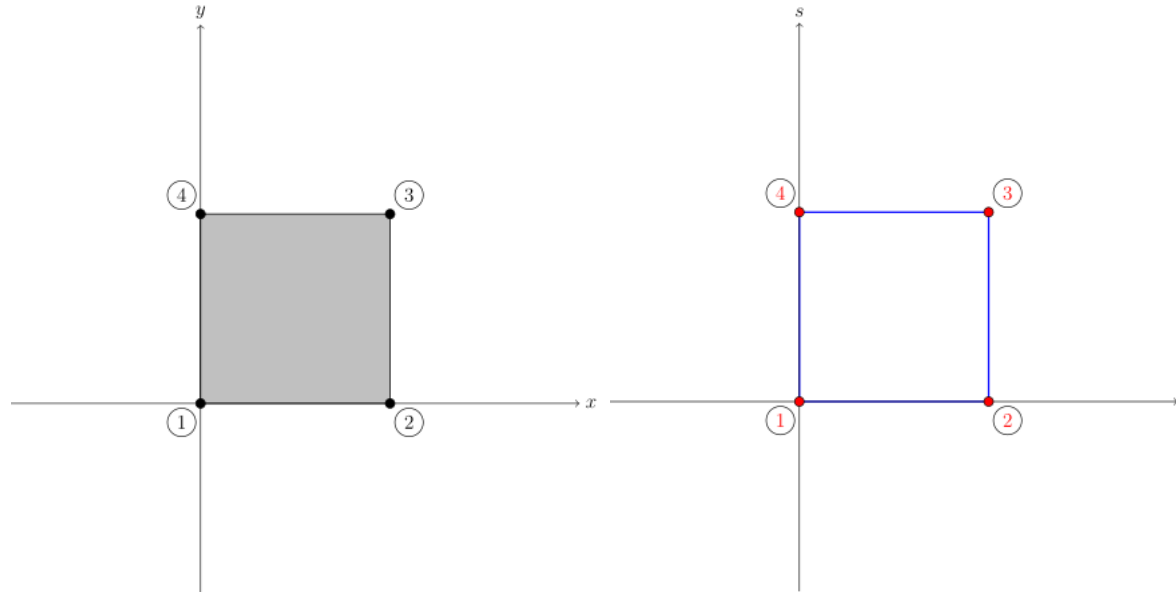


Introducción a elementos finitos

Tarea ? I-2017

Calcular la matriz de rigidez de la placa de acero A36 con dimensiones 250 mm \times 250 mm, espesor 20 mm, coeficiente de Poisson 0.26 y módulo de elasticidad 200 GPa sujeta a esfuerzo plano, usando un elemento en coordenadas naturales



Solución 1

La matriz de rigidez es

$$K = \int_0^1 \int_0^1 B^T C B \det J \, ds \, dr$$

La matriz constitutiva es

$$C = \frac{E}{1 - \nu^2} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & \frac{1-\nu}{2} \end{bmatrix} = \frac{200000}{1 - 0.26^2} \begin{bmatrix} 1 & 0.26 & 0 \\ 0.26 & 1 & 0 \\ 0 & 0 & \frac{1-0.26}{2} \end{bmatrix} = \begin{bmatrix} 214500.214 & 55770.056 & 0 \\ 55770.056 & 214500.214 & 0 \\ 0 & 0 & 79365.079 \end{bmatrix}$$

Coordenadas de los nodos del elemento lagrangiano

$$\begin{aligned}\textcircled{1} &= [r_1, s_1] = [0, 0] & \textcircled{3} &= [r_3, s_3] = [1, 1] \\ \textcircled{2} &= [r_2, s_2] = [1, 0] & \textcircled{4} &= [r_4, s_4] = [0, 1]\end{aligned}$$

Funciones que interpolan los desplazamientos

$$\begin{aligned}N_1 &= \frac{r - r_2}{r_1 - r_2} \cdot \frac{s - s_4}{s_1 - s_4} = \frac{r - 1}{0 - 1} \cdot \frac{s - 1}{0 - 1} = (r - 1)(s - 1) \\ N_2 &= \frac{r - r_1}{r_2 - r_1} \cdot \frac{s - s_3}{s_2 - s_3} = \frac{r - 0}{1 - 0} \cdot \frac{s - 1}{0 - 1} = -r(s - 1) \\ N_3 &= \frac{r - r_4}{r_3 - r_4} \cdot \frac{s - s_2}{s_3 - s_2} = \frac{r - 0}{1 - 0} \cdot \frac{s - 0}{1 - 0} = rs \\ N_4 &= \frac{r - r_3}{r_4 - r_3} \cdot \frac{s - s_1}{s_4 - s_1} = \frac{r - 1}{0 - 1} \cdot \frac{s - 0}{1 - 0} = -s(r - 1)\end{aligned}$$

Escribiendo en la forma matricial

$$N = \begin{bmatrix} (r - 1)(s - 1) & -r(s - 1) & rs & -s(r - 1) \end{bmatrix} = \begin{bmatrix} N_1 & N_2 & N_3 & N_4 \end{bmatrix}$$

Coordenadas de los nodos de la placa

$$\begin{aligned}\textcircled{1} &= [x_1, y_1] = [0, 0] & \textcircled{3} &= [x_3, y_3] = [250, 250] \\ \textcircled{2} &= [x_2, y_2] = [250, 0] & \textcircled{4} &= [x_4, y_4] = [0, 250]\end{aligned}$$

Funciones que interpolan la geometría

$$\begin{aligned}x &= N_1x_1 + N_2x_2 + N_3x_3 + N_4x_4 \\ y &= N_1y_1 + N_2y_2 + N_3y_3 + N_4y_4\end{aligned}$$

Reemplazando las coordenadas de los nodos

$$\begin{aligned}x &= 250r \\ y &= 250s\end{aligned}$$

El jacobiano y el jacobiano inverso son

$$J = \begin{bmatrix} \frac{\partial x}{\partial r} & \frac{\partial y}{\partial r} \\ \frac{\partial x}{\partial s} & \frac{\partial y}{\partial s} \end{bmatrix} \quad J^{-1} = \begin{bmatrix} \frac{\partial r}{\partial x} & \frac{\partial r}{\partial y} \\ \frac{\partial s}{\partial x} & \frac{\partial s}{\partial y} \end{bmatrix}$$

Reemplazando derivadas

$$J = \begin{bmatrix} 250 & 0 \\ 0 & 250 \end{bmatrix} \quad J^{-1} = \begin{bmatrix} \frac{1}{250} & 0 \\ 0 & \frac{1}{250} \end{bmatrix}$$

Determinante del jacobiano

$$\det J = 62500$$

La matriz de deformaciones es

$$B = \begin{bmatrix} \frac{\partial N_1}{\partial x} & 0 & \frac{\partial N_2}{\partial x} & 0 & \frac{\partial N_3}{\partial x} & 0 & \frac{\partial N_4}{\partial x} & 0 \\ 0 & \frac{\partial N_1}{\partial y} & 0 & \frac{\partial N_2}{\partial y} & 0 & \frac{\partial N_3}{\partial y} & 0 & \frac{\partial N_4}{\partial y} \\ \frac{\partial N_1}{\partial y} & \frac{\partial N_1}{\partial x} & \frac{\partial N_2}{\partial y} & \frac{\partial N_2}{\partial x} & \frac{\partial N_3}{\partial y} & \frac{\partial N_3}{\partial x} & \frac{\partial N_4}{\partial y} & \frac{\partial N_4}{\partial x} \end{bmatrix}$$

Debido a que las funciones de forma están en función de r y s , se usará la regla de la cadena

$$\begin{aligned} \frac{\partial N_i}{\partial x} &= \frac{\partial N_i}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_i}{\partial s} \frac{\partial s}{\partial x} \\ \frac{\partial N_i}{\partial y} &= \frac{\partial N_i}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_i}{\partial s} \frac{\partial s}{\partial y} \end{aligned}$$

Reemplazando en B_i

$$\begin{aligned} B_1 &= \begin{bmatrix} \frac{\partial N_1}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_1}{\partial s} \frac{\partial s}{\partial x} & 0 & \frac{\partial N_1}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_1}{\partial s} \frac{\partial s}{\partial y} \\ 0 & \frac{\partial N_1}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_1}{\partial s} \frac{\partial s}{\partial y} & \frac{\partial N_1}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_1}{\partial s} \frac{\partial s}{\partial x} \\ \frac{\partial N_1}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_1}{\partial s} \frac{\partial s}{\partial y} & \frac{\partial N_1}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_1}{\partial s} \frac{\partial s}{\partial x} & \frac{\partial N_1}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_1}{\partial s} \frac{\partial s}{\partial y} \end{bmatrix} = \begin{bmatrix} \frac{s-1}{250} & 0 \\ 0 & \frac{r-1}{250} \\ \frac{r-1}{250} & \frac{s-1}{250} \end{bmatrix} \\ B_2 &= \begin{bmatrix} \frac{\partial N_2}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_2}{\partial s} \frac{\partial s}{\partial x} & 0 & \frac{\partial N_2}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_2}{\partial s} \frac{\partial s}{\partial y} \\ 0 & \frac{\partial N_2}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_2}{\partial s} \frac{\partial s}{\partial y} & \frac{\partial N_2}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_2}{\partial s} \frac{\partial s}{\partial x} \\ \frac{\partial N_2}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_2}{\partial s} \frac{\partial s}{\partial y} & \frac{\partial N_2}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_2}{\partial s} \frac{\partial s}{\partial x} & \frac{\partial N_2}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_2}{\partial s} \frac{\partial s}{\partial y} \end{bmatrix} = \begin{bmatrix} -\frac{s-1}{250} & 0 \\ 0 & -\frac{r}{250} \\ -\frac{r}{250} & -\frac{s-1}{250} \end{bmatrix} \\ B_3 &= \begin{bmatrix} \frac{\partial N_3}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_3}{\partial s} \frac{\partial s}{\partial x} & 0 & \frac{\partial N_3}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_3}{\partial s} \frac{\partial s}{\partial y} \\ 0 & \frac{\partial N_3}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_3}{\partial s} \frac{\partial s}{\partial y} & \frac{\partial N_3}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_3}{\partial s} \frac{\partial s}{\partial x} \\ \frac{\partial N_3}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_3}{\partial s} \frac{\partial s}{\partial y} & \frac{\partial N_3}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_3}{\partial s} \frac{\partial s}{\partial x} & \frac{\partial N_3}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_3}{\partial s} \frac{\partial s}{\partial y} \end{bmatrix} = \begin{bmatrix} \frac{s}{250} & 0 \\ 0 & \frac{r}{250} \\ \frac{r}{250} & \frac{s}{250} \end{bmatrix} \\ B_4 &= \begin{bmatrix} \frac{\partial N_4}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_4}{\partial s} \frac{\partial s}{\partial x} & 0 & \frac{\partial N_4}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_4}{\partial s} \frac{\partial s}{\partial y} \\ 0 & \frac{\partial N_4}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_4}{\partial s} \frac{\partial s}{\partial y} & \frac{\partial N_4}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_4}{\partial s} \frac{\partial s}{\partial x} \\ \frac{\partial N_4}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_4}{\partial s} \frac{\partial s}{\partial y} & \frac{\partial N_4}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial N_4}{\partial s} \frac{\partial s}{\partial x} & \frac{\partial N_4}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial N_4}{\partial s} \frac{\partial s}{\partial y} \end{bmatrix} = \begin{bmatrix} -\frac{s}{250} & 0 \\ 0 & -\frac{r-1}{250} \\ -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix} \end{aligned}$$

Reemplazando en B

$$B = \begin{bmatrix} \frac{s-1}{250} & 0 & -\frac{s-1}{250} & 0 & \frac{s}{250} & 0 & -\frac{s}{250} & 0 \\ 0 & \frac{r-1}{250} & 0 & -\frac{r}{250} & 0 & \frac{r}{250} & 0 & -\frac{r-1}{250} \\ \frac{r-1}{250} & \frac{s-1}{250} & -\frac{r}{250} & -\frac{s-1}{250} & \frac{r}{250} & \frac{s}{250} & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix}$$

Reemplazando en la fórmula de la matriz de rigidez

$$K = \int_0^1 \int_0^1 \begin{bmatrix} \frac{s-1}{250} & 0 & \frac{r-1}{250} \\ 0 & \frac{r-1}{250} & \frac{s-1}{250} \\ -\frac{s-1}{250} & 0 & -\frac{r}{250} \\ 0 & -\frac{r}{250} & -\frac{s-1}{250} \\ \frac{s}{250} & 0 & \frac{r}{250} \\ 0 & \frac{r}{250} & \frac{s}{250} \\ -\frac{s}{250} & 0 & -\frac{r-1}{250} \\ 0 & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix} \begin{bmatrix} 214500.214 & 55770.056 & 0 \\ 55770.056 & 214500.214 & 0 \\ 0 & 0 & 79365.079 \end{bmatrix} \begin{bmatrix} \frac{s-1}{250} & 0 & -\frac{s-1}{250} & 0 & \frac{s}{250} & 0 & -\frac{s}{250} & 0 \\ 0 & \frac{r-1}{250} & 0 & -\frac{r}{250} & 0 & \frac{r}{250} & 0 & -\frac{r-1}{250} \\ \frac{r-1}{250} & \frac{s-1}{250} & -\frac{r}{250} & -\frac{s-1}{250} & \frac{r}{250} & \frac{s}{250} & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix} 62500 \cdot 20 \, ds \, dr$$

Integrando

$$K = \begin{bmatrix} 1959101.959 & 675675.6755 & -1165451.165 & -117975.1180 & -979550.9793 & -675675.6757 & 185900.1856 & 117975.1178 \\ 675675.6755 & 1959101.960 & 117975.1180 & 185900.1852 & -675675.6756 & -979550.9795 & -117975.1181 & -1165451.166 \\ -1165451.165 & 117975.1180 & 1959101.959 & -675675.6755 & 185900.1856 & -117975.1178 & -979550.9793 & 675675.6757 \\ -117975.1180 & 185900.1852 & -675675.6755 & 1959101.960 & 117975.1181 & -1165451.166 & 675675.6756 & -979550.9795 \\ -979550.9796 & -675675.6756 & 185900.1859 & 117975.1181 & 1959101.959 & 675675.6755 & -1165451.165 & -117975.1180 \\ -675675.6757 & -979550.9797 & -117975.1178 & -1165451.165 & 675675.6755 & 1959101.959 & 117975.1180 & 185900.1860 \\ 185900.1859 & -117975.1181 & -979550.9796 & 675675.6756 & -1165451.165 & 117975.1180 & 1959101.959 & -675675.6755 \\ 117975.1178 & -1165451.165 & 675675.6757 & -979550.9797 & -117975.1180 & 185900.1860 & -675675.6755 & 1959101.959 \end{bmatrix}$$

Solución 2

La matriz de rigidez es

$$K = \int_0^1 \int_0^1 B^T C B \det J \, t \, ds \, dr$$

La matriz constitutiva es

$$C = \frac{E}{1-\nu^2} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & \frac{1-\nu}{2} \end{bmatrix} = \frac{200000}{1-0.26^2} \begin{bmatrix} 1 & 0.26 & 0 \\ 0.26 & 1 & 0 \\ 0 & 0 & \frac{1-0.26}{2} \end{bmatrix} = \begin{bmatrix} 214500.214 & 55770.056 & 0 \\ 55770.056 & 214500.214 & 0 \\ 0 & 0 & 79365.079 \end{bmatrix}$$

Coordenadas de los nodos del elemento lagrangiano

$$\begin{aligned} \textcircled{1} &= [r_1, s_1] = [0, 0] & \textcircled{3} &= [r_3, s_3] = [1, 1] \\ \textcircled{2} &= [r_2, s_2] = [1, 0] & \textcircled{4} &= [r_4, s_4] = [0, 1] \end{aligned}$$

Funciones que interpolan los desplazamientos

$$\begin{aligned} N_1 &= \frac{r-r_2}{r_1-r_2} \cdot \frac{s-s_4}{s_1-s_4} = \frac{r-1}{0-1} \cdot \frac{s-1}{0-1} = (r-1)(s-1) \\ N_2 &= \frac{r-r_1}{r_2-r_1} \cdot \frac{s-s_3}{s_2-s_3} = \frac{r-0}{1-0} \cdot \frac{s-1}{0-1} = -r(s-1) \\ N_3 &= \frac{r-r_4}{r_3-r_4} \cdot \frac{s-s_2}{s_3-s_2} = \frac{r-0}{1-0} \cdot \frac{s-0}{1-0} = rs \\ N_4 &= \frac{r-r_3}{r_4-r_3} \cdot \frac{s-s_1}{s_4-s_1} = \frac{r-1}{0-1} \cdot \frac{s-0}{1-0} = -s(r-1) \end{aligned}$$

Escribiendo en la forma matricial

$$N = \begin{bmatrix} (r-1)(s-1) & -r(s-1) & rs & -s(r-1) \end{bmatrix} = \begin{bmatrix} N_1 & N_2 & N_3 & N_4 \end{bmatrix}$$

Coordenadas de los nodos de la placa

$$\begin{aligned} \textcircled{1} &= [x_1, y_1] = [0, 0] & \textcircled{3} &= [x_3, y_3] = [250, 250] \\ \textcircled{2} &= [x_2, y_2] = [250, 0] & \textcircled{4} &= [x_4, y_4] = [0, 250] \end{aligned}$$

Funciones que interpolan la geometría

$$\begin{aligned} x &= N_1x_1 + N_2x_2 + N_3x_3 + N_4x_4 \\ y &= N_1y_1 + N_2y_2 + N_3y_3 + N_4y_4 \end{aligned}$$

Reemplazando las coordenadas de los nodos

$$\begin{aligned} x &= 250r \\ y &= 250s \end{aligned}$$

El jacobiano y el jacobiano inverso son

$$J = \begin{bmatrix} \frac{\partial x}{\partial r} & \frac{\partial y}{\partial r} \\ \frac{\partial x}{\partial s} & \frac{\partial y}{\partial s} \end{bmatrix} \quad J^{-1} = \begin{bmatrix} \frac{\partial r}{\partial x} & \frac{\partial s}{\partial x} \\ \frac{\partial r}{\partial y} & \frac{\partial s}{\partial y} \end{bmatrix}$$

Reemplazando derivadas

$$J = \begin{bmatrix} 250 & 0 \\ 0 & 250 \end{bmatrix} \quad J^{-1} = \begin{bmatrix} \frac{1}{250} & 0 \\ 0 & \frac{1}{250} \end{bmatrix}$$

Determinante del jacobiano

$$\det J = 62500$$

La matriz de deformaciones es

$$B = \begin{bmatrix} \frac{\partial N_1}{\partial x} & 0 & \frac{\partial N_2}{\partial x} & 0 & \frac{\partial N_3}{\partial x} & 0 & \frac{\partial N_4}{\partial x} & 0 \\ 0 & \frac{\partial N_1}{\partial y} & 0 & \frac{\partial N_2}{\partial y} & 0 & \frac{\partial N_3}{\partial y} & 0 & \frac{\partial N_4}{\partial y} \\ \frac{\partial N_1}{\partial y} & \frac{\partial N_1}{\partial x} & \frac{\partial N_2}{\partial y} & \frac{\partial N_2}{\partial x} & \frac{\partial N_3}{\partial y} & \frac{\partial N_3}{\partial x} & \frac{\partial N_4}{\partial y} & \frac{\partial N_4}{\partial x} \end{bmatrix}$$

Las derivadas de las funciones de forma se calcularán en forma matricial

$$\begin{bmatrix} \frac{\partial N_i}{\partial x} \\ \frac{\partial N_i}{\partial y} \end{bmatrix} = J^{-1} \begin{bmatrix} \frac{\partial N_i}{\partial r} \\ \frac{\partial N_i}{\partial s} \end{bmatrix} = \begin{bmatrix} \frac{\partial r}{\partial x} & \frac{\partial s}{\partial x} \\ \frac{\partial r}{\partial y} & \frac{\partial s}{\partial y} \end{bmatrix} \begin{bmatrix} \frac{\partial N_i}{\partial r} \\ \frac{\partial N_i}{\partial s} \end{bmatrix}$$

Reemplazando en N_i

$$\begin{aligned} \begin{bmatrix} \frac{\partial N_1}{\partial x} \\ \frac{\partial N_1}{\partial y} \end{bmatrix} &= \begin{bmatrix} \frac{\partial r}{\partial x} & \frac{\partial s}{\partial x} \\ \frac{\partial r}{\partial y} & \frac{\partial s}{\partial y} \end{bmatrix} \begin{bmatrix} \frac{\partial N_1}{\partial r} \\ \frac{\partial N_1}{\partial s} \end{bmatrix} = \begin{bmatrix} \frac{1}{250} & 0 \\ 0 & \frac{1}{250} \end{bmatrix} \begin{bmatrix} s-1 \\ r-1 \end{bmatrix} = \begin{bmatrix} \frac{s-1}{250} \\ \frac{r-1}{250} \end{bmatrix} \\ \begin{bmatrix} \frac{\partial N_2}{\partial x} \\ \frac{\partial N_2}{\partial y} \end{bmatrix} &= \begin{bmatrix} \frac{\partial r}{\partial x} & \frac{\partial s}{\partial x} \\ \frac{\partial r}{\partial y} & \frac{\partial s}{\partial y} \end{bmatrix} \begin{bmatrix} \frac{\partial N_2}{\partial r} \\ \frac{\partial N_2}{\partial s} \end{bmatrix} = \begin{bmatrix} \frac{1}{250} & 0 \\ 0 & \frac{1}{250} \end{bmatrix} \begin{bmatrix} -(s-1) \\ -r \end{bmatrix} = \begin{bmatrix} -\frac{s-1}{250} \\ -\frac{r}{250} \end{bmatrix} \\ \begin{bmatrix} \frac{\partial N_3}{\partial x} \\ \frac{\partial N_3}{\partial y} \end{bmatrix} &= \begin{bmatrix} \frac{\partial r}{\partial x} & \frac{\partial s}{\partial x} \\ \frac{\partial r}{\partial y} & \frac{\partial s}{\partial y} \end{bmatrix} \begin{bmatrix} \frac{\partial N_3}{\partial r} \\ \frac{\partial N_3}{\partial s} \end{bmatrix} = \begin{bmatrix} \frac{1}{250} & 0 \\ 0 & \frac{1}{250} \end{bmatrix} \begin{bmatrix} s \\ r \end{bmatrix} = \begin{bmatrix} \frac{s}{250} \\ \frac{r}{250} \end{bmatrix} \\ \begin{bmatrix} \frac{\partial N_4}{\partial x} \\ \frac{\partial N_4}{\partial y} \end{bmatrix} &= \begin{bmatrix} \frac{\partial r}{\partial x} & \frac{\partial s}{\partial x} \\ \frac{\partial r}{\partial y} & \frac{\partial s}{\partial y} \end{bmatrix} \begin{bmatrix} \frac{\partial N_4}{\partial r} \\ \frac{\partial N_4}{\partial s} \end{bmatrix} = \begin{bmatrix} \frac{1}{250} & 0 \\ 0 & \frac{1}{250} \end{bmatrix} \begin{bmatrix} -s \\ -(r-1) \end{bmatrix} = \begin{bmatrix} -\frac{s}{250} \\ -\frac{r-1}{250} \end{bmatrix} \end{aligned}$$

Reemplazando en B

$$B = \begin{bmatrix} \frac{s-1}{250} & 0 & -\frac{s-1}{250} & 0 & \frac{s}{250} & 0 & -\frac{s}{250} & 0 \\ 0 & \frac{r-1}{250} & 0 & -\frac{r}{250} & 0 & \frac{r}{250} & 0 & -\frac{r-1}{250} \\ \frac{r-1}{250} & \frac{s-1}{250} & -\frac{r}{250} & -\frac{s-1}{250} & \frac{r}{250} & \frac{s}{250} & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix}$$

Reemplazando en la fórmula de la matriz de rigidez

$$K = \int_0^1 \int_0^1 \begin{bmatrix} \frac{s-1}{250} & 0 & \frac{r-1}{250} \\ 0 & \frac{r-1}{250} & \frac{s-1}{250} \\ -\frac{s-1}{250} & 0 & -\frac{r}{250} \\ 0 & -\frac{r}{250} & -\frac{s-1}{250} \\ \frac{s}{250} & 0 & \frac{r}{250} \\ 0 & \frac{r}{250} & \frac{s}{250} \\ -\frac{s}{250} & 0 & -\frac{r-1}{250} \\ 0 & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix} \begin{bmatrix} 214500.214 & 55770.056 & 0 \\ 55770.056 & 214500.214 & 0 \\ 0 & 0 & 79365.079 \end{bmatrix} \begin{bmatrix} \frac{s-1}{250} & 0 & -\frac{s-1}{250} & 0 & \frac{s}{250} & 0 & -\frac{s}{250} & 0 \\ 0 & \frac{r-1}{250} & 0 & -\frac{r}{250} & 0 & \frac{r}{250} & 0 & -\frac{r-1}{250} \\ \frac{r-1}{250} & \frac{s-1}{250} & -\frac{r}{250} & -\frac{s-1}{250} & \frac{r}{250} & \frac{s}{250} & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix} 62500 \cdot 20 \, ds \, dr$$

Integrando

$$K = \begin{bmatrix} 1959101.959 & 675675.6755 & -1165451.165 & -117975.1180 & -979550.9793 & -675675.6757 & 185900.1856 & 117975.1178 \\ 675675.6755 & 1959101.960 & 117975.1180 & 185900.1852 & -675675.6756 & -979550.9795 & -117975.1181 & -1165451.166 \\ -1165451.165 & 117975.1180 & 1959101.959 & -675675.6755 & 185900.1856 & -117975.1178 & -979550.9793 & 675675.6757 \\ -117975.1180 & 185900.1852 & -675675.6755 & 1959101.960 & 117975.1181 & -1165451.166 & 675675.6756 & -979550.9795 \\ -979550.9796 & -675675.6756 & 185900.1859 & 117975.1181 & 1959101.959 & 675675.6755 & -1165451.165 & -117975.1180 \\ -675675.6757 & -979550.9797 & -117975.1178 & -1165451.165 & 675675.6755 & 1959101.959 & 117975.1180 & 185900.1860 \\ 185900.1859 & -117975.1181 & -979550.9796 & 675675.6756 & -1165451.165 & 117975.1180 & 1959101.959 & -675675.6755 \\ 117975.1178 & -1165451.165 & 675675.6757 & -979550.9797 & -117975.1180 & 185900.1860 & -675675.6755 & 1959101.959 \end{bmatrix}$$

Solución 3

La matriz de rigidez es

$$K = \int_0^1 \int_0^1 B^T C B \det J \, t \, ds \, dr$$

La matriz constitutiva es

$$C = \frac{E}{1-\nu^2} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & \frac{1-\nu}{2} \end{bmatrix} = \frac{200000}{1-0.26^2} \begin{bmatrix} 1 & 0.26 & 0 \\ 0.26 & 1 & 0 \\ 0 & 0 & \frac{1-0.26}{2} \end{bmatrix} = \begin{bmatrix} 214500.214 & 55770.056 & 0 \\ 55770.056 & 214500.214 & 0 \\ 0 & 0 & 79365.079 \end{bmatrix}$$

Coordenadas de los nodos del elemento lagrangiano

$$\begin{aligned} \textcircled{1} &= [r_1, s_1] = [0, 0] & \textcircled{3} &= [r_3, s_3] = [1, 1] \\ \textcircled{2} &= [r_2, s_2] = [1, 0] & \textcircled{4} &= [r_4, s_4] = [0, 1] \end{aligned}$$

Funciones que interpolan los desplazamientos

$$\begin{aligned} N_1 &= \frac{r-r_2}{r_1-r_2} \cdot \frac{s-s_4}{s_1-s_4} = \frac{r-1}{0-1} \cdot \frac{s-1}{0-1} = (r-1)(s-1) \\ N_2 &= \frac{r-r_1}{r_2-r_1} \cdot \frac{s-s_3}{s_2-s_3} = \frac{r-0}{1-0} \cdot \frac{s-1}{0-1} = -r(s-1) \\ N_3 &= \frac{r-r_4}{r_3-r_4} \cdot \frac{s-s_2}{s_3-s_2} = \frac{r-0}{1-0} \cdot \frac{s-0}{1-0} = rs \\ N_4 &= \frac{r-r_3}{r_4-r_3} \cdot \frac{s-s_1}{s_4-s_1} = \frac{r-1}{0-1} \cdot \frac{s-0}{1-0} = -s(r-1) \end{aligned}$$

Escribiendo en la forma matricial

$$N = \begin{bmatrix} (r-1)(s-1) & -r(s-1) & rs & -s(r-1) \end{bmatrix} = \begin{bmatrix} N_1 & N_2 & N_3 & N_4 \end{bmatrix}$$

Coordenadas de los nodos de la placa

$$\begin{aligned} \textcircled{1} &= [x_1, y_1] = [0, 0] & \textcircled{3} &= [x_3, y_3] = [250, 250] \\ \textcircled{2} &= [x_2, y_2] = [250, 0] & \textcircled{4} &= [x_4, y_4] = [0, 250] \end{aligned}$$

Funciones que interpolan la geometría

$$\begin{aligned} x &= N_1x_1 + N_2x_2 + N_3x_3 + N_4x_4 \\ y &= N_1y_1 + N_2y_2 + N_3y_3 + N_4y_4 \end{aligned}$$

Reemplazando las coordenadas de los nodos

$$\begin{aligned} x &= 250r \\ y &= 250s \end{aligned}$$

El jacobiano y el jacobiano inverso son

$$J = \begin{bmatrix} \frac{\partial x}{\partial r} & \frac{\partial y}{\partial r} \\ \frac{\partial x}{\partial s} & \frac{\partial y}{\partial s} \end{bmatrix} \quad J^{-1} = \begin{bmatrix} \frac{\partial r}{\partial x} & \frac{\partial s}{\partial x} \\ \frac{\partial r}{\partial y} & \frac{\partial s}{\partial y} \end{bmatrix}$$

Reemplazando derivadas

$$J = \begin{bmatrix} 250 & 0 \\ 0 & 250 \end{bmatrix} \quad J^{-1} = \begin{bmatrix} \frac{1}{250} & 0 \\ 0 & \frac{1}{250} \end{bmatrix}$$

Determinante del jacobiano

$$\det J = 62500$$

La matriz de deformaciones es

$$B = \begin{bmatrix} \frac{\partial N_1}{\partial x} & 0 & \frac{\partial N_2}{\partial x} & 0 & \frac{\partial N_3}{\partial x} & 0 & \frac{\partial N_4}{\partial x} & 0 \\ 0 & \frac{\partial N_1}{\partial y} & 0 & \frac{\partial N_2}{\partial y} & 0 & \frac{\partial N_3}{\partial y} & 0 & \frac{\partial N_4}{\partial y} \\ \frac{\partial N_1}{\partial y} & \frac{\partial N_1}{\partial x} & \frac{\partial N_2}{\partial y} & \frac{\partial N_2}{\partial x} & \frac{\partial N_3}{\partial y} & \frac{\partial N_3}{\partial x} & \frac{\partial N_4}{\partial y} & \frac{\partial N_4}{\partial x} \end{bmatrix}$$

Las derivadas de las funciones de forma se calcularán usando una forma alternativa del jacobiano inverso

$$\begin{bmatrix} \frac{\partial N_i}{\partial x} \\ \frac{\partial N_i}{\partial y} \end{bmatrix} = \frac{1}{\det J} \begin{bmatrix} J_{22} & -J_{12} \\ -J_{21} & J_{11} \end{bmatrix} \begin{bmatrix} \frac{\partial N_i}{\partial r} \\ \frac{\partial N_i}{\partial s} \end{bmatrix} = \frac{1}{\det J} \begin{bmatrix} \frac{\partial y}{\partial s} & -\frac{\partial y}{\partial r} \\ -\frac{\partial x}{\partial s} & \frac{\partial x}{\partial r} \end{bmatrix} \begin{bmatrix} \frac{\partial N_i}{\partial r} \\ \frac{\partial N_i}{\partial s} \end{bmatrix}$$

Reemplazando en N_i

$$\begin{aligned} \begin{bmatrix} \frac{\partial N_1}{\partial x} \\ \frac{\partial N_1}{\partial y} \end{bmatrix} &= \frac{1}{\det J} \begin{bmatrix} \frac{\partial y}{\partial s} & -\frac{\partial y}{\partial r} \\ -\frac{\partial x}{\partial s} & \frac{\partial x}{\partial r} \end{bmatrix} \begin{bmatrix} \frac{\partial N_1}{\partial r} \\ \frac{\partial N_1}{\partial s} \end{bmatrix} = \frac{1}{62500} \begin{bmatrix} 250 & 0 \\ 0 & 250 \end{bmatrix} \begin{bmatrix} s-1 \\ r-1 \end{bmatrix} = \begin{bmatrix} \frac{s-1}{250} \\ \frac{r-1}{250} \end{bmatrix} \\ \begin{bmatrix} \frac{\partial N_2}{\partial x} \\ \frac{\partial N_2}{\partial y} \end{bmatrix} &= \frac{1}{\det J} \begin{bmatrix} \frac{\partial y}{\partial s} & -\frac{\partial y}{\partial r} \\ -\frac{\partial x}{\partial s} & \frac{\partial x}{\partial r} \end{bmatrix} \begin{bmatrix} \frac{\partial N_2}{\partial r} \\ \frac{\partial N_2}{\partial s} \end{bmatrix} = \frac{1}{62500} \begin{bmatrix} 250 & 0 \\ 0 & 250 \end{bmatrix} \begin{bmatrix} -(s-1) \\ -r \end{bmatrix} = \begin{bmatrix} -\frac{s-1}{250} \\ -\frac{r}{250} \end{bmatrix} \\ \begin{bmatrix} \frac{\partial N_3}{\partial x} \\ \frac{\partial N_3}{\partial y} \end{bmatrix} &= \frac{1}{\det J} \begin{bmatrix} \frac{\partial y}{\partial s} & -\frac{\partial y}{\partial r} \\ -\frac{\partial x}{\partial s} & \frac{\partial x}{\partial r} \end{bmatrix} \begin{bmatrix} \frac{\partial N_3}{\partial r} \\ \frac{\partial N_3}{\partial s} \end{bmatrix} = \frac{1}{62500} \begin{bmatrix} 250 & 0 \\ 0 & 250 \end{bmatrix} \begin{bmatrix} s \\ r \end{bmatrix} = \begin{bmatrix} \frac{s}{250} \\ \frac{r}{250} \end{bmatrix} \\ \begin{bmatrix} \frac{\partial N_4}{\partial x} \\ \frac{\partial N_4}{\partial y} \end{bmatrix} &= \frac{1}{\det J} \begin{bmatrix} \frac{\partial y}{\partial s} & -\frac{\partial y}{\partial r} \\ -\frac{\partial x}{\partial s} & \frac{\partial x}{\partial r} \end{bmatrix} \begin{bmatrix} \frac{\partial N_4}{\partial r} \\ \frac{\partial N_4}{\partial s} \end{bmatrix} = \frac{1}{62500} \begin{bmatrix} 250 & 0 \\ 0 & 250 \end{bmatrix} \begin{bmatrix} -s \\ -(r-1) \end{bmatrix} = \begin{bmatrix} -\frac{s}{250} \\ -\frac{r-1}{250} \end{bmatrix} \end{aligned}$$

Reemplazando en B

$$B = \begin{bmatrix} \frac{s-1}{250} & 0 & -\frac{s-1}{250} & 0 & \frac{s}{250} & 0 & -\frac{s}{250} & 0 \\ 0 & \frac{r-1}{250} & 0 & -\frac{r}{250} & 0 & \frac{r}{250} & 0 & -\frac{r-1}{250} \\ \frac{r-1}{250} & \frac{s-1}{250} & -\frac{r}{250} & -\frac{s-1}{250} & \frac{r}{250} & \frac{s}{250} & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix}$$

Reemplazando en la fórmula de la matriz de rigidez

$$K = \int_0^1 \int_0^1 \begin{bmatrix} \frac{s-1}{250} & 0 & \frac{r-1}{250} \\ 0 & \frac{r-1}{250} & \frac{s-1}{250} \\ -\frac{s-1}{250} & 0 & -\frac{r}{250} \\ 0 & -\frac{r}{250} & -\frac{s-1}{250} \\ \frac{s}{250} & 0 & \frac{r}{250} \\ 0 & \frac{r}{250} & \frac{s}{250} \\ -\frac{s}{250} & 0 & -\frac{r-1}{250} \\ 0 & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix} \begin{bmatrix} 214500.214 & 55770.056 & 0 \\ 55770.056 & 214500.214 & 0 \\ 0 & 0 & 79365.079 \end{bmatrix} \begin{bmatrix} \frac{s-1}{250} & 0 & -\frac{s-1}{250} & 0 & \frac{s}{250} & 0 & -\frac{s}{250} & 0 \\ 0 & \frac{r-1}{250} & 0 & -\frac{r}{250} & 0 & \frac{r}{250} & 0 & -\frac{r-1}{250} \\ \frac{r-1}{250} & \frac{s-1}{250} & -\frac{r}{250} & -\frac{s-1}{250} & \frac{r}{250} & \frac{s}{250} & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix} 62500 \cdot 20 \, ds \, dr$$

Integrando

$$K = \begin{bmatrix} 1959101.959 & 675675.6755 & -1165451.165 & -117975.1180 & -979550.9793 & -675675.6757 & 185900.1856 & 117975.1178 \\ 675675.6755 & 1959101.960 & 117975.1180 & 185900.1852 & -675675.6756 & -979550.9795 & -117975.1181 & -1165451.166 \\ -1165451.165 & 117975.1180 & 1959101.959 & -675675.6755 & 185900.1856 & -117975.1178 & -979550.9793 & 675675.6757 \\ -117975.1180 & 185900.1852 & -675675.6755 & 1959101.960 & 117975.1181 & -1165451.166 & 675675.6756 & -979550.9795 \\ -979550.9796 & -675675.6756 & 185900.1859 & 117975.1181 & 1959101.959 & 675675.6755 & -1165451.165 & -117975.1180 \\ -675675.6757 & -979550.9797 & -117975.1178 & -1165451.165 & 675675.6755 & 1959101.959 & 117975.1180 & 185900.1860 \\ 185900.1859 & -117975.1181 & -979550.9796 & 675675.6756 & -1165451.165 & 117975.1180 & 1959101.959 & -675675.6755 \\ 117975.1178 & -1165451.165 & 675675.6757 & -979550.9797 & -117975.1180 & 185900.1860 & -675675.6755 & 1959101.959 \end{bmatrix}$$

Solución 4

La matriz de rigidez es

$$K = \int_0^1 \int_0^1 B^T C B \det J \, t \, ds \, dr$$

La matriz constitutiva es

$$C = \frac{E}{1-\nu^2} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & \frac{1-\nu}{2} \end{bmatrix} = \frac{200000}{1-0.26^2} \begin{bmatrix} 1 & 0.26 & 0 \\ 0.26 & 1 & 0 \\ 0 & 0 & \frac{1-0.26}{2} \end{bmatrix} = \begin{bmatrix} 214500.214 & 55770.056 & 0 \\ 55770.056 & 214500.214 & 0 \\ 0 & 0 & 79365.079 \end{bmatrix}$$

Coordenadas de los nodos del elemento lagrangiano

$$\begin{aligned} \textcircled{1} &= [r_1, s_1] = [0, 0] & \textcircled{3} &= [r_3, s_3] = [1, 1] \\ \textcircled{2} &= [r_2, s_2] = [1, 0] & \textcircled{4} &= [r_4, s_4] = [0, 1] \end{aligned}$$

Funciones que interpolan los desplazamientos

$$\begin{aligned} N_1 &= \frac{r-r_2}{r_1-r_2} \cdot \frac{s-s_4}{s_1-s_4} = \frac{r-1}{0-1} \cdot \frac{s-1}{0-1} = (r-1)(s-1) \\ N_2 &= \frac{r-r_1}{r_2-r_1} \cdot \frac{s-s_3}{s_2-s_3} = \frac{r-0}{1-0} \cdot \frac{s-1}{0-1} = -r(s-1) \\ N_3 &= \frac{r-r_4}{r_3-r_4} \cdot \frac{s-s_2}{s_3-s_2} = \frac{r-0}{1-0} \cdot \frac{s-0}{1-0} = rs \\ N_4 &= \frac{r-r_3}{r_4-r_3} \cdot \frac{s-s_1}{s_4-s_1} = \frac{r-1}{0-1} \cdot \frac{s-0}{1-0} = -s(r-1) \end{aligned}$$

Escribiendo en la forma matricial

$$N = \begin{bmatrix} (r-1)(s-1) & -r(s-1) & rs & -s(r-1) \end{bmatrix} = \begin{bmatrix} N_1 & N_2 & N_3 & N_4 \end{bmatrix}$$

Coordenadas de los nodos de la placa

$$\begin{aligned} \textcircled{1} &= [x_1, y_1] = [0, 0] & \textcircled{3} &= [x_3, y_3] = [250, 250] \\ \textcircled{2} &= [x_2, y_2] = [250, 0] & \textcircled{4} &= [x_4, y_4] = [0, 250] \end{aligned}$$

Funciones que interpolan la geometría

$$\begin{aligned} x &= N_1x_1 + N_2x_2 + N_3x_3 + N_4x_4 \\ y &= N_1y_1 + N_2y_2 + N_3y_3 + N_4y_4 \end{aligned}$$

Reemplazando las coordenadas de los nodos

$$\begin{aligned} x &= 250r \\ y &= 250s \end{aligned}$$

El jacobiano y el jacobiano inverso son

$$J = \begin{bmatrix} \frac{\partial x}{\partial r} & \frac{\partial y}{\partial r} \\ \frac{\partial x}{\partial s} & \frac{\partial y}{\partial s} \end{bmatrix} \quad J^{-1} = \begin{bmatrix} \frac{\partial r}{\partial x} & \frac{\partial s}{\partial x} \\ \frac{\partial r}{\partial y} & \frac{\partial s}{\partial y} \end{bmatrix}$$

Reemplazando derivadas

$$J = \begin{bmatrix} 250 & 0 \\ 0 & 250 \end{bmatrix} \quad J^{-1} = \begin{bmatrix} \frac{1}{250} & 0 \\ 0 & \frac{1}{250} \end{bmatrix}$$

Determinante del jacobiano

$$\det J = 62500$$

La matriz de deformaciones es

$$B = M_1 M_2 M_3$$

$$M_1 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 1 & 1 & 0 \end{bmatrix}$$

$$M_2 = \begin{bmatrix} \frac{\partial r}{\partial x} & \frac{\partial s}{\partial x} & 0 & 0 \\ \frac{\partial r}{\partial y} & \frac{\partial s}{\partial y} & 0 & 0 \\ 0 & 0 & \frac{\partial r}{\partial x} & \frac{\partial s}{\partial x} \\ 0 & 0 & \frac{\partial r}{\partial y} & \frac{\partial s}{\partial y} \end{bmatrix}$$

$$M_3 = \begin{bmatrix} \frac{\partial N_1}{\partial r} & 0 & \frac{\partial N_2}{\partial r} & 0 & \frac{\partial N_3}{\partial r} & 0 & \frac{\partial N_4}{\partial r} & 0 \\ \frac{\partial N_1}{\partial s} & 0 & \frac{\partial N_2}{\partial s} & 0 & \frac{\partial N_3}{\partial s} & 0 & \frac{\partial N_4}{\partial s} & 0 \\ 0 & \frac{\partial N_1}{\partial r} & 0 & \frac{\partial N_2}{\partial r} & 0 & \frac{\partial N_3}{\partial r} & 0 & \frac{\partial N_4}{\partial r} \\ 0 & \frac{\partial N_1}{\partial s} & 0 & \frac{\partial N_2}{\partial s} & 0 & \frac{\partial N_3}{\partial s} & 0 & \frac{\partial N_4}{\partial s} \end{bmatrix}$$

Reemplazando en M_2 y M_3

$$M_2 = \begin{bmatrix} \frac{1}{250} & 0 & 0 & 0 \\ 0 & \frac{1}{250} & 0 & 0 \\ 0 & 0 & \frac{1}{250} & 0 \\ 0 & 0 & 0 & \frac{1}{250} \end{bmatrix}$$

$$M_3 = \begin{bmatrix} s-1 & 0 & -(s-1) & 0 & s & 0 & -s & 0 \\ r-1 & 0 & -r & 0 & r & 0 & -(r-1) & 0 \\ 0 & s-1 & 0 & -(s-1) & 0 & s & 0 & -s \\ 0 & r-1 & 0 & -r & 0 & r & 0 & -(r-1) \end{bmatrix}$$

Reemplazando en B

$$B = \begin{bmatrix} \frac{s-1}{250} & 0 & -\frac{s-1}{250} & 0 & \frac{s}{250} & 0 & -\frac{s}{250} & 0 \\ 0 & \frac{r-1}{250} & 0 & -\frac{r}{250} & 0 & \frac{r}{250} & 0 & -\frac{r-1}{250} \\ \frac{r-1}{250} & \frac{s-1}{250} & -\frac{r}{250} & -\frac{s-1}{250} & \frac{r}{250} & \frac{s}{250} & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix}$$

Reemplazando en la fórmula de la matriz de rigidez

$$K = \int_0^1 \int_0^1 \begin{bmatrix} \frac{s-1}{250} & 0 & \frac{r-1}{250} \\ 0 & \frac{r-1}{250} & \frac{s-1}{250} \\ -\frac{s-1}{250} & 0 & -\frac{r}{250} \\ 0 & -\frac{r}{250} & -\frac{s-1}{250} \\ \frac{s}{250} & 0 & \frac{r}{250} \\ 0 & \frac{r}{250} & \frac{s}{250} \\ -\frac{s}{250} & 0 & -\frac{r-1}{250} \\ 0 & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix} \begin{bmatrix} 214500.214 & 55770.056 & 0 \\ 55770.056 & 214500.214 & 0 \\ 0 & 0 & 79365.079 \end{bmatrix} \begin{bmatrix} \frac{s-1}{250} & 0 & -\frac{s-1}{250} & 0 & \frac{s}{250} & 0 & -\frac{s}{250} & 0 \\ 0 & \frac{r-1}{250} & 0 & -\frac{r}{250} & 0 & \frac{r}{250} & 0 & -\frac{r-1}{250} \\ \frac{r-1}{250} & \frac{s-1}{250} & -\frac{r}{250} & -\frac{s-1}{250} & \frac{r}{250} & \frac{s}{250} & -\frac{r-1}{250} & -\frac{s}{250} \end{bmatrix} 62500 \cdot 20 \, ds \, dr$$

Integrando

$$K = \begin{bmatrix} 1959101.959 & 675675.6755 & -1165451.165 & -117975.1180 & -979550.9793 & -675675.6757 & 185900.1856 & 117975.1178 \\ 675675.6755 & 1959101.960 & 117975.1180 & 185900.1852 & -675675.6756 & -979550.9795 & -117975.1181 & -1165451.166 \\ -1165451.165 & 117975.1180 & 1959101.959 & -675675.6755 & 185900.1856 & -117975.1178 & -979550.9793 & 675675.6757 \\ -117975.1180 & 185900.1852 & -675675.6755 & 1959101.960 & 117975.1181 & -1165451.166 & 675675.6756 & -979550.9795 \\ -979550.9796 & -675675.6756 & 185900.1859 & 117975.1181 & 1959101.959 & 675675.6755 & -1165451.165 & -117975.1180 \\ -675675.6757 & -979550.9797 & -117975.1178 & -1165451.165 & 675675.6755 & 1959101.959 & 117975.1180 & 185900.1860 \\ 185900.1859 & -117975.1181 & -979550.9796 & 675675.6756 & -1165451.165 & 117975.1180 & 1959101.959 & -675675.6755 \\ 117975.1178 & -1165451.165 & 675675.6757 & -979550.9797 & -117975.1180 & 185900.1860 & -675675.6755 & 1959101.959 \end{bmatrix}$$