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1. Inverse Matrix

• Recall that the inverse of A is equal to:
$$\frac{1}{|A|} \times Adjugate \text{ of } A$$

- Further recall that the adjugate is equal to the transpose of the cofactor matrix.
- Find the inverse of the following matrix:

$$A = \begin{bmatrix} 4 & 1 & -1 \\ 0 & 3 & 2 \\ 3 & 0 & 7 \end{bmatrix}$$
 determinant:
$$-1[(0 \cdot 7) - (3 \cdot 2)] + (-1) \cdot [(0 \cdot 0) - (3 \cdot 3)] = 84 + 6 + 9 = 99$$

1. Inverse Matrix

The cofactor matrix of is:

$$A = \begin{bmatrix} 4 & 1 & -1 \\ 0 & 3 & 2 \\ 3 & 0 & 7 \end{bmatrix}$$

$$\begin{bmatrix} \begin{vmatrix} 3 & 2 \\ 0 & +7 \end{vmatrix} & -\begin{vmatrix} 0 & 2 \\ 3 & 7 \end{vmatrix} & \begin{vmatrix} 0 & 3 \\ 3 & 0 \end{vmatrix} \\ -\begin{vmatrix} 1 & -1 \\ 0 & 7 \end{vmatrix} & +\begin{vmatrix} 4 & -1 \\ 3 & 7 \end{vmatrix} & -\begin{vmatrix} 4 & 1 \\ 3 & 0 \end{vmatrix} \\ \begin{vmatrix} 1 & -1 \\ 3 & 2 \end{vmatrix} & -\begin{vmatrix} 4 & -1 \\ 0 & 2 \end{vmatrix} & \begin{vmatrix} 4 & 1 \\ 0 & 3 \end{vmatrix} \end{bmatrix} = \begin{bmatrix} 21 & 6 & -9 \\ -7 & 31 & 3 \\ 5 & -8 & 12 \end{bmatrix}$$

1. Inverse Matrix

Cofactor matrix

$$\begin{bmatrix} 21 & 6 & -9 \\ -7 & 31 & 3 \\ 5 & -8 & 12 \end{bmatrix}$$

• Transpose of cofactors:

$$\begin{bmatrix} 21 & -7 & 5 \\ 6 & 31 & -8 \\ -9 & 3 & 12 \end{bmatrix}$$

• Inverse of A:

$$\frac{1}{|A|}adjA = \frac{1}{99} \begin{bmatrix} 21 & -7 & 5\\ 6 & 31 & -8\\ -9 & 3 & 12 \end{bmatrix}$$

2. SVAR Identification: restrictions

 Imposing the restriction makes the number of unknown parameters in the structural model equal to the number of parameters known from the standard **VAR** estimation:

1.
$$g_{10} = \beta_{10}$$

4.
$$g_{21} = -a_{21}\beta_{11} + \beta_{12}$$

2.
$$g_{20} = -a_{21}\beta_{10} + \beta_{20}$$
 5. $g_{12} = \beta_{12}$

5.
$$g_{12} = \beta_{12}$$

3.
$$g_{11} = \beta_{11}$$

6.
$$g_{22} = -a_{21}\beta_{12} + \beta_{22}$$

Since $e_{_{\mathcal{M}}} = u_{_{\mathcal{M}}}$ then,

7.
$$\operatorname{var}(e_{yt}) = \sigma_{uy}^2$$

8.
$$\operatorname{var}(e_{rt}) = \sigma_{ur}^2 + a_{21}^2 \sigma_{uy}^2$$

9.
$$cov(e_{yt}e_{rt}) = E(u_{yt})(u_{rt} - a_{21}u_{yt}) = -a_{21}\sigma_{uy}^2$$

• Substitute the estimated values for these 9 parameters g_{10} , g_{11} , g_{12} , g_{20} , g_{21} , g_{22} , σ_{ev}^2 , σ_{er}^2 and σ_{ev-er} in the 9 equations, to solve for: a_{21} , β_{10} , β_{20} , β_{11} , β_{12} , $\beta_{2l}, \beta_{22}, \sigma^2_{vv}$, and σ^2_{vr} .

3. Impulse-responses

In a first order autoregressive model:

$$\mathbf{y}_{t} = \mathbf{g}_{0} + \mathbf{g}_{1}\mathbf{y}_{t-1} + \mathbf{\varepsilon}_{t}$$

- The stability condition is that | |<1
- In the case of a VAR, an equivalent condition is required. It becomes clear when the standard VAR is iterated backwards. For a simple VAR(1):

$$X_{t} = G_{0} + G_{1}X_{t-1} + \mathcal{C}_{t} \longrightarrow X_{t-1} = G_{0} + G_{1}X_{t-2} + \mathcal{C}_{t-1}$$

$$X_{t} = G_{0} + G_{1}(G_{0} + G_{1}X_{t-2} + \mathcal{C}_{t-1}) + \mathcal{C}_{t}$$

3. Impulse-responses

Successive iterations generate:

$$X_{t} = G_{0} + G_{1} \underbrace{(G_{0} + G_{1} \underbrace{(G_{0} + G_{1} X_{t-3} + \mathcal{C}_{t-2})}_{X_{t-2}} + \mathcal{C}_{t-1}) + \mathcal{C}_{t}}_{X_{t-2}}$$

$$X_{t} = (I + G_{1} + G_{1}^{2} + \cdots + G_{1}^{\infty})G_{0} + \mathcal{C}_{t} + \sum_{i=1}^{\infty} G_{1}^{i} \mathcal{C}_{t-i} + G_{1}^{i} X_{t-n-i}) \longrightarrow 0$$

As i $\rightarrow +\infty$ X reduces to a sum of errors or Wold representation of X:

$$X_t = \mu + \sum_{i=1}^{+\infty} G_1^i \mathcal{C}_{t-i} + \mathcal{C}_t \text{ assume } \psi_i = G_1^i \text{ then } X_t = \mu + \sum_{i=1}^{+\infty} \psi_i \mathcal{C}_{t-i} + \mathcal{C}_t$$

If **X** has a Wold representation then **X** is **stable**. The condition that guarantees it is that **G** has eigenvalues smaller than **1** in modulus. It is a general result, not only valid for a VAR (1) but valid for any VAR(p).

3. Impulse-responses

Since the VAR is stationary, the estimated reduced-form VAR ha a moving average:

$$X_{t} = \boldsymbol{\mu} + \boldsymbol{e}_{t} + \sum_{i=1}^{\infty} \psi_{i} \boldsymbol{e}_{t-i}$$

- Using the same old relation between forecast errors and structural shocks $e_{r} = A^{-1}u_{r}$ we find: $X_t = \mu + A^{-1} \mathcal{U}_t + \sum_{i=1}^{\infty} \psi_i A^{-1} \mathcal{U}_{t-i}$ or more compactly $X_t = \mu + \sum_{i=0}^{\infty} C_i \mathcal{U}_{t-i}$ $c_{11,i}$ and $c_{12,i}$ are the responses of **y** and **r** to a change u_{v} and u_{r} respectively.
- Note that $c_{11,0}$ is the effect at impact, $c_{11,1}$ is the effect of u_{tt} on y on t+1, and so on in succession: $\frac{\partial y_{t+k}}{\partial u_{yt}} = C_{11,k}$ • Also, the cumulative effect is $\sum_{i=0}^{\infty} C_{11,i}$.

4. Variance Decomposition

- Knowledge of the prediction errors can be extremely valuable in examining the relationships among the variables.
- Assume that we know the coefficients G_0 and G_1 and wish to project the values of X_{t+1} conditional on the observed values of X_t .
- If the equation $X_t = G_0 + G_1 X_{t-1} + \mathcal{C}_t$ is advanced one period, we obtain $X_{t+1} = G_0 + G_1 X_t + \mathcal{C}_{t+1}$ and the prediction error will be $X_{t+1} EX_{t+1} = \mathcal{C}_{t+1}$ for innovation in t+1.

$$X_{t+3} = G_0 + G_1 \underbrace{(G_0 + G_1 \underbrace{(G_0 + G_1 X_t + \mathcal{C}_{t+1})}_{X_{t+1}} + \mathcal{C}_{t+2})}_{X_{t+1}} + \mathcal{C}_{t+2}) + \mathcal{C}_{t+3}$$

$$X_{t+3} - EX_{t+3} = G_1^2 \mathcal{C}_{t+1} + G_1 \mathcal{C}_{t+2} + \mathcal{C}_{t+3}$$

4. Variance Decomposition

$$EX_{t+n} = (I + G_1 + G_1^2 + ... + G_1^{n-1})G_0 + G_1^n X_{t+n}$$

This may also be expressed in terms of structural errors:

$$X_{t+n} - EX_{t+n} = \mathcal{C}_{t+n} + G_1 \mathcal{C}_{t+n-1} + G_1^2 \mathcal{C}_{t+n-2} + \dots + G_1^{n-1} \mathcal{C}_{t+1}$$

• The prediction error for only GDP gap *n* steps forward will be:

$$X_{t+n} = \mu + \sum_{i=0}^{n} G_{1}^{i} A^{-1} u_{t+n-i} = X_{t+n} = \mu + \sum_{i=0}^{n} \psi_{i} A^{-1} u_{t+n-i} = X_{t+n} = \mu + \sum_{i=0}^{n} C_{i} u_{t+n-i}$$

The variance of this prediction error is:

$$y_{t+n} - Ey_{t+n} = c_{11,0}u_{yt+n} + c_{11,1}u_{yt+n-1} + \dots + c_{11,n-1}u_{yt+1} + c_{12,0}u_{rt+n} + c_{12,1}u_{rt+n-1} + \dots + c_{12,n-1}u_{rt+n}$$

$$\sigma_{y,n}^2 = \sigma_y^2 [c_{11,0}^2 + c_{11,1}^2 + \dots + c_{11,n-1}^2] + c_{12,0}^2 + c_{12,0}^2 + c_{12,1}^2 + \dots + c_{12,n-1}^2]$$

4. Variance Decomposition

- As the values of $c_{11.0}^2$ are necessarily positive, the variance of the errors increases with the projection horizon.
- It is possible to decompose the prediction error n periods forward by the contribution each of the two shocks in our example.
- The proportions of $\sigma_{v,n}^2$ attributable to each structural shock are:

$$\frac{\sigma_{y}^{2}[c_{11,0}^{2}+c_{11,1}^{2}+\cdots+c_{11,n-1}^{2}]}{\sigma_{y,n}^{2}} \qquad \frac{\sigma_{r}^{2}[c_{12,0}^{2}+c_{12,1}^{2}+\cdots+c_{12,n-1}^{2}]}{\sigma_{y,n}^{2}}$$

$$\frac{\sigma_r^2[c_{12,0}^2 + c_{12,1}^2 + \dots + c_{12,n-1}^2]}{\sigma_{v,n}^2}$$

- This is the proportion of the changes in one variable attributable to shocks to it and to shocks in another variable.
- If u_{n-i} fails to explain any changes in **y** the latter is exogenous.
- The restriction imposed above requires that the entire variance in the prediction error for ${m y}$ one period forward be attributable to $u_{{m u}\!-\!i}$