

Off network content for approval 😊

REV	DATE	DESCRIPTION
A	30_May_23	

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LAST EDITED
1-Oct-21



PP Summary

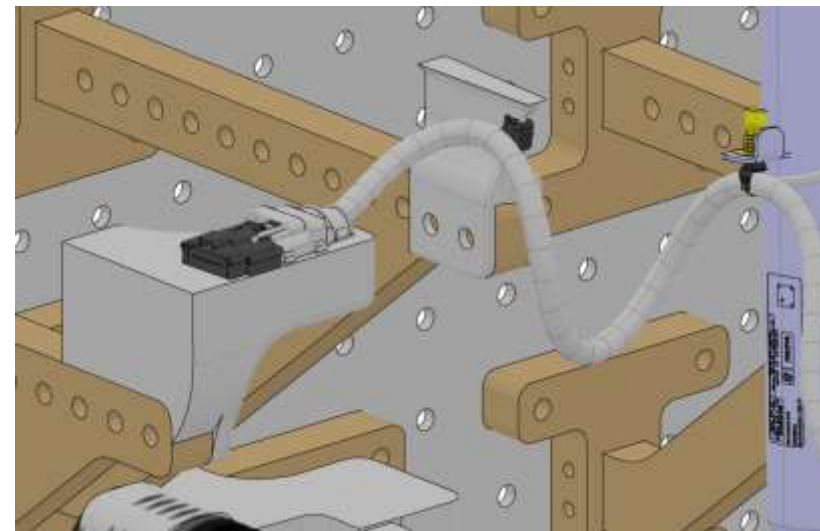
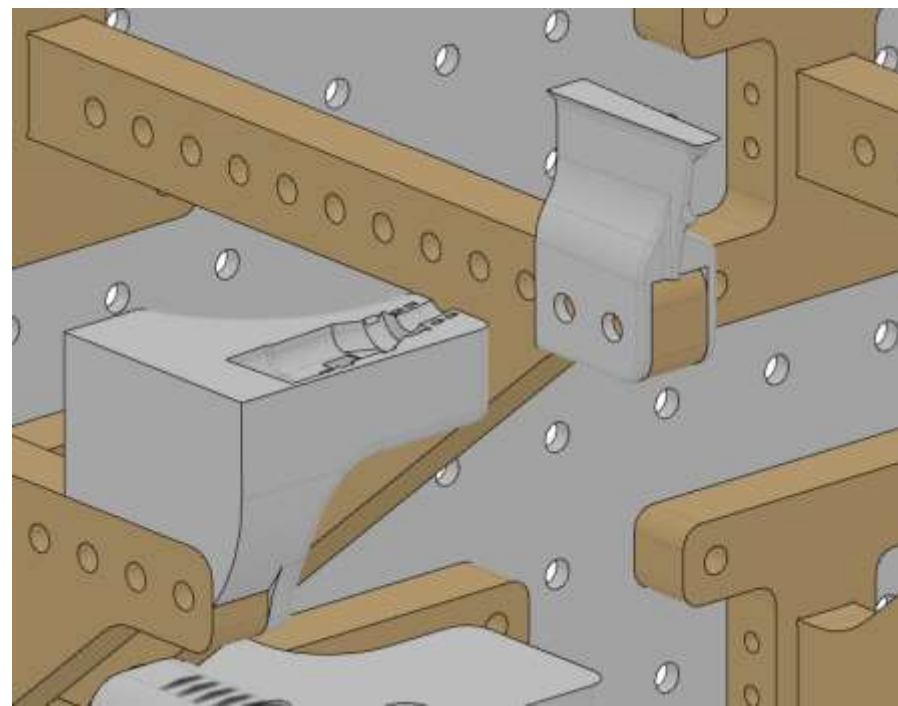
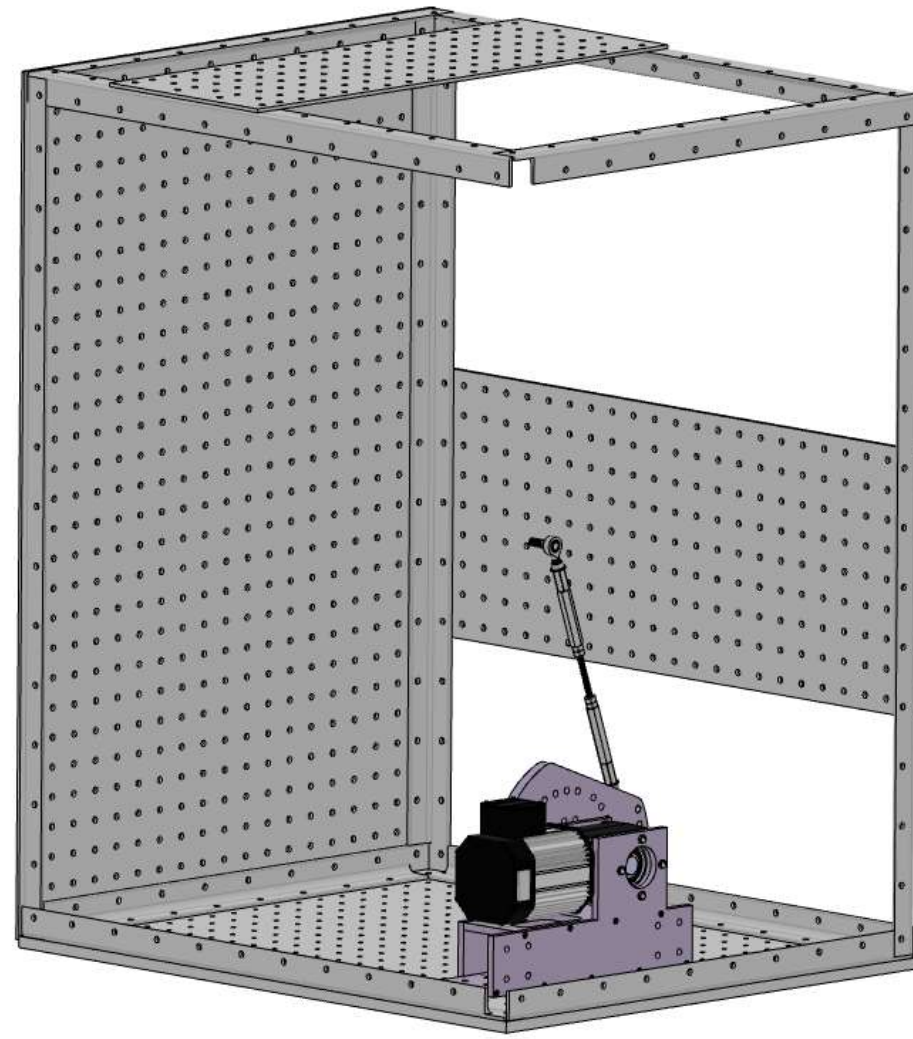
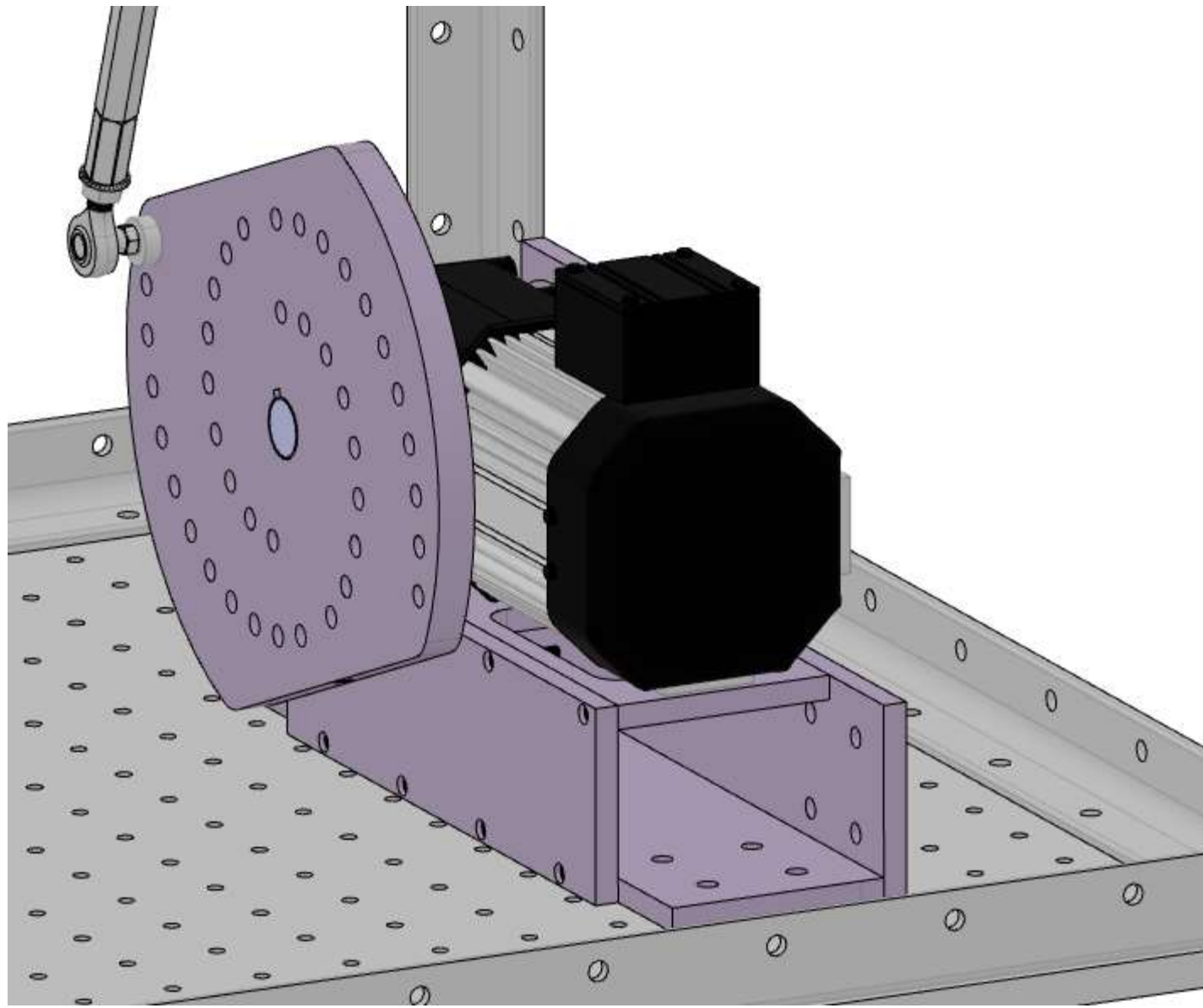
Ran out of time to make proper school presentation.

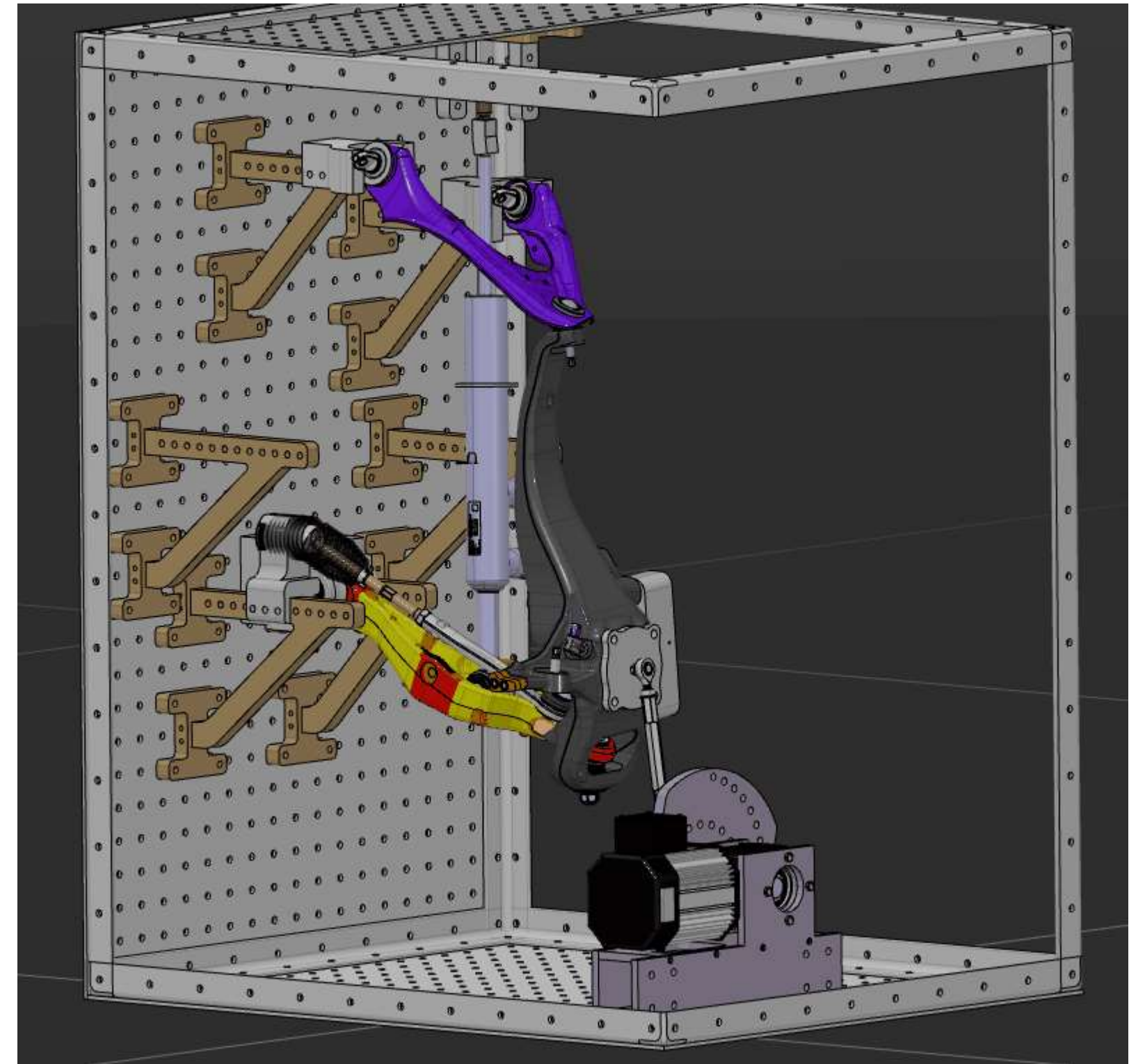
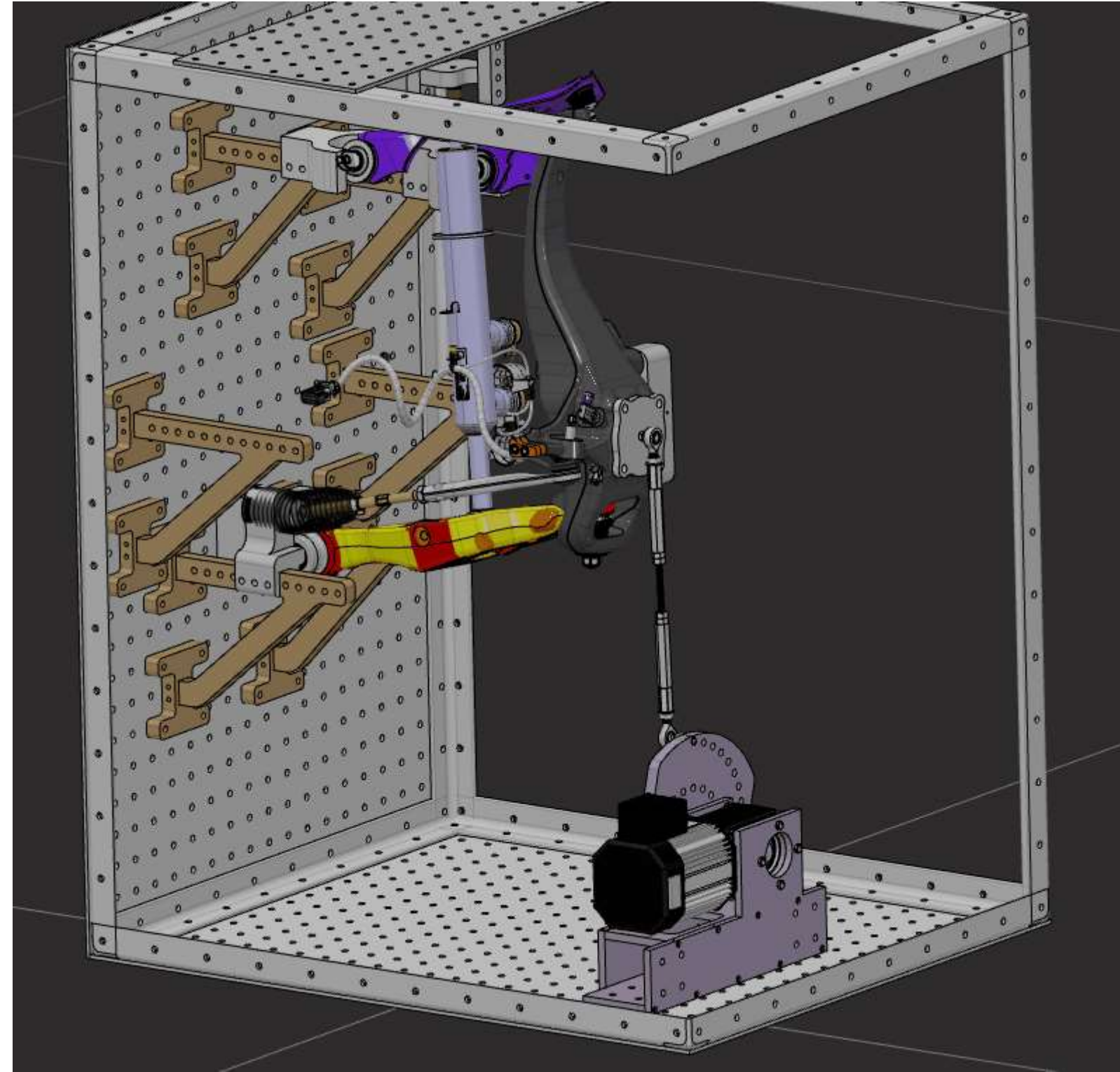
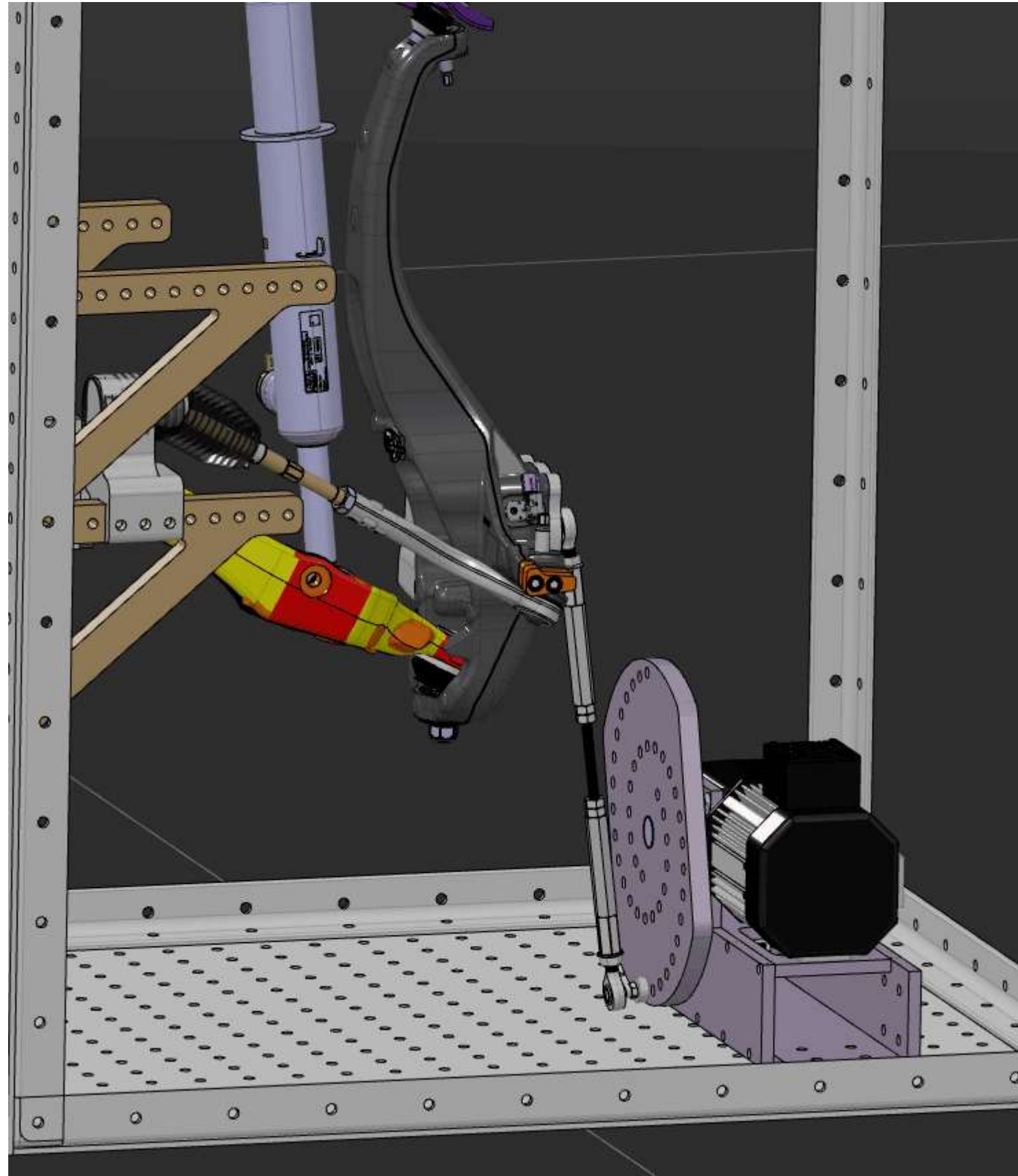
PP includes slides from internal presentations & pictures of the rig

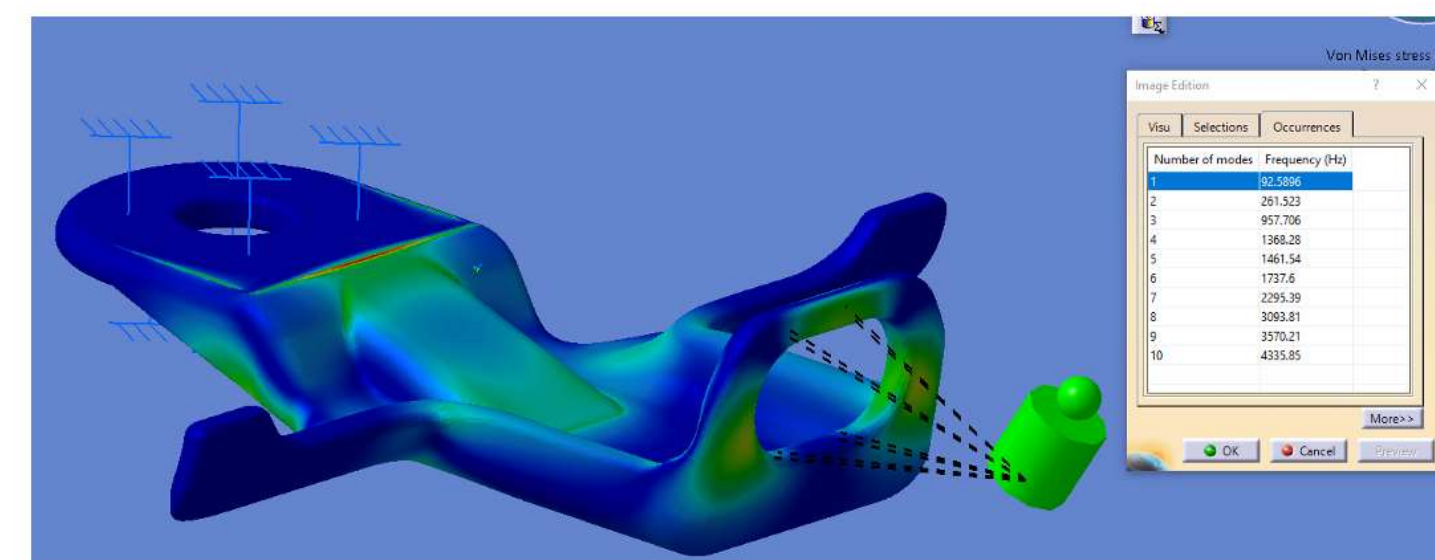
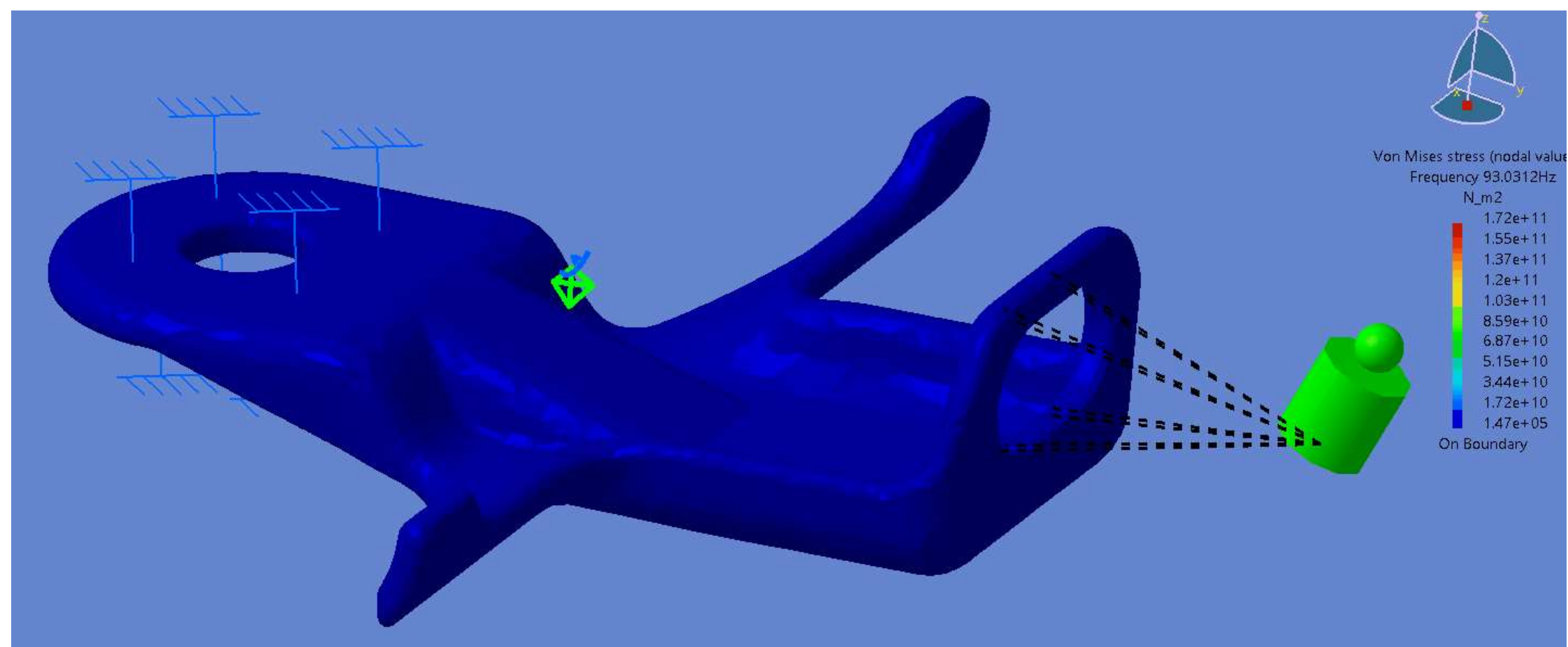
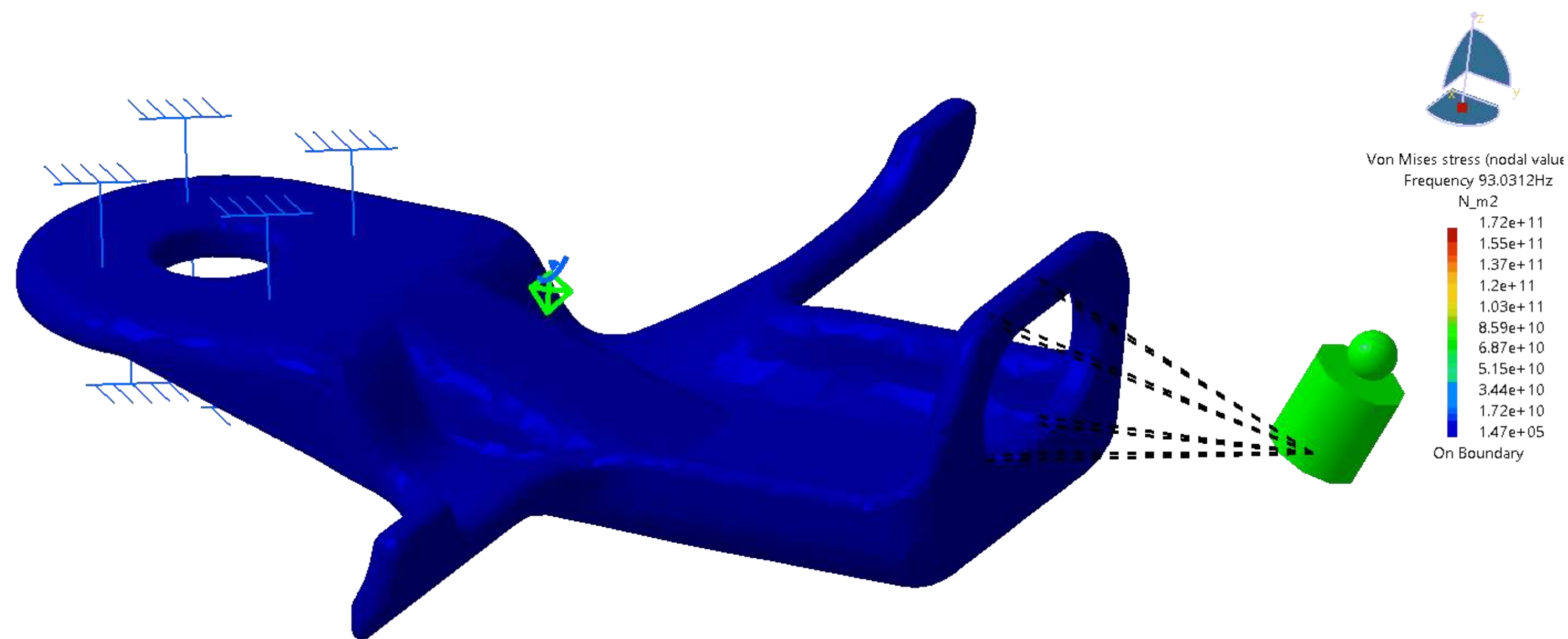
For approval to send off network

Includes

- Stroke testing rig
- Potential M3 mass down rr upper fore link
- CT aeroshield
- CT harness bracket (old)







Gusset Impact

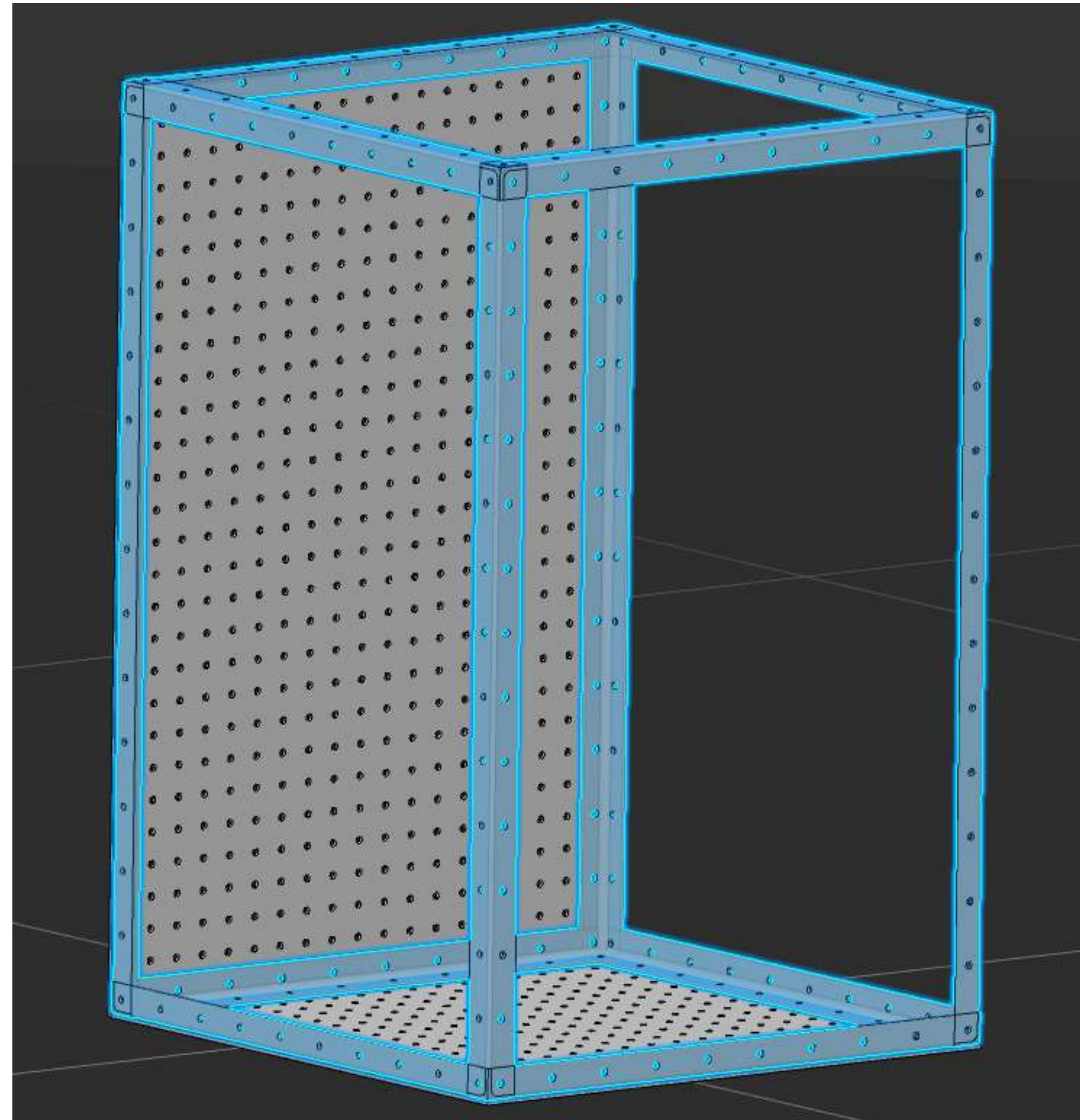
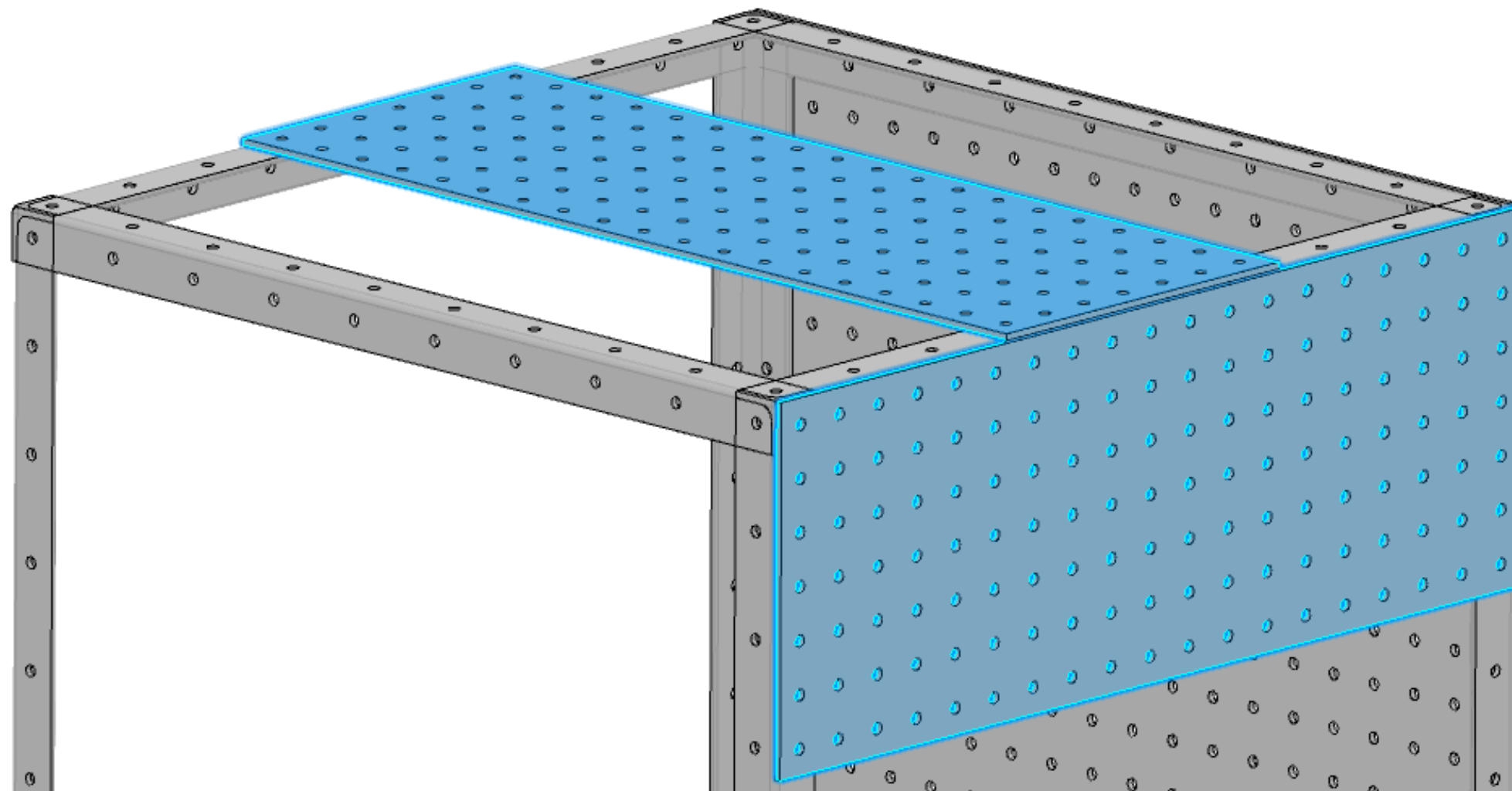
Far end
Without: 74 @ 3.97g
With: 87 @ 4.22g
+Thicken close end: 91 @ 4.33g

Final Solve

- Added gussets
- Increased thk 15%
 - o Linear relationship w resonance

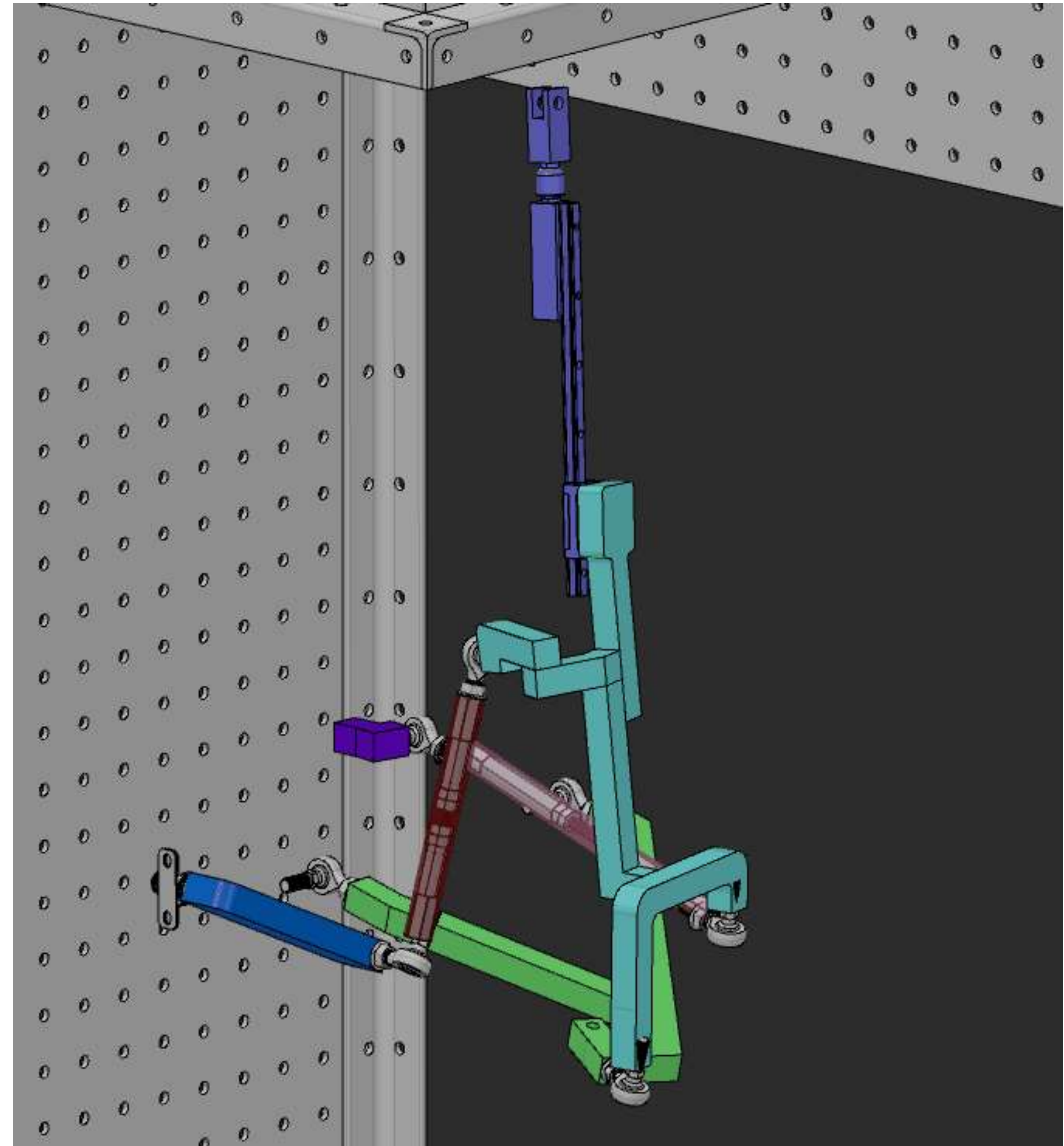
Frame

- 2" Angle iron – 1 x 1 x 1.5m
- ¼" Aluminum pegboard
 - Floor
 - Wall
 - Moveable sections
- Natural frequency $\approx 18\text{Hz}$
- Weight $\approx 100\text{kg}$



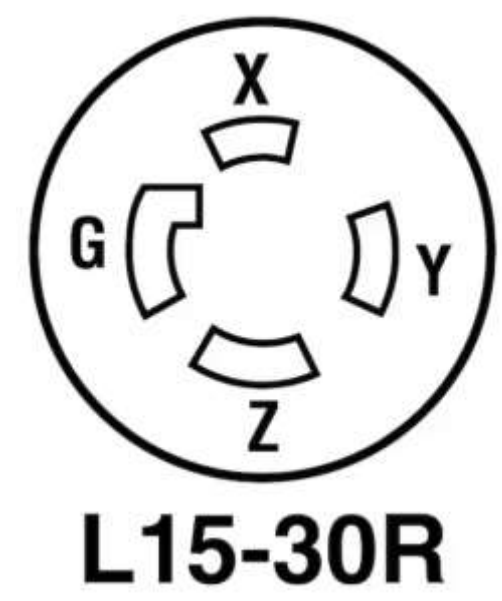
Suspension Quarter

- Adjustable 2-force members
- Water jet aluminum plate
- Linkage
 - ½" BJs & bearings
 - Strut: Ball bearing carriage
 - Ignore compliance
- Harness & hose connections
 - 3D printed mounts



Motor

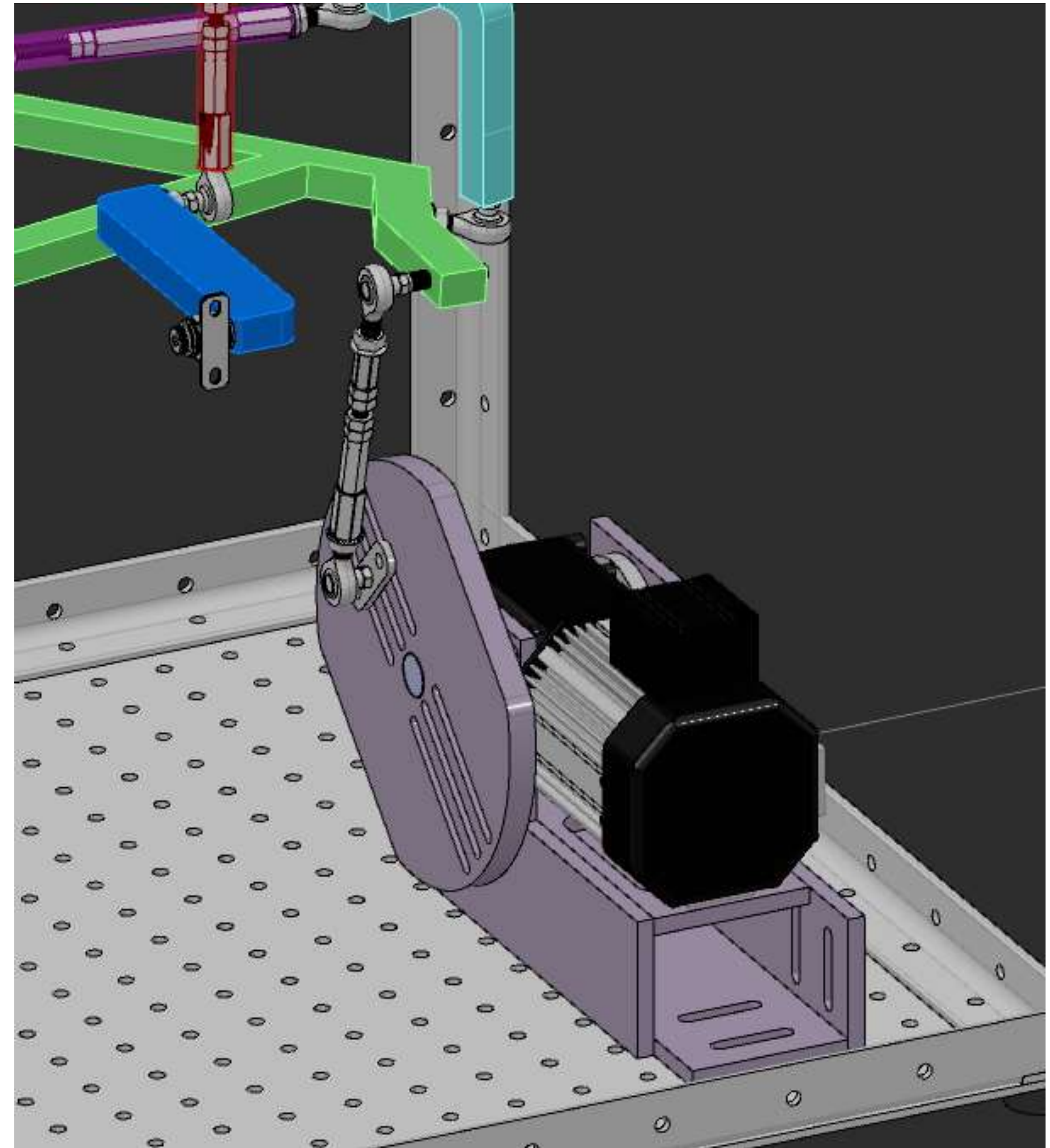
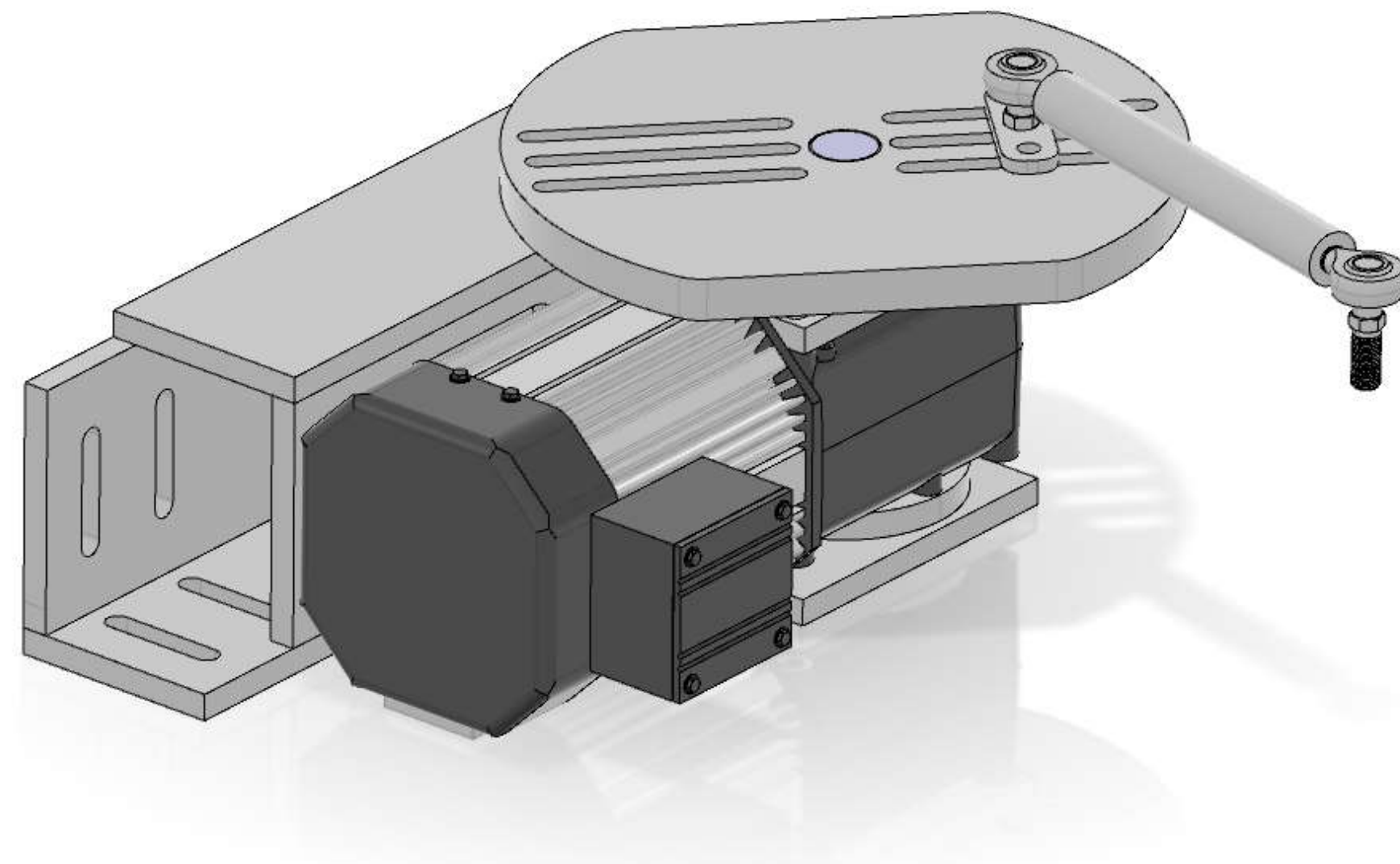
- 3-phase 230V Rotary
 - 160 rpm (2.7Hz)
 - 14 ft*lb
 - Plug type: L15-30P



Product Series	730	Weight (Lbs)	24.6
Speed (RPM)	160	Output Shaft Diameter (In)	1.25
Torque (InLb)	168	Lubrication (Type)	Semi-Fluid Grease
Ratio :1	10	Motor Size Input	NA
Input Hp (HP)	1/2	Construction File	E89715
Input Hp (HP)	0.5	Insulation File	E199928
Volts (V)	230	Construction File	150393
Amps (A)	1.9	CE Certification	Yes
Overhung Load (Lbs)	465	IP Rating	IP54

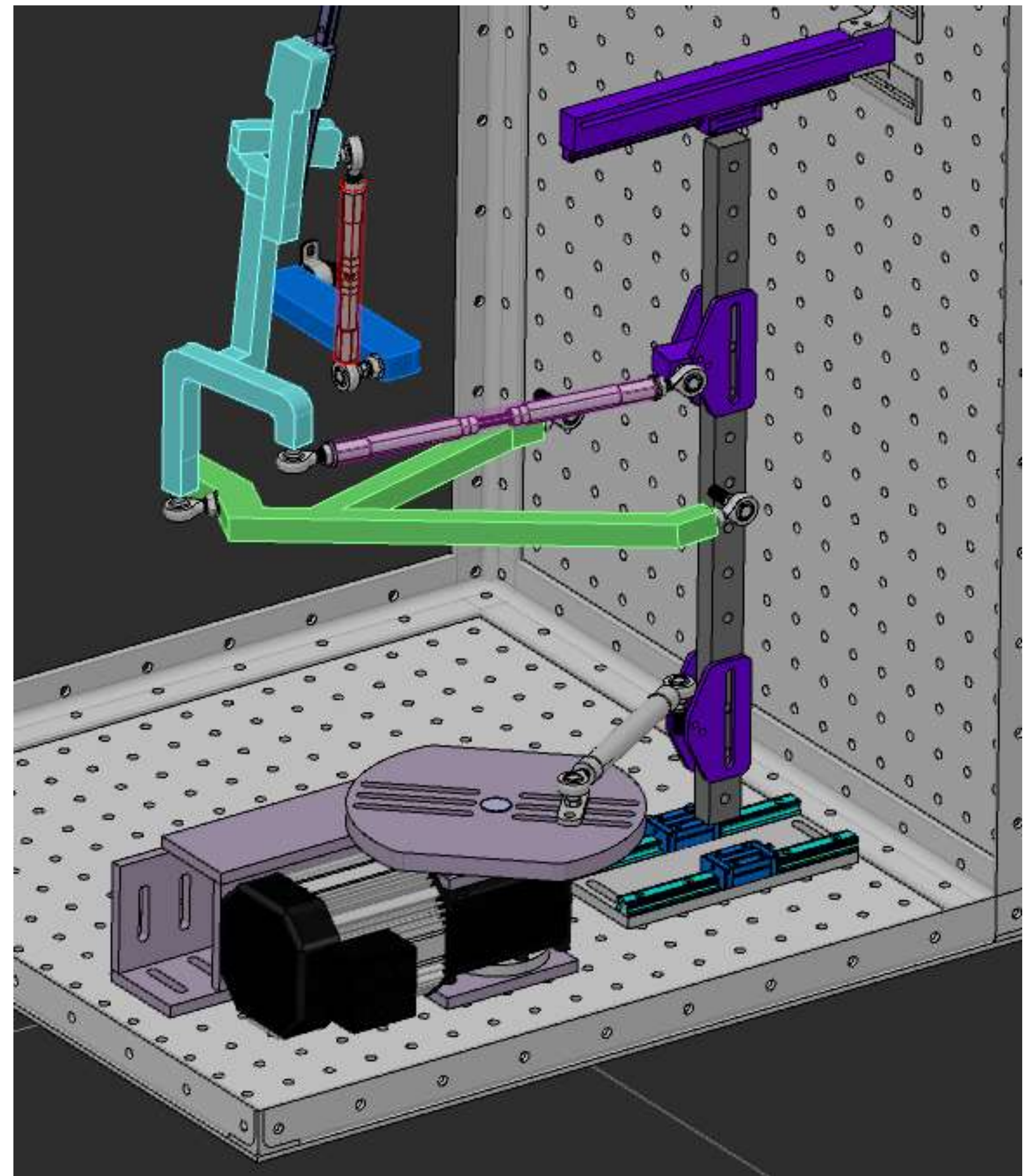
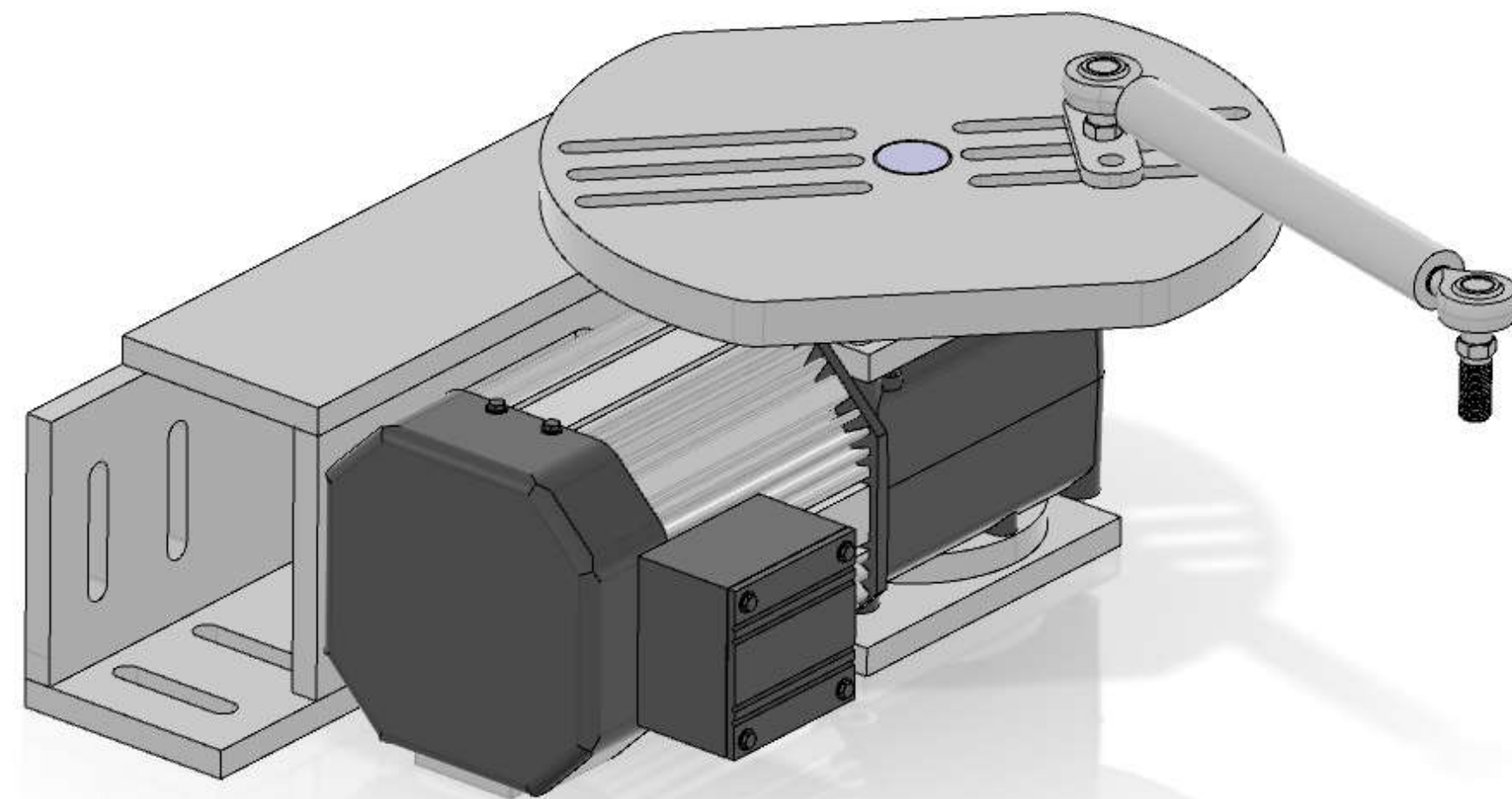
Motor Linkages - Damper

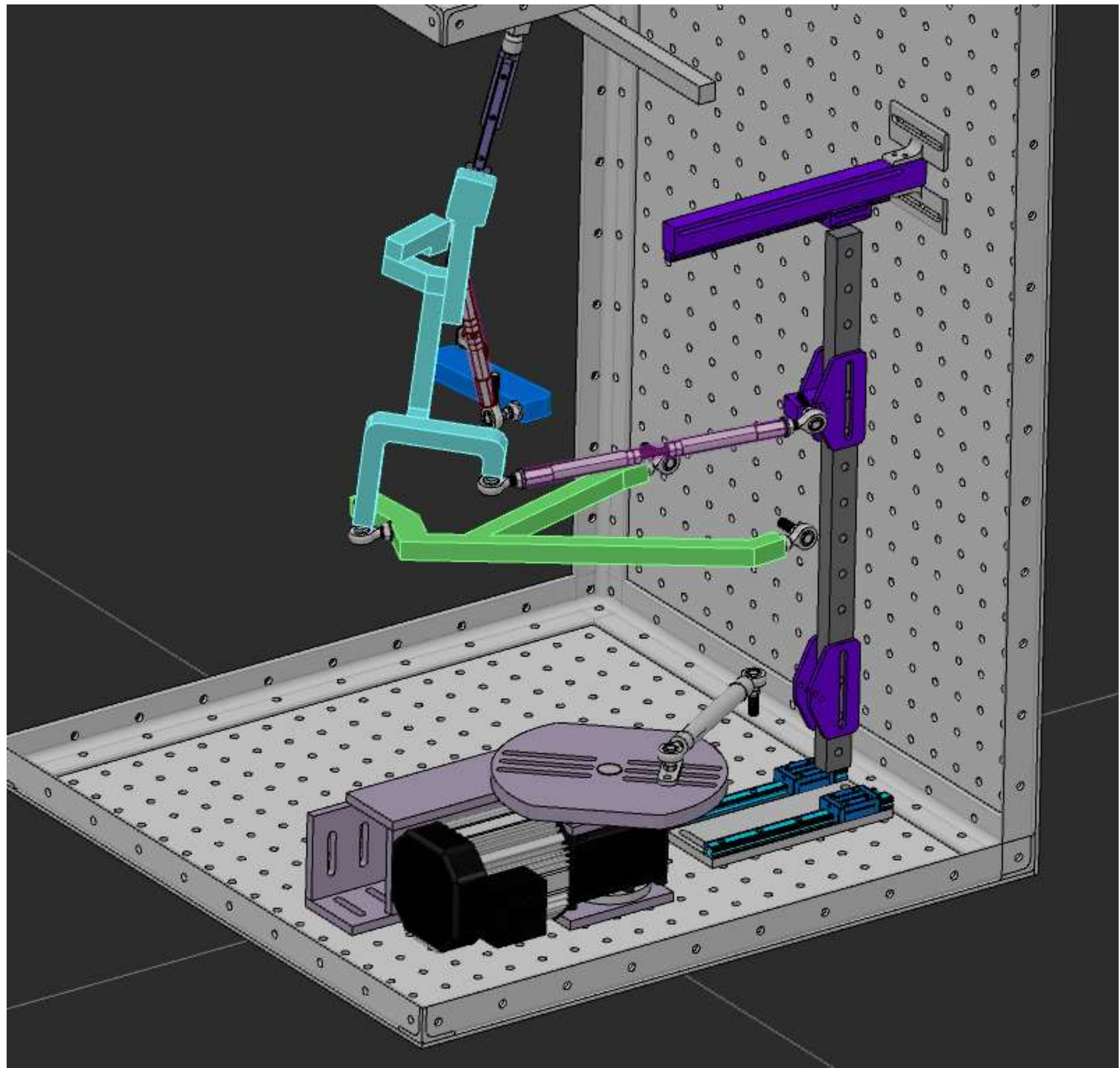
- Adjustable stroke length
 - Continuous vs discrete?
- Link length
 - Adjustable vs fixed?
- Y-compliance via BJ
- Mount on vibration dampeners?



Motor Linkages - Steer

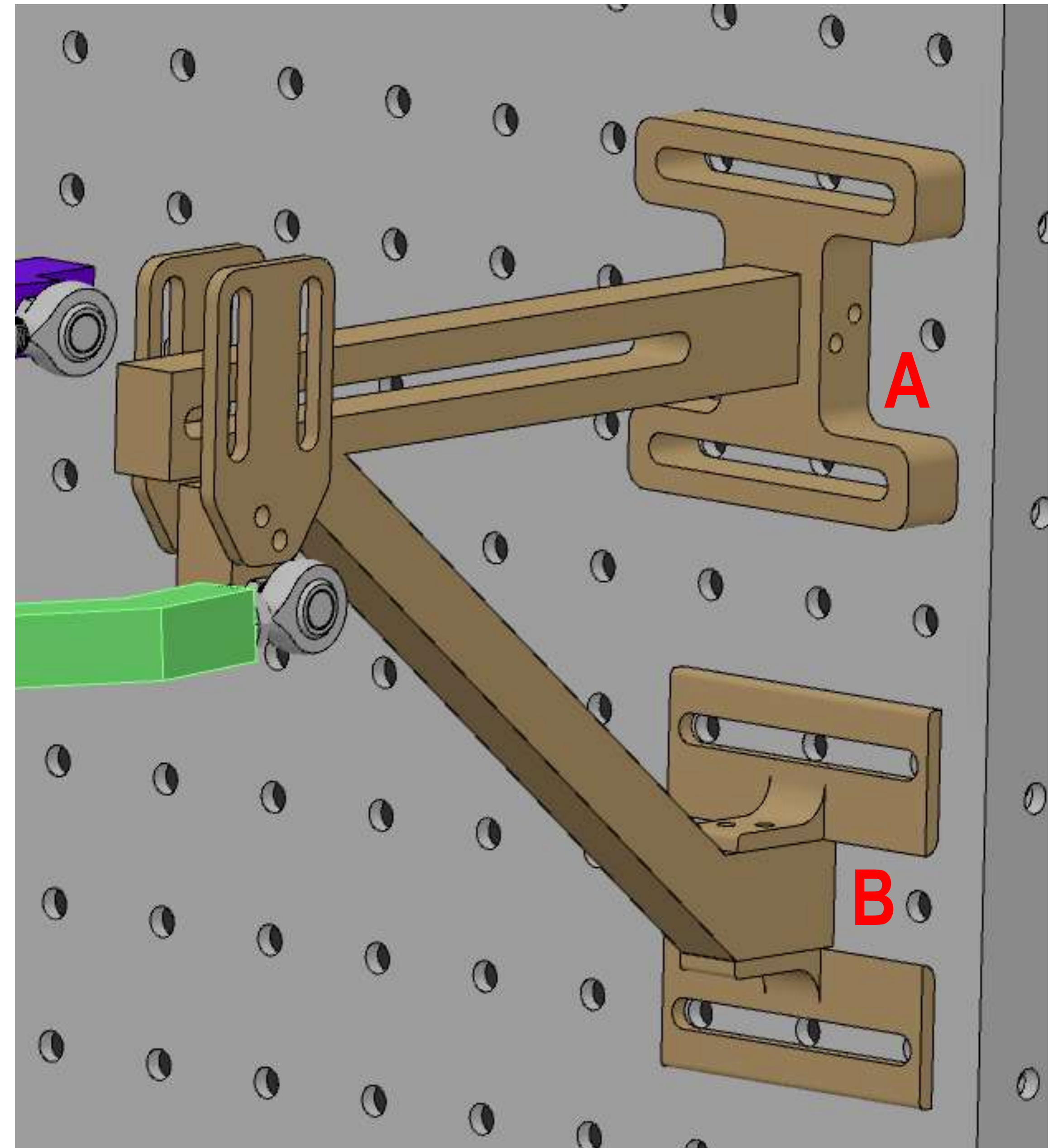
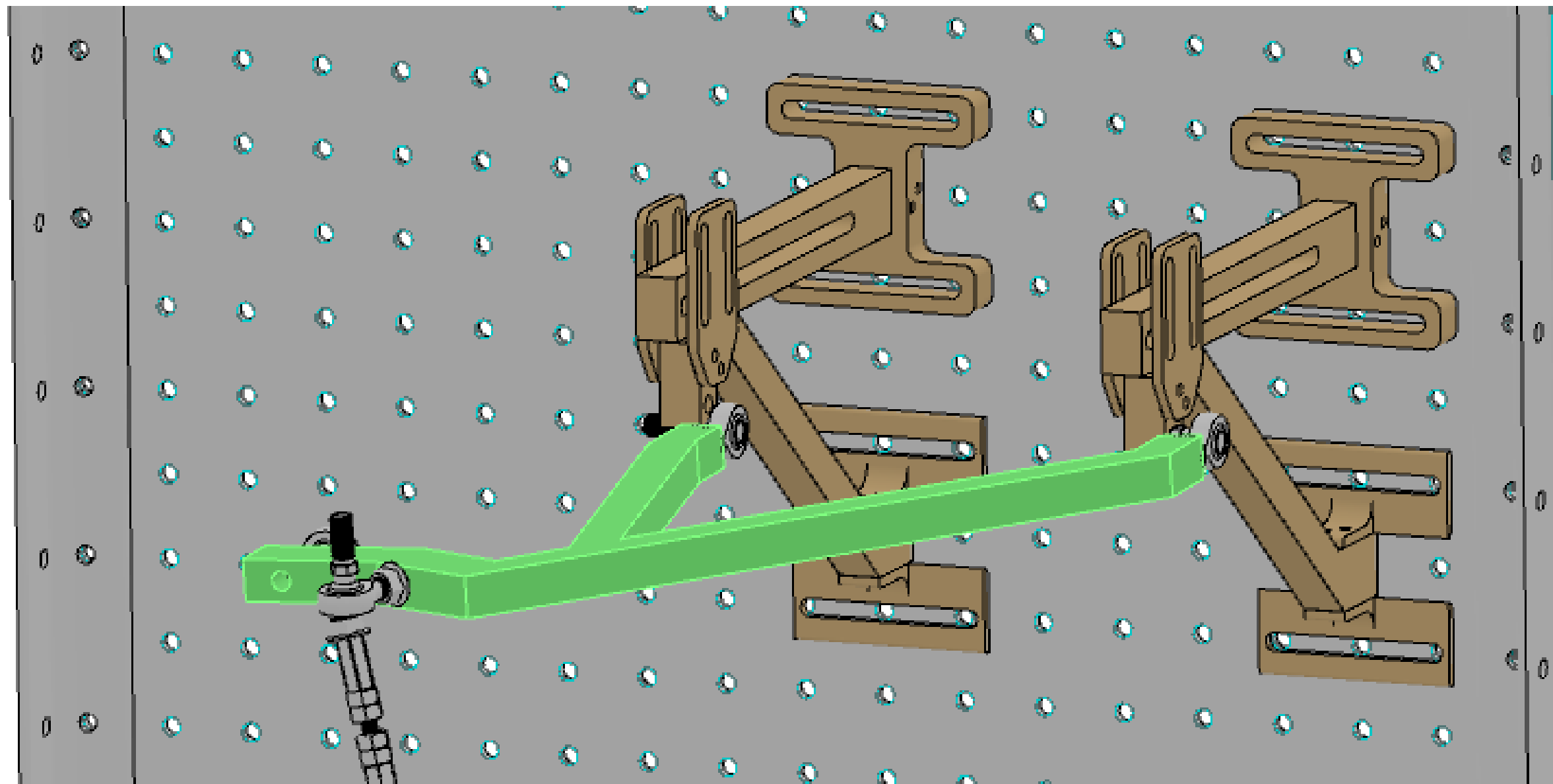
- Adjustable stroke length
 - Continuous vs discrete?
- Link length
 - Adjustable vs fixed?





Mounts - Arm

- Adjustable in x, y, z
- Breadboard mounts
 - A – Water jet 1" aluminum plate (or steel)
 - B – Machined $\frac{1}{4}$ " angle iron



Front Upper Control Arm

- Press bushings out of FUCA
- Press new ball joints into plugs
- Press plugs into FUCA



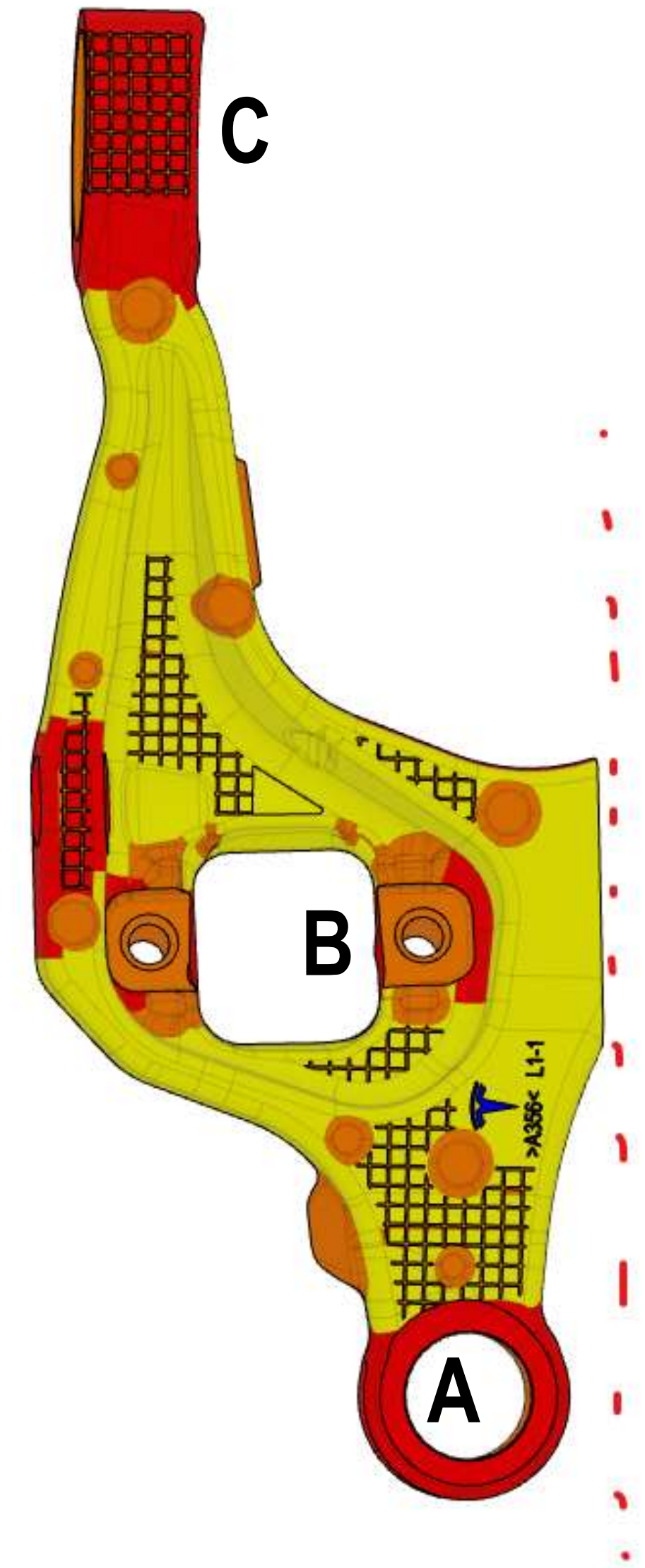
Front Lower Control Arm

- Press bushing out of FLCA
- Press plug into FLCA
- NOTE: FLCA is not currently cut. If KFS can support the cut as well please see following slide, otherwise this can be done by a separate team after this task



Front Lower Control Arm Cut

- FLCA aft arm to be removed
- Features that must remain undamaged:
 - A
 - B
 - C



Project Constraints

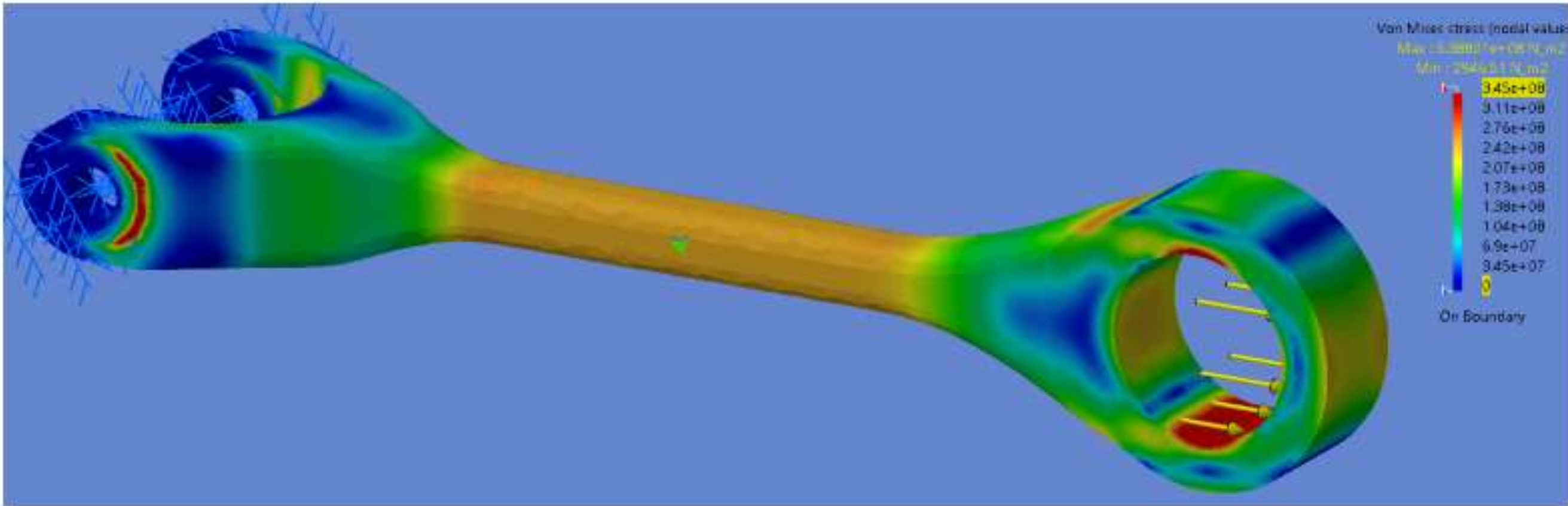
	Target	Previous	Achieved	Comments
Mass (kg)	<562	687	464	-0.446kg per vehicle
Compression/ Tension (KN)	>60KN	90KN	90KN	Will fail in buckling
Clevis Stiffness (KN/mm)		14.2	8.7	Previous in this case is MY forged Must be <= previous

Task: Design forged Al link to replace stamped steel link

Objective: Mass down

Strength Validation

Catia Yield Check



Forged Al NV35, 60KN - Al NV35 Upper Fore Link Development V2.CATAnalysis

Colors: 0 - 100% yield

79% at corners

76% in bar

6110-T6 Aluminum

Yield: 345Mpa

Mass: 475g

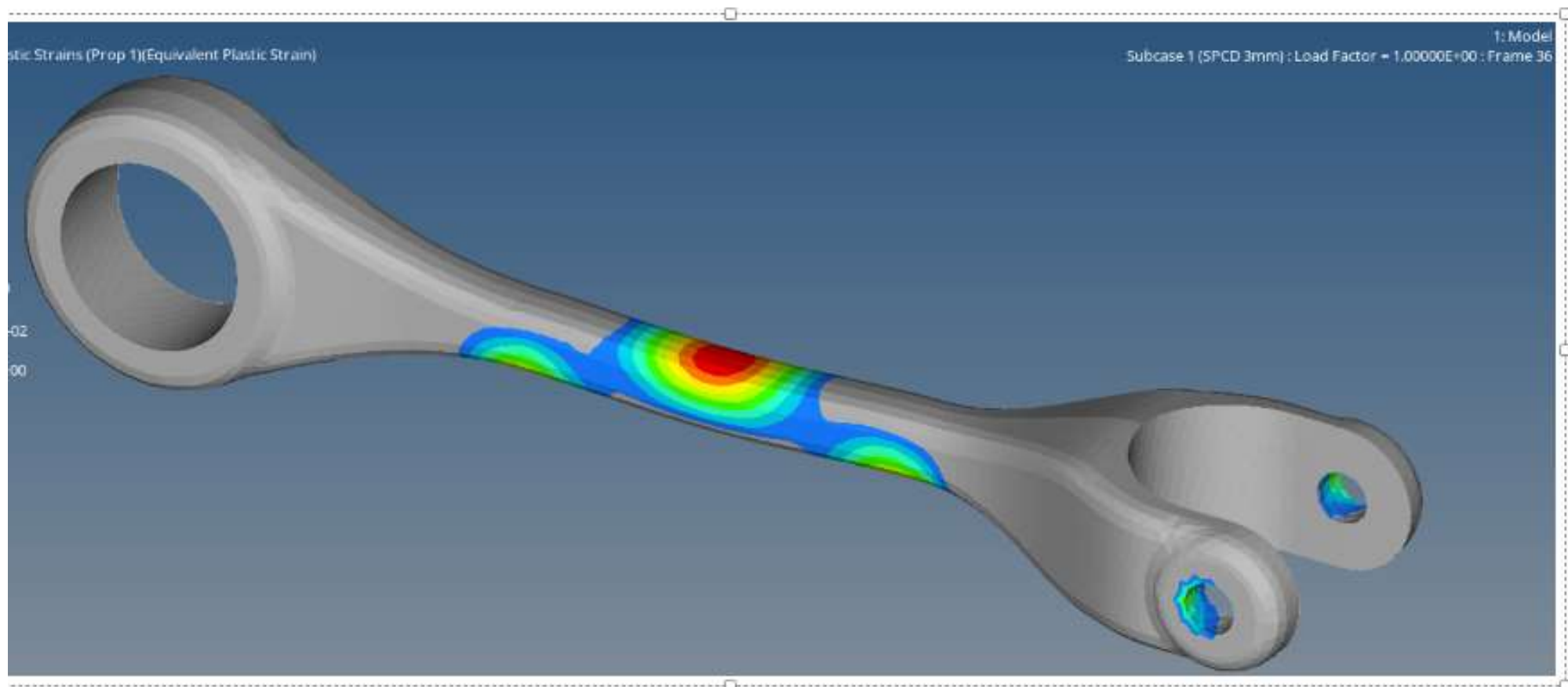
16x16

Mass down: 212g

Total Mass Down: 424g

Buckling Analysis Sim (Hypermesh)

Results: 80KN, 3mm displacement



Strength Validation

Buckling Hand Calculations

$$F_{cr} = \frac{\pi^2 EI}{l^2} \quad \begin{array}{l} E = 69\text{GPa} \\ I = 4.43 \text{ e-}9 \text{ m}^2, \text{ for length} = \text{width} = 0.016\text{m} \end{array}$$

Knowing that $F = 80\text{KN}$ from hypermesh sim, we can solve for effective length
 $l = .194\text{m}$

Now to design for 90KN , using $l = .194\text{m}$, we can solve for required moment of inertia
 $I = 5 \text{ e-}9\text{m}^2$

This corresponds to a side length of 0.0165m , or **16.5mm**

NOTE: Moment of inertia I is calculated for a square cross section with 5mm fillets
- This website is great & reliable

Other Design Considerations

Split line

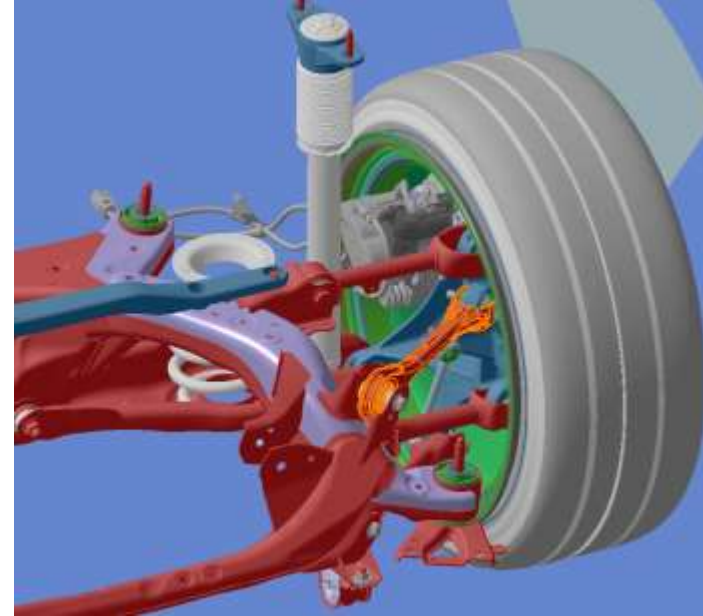
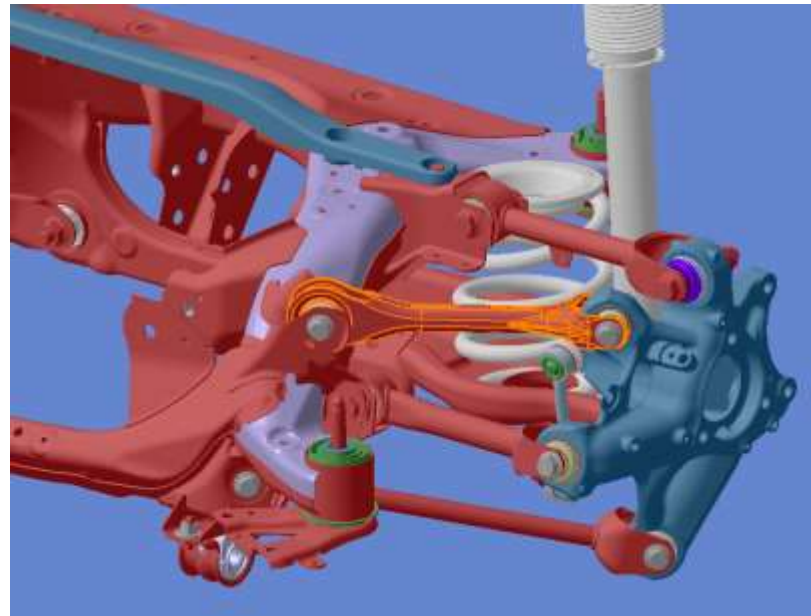
- Plane chosen for least possible machining

Clevis geometry

- Matched to current MY forged AI design
- Lower clevis stiffness

Next Steps

- LO Check
 - Current design lies within the bounding boxes of existing stamped & forged parts, but a check should still be performed
- Drawing Feedback
 - Module & part level drawing submitted to Steve for review
- DFM Feedback
- RFQ



Final Design Thickness

$$F_{cr} = \frac{\pi^2 EI}{l^2} = \dots = 80 \text{ kN}$$

Where

$$E = 69 \text{ GPa}, I = 4.43 \text{ e-9 m}^2$$

Solving

$$l = .194 \text{ m}, \rightarrow 16.5 \times 16.5 \text{ for } 90 \text{ kN}$$

$$17 \times 17 \text{ for } 104 \text{ kN}$$

l - effective length found from
buckling analysis sim results.

- Have force, solve for *l*

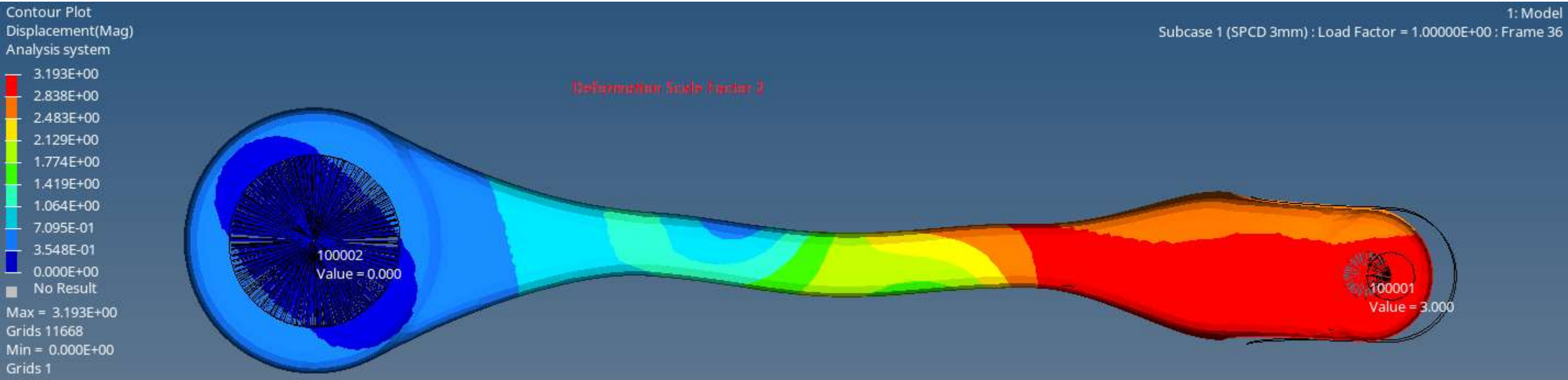
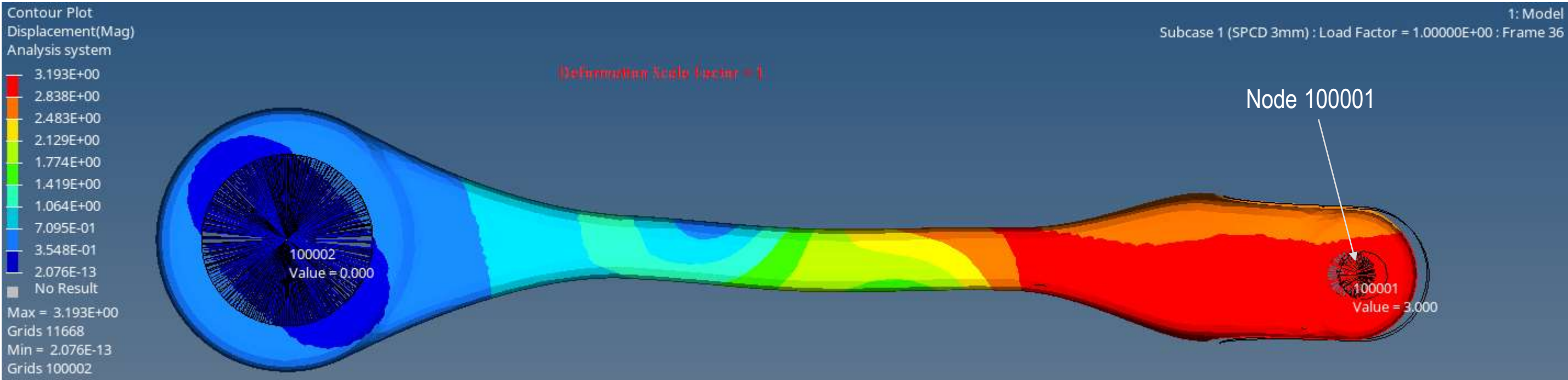
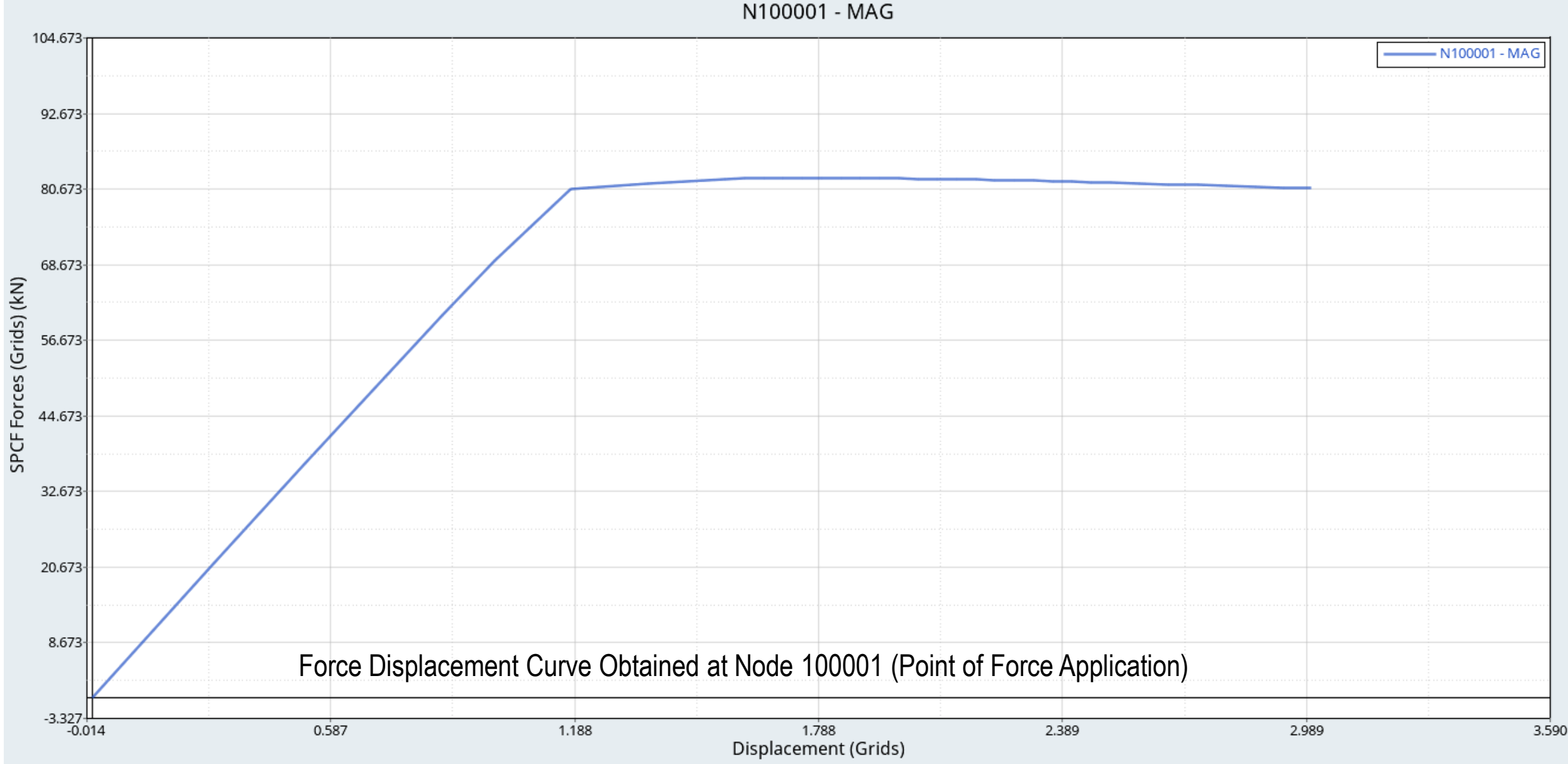
Summary

Objective: Determine compression load at which the link fails in buckling.

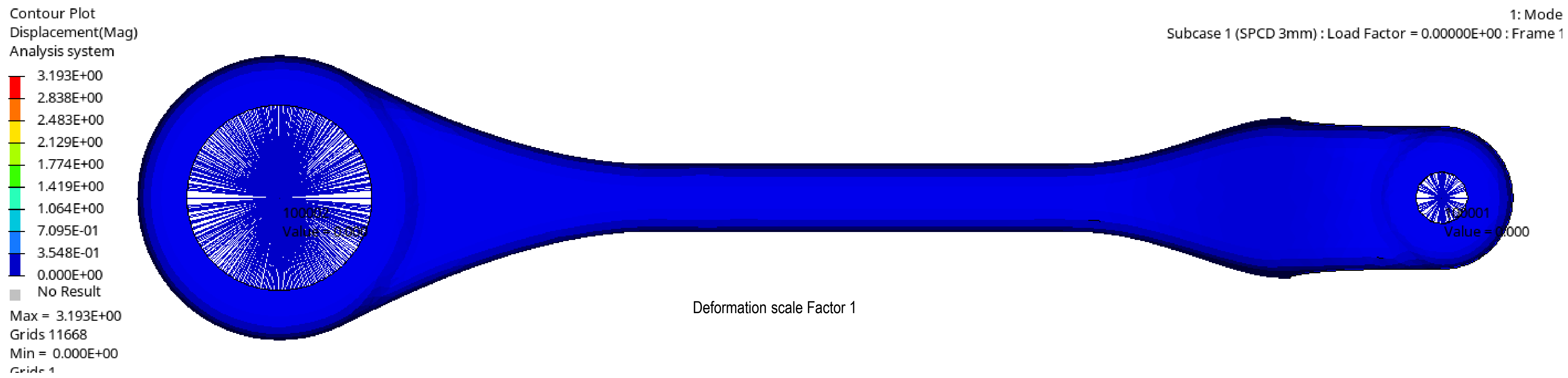
Conclusion: Buckling Load = **80 kN**

(Refer Force-displacement curve)

Enforced Displacement = 3mm at Node 100001



Animation

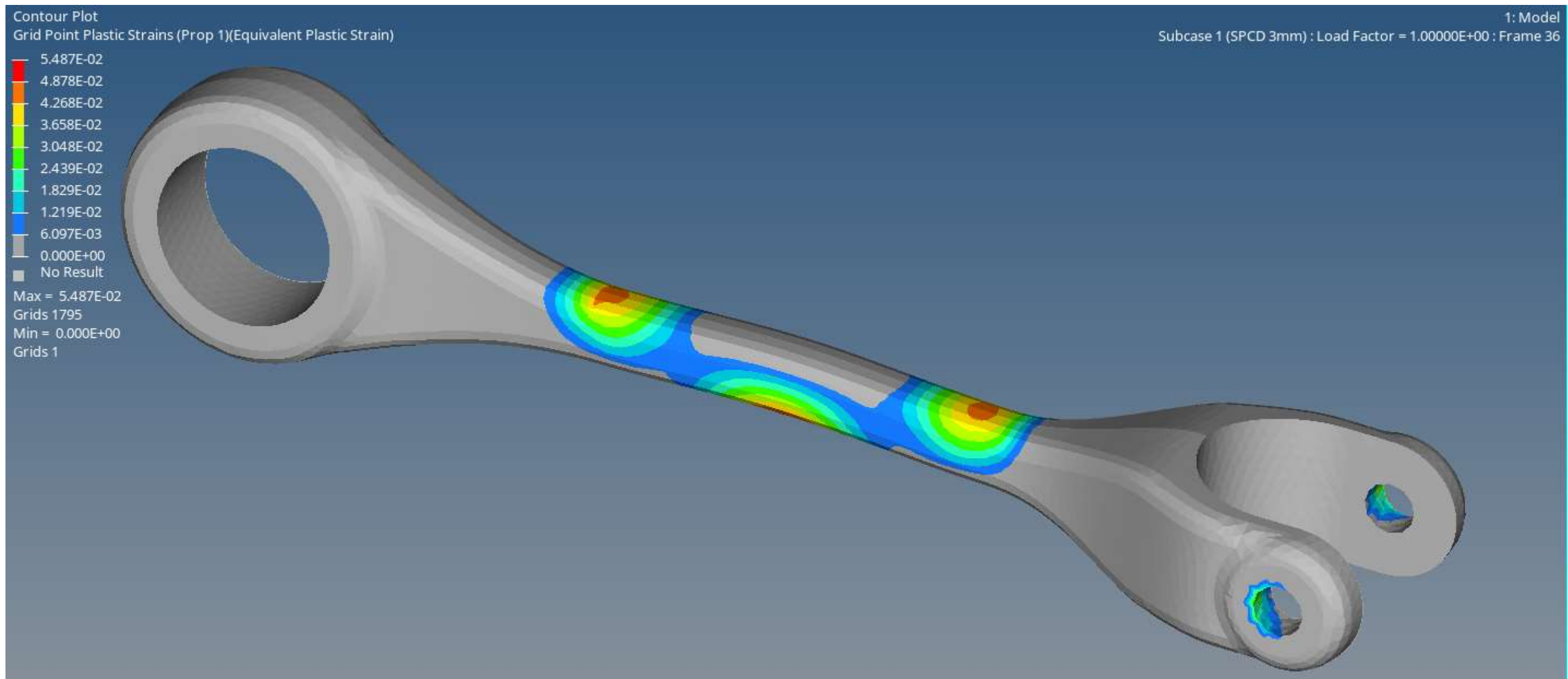
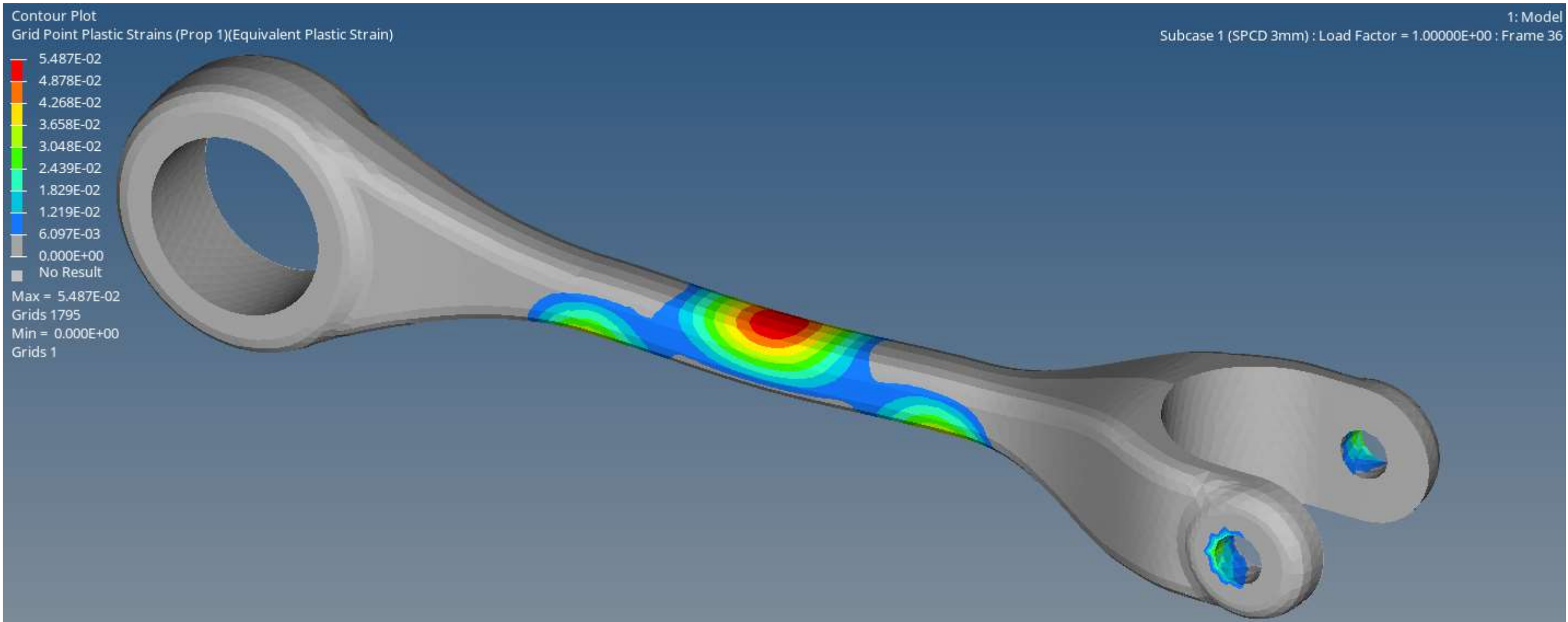


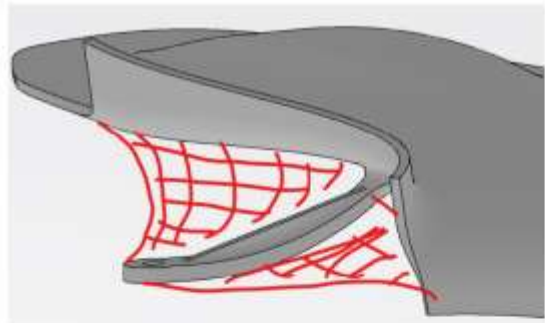
Plastic Strain

Tensile Elongation Uniform = 0.091

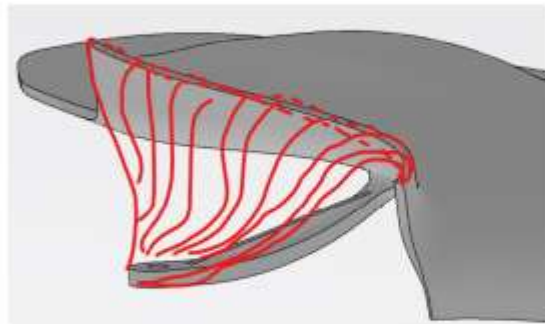
Tensile Elongation Total = 0.12

Max Plastic Strain in part = 0.055

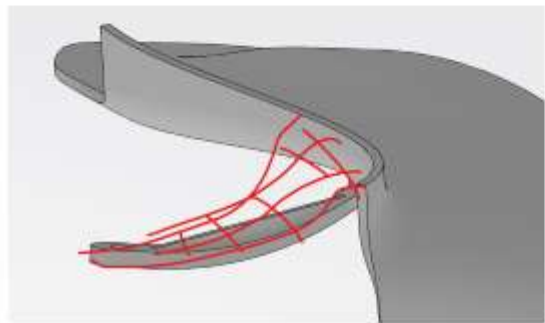




Not moldable



Too much



Yeah BUDDY

