AERO3600 — Embedded Control Systems

Practice problems: Continuous-time state-feedback control design¹

Important



This document proposes several practice problem on state-feedback control desing for continuous time systems.

Problem 1

Consider the system

$$\dot{x}_1 = -3x_1 + x_2 + u$$
$$\dot{x}_2 = -2x_1 + 1.5x_2 + 4u.$$

a) Is the system completely controllable? Justify your answer.

Check your solutions with MATLAB.

Problem 2

Consider four different LTI system written in the form

$$\dot{x} = A_i \, x + B_i \, u$$

where $i = \{1, 2, 3, 4\}$ indicate the index of the system i. The corresponding controllability matrices of the systems are as follows

$$Co_1 = \begin{bmatrix} 2 & 0 \\ 0 & -3 \end{bmatrix}, \quad Co_2 = \begin{bmatrix} -2 & 2 \\ 1 & -1 \end{bmatrix}, \quad Co_3 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}, \quad Co_4 = \begin{bmatrix} 1 & 0 & -2 & 0 \\ 0 & 1 & 0 & -2 \end{bmatrix}.$$

- a) Determine the dimension of the matrices A_i and B_i that corresponde to system i.
- b) Analyse the controllability of each system. Justify your answer.

Check your solutions with MATLAB.

Problem 3

Consider the system

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ 20.6 & 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

- a) Is the system internally stable?
- b) Design a zero-state regulator controller with desired closed-loop eigenvalues at $\lambda_{1,2} = -1.8 \pm j2.4$.
- c) Draw the block-diagram of the control system.

Check your solutions with MATLAB.

¹Updated: 5 May 2021.

Consider the system

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u.$$

- a) Is the system controllable? Justify your answer
- b) Find the controller that results in closed-loop eigenvalues $\lambda_1 = \lambda_2 = -1$.

Check your solutions with MATLAB.

Problem 5

Consider the system

$$\dot{x} = \begin{bmatrix} 1 & 1 \\ -4 & 3 \end{bmatrix} x + \begin{bmatrix} 0 \\ 2 \end{bmatrix} u,$$

$$y = \begin{bmatrix} 1 & 0 \end{bmatrix} x.$$

- a) Find the state transformation T that takes the system into the companion form.
- b) Find the controller that results in closed-loop eigenvalues $\lambda_1 = -1$ and $\lambda_2 = -2$.
- c) Find the set-point regulator that takes the output y to a desired constant output \bar{y} , that is

$$\lim_{t \to \infty} y = \bar{y}$$

Check your solutions with MATLAB.

Problem 6

For each of the following systems, use linearisation to design a state-feedback controller to stabilise the origin. Select the desired closed-loop eigenvalues to achieve a particular dynamic response, for example certain overshoot and time response.

1.

$$\dot{x}_1 = x_1 + x_2$$

$$\dot{x}_2 = 3x_1^2x_2 + x_1 + u$$

$$y = -x_1^3 + x_2$$

2.

$$\begin{aligned} \dot{x}_1 &= x_1 + x_2 \\ \dot{x}_2 &= x_1 x_2^2 - x_1 + x_3 \\ \dot{x}_3 &= u \\ y &= -x_1^3 + x_2 \end{aligned}$$

3.

$$\begin{aligned} \dot{x}_1 &= -x_1 + x_2 \\ \dot{x}_2 &= x_1 - x_2 - x_1 x_3 + u \\ \dot{x}_3 &= x_1 + x_1 x_2 - 2x_3 \\ y &= x_1 \end{aligned}$$

Check your solutions with MATLAB.

A simplified model of a low-frequency motion of a ship can be written as follows

$$\dot{x}_1 = x_2$$

$$\dot{x}_2 = -10x_2 + 0.1u$$

$$y = x_1$$

where x_1 is the heading angle (in radians), x_2 is the heading angular rate and u is the rudder angle.

- 1. Find the equilibrium point and input that correspond to $\bar{y} = \frac{\pi}{4}$.
- 2. Use linearisation to design a state feedback controller to ensure that the output y tracks the reference values \bar{y} and such that the closed loop eigenvalues are -1 and -1.
- 3. Design an integral action that ensure that the output tracks the reference \bar{y} . The desired eigenvalues of the closed loop are -1 -1 -15.

Check your solutions with MATLAB.

Problem 8

Consider the system

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ 1 & -3 \end{bmatrix} x + \begin{bmatrix} 0 \\ 2 \end{bmatrix} u.$$

- a) Determine if the system is controllable. Justify your answer.
- b) Find the gain of the controller $u = -\begin{bmatrix} k_1 & k_2 \end{bmatrix} x$, such that the closed loop eigenvalues are $\lambda_1 = -1$ and $\lambda_2 = -2$.
- c) Determine if it possible to arbitrarily assign the closed loop eigenvalues, that is, can we assign the values λ_1 and λ_2 arbitrarily?
- d) Consider now the controller $u = -\begin{bmatrix} k_3 & 3k_3 \end{bmatrix} x$. Determine the gain k_3 such that one of the closed loop eigenvalues $\lambda_1 = -1$. Determine if it is possible to arbitrarily assign the second closed loop eigenvalue λ_2 .
- e) Consider the controller in d). Determine if the closed loop is stable. Justify your answer.

Check your solutions with MATLAB.

Problem 9

Consider the dynamics of the magnetic levitation system²

$$35\ddot{\phi} + 4\ddot{\theta} - 100\sin(\phi) = -\tau$$
$$4\ddot{\phi} + \ddot{\theta} - 4\sin(\phi)\dot{\phi}^2 = \tau$$
$$y_1 = \phi$$
$$y_2 = \theta$$

where ϕ is the absolute angle of the body and θ is angle of the ball.

- 1. Write the system in state space form with $x_1 = \phi$, $x_2 = \theta$, $x_3 = \dot{\phi}$ and $x_4 = \dot{\theta}$.
- 2. Find the equilibrium point and input that correspond to $\bar{x}_1 = 0$ and $\bar{x}_2 = 0$.
- 3. Use linearisation to design a state feedback controller to ensure that the output y tracks the reference values \bar{y} and such that the closed loop eigenvalues are -10, -10, -15 and -15.
- 4. Design an integral action that ensures that the outputs track the reference values $\bar{y}_1 = 0$ and $\bar{y}_2 = 4$. If possible, the desired eigenvalues of the closed loop should be -10, -10, -15, -5 and -5.

Solve numerically using MATLAB and simulate the closed loop.

²See for example the article Balancing and Transferring Control of a Ball Segway Using a Double-Loop Approach in IEEE Control Systems Magazine, vol. 38, no. 2, pp. 15-37, 2018, D. B. Pham, H. Kim, J. Kim and S. Lee.

Consider the dynamics of the robot known as Ballbot system³

$$35\ddot{\phi} + 4\ddot{\theta} - 100\sin(\phi) = -\tau$$
$$4\ddot{\phi} + \ddot{\theta} - 4\sin(\phi)\dot{\phi}^2 = \tau$$
$$y_1 = \phi$$
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where ϕ is the absolute angle of the body and θ is angle of the ball.

- 1. Write the system in state space form with $x_1 = \phi$, $x_2 = \theta$, $x_3 = \dot{\phi}$ and $x_4 = \dot{\theta}$.
- 2. Find the equilibrium point and input that correspond to $\bar{x}_1 = 0$ and $\bar{x}_2 = 0$.
- 3. Use linearisation to design a state feedback controller to ensure that the output y tracks the reference values \bar{y} and such that the closed loop eigenvalues are -10, -15 and -15.
- 4. Design an integral action that ensures that the outputs track the reference values $\bar{y}_1 = 0$ and $\bar{y}_2 = 4$. If possible, the desired eigenvalues of the closed loop should be -10, -10, -15, -15, -5 and -5.

Solve numerically using MATLAB and simulate the closed loop.

Additional exercises

You can find additional exercises in the chapter 11—the Design of State variable feedback systems—of the book *Modern Control Systems* by R. C. Dorf and R. H. Bishop. The book is available at UON Library.

³See for example the article Balancing and Transferring Control of a Ball Segway Using a Double-Loop Approach in IEEE Control Systems Magazine, vol. 38, no. 2, pp. 15-37, 2018, D. B. Pham, H. Kim, J. Kim and S. Lee.

Answer to a some practice problems

Page 1

(stele-space feedback Combrol design)

Problem 1

$$\Delta = \begin{bmatrix} -3 & 1 \\ -2 & 1.5 \end{bmatrix} ; B = \begin{bmatrix} 1 \\ 4 \end{bmatrix} ; C_{AB} = \begin{bmatrix} 1 & 1 \\ 4 & 4 \end{bmatrix}$$

-> The matrix Cos is square (2-by-2) and its determinant is rank (Cas) = 1 3000 => rank (Cos) = 1 Also notice that the columns of Coo me linearly dependent. (see the note on nothernotical review for the definition of rank of a natrix)

Since rank (Cas) is smaller than the number of the states => the system is not completely controllable

Problem 2

First whice the that for a system is A 2+Bu, with 26P, AER" and uER", where n is the number of states and m is number of inputs, the controllability matrix is.

$$C_0 = \begin{bmatrix} B & AB & A^2B & A^1B \end{bmatrix} \implies C_0 \in \mathbb{R}^{n \times nm}$$
, that is the norm norm norm norm of the norm norm of the norm norm of the norm norm of the nor

then for.

= System 1: Co, E R2x2 => A, E R2x2, B, E R2x1; rank (Cq) = 2) => System 1 is completely no of states = 2) => System 1 is completely

= System 2. Coz E P2x2 => Az E P2x2; Bz E P2x1; rank (Coz)=1 } => System 2 is not no of states = 2) campletely Short mass

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- System 3:
$$Co_3 \in \mathbb{R}^{3\times 3} = A_3 \in \mathbb{R}^{3\times 5}$$
, $B_3 \in \mathbb{R}^{3\times 1}$; $rank(Co_5) = 3$ => System 3 is completely controllable.

- System 4:
$$\cos 6\mathbb{R}^{2\times 4} =$$
 Ay $6\mathbb{R}^{2\times 2}$, $B_4 \in \mathbb{R}^{2\times 2}$, $rank(\cos) = 2$ = $\frac{1}{2}$ Suske 4 is $\frac{1}{2}$ Suske 4 is $\frac{1}{2}$ Completely controllable.

Problem 3

$$A = \begin{bmatrix} 0 & 4 \\ 20.6 & 0 \end{bmatrix} ; B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

a)
$$\pm i \epsilon \cos \log d A \rightarrow coll [\lambda J - \Delta] = coll [\lambda - 1] = \lambda^2 - 20.6 \rightarrow \lambda_{12} = \pm \sqrt{20.6}$$

the system is intendly unstable because A has a positive eigenvalue.

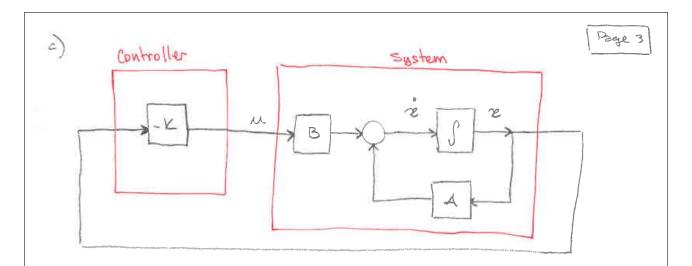
b) Desired Characteristic polynomial

$$(5+1.8+j2.4)(5+1.8-j2.4) = 5^{2}+1.85-j2.45+1.85+1.8^{2}-j2.4.1.8+j2.45$$

$$+j2.4\cdot1.8+2.4^{2}$$

$$= 5^{2}+3.65+9 \quad (*)$$

$$K = [ko \ k_1] =$$
 $(A - B K) = \begin{bmatrix} 0 & 1 \\ -(-20.6+k_0) & -k_1 \end{bmatrix}$



$$A = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}; B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, Cas = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}; renk(Cas) = 2$$

$$= \begin{cases} carpletely \\ controllable \end{cases}$$

$$= \begin{cases} controllable$$

b). Desired characteristic polynomial $(5+1)(5+1) = 5^2 + 25 + 1$

the system is in companion form, then with K= [ko ki]

$$(\Delta - BK) = \begin{bmatrix} 0 & 1 \\ -bo & -b_1 \end{bmatrix} \rightarrow Char(\Delta - BK) = S^2 + k_1 S + k_0$$

Matching the desired ohar polynomial and char (A-BE) = 1; k, = 2

Problem 5

a)
$$\Delta = \begin{bmatrix} 1 & 1 \\ -4 & 3 \end{bmatrix}$$
; $B = \begin{bmatrix} 0 \\ z \end{bmatrix}$; $C_{AB} = \begin{bmatrix} 0 & z \\ z & 6 \end{bmatrix}$; $C_{SNE}(C_{SO}) = 2$ => Completely $C_{CAB}(C_{SO}) = 2$ => Completely $C_{CAB}(C_{SI}) = 2$ =>

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the the companion form is

$$\Delta_{C} = \begin{bmatrix} O & \Delta \\ -7 & 4 \end{bmatrix} ; B_{C} = \begin{bmatrix} O \\ \Delta \end{bmatrix} ; C_{ACBC} = \begin{bmatrix} O & 1 \\ 1 & 4 \end{bmatrix}$$

$$\exists T / Z = T' X \rightarrow Z = Ac Z + Bc M$$
, with $Ac = T'AT$

$$Bc = T'B$$

$$C_{AcBc} = \begin{bmatrix} -4 & 1 \\ 1 & 0 \end{bmatrix} \implies \overline{T} = \begin{bmatrix} 0 & 2 \\ 2 & 6 \end{bmatrix} \begin{bmatrix} -4 & 1 \\ 1 & 0 \end{bmatrix} = \begin{bmatrix} 2 & 0 \\ -2 & 2 \end{bmatrix}$$

6)

Desired characteristic polynomial $\lambda_1 = -1$; $\lambda_2 = -2$ $(S+1)(S+2) = S^2 + 3S + 2$

Desig using the companion form for the 3 he space model == AcZ+Bc 11 =>

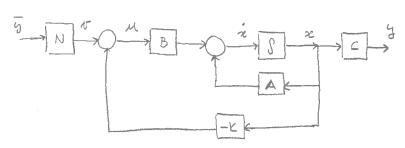
=>
$$7+kz_0=2$$
 => $kz_0=-5$ =>

However, the controller has to be expressed in the original states

$$\mathcal{U} = -\mathbf{k}_{2} \, \mathbf{T}^{T} \mathbf{x} = -\begin{bmatrix} -5 & 7 \end{bmatrix} \begin{bmatrix} \frac{1}{2} & 0 \\ \frac{1}{2} & \frac{1}{2} \end{bmatrix} \mathbf{x} = -\begin{bmatrix} 1 & \frac{7}{2} \end{bmatrix} \mathbf{x}$$

$$\mathbf{k} = \begin{bmatrix} 1 & \frac{7}{2} \end{bmatrix} \mathbf{x}$$

alterative solution



$$\mathring{z} = (A - BE)z + BN\overline{g}$$
 $y = Cz$

new sketes $z = x + (A - BE)BN\overline{g}$
 $y = C[\overline{z} - (A - BE)^TBN\overline{g}]$

the syster in states Z is

$$\begin{cases} \dot{z} = (A - BE) \dot{z} \\ \dot{y} = C \dot{z} - C(A - BE) \dot{b} N \ddot{y} \end{cases}$$

 $\begin{cases} \dot{z} = (A - BE) \dot{z} \\ \dot{y} = C \dot{z} - C(A - BE)^{\dagger} B N \ddot{y} \end{cases}$ Since eig $(A - BE) \dot{\zeta}_{-2}^{-1}$, then the system is a label of \dot{z}_{-2} since eig $(A - BE) \dot{\zeta}_{-2}^{-1}$, then the system is a label of \dot{z}_{-2} . and thus lin = 0, which implies that

lim y=-c(A-BK)BNg. On the other side, it 15 required that lim y = 5 11

therefore C(A-BK) BN=-1 => [1 0] [1 4] [0] N=-1 => $\Rightarrow \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} -2 & -\frac{1}{2} \end{bmatrix} \begin{bmatrix} 0 \\ 3 & \frac{1}{2} \end{bmatrix} \begin{bmatrix} 0 \\ 0 \end{bmatrix} N = -1 \Rightarrow -1 N = -1 \Rightarrow N = 1$