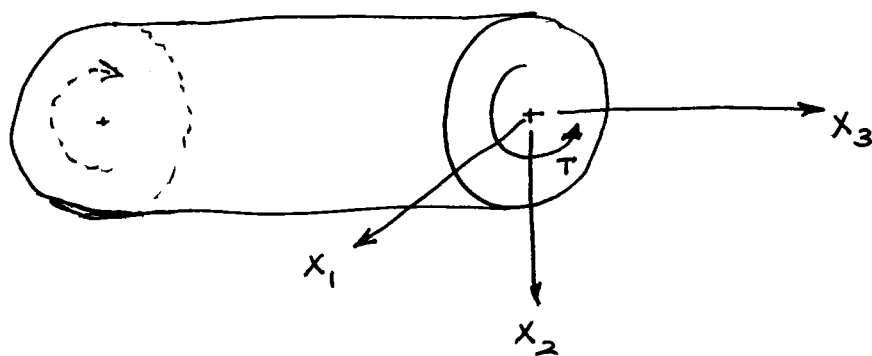


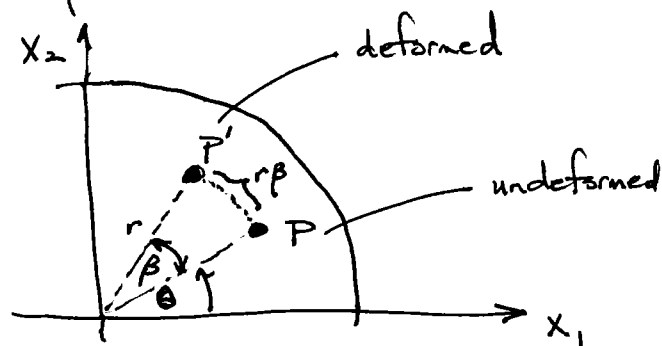
# Torsion



## Observations:

- 1) each section rotates as a rigid body about the center axis,
- 2) for small deformations, rotation is a linear function of axial distance,
- 3) because of symmetry, cross-section remains planar after deformation.

Assume a displacement field:



$$\therefore u_1 = -r\beta \sin\theta = -\beta x_2$$

$$u_2 = r\beta \cos\theta = \beta x_1$$

$$u_3 = 0 \quad (\text{no warping})$$

but we also realize that rotations are linear function of axial coordinate,

$$\beta = \alpha x_3$$

angle of twist per unit length

$$\therefore \begin{array}{l} u_1 = -\alpha x_2 x_3 \\ u_2 = \alpha x_1 x_3 \\ u_3 = 0 \end{array}$$

$\Rightarrow$  candidate displacement field

Strains:

$$\epsilon_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i})$$

$$\epsilon_{11} = u_{1,1} = 0$$

$$\epsilon_{22} = u_{2,2} = 0$$

$$\epsilon_{33} = u_{3,3} = 0$$

$$\epsilon_{12} = \frac{1}{2}(u_{1,2} + u_{2,1}) = \frac{1}{2}(-\alpha x_3 + \alpha x_3) = 0$$

$$\epsilon_{13} = \frac{1}{2}(u_{1,3} + u_{3,1}) = \frac{1}{2}(-\alpha x_2 + 0) = -\frac{\alpha x_2}{2}$$

$$\epsilon_{23} = \frac{1}{2}(u_{2,3} + u_{3,2}) = \frac{1}{2}(\alpha x_1 + 0) = \frac{\alpha x_1}{2}$$

$$\epsilon_{ij} = \begin{bmatrix} 0 & 0 & -\frac{\alpha x_2}{2} \\ 0 & 0 & \frac{\alpha x_1}{2} \\ -\frac{\alpha x_2}{2} & \frac{\alpha x_1}{2} & 0 \end{bmatrix}$$

Stresses:

$$\sigma_{ij} = \lambda \delta_{ij} \epsilon_{kk} + 2\mu \epsilon_{ij}$$

$$\sigma_{13} = -\mu \alpha x_2$$

$$\sigma_{23} = \mu \alpha x_1$$

$$\text{all other } \sigma_{ij} = 0$$

Check equilibrium:

$$\sigma_{ij,j} = 0 \quad (\text{no body forces})$$

$$\cancel{\sigma_{11,1}} + \cancel{\sigma_{12,2}} + \cancel{\sigma_{13,3}} = 0$$

$$0 = 0 \quad \checkmark$$

$$\cancel{\sigma_{21,1}} + \cancel{\sigma_{22,2}} + \cancel{\sigma_{23,3}} = 0$$

$$0 = 0 \quad \checkmark$$

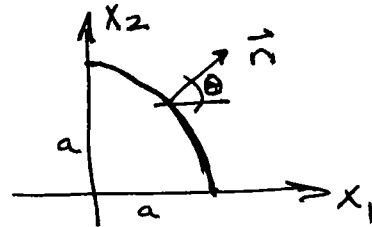
$$\sigma_{13,1} + \sigma_{23,2} + \cancel{\sigma_{33,3}} = 0$$

$$0 + 0 = 0 \quad \checkmark$$

Now, boundary conditions:

later surface:

$$T_i = \sigma_{ij} n_j$$



$$\vec{n} = \{\cos \theta, \sin \theta, 0\} = \left\{ \frac{x_1}{a}, \frac{x_2}{a}, 0 \right\}$$

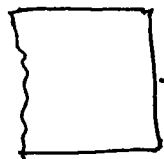
$$T_1 = \cancel{\sigma_{11} n_1} + \cancel{\sigma_{12} n_2} + \cancel{\sigma_{13} n_3} = 0 \quad \checkmark$$

$$T_2 = \cancel{\sigma_{21} n_1} + \cancel{\sigma_{22} n_2} + \cancel{\sigma_{23} n_3} = 0 \quad \checkmark$$

$$T_3 = \sigma_{13} n_1 + \sigma_{23} n_2 + \cancel{\sigma_{33} n_3}$$

$$= -\mu \alpha x_2 \left( \frac{x_1}{a} \right) + \mu \alpha x_1 \left( \frac{x_2}{a} \right) = 0 \quad \checkmark$$

end faces :



$$\vec{n} = \{0, 0, 1\} \quad T_i = \sigma_{ij} n_j$$

$$T_1 = \cancel{\sigma_{11} n_1} + \cancel{\sigma_{12} n_2} + \sigma_{13} n_3$$

$$= \sigma_{13} \quad ?$$

$$T_2 = \sigma_{23}$$

$$T_3 = \sigma_{33} = 0 \quad (\text{satisfied exactly})$$

what about  $(T_1, T_2)$  ?

→ Invoke St. Venant's Principle

$$\therefore \text{want } F_1^{\text{net}} = 0 = \int_A T_1 dA = \int_A \sigma_{13} dA$$

$$\int_A \sigma_{13} dA = -\cancel{\alpha x_1} \int_A x_2 dA$$

$$\text{but } \int_A x_2 dA = 0 \text{ for centroidal axes}$$

$$\therefore F_1^{\text{net}} = 0$$

$$\text{Similarly, } F_2^{\text{net}} = 0$$

} ✓

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$$M_3^{\text{net}} = \text{Avg. Torque} = T \quad \text{applied torque}$$

$$T = \int_A (\sigma_{23} x_1 - \sigma_{13} x_2) dA$$

$$= \int_A (\mu \alpha x_1^2 + \mu \alpha x_2^2) dA$$

$$= \mu \alpha \underbrace{\int_A (x_1^2 + x_2^2) dA}_{J: \text{polar moment of area}}$$

$$\therefore \boxed{T = \mu \alpha J} \Rightarrow \boxed{\alpha = \frac{T}{\mu J}}$$

Complete solution:

$$[\sigma] = \begin{bmatrix} 0 & 0 & -\frac{T x_2}{J} \\ 0 & 0 & \frac{T x_1}{J} \\ -\frac{T x_2}{J} & \frac{T x_1}{J} & 0 \end{bmatrix}$$

$$[\epsilon] = \begin{bmatrix} 0 & 0 & -\frac{T x_2}{2\mu J} \\ 0 & 0 & \frac{T x_1}{2\mu J} \\ \frac{-T x_2}{2\mu J} & \frac{T x_1}{2\mu J} & 0 \end{bmatrix}$$

$$\{u\} = \begin{Bmatrix} -\frac{T}{\mu J} x_2 x_3 \\ \frac{T}{\mu J} x_1 x_3 \\ 0 \end{Bmatrix}$$

Observations:

1. For a circular section  $J = \frac{\pi}{2} a^4$

2. Deformed shape is a cylinder,

$$\epsilon_{kk} = 0 \Rightarrow \text{volume preserving deformation}$$

3. Since we applied St. Venant, our solution is good only for long cylinders ( $L \gg D$ )