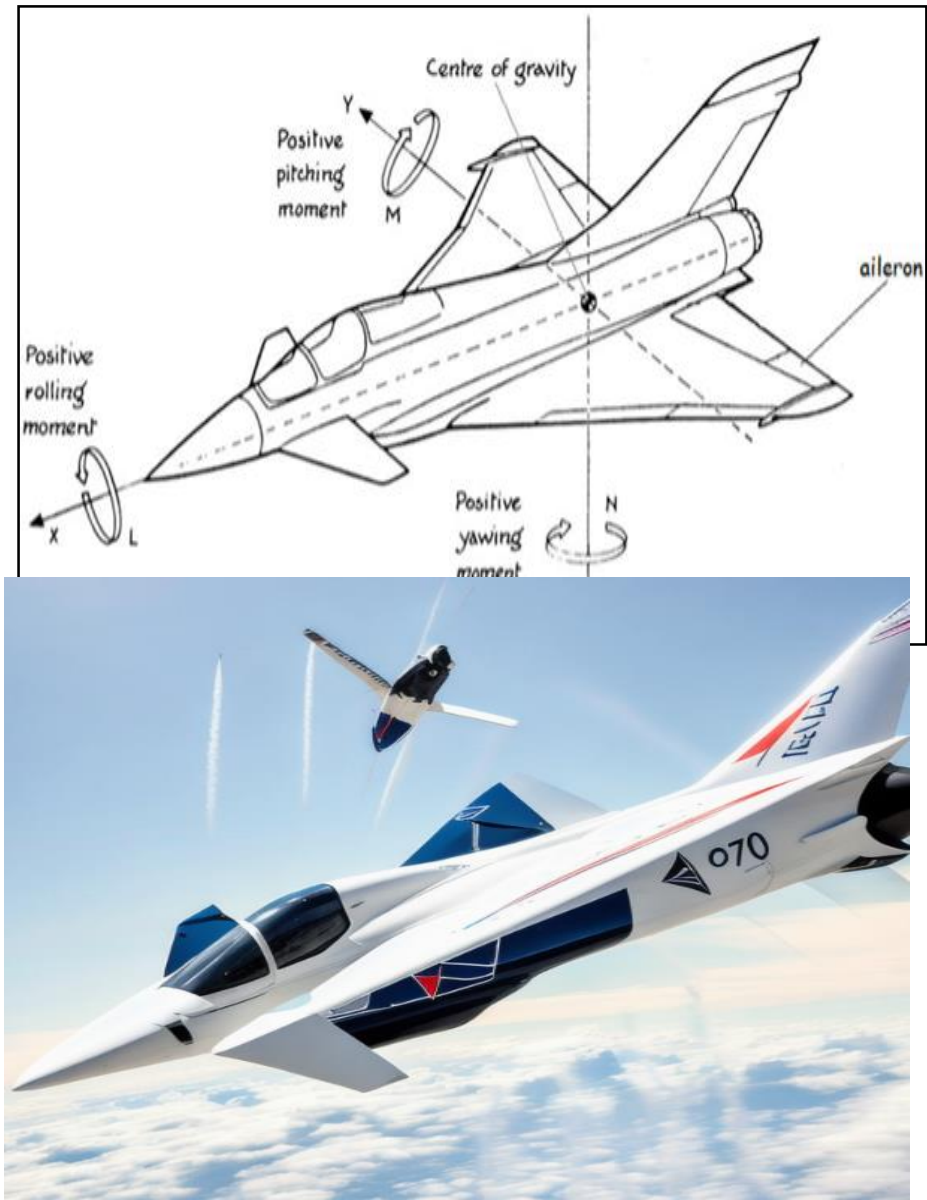


Data-Driven Control

Model Reference Adaptive Control (MRAC)



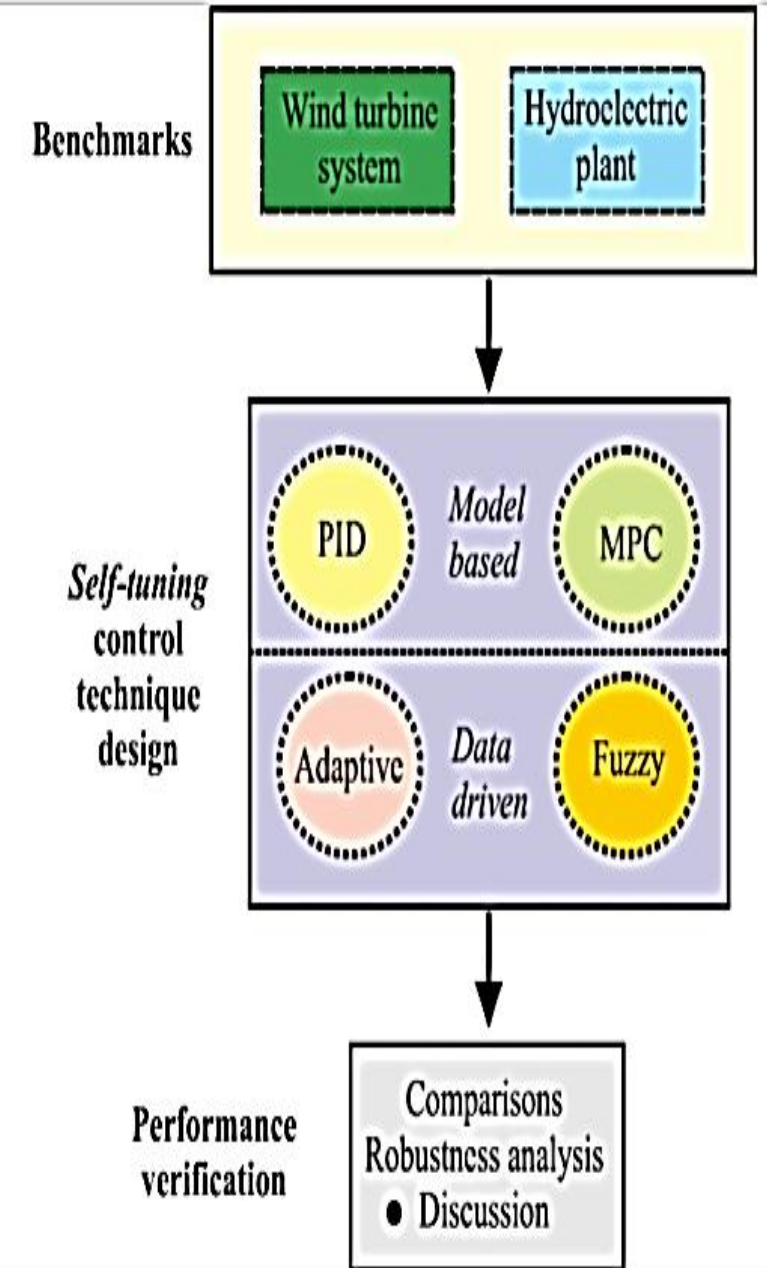
Working with:

1. Introduction Presentation
2. Introduction System Modeling (a Live Script)

Data-driven Control Systems

A control systems in which the identification of the process model and/or the design of the controller are based entirely on experimental data collected from the plant.

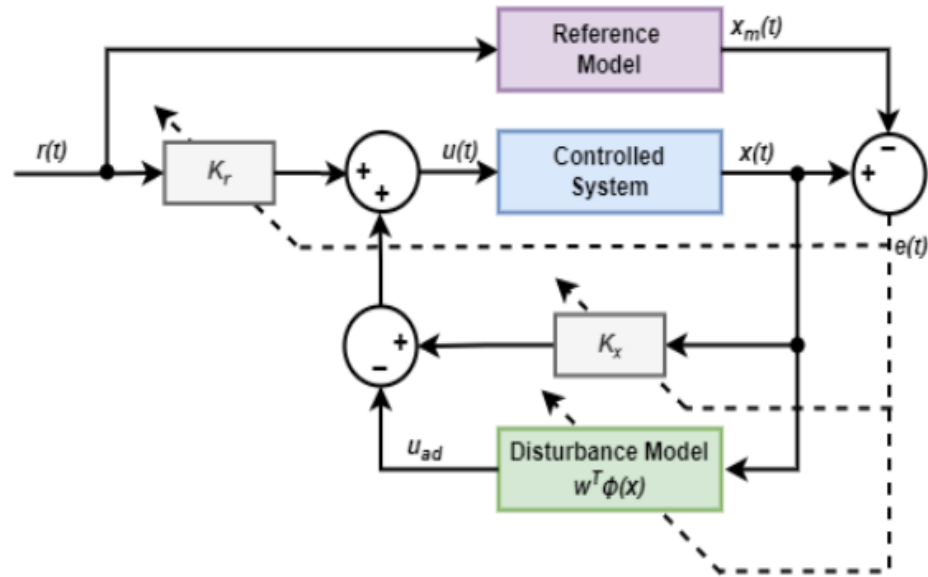
- It is difficult to find a simple reliable model for a physical system and control specifications.
- Direct data-driven methods allow to tune a controller without an identified model of the system.
- It can also simply weight process dynamics of interest inside a cost function, and exclude those dynamics that are out of interest.



Model Reference Adaptive Control (MRAC)

Direct MRAC

A direct MRAC controller has the following control structure.



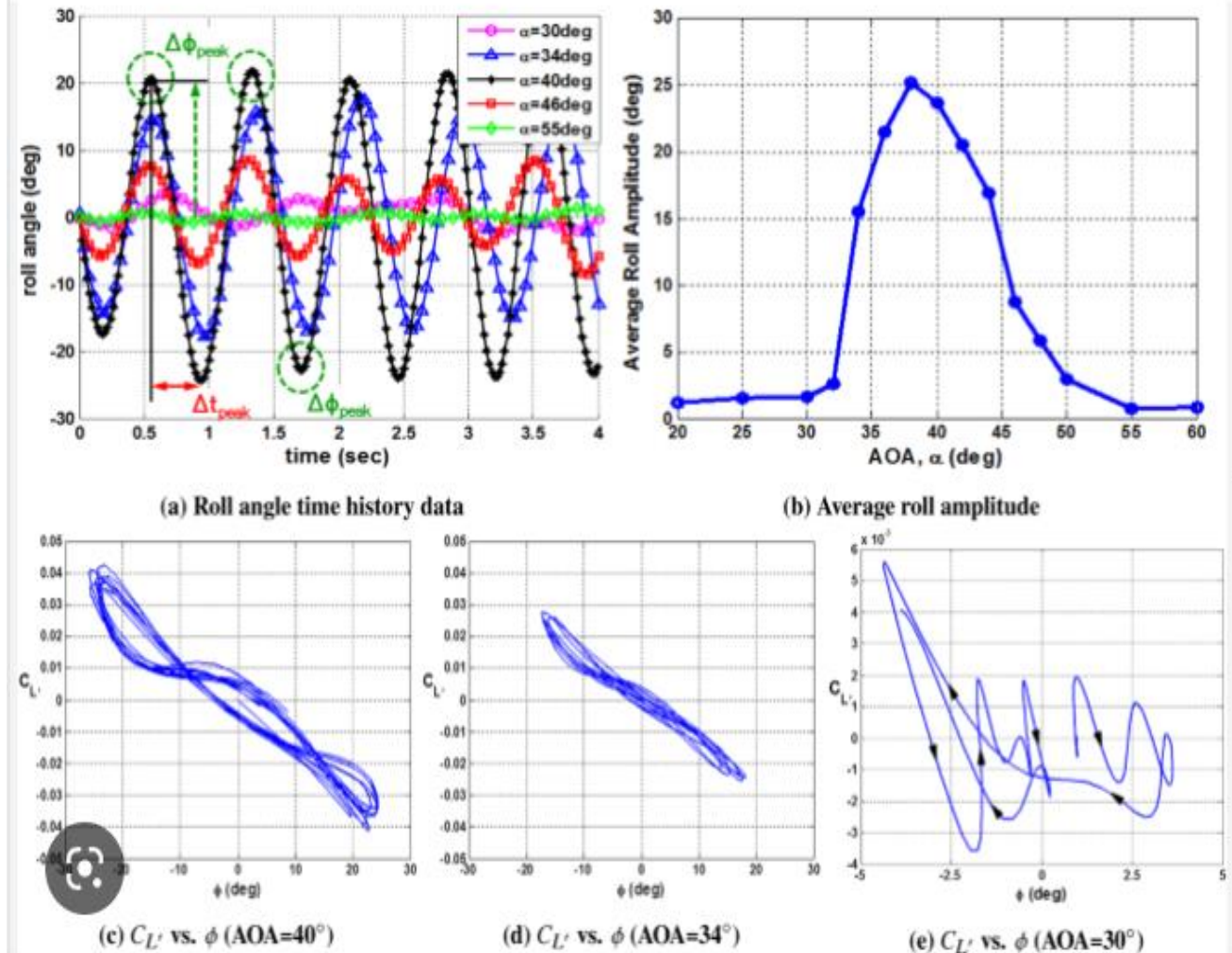
Roll angle



Aircraft Undergoing Wing Rock

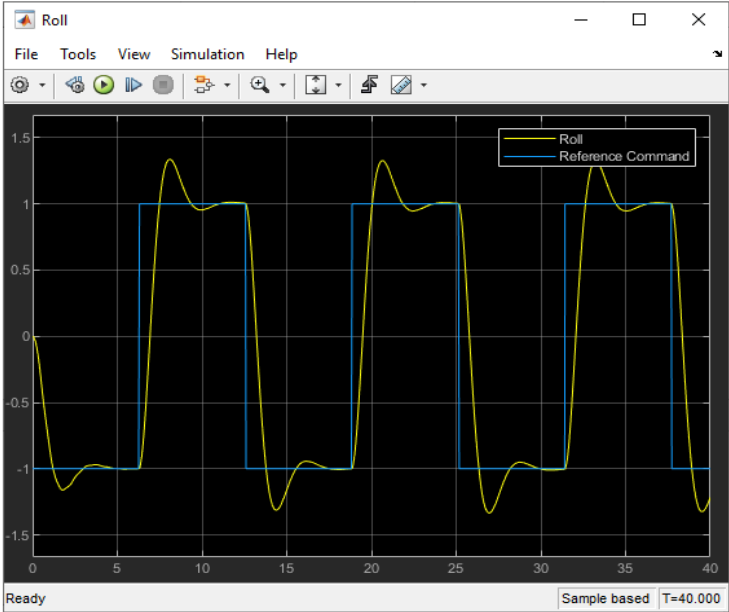
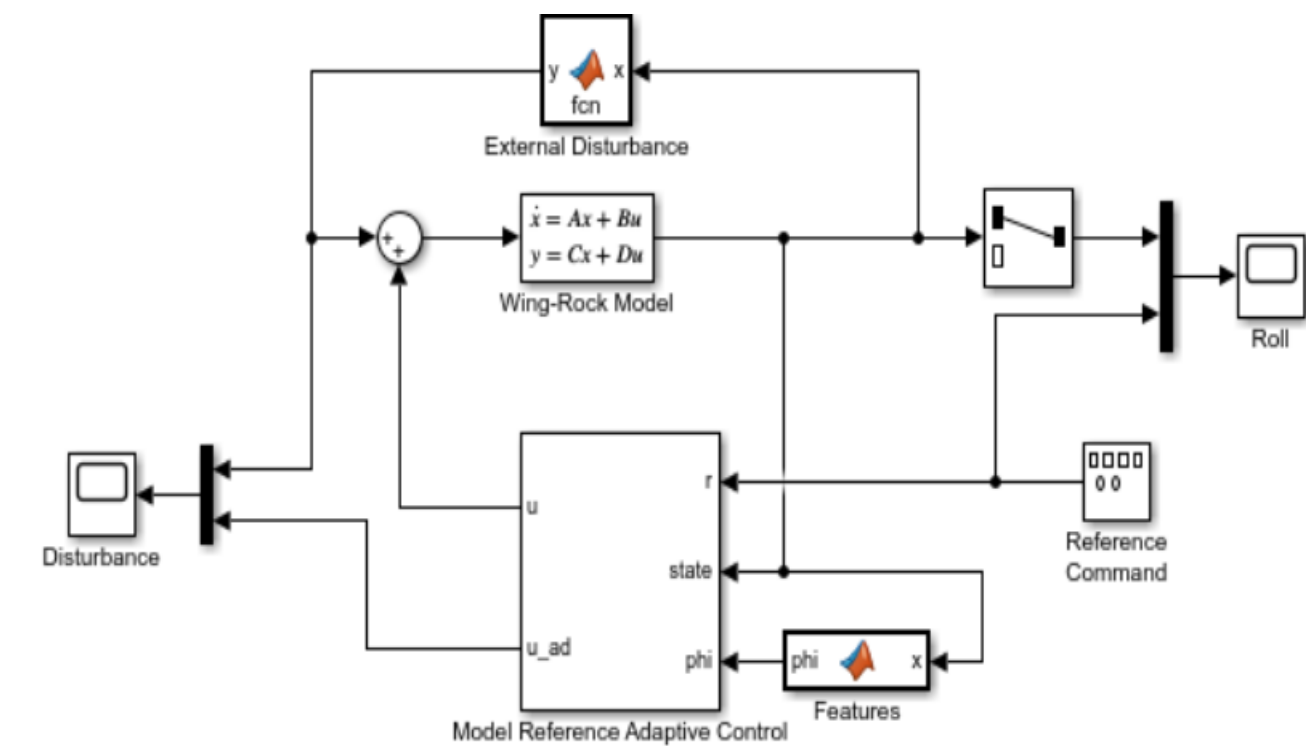
Wing-Rock Control System

Wing rock is a phenomenon observed in delta wing aircraft flying at low speeds and high angles of attack. The aircraft experiences undesired roll oscillations that make the aircraft more difficult for the pilot to control. The goal of the MRAC controller is to cancel the undesired roll oscillation. You can then design a baseline controller to achieve the desired reference behaviour.



rolling moment coefficients vs Angle Of Attack

Model Reference Adaptive Control (MRAC)

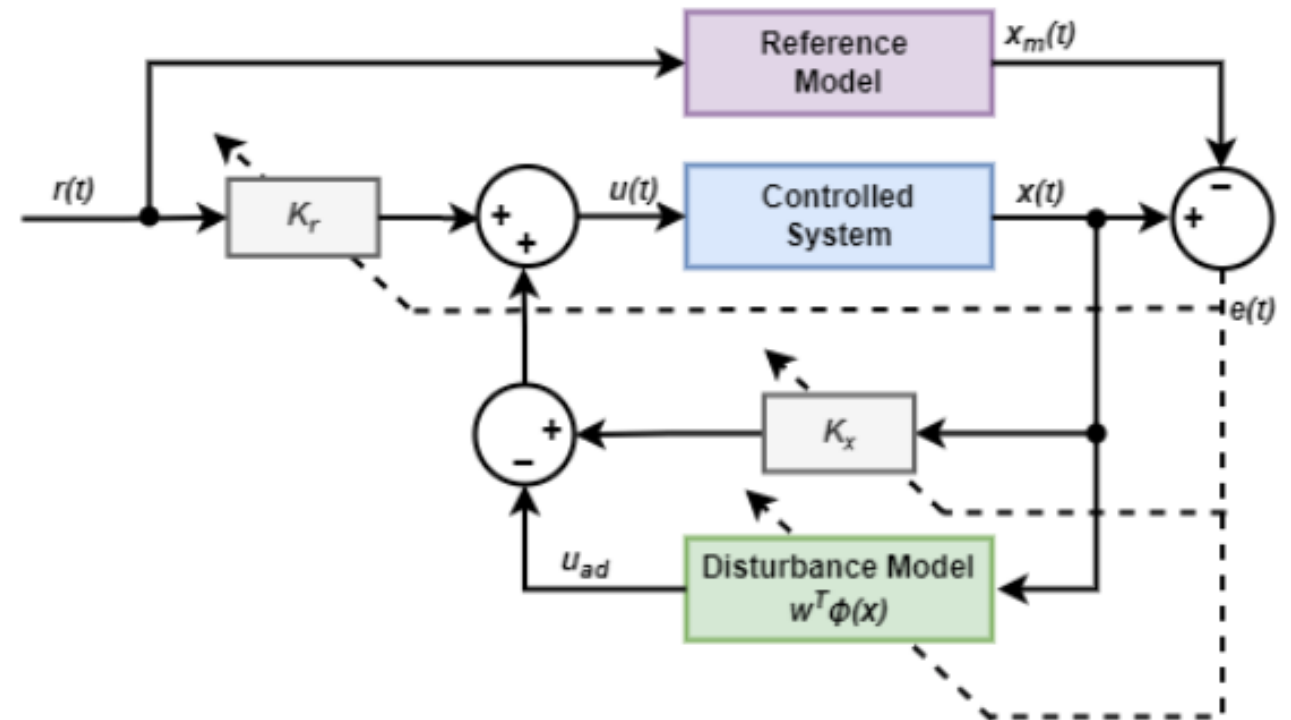


Model Reference Adaptive Control (MRAC) computes control actions to make an uncertain controlled system track the behavior of a given reference plant model.

Direct MRAC — Estimate the feedback and feedforward controller gains based on the real-time tracking error between the states of the reference plant model and the controlled system.

Direct MRAC

A direct MRAC controller has the following control structure.



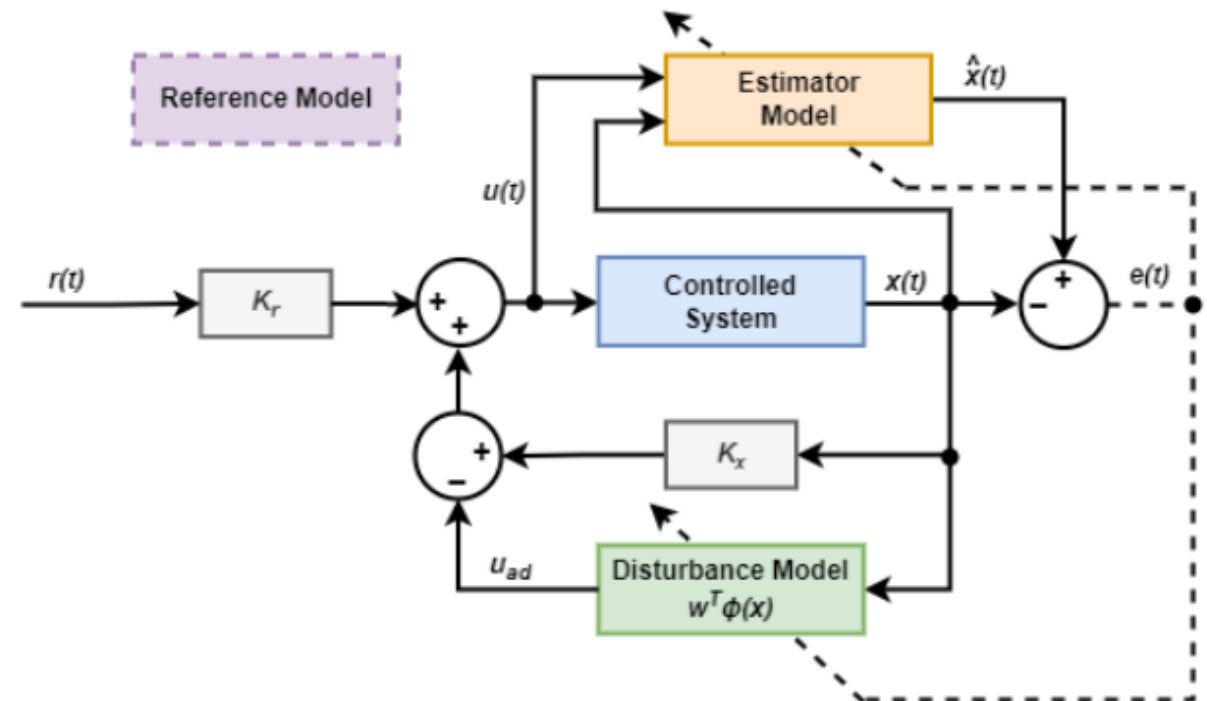
The controller updates the estimated parameters and disturbance model in real-time based on the tracking error.

Indirect MRAC — Estimate the parameters of the controlled system based on the tracking error between the states of the reference plant model and the estimated system. Then, derive the feedback and feedforward controller gains based on the parameters of the estimated system and the reference model.

The controller updates the estimated parameters and disturbance model in real-time based on the tracking error.

Indirect MRAC

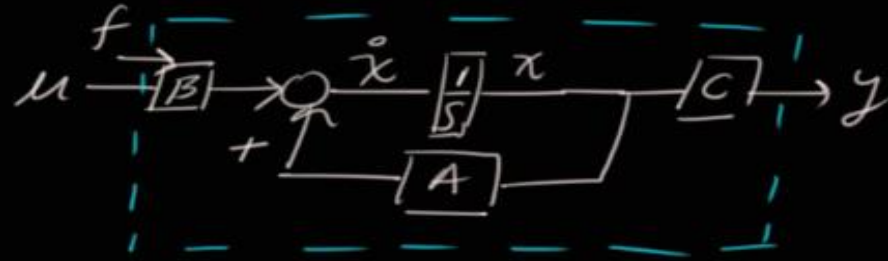
An indirect MRAC controller has the following control structure. The reference model is



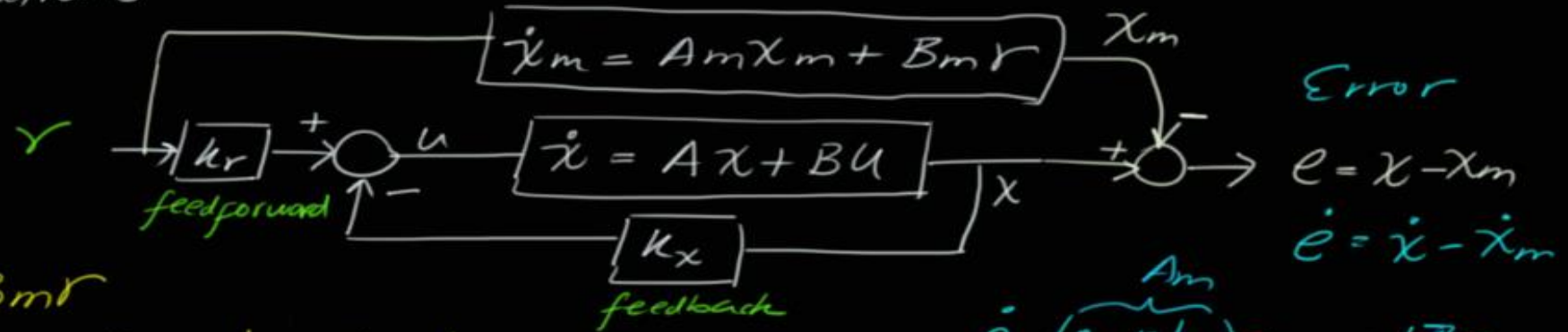
System $\dot{x} = Ax + Bu$

- + Disturbance
- Environmental Changes
- Changes Dynamics
- Changes Parameters
- System Uncertainties
- No modelled dynamics

→ $\dot{x} = Ax + B(u + f)$



Control that
Adapts to variations



$\dot{x}_m = A_m x_m + B_m r$

$\dot{x} = Ax + Bu$; $u = k_r r - k_x x$

$\dot{x} = Ax + B(k_r r - k_x x) = \underbrace{(A - Bk_x)}_{A_m} x + \underbrace{Bk_r}_{B_m} r$

Model Matching

Pole placement

$A_m = A - Bk_x$

$B_m = Bk_r$

$\dot{e} = \overbrace{(A - Bk_x)}^{A_m} x + Bk_r r - A_m x_m - B_m r$

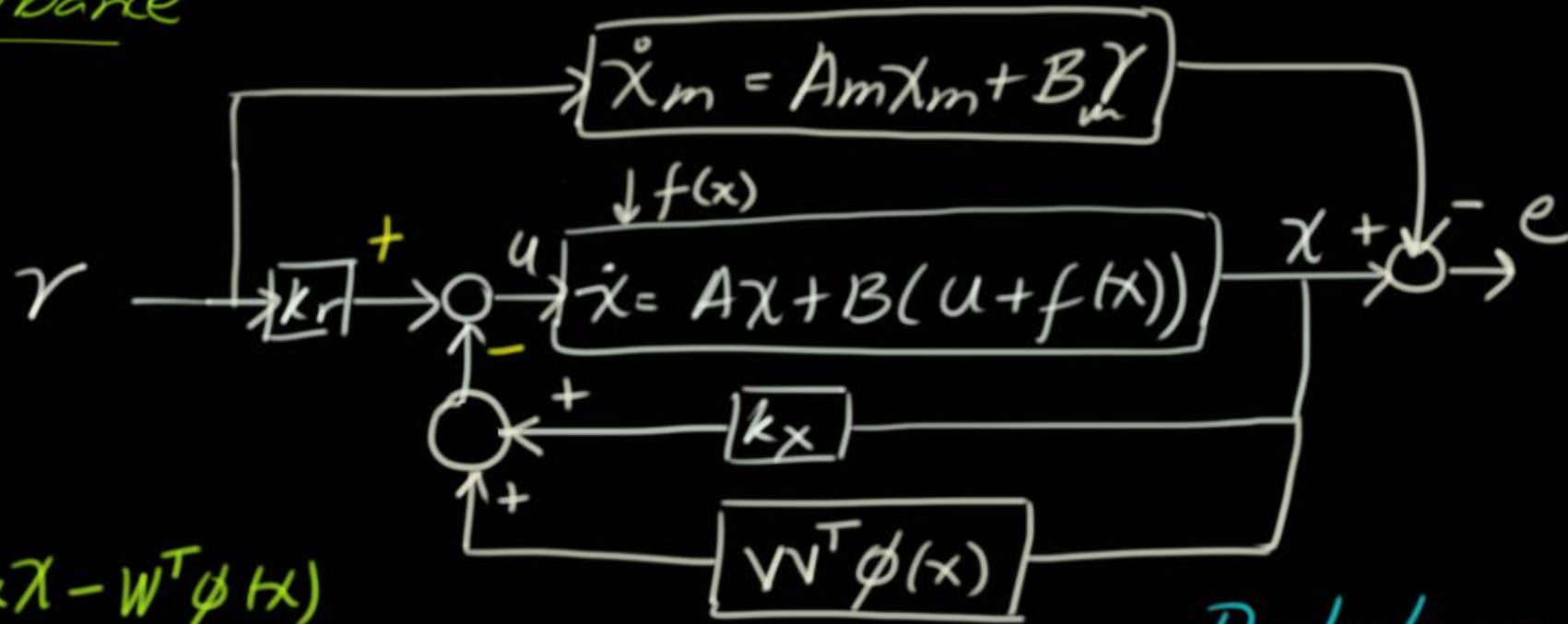
$\dot{e} = A_m x - A_m x_m$

$\dot{e} = A_m (x - x_m)$

$= A_m e$ *stable!*

$e = \lim_{t \rightarrow \infty} (A_m e) \approx 0$

With Disturbance



$$u = k_r r - k_x x - W^T \phi(x)$$

$$\dot{x} = A x + B(k_r r - k_x x - \underbrace{W^T \phi(x)}_{\text{Disturbance compensation}} + \underbrace{f(x)}_{\text{Disturbance}})$$

Disturbance compensation

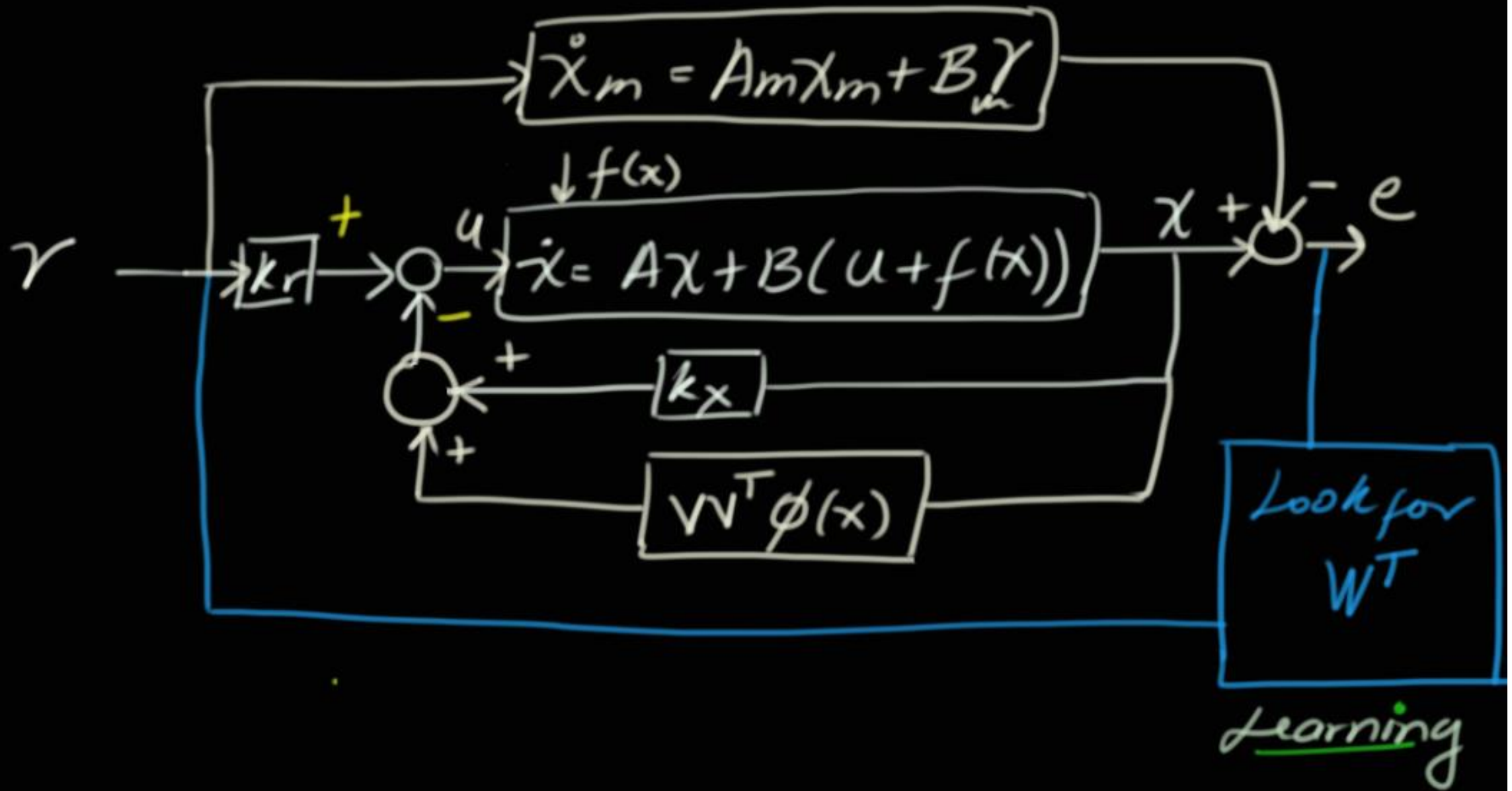
$$W^T \phi(x) = f(x)$$

$$\downarrow$$

$$\dot{x} = A x + B(k_r r - k_x x) \checkmark$$

$W^T \phi(x)$ → Set of basic functions

A weighting vector



1) We know the $f(x)$ can be represented using $x \rightarrow$ System States

θ , $\dot{\theta} = p$ system states. $\rightarrow f(x) = 1 + 2\theta + 3p + 4|\theta|\theta + 1|p|p + 2\theta^3$

$W_T \phi(x)$

$\phi(x) = [1, \theta, p, |\theta|\theta, |p|p, \theta^3]$

$W_T = [1; 2; 3; 4; 1; 2]$

2) Use some of the states as features

$\rightarrow \phi(x) = [1 \ \theta \ p \ |\theta|]$

$W_T = [\dots] ?$

3) Use Sum of Gaussians 

Nominal Model

→ Second Order model $\ddot{x}(t) = u(t) \rightarrow s^2 X(s) = U(s)$



Roll state vector
 $x = \begin{bmatrix} x \\ \dot{x} \end{bmatrix} = \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} \theta \\ p \end{bmatrix}$ Second order integrator

$$\frac{U(s)}{X(s)} = \frac{1}{s^2}$$

$$\dot{x} = \underbrace{\begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}}_A \begin{bmatrix} x \\ \dot{x} \end{bmatrix} + \underbrace{\begin{bmatrix} 0 \\ 1 \end{bmatrix}}_B u \quad \text{State equation}$$

$$y = \underbrace{\begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}}_C \begin{bmatrix} x \\ \dot{x} \end{bmatrix} + \underbrace{\begin{bmatrix} 0 \\ 0 \end{bmatrix}}_D u \quad \text{Output equation}$$

Reference Model → stable second order model

$$\ddot{x}_m = -4x_m - 2\dot{x}_m + 4r$$

x_m Reference model state vector

r Roll reference given by the pilot

$$x_m = \begin{bmatrix} x_m \\ \dot{x}_m \end{bmatrix}; \quad \begin{bmatrix} \dot{x}_m \\ \ddot{x}_m \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -4 & -2 \end{bmatrix} \begin{bmatrix} x_m \\ \dot{x}_m \end{bmatrix} + \begin{bmatrix} 0 \\ 4 \end{bmatrix} r(t)$$

Pole placement

Model Matching

$$\textcircled{1} \quad A_m = A - Bk_x$$

$$\textcircled{2} \quad B_m = Bk_r$$

$$\textcircled{1} \quad \begin{bmatrix} 0 & 1 \\ -4 & -2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} - \begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} k_{x1} & k_{x2} \end{bmatrix}$$

$$\begin{bmatrix} 0 & 1 \\ -4 & -2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} - \begin{bmatrix} 0 & 0 \\ k_{x1} & k_{x2} \end{bmatrix}$$

feedback gains

$$\begin{aligned} -4 &= -k_{x1} \\ -2 &= -k_{x2} \end{aligned} \quad \left\{ \begin{aligned} k_{x1} &= 4 \\ k_{x2} &= 2 \end{aligned} \right.$$

$$\textcircled{2} \quad \begin{bmatrix} 0 \\ 4 \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} k_{r1} \end{bmatrix} \quad \left\{ \begin{aligned} &\text{feedforward gain} \\ 4 &= k_{r1} \end{aligned} \right.$$