# ASEN 3128 - Assignment 1

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Group 14 - Station 7b February 12, 2018 University of Colorado - Boulder Linearized Models

$$\int \hat{p} \approx \frac{Q}{I_{x}} \left( \Delta f_{z} + \Delta f_{y} - \Delta f_{z} - \Delta f_{z} \right) \qquad R = \frac{d}{f_{z}}$$

$$\Delta \hat{q} \approx \frac{Q}{I_{x}} \left( \Delta f_{z} + \Delta f_{y} - \Delta f_{z} - \Delta f_{z} \right)$$

$$\Delta \hat{r} \approx \frac{h}{I_{z}} \left( \Delta f_{z} + \Delta f_{y} - \Delta f_{z} - \Delta f_{z} \right)$$

$$\Delta \dot{w}^{\epsilon} = -g\Delta \Phi$$

$$\Delta \dot{w}^{\epsilon} \approx g\Delta \Phi$$

$$\Delta \dot{w}^{\epsilon} \approx \frac{1}{m} \left( -\Delta f_{1} - \Delta f_{2} - \Delta f_{3} - \Delta f_{4} \right)$$

10 ≈ Ap 00 ≈ Aq 14 ≈ Ar

## Problem 2 - 3

The following plots indicate where the linear and nonlinear models deviate from each other when the quad copter strays from the nominal trim state.

# Part a) - $5^{\circ}$ Bank Deviation

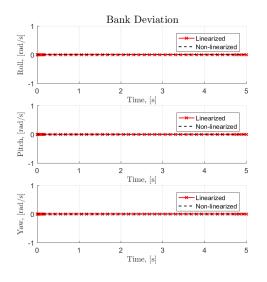


Figure 1: Body coordinate angular velocity as a function of time.

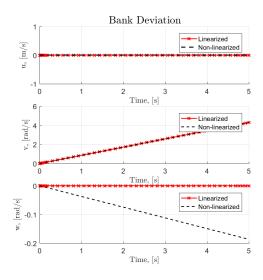


Figure 2: Body coordinate velocity as a function of time.

#### Part b) - 5° Elevation Deviation

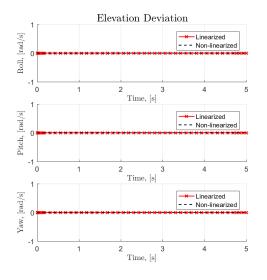


Figure 3: Body coordinate angular velocity as a function of time.

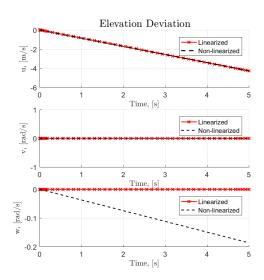


Figure 4: Body coordinate velocity as a function of time.

# Part c) - 5° Azimuth Deviation

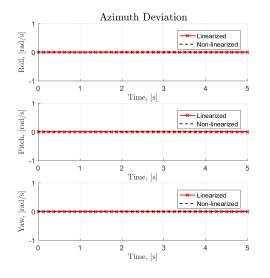


Figure 5: Body coordinate angular velocity as a function of time.

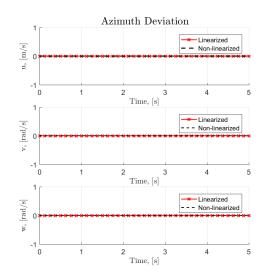


Figure 6: Body coordinate velocity as a function of time.

## Part d) - 0.1 rad/s Roll Deviation

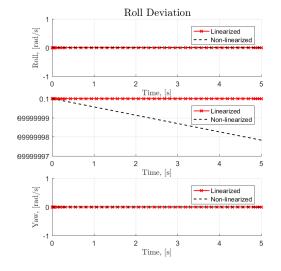


Figure 7: Body coordinate angular velocity as a function of time.

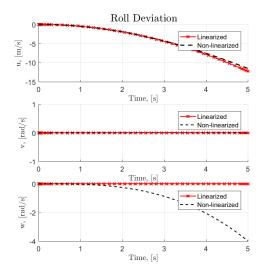


Figure 8: Body coordinate velocity as a function of time.

## Part e) - 0.1 rad/s Pitch Deviation

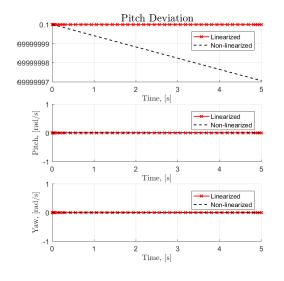


Figure 9: Body coordinate angular velocity as a function of time.

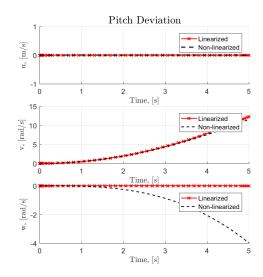


Figure 10: Body coordinate velocity as a function of time.

#### Part f) - 0.1 rad/s Yaw Deviation

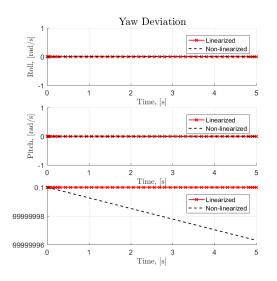


Figure 11: Body coordinate angular velocity as a function of time.

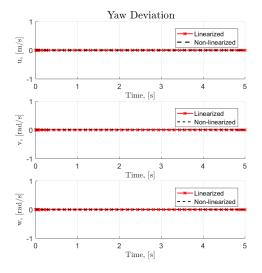


Figure 12: Body coordinate velocity as a function of time.

## Problem 4

This next problem introduces control moments for the quad copter based on angular rates, roll, pitch, and yaw. The gains for these are as follows.

- 1.  $K_p = 0.003 [N \cdot /(rad/s)]$
- 2.  $K_q = 0.003 [N \cdot / (rad/s)]$
- 3.  $K_r = 0.0012 [N \cdot /(rad/s)]$

These gains were then implemented as follows:

1. 
$$L_c = -k_p \cdot p$$

$$2. M_c = -k_q \cdot q$$

3. 
$$N_c = -k_r \cdot r$$

This was tested with the **non-linear** model by implementing deviations in roll, pitch, and yaw rate. The results of this are shown below.

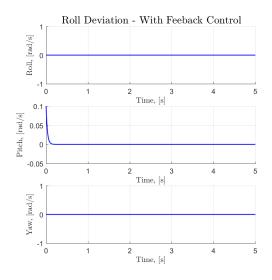


Figure 13: Body coordinate angular velocity as a function of time.

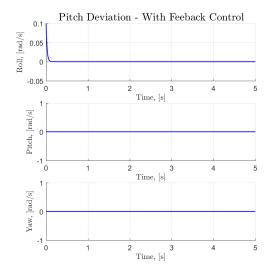


Figure 15: Body coordinate angular velocity as a function of time.

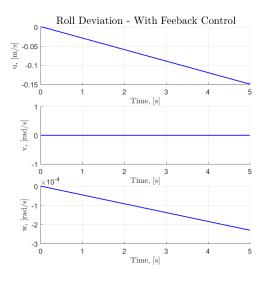


Figure 14: Body coordinate velocity as a function of time.

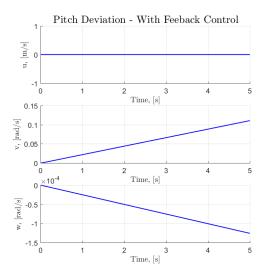
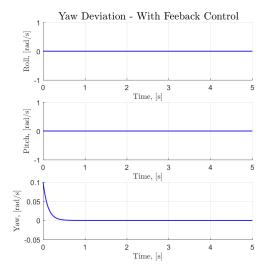


Figure 16: Body coordinate velocity as a function of time.



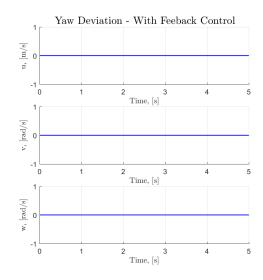
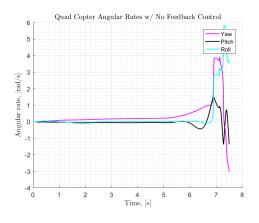


Figure 17: Body coordinate angular velocity as a function of time.

Figure 18: Body coordinate velocity as a function of time.

#### Problem 5

This problem looked into the difference between zero control and derivative control for the physical quad copter. The difference between the two in terms of state variables roll, pitch, and yaw can be seen in the following figures. From a more qualitative point of view, it was seen that the scenario with no control tumbled to the ground almost immediately. Conversely, the scenario with derivative feedback control drifted like a lovely little leaf for some time before entering a tumble and crashing.



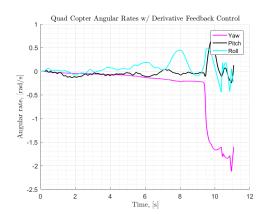


Figure 19: Body coordinate angular velocity as a function of time.

Figure 20: Body coordinate angular velocity as a function of time.

Note here that control was removed approximately 5 seconds in to the experiment for both scenarios, and while the case with no feedback control tumbled almost immediately, the case with derivative feedback control is able to maintain some semblance of hover for approximately 3-4 seconds after moving to derivative control.

#### MATLAB Code

```
% quadCopterSim_Ass3 simulates the dynamics of a small quad copter using
3 % numeical integration of Euler's Moment Equations
5 % Created: 1/30/18 - Connor Ott
6 % Last Modified: 1/30/18 - Connor Ott
8
9
   clc; clear; close all;
10 set (0, 'defaulttextinterpreter', 'latex');
11
12 % Hover Trim
13 ti = 0;
14 tf = 5; \% s
   analyticalTrim = 0 * ones(1, 4);
   initConds = zeros(1, 12);
   initConds(12) = -1;
17
18
   options = odeset('Events', @termEvents, 'RelTol', 1e-8);
19
   [t, F] = ode45(@(t, F)quadCopterODE_lin(t, F, analyticalTrim), ...
20
21
                                                 [ti, tf], initConds, options);
22
23 figure ('visible', 'off')
   hold on; grid on; axis equal;
24
   plot3(F(:, 10), F(:, 11), F(:, 12), 'ro')
   set(gca, 'zdir', 'reverse')
   zlabel('Down Position, [m]')
   xlabel ('East Position, [m]')
   ylabel ('North Position, [m]')
30 title ('Steady Hover Trim - Linearized')
   set (gca, 'ticklabelinterpreter', 'latex', ...
            'fontsize', 12);
33 view (-59, 17)
34
35 % Part 2
   % a) − f) Deviations in different parameters and comparision between linear
37 % and nonlinear models.
38 ti = 0:
39 tf = 5; \% s
40 \quad linTrim = 0 * ones(1, 4);
   nLTrim = ones(1, 4)*0.068*9.81 / 4;
41
42
43
44 \quad \text{condMat} = \text{zeros}(6, 12);
45 condMat(:, 12) = -4; % initial height
46 \operatorname{condMat}(1, 7) = \operatorname{deg2rad}(5); \% [rad]
   condMat(2, 8) = deg2rad(5); \% [rad]
   condMat(3, 9) = deg2rad(5); \% [rad]
   condMat(4, 4) = 0.1; \% [rad/s]
   condMat(5, 5) = 0.1; \% [rad/s]
   condMat(6, 6) = 0.1; \% [rad/s]
52
   titleCell = { 'Bank Deviation', 'Elevation Deviation', ...
```

```
'Azimuth Deviation', 'Pitch Deviation', ...
54
                   'Roll Deviation', 'Yaw Deviation'};
56
    options = odeset('Events', @termEvents, 'RelTol', 1e-8);
57
58
    [r, \tilde{}] = size(condMat);
    sSize = get(0, 'screensize');
59
60
    for i = 1:r
61
62
         tspan = [0, 5]; %s
63
         initConds = condMat(i, :);
64
65
         [t_lin, F_lin] = ode45(@(t, F)quadCopterODE_lin(t, F, linTrim), ...
66
                                       tspan, initConds);
         [t_nL, F_nL] = ode45(@(t, F)quadCopterODE(t, F, nLTrim), ...
67
68
                                       tspan, initConds);
69
70
        % pqr Plots
         figure ('pos', [sSize(3)*0.25, sSize(4)*0.20, ...
71
72
                         sSize(3)*0.40, sSize(4)*0.70);
         subplot (3, 1, 1)
73
74
         hold on; grid on;
         plot(t_lin, F_lin(:, 4), 'rx-', 'linewidth', 1.2)
         plot\left(t\_nL\,,\ F\_nL\left(:\,,\ 4\right),\ 'k--'\,,\ 'linewidth'\,,\ 1.2\right)
76
         xlabel('Time, [s]')
77
         ylabel('Roll, [rad/s]')
78
         legend('Linearized', 'Non-linearized')
79
80
81
         subplot(3, 1, 2)
         hold on; grid on;
82
         plot(t_lin, F_lin(:, 5), 'rx-', 'linewidth', 1.2)
83
         plot(t_nL, F_nL(:, 5), 'k—', 'linewidth', 1.2)
84
         xlabel('Time, [s]')
85
         ylabel('Pitch, [rad/s]')
86
         legend ('Linearized', 'Non-linearized')
87
88
         subplot (3, 1, 3)
89
         hold on; grid on;
90
         plot(t_lin, F_lin(:, 6), 'rx-', 'linewidth', 1.2)
91
92
         plot(t_nL, F_nL(:, 6), 'k-', 'linewidth', 1.2)
         xlabel('Time, [s]')
93
         ylabel('Yaw, [rad/s]')
94
         legend('Linearized', 'Non-linearized')
95
96
         [", t] = \text{suplabel}(\text{titleCell}\{i\}, 't', [.1 .1 .84 .84]);
97
         set(t, 'fontsize', 15)
98
         set(gcf,'Visible','off')
99
           if exist(['./Ass3figs/',titleCell{i}, '_pqr.png'], 'file') ~=2
100
    %
             saveas(gcf, ['./Ass3figs/',titleCell{i}, '_pqr.png']);
    %
           end
102
104
        % uvw Plots
106
         figure ('pos', [sSize(3)*0.25, sSize(4)*0.20, ...
                         sSize(3)*0.40, sSize(4)*0.70);
         suplabel(titleCell{i}, 't');
108
```

```
109
         subplot (3, 1, 1)
110
         hold on; grid on;
         plot(t_lin, F_lin(:, 1), 'rx-', 'linewidth', 1.2)
111
         plot(t_nL, F_nL(:, 1), 'k-', 'linewidth', 1.5)
112
113
         xlabel('Time, [s]')
114
         ylabel('u, [m/s]')
         legend ('Linearized', 'Non-linearized')
115
116
117
         subplot (3, 1, 2)
118
         hold on; grid on;
119
         plot(t_lin, F_lin(:, 2), 'rx-', 'linewidth', 1.2)
         plot\left(t\_nL\,,\ F\_nL\left(:\,,\ 2\right),\ ^{\prime}k\_{}^{\prime}\,,\ ^{\prime}linewidth\,^{\prime}\,,\ 1.2\right)
         xlabel('Time, [s]')
121
         vlabel('v, [rad/s]')
122
         legend('Linearized', 'Non-linearized')
123
124
125
         subplot (3, 1, 3)
126
         hold on; grid on;
         plot(t_lin, F_lin(:, 3), 'rx-', 'linewidth', 1.2)
127
128
         plot(t_nL, F_nL(:, 3), 'k—', 'linewidth', 1.2)
129
         xlabel('Time, [s]')
         ylabel('w, [rad/s]')
         legend('Linearized', 'Non-linearized')
131
132
         [~, t] = suplabel(titleCell{i}, 't', [.1 .1 .84 .84]);
133
         set(t, 'fontsize', 15)
134
         set(gcf,'Visible','off')
           if exist (['./Ass3figs/', titleCell{i}, '_uvw.png'], 'file') ~=2
136 %
             saveas(gcf, ['./Ass3figs/',titleCell{i}, '_uvw.png']);
138
    %
           end
139
    end
141 % Plotting experimental quad copter data
    load('RSdata_Drone01_1330.mat');
    times = rt_estim.time(:);
144
    pdata = rt_estim.signals.values(:, 4);
    qdata = rt_estim.signals.values(:, 5);
146
    rdata = rt_estim.signals.values(:, 6);
147
    load ('RSdata_Wed_1315.mat')
148
149
    time_d = rt_estim.time(:);
    pdata_d = rt_estim.signals.values(:, 4);
150
151
    qdata_d = rt_estim.signals.values(:, 5);
152
    rdata_d = rt_estim.signals.values(:, 6);
154
    figure
    hold on; grid on; grid minor;
156
    plot(times, pdata, 'm-', 'linewidth', 1.3)
157
    plot (times, qdata, 'k-', 'linewidth', 1.3)
    plot(times, rdata, 'c-', 'linewidth', 1.3)
title('Quad Copter Angular Rates w/ No Feedback Control')
159
160
    xlabel('Time, [s]')
    ylabel ('Angular rate, [rad/s]')
    legend ('Yaw', 'Pitch', 'Roll')
```

```
164
165 figure
    hold on; grid on; grid minor;
166
    plot(time_d, pdata_d, 'm-', 'linewidth', 1.3) plot(time_d, qdata_d, 'k-', 'linewidth', 1.3) plot(time_d, rdata_d, 'c-', 'linewidth', 1.3)
169
    title ('Quad Copter Angular Rates w/ Derivative Feedback Control')
170
    xlabel('Time, [s]')
    ylabel('Angular rate, [rad/s]')
172
    legend ('Yaw', 'Pitch', 'Roll')
173
    function dfdt = quadCopterODE(t, F, trim)
    % Defines dynamics of quad copter
 3
 4
 5 % Physical properties and constants
 6 \text{ alpha} = 2e - 6;
                       \% [N/(m/s)^2]
 7 beta = 1e-6;
                       \% [N/(m/s)^2]
                       \% [N/(rad/s)^2]
 8 \text{ heta} = 1e-3;
                       \% [N/(rad/s)^2]
 9 \text{ xsi} = 3e-3;
 10
11 I_x = 6.8e - 5;
                       % [kg m<sup>2</sup>]
 12 I_{-y} = 9.2e - 5;
                       % ['']
13 I_z = 1.35e - 4; \% ['']
14
 15 \text{ m} = 0.068;
                       % [kg]
 16 	 d = 0.06:
                       % [m]
                       % [~]
17 \quad k = 0.0024;
18 rad = d/sqrt(2); % [m]
                       \% [m/s^2]
 19
    g = 9.81;
20
21 % Pulling from input, F and trim
22 % Inertial velocity in body coords
23 u = F(1);
24 	 v = F(2);
25 \text{ w} = F(3);
26
 27 % Inertial angular velocity in body coords
28 p = F(4);
29 q = F(5);
30 r = F(6);
31
32 % Euler angles
33 phi = F(7);
34 \text{ theta} = F(8);
35 psi = F(9);
36
37 % Position vector from origin to COM in inertial coords
38 x_E = F(10);
39 y_E = F(11);
40 	 z_e = F(12);
41
42 	ext{ f1} = trim(1); \% motor forces
43 f2 = trim(2);
44 f3 = trim(3);
45 	ext{ f4} = trim(4);
```

```
46
47
   % Aerodynamic and Control Moments and Forces
48
49 % Moments
50 L_a = - alpha^2 * p^2 * sign(p);
   M_{-}a = - \operatorname{alpha}^2 * \operatorname{q}^2 * \operatorname{sign}(q);
52 N_a = - beta^2 * r^2 * sign(r);
L_c = ((f2 + f3) - (f1 + f4)) * rad;
   M_c = ((f3 + f4) - (f1 + f2)) * rad;
56 \text{ N}_{-c} = (f2 + f4 - (f1 + f2)) * k;
58 L = L_a + L_c;
59 \text{ M} = \text{M}_{-a} + \text{M}_{-c};
60 \text{ N} = \text{N}_{-}\text{a} + \text{N}_{-}\text{c};
61
62 % Forces
63 X_a = - heta^2 * u^2 * sign(u);
64 	ext{ } Y_a = - 	ext{ heta } ^2 	ext{ } v^2 	ext{ } sign(v);
65 \quad Z_a = -x \sin^2 * w^2 * sign(w);
66
67 \quad X_c = 0;
68 Y_c = 0;
69 Z_c = -sum(trim);
70
71 X = X_a + X_c;
72 	ext{ } 	ext{Y} = 	ext{Y}_a + 	ext{Y}_c;
73 	ext{ } Z = Z_a + Z_c;
74
75 % Determining Roll, Pitch, and Yaw rates of change
76 p_{dot} = (I_{y} - I_{z})/I_{x} * q * r + 1/I_{x} * L;
   q_{-}dot = (I_{-}z - I_{-}x)/I_{-}y * p * r + 1/I_{-}y * M;
   r_{-}dot = (I_{-}x - I_{-}y)/I_{-}z * p * q + 1/I_{-}z * N;
   dOmega\_bdt = [p\_dot, q\_dot, r\_dot]';
79
80
81
   % Determining translation rates
    u_{-}dot = r*v - q*w - g*sin(theta) + 1/m * X;
   v_{dot} = p*w - r*u + g*sin(phi)*cos(theta) + 1/m * Y;
   w_{-}dot = q*u - p*v + g*cos(phi)*cos(theta) + 1/m * Z;
85
    dV_{-}bdt = [u_{-}dot, v_{-}dot, w_{-}dot]';
86
   % Tranlating body to inertial coordinates
   x_{-}dot = u * cos(theta)*cos(psi) + ...
              v * (\sin(phi)*\sin(theta)*\cos(psi) - \cos(phi)*\sin(psi)) + ...
89
90
              w * (\cos(phi)*\sin(theta)*\cos(psi) + \sin(phi)*\sin(psi));
    y_{-}dot = u * cos(theta)*sin(psi) + ...
91
              v * (\sin(phi)*\sin(theta)*\sin(psi) + \cos(phi)*\cos(psi)) + ...
92
              w * (\cos(phi)*\sin(theta)*\sin(psi) - \sin(phi)*\cos(psi));
94
    z_{-}dot = -u * sin(theta) + ...
              v * \sin(phi)*\cos(theta) + ...
96
              w * cos(phi)*cos(theta);
97
    dV_Edt = [x_dot, y_dot, z_dot]';
   % Translating Angular Momentum to Euler angles
    phi_dot = p + (q*sin(phi) + r*cos(phi))*tan(theta);
```

```
theta_dot = q*cos(phi) - r*sin(phi);
    psi_dot = q*sin(phi)*sec(theta) + r*cos(phi)*sec(theta);
    dEuldt = [phi_dot, theta_dot, psi_dot]';
104
105 % Concatenating for output
    dfdt = [dV_bdt; dOmega_bdt; dEuldt; dV_Edt];
106
107
108
109
    end
    function dfdt = quadCopterODE_lin(t, F, trim)
    % Defines dynamics of quad copter
 3
 4
 5 % Physical properties and constants
 6 \text{ alpha} = 2e - 6;
                     \% [N/(m/s)^2]
 7 beta = 1e-6;
                     \% [N/(m/s)^2]
                     \% [N/(rad/s)^2]
 8 \text{ heta} = 1e-3;
                     \% [N/(rad/s)^2]
 9 \text{ xsi} = 3e-3;
10
11 I_x = 6.8e - 5;
                     % [kg m<sup>2</sup>]
12 I_{-y} = 9.2e - 5;
                     % ['']
13 I_z = 1.35e - 4; \% ['']
14
                     % [kg]
15 \text{ m} = 0.068;
16 d = 0.06:
                      % [m]
                     % [~]
17 \quad k = 0.0024;
18 rad = d/sqrt(2); % [m]
                      \% [m/s^2]
19
    g = 9.81;
20
21 %% Pulling from input, F and trim
22 % Inertial velocity in body coords
23 delta_u = F(1);
24 \text{ delta-v} = F(2);
25 delta_w = F(3);
26
27 % Inertial angular velocity in body coords
28 delta_p = F(4);
29 delta_q = F(5);
30 delta_r = F(6);
31
32 % Euler angles
33 delta_phi = F(7);
    delta\_theta = F(8);
34
    delta_psi = F(9);
36
37
    % Position vector from origin to COM in inertial coords
38 x_E = F(10);
39 y_E = F(11);
40 	 z_e = F(12);
41
42
    delta_f1 = trim(1); \% motor forces
43 \quad delta_f2 = trim(2);
44 \quad delta_f3 = trim(3);
45 \quad delta_f 4 = trim(4);
```

```
46
   % Aerodynamic and Control Moments and Forces
47
48
49 % Moments
50 L_a = 0; %— alpha^2 * p^2 * sign(p);
   M_a = 0; %— alpha^2 * q^2 * sign(q);
   N_a = 0; \% - beta^2 * r^2 * sign(r);
52
L_c = ((delta_f2 + delta_f3) - (delta_f1 + delta_f4)) * rad;
   M_c = ((delta_f3 + delta_f4) - (delta_f1 + delta_f2)) * rad;
   N_c = (delta_f2 + delta_f4 - (delta_f1 + delta_f2)) * k;
58 L = L_a + L_c;
   M = M_a + M_c;
60 \text{ N} = \text{N}_{-}\text{a} + \text{N}_{-}\text{c};
61
62\% if t>1 && t<1.5\% Throw a moment perturbation in for 0.2 seconds
         L = L + momPert(1);
63
64 %
         M = M + momPert(2);
65 %
         N = N + momPert(3);
66 % end
67
68 % Forces
69 X_a = 0; %— heta^2 * delta_u^2 * sign(delta_u);
70 Y_a = 0; %— heta^2 * delta_v^2 * sign(delta_v);
   Z_a = 0; % xsi^2 * delta_w^2 * sign(delta_w);
72
73 X_c = 0;
74
   Y_c = 0;
75
   Z_c = -sum(trim);
76
   X = X_a + X_c;
78
   Y = Y_a + Y_c;
   Z = Z_a + Z_c;
79
80
   % Determining Roll, Pitch, and Yaw rates of change
81
   deltap_dot = rad/I_x * (delta_f2 + delta_f3 - delta_f1 - delta_f4);
82
   deltaq_dot = rad/I_y * (delta_f3 + delta_f4 - delta_f1 - delta_f2);
   delta_dot = k/I_z * (delta_f2 + delta_f4 - delta_f4 - delta_f3);
   dOmega_bdt = [deltap_dot, deltaq_dot, deltar_dot]';
85
86
   % Determining translation rates
   deltau_dot = -g * delta_theta;
   deltav_dot = g * delta_phi;
90
   deltaw_dot = 1/m * Z;
91
   dV_bdt = [deltau_dot, deltav_dot, deltaw_dot]';
92
   % Tranlating body to inertial coordinates
   x_{dot} = delta_{u} * cos(delta_{theta})*cos(delta_{psi}) + ...
94
             delta_v * (sin(delta_phi)*sin(delta_theta)*cos(delta_psi) - cos(
                delta_phi)*sin(delta_psi)) + ...
96
             delta_w * (cos(delta_phi)*sin(delta_theta)*cos(delta_psi) + sin(
                delta_phi)*sin(delta_psi));
             delta_u * cos(delta_theta)*sin(delta_psi) + ...
             delta_v * (sin(delta_phi)*sin(delta_theta)*sin(delta_psi) + cos(
98
```

```
delta_phi)*cos(delta_psi)) + ...
99
              delta_w * (cos(delta_phi)*sin(delta_theta)*sin(delta_psi) - sin(
                 delta_phi)*cos(delta_psi));
100
    z_{dot} = -delta_{u} * sin(delta_{theta}) + ...
101
              delta_v * sin(delta_phi)*cos(delta_theta) + ...
              delta_w * cos(delta_phi)*cos(delta_theta);
102
    dV_Edt = [x_dot, y_dot, z_dot]';
104
   % Translating Angular Momentum to Euler angles
    deltaphi_dot
                   = delta_p;
106
    deltatheta_dot = delta_q;
    deltapsi_dot
                   = delta_r;
    dEuldt = [deltaphi_dot, deltatheta_dot, deltapsi_dot]';
109
111
   % Concatenating for output
    dfdt = [dV_bdt; dOmega_bdt; dEuldt; dV_Edt];
113
114
115
116 end
 1
   %
   % quadCopterSim_FBC simulates the dynamics of a quad copter with
 3 % derivative feedback control.
 4 %
 5 % Dependancies:
            quadCopterODE_FBC - ODE function defining dynamics of quad copter.
 6 %
 7 %
 8 % Created: 2/10/18 - Connor Ott
 9 % Last Modified: 2/10/18 - Connor Ott
10 %
11 % Introducing Feedback control
12
13 sSize = get(0, 'screensize');
14 \quad \text{condMat} = \text{zeros}(3, 12);
15 condMat(:, 12) = -4; % initial height
16 condMat(1, 4) = 0.1; \% [rad/s]
    condMat(2, 5) = 0.1; \% [rad/s]
17
    condMat(3, 6) = 0.1; \% [rad/s]
18
19
20 titleCell = {'Pitch Deviation', 'Roll Deviation', 'Yaw Deviation'};
    tspan = [0, 5]; %s
    fbcTrim = ones(1, 4)*0.068*9.81 / 4;
    for i = 1:length(titleCell)
24
        initConds = condMat(i, :);
        [t_FBC, F_FBC] = ode45(@(t, F)quadCopterODE_FBC(t, F, fbcTrim), ...
26
27
                                                           tspan, initConds);
28
29
        % pqr Plots
        figure ('pos', [sSize(3)*0.25, sSize(4)*0.15, ...
30
31
                        sSize(3)*0.40, sSize(4)*0.70);
32
        subplot (3, 1, 1)
33
        hold on; grid on;
34
        plot(t\_FBC, F\_FBC(:, 4), 'b-', 'linewidth', 1.2)
        xlabel('Time, [s]')
```

```
ylabel('Roll, [rad/s]')
36
37
38
        subplot (3, 1, 2)
39
        hold on; grid on;
40
        plot(t\_FBC, F\_FBC(:, 5), 'b-', 'linewidth', 1.2)
        xlabel('Time, [s]')
41
42
        ylabel('Pitch, [rad/s]')
43
44
        subplot (3, 1, 3)
45
        hold on; grid on;
46
        plot(t_FBC, F_FBC(:, 6), 'b-', 'linewidth', 1.2)
        xlabel('Time, [s]')
47
        ylabel('Yaw, [rad/s]')
48
49
50
        [, t] = suplabel([titleCell{i}, '- With Feeback Control'],...
                            't', [.1 .1 .84 .84]);
       set(t, 'fontsize', 15)
set(gcf,'Visible','off')
52
53
        if exist(['./Ass3figs_fbc/',titleCell{i}, '_pqrFBC.png'], 'file') ~=2
54
            saveas(gcf, ['./Ass3figs_fbc/',titleCell{i}, '_pqrFBC.png']);
56
        end
58
       % uvw Plots
59
        figure ('pos', [sSize(3)*0.25, sSize(4)*0.15, ...
60
61
                        sSize(3)*0.40, sSize(4)*0.70);
        suplabel(titleCell{i}, 't');
62
63
        subplot(3, 1, 1)
        hold on; grid on;
64
        plot(t_FBC, F_FBC(:, 1), 'b-', 'linewidth', 1.2)
65
66
        xlabel('Time, [s]')
        ylabel('u, [m/s]')
67
68
69
        subplot (3, 1, 2)
70
        hold on; grid on;
71
        plot(t_FBC, F_FBC(:, 2), 'b-', 'linewidth', 1.2)
72
        xlabel('Time, [s]')
73
        ylabel('v, [rad/s]')
74
75
        subplot (3, 1, 3)
76
        hold on; grid on;
77
        plot(t_FBC, F_FBC(:, 3), 'b-', 'linewidth', 1.2)
78
        xlabel('Time, [s]')
        ylabel('w, [rad/s]')
79
80
        [", t] = suplabel([titleCell{i}, '-With Feeback Control'], ...
81
                                           't', [.1 .1 .84 .84]);
82
        set(t, 'fontsize', 15)
83
        set (gcf, 'Visible', 'off')
84
        if exist(['./Ass3figs_fbc/',titleCell{i}, '_uvwFBC.png'], 'file') ~=2
85
86
            saveas(gcf, ['./Ass3figs_fbc/',titleCell{i}, '_uvwFBC.png']);
87
        end
88
   end
   function dfdt = quadCopterODE_FBC(t, F, trim)
   % Defines dynamics of quad copter
```

```
3
   % Physical properties and constants
4
                      \% [N/(m/s)^2]
5
   alpha = 2e-6;
6 beta = 1e-6;
                      \% [N/(m/s)^2]
7
   heta = 1e-3;
                      \% [N/(rad/s)^2]
   xsi = 3e-3;
                      \% [N/(rad/s)^2]
9
10 I_x = 6.8e - 5;
                      % [kg m<sup>2</sup>]
                      % ['']
11 I_{-y} = 9.2e - 5;
                      % [''']
12
   I_z = 1.35e - 4;
13
                      % [kg]
14 \text{ m} = 0.068;
15 d = 0.06;
                      % [m]
                      %
16 \quad k = 0.0024;
17 rad = d/sqrt(2); % [m]
   g = 9.81;
                      \% [m/s^2]
19
20 % Gains
21 	 k_p = 0.003;
                      \% [Nm/(rad/s)]
k_q = 0.003;
                      \% [Nm/(rad/s)]
k_r = 0.0012;
                      \% [Nm/(rad/s)]
24
25 %% Pulling from input, F and trim
26 % Inertial velocity in body coords
27 u = F(1);
28 v = F(2);
29 w = F(3);
30
31 % Inertial angular velocity in body coords
32 p = F(4);
33 q = F(5);
34 	 r = F(6);
36 % Euler angles
37 phi = F(7);
38
   theta = F(8);
39
   psi = F(9);
40
41 % Position vector from origin to COM in inertial coords
42 \quad x_{-}E = F(10);
43 y_E = F(11);
   z_{-}e = F(12);
44
45
   f1 = trim(1); % motor forces
47
   f2 = trim(2);
48 	ext{ f3} = trim(3);
49
   f4 = trim(4);
50
51 % Aerodynamic and Control Moments and Forces
53 % Moments
L_a = - alpha^2 * p^2 * sign(p);
55 \text{ M}_a = - \text{ alpha}^2 * \text{ q}^2 * \text{ sign}(\text{q});
N_a = - beta^2 * r^2 * sign(r);
```

ASEN 3128 Section 012 17 of 19 Spring 2018

```
58 L_c = -k_p * p;
  M_c = -k_q * q;
  60 \text{ N}_{\text{c}} = -k_{\text{r}} * r;
  61
  62 L = L_a + L_c;
  63 M = M_a + M_c;
  64 \text{ N} = \text{N}_{-}\text{a} + \text{N}_{-}\text{c};
  65
  66 % Forces
              X_a = - heta^2 * u^2 * sign(u);
  68 Y_a = - heta^2 * v^2 * sign(v);
  69 Z_a = -x \sin^2 x \cdot 
   70
   71 X_c = 0;
   72 \quad Y_c = 0;
   73 Z_c = -sum(trim);
   74
   75 X = X_a + X_c;
   76 	ext{ } 	ext{Y} = 	ext{Y}_{-}a + 	ext{Y}_{-}c;
   77 	ext{ Z} = 	ext{Z}_{-a} + 	ext{Z}_{-c};
   78
             % Determining Roll, Pitch, and Yaw rates of change
              p_{-}dot = (I_{-}y - I_{-}z)/I_{-}x * q * r + 1/I_{-}x * L;
              q_{-}dot = (I_{-}z - I_{-}x)/I_{-}y * p * r + 1/I_{-}y * M;
              r_{dot} = (I_{x} - I_{y})/I_{z} * p * q + 1/I_{z} * N;
              dOmega\_bdt = [p\_dot, q\_dot, r\_dot]';
  83
  84
  85 % Determining translation rates
              u_{-}dot = r*v - q*w - g*sin(theta) + 1/m * X;
              v_{dot} = p*w - r*u + g*sin(phi)*cos(theta) + 1/m * Y;
              w_{-}dot = q*u - p*v + g*cos(phi)*cos(theta) + 1/m * Z;
              dV_bdt = [u_dot, v_dot, w_dot]';
  89
  90
             % Tranlating body to inertial coordinates
  91
              x_{-}dot = u * cos(theta)*cos(psi) + ...
                                              v * (\sin(phi)*\sin(theta)*\cos(psi) - \cos(phi)*\sin(psi)) + ...
  94
                                              w * (\cos(phi)*\sin(theta)*\cos(psi) + \sin(phi)*\sin(psi));
              y_{-}dot = u * cos(theta)*sin(psi) + ...
  96
                                              v * (\sin(phi)*\sin(theta)*\sin(psi) + \cos(phi)*\cos(psi)) + \dots
                                              w * (\cos(phi)*\sin(theta)*\sin(psi) - \sin(phi)*\cos(psi));
  97
  98
              z_{-}dot = -u * sin(theta) + ...
  99
                                              v * \sin(phi)*\cos(theta) + ...
                                              w * cos(phi)*cos(theta);
100
              dV_Edt = [x_dot, y_dot, z_dot]';
102
             % Translating Angular Momentum to Euler angles
104
              phi_dot = p + (q*sin(phi) + r*cos(phi))*tan(theta);
               theta_dot = q*cos(phi) - r*sin(phi);
                                            = q*sin(phi)*sec(theta) + r*cos(phi)*sec(theta);
106
              dEuldt = [phi_dot, theta_dot, psi_dot]';
107
108
             % Concatenating for output
              dfdt = [dV_bdt; dOmega_bdt; dEuldt; dV_Edt];
111
112
              end
```

```
 \begin{array}{lll} 1 & function \; [\, value \, , \; isTerm \, , \; direction \, ] \; = \; termEvents(t \, , \; F) \\ 2 & \% & Define \; events \; for \; quad \; copter \; ODE \\ 3 & value \; = \; [F(12) \, , \; F(12) \, + \; 100] \; '; \\ 4 & isTerm \; = \; [1 \, , 1] \; '; \\ 5 & direction \; = \; [] \; ; \\ 6 & end \\ \end{array}
```