

第五章作业分享





纲要



- > MPC Cost Function
- > MPC Equality Constraints

MPC Cost Function



- Objective 1: Keep close to reference values
- Objective 2: Avoid to actuate as much as possible
- Objective 3: Enforce actuators smoothness in change

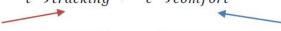
The objective function has different types of components:

Tracking objectives (Reference from planner)

Comfort objectives (Comfortability of vehicle motion, perceived danger)

Different weights can be applied to separate cost terms in order to favor a certain trade-off.

$$J = w_t \cdot J_{tracking} + w_c \cdot J_{comfort}$$



MPC Cost Function



• Objective 1: Keep close to reference values

```
J = w_t \cdot J_{tracking}
```

posion error, e_p + velocity error, e_v + heading error, e_{φ}

```
/* TODO: Objective term 1: Keep close to reference values.*/
for (size_t t = 0; t < Np; t++)
{
    // See below in mpc_controller::Solve() for reference of vars, Np, and Nc
    // (1) error
    // NOTE: reported error: no suitable conversion function from "CppAD::AD<double>" to "double" exists
    CppAD::AD<double> e_cte = vars[cte_start + t] - ref_cte;
    CppAD::AD<double> e_epsi = vars[epsi_start + t] - ref_epsi;
    CppAD::AD<double> e_v_longitudinal = vars[v_longitudinal_start + t] - ref_v; // ref_v should be the longitudinal velocity
    // (2) quadratic cost function
    fg[0] += cte_weight * pow(e_cte, 2);
    fg[0] += epsi_weight * pow(e_epsi, 2);
    fg[0] += v_weight * pow(e_v_longitudinal, 2);
}
```

MPC Cost Function



- Objective 2: Avoid to actuate as much as possible
- Objective 3: Enforce actuators smoothness in change

```
control input: steering, \delta, \dot{\delta} + accel, a, \dot{a}
```

 $W_c \cdot J_{comfort}$

```
TODO: Objective term 2: Avoid to actuate as much as possible, minimize the use of actuators.*/
for (size t t = 0; t < Nc; t++)
    fg[0] += steer actuator cost weight fg * pow(vars[front wheel angle start + t], 2);
    fg[0] += acc actuator cost weight fg * pow(vars[longitudinal acceleration start + t], 2);
   TODO: Objective term 3: Enforce actuators smoothness in change, minimize the value gap between sequential actuation.*/
   (size t t = 0; t < Nc - 1; t++)
   // NOTE: front wheel angle increment start & longitudinal acceleration increment start are commented?
   CppAD::AD<double> change steer = vars[front wheel angle start + t + 1] - vars[front wheel angle start + t];
   CppAD::AD<double> change accel = vars[longitudinal acceleration start + t + 1] - vars[longitudinal acceleration start + t];
   // (2) quadratic cost function
    fg[0] += change steer cost weight * pow(change steer, 2);
    fg[0] += change accel cost weight * pow(change accel, 2);
```

纲要



- > MPC Cost Function
- **► MPC Equality Constraints**

Dynamic Bicycle Model



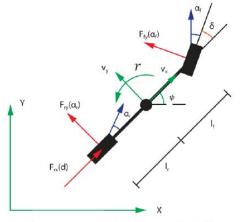
	全局坐标系位置约束	<i>x</i> , <i>y</i>
--	-----------	---------------------

• 航向角约束

• 车辆纵向速度约束 v_x

 \bullet 车辆侧向速度约束 v_y

● 车辆横摆角速度约束 r



$$\dot{x} = v_x \cos(\psi) - v_y \sin(\psi)$$

$$\dot{y} = v_x \sin(\psi) + v_y \cos(\psi)$$

$$\dot{\varphi} = r$$

$$\dot{v_x} = \frac{1}{m} (F_{r,x} - F_{f,y} \sin(\delta) + mv_y r)$$

$$\dot{v_y} = \frac{1}{m} (F_{r,y} + F_{f,y} \cos(\delta) - mv_x r)$$

$$\dot{r} = \frac{1}{I_z} (F_{f,y} l_f \cos(\delta) - F_{r,y} l_r)$$



● 全局坐标系位置约束 x, y

$$\dot{x} = v_x \cos \psi - v_y \sin \psi$$

$$\dot{y} = v_x \sin \psi + v_y \cos \psi$$

$$x_{k+1} = x_k + \dot{x}\Delta t$$

$$y_{k+1} = y_k + \dot{y}\Delta t$$

```
// Approach II: Reference to Eq 1, 2 of "Dynamic Bicycle Model" in Lecture Slide 5 P33
CppAD::AD<double> vx_in_world_frame = v_longitudinal_0 * cos(psi_0) + v_lateral_0 * (-sin(psi_0));
CppAD::AD<double> vy_in_world_frame = v_longitudinal_0 * sin(psi_0) + v_lateral_0 * cos(psi_0);
fg[1 + x_start + t] = x_1 - (x_0 + vx_in_world_frame * dt);
fg[1 + y_start + t] = y_1 - (y_0 + vy_in_world_frame * dt);
```



●航向角约束





$$\dot{\psi} = \frac{v}{I} \tan \delta$$

Kinematic Bicycle Model

$$\dot{\psi} = r$$

$$\psi_{k+1} = \psi_k + \dot{\psi}\Delta t$$

 $\dot{x} = v_x \cos(\psi) - v_y \sin(\psi)$ $\dot{y} = v_x \sin(\psi) + v_y \cos(\psi)$ $\dot{\varphi} = r$ $\dot{v_x} = \frac{1}{m} (F_{r,x} - F_{f,y} \sin(\delta) + mv_y r)$ $\dot{v_y} = \frac{1}{m} (F_{r,y} + F_{f,y} \cos(\delta) - mv_x r)$ $\dot{r} = \frac{1}{L} (F_{f,y} l_f \cos(\delta) - F_{r,y} l_r)$



● 车辆纵向速度约束

$$v_x$$

$$\dot{v}_x = \frac{1}{m} (F_{xr} - F_{fy} \sin \delta + m v_y r)$$

$$\begin{aligned}
\dot{v}_x &= a_x \\
v_{x_{k+1}} &= v_{x_k} + \dot{v}_x \Delta t
\end{aligned}$$

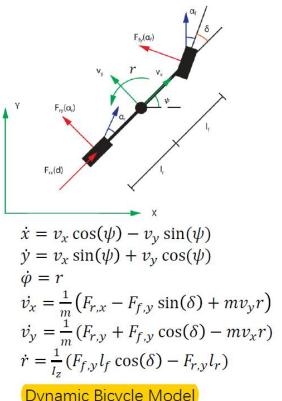
```
longitudinal velocity constraint is v long 1 = v long 0 + a long * dt
fg[1 + v longitudinal start + t] = v longitudinal 1 - (v longitudinal 0 + longitudinal acceleration 0 * dt);
```



车辆侧向速度约束

$$v_{\nu}$$

$$\begin{split} \dot{v_y} &= \frac{1}{m} (F_{yr} - F_{fy} \cos \delta - m v_x r) \\ F_{yf} &= 2 c_f \left(\delta - \theta_{vf} \right) \\ F_{yr} &= 2 c_r (-\theta_{vr}) \\ \theta_{vf} &= \tan^{-1} \left(\frac{v_y + l_f r}{v_x} \right) \\ \theta_{vf} &= \tan^{-1} \left(\frac{v_y + l_f r}{v_x} \right) \\ v_{y_{k+1}} &= v_{y_k} + \dot{v_y} \Delta t \end{split}$$





● 车辆侧向速度约束

$$\begin{split} \dot{v_y} &= \frac{1}{m} \big(F_{yr} - F_{fy} \cos \delta - m v_x r \big), \ F_{yf} = 2 c_f \big(\delta - \theta_{vf} \big), \ F_{yr} = 2 c_r (-\theta_{vr}) \\ \theta_{vf} &= \tan^{-1} \big(\frac{v_y + l_f r}{v_x} \big), \ \theta_{vf} = \tan^{-1} \big(\frac{v_y + l_f r}{v_x} \big) \\ v_{y_{k+1}} &= v_{y_k} + \dot{v_y} \Delta t \end{split}$$

 v_{ν}

CppAD::AD<double> delta = -front wheel angle 0;

```
/* 车辆侧向速度 */
// Reference to Eq 5 of "Dynamic Bicycle Model" in Lecture Slide 5 P33
// (1) tire forces
// Reference to Lecture Slide 4 P11 "Front and Rear Tire Forces"

CppAD::AD<double> theta_vf = atan((v_lateral_0 + lf * yaw_rate_0) / v_longitudinal_0);

CppAD::AD<double> F_yf = 2 * Cf * (delta - theta_vf);

CppAD::AD<double> theta_vr = atan((v_lateral_0 - lr * yaw_rate_0) / v_longitudinal_0);

CppAD::AD<double> F_yr = 2 * Cr * (-theta_vr);

// (2) Derive tire forces into Eq 5 to obtain a_lateral, denoted as dot_v_y in Eq 5

CppAD::AD<double> lateral_acceleration = (1 / m) * (F_yr + F_yf * cos(delta) - m * v_longitudinal_0 * yaw_rate_0);

// (3) lateral velocity constraint is v_lateral_1 = v_lateral_0 + a_lateral * dt

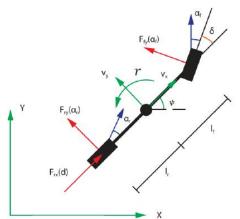
fg[1 + v_lateral_start + t] = v_lateral_1 - (v_lateral_0 + lateral_acceleration * dt);
```



●车辆横摆角速度约束

$$\dot{r} = \frac{1}{I_z} (F_{yf} l_f \cos \delta - F_{fy} l_r)$$
$$r_{k+1} = r_k + \dot{r} \Delta t$$

```
/* 车辆模摆角速度 */
// Reference to Eq 6 of "Dynamic Bicycle Model" in Lecture Slide 5 P33
// (1) Derive tire forces into Eq 6 to obtain yaw_rate_rate, denoted as dot_r in Eq 6
CppAD::AD<double> yaw_rate_rate = (1 / I) * (F_yf * lf * cos(delta) - F_yr * lr);
// (2) yaw rate constraint is yaw_rate_1 = yaw_rate_0 + yaw_rate_rate * dt
fg[1 + yaw_rate_start + t] = yaw_rate_1 - (yaw_rate_0 + yaw_rate_rate * dt);
```



$$\dot{x} = v_x \cos(\psi) - v_y \sin(\psi)$$

$$\dot{y} = v_x \sin(\psi) + v_y \cos(\psi)$$

$$\dot{\varphi} = r$$

$$\dot{v}_x = \frac{1}{m} (F_{r,x} - F_{f,y} \sin(\delta) + mv_y r)$$

$$\dot{v}_y = \frac{1}{m} (F_{r,y} + F_{f,y} \cos(\delta) - mv_x r)$$

$$\dot{r} = \frac{1}{I_z} (F_{f,y} l_f \cos(\delta) - F_{r,y} l_r)$$

在线问答







感谢各位聆听 Thanks for Listening

