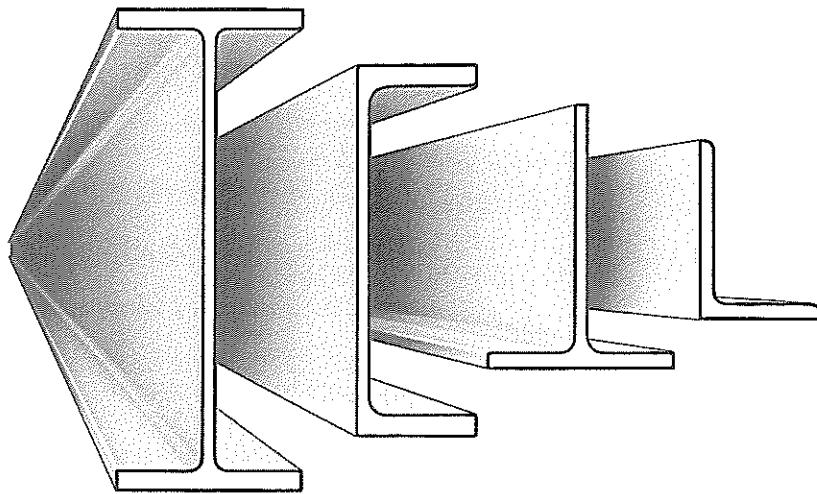


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# design capacity tables for structural steel

- second edition -



## Volume 1: Open Sections

**WB, WC – Grade 300/400**

**UB, UC, BT, CT, PFC – Grade 300**

**TFB, TFC – Grade 250**

**EA<sup>#</sup>, UA<sup>#</sup> – Grade 300/250**

<sup>#</sup> Grade for angles is dependent on section

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LIMIT STATES  
EDITION STATES  
AS 4100-1990  
S<sup>✓</sup> RRU

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# DESIGN CAPACITY TABLES FOR STRUCTURAL STEEL

second edition

## Volume 1: Open Sections

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## Foreword

The Australian Institute of Steel Construction (AISC) was formed in 1962 to serve the interests of all concerned in the design, specification, fabrication, and erection of steel structures.

Today, the AISC is a national body whose purpose is to promote and optimise the use of fabricated structural steel through engineering, research, and the dissemination of knowledge to specifiers, fabricators, suppliers, and students.

Its activities are directed towards fostering the economic and efficient use of steel in buildings, bridges, civil engineering projects, pressure vessels, pipelines, marine and offshore structures, and other fabricated forms.

The Institute is a non-profit organisation which is primarily financed by membership dues.

Engineers, architects and others interested in steel construction are invited to make use of the Institute's services.

## Acknowledgments

In the compilation of the *Design Capacity Tables for Structural Steel* - Second Edition, Volume 1, AISC acknowledges with grateful thanks the contribution and assistance of the following organisations and individuals:

- Mr Tim Wilkinson for the preparation of the majority of the tables and text;
- AISC - Technical Services, in particular Mr Arun Syam and Mr Bruce Chapman;
- Palmer Tube Mills (Aust) Pty Ltd, in particular Mr Russell Watkins for the production of the design curves;
- Staff from BHP Research, Melbourne Laboratories, who prepared much of the text and tables in the first edition of this publication, for their advice on this edition;
- Mr Tony Edwards (Redmark Pty Ltd) for the production and artwork in this publication;
- and all those who gave constructive comment and advice on the technical and editorial content of the document.

## Preface

The second edition of the *Design Capacity Tables for Structural Steel* (DCT) is a design aid to the limit states Standard AS 4100-1990: *Steel Structures*, published by Standards Australia.

The first edition of the DCT considered standard hot-rolled sections (Grades 250 and 350), welded sections (Grades 300 and 400) and structural steel hollow sections. Due to this large and varying range of sections it was decided to split the future editions of the DCT into volumes. This permits information specific to hot-rolled and welded sections, and hollow sections to be considered separately, without producing a large single publication. In fact, prior to the publication of the second edition of the DCT, the *Design Capacity Tables for Structural Steel Hollow Sections* (DCTHS) was published by AISC. The DCTHS contains information specific to hollow sections in a format similar to the DCT.

The second edition of the DCT is an update of the first edition. At the time of publication, the second edition incorporates the current range of standard hot-rolled and welded structural steel sections. The first volume of the second edition is subtitled *Volume 1: Open Sections* to reflect the section types considered. (The second edition of the DCTHS will be published as *Volume 2: Hollow Sections*).

This volume provides information in a similar format to that contained in the first edition of the DCT with revisions which consider the:

- change of the base steel grade from Grade 250 to Grade 300 for most hot-rolled sections
- introduction of new Universal Beam sections ("Lean Beams")
- deletion of Universal Bearing Piles and the larger Universal Beam and Universal Column sections
- minor dimensional changes to some Universal Beam, Universal Column and Angle sections
- transfer of structural steel hollow sections into a separate volume
- incorporation of Amendments 1 and 2 to AS 4100.

Additionally, comments received from industry have suggested improved methods of listing the information contained in the first edition of the DCT. The suggestions adopted in this edition include:

- renumbering of parts to match, as far as possible, the sections of AS 4100
- restructuring of specific tables (e.g. surface areas, bending) to provide a concise set of information in one table
- section capacities included in member capacity tables
- graphs of members in bending and compression presented in an easier to read format
- a set of tables including all section capacities and capacity information for combined actions.

For information on structural steel hollow sections, and Grade 350 or Grade 250 hot-rolled sections not included in this publication, reference should be made to the DCTHS and the first edition of the DCT respectively.

Arun Syam / Tim Wilkinson  
Editors  
1994

## NOTATION

$A_e$	effective area of a cross-section
$A_c$	minor diameter area of a bolt
$A_g$	gross area of a cross-section
$A_n$	net area of a cross-section
$A_o$	plain shank area of a bolt
$A_s$	tensile stress area of a bolt
$b_b, b_{bf}$	bearing widths
$b_f$	width of a flange
$b_s$	stiff bearing length
$b_1, b_2$	greater and lesser leg lengths of an angle section
$c_m$	factor for unequal moments
$d$	depth of a section
$d_w$	depth of web
$d_1$	clear depth between flanges ignoring fillets or welds
$E$	Young's modulus of elasticity
$e$	eccentricity
$f_u$	tensile strength used in design
$f_{uf}$	minimum tensile strength of a bolt
$f_{up}$	tensile strength of a ply
$f_y$	yield stress used in design
$f_{va}^*$	average design shear stress in a web
$f_{vm}^*$	maximum design shear stress in a web
$G$	shear modulus of elasticity; or nominal dead load
$h_s$	storey height
$I$	second moment of area of a cross-section
$I_n$	$I$ about the (non-principal rectangular) $n$ -axis (for angles)
$I_p$	$I$ about the (non-principal rectangular) $p$ -axis (for angles)
$I_w$	warping constant for a cross-section
$I_x$	$I$ about the cross-sectional major principal $x$ -axis
$I_y$	$I$ about the cross-sectional minor principal $y$ -axis
$J$	torsion constant for a cross-section
$k_e$	member effective length factor
$k_f$	form factor for members subject to axial compression
$k_l$	load height effective length factor
$k_r$	effective length factor for restraint against lateral rotation
$k_{sm}$	exposed surface area to mass ratio
$k_t$	correction factor for distribution of forces in a tension member; or twist restraint effective length factor
$L$	span or member length; or segment or sub-segment length
$L_e$	effective length of a compression member or laterally unrestrained member
$M_b$	nominal member moment capacity
$M_{bx}$	$M_b$ about major principal $x$ -axis
$M_{cx}$	lesser of $M_{ix}$ and $M_{ox}$
$M_i$	nominal in-plane member moment capacity
$M_{ix}$	$M_i$ about major principal $x$ -axis
$M_{iy}$	$M_i$ about minor principal $y$ -axis

$M_o$	reference elastic buckling moment for a member subject to bending: or nominal out-of-plane member moment capacity
$M_{oa}$	amended elastic buckling moment for a member subject to bending
$M_{ox}$	$M_o$ about major principal x-axis
$M_{rx}$	$M_s$ about major principal x-axis reduced by axial force
$M_{ry}$	$M_s$ about minor principal y-axis reduced by axial force
$M_s$	nominal section moment capacity
$M_{sx}$	$M_s$ about major principal x-axis
$M'_{sx}$	$M_s$ about major principal x-axis with two holes in tension flange
$M''_{sx}$	$M_s$ about major principal x-axis with four holes in tension flange
$M_{sy}$	$M_s$ about minor principal y-axis
$M^*$	design bending moment
$M_m^*$	maximum calculated design bending moment along the length of a member or segment
$M_x^*$	design bending moment about major principal x-axis
$M_y^*$	design bending moment about minor principal y-axis
$N_c$	nominal member capacity in compression
$N_{cx}$	$N_c$ for member buckling about major principal x-axis
$N_{cy}$	$N_c$ for member buckling about minor principal y-axis
$N_{om}$	elastic flexural buckling load of a member
$N_{omb}$	$N_{om}$ for a braced member
$N_s$	nominal section capacity of a concentrically loaded compression member
$N_t$	nominal section capacity in tension
$N_{tf}$	nominal tension capacity of a bolt
$N_{ti}$	minimum bolt tension at installation
$N^*$	design axial force, tensile or compressive
$N_{if}^*$	design tensile force on a bolt
$n_{ei}$	number of effective interfaces
$P$	applied concentrated load
$Q$	nominal live load
$R_b$	nominal bearing capacity of a web
$R_{bb}$	nominal bearing buckling capacity
$R_{by}$	nominal bearing yield capacity
$R_u$	nominal capacity
$r$	radius of gyration
$r_x$	radius of gyration about major principal x-axis
$r_y$	radius of gyration about minor principal y-axis
$r_1$	root radius
$r_2$	toe radius
$R^*$	design bearing force
$S$	plastic section modulus
$S_x$	$S$ about major principal x-axis
$S_y$	$S$ about minor principal y-axis
$S^*$	design action effect
$s_p$	staggered pitch of bolts
$t$	thickness of a section
$t_f$	thickness of a flange
$t_p$	thickness of a ply
$t_i$	design throat thickness of a weld

$t_w$	thickness of a web; or size of a fillet weld
$V_b$	nominal bearing capacity of a ply
$V_{fn}$	nominal shear capacity of a bolt - strength limit state - shear on threaded area
$V_{fx}$	nominal shear capacity of a bolt - strength limit state - shear on unthreaded area
$V_{sf}$	nominal shear capacity of a bolt - serviceability limit state
$V_u$	nominal shear capacity of a web with a uniform shear stress distribution
$V_v$	nominal shear capacity of a web
$V_{vm}$	nominal shear capacity of a web in the presence of bending moment
$V^*$	design shear force
$V_f^*$	design shear force on a bolt - strength limit state
$V_{sf}^*$	design shear force on a bolt - serviceability limit state
$V_w$	nominal capacity of a fillet weld per unit length
$V_w^*$	design force per unit length on a fillet weld
$V_{wj}$	nominal capacity of a welded joint
$W$	total uniformly distributed applied load
$W^*$	design action
$W_L^*$	strength limit state maximum design load
$W_s^*$	serviceability limit state maximum design load
$Z$	elastic section modulus
$Z_e$	effective section modulus
$Z_{ex}$	$Z_e$ for bending about major principal $x$ -axis
$Z_{ey}$	$Z_e$ for bending about minor principal $y$ -axis
$Z_x$	$Z$ for bending about major principal $x$ -axis
$Z_y$	$Z$ for bending about minor principal $y$ -axis
$\alpha_a$	compression member factor
$\alpha_b$	compression member section constant
$\alpha_c$	compression member slenderness reduction factor
$\alpha_m$	moment modification factor for bending
$\alpha_s$	slenderness reduction factor
$\beta_m$	ratio of smaller to larger bending moments at the ends of a member
$\Delta_s$	deflection
$\Delta_b$	translational displacement of the top relative to the bottom for a storey height
$\delta_b$	moment amplification factor for a braced member
$\delta_m$	moment amplification factor, taken as the greater of $\delta_b$ and $\delta_s$
$\delta_s$	moment amplification factor for a sway member
$\xi$	compression member factor
$\eta$	compression member imperfection factor
$\pi$	pi ( $\approx 3.14159$ )
$\lambda$	slenderness ratio
$\lambda_c$	elastic buckling load factor
$\lambda_e$	plate element slenderness
$\lambda_{ep}$	plate element plasticity slenderness limit
$\lambda_{ey}$	plate element yield slenderness limit
$\lambda_n$	modified compression member slenderness
$\nu$	Poisson's ratio
$\rho$	density of a material
$\phi$	capacity factor

Note: Additional notation for floor plates is defined in Section 11.8.

## PART 1 INTRODUCTION

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### NOTE

*The maximum design loads and design capacities listed in this publication are based on the limit states design method of AS 4100 and the factored limit states design loads and combinations considered within AS 1170. Hence, much of the information contained herein will only be of use to persons familiar with the limit states design method and the use of:*

**AS 4100: Steel Structures**

**AS 1170: SAA Loading Code**

**PART 1 INTRODUCTION****1.1 Steel Structures Standard**

The tables in this publication have been calculated in accordance with the Australian Standard AS 4100-1990: *Steel Structures*. As far as possible, the notation and terminology used are the same as those adopted in that Standard. Within this publication:

- "AS 4100" refers to AS 4100-1990: Steel Structures incorporating Amendments 1 and 2;
- "the Tables", "Table" or "Tables" refer to this edition and volume of the *Design Capacity Tables for Structural Steel*.

**1.2 Range of Structural Steel Grades and Sections**

The Tables contain information on the currently available (at the time of publication) standard open<sup>#</sup> sections that are within the scope of AS 4100. This includes hot-rolled and welded sections commonly specified in structural engineering. Reference should be made to Section 2 for further details on the structural steel sections considered in the Tables.

Consultation should be made with AISC for current information on structural steel grades and sections that are not contained within this publication.

*# Note: Sections other than hollow sections are regarded as 'open' sections in the context of this publication.*

**1.2.1 Member Sizes Excluded**

Sections made from elements less than 3 mm thick are beyond the scope of AS 4100 (Clause 1.1) and are not considered in the Tables.

**1.3 Units**

The units in the Tables are consistent with those in the SI (metric) system. The base units utilised in the Tables are *newton* (N) for force, *metre* (m) for length, and *kilogram* (kg) for mass.

With some minor exceptions, all values in the Tables are rounded to three (3) significant figures.

**1.4 Limit States Design Using these Tables**

AS 4100 sets out the minimum requirements for the design, fabrication and erection of steelwork in accordance with the limit states design method. AS 4100 follows a semi-probabilistic limit state basis presented in a deterministic format.

*Definition of limit states* - When a structure or part of a structure is rendered unfit for use it reaches a 'limit state'. In this state it ceases to perform the functions or to satisfy the conditions for which it was designed. Relevant limit states for structural steel include strength, serviceability, stability, fatigue, brittle fracture, fire, and earthquake. Only two limit states are considered in the Tables - the strength limit state and, where applicable, the serviceability limit state.

Limit states design requires structural members and connections to be proportioned such that the **design action effect** ( $S^*$ ) resulting from the **design action** ( $W^*$ ), is less than or equal to the **design capacity** ( $\phi R_u$ ) i.e.

$$S^* \leq \phi R_u$$

**Design action or design load** ( $W^*$ ) is the combination of the nominal actions or loads imposed upon the structure (e.g. transverse loads on a beam) multiplied by the appropriate load factors as specified in AS 1170 (SAA Loading Code). These **design actions/loads** are identified by an asterisk (\*) after the appropriate action/load (e.g.  $W_L^*$  is the maximum design transverse load on a beam).

**Design action effects** ( $S^*$ ) are the actions (e.g. design bending moments, shear forces, axial loads) calculated from the **design actions** or **design loads** using an acceptable method of analysis (Section 4 of AS 4100). These effects are identified by an asterisk (\*) after the appropriate action effect (e.g.  $M^*$  describes the design bending moment).

**Design capacity** ( $\phi R_u$ ) is the product of the **nominal capacity** ( $R_u$ ) and the appropriate value of the capacity factor ( $\phi$ ) found in Table 3.4 of AS 4100.  $R_u$  is determined from the characteristic values and specified parameters found in Sections 5 to 9 of AS 4100.

For example, consider the strength limit state design of a simply supported beam which has full lateral restraint subject to a total transverse **design load** ( $W^*$ ) distributed uniformly along the beam.

For flexure, the appropriate **design action effect** ( $S^*$ ) is the design bending moment ( $M^*$ ) which is determined by:

$$M^* = \frac{W^* L}{8}$$

where  $L$  = span of the beam.

In this case the design capacity ( $\phi R_u$ ) is equal to the design section moment capacity ( $\phi M_s$ ), given by:

$$\phi M_s = \phi f_y Z_e$$

where  $\phi$  = the capacity factor

$Z_e$  = effective section modulus

$f_y$  = yield stress used in design

To satisfy the strength limit state, the following relationship (equivalent to  $S^* \leq \phi R_u$ ) is used:

$$M^* \leq \phi M_s$$

The maximum design bending moment ( $M^*$ ) is therefore equal to the design section moment capacity ( $\phi M_s$ ), and the **maximum design load** is that design load ( $W^*$ ) which corresponds to the maximum  $M^*$ . (It should be noted that other checks on the beam may be necessary; e.g. shear capacity, bearing capacity).

When considering external loads, in the context of this publication, the **maximum design load** ( $W_L^*$ ) must be greater than or equal to the imposed **design load** ( $W^*$ ).

Where applicable, the Tables give values of **design capacity** ( $\phi R_u$ ) and **maximum design load** ( $W_L^*$ ) determined in accordance with AS 4100. When using the Tables, the designer must determine the relevant **strength limit state design action** ( $W^*$ ) and/or corresponding **design action effect** ( $S^*$ ) to ensure that the strength limit state requirements of AS 4100 are satisfied. Where relevant, other limit states (e.g. serviceability, fatigue, etc) must also be considered by the designer. Some information useful for checking the serviceability limit state is included in the Tables.

## 1.5 Table Contents

For the range of structural steel grades and sections considered, tables are provided for:

- (i) **section dimensions and section properties:**
  - Dimensions and Properties (PART 3)
  - Properties for Assessing Section Capacity (PART 3)
  - Surface Areas (PART 3)
  - Properties for Fire Design (PART 3)
  - Detailing Parameters (PART 10)
  - Rails, Gantry Girders (PARTS 12 & 13)
  
- (ii) **design capacity ( $\phi R_u$ ) for:**
  - Members Subject to Bending (PART 5)
  - Members Subject to Axial Compression (PART 6)
  - Members Subject to Axial Tension (PART 7)
  - Members Subject to Combined Actions (PART 8)
  - Connections - Bolts/Welds (PART 9)
  
- (iii) **elastic flexural buckling load ( $N_{om}$ )** (PART 4)
  
- (iv) **maximum design load ( $W^*$ ) for:**
  - Strength Limit State ( $W_L^*$ ) for Beams (PART 5)
  - Serviceability Limit State ( $W_S^*$ ) for Beams (PART 5)
  - Strength Limit State ( $q_{st}^*, P_{st}^*$ ) for Floor Plates (PART 11)
  - Serviceability Limit State for Floor Plates (PART 11)

Acceptable methods of analysis for determining the **design action effects** are described in Section 4 of AS 4100 and material relevant to some of these methods of analysis is presented briefly in Part 4 of this publication.

## PART 2 MATERIALS

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2.2	Yield Stress and Tensile Strength .....
2.3	Properties of Steel .....
2.4	Availability .....
2.4.1	Welded Sections.....
2.4.2	Hot-rolled Sections .....

**PART 2 MATERIALS****2.1 Range of Structural Steel Grades and Sections**

Where applicable, these Tables cover the range of structural steel products manufactured in accordance with the general requirements of the following Australian Standards:

**AS 3678: Hot-rolled structural steel plates, floorplates and slabs**

**AS 3679 - Part 1: Hot-rolled structural steel bars and sections**

**AS 3679 - Part 2: Welded sections**

The section sizes and their respective grades listed in the Tables include:

**Grade 300 and Grade 400 Welded Beams and Welded Columns to AS 3679.2**

**Grade 300<sup>\*</sup> Universal Beams, Universal Columns, Parallel Flange Channels and large Angles<sup>#</sup>**

**Grade 300<sup>\*</sup> Tees cut from Universal Beams and Tees cut from Universal Columns**

**Grade 250 Taper Flange Channels, Taper Flange Beams and small Angles<sup>#</sup> to AS 3679.1**

These reflect the *most readily available* selection of steel grades for the above sections. Grade 350 is sometimes available as a higher strength alternative for hot-rolled sections. Grade 300 for welded sections is the standard grade available.

The grade designation (e.g. 300) is based on the nominal yield strength of the steel (in MPa).

Notes: (1) \* All references to Grade 300 steel for hot-rolled sections in this publication refer to the specification of BHP Grade 300PLUS™. At the time of publication, the specification for Grade 300 hot-rolled sections listed in AS 3679.1 varies from that used in these Tables. The difference occurs in the tensile properties required whereas all other requirements are met. It is envisaged that the Australian Standard will be revised to embrace the BHP Grade 300PLUS™ specification. Grade 300PLUS™ replaced Grade 250 as the base steel grade for these sections in October 1994.

- (2) # Large Angles refer to Equal Angles with leg lengths 125 x 125 mm and higher, and Unequal Angles with leg lengths 150 x 90 mm and higher. Small Angles refer to angle sections not included in the above definition for large angles.
- (3) The new range of Universal Beams, known as "Lean Beams", introduced in 1994, are included in the Universal Beam listings. These sections are 310UB32.0, 250UB25.7, 200UB22.3, 200UB18.2 and 180UB16.1.

## 2.2 Yield Stress and Tensile Strength

Table 2.1 lists the minimum yield stresses and tensile strengths for the steel grades covered by this publication and used for calculating the design capacities.

**TABLE 2.1: Strengths of Steels**

Steel Standard	Form	Steel Grade	Thickness of Material $t$	Yield Stress $f_y$	Tensile Strength $f_u$
			mm	MPa	MPa
AS 3679.2	Plate	400	$t \leq 12$ $12 < t \leq 20$ $20 < t \leq 50$	400 380 360	480
AS 3679.2	Plate	300	$8 < t \leq 12$ $12 < t \leq 20$ $20 < t \leq 150$	310 300 280	430
300PLUS™	Sections	300	$t < 11$ $11 \leq t \leq 17$ $t > 17$	320 300 280	440
AS 3679.1	Sections	250	$t \leq 12$ $12 < t < 40$ $t \geq 40$	260 250 230	410

More details on the strengths of steels can be found in Table 2.1 of AS 4100, the relevant material Standard, or the BHP publication "Hot Rolled and Structural Steel Products - 1994 Edition".

## 2.3 Properties of Steel

The properties of steel adopted in this publication are shown in Table 2.2.

**TABLE 2.2: Properties of Steels**

Property	Symbol	Value
Elastic Modulus	$E$	$200 \times 10^3$ MPa
Shear Modulus	$G$	$80 \times 10^3$ MPa
Density	$\rho$	7850 kg/m <sup>3</sup>
Poisson's Ratio	$\nu$	0.25
Coefficient of Thermal Expansion	$\alpha_T$	$11.7 \times 10^{-6}$ per °C

## Masses

The masses given in these Tables are based on a steel density of 7850 kg/m<sup>3</sup>. In practice the tabulated values are affected by rolling tolerances. Masses per metre listed are for the sections only, and do not include any allowances for cleats, end plates, weld metal, etc.

## 2.4 Availability

### 2.4.1 Welded Sections

The standard grade for Welded Beams (WB) and Welded Columns (WC) is Grade 300 steel. A higher strength option of Grade 400 is also available.

Lengths of welded sections are available from a minimum of 9 m to a maximum of 30 m. Standard lengths are 12.0, 15.0 and 18.0 metres.

### 2.4.2 Hot-rolled Sections

The standard base grade for Universal Beams (UB), Universal Columns (UC), Parallel Flange Channels (PFC), large Equal Angles (EA) and large Unequal Angles (UA) is Grade 300 steel (see Section 2.1 above).

The standard base steel grade for Taper Flange Channels (TFC), Taper Flange Beams (TFB), small Equal Angles (EA) and small Unequal Angles (UA) is Grade 250 (see Section 2.1 above).

Higher strength grades, and grades with special impact properties, such as Grade 350L0, are also available as non-standard grades.

Standard lengths for Universal Beams and Universal Columns range from 9 m to 18 m. Standard lengths for Parallel Flange Channels are in the range of 9 m to 16.5 m. Angles are available in lengths from 9 m to 15 m (for the larger sections in Grade 300), and from 7.5 to 12 m (for the smaller angles in Grade 250). Taper Flange Channels and Taper Flange Beams are available in 9 m or 12 m lengths.

Universal Bearing Piles, the 760UB series, the 690UB series, and the some of the 310UC series (198 kg/m and larger) are no longer manufactured.

Further details on length and grade availability can be found in the 1994 edition of the "Hot Rolled and Structural Steel Products" manual produced by BHP or from steel stockists.

Before specifying a section it is wise to check the supply situation if the project requires:

- large tonnages of individual sections,
- larger sizes of welded sections,
- lengths over - 15 m for hot-rolled sections  
18 m for welded sections,
- sections with non-standard grades.

## PART 3 SECTION PROPERTIES

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**PART 3 SECTION PROPERTIES****3.1 Introduction**

The section property tables include all relevant section dimensions and properties necessary for assessing the various limit states of steel structures in accordance with AS 4100. The structural sections included in these tables are:

- Welded Beams
- Welded Columns
- Universal Beams
- Universal Columns
- Structural Tees cut symmetrically from Universal Beams
- Structural Tees cut symmetrically from Universal Columns
- Parallel Flange Channels
- Taper Flange Channels
- Taper Flange Beams
- Equal Angles
- Unequal Angles
- Round and Square Bars
- Square Edge Flat Bars

**3.2 Section Property Tables**

For each group of sections (except Bars and I- sections with holes) the Tables include:

- Dimensions and Properties (Table type (A)), followed by
- Properties for Assessing Section Capacity to AS 4100 (Table type (B)).

**3.2.1 Dimensions and Properties**

The Tables give standard dimensions and properties for the structural steel sections listed above. These properties such as area ( $A_g$ ), second moments of area ( $I_x$ ,  $I_y$ ), elastic and plastic section moduli ( $Z_x$ ,  $S_x$ ,  $Z_y$ ,  $S_y$ ) and torsion and warping constants ( $J$ ,  $I_w$ ) are the fundamental geometric properties required by design standards.

**3.2.2 Properties for Assessing Section Capacity**

These properties are necessary for calculating the section capacities of the structural sections in accordance with AS 4100. The effective section moduli, "compactness" (for I- sections only), and the form factor are tabulated. These values are dependent on the steel grade.

**3.2.2.1 Compactness**

In Clauses 5.2.3, 5.2.4, and 5.2.5 of AS 4100, sections are described as **compact**, **non-compact** or **slender** (C, N or S). This categorisation provides a measure of the relative importance of yielding and local buckling of the plate elements in compression caused by bending.

For I- sections, the tables include a column headed "Compactness" where the compactness or otherwise of the sections is indicated for a given axis of bending.

The compactness of an I- section is important when selecting the methods of analysis (elastic or plastic) used to determine the design action effects (Clause 4.5 of AS 4100) or in using the higher tier provisions of Section 8 of AS 4100 for designing members subject to combined actions.

### 3.2.2.2 Effective Section Modulus

Having evaluated the compactness of a section, the effective section modulus ( $Z_e$ ) is then calculated. This parameter is based on the section moduli ( $S$ ,  $Z$ ) and is used in the determination of the design section moment capacity ( $\phi M_s$ ).  $Z_e$  is calculated using Clauses 5.2.3, 5.2.4 and 5.2.5 of AS 4100. The equations for determining  $Z_e$  reflect the proportion of the section that is effective in resisting the compression in the section caused by flexure.

For bending of sections about an asymmetric axis the value of  $Z_e$  may depend upon the direction of bending.

Additional notes on the calculation of  $Z_e$  are given in Section 3.2.2.3.

### 3.2.2.3 Form Factor

The form factor ( $k_f$ ) is defined in Clause 6.2.2 of AS 4100.  $k_f$  is used to determine the design section capacity of a concentrically loaded compression member ( $\phi N_s$ ). The calculation of  $k_f$  indicates the degree to which the column section will buckle locally before squashing.  $k_f$  represents the proportion of the section that is effective in compression and is based on the effective width of each element in the section (i.e.  $k_f = 1.0$  signifies a column section which will yield rather than buckle locally in a short or stub column test). A knowledge of  $k_f$  is also important when using the higher tier provisions of Section 8 of AS 4100 for designing members subject to combined actions.

In calculating both  $Z_e$  and  $k_f$  the following are used:

- for hot rolled sections, the HR (hot-rolled) residual stress classification,
- for welded sections, the HW (heavily welded longitudinally) residual stress classification,
- the values of plate element slenderness depend on the element width and thickness, and the yield stress. For sections where the web and flange yield stresses ( $f_{yw}$ ,  $f_{yl}$ ) are different the **lower** of the two is applied to both the web and flange to determine the slenderness of these elements.

Section 3.4 provides an example for calculating  $Z_{ex}$  and  $k_f$ . More examples can be found in *Worked Examples for Steel Structures*, 2nd Ed., published by AISI.

### 3.2.3 I- Sections with Holed Flanges

Tables of selected section properties ( $A_n$ ,  $Z_x$ ,  $Z_y$ ,  $S_x$ ,  $S_y$ ,  $Z_{ex}$  and  $Z_{ey}$ ) are given for I- sections with holes in the flanges. Standard bolt gauge lengths and number of holes are assumed in these tables. Holes in the tension flange can result in a reduction of the effective section modulus (Clause 5.2.6 of AS 4100).

If the area of the holes in the flange is less than the limit prescribed in Clause 5.2.6 of AS 4100 then the gross section properties may be used. Tables 3.1-15 to 3.1-18 list the net area, and the gross section properties (if the area of the holes is less than the limit described above), or the net section properties (if the area of the holes exceeds the limit).

### 3.3 Surface Areas & Properties for Fire Design

Tables 3.2-1(A) to 3.2-11(A) list surface areas for structural steel sections. In addition, to assist with the design of structural steel sections for fire resistance (Section 12 of AS 4100), values of the exposed surface area to mass ratio ( $k_{sm}$ ) are tabulated in Tables 3.2-1(B) to 3.2-11(B) for the various cases shown in the figure below. These tables immediately follow each surface area table.

For **unprotected steel sections** the values of  $k_{sm}$  corresponding to four- and three- sided exposure should be taken as those corresponding to Cases 1 and 4 respectively.

For members requiring the addition of fire protection materials the reference below may be used to determine the thickness of proprietary materials required for a given value of  $k_{sm}$  and Fire-Resistance Level. In the AISC Handbook, the notation  $E$  is equivalent to  $k_{sm}$ .

Suggested reference for Fire Design:

- [1] Proe, D.J., Bennetts, I.D., Thomas, I.R., Szeto, W.T., *Handbook of Fire Protection Materials for Structural Steel*, Australian Institute of Steel Construction, 1990.

Case 1	Case 2	Case 3	Case 4	Case 5	Case 6
4 - SIDED EXPOSURE			3 - SIDED EXPOSURE TO FIRE		

Cases of fire exposure considered:

1 = Profile-protected

4 = Top Flange Excluded, Profile-protected

2 = Total Perimeter, Box-protected, No Gap

5 = Top Flange Excluded, Box-protected, No Gap

3 = Total Perimeter, Box-protected, 25 mm Gap

6 = Top Flange Excluded, Box-protected, 25 mm Gap

### 3.4 Example

Determine  $Z_{ex}$  and  $k_f$  for a 250UB31.4 - Grade 300 steel section.

Solution: (All relevant data are obtained from Tables 3.1-3(A) and 3.1-3(B))

Yield stress,  $f_y = 320 \text{ MPa}$

$$\text{Flange slenderness} \quad \lambda_{ef} = \frac{b_f - t_w}{2t_f} \sqrt{\frac{f_y}{250}} = 8.13 \sqrt{\frac{320}{250}} = 9.19$$

$$\text{Web slenderness} \quad \lambda_{ew} = \frac{d_t}{t_w} \sqrt{\frac{f_y}{250}} = 38.4 \sqrt{\frac{320}{250}} = 43.4$$

- (a) To calculate  $Z_{ex}$  the plate element slenderness values are compared with the plate element slenderness limits in Table 5.2 of AS 4100.

Bending about the  $x$ -axis puts the flange in uniform compression. Hence

$$\lambda_{ef} = 9.19 \quad \lambda_{ep} = 9 \quad \lambda_{ey} = 16 \quad \lambda_{ef}/\lambda_{ey} = 0.574 \quad (\text{Table 5.2 of AS 4100})$$

Bending about the  $x$ -axis places one edge of the web in tension and the other in compression. Hence

$$\lambda_{ew} = 43.4 \quad \lambda_{ep} = 82 \quad \lambda_{ey} = 115 \quad \lambda_{ew}/\lambda_{ey} = 0.377 \quad (\text{Table 5.2 of AS 4100})$$

The flange has the higher value of  $\lambda_e/\lambda_{ey}$  and hence is the critical element in the section. From Clause 5.2.2 of AS 4100 the section slenderness and slenderness limits are the flange values, i.e.

$$\lambda_s = 9.19 \quad \lambda_{sp} = 9 \quad \lambda_{sy} = 16$$

Now  $\lambda_{sp} < \lambda_s \leq \lambda_{sy}$ .  $\therefore$  The section is NON-COMPACT.

$$Z_x = 354 \times 10^3 \text{ mm}^3 \quad S_x = 397 \times 10^3 \text{ mm}^3$$

$$Z_c = \min [S_x, 1.5 Z_x] = \min [397, 1.5 \times 354] \times 10^3 = 397 \times 10^3 \text{ mm}^3$$

$$Z_{ex} = Z + \left[ \frac{(\lambda_{sy} - \lambda_s)}{(\lambda_{sy} - \lambda_{sp})} (Z_c - Z) \right] = 354 \times 10^3 + \left[ \frac{(16 - 9.19)}{(16 - 9)} (397 - 354) \right] \times 10^3 \\ = 395 \times 10^3 \text{ mm}^3$$

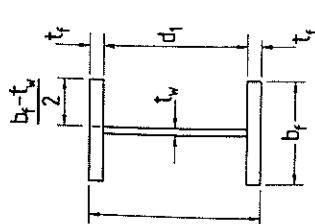
- (b) To determine the form factor ( $k_f$ ) the plate element slenderness for both the flange and web are compared with the plate element yield slenderness limits ( $\lambda_{ey}$ ) in Table 6.2.4 of AS 4100.

$$\text{Flange} \quad \lambda_{ef} = 9.19 \quad \lambda_{ey} = 16$$

$$\text{Web} \quad \lambda_{ew} = 43.4 \quad \lambda_{ey} = 45$$

For both the web and the flange  $\lambda_e < \lambda_{ey}$ . Hence both the web and the flange are fully effective and hence the effective area equals the gross area ( $A_e = A_g$ ).

$$\therefore k_f = A_e/A_g = 1$$



**WELDED BEAMS**  
**DIMENSIONS AND PROPERTIES**

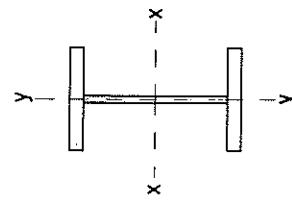


TABLE 3.1-1(A)

Designation	Depth of Section d	DIMENSIONS				RATIOS		PROPERTIES										
		Flange Width b <sub>f</sub>		Web Thickness t <sub>w</sub>	Depth Between Flanges d <sub>1</sub>	$\frac{d_1}{t_w}$	$\frac{(b_f-t_w)}{2t_f}$	Gross Section Area		About x-axis		About y-axis		Torsion Constant J	Warping Constant I <sub>w</sub>			
		mm	mm					mm <sup>2</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm <sup>2</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	10 <sup>3</sup> mm <sup>3</sup>					
1200WB455	1200	500	40.0	16.0	1120	70.0	6.05	57900	15300	25600	28200	515	834	3330	5070	120	22000	280000
423	1192	500	36.0	16.0	1120	70.0	6.72	53900	13900	23300	25800	508	750	3000	4570	118	16500	251000
392	1184	500	32.0	16.0	1120	70.0	7.56	49900	12500	21100	23400	500	667	2670	4070	116	12100	221000
342	1184	400	32.0	16.0	1120	70.0	6.00	43500	10400	17500	19800	488	342	1710	2630	88.6	9960	113000
317	1176	400	28.0	16.0	1120	70.0	6.86	40300	9250	15700	17900	479	299	1500	2310	86.1	7230	98500
278	1170	350	25.0	16.0	1120	70.0	6.68	35400	7610	13000	15000	464	179	1020	1600	71.1	5090	58700
249	1170	275	25.0	16.0	1120	70.0	5.18	31700	6380	10900	12500	449	87.0	633	1020	52.4	4310	28500
1000WB322	1024	400	32.0	16.0	960	60.0	6.00	41000	7480	14600	16400	427	342	1710	2300	91.3	9740	84100
296	1016	400	28.0	16.0	960	60.0	6.86	37800	6650	13100	14800	420	299	1490	1020	89.0	7010	73000
258	1010	350	25.0	16.0	960	60.0	6.68	32900	5430	10700	12500	406	179	1020	1590	73.8	4870	43400
215	1000	300	20.0	16.0	960	60.0	7.10	27400	4060	8120	9570	385	90.3	602	961	57.5	2890	21700
900WB282	924	400	32.0	12.0	860	71.7	6.06	35900	5730	12400	13600	399	341	1710	2590	97.5	8870	67900
257	916	400	28.0	12.0	860	71.7	6.93	32700	5050	11000	12200	393	299	1490	2270	95.6	6150	58900
218	910	350	25.0	12.0	860	71.7	6.76	27800	4060	8930	9960	382	179	1020	1560	80.2	4020	35000
175	900	300	20.0	12.0	860	71.7	7.20	22300	2960	6580	7500	364	90.1	601	931	63.5	2060	17400
800WB192	816	300	28.0	10.0	760	76.0	5.18	24400	2970	7290	8060	349	126	840	1280	71.9	4420	19600
168	810	275	25.0	10.0	760	76.0	5.30	21400	2480	6140	6840	341	86.7	631	964	63.7	2990	13400
146	800	275	20.0	10.0	760	76.0	6.62	18600	2040	5100	5730	331	69.4	505	775	61.1	1670	10600
122	792	250	16.0	10.0	760	76.0	7.50	15600	1570	3970	4550	317	41.7	334	54.9	51.7	921	6280
700WB173	716	275	28.0	10.0	660	66.0	4.73	22000	2060	5760	6390	306	97.1	706	1080	66.4	4020	11500
150	710	250	25.0	10.0	660	66.0	4.80	19100	1710	4810	5370	299	65.2	521	642	56.4	2690	7640
130	700	250	20.0	10.0	660	66.0	6.00	16600	1400	3980	4490	290	52.1	417	56.0	1510	6030	4770
115	692	250	16.0	10.0	660	66.0	7.50	14600	1150	3330	3790	281	41.7	334	54.7	53.5	888	4770

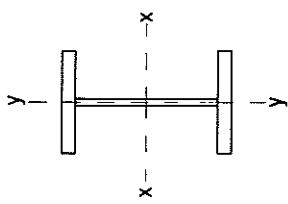
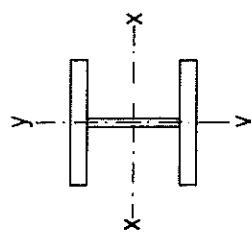
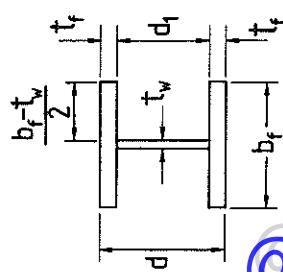


TABLE 3.1-1(B)

**WELDED BEAMS**  
**GRADE 300 & 400**  
**PROPERTIES FOR ASSESSING SECTION CAPACITY**

Designation	GRADE 300: AS 3679.2						GRADE 400: AS 3679.2						
	About x-axis			About y-axis			About x-axis			About y-axis			
	Yield Stress	Form Factor	Compactness (C, N, S)	Yield Stress	Form Factor	Compactness (C, N, S)	Yield Stress	Form Factor	Compactness (C, N, S)	Yield Stress	Form Factor	Compactness (C, N, S)	
	Flange $f_{yf}$	Web $f_{yw}$		Flange $f_{yf}$	Web $f_{yw}$		Flange $f_{yf}$	Web $f_{yw}$		Flange $f_{yf}$	Web $f_{yw}$		
	MPa	MPa		MPa	MPa		MPa	MPa		MPa	MPa		
1200WB455	280	300	0.837	C	28200	C	5000	360	0.820	N	28100	C	5000
423	280	300	0.825	C	25800	C	4500	360	0.806	N	25700	N	4500
392	280	300	0.811	C	23400	N	4000	360	0.791	N	23300	N	3900
342	280	300	0.783	C	19800	C	2560	360	0.760	N	19600	C	2560
317	280	300	0.766	C	17900	C	2240	360	0.741	N	17700	N	2230
278	280	300	0.733	C	15000	C	1530	360	0.705	N	14900	N	1530
249	280	300	0.701	C	12900	C	949	360	0.670	N	12800	C	949
1000WB322	280	300	0.832	C	16400	C	2560	360	0.807	C	16400	C	2560
296	280	300	0.817	C	14800	C	2240	360	0.791	C	14800	N	2230
258	280	300	0.790	C	12300	C	1530	360	0.760	C	12300	N	1530
215	300	300	0.738	C	9570	C	903	380	0.704	C	9570	N	887
900WB282	280	310	0.845	C	13600	C	2560	360	0.830	N	13500	C	2560
257	280	310	0.830	C	12200	C	2240	360	0.813	N	12000	N	2220
218	280	310	0.800	C	9960	C	1530	360	0.780	N	9480	N	1530
175	300	310	0.744	C	7500	C	901	380	0.721	N	7320	N	882
800WB192	280	310	0.824	C	8060	C	1260	360	0.808	N	7850	C	1260
168	280	310	0.799	C	6840	C	946	360	0.781	N	6640	C	946
146	300	310	0.763	N	5710	C	757	380	0.744	N	5510	N	754
122	300	310	0.718	N	4530	N	498	380	0.695	N	4340	N	486
700WB173	280	310	0.850	C	6390	C	1060	360	0.833	C	6390	C	1060
150	280	310	0.828	C	5370	C	782	360	0.807	C	5370	C	782
130	300	310	0.795	C	4490	C	626	380	0.773	C	4490	C	626
115	300	310	0.767	C	3790	N	498	380	0.742	C	3790	N	486

Notes: (1) For Grade 300 sections the tensile strength ( $f_u$ ) is 430 MPa.  
(2) For Grade 400 sections the tensile strength ( $f_u$ ) is 480 MPa.  
(3) C: Compact Section; N: Non-compact Section; S: Slender Section.



**TABLE 3.1-2(A)**  
**WELDED COLUMNS**  
**DIMENSIONS AND PROPERTIES**

Designation kg/m	Depth of Section d	DIMENSIONS				RATIOS		PROPERTIES										
		Flange		Web Thickness t <sub>w</sub>	Depth Between Flanges d <sub>i</sub>	$\frac{d_1}{t_w}$	$\frac{(b_i - t_w)}{2t_i}$	About x-axis			About y-axis			Warping Constant I <sub>w</sub>				
		Width b <sub>i</sub>	Thickness t <sub>i</sub>					I <sub>x</sub>	S <sub>x</sub>	I <sub>y</sub>	S <sub>y</sub>	r <sub>y</sub>						
500WC440	480	500	40.0	40.0	400	10.0	5.75	56000	2150	8980	10400	196	835	3340	5160	122	30100	40400
414	480	500	40.0	32.0	400	12.5	5.85	52800	2110	8800	10100	200	834	3340	5100	126	25400	40400
383	472	500	36.0	32.0	400	12.5	6.50	48800	1890	7990	9130	197	751	3000	4600	124	19900	35700
340	514	500	32.0	25.0	450	18.0	7.42	43300	2050	7980	8980	218	667	2670	4070	124	13100	38800
290	506	500	28.0	20.0	450	22.5	8.57	37000	1750	6930	7700	218	584	2330	3550	126	8420	33300
267	500	500	25.0	20.0	450	22.5	9.60	34000	1560	6250	6950	214	521	2080	3170	124	6370	29400
228	490	500	20.0	450	22.5	12.0	29000	1260	5130	5710	208	417	1670	2550	120	3880	23000	
400WC361	430	400	40.0	40.0	350	8.75	4.50	46000	1360	6340	7470	172	429	2140	3340	96.5	24800	16300
328	430	400	40.0	28.0	350	12.5	4.65	41800	1320	6140	7100	178	427	2140	3270	101	19200	16200
303	422	400	36.0	28.0	350	12.5	5.17	38600	1180	5570	6420	175	385	1920	2850	99.8	14800	14300
270	414	400	32.0	25.0	350	14.0	5.86	34400	1030	4950	5660	173	342	1710	2610	99.8	10400	12500
212	400	400	25.0	20.0	350	17.5	7.60	27000	776	3880	4360	169	267	1330	2040	99.4	5060	9380
181	390	400	20.0	20.0	350	17.5	9.50	23000	620	3180	3570	164	214	1070	1640	96.4	3080	7310
144	382	400	16.0	16.0	350	21.9	12.0	18400	486	2550	2830	163	171	854	1300	96.3	1580	5720
350WC280	355	350	40.0	28.0	275	9.82	4.02	35700	747	4210	4940	145	286	1640	2500	89.6	16500	7100
258	347	350	36.0	28.0	275	9.82	4.47	32900	661	3810	4450	142	258	1470	2260	88.5	12700	6230
230	339	350	32.0	25.0	275	11.0	5.08	29900	573	3380	3910	140	229	1310	2000	88.4	8960	5400
197	331	350	28.0	20.0	275	13.8	5.89	25100	486	2940	3350	139	200	1140	1740	89.3	5750	4600

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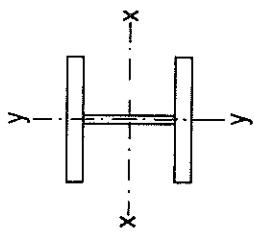


TABLE 3.1-2(B)

**WELDED COLUMNS  
GRADE 300 & 400**
**PROPERTIES FOR ASSESSING SECTION CAPACITY**

Designation	GRADE 300: AS 3679.2						GRADE 400: AS 3679.2						
	About x-axis			About y-axis			About x-axis			About y-axis			
	Yield Stress Flange $f_{y1}$	Web $f_{yw}$	Form Factor $k_f$	Compactness (C, N, S)	$Z_{ex}$	Compactness (C, N, S)	$Z_{ey}$	Yield Stress Flange $f_{y1}$	Web $f_{yw}$	Form Factor $k_f$	Compactness (C, N, S)	$Z_{ex}$	Compactness (C, N, S)
	MPa	MPa			$10^3 \text{ mm}^3$		$10^3 \text{ mm}^3$	MPa	MPa			$10^3 \text{ mm}^3$	
500WC440	280	280	1.00	C	10400	C	5010	360	360	1.00	C	10400	C
414	280	280	1.00	C	10100	C	5010	360	360	1.00	C	10100	C
383	280	280	1.00	C	9130	C	4510	360	360	1.00	C	9130	C
340	280	280	1.00	C	8980	C	4000	360	360	1.00	C	8830	C
290	280	300	1.00	N	7570	N	3410	360	380	1.00	N	7410	N
267	280	300	1.00	N	6700	N	2970	360	380	1.00	N	6540	N
228	300	300	1.00	N	5210	N	2200	360	380	0.964	S	4860	N
400WC361	280	280	1.00	C	7470	C	3210	360	360	1.00	C	7470	C
328	280	280	1.00	C	7100	C	3200	360	360	1.00	C	7100	C
303	280	280	1.00	C	6420	C	2880	360	360	1.00	C	6420	C
270	280	280	1.00	C	5660	C	2560	360	360	1.00	C	5660	C
212	280	300	1.00	N	4360	N	2000	360	380	1.00	N	4270	N
181	300	300	1.00	N	3410	N	1510	380	380	1.00	N	3330	N
144	300	300	1.00	N	2590	N	1120	360	380	0.964	S	2410	N
360WC280	280	280	1.00	C	4940	C	2450	360	360	1.00	C	4940	C
258	280	280	1.00	C	4450	C	2210	360	360	1.00	C	4450	C
230	280	280	1.00	C	3910	C	1960	360	360	1.00	C	3910	C
197	280	300	1.00	C	3350	C	1720	360	380	1.00	C	3350	C

Notes: (1) For Grade 300 sections the tensile strength ( $f_u$ ) is 430 MPa.

(2) For Grade 400 sections the tensile strength ( $f_u$ ) is 460 MPa.

(3) C: Compact Section; N: Non-compact Section; S: Slender Section.

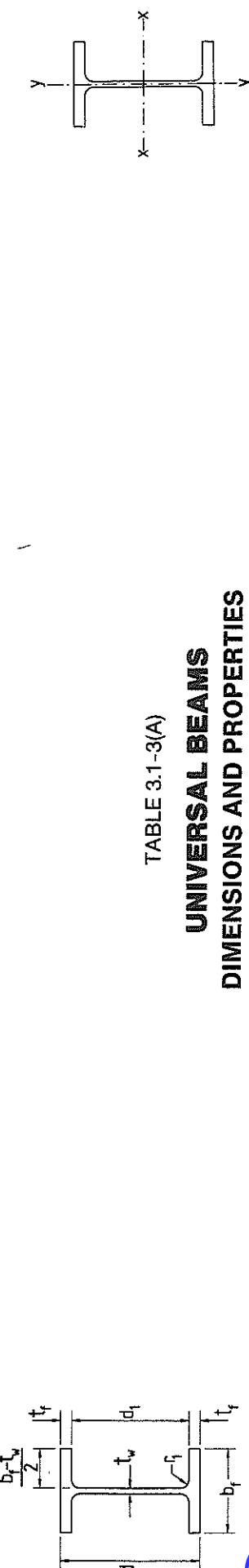
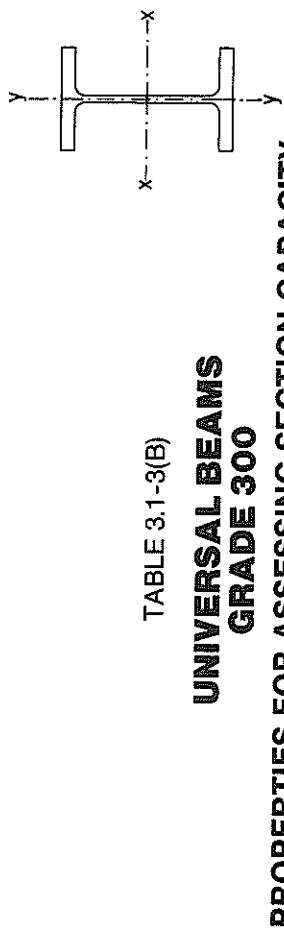


TABLE 3.1-3(A)  
UNIVERSAL BEAMS  
DIMENSIONS AND PROPERTIES

Designation	Depth of Section <i>d</i>	DIMENSIONS						RATIOS		PROPERTIES										
		Flange Width <i>b</i>		Flange Thickness <i>t</i> <sub>f</sub>		Web Thickness <i>t</i> <sub>w</sub>		Root Radius <i>r</i> <sub>1</sub>	Depth Between Flanges <i>d</i> <sub>1</sub>	$\frac{d_1}{t_w}$	$\frac{(b_f - t_w)}{2t_f}$	Gross Section Area			About x-axis			About y-axis		
		mm	mm	mm	mm	mm	mm					$\text{mm}^2$	$10^3\text{mm}^4$	$10^3\text{mm}^3$	$10^3\text{mm}^3$	$10^6\text{mm}^4$	$I_y$	$Z_y$	$S_y$	$r_y$
610UB-25	612	229	19.6	11.9	14.0	572	48.1	5.54	16000	986	3230	3680	249	39.3	343	536	49.6	1560	3450	3450
610UB-113	607	228	17.3	11.2	14.0	572	51.1	6.27	14500	875	2880	3280	246	34.3	300	469	48.7	1140	2980	2980
602	602	228	14.8	10.6	14.0	572	54.0	7.34	13000	761	2530	2900	242	29.3	257	402	47.5	790	2530	2530
550UB-924	533	209	15.6	10.2	14.0	502	49.2	6.37	11800	554	2080	2370	217	23.8	228	355	44.9	775	1590	1590
520	528	209	13.2	9.6	14.0	502	52.3	7.55	10500	477	1810	2070	213	20.1	193	301	43.8	526	1330	1330
460UB-82.1	460	191	16.0	9.9	11.4	428	43.3	5.66	10500	372	1610	1840	188	18.6	195	303	42.2	701	919	919
74.6	457	190	14.5	9.1	11.4	428	47.1	6.24	9520	335	1460	1660	188	16.6	175	271	41.8	530	815	815
67.1	454	190	12.7	8.5	11.4	428	50.4	7.15	8580	296	1300	1480	186	14.5	153	238	41.2	378	708	708
410UB-59.7	406	178	12.8	7.8	11.4	381	48.8	6.65	7640	216	1060	1200	168	12.1	135	209	39.7	337	467	467
53.7	403	178	10.9	7.6	11.4	381	50.1	7.82	6890	188	933	1060	165	10.3	115	179	38.6	234	394	394
359	172	13.0	8.0	11.4	333	41.6	6.31	7240	161	899	1010	149	11.0	128	198	39.0	338	330	330	
56.7	356	171	11.5	7.3	11.4	333	45.6	7.12	6470	142	798	897	148	9.60	112	173	38.5	241	284	284
44.7	352	171	9.7	6.9	11.4	333	48.2	8.46	5720	121.	689	777	146	8.10	94.7	146	37.6	161	237..	237..
310UB-46.2	307	166	11.8	6.7	11.4	284	42.3	6.75	5930	100	654	729	130	9.01	109	166	39.0	233	197	197
40.4	304	165	10.2	6.1	11.4	284	46.5	7.79	5210	86.4	659	633	129	7.65	92.7	142	38.3	157	165	165
32.0	298	149.	8.0	5.5	13.0	282	51.3	8.97	4080	63.2	424	475	124	4.42	59.3	91.8	32.9	86.5	92.9	92.9
256	146	10.9	6.4	8.9	234	36.6	6.40	4750	55.7	435	486	108	5.66	77.5	119	34.5	158	85.2	85.2	
31.4	252	146	8.6	6.1	8.9	234	38.4	8.13	4010	44.5	354	397	105	4.47	61.2	94.2	33.4	89.3	165.9	165.9
25.7	248	8.0	5.0	12.0	232	46.4	7.44	3270	35.4	285	319	104	2.55	41.1	63.6	27.9	67.4	36.7	36.7	
250UB-37.3	256	134	9.6	6.3	8.9	188	6.65	3820	29.1	281	316	87.3	3.86	57.5	88.4	31.8	105	37.6	37.6	
207	134	9.6	6.3	8.9	188	32.3	8.15	3230	23.6	232	260	85.4	3.06	46.1	70.9	30.8	62.7	29.2	29.2	
200UB-29.8	133	7.8	5.8	8.9	188	37.5	9.14	2870	21.0	208	231	85.5	2.75	41.3	63.4	31.0	45.0	26.0	26.0	
25.4	133	7.0	5.0	8.9	188	40.9	6.75	2320	15.8	160	180	82.6	1.14	23.0	35.7	22.1	38.6	10.4	10.4	
22.3	202	7.0	5.0	8.9	188	40.9	6.75	2320	15.8	160	180	82.6	1.14	23.0	35.7	22.1	38.6	10.4	10.4	
18.2	198	9.9	7.0	4.5	11.0	184	40.9	6.75	2320	15.8	160	180	82.6	1.14	23.0	35.7	22.1	38.6	10.4	10.4
180UB-179	90	10.0	6.0	8.9	159	26.5	4.20	2820	15.3	171	195	73.6	1.22	27.1	42.3	20.8	81.6	8.71	8.71	
18.1	175	90	8.0	5.0	8.9	159	31.8	5.31	2300	12.1	139	157	72.6	0.95	21.7	33.7	20.6	44.8	6.80	6.80
16.1	173	90	7.0	4.5	8.9	159	35.3	6.11	2040	10.6	123	138	72.0	0.853	19.0	29.4	20.4	31.5	5.88	5.88
150UB-155	75	9.5	6.0	8.0	136	22.7	3.63	2300	9.05	117	135	62.8	0.672	17.9	28.2	17.1	60.5	3.56	3.56	
14.0	150	75	7.0	5.0	8.0	136	5.00	1780	6.66	88.8	102	61.1	0.495	13.2	20.8	16.6	28.1	2.53	2.53	



**TABLE 3.1-3(B)**  
**UNIVERSAL BEAM**  
**GRADE 300**  
**PROPERTIES FOR ASSESSING S**

Designation	Yield Stress		Form Factor $k_t$	About x-axis		About y-axis		
	Flange $f_y$	Web $f_{y,w}$		Compactness (C, N, S)		$Z_x$	$Z_y$	
				MPa	MPa	$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$	
610UB125	280	300	0.950	C	3680	C	515	
	113	280	0.926	C	3290	C	451	
	101	300	0.888	C	2900	C	386	
530UB 92.4	300	320	0.928	C	2370	C	342	
	82.0	300	0.902	C	2070	C	289	
	74.6	300	0.979	C	1840	C	292	
460UB 82.1	74.6	320	0.948	C	1660	C	262	
	67.1	300	0.922	C	1480	C	230	
	59.7	300	0.988	C	1200	C	203	
360UB 56.7	53.7	320	0.913	C	1060	C	173	
	50.7	300	0.996	C	1010	C	193	
	44.7	320	0.963	C	897	C	168	
310UB 46.2	300	320	0.991	C	72.9	C	140	
	40.4	320	0.952	C	63.3	C	139	
	32.0	320	0.915	N	46.7	N	86.9	
250UB 37.3	320	320	1.00	C	48.6	C	116	
	31.4	320	1.00	N	39.5	N	91.4	
	25.7	320	0.949	C	31.9	C	61.7	
200UB 29.8	320	320	1.00	C	31.6	C	86.3	
	25.4	320	1.00	N	25.9	N	68.8	
	22.3	320	1.00	N	22.7	N	60.3	
180UB 22.2	320	320	1.00	C	18.0	C	34.4	
	18.1	320	1.00	C	19.5	C	40.7	
	16.1	320	1.00	C	15.7	C	32.5	
150UB 18.0	320	320	1.00	C	13.8	C	28.4	
	14.0	320	1.00	C	13.5	C	26.9	
	12.0	320	1.00	C	10.2	C	19.8	

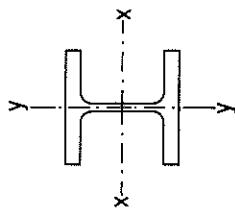
Notes: (1) For Grade 300 sections the tensile strength ( $f_u$ ) is 440 MPa.  
 (2) C: Compact Section; N: Non-compact Section; S: Slender Section.  
 (3) Grade 300 refers to BHP Grade 300 PLUS™. See Note (1) on page 2-1.



TABLE 3.1-4(A)  
UNIVERSAL COLUMNS  
DIMENSIONS AND PROPERTIES

Designation	Depth of Section $d$	DIMENSIONS				RATIOS		PROPERTIES										Warping Constant $I_w$		
		Flange		Web Thickness $t_w$	Root Radius $r_i$	Depth Between Flanges $d_1$	$\frac{d_1}{t_w}$	Gross Section Area $A_g$		About x-axis		About y-axis		$I_x$	$I_y$	$S_x$	$S_y$	$r_x$	$r_y$	Torsion Constant $J$
		Width $b_f$	Thickness $t_f$					$10^3 \text{ mm}^4$	$10^3 \text{ mm}^3$											
310UC158	327	311	25.0	15.7	16.5	277	17.7	5.91	20100	388	2370	2680	139	125	807	1230	78.9	3810	2860	
310UC158	321	309	21.7	13.8	16.5	277	20.1	6.80	17500	329	2050	2300	137	107	691	1050	78.2	2520	2380	
310UC158	315	307	18.7	11.9	16.5	277	23.3	7.89	15000	277	1760	1960	136	90.2	588	893	77.5	1630	1980	
310UC158	308	305	15.4	9.9	16.5	277	28.0	9.58	12400	223	1450	1600	134	72.9	478	725	76.7	928	1560	
250UC 89.5	260	256	17.3	10.5	14.0	225	21.5	7.10	11400	143	1100	1230	112	48.4	378	575	65.2	1040	713	
250UC 89.5	254	254	14.2	8.6	14.0	225	26.2	8.64	9320	114	897	992	111	38.8	306	463	64.5	586	557	
200UC 59.5	210	205	14.2	9.3	11.4	181	19.5	6.89	7620	61.3	584	656	89.7	20.4	199	303	51.7	477	195	
200UC 59.5	206	204	12.5	8.0	11.4	181	22.7	7.84	6660	52.8	512	570	89.1	17.7	174	264	51.5	325	166	
200UC 59.5	203	203	11.0	7.3	11.4	181	24.8	8.90	5900	45.9	451	500	88.2	15.3	151	230	51.0	228	142	
150UC 37.2	162	154	11.5	8.1	8.9	139	17.1	6.34	4730	22.2	274	310	68.4	7.01	91.0	139	38.5	197	39.6	
150UC 37.2	158	153	9.4	6.6	8.9	139	21.0	7.79	3860	17.6	223	250	67.5	5.62	73.4	112	38.1	109	30.8	
150UC 37.2	152	152	6.8	6.1	8.9	139	22.8	10.7	2980	12.6	166	184	65.1	3.98	52.4	80.2	36.6	50.2	21.1	
100UC 14.8	97	99	7.0	5.0	10.0	83	16.6	6.71	1890	3.18	65.6	74.4	41.1	1.14	22.9	35.2	24.5	34.9	2.30	

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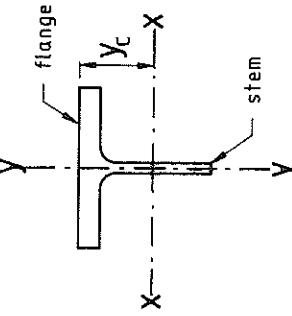


**TABLE 3.1-4(B)**  
**UNIVERSAL COLUMNS**  
**GRADE 300**  
**PROPERTIES FOR ASSESSING SECTION CAPACITY**

Designation	Yield Stress Flange $f_y$	Web $f_{yw}$	Form Factor $k_t$	About x-axis		Compacness (C, N, S)	$Z_{sy}$ $\cdot 10^3 \text{ mm}^3$
				Compactness (C, N, S)	$Z_x$ $\cdot 10^3 \text{ mm}^3$		
310JC158	280	300	1.00	C	2680	C	1210
137	280	300	1.00	C	2300	C	1040
118	280	300	1.00	C	1960	C	882
96.8	300	320	1.00	N	1560	N	694
250JC 89.5	280	320	1.00	C	1230	C	567
72.9	300	320	1.00	N	986	N	454
200JC 59.5	300	320	1.00	C	656	C	299
52.2	300	320	1.00	C	570	C	260
46.2	300	320	1.00	N	494	N	223
150JC 37.2	300	320	1.00	C	310	C	137
30.0	320	320	1.00	C	250	C	110
23.4	320	320	1.00	N	176	N	73.5
100JC 14.8	320	320	1.00	C	74.4	C	34.3

Notes:

- (1) For Grade 300 sections the tensile strength ( $f_u$ ) is 440 MPa.
- (2) C: Compact Section; N: Non-compact Section; S: Slender Section.
- (3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TEES CUT FROM UNIVERSAL BEAMS  
DIMENSIONS AND PROPERTIES**

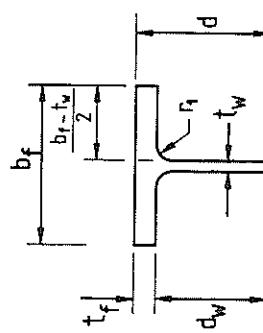


TABLE 3.1-5(A)

Designation kg/m	From Universal Section	Depth of Section d	DIMENSIONS				RATIOS		PROPERTIES											
			Flange Width $b_i$		Web Thickness $t_i$	Root Radius $r_i$	Depth to Flange $d_w$	$\frac{d_w}{t_w}$	Gross Section Area $A_g$	Coordinate of Centroid $y_c$	About x-axis		About y-axis		Torsion Constant $J$					
			mm	mm	mm	mm	mm	$\frac{(b_i-t_w)}{2t_w}$	mm <sup>2</sup>	mm	$I_x$	$Z_x$	$S_x$	$r_x$	$I_y$	$Z_y$	$S_y$	$r_y$		
405BT62.5	610UB125	305	229	19.6	11.9	14.0	285	24.0	5.54	7970	74.8	68.3	913	297	527	92.6	19.7	268	49.7	
56.5	113	303	228	17.3	11.2	14.0	285	25.5	6.27	7220	75.6	62.4	825	275	489	92.9	17.1	150	235	
50.5	101	300	228	14.8	10.6	14.0	285	26.9	7.34	6480	77.4	56.7	733	265	456	93.6	14.7	129	201	
255BT46.3	530UB92.4	266	209	15.6	10.2	14.0	250	24.5	6.37	5690	65.3	38.7	593	193	344	81.1	11.9	114	178	
41.0	82.0	263	209	13.2	9.6	14.0	250	26.0	7.55	5240	66.9	35.0	522	178	318	81.7	10.1	96.3	151	
255BT41.1	460UB82.1	229	191	16.0	9.9	11.4	213	21.5	5.66	5220	54.4	24.5	451	140	249	68.5	9.31	97.5	152	
37.3	74.6	228	190	14.5	9.1	11.4	213	23.4	6.24	4750	53.8	22.2	413	128	226	68.4	8.30	87.4	136	
33.6	67.1	226	190	12.7	8.5	11.4	213	25.1	7.15	4280	54.2	20.2	372	118	208	68.7	7.27	76.6	119	
245BT29.9	410UB59.7	202	178	12.8	7.8	11.4	189	24.3	6.85	3810	45.6	13.7	299	87.3	154	59.9	6.03	67.7	105	
25.9	53.7	200	178	10.9	7.6	11.4	189	24.9	7.82	3440	47.5	12.7	267	83.0	147	60.7	5.13	57.7	89.4	
360UB56.7	360UB56.7	178	172	13.0	8.0	11.4	165	20.7	6.31	3610	39.2	9.68	247	69.6	123	51.7	5.52	64.2	99.2	
50.7	50.7	177	171	11.5	7.3	11.4	165	22.6	7.12	3230	38.9	8.65	223	62.7	110	51.8	4.80	56.1	86.6	
22.4	44.7	175	171	9.7	6.9	11.4	165	24.0	8.46	2860	39.9	7.83	196	57.9	102	52.4	4.05	47.4	73.2	
310UB46.2	153	166	11.8	6.7	11.4	141	21.0	6.75	2960	30.3	5.30	175	43.4	76.7	42.3	4.50	54.3	83.2	39.0	
20.2	40.4	151	165	10.2	6.1	11.4	141	23.1	7.79	2600	30.1	4.69	156	38.8	68.3	42.5	3.82	46.3	71.0	
16.0	32.0	148	149	8.0	5.5	13.0	140	25.5	8.97	2030	32.2	3.86	120	33.3	58.7	43.6	2.21	29.7	45.9	
255BT18.7	250UB37.3	127	146	10.9	6.4	8.9	116	18.2	6.40	2370	25.4	2.91	114	286	50.8	35.0	2.83	38.8	59.5	34.6
15.7	31.4	125	146	8.6	6.1	8.9	116	19.0	8.13	2000	26.5	2.58	97.3	26.2	46.2	35.9	2.23	30.6	47.1	33.4
12.9	25.7	123	124	8.0	5.0	12.0	115	23.0	7.44	1630	25.9	2.03	78.6	20.9	36.9	35.3	1.27	20.6	31.8	33.6
100BT14.9*	200UB29.8	103	134	9.6	6.3	8.9	93	14.7	6.65	1910	20.6	1.49	72.3	18.2	32.6	28.0	1.93	28.8	44.2	31.8
12.7*	25.4	101	133	7.8	5.8	8.9	93	16.0	8.15	1610	20.8	1.29	62.1	16.2	28.7	28.3	1.53	23.0	35.4	31.2
11.2*	22.3	100	133	7.0	5.0	8.9	93	18.6	9.14	1430	19.8	1.11	56.2	13.9	24.5	27.9	1.37	20.7	31.7	31.0
9.1	18.2	98	99	7.0	4.5	11.0	91	20.2	6.75	1150	21.0	0.911	43.3	11.8	21.0	28.1	0.568	11.5	17.9	22.4
90BT11.1	180UB22.2	89	90	10.0	6.0	8.9	79	13.1	4.20	1400	19.9	0.857	43.1	12.5	22.6	24.7	0.610	13.6	21.1	40.6
9.1	18.1	87	90	8.0	5.0	8.9	79	15.7	5.31	1150	18.9	0.684	36.2	10.1	18.1	24.4	0.488	10.8	16.8	22.3
8.1	16.1	86	90	7.0	4.5	8.9	79	17.4	6.11	1020	18.4	0.601	32.6	8.96	16.0	24.3	0.427	9.48	14.7	20.5
75BT9.0	150UB18.0	77	75	9.5	6.0	8.0	67	11.2	3.63	1140	18.3	0.533	292	9.16	16.6	21.6	0.336	8.96	14.1	17.2
7.0	14.0	74	75	7.0	5.0	8.0	67	13.4	5.00	887	17.6	0.410	28.3	7.26	13.0	21.5	0.247	6.60	10.4	13.9

Notes: (1) \* indicates x- and y-axes are interchanged from that shown on the diagram.  
(2) The value of the warping constant,  $I_{w0}$ , for Tees is approximately zero.  
(3) A 1 mm cutting allowance has been provided off each split tee.

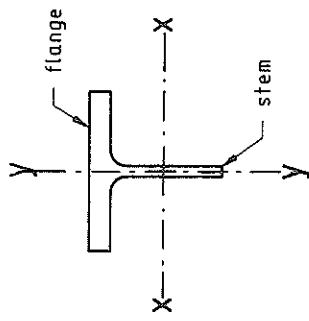


TABLE 3.1-5(B)  
TEES CUT FROM UNIVERSAL BEAMS  
GRADE 300  
PROPERTIES FOR ASSESSING SECTION CAPACITY

Designation	Yield Stress		Form Factor $K_t$	About x-axis			About y-axis	
	Flange $t_{yf}$	Web $t_{yw}$		Flange $Z_{ex}$	Flange $Z_{ey}$	Stem $Z_{sx}$	Stem $Z_{sy}$	
	MPa	MPa		$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$	
305BT62.5	280	300	0.843	445	288	258	225	
56.5	280	300	0.820	412	237	193		
50.5	300	320	0.787	382	183			
265BT46.3	300	320	0.825	290	168	171		
41.0	300	320	0.799	267	137	144		
230BT41.1	300	320	0.870	210	146	146		
37.3	300	320	0.846	192	121	131		
33.6	300	320	0.823	176	97.3	115		
205BT29.9	300	320	0.846	131	77.1	102		
26.9	320	320	0.819	124	65.2	86.5		
180BT28.4	300	320	0.893	104	74.7	96.3		
25.4	300	320	0.867	94.0	63.1	84.2		
22.4	320	320	0.836	84.6	49.3	70.2		
155BT23.1	300	320	0.903	65.0	46.0	81.4		
20.2	320	320	0.872	58.2	35.6	69.5		
16.0	320	320	0.832	47.3	25.1	43.4		
125BT18.7	320	320	0.931	42.9	32.6	58.2		
15.7	320	320	0.909	39.0	29.1	45.7		
12.9	320	320	0.864	31.4	19.3	30.8		
100BT14.9 *	320	320	0.987	27.3	22.9	43.2		
12.7 *	320	320	0.961	24.0	19.7	34.4		
11.2 *	320	320	0.923	19.5	15.6	30.1		
9.1	320	320	0.893	17.8	12.6	17.2		
90BT11.1	320	320	1.00	18.7	16.5	20.3		
9.1	320	320	0.966	15.2	12.4	16.3		
8.1	320	320	0.934	13.4	10.4	14.2		
75BT 9.0	320	320	1.00	13.7	12.7	13.4		
7.0	320	320	1.00	10.9	9.49	9.89		

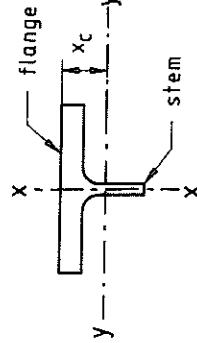
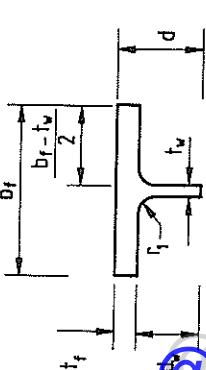
Notes: (1) \* indicates X- and y-axes are interchanged from that shown on the diagram.

(2) For Grade 30 sections the tensile strength ( $t_y$ ) is 440 MPa.

(3)  $Z_{ex}$  Flange — For bending about x-axis which produces compression in the flange.

(4)  $Z_{ey}$  Stem — For bending about y-axis which produces compression at the stem.

(5) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 3.1-6(A)**  
**TEES CUT FROM UNIVERSAL COLUMNS**  
**DIMENSIONS AND PROPERTIES**

Designation kg/m	From Universal Section	Depth of Section d	DIMENSIONS				RATIOS			PROPERTIES													
			Flange Width $b_f$	Flange Thickness $t_f$	Web Thickness $t_w$	Root Radius $r_1$	Depth to Flange $d_w$	$\frac{d_w}{t_w}$	$\frac{(b_f-t_w)}{2t_f}$	Gross Section Area $A_g$			Coordinate of Centroid $X_c$			About x-axis			Torsion Constant $J$				
										$I_y$	$Z_y$	$S_y$	$t_y$	$I_x$	$Z_x$	$S_x$	$t_x$	$10^6 \text{ mm}^4$	$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$	$10^6 \text{ mm}^4$	$10^6 \text{ mm}^3$	$10^3 \text{ mm}^3$
65CT79.0	310UC158	163	311	25.0	15.7	16.5	13.8	8.76	5.91	10100	30.1	15.0	499	113	222	38.6	62.7	403	614	79.0	1900	1900	1900
68.5	137	159	309	21.7	13.8	16.5	13.8	10.0	6.80	8720	28.3	12.6	447	96.5	186	38.1	53.4	346	526	78.2	1250	1250	1250
59.0	118	156	307	18.7	11.9	16.5	13.8	11.6	7.89	7500	26.5	10.5	397	81.2	154	37.5	45.1	294	447	77.6	810	810	810
48.4	96.8	153	305	15.4	9.9	16.5	13.8	13.9	9.58	6180	24.7	8.43	341	65.7	122	36.9	36.4	239	363	76.8	463	463	463
125CT44.8	250UC 89.5	129	256	17.3	10.5	14.0	11.2	10.7	5.91	5690	22.0	5.19	236	48.5	94.3	30.2	24.2	189	287	65.2	521	521	521
36.5	72.9	126	254	14.2	8.6	14.0	11.2	13.0	8.64	4650	20.2	4.07	201	38.5	73.1	29.6	19.4	153	232	64.6	292	292	292
250UC 59.5	104	205	142	9.3	11.4	9.0	9.65	6.89	3800	18.6	2.36	127	53.2	24.9	10.2	99.5	152	51.8	237	237	237	237	
26.1	52.2	102	204	12.5	8.0	11.4	9.0	11.3	7.84	3320	17.4	1.98	114	23.3	44.4	24.4	8.85	86.8	132	51.6	162	162	
23.1	46.2	101	203	11.0	7.3	11.4	9.0	12.4	8.90	2940	16.8	1.75	104	20.8	38.9	24.4	7.67	75.6	115	51.1	113	113	
75CT18.6	150UC 37.2	80	154	11.5	8.1	8.9	6.8	8.44	6.34	2360	15.2	0.909	59.8	14.1	26.9	19.6	3.50	45.5	69.5	38.5	97.9	97.9	
15.0	30.0	78	153	9.4	6.6	8.9	6.8	10.4	7.79	1920	13.9	0.707	50.9	11.1	20.8	19.2	2.81	36.7	55.9	38.2	54.3	54.3	
11.7	23.4	75	152.	6.8	6.1	8.9	6.8	11.3	10.7	1480	14.1	0.588	41.8	9.62	17.3	19.9	1.99	26.2	40.1	36.6	24.9	24.9	
50CT 7.4	100UC 14.8	48	99	7.0	5.0	10.0	4.1	8.10	6.71	938	8.85	0.119	13.5	3.08	6.10	11.3	0.568	11.5	17.6	24.6	17.3	17.3	

Notes: (1) A 1 mm cutting allowance has been provided off each split tee.

(2) The value of the warping constant,  $|w|$ , for Tees is approximately zero.

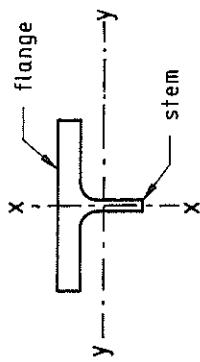


TABLE 3.1-6(B)  
**TEES CUT FROM UNIVERSAL COLUMNS  
GRADE 300**  
**PROPERTIES FOR ASSESSING SECTION CAPACITY**

Designation	Yield Stress			About y-axis			$10^3\text{mm}^3$	$10^3\text{mm}^3$	$10^3\text{mm}^3$
	Flange $f_{yH}$	Web $f_{yw}$	Form Factor $k_f$	Flange		Stem			
				$Z_{ey}$	$Z_{sy}$	$Z_{sx}$			
155CT79.0	280	300	1.00	170	169	169	605		
68.5	280	300	1.00	145	140	140	518		
59.0	280	300	1.00	122	114	114	441		
48.4	300	320	1.00	91.5	85.7	85.7	347		
125CT44.8	280	320	1.00	72.8	69.3	69.3	284		
36.5	300	320	1.00	56.4	51.4	51.4	227		
100CT29.8	300	320	1.00	41.5	40.1	40.1	149		
26.1	300	320	1.00	35.0	32.6	32.6	130		
23.1	300	320	1.00	30.1	28.3	28.3	112		
75CT18.6	300	320	1.00	21.1	21.0	21.0	68.3		
15.0	320	320	1.00	16.6	15.7	15.7	55.1		
11.7	320	320	1.00	12.3	13.3	13.3	36.8		
50CT 7.4	320	320	1.00	4.60	4.60	4.60	17.2		

Notes: (1) For Grade 300 sections the tensile strength ( $f_u$ ) is 440 MPa.  
(2)  $Z_{ey}$  Flange — For bending about y-axis which produces compression in the flange.  
(3)  $Z_{sy}$  Stem — For bending about y-axis which produces compression at the stem.  
(4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



TABLE 3.1-7(A)

### PARALLEL FLANGE CHANNELS DIMENSIONS AND PROPERTIES

Designation	Mass per m	Depth of Section	DIMENSIONS			RATIOS		PROPERTIES										Torsion Constant	Warping Constant	Coordinate of Shear Centre		
			Flange Width		Web Thickness	Root Radius	Depth Between Flanges	$\frac{d_f}{t_w}$	$\frac{(b_f-t_w)}{t_f}$	Gross Section Area		Coordinate of Centroid		About x-axis		About y-axis		J	I <sub>w</sub>	x <sub>o</sub>		
			b <sub>f</sub>	t <sub>f</sub>	t <sub>w</sub>	r	d <sub>r</sub>			A <sub>g</sub>	x <sub>c</sub>	I <sub>x</sub>	S <sub>x</sub>	I <sub>y</sub>	S <sub>y</sub>	Z <sub>R</sub>	Z <sub>L</sub>	10 <sup>9</sup> mm <sup>3</sup>	10 <sup>9</sup> mm <sup>3</sup>	mm		
310 PFC	55.2	380	100	17.5	10.0	14.0	345	34.5	5.14	7030	27.5	152	798	946	147	6.48	89.4	236	161	30.4	472	151
300 PFC	40.1	300	90	16.0	8.0	14.0	268	33.5	5.12	5110	27.2	72.4	483	564	119	4.04	64.4	149	117	28.1	290	58.2
270 PFC	35.5	250	90	15.0	8.0	12.0	220	27.5	5.47	4520	28.6	45.1	361	421	99.9	3.64	59.3	128	107	28.4	238	35.8
230 PFC	25.1	230	75	12.0	6.5	12.0	206	31.7	5.71	3200	22.6	26.8	233	271	91.4	1.76	33.6	77.8	60.9	23.5	103	15.0
200 PFC	22.9	200	75	12.0	6.0	12.0	176	29.3	5.75	2920	24.4	19.1	191	221	80.9	1.66	32.7	67.8	58.9	23.8	101	10.6
180 PFC	20.9	180	75	11.0	6.0	12.0	158	26.3	6.27	2680	24.5	14.1	157	182	72.9	1.51	29.9	61.5	53.8	23.8	81.4	7.81
150 PFC	17.7	150	75	9.5	6.0	10.0	131	21.8	7.26	2250	24.9	8.34	111	129	60.8	1.29	25.7	51.6	46.1	23.9	54.9	51.0

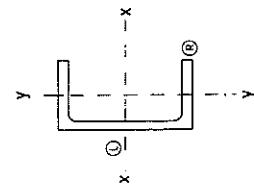


TABLE 3.1-7(B)

### PARALLEL FLANGE CHANNELS GRADE 300

#### PROPERTIES FOR ASSESSING SECTION CAPACITY

Designation	mass per metre	Yield Stress		Form Factor	About x-axis		About y-axis	
		Flange $f_{yf}$	Web $f_{yw}$		$Z_{ex}$	$Z_{ey}$	$Z_{ryl}$	$Z_{lyl}$
380 PFC	55.2	280	320	1.00	946	115	82.3	96.6
300 PFC	40.1	300	320	1.00	564	421	88.7	89.0
250 PFC	35.5	300	320	1.00	271	45.1	50.4	
230 PFC	25.1	300	320	1.00	221	46.7	49.1	
200 PFC	22.9	300	320	1.00	182	44.9	44.9	
180 PFC	20.9	300	320	1.00	129	38.5	38.5	
150 PFC	17.7	320	320	1.00	129			

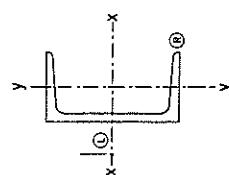
Notes: (1) For Grade 300 sections the tensile strength ( $f_y$ ) is 440 MPa.(2)  $Z_{eyl}$  — For bending about the y-axis that causes compression in the web 'L'.(3)  $Z_{ryl}$  — For bending about the y-axis that causes compression in the toe 'R'.

(4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 3.1-8(A)**  
**TAPER FLANGE CHAMFER DIMENSIONS AND PROCESSES**

Design- nation	Mass per metre	Depth of Section $d$	DIMENSIONS				RATIOS				PROPERTIES													
			Flange Width $b_f$	Web Thickness $t_w$	Flange Thickness $t_f$	Web Thickness $t_w$	Radius $r_1$	Radius $r_2$	Depth Between Flanges $d_1$	Depth Between Flanges $d_2$	Gross Section Area $A_g$	Coordinate of Centroid $x_c$	Coordinate of Centroid $y_c$	Coordinate of Centroid $z_c$	Coordinate of Centroid $z_y$	Coordinate of Centroid $z_y$	Constant $I_x$	Constant $I_y$	Constant $J$	Warping Constant $I_w$	Torsion Constant $J$	Coordinate of Shear Centre $x_0$		
12.5 TFC	13.4	65	8.0	6.0	8.0	4.0	109	18.2	7.37	1710	19.0	4.24	67.8	79.3	49.8	0.618	13.4	32.4	27.4	19.0	35.2	1.74	40.8	
100 TFC	9.34	100	50	7.5	5.0	8.0	4.0	85	17.0	1190	15.4	1.88	37.6	44.3	39.7	0.260	7.52	16.9	15.1	14.8	20.2	0.450	32.1	
75 TFC	6.65	75	40	6.5	5.0	8.0	4.0	62	12.4	538	847	12.4	0.721	19.2	23.0	29.2	0.115	4.15	9.25	8.52	11.6	12.0	0.109	24.8



**TAPER FLANGE CHART**

## PAPER FLANGE CHANNELS GRADE 250

PROPERTIES FOR ASSESSING SECTION CAPACITY

Designation	Mass per metre	Yield Stress		Form Factor $K_f$	About x-axis		About y-axis	
		Flange $f_{yf}$	Web $f_{yw}$		$Z_{sx}$	$10^3\text{mm}^3$	$Z_{syL}$	$Z_{syR}$
	kg/m	MPa	MPa				$10^3\text{mm}^3$	
125 TFC	13.4	260	260	1.00	79.3	20.2	20.2	
100 TFC	9.34	260	260	1.00	44.3	11.3	11.3	
75 TFC	6.65	260	260	1.00	23.0	6.22	6.22	

Notes: (1) For Grade 250 sections the tensile strength ( $f_u$ ) is 410 MPa.  
 (2)  $Z_{ey}$  — For bending about y-axis that causes compression in the web marked 'L'.  
 (3)  $Z_{eyr}$  — For bending about y-axis that causes compression at the toe marked 'R'.

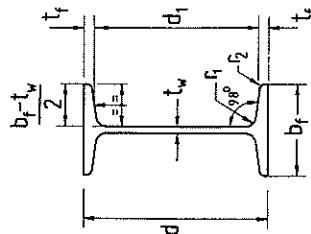


TABLE 3.1-9(A)

**TAPER FLANGE BEAMS  
DIMENSIONS AND PROPERTIES**

Designation	Mass per metre	Depth of Section d	DIMENSIONS						RATIOS						PROPERTIES						
			Flange Width		Web Thickness		Root Radii		Depth Between Flanges d <sub>1</sub>	$\frac{d_1}{t_w}$	Gross Section Area A <sub>g</sub>		About x-axis		About y-axis		Warping Constant J <sub>w</sub>	Torsion Constant J	Warping Constant I <sub>w</sub>		
			b <sub>f</sub>	t <sub>w</sub>	t <sub>w</sub>	t <sub>w</sub>	r <sub>1</sub>	r <sub>2</sub>			Z <sub>x</sub>	S <sub>x</sub>	r <sub>x</sub>	I <sub>y</sub>	Z <sub>y</sub>	S <sub>y</sub>					
125 TFB	13.1	125	65	8.5	5.0	8.0	4.0	108	21.6	3.53	1670	4.34	69.4	80.3	50.9	0.337	10.4	17.2	14.2	40.2	1.14
100 TFB	7.20	100	45	6.0	4.0	7.0	3.0	88	22.0	3.42	917	1.46	29.2	34.1	39.9	0.0795	3.53	6.00	9.31	11.6	0.176

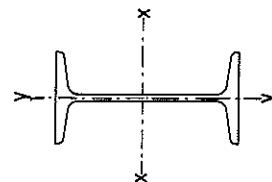
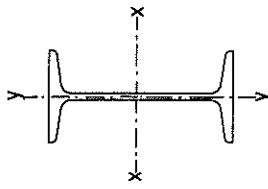


TABLE 3.1-9(B)

**TAPER FLANGE BEAMS  
GRADE 250**

**PROPERTIES FOR ASSESSING SECTION CAPACITY**

Designation	Mass per metre	Yield Stress Flange f <sub>yf</sub>	Yield Stress Web f <sub>yw</sub>	Form Factor k <sub>f</sub>	About x-axis		About y-axis	
					Compactness (C, N, S)	Z <sub>ex</sub>	Compactness (C, N, S)	Z <sub>ey</sub>
125 TFB	13.1	260	260	1.00	C	80.3	C	15.6
100 TFB	7.20	260	260	1.00	C	34.1	C	5.30

Notes: (1) For Grade 250 sections the tensile strength (f<sub>y</sub>) is 410 MPa.  
(2) C: Compact Section; N: Non-compact Section; S: Slender Section.

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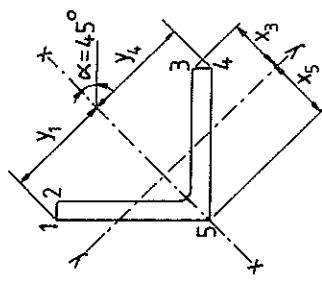
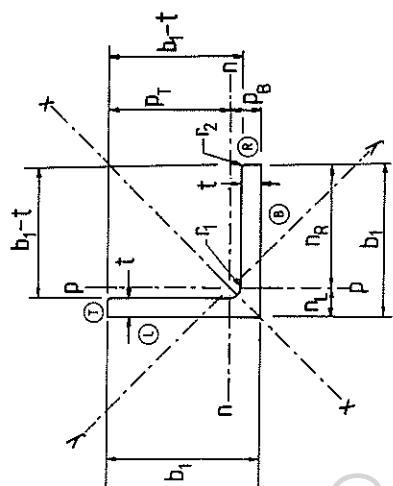


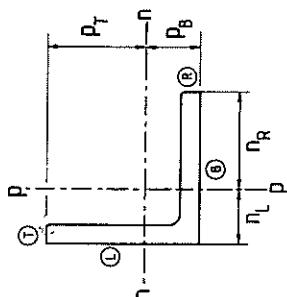
TABLE 3.1-10(A)-1  
**EQUAL ANGLES**  
DIMENSIONS AND PROPERTIES  
principal x- and y-axes



DIMENSIONS AND RATIOS

Designation Nominal Leg Size $b_1 \times b_1$	Thickness mm	Mass per metre kg/m	DIMENSIONS AND RATIOS			PROPERTIES										Torsion constant $J$			
						Coordinate of Centroid			About x-axis			About y-axis							
			Actual Thickness $t$	Root Radius $r_1$	Toe Radius $r_2$	$(b_1-t)$	$A_g$	$\eta_L = \rho_S$	$\eta_R = \rho_T$	$I_x$	$I_y$	$S_x$	$S_y$	$I_{xy}$	$x_3$	$Z_{x3}$	$x_5$	$Z_{x5}$	$S_y$
200 x 200 x 26EA	76.8	76.80	6.69	9.780	59.3	141	56.8	141	402	643	76.2	14.9	73.9	202	83.8	178	329	39.1	2250
200 x 200 x 20EA	60.1	76.60	9.00	57.0	143	45.7	323	141	511	77.2	11.8	72.9	163	80.6	147	260	39.3	1060	
18EA	54.4	69.30	18.0	56.2	144	41.7	141	295	464	77.6	10.8	72.6	149	79.5	136	236	39.5	778	
16EA	48.7	62.00	11.5	55.4	145	37.6	141	266	417	77.9	9.73	72.3	135	78.4	124	212	39.6	554	
13EA	40.0	50.90	14.4	54.2	146	31.2	141	221	344	78.3	8.08	71.9	112	76.6	105	176	39.9	304	
150 x 150 x 19EA	42.1	53.60	6.89	44.2	106	17.6	106	166	265	57.2	4.60	54.9	63.8	62.6	73.5	135	29.3	657	
16EA	35.4	45.20	8.49	43.0	107	15.1	106	142	225	57.8	3.91	54.3	71.9	60.8	64.2	115	29.4	386	
12EA	27.3	34.80	11.5	41.5	108	11.9	106	112	175	58.4	3.06	53.7	57.0	58.7	52.1	89.3	29.6	174	
10EA	21.9	27.90	13.0	40.5	109	9.61	106	90.6	141	58.7	2.48	53.4	46.4	57.3	43.3	72.0	29.8	88.9	
125 x 125 x 16EA	29.1	37.10	10.0	6.91	88.2	8.43	88.4	95.4	153	47.7	2.20	45.4	48.5	52.1	42.3	77.8	24.4	313	
12EA	22.5	28.70	12.0	9.42	85.4	89.6	6.69	88.4	75.7	120	48.3	1.73	44.7	38.6	50.1	34.5	60.8	24.5	141
10EA	18.0	34.4	9.5	10.0	12.2	90.6	5.44	88.4	61.6	96.5	48.7	1.40	44.4	31.5	48.7	28.8	49.0	24.7	71.9
8EA	14.9	19.00	7.8	10.0	15.0	15.0	33.7	91.3	4.55	88.4	51.5	80.2	48.9	1.17	44.2	26.5	47.7	24.6	40.8
																		40.6	

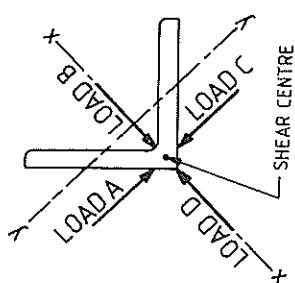
Note: The value of the warping constant,  $\lambda_w$ , for angles is approximately zero.



**TABLE 3.1-10(C)-1**

**EQUAL ANGLES**  
**DIMENSIONS AND PROPERTIES**  
**non-principal n- and p-axes**

Designation	About n- and p-axes						Product 2nd Moment of Area $I_{np}$
	$n_L = l_p$	$n_L = p_s$	$Z_{nL} = Z_{pL}$	$n_R = p_T$	$Z_{nR} = Z_{pR}$	$S_{nL} - S_p$	
	$10^6 \text{mm}^4$	mm	$10^3 \text{mm}^3$	mm	$10^3 \text{mm}^3$	$10^3 \text{mm}^3$	mm
200 x 200 x 26EA	35.8	59.3	605	141	255	460	60.5
20EA	28.8	57.0	505	143	201	363	61.3
18EA	26.3	56.2	467	144	183	330	61.5
16EA	23.7	55.4	427	145	164	296	61.8
13EA	19.7	54.2	363	146	135	243	62.2
150 x 150 x 19EA	11.1	44.2	250	106	105	189	45.4
16EA	9.48	43.0	220	107	88.7	160	45.8
12EA	7.46	41.5	180	108	68.8	124	46.3
10EA	6.04	40.5	149	109	55.2	99.9	46.6
125 x 125 x 16EA	5.32	36.8	144	88.2	60.3	109	37.9
12EA	4.21	35.4	119	89.6	47.0	85.0	38.3
10EA	3.42	34.4	99.4	90.6	37.8	68.4	38.6
8EA	2.86	33.7	84.9	91.3	31.3	56.8	38.8



**PROPERTIES FOR ASSESSING SECTION CAPACITY**

**EQUAL ANGLES  
GRADE 300**

TABLE 3.1-10(B)-1

Designation	Yield Stress $f_y$	Form Factor $k_f$	About x-axis		About y-axis	
			Load A or C $Z_{ex}$	Load B $Z_{ey}$	Load D $Z_{sy}$	Load E $Z_{gy}$
	MPa	$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$
200 x 200 x 26EA	280	1.00	602	267	267	267
20FA	280	1.00	479	218	221	221
18EA	280	1.00	427	197	204	204
16EA	280	1.00	369	172	186	186
13EA	280	1.00	285	136	158	158
150 x 150 x 19EA	280	1.00	248	110	110	110
16EA	300	1.00	212	95.7	96.3	96.3
12EA	300	1.00	155	72.3	78.1	78.1
10EA	320	0.958	114	54.5	65.0	65.0
125 x 125 x 16EA	300	1.00	143	63.4	63.4	63.4
12EA	300	1.00	110	50.3	51.7	51.7
10EA	320	1.00	83.2	38.9	43.1	43.1
8EA	320	0.943	64.3	30.7	36.8	36.8

Notes: (1) For Grade 300 sections the tensile strength( $f_u$ ) is 440 MPa.

[2] The values of  $Z_{\text{ax}}$  &  $Z_{\text{ay}}$  depend on the direction of the bending moment. The appropriate value depends on the direction of the load (A, B, C or D) as shown in the diagram.

[3] Grade 300 refers to BHP Grade 300 PLATE. See note (1) on page 2-2

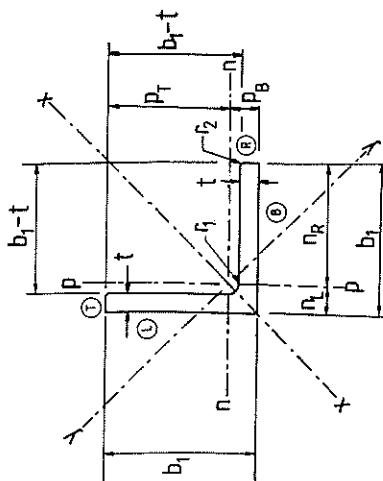


TABLE 3.1-10(A)-2  
EQUAL ANGLES  
DIMENSIONS AND PROPERTIES  
principal x- and y- axes

## DIMENSIONS AND RATIOS

Designation	Nominal Leg Size mm	Mass per metre kg/m	Actual Thickness t mm	Root Radius r <sub>1</sub> mm	Toe Radius r <sub>2</sub> mm	$\frac{(b_1-t)}{t}$	Gross Section Area A <sub>g</sub> mm <sup>2</sup>		Coordinate of Centroid		About x-axis		About y-axis	
							I <sub>x</sub> mm <sup>3</sup>	I <sub>y</sub> mm <sup>3</sup>	Z <sub>x1</sub> = Z <sub>x4</sub> 10 <sup>3</sup> mm <sup>4</sup>	S <sub>x</sub> mm <sup>3</sup>	I <sub>x</sub> mm <sup>3</sup>	I <sub>y</sub> mm <sup>3</sup>	Z <sub>y3</sub> = Z <sub>y4</sub> 10 <sup>3</sup> mm <sup>4</sup>	S <sub>y</sub> mm <sup>3</sup>
100 x 100 x 12EA	17.7	12.0	8.0	5.0	7.33	2260	29.2	70.8	3.29	70.7	46.6	74.5	38.2	0.857
10EA	14.2	9.5	8.0	5.0	9.53	1810	28.2	71.8	2.70	70.7	38.2	60.4	38.6	0.696
8EA	11.8	7.8	8.0	5.0	11.8	1500	27.5	72.5	2.27	70.7	32.0	50.3	38.8	0.582
6EA	9.16	6.0	8.0	5.0	15.7	1170	26.8	73.2	1.78	70.7	35.2	39.3	38.9	0.458
90 x 90 x 10EA	12.7	9.5	8.0	5.0	8.47	1620	25.7	64.3	1.93	63.6	30.4	48.3	34.5	0.501
8EA	10.6	7.8	8.0	5.0	10.5	1350	25.0	65.0	1.63	63.6	25.6	40.4	34.8	0.419
6EA	8.22	6.0	8.0	5.0	14.0	1050	24.3	65.7	1.28	63.6	20.1	31.6	35.0	0.330
75 x 75 x 10EA	10.5	9.5	8.0	5.0	6.89	1340	22.0	53.0	1.08	53.0	20.4	32.8	28.4	0.283
8EA	8.73	7.8	8.0	5.0	8.62	1110	21.3	53.7	0.913	53.0	17.2	27.5	28.7	0.237
6EA	6.81	6.0	8.0	5.0	11.5	867	20.5	54.5	0.722	53.0	13.6	21.6	28.9	0.187
5EA	5.27	4.6	8.0	5.0	15.3	672	19.9	55.1	0.563	53.0	10.6	16.7	29.0	0.147
65 x 65 x 10EA	9.02	9.5	6.0	3.0	5.84	1150	19.6	45.4	0.691	46.0	15.0	24.3	24.5	0.183
8EA	7.51	7.8	6.0	3.0	7.33	957	19.0	46.0	0.589	46.0	12.8	20.5	24.8	0.154
6EA	5.87	6.0	6.0	3.0	9.83	748	18.3	46.7	0.471	46.0	10.2	16.2	25.1	0.122
5EA	4.56	4.6	6.0	3.0	13.1	581	17.7	47.3	0.371	46.0	8.08	12.7	25.3	0.0959
55 x 55 x 6EA	4.93	6.0	6.0	3.0	8.17	628	15.8	39.2	0.277	38.9	7.14	11.4	21.0	0.0723
5EA	3.84	4.6	6.0	3.0	11.0	489	15.2	39.8	0.220	38.9	5.65	8.93	21.2	0.0571
50 x 50 x 8EA	5.68	7.8	6.0	3.0	5.41	723	15.2	34.8	0.253	35.4	7.16	18.7	30.7	0.0575
6EA	4.46	6.0	6.0	3.0	7.33	568	14.5	35.5	0.205	35.4	5.79	9.30	19.0	0.0556
5EA	3.48	4.6	6.0	3.0	9.87	443	13.9	36.1	0.163	35.4	4.60	7.32	19.2	0.0424
3EA	2.31	3.0	6.0	3.0	15.7	295	13.2	36.8	0.110	35.4	3.11	4.90	19.3	0.0289
45 x 45 x 6EA	3.97	6.0	5.0	3.0	6.50	506	13.3	31.7	0.146	31.8	4.59	7.41	17.0	0.0363
5EA	3.10	4.6	5.0	3.0	8.78	394	12.7	32.3	0.117	31.8	3.66	5.84	17.2	0.0303
3EA	2.06	3.0	5.0	3.0	14.0	263	12.0	33.0	0.0790	31.8	2.48	3.92	17.3	0.0206
40 x 40 x 6EA	3.50	6.0	5.0	3.0	5.67	446	12.0	28.0	0.0997	28.3	3.53	5.75	15.0	0.0265
5EA	2.73	4.6	5.0	3.0	7.70	348	11.5	28.5	0.0800	28.3	2.83	4.55	15.2	0.0209
3EA	1.83	3.0	5.0	3.0	12.3	233	10.8	29.2	0.0545	28.3	1.93	3.06	15.3	0.0142
30 x 30 x 6EA	2.56	6.0	5.0	3.0	4.00	326	9.53	20.5	0.0387	21.2	1.83	3.06	10.9	0.0107
5EA	2.01	4.6	5.0	3.0	5.52	256	8.99	21.0	0.0316	21.2	1.49	2.45	11.1	0.00839
3EA	1.35	3.0	5.0	3.0	9.00	173	8.30	21.7	0.0218	21.2	1.03	1.67	11.2	0.00574
25 x 25 x 6EA	2.08	6.0	5.0	3.0	3.17	266	8.28	16.7	0.0210	17.7	1.19	2.03	8.89	0.00600
5EA	1.65	4.6	5.0	3.0	4.43	210	7.75	17.3	0.0173	17.7	0.980	1.65	9.07	0.00469
3EA	1.12	3.0	5.0	3.0	7.33	143	7.07	17.9	0.0121	17.7	0.684	1.13	9.21	0.00319

Note: The value of the warping constant, l<sub>w</sub>, for angles is approximately zero.

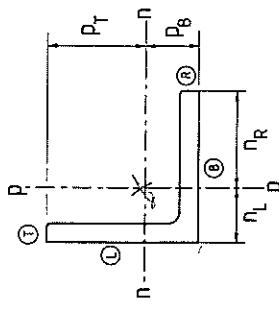


TABLE 3.1-10(C)-2  
EQUAL ANGLES  
DIMENSIONS AND PROPERTIES  
non-principal n- and p-axes

Designation	About n- and p-axes				$I_n = I_p$	$\eta_{nL} = \eta_{pB}$	$Z_{nB} = Z_{pL}$	$Z_{nT} = Z_{pR}$	$S_{nL} = S_{pB}$	$t_n = t_p$	Product 2nd Moment of Area $I_{np}$	
	$I_{10} \text{ mm}^4$	$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$	$10^3 \text{ mm}^3$								
100 x 100 x 12EA	2.08	29.2	71.1	29.3	53.2	30.3	-1.22					
10EA	1.70	28.2	60.1	23.6	42.9	30.6	-1.00					
8EA	1.42	27.5	51.7	19.6	35.7	30.8	-0.842					
6EA	1.12	26.8	41.8	15.3	27.8	31.0	-0.661					
90 x 90 x 10EA	1.22	25.7	47.3	64.3	18.9	34.4	27.4	-0.716				
8EA	1.02	25.0	40.9	65.0	15.7	28.7	27.6	-0.604				
6EA	0.805	24.3	33.2	65.7	12.3	22.4	27.7	-0.475				
90 x 90 x 10EA	0.681	22.0	31.0	53.0	12.8	23.4	22.6	-0.399				
8EA	0.575	21.3	27.0	53.7	10.7	19.5	22.7	-0.338				
6EA	0.455	20.5	22.1	54.5	8.35	15.3	22.9	-0.288				
5EA	0.356	19.9	17.9	55.1	6.44	11.8	23.0	-0.208				
75 x 75 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234	17.7	13.2	47.3	4.94	8.97	20.1	-0.138				
65 x 65 x 10EA	0.437	19.6	22.3	45.4	9.62	17.4	19.5	-0.254				
8EA	0.371	19.0	19.6	46.0	8.07	14.6	19.7	-0.218				
6EA	0.296	18.3	16.2	46.7	6.34	11.5	19.9	-0.175				
5EA	0.234											

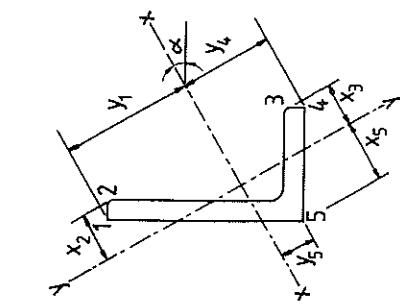
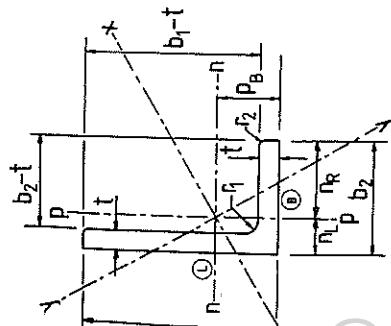


TABLE 3.1-11(A)  
UNEQUAL ANGLES  
DIMENSIONS AND PROPERTIES  
principal x- and y-axes



Designation Nominal Leg Size $b_1 \times b_2$ mm mm	Mass per metre kg/m	DIMENSIONS			RATIOS		PROPERTIES						About x-axes						About y-axes			Tension constant $\sigma$										
		Root Radius $r_1$ mm	Toe Radius $r_2$ mm	$b_1-t$ $b_2-t$ mm	$b_1-t$ $b_2-t$ 1 1	$b_1-t$ $b_2-t$ mm	About x-axes			About y-axes			About x-axes			About y-axes			Tension constant $\sigma$													
							$I_x$ mm <sup>4</sup>	$I_y$ mm <sup>4</sup>	$Z_{x1}$ mm	$y_1$ mm	$Z_{y1}$ mm	$y_5$ mm	$S_x$ mm <sup>3</sup>	$S_y$ mm <sup>3</sup>	$I_y$ mm <sup>4</sup>	$Z_{x2}$ mm	$x_5$ mm	$Z_{y2}$ mm	$x_2$ mm	$I_x$ mm <sup>4</sup>	$Z_{z3}$ mm	$x_5$ mm	$Z_{z5}$ mm	$I_y$ mm <sup>4</sup>	$R_y$ mm	$R_j$ mm	Tan $\alpha$					
150 x 90 x 16UA	27.9	15.8	10.0	5.0	11.5	7.33	2870	49.1	24.3	7.51	102	73.5	75.3	99.7	352	213	127	51.2	1.35	27.6	48.8	52.9	25.5	42.0	32.1	51.7	21.7	141	0.438			
120A	21.6	12.0	10.0	5.0	14.8	9.53	2300	48.1	23.3	6.11	103	59.5	74.9	81.5	346	176	102	51.6	1.09	26.9	40.7	53.0	20.6	40.7	26.9	41.8	21.8	71.9	0.441			
10UA	17.3	9.5	10.0	5.0	14.8	9.5	2200	51.0	21.2	6.97	100	69.4	71.2	97.8	40.8	171	120	50.4	1.04	23.4	44.5	50.1	20.8	37.2	28.0	43.8	19.3	30.0	0.353			
8UA	14.3	7.8	10.0	5.0	18.2	10.5	1820	49.2	19.6	4.73	101	56.1	70.7	80.1	40.1	141	96.6	50.7	0.847	22.6	37.5	50.4	16.8	36.1	23.5	35.4	19.5	19.6	0.359			
125 x 75 x 12UA	17.7	12.0	8.0	5.0	9.42	5.25	2280	43.3	18.4	3.91	83.2	47.0	59.7	65.5	346	113	81.1	81.4	41.6	0.385	19.9	29.4	41.4	31.9	42.0	24.1	56.2	11.0	0.356			
10UA	14.2	9.5	8.0	5.0	12.2	6.89	42.3	17.5	3.20	83.8	38.2	59.3	63.9	33.9	94.4	65.8	42.0	0.476	19.1	24.6	41.6	30.7	15.5	24.1	42.4	11.4	30.7	0.356				
8UA	11.8	7.8	8.0	5.0	15.0	8.62	41.5	16.8	2.68	84.2	31.8	58.9	45.5	31.3	80.3	54.6	42.2	0.400	18.6	21.5	41.8	9.65	29.9	13.3	20.1	16.3	31.7	0.363				
6UA	9.16	6.0	8.0	5.0	19.8	11.5	1170	40.7	16.0	2.10	84.7	24.8	58.5	36.0	32.8	64.1	42.4	42.4	0.315	18.0	17.5	42.1	7.47	29.0	10.9	15.7	16.4	14.8	0.364			
100 x 75 x 10UA	12.4	9.5	8.0	5.0	9.53	6.89	1580	31.8	19.4	1.89	69.2	27.3	54.5	34.6	18.6	101	46.5	34.6	0.402	22.3	18.0	36.4	11.0	32.2	12.5	21.2	16.0	49.1	0.546			
8UA	10.3	7.8	8.0	5.0	11.8	8.62	15.0	11.8	8.62	13.10	31.1	18.7	1.59	69.4	22.9	54.3	28.2	18.2	87.0	38.7	34.8	0.337	21.8	15.4	36.4	9.26	31.3	10.7	17.8	16.1	27.8	0.549
6UA	7.98	6.0	8.0	5.0	15.7	11.5	1020	30.3	17.9	1.25	69.7	17.9	54.0	23.1	17.9	68.9	30.1	35.1	0.286	21.4	12.4	36.5	7.28	30.3	8.76	13.9	16.2	13.0	0.550			
75 x 50 x 8UA	7.23	7.8	7.0	3.0	8.62	5.41	921	25.2	12.8	0.586	50.8	11.5	37.8	15.5	18.0	32.5	20.0	25.2	0.106	14.2	7.47	26.4	4.02	21.7	4.88	8.19	10.7	19.5	0.450			
6UA	5.66	6.0	7.0	3.0	11.5	7.33	721	24.4	12.1	0.468	51.2	9.15	37.5	12.5	17.6	26.7	15.8	25.5	0.0843	13.6	6.18	26.5	3.18	20.8	4.05	6.48	10.8	9.21	0.455			
5UA	4.40	4.6	7.0	3.0	15.3	9.87	560	23.8	11.5	0.370	51.5	7.17	37.2	9.93	17.2	21.5	12.3	25.7	0.0667	13.2	5.05	26.6	2.50	20.1	3.32	5.09	10.9	4.32	0.457			
65 x 50 x 8UA	6.59	7.8	6.0	3.0	7.33	5.41	840	21.1	13.6	0.421	44.9	9.37	36.3	11.6	11.6	36.4	16.1	22.4	0.0936	15.6	6.00	23.9	3.91	22.3	4.20	7.49	10.6	17.6	0.570			
6UA	5.16	6.0	6.0	3.0	9.83	7.33	658	20.4	12.9	0.338	45.2	7.48	36.1	9.35	11.2	30.2	12.7	22.7	0.0744	15.1	4.91	23.9	3.11	21.4	3.48	5.93	10.6	8.29	0.575			
5UA	4.02	4.6	6.0	3.0	13.1	9.87	512	19.8	12.4	0.267	45.4	5.89	35.9	7.43	10.9	24.4	9.92	22.8	0.0587	14.8	3.97	23.9	2.46	20.6	2.85	4.66	10.7	3.87	0.577			

Note: The value of the warping constant,  $I_w$ , for angles is approximately zero.

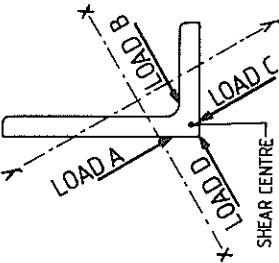


TABLE 3.1-11(B)

**UNEQUAL ANGLES  
GRADE 300 & 250  
PROPERTIES FOR ASSESSING SECTION CAPACITY**

Designation	Yield Stress $f_y$ MPa	Form Factor $k_f$	About x-axis		About y-axis	
			Load A $Z_{ax}$	Load C $Z_{ay}$	Load B $Z_{bx}$	Load D $Z_{by}$
150 x 100 x 12UA 10UA	300 320	1.00 0.975	102 74.8	110 81.7	35.3 26.0	38.2 31.0
150 x 90 x 16UA 12UA 10UA 8UA	300 300 320 320	1.00 1.00 0.973 0.863	132 96.3 70.6 53.0	133 104 81.8 60.3	39.5 28.8 21.2 15.9	39.8 31.2 25.2 21.0
125 x 75 x 12UA 10UA 8UA 6UA	260 260 260 260	1.00 1.00 0.872	69.7 53.2 28.5	70.5 57.2 32.4	20.9 15.9 8.59	21.2 17.2 11.2
100 x 75 x 10UA 8UA 6UA	260 260 260 260	1.00 1.00 0.872	40.3 32.1 23.0	40.9 34.3 23.4	16.3 13.0 9.33	16.6 13.9 10.9
75 x 50 x 8UA 6UA 5UA	260 260 260	1.00 1.00 1.00	17.3 12.9 9.27	17.3 13.7 10.2	6.02 4.51 3.24	6.02 4.78 3.76
65 x 50 x 8UA 6UA 5UA	260 260 260	1.00 1.00 1.00	14.0 11.0 8.02	14.0 11.2 8.38	5.87 4.57 3.35	5.87 4.67 3.69

Notes: (1) For 150 x 90 angles and above: Grade 300.

(2) For 125 x 75 angles and below: Grade 250.

(3) For Grade 250 sections the tensile strength ( $f_y$ ) is 410 MPa.

(4) For Grade 300 sections the tensile strength ( $f_y$ ) is 440 MPa.

(5) The values of  $Z_{ax}$  and  $Z_{ay}$  depend on the direction of the bending moment. The appropriate value depends on the direction of the load (A, B, C or D) as shown in the diagram.

(6) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

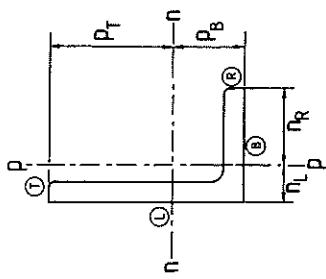


TABLE 3.1-11(C)  
UNEQUAL ANGLES  
DIMENSIONS AND PROPERTIES  
Non-principal  $n$ - and  $p$ -axes

Designation	About $n$ -axis						About $p$ -axis							
	$I_n$ $10^6 \text{mm}^4$	$P_n$ mm	$Z_{nB}$ $10^3 \text{mm}^3$	$P_T$ mm	$Z_{nT}$ $10^3 \text{mm}^3$	$S_n$ mm	$r_n$ mm	$I_p$ $10^6 \text{mm}^4$	$n_L$ mm	$Z_{pL}$ $10^3 \text{mm}^3$	$n_R$ mm	$Z_{pR}$ $10^3 \text{mm}^3$	$S_p$ mm	$r_p$ mm
150 x 100 x 120A 100A	6.52 5.29	49.1 48.1	133 110	101 102	64.6 51.9	117 94.0	47.7 48.0	2.34 1.91	24.3 23.3	96.2 81.9	75.7 76.7	30.9 24.9	56.0 44.7	28.6 26.8
150 x 90 x 160A 120A 100A 80A	7.97 6.29 5.10 4.26	52.5 152 102 49.2	97.5 99.0 100 86.6	81.7 63.5 101 42.3	145 114 51.0 76.0	47.4 47.8 48.2 48.4	2.15 1.72 1.41 1.18	22.7 21.2 20.2 19.6	94.9 81.0 69.5 60.4	67.3 68.8 69.8 70.4	32.0 25.0 20.2 16.8	59.6 45.8 69.8 70.4	24.6 25.0 25.3 30.1	-2.27 -1.85 -1.89 -1.54
125 x 75 x 120A 100A 80A 60A	3.54 2.88 2.41 1.89	43.3 42.3 41.5 40.7	81.8 68.2 83.5 84.3	81.7 34.9 28.9 22.5	43.3 62.5 52.0 40.6	77.3 39.9 40.1 40.3	39.6 0.789 0.664 0.524	0.958 17.5 16.8 16.0	18.4 45.2 39.6 32.7	52.0 57.5 58.2 59.0	56.6 13.7 11.4 8.89	16.9 13.7 11.4 16.0	31.4 25.1 20.7 16.0	-1.05 -0.867 -0.730 -0.575
100 x 75 x 100A 80A 60A	1.55 1.30 1.02	31.8 31.1 30.3	48.6 41.8 33.7	68.2 66.9 69.7	22.6 34.5 14.6	41.3 31.3 26.9	31.3 31.5 31.7	0.743 0.626 0.494	19.4 18.7 17.9	38.3 33.5 27.5	55.6 56.3 57.1	13.4 11.1 8.67	24.3 20.2 15.7	-0.625 -0.527 -0.416
75 x 50 x 80A 60A 50A	0.511 0.407 0.321	25.2 24.4 23.8	20.3 16.7 13.5	49.8 50.6 51.2	10.3 8.05 6.27	18.5 14.6 11.4	23.6 23.8 23.9	0.181 0.145 0.115	12.8 12.1 11.5	14.1 12.0 10.0	37.2 37.9 38.5	8.96 8.84 3.00	14.0 14.2 5.41	-0.174 -0.141 -0.111
65 x 50 x 80A 60A 50A	0.341 0.272 0.215	21.1 20.4 19.8	16.2 13.4 10.9	43.9 44.6 45.2	7.75 11.1 8.71	14.1 10.8 8.71	20.1 0.140 0.111	0.174 12.9 12.4	13.6 10.8 8.96	36.4 37.1 37.6	4.78 3.77 2.95	8.74 6.85 5.32	14.4 14.6 14.7	-0.141 -0.114 -0.0903

TABLE 3.1-12  
**ROUND BARS**  
**DIMENSIONS AND PROPERTIES**

Diameter mm	Mass kg/m	$A_g$ mm <sup>2</sup>	Circumference mm	$I$ 10 <sup>3</sup> mm <sup>4</sup>	$Z$ 10 <sup>3</sup> mm <sup>3</sup>	$Z_e$ 10 <sup>3</sup> mm <sup>3</sup>	$S$ 10 <sup>3</sup> mm <sup>3</sup>	$r$ mm	Diameter mm	Mass kg/m	$A_g$ mm <sup>2</sup>	Circumference mm	$I$ 10 <sup>3</sup> mm <sup>4</sup>	$Z$ 10 <sup>3</sup> mm <sup>3</sup>	$Z_e$ 10 <sup>3</sup> mm <sup>3</sup>	$S$ 10 <sup>3</sup> mm <sup>3</sup>	$r$ mm
10	0.616	78.5	31.4	0.000491	0.0982	0.147	0.167	2.50	50	15.4	1960	157	0.307	12.3	18.4	20.8	12.5
12	0.887	113	37.7	0.00102	0.170	0.254	0.288	3.00	56	19.3	2460	176	0.483	17.2	25.9	29.3	14.0
14	1.21	154	44.0	0.00189	0.269	0.404	0.457	3.50	60	22.2	2830	188	0.636	21.2	31.8	36.0	15.0
16	1.58	201	50.3	0.00322	0.402	0.603	0.683	4.00	63	24.5	3120	198	0.773	24.5	36.8	41.7	15.8
18	2.00	254	56.5	0.00515	0.573	0.859	0.972	4.50	65	26.0	3320	204	0.876	27.0	40.4	45.8	16.2
20	2.46	314	62.8	0.00785	0.785	1.18	1.33	5.00	70	30.2	3850	220	1.18	33.7	50.5	57.2	17.5
22	2.98	380	69.1	0.0115	1.05	1.57	1.77	5.50	75	34.7	4420	236	1.55	41.4	62.1	70.3	18.8
24	3.55	452	75.4	0.0163	1.36	2.04	2.30	6.00	80	39.5	5030	251	2.01	50.3	75.4	85.3	20.0
26	4.17	531	81.7	0.0224	1.73	2.59	2.93	6.50	90	49.9	6360	283	3.22	71.6	107	122	22.5
27	4.49	573	84.8	0.0261	1.93	2.90	3.28	6.75	100	61.7	7850	314	4.91	98.2	147	167	25.0
30	5.55	707	94.2	0.0398	2.65	3.98	4.50	7.50	110	74.6	9500	346	7.19	131	196	222	27.5
32	6.31	804	101	0.0515	3.22	4.83	5.46	8.00	120	88.8	11300	377	10.2	170	254	288	30.0
33	6.71	855	104	0.0582	3.53	5.29	5.99	8.25	130	104	13300	408	14.0	216	324	366	32.5
35	7.55	962	110	0.0737	4.21	6.31	7.15	8.75	140	121	15400	440	18.9	269	404	457	35.0
36	7.99	1020	113	0.0824	4.58	6.87	7.78	9.00	150	139	17700	471	24.9	331	497	562	37.5
38	8.90	1130	119	0.102	5.39	8.08	9.15	9.50	160	158	20100	503	32.2	402	603	683	40.0
39	9.38	1190	123	0.114	5.82	8.74	9.89	9.75	170	178	22700	534	41.0	482	723	819	42.5
42	10.9	1390	132	0.153	7.27	10.9	12.3	10.5	180	200	25400	565	51.5	573	859	972	45.0
45	12.5	1590	141	0.201	8.95	13.4	15.2	11.2	190	223	28400	597	64.0	673	1010	1140	47.5
48	14.2	1810	151	0.261	10.9	16.3	18.4	12.0	200	247	31400	628	78.5	785	1180	1330	50.0
									215	285	36300	675	105	976	1460	1660	53.8

Note: Not all the listed sizes are available in some grades and finishes. Check manufacturers' catalogues before specifying.

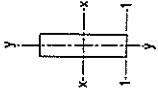
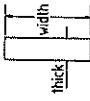
TABLE 3.1-13  
**SQUARE BARS**  
**DIMENSIONS AND PROPERTIES**

Width mm	Mass kg/m	$A_g$ $\text{mm}^2$	1 $10^4 \text{mm}^4$	Z $10^3 \text{mm}^3$	$Z_c$ $10^3 \text{mm}^3$	S $10^3 \text{mm}^3$	r mm
10	0.790	100	0.000833	0.167	0.250	0.250	2.89
12	1.13	144	0.00173	0.288	0.432	0.432	3.46
14	1.54	196	0.00320	0.457	0.686	0.686	4.04
16	2.01	256	0.00546	0.683	1.02	1.02	4.62
18	2.54	324	0.00875	0.972	1.46	1.46	5.20
20	3.14	400	0.0133	1.33	2.00	2.00	5.77
25	4.91	625	0.0326	2.60	3.91	3.91	7.22
28	6.15	784	0.0512	3.66	5.49	5.49	8.08
32	8.04	1020	0.0874	5.46	8.19	8.19	9.24
35	9.62	1220	0.125	7.15	10.7	10.7	10.1
40	12.5	1600	0.213	10.7	16.0	16.0	11.5

Notes: (1) Not all the listed sizes are available in some grades and finishes. Check manufacturers' catalogues before specifying.  
(2) Value of section properties are about principal axes.

TABLE 3.1-14

## SQUARE EDGE FLAT BARS DIMENSIONS AND PROPERTIES



Width x Thickness	Mass per Metre	Cross-Section Area	Second Moment of Area About x-axis	Second Moment of Area About t-axis	Width x Thickness	Mass per Metre	Cross-Section Area	Second Moment of Area About x-axis	Second Moment of Area About t-axis	Width x Thickness	Mass per Metre	Cross-Section Area	Second Moment of Area About x-axis	Second Moment of Area About t-axis			
mm	mm	mm <sup>2</sup>	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>6</sup> mm <sup>4</sup>	mm	mm	kg/m	mm <sup>2</sup>	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>6</sup> mm <sup>4</sup>	mm	mm	kg/m	mm <sup>2</sup>	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>6</sup> mm <sup>4</sup>	
16 x 5	0.628	80.0	0.001171	0.00583	65 x 3	1.53	195	0.0687	0.275	0.000146	150 x 5	5.89	750	1.41	5.62	0.00156	
16 x 6	0.754	96.0	0.00205	0.00819	65 x 5	2.55	325	0.114	0.458	0.000677	150 x 6	7.06	900	1.69	6.75	0.00270	
16 x 8	1.00	128	0.00273	0.0109	65 x 6	3.06	390	0.137	0.549	0.00117	150 x 8	9.42	1200	2.25	9.00	0.00640	
16 x 10	1.26	160	0.00341	0.0137	65 x 8	4.08	520	0.183	0.732	0.00277	150 x 10	11.8	1500	2.81	11.2	0.0125	
20 x 3	0.471	60.0	0.00200	0.00800	65 x 10	5.10	650	0.229	0.915	0.00542	150 x 12	14.1	1800	3.38	13.5	0.0216	
20 x 5	0.785	100	0.00383	0.0133	65 x 12	6.12	780	0.275	1.10	0.00936	150 x 16	18.6	2400	4.50	18.0	0.0512	
20 x 6	1.042	120	0.00400	0.0160	65 x 16	8.16	1040	0.366	1.46	0.0222	150 x 20	23.5	3000	5.62	22.5	0.10	
20 x 10	1.57	200	0.00667	0.0267	65 x 25	12.8	1620	0.572	2.29	0.0846	150 x 25	29.4	3750	7.03	28.1	0.195	
22 x 6	1.04	132	0.00532	0.0213	0.000396	70 x 5	2.75	350	0.143	0.572	0.000729	150 x 32	37.7	4800	9.00	36.0	0.410
25 x 3	0.589	75.0	0.00391	0.0156	0.000056	75 x 5	2.94	375	0.176	0.703	0.000781	150 x 40	47.1	6000	11.2	45.0	0.800
25 x 5	0.981	125	0.00651	0.0260	0.000260	75 x 8	3.53	450	0.211	0.844	0.00135	150 x 50	58.9	7500	14.1	56.3	1.56
25 x 6	1.18	150	0.00781	0.0312	0.000450	75 x 10	4.71	600	0.281	1.12	0.00320	160 x 5	7.06	900	2.43	6.83	0.00167
25 x 8	1.57	200	0.0104	0.0417	0.00107	75 x 12	7.06	900	0.422	1.69	0.0108	180 x 6	8.48	1080	2.92	11.7	0.0324
25 x 10	1.96	250	0.0130	0.0521	0.00208	75 x 16	9.42	1200	0.562	2.25	0.0256	180 x 10	14.1	1800	4.86	19.4	0.0150
25 x 12	2.36	300	0.0156	0.0625	0.00360	75 x 20	11.8	1500	0.703	2.81	0.0500	180 x 12	17.0	2160	5.83	23.3	0.0259
32 x 3	0.754	96.0	0.00819	0.0328	0.000072	75 x 25	14.7	1880	0.879	3.52	0.0977	180 x 20	28.3	3600	9.72	38.9	0.120
32 x 5	1.26	160	0.0137	0.0546	0.000333	75 x 40	23.6	3000	1.41	5.62	0.400	180 x 25	35.3	4500	12.2	48.6	0.234
32 x 6	1.51	192	0.0164	0.0655	0.000576	90 x 6	4.24	540	0.364	1.46	0.00162	190 x 5	7.46	950	2.86	11.4	0.00198
32 x 8	2.01	256	0.0218	0.0874	0.00137	90 x 8	5.65	720	0.486	1.94	0.00384	200 x 5	7.85	1000	3.33	13.3	0.00208
32 x 10	2.51	320	0.0273	0.109	0.00267	90 x 10	7.06	900	0.608	2.43	0.00750	200 x 6	9.42	1200	4.00	16.0	0.00360
32 x 12	3.01	384	0.0328	0.131	0.00461	90 x 12	8.48	1080	0.729	2.92	0.0130	200 x 10	15.7	2000	6.67	26.7	0.0167
40 x 3	0.942	120	0.0160	0.0640	0.000090	90 x 16	11.3	1440	0.972	3.89	0.0307	200 x 12	18.8	2400	8.00	32.0	0.0288
40 x 5	1.57	200	0.0267	0.1107	0.000417	90 x 20	14.1	1800	1.22	4.86	0.0500	200 x 16	25.1	3200	10.7	42.7	0.0683
40 x 6	1.88	240	0.0320	0.128	0.000720	100 x 5	3.92	500	0.417	1.67	0.00104	200 x 20	31.4	4000	13.3	53.3	0.133
40 x 8	2.51	320	0.0427	0.171	0.00171	100 x 6	4.71	600	0.500	2.00	0.00180	200 x 25	39.2	5000	16.7	66.7	0.260
40 x 10	3.14	400	0.0533	0.213	0.00333	100 x 8	6.28	800	0.667	2.67	0.0427	250 x 5	9.81	1250	6.51	26.0	0.00260
40 x 12	3.77	480	0.0640	0.256	0.00576	100 x 10	7.85	1000	0.833	3.38	0.0833	250 x 6	11.8	1500	7.81	31.2	0.00450
40 x 16	5.02	640	0.0853	0.341	0.0137	100 x 12	9.42	1200	1.00	4.00	0.0144	250 x 10	19.6	2500	13.0	52.1	0.0208
40 x 20	6.28	800	0.107	0.427	0.0267	100 x 16	12.6	1600	1.33	5.33	0.0341	250 x 12	23.5	3000	15.6	62.5	0.0360
45 x 5	1.77	225	0.0380	0.152	0.000469	100 x 25	19.6	2500	2.08	8.33	0.130	250 x 16	31.4	4000	20.8	83.3	0.0853
45 x 8	2.12	270	0.0456	0.182	0.000810	100 x 50	39.2	5000	4.17	16.70	1.04	250 x 20	39.2	5000	26.0	104	0.167
45 x 10	2.83	360	0.0608	0.243	0.00192	110 x 6	5.18	660	0.666	2.22	0.0115	250 x 25	49.1	6250	32.6	130	0.326
45 x 12	3.53	450	0.0759	0.304	0.00375	110 x 5	4.32	550	0.555	2.22	0.00198	300 x 8	9.81	1250	6.51	26.0	0.00540
50 x 3	1.18	150	0.0312	0.125	0.000112	110 x 6	5.18	660	0.666	2.22	0.00198	300 x 10	18.8	2400	18.0	72.0	0.0128
50 x 5	1.96	250	0.0521	0.208	0.000521	110 x 12	8.64	880	0.887	3.55	0.00469	300 x 12	23.5	3000	22.5	90.0	0.0250
50 x 6	2.36	300	0.0625	0.250	0.000900	110 x 16	13.8	1760	1.77	7.10	0.0375	300 x 12	28.3	3600	27.0	106	0.0432
50 x 8	3.14	400	0.0833	0.333	0.00213	130 x 5	5.1	650	0.915	3.66	0.0135						
50 x 10	3.92	500	0.104	0.417	0.00417	130 x 6	6.12	780	1.10	4.39	0.00234						
50 x 12	4.71	600	0.125	0.500	0.00720	130 x 8	8.16	1040	1.46	5.86	0.00555						
50 x 16	6.28	800	0.167	0.667	0.0171	130 x 10	9.42	1300	1.83	7.32	0.0108						
50 x 20	7.85	1000	0.208	0.833	0.0333	130 x 12	10.2	1560	2.20	8.79	0.0187						
50 x 25	9.81	1250	0.260	1.04	0.0651	130 x 16	12.6	2080	3.14	11.70	0.0444						
55 x 5	2.16	275	0.0693	0.277	0.000573	130 x 20	20.4	2600	3.66	14.60	0.0867						
55 x 6	2.59	330	0.0832	0.353	0.000990	130 x 25	25.5	3250	4.58	19.30	0.169						
55 x 10	4.32	550	0.139	0.555	0.00458	130 x 40	40.8	5200	7.32	29.30	0.693						

Only a limited range of the sizes listed is available as square edge flat bars — check manufacturer's catalogues for availability. Other sizes may be cut from plate.

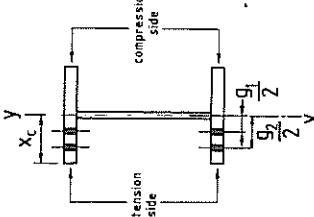
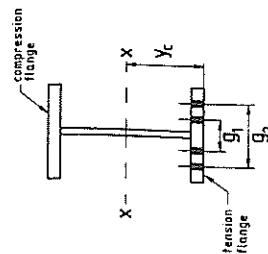


TABLE 3.1-15(1)  
**WELDED BEAMS**  
**GRADE 300**  
**SECTION PROPERTIES**  
two/four holes on tension flange



Designation	Holes Deducted			About x-axis			About y-axis							
	Gauges	$g_1$	$g_2$	Diameter	$A_c$	$y_c$	$Z_t$ (tens)	$Z_x$	$S_x$	$x_c$	$Z_t$ (comp)	$Z_y$ (tens)	$Z_{xy}$	$S_y$
	mm	mm	mm	mm <sup>2</sup>	mm	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	10 <sup>3</sup> mm <sup>3</sup>				
1200WB455	140	—	26	55800	600	25600	25600	28200	253	3330	3260	4890	4890	4930
455*	140	280	26	53800	600	25600	25600	28200	258	3220	3020	4550	4550	4630
423	140	—	26	52000	596	23300	23300	25800	253	2990	2930	4400	4400	4440
423*	140	280	26	50200	596	23800	23300	25800	258	2900	2720	4080	4080	4180
392	140	—	26	48300	592	21100	21100	23400	252	2660	2610	3910	3910	3950
392*	140	280	26	46600	592	21100	21100	23400	258	2570	2420	3630	3630	3720
342	140	—	26	41900	592	17500	17500	19800	203	1690	1640	2460	2460	2510
342*	140	280	26	40200	640	16900	14300	17700	209	1560	1430	2140	2140	2280
317	140	—	26	38900	588	15700	15700	17900	203	1480	1440	2160	2160	2210
317*	140	280	26	37400	633	15100	13000	16100	208	1360	1250	1880	1880	2000
278	140	—	26	34100	585	13000	13000	15000	178	1000	970	1450	1450	1510
249	140	—	26	30400	585	10900	10900	12900	140	597	572	858	858	926
1000WB322	140	—	26	39300	512	14600	14600	16400	203	1690	1640	2460	2460	2500
322*	140	280	26	37600	556	14100	11900	14600	209	1560	1420	2130	2130	2270
296	140	—	26	36300	508	13100	13100	14800	203	1480	1440	2160	2160	2200
296*	140	280	26	34800	549	12600	10700	13200	209	1360	1250	1870	1870	1990
258	140	—	26	31600	505	10700	10700	12300	178	1000	968	1450	1450	1500
215	140	—	26	26300	500	8120	6580	7500	153	577	556	834	834	888
900WB282	140	—	26	34300	462	12400	12400	13600	203	1690	1640	2450	2450	2470
282*	140	280	26	32600	508	12000	9850	11900	211	1570	1410	2110	2110	2240
257	140	—	26	31300	458	11000	11000	12200	203	1480	1430	2150	2150	2170
257*	140	280	26	29800	501	10700	8820	10700	210	1370	1240	1850	1850	1960
218	140	—	26	26500	455	8930	8930	9960	178	1000	964	1450	1450	1500
175	140	—	26	21300	450	6580	6580	7500	153	578	552	828	828	858
800WB192	140	—	26	22900	408	7290	7290	8060	154	813	767	1150	1150	1180
168	140	—	26	20100	405	6140	6140	6840	142	601	562	843	843	873
146	140	—	26	17600	423	4970	4420	5270	142	479	451	677	677	702
122	140	—	26	14800	418	3840	3440	4180	129	309	290	433	433	461
700WB173	140	—	26	20500	358	5760	5760	6390	142	674	627	941	941	973
150	140	—	26	17800	355	4810	4810	5370	130	486	448	672	672	706
130	140	—	26	15600	373	3870	3400	4110	130	388	360	540	540	566
115	140	—	26	13800	366	3230	2870	3490	129	309	289	431	431	456

Notes: (1) Gauges and hole diameters are those recommended in "Standardised Structural Connections".  
(2) \* indicates four holes on flange.

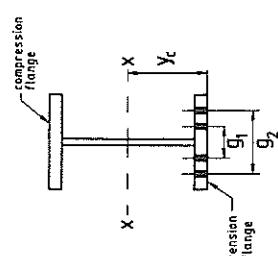


TABLE 3.1-15(2)  
**WELDED BEAMS**  
**GRADE 400**  
**SECTION PROPERTIES**  
two/four holes on tension flange

Designation	Holes Deducted		A <sub>in</sub>	mm	mm <sup>2</sup>	About x-axis			About y-axis			
	Gauges	g <sub>1</sub>	g <sub>2</sub>			Diameter	mm	10 <sup>3</sup> mm <sup>3</sup>	Z <sub>x</sub>	10 <sup>3</sup> mm <sup>3</sup>	Z <sub>y</sub> (tens)	S <sub>y</sub>
1200WB455	140	—	26	55800	600	25600	25600	28100	28200	253	3330	4890
455*	140	280	26	53800	645	24900	21400	25300	25500	258	3220	4530
423	140	—	26	52000	596	23300	23300	25700	25800	253	2990	4390
423*	140	280	26	50200	639	22700	19700	23200	23400	258	2900	4070
392	140	—	26	48300	592	21100	21100	23300	23400	252	2660	2610
392*	140	280	26	46600	633	20500	17900	21100	21400	258	2570	2420
342	140	—	26	41900	615	17200	15900	18600	18800	203	1690	1640
342*	140	280	26	40200	640	16800	14300	17500	17700	209	1560	1430
317	140	—	26	38900	610	15500	14400	16800	17000	203	1480	1440
317*	140	280	26	37400	633	15100	13000	15900	16100	208	1360	1250
278	140	—	26	34100	607	12700	11800	14100	14300	178	1000	970
249	140	—	26	30400	610	10500	9740	12000	12100	140	597	572
1000WB322	140	—	26	39300	533	14400	13200	15500	15500	203	1690	1640
322*	140	280	26	37600	556	14100	11900	14600	14600	209	1560	1420
296	140	—	26	36300	528	12900	11900	14000	14000	203	1480	1440
296*	140	280	26	34800	549	12600	10700	13200	13200	209	1360	1250
258	140	—	26	31600	525	10500	9700	11600	11600	178	1000	968
215	140	—	26	26300	519	7910	7320	9040	9040	153	577	556
900WB282	140	—	26	34300	484	12200	11100	12600	12800	203	1690	1640
282*	140	280	26	32600	508	12000	9850	11700	11900	211	1570	1420
257	140	—	26	31300	479	10900	9300	11300	11500	203	1480	1430
257*	140	280	26	29800	501	10700	8820	10500	10700	210	1370	1240
218	140	—	26	26500	477	8760	7960	9180	9350	178	1000	964
175	140	—	26	21300	472	6410	5830	6790	7020	153	578	552
800WB192	140	—	26	22900	433	7140	6320	7120	7440	154	813	767
168	140	—	26	20100	430	5980	5280	6010	6290	142	601	562
146	140	—	26	17600	428	4970	4420	4990	5300	142	479	451
122	140	—	26	14800	418	3840	3440	3940	4210	129	309	290
700WB173	140	—	26	20500	382	5630	4910	5830	5830	142	674	627
150	140	—	26	17800	380	4680	4060	4880	4880	130	486	448
130	140	—	26	15600	373	3870	3400	4110	4110	130	388	360
115	140	—	26	13800	366	3230	2870	3490	3490	129	309	289

Notes: (1) Gauges and hole diameters are those recommended in "Standardised Structural Connections".  
(2) \* indicates four holes on flange.

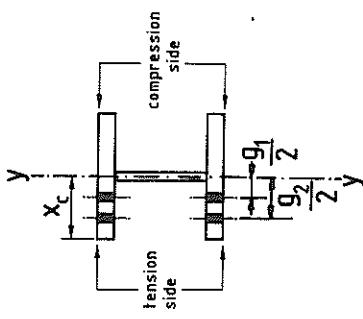
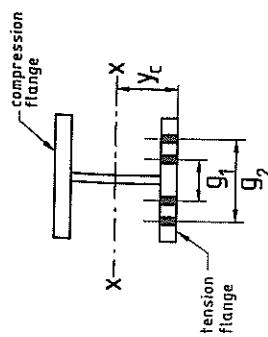


TABLE 3.1-16(1)  
**WELDED COLUMNS  
GRADE 300**  
**SECTION PROPERTIES**  
**two/four holes on tension flange**



Designation	Holes Deducted		Diameter mm	$A_n$ mm <sup>2</sup>	About x-axis			About y-axis				
	$g_1$ mm	$g_2$ mm			$y_c$ mm	$Z_x$ (comp) $10^3\text{mm}^3$	$Z_x$ (tens) $10^3\text{mm}^3$	$S_x$ $10^3\text{mm}^3$	$x_c$ mm	$Z_y$ (comp) $10^3\text{mm}^3$	$Z_y$ (tens) $10^3\text{mm}^3$	$S_y$ $10^3\text{mm}^3$
500WC440	140	—	26	53900	240	8980	8980	10400	10400	253	3340	3260
440*	140	280	26	51800	240	8980	8980	10400	10400	253	3230	3020
414	140	—	26	50700	240	8800	8800	10100	10100	253	3230	3260
414*	140	280	26	48680	240	8800	8800	10100	10100	253	3010	4950
383	140	—	26	46900	286	7990	7990	9130	9130	253	3000	4660
383*	140	280	26	45100	286	7990	7990	9130	9130	253	2930	4400
340	140	—	26	41600	257	7980	7980	8980	8980	253	2910	4470
340*	140	280	26	39900	257	7980	7980	8980	8980	253	2610	4200
290	140	—	26	35500	253	6980	6980	6930	6930	253	2580	3950
290*	140	280	26	34100	253	6930	6930	7570	7570	253	2330	3720
267	140	—	26	32700	250	6250	6250	6700	6700	253	2260	3440
267*	140	280	26	31400	250	6250	6250	6950	6950	253	2100	3240
228	140	—	26	28800	245	5130	5130	5210	5210	253	2080	3080
228*	140	280	26	26900	263	5000	5000	4310	4310	253	1880	2890
400WC361	140	—	26	43900	215	6340	6340	7460	7460	253	1660	2140
361*	140	280	26	41880	234	6080	5070	6550	6550	210	2120	2470
328	140	—	26	39700	215	6140	6140	7100	7100	204	1970	3190
328*	140	280	26	37600	237	5920	5920	4840	6130	212	2120	2890
303	140	—	26	36700	211	5570	5570	6420	6420	204	1970	3120
303*	140	280	26	34900	232	5370	5370	4410	5570	211	1910	2820
270	140	—	26	32700	207	4950	4950	5660	5660	204	1770	2820
270*	140	280	26	31000	227	4780	3920	4910	4910	211	1700	2550
212	140	—	26	25700	200	3880	3880	4360	4360	204	1320	2450
212*	140	280	26	24400	220	3750	3750	3790	3790	211	1230	2260
181	140	—	26	22000	195	3180	3180	3410	3410	203	1060	1940
181*	140	280	26	20800	213	3060	2540	2890	3130	210	980	1760
144	140	—	26	17600	191	2550	2550	2590	2590	203	882	1450
144*	140	280	26	16700	209	2460	2460	2100	2480	210	819	1560
350WC280	140	—	26	33600	178	4210	4210	4940	4940	179	1610	1410
258	140	—	26	31000	174	3810	3810	4450	4450	179	1450	1250
230	140	—	26	27600	170	3380	3380	3910	3910	179	1290	1080
197	140	—	26	23600	166	2940	2940	3350	3350	179	1130	1640

Notes: (1) Gauges and hole diameters are those recommended in "Standardised Structural Connections".  
(2) \* indicates four holes on flange.

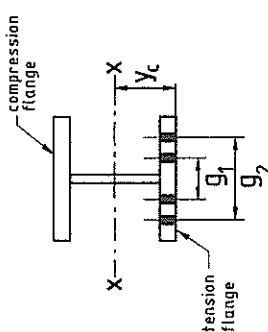


TABLE 3.1-16(2)  
**WELDED COLUMNS  
GRADE 400**  
**SECTION PROPERTIES**  
**two/four holes on tension flange**

Designation	Holes Dedicated			About x-axis						About y-axis					
	g <sub>1</sub>	g <sub>2</sub>	Diameter	A <sub>n</sub>	y <sub>c</sub>	Z <sub>x</sub> (comp)	Z <sub>x</sub> (tens)	S <sub>x</sub>	10 <sup>3</sup> mm <sup>3</sup>	S <sub>y</sub>					
500WC440	140	—	26	53900	240	8980	8980	10400	10400	253	3330	3260	4900	5010	5010
440*	140	280	26	51800	258	8710	7520	9380	9380	258	3230	3230	4530	4710	4710
414	140	—	26	50700	240	8800	8800	10100	10100	263	3330	3260	4890	4950	4950
414*	140	280	26	48600	259	8560	7310	9030	9030	259	3230	3230	4510	4660	4660
383	140	—	26	46900	236	7990	7990	9130	9130	253	3000	2930	4400	4470	4470
383*	140	280	26	45100	254	7770	6660	8200	8200	259	2910	2710	4070	4200	4200
340	140	—	26	41600	257	7980	7980	6830	6830	253	2660	2610	3820	3950	3950
340*	140	280	26	39900	277	7770	6650	7850	7850	259	2580	2580	2410	3530	3720
290	140	—	26	35500	253	6930	6930	7410	7700	253	2330	2280	3230	3440	3440
290*	140	280	26	34100	273	6760	5750	6460	6460	259	2260	2100	2990	3240	3240
267	140	—	26	32700	250	6250	6250	6540	6540	253	2080	2030	2800	3080	3080
267*	140	280	26	31400	270	6100	5210	6250	6250	259	2020	1880	2590	2890	2890
228	140	—	26	28000	254	5070	4720	4470	4470	253	1660	1630	2050	2470	2470
228*	140	280	26	26900	263	5000	4310	4070	4070	253	1610	1510	1900	2320	2320
400WC361	140	—	26	43900	224	6220	5710	7030	7030	203	2120	2050	3080	3190	3190
361*	140	280	26	41800	234	6080	5070	6550	6550	210	1970	1770	2660	2890	2890
328	140	—	26	39700	225	6040	5500	6650	6650	204	2120	2040	3070	3120	3120
328*	140	280	26	37600	237	5920	4840	6130	6130	212	1970	1750	2630	2820	2820
303	140	—	26	36700	221	5480	4990	6020	6020	204	1910	1840	2760	2820	2820
303*	140	280	26	34900	232	5370	4410	5570	5570	211	1770	1580	2370	2550	2550
270	140	—	26	32700	217	4870	4440	5310	5310	204	1700	1640	2450	2500	2500
270*	140	280	26	31000	227	4780	3920	4910	4910	211	1570	1410	2110	2260	2260
212	140	—	26	25700	209	3820	3470	3980	3980	204	1320	1280	1870	1940	1940
212*	140	280	26	24400	220	3760	3070	3660	3660	211	1230	1100	1600	1760	1760
181	140	—	26	22000	204	3130	2860	3050	3050	203	1060	1020	1400	1560	1560
181*	140	280	26	20900	213	3060	2840	2760	2760	210	980	882	1210	1410	1410
144	140	—	26	17600	200	2510	2290	2170	2670	203	846	819	1030	1240	1240
144*	140	280	26	16700	209	2460	2030	1920	2480	210	783	706	887	1130	1130
350WC280	140	—	26	33600	187	4120	3690	4570	4570	179	1610	1540	2300	2360	2360
258	140	—	26	31000	183	3730	3550	4130	4130	179	1450	1380	2070	2130	2130
230	140	—	26	27600	179	3320	2970	3630	3630	179	1290	1230	1840	1880	1880
197	140	—	26	23600	175	2880	2580	3100	3100	179	1130	1070	1610	1640	1640

Notes: (1) Gauges and hole diameters are those recommended in "Standardised Structural Connections".  
(2) \* Indicates four holes on flange.

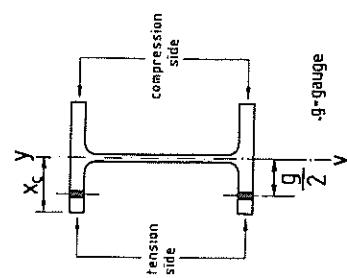
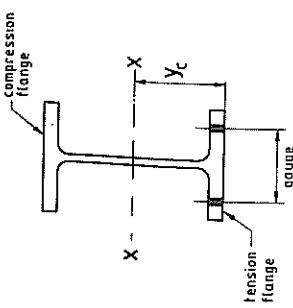


TABLE 3.1-17  
**UNIVERSAL BEAMS  
GRADE 300**  
**SECTION PROPERTIES**  
**two holes on tension flange**



Designation	Holes Deducted	Gauge	Diameter	$A_n$	$y_c$	$Z_x$ (comp) $10^3 \text{mm}^3$	$Z_x$ (tens) $10^3 \text{mm}^3$	$Z_{ex}$ $10^3 \text{mm}^3$	About x-axis			About y-axis			
									$x_c$	$Z_y$ (comp) $10^3 \text{mm}^3$	$Z_y$ (tens) $10^3 \text{mm}^3$	$Z_{ey}$	$S_x$	$S_y$	
610UB125	140	22	15100	306	3230	3230	3680	3680	118	315	294	441	475	10 <sup>3</sup> mm <sup>3</sup>	
113	140	22	13700	304	2880	2880	3290	3290	118	275	257	385	416	10 <sup>3</sup> mm <sup>3</sup>	
101	140	22	12300	301	2530	2530	2900	2900	118	235	220	330	356	10 <sup>3</sup> mm <sup>3</sup>	
530UB 92.4	140	22	11100	282	2020	1790	2180	2180	109	202	186	278	307	10 <sup>3</sup> mm <sup>3</sup>	
82.0	140	22	9920	279	1750	1560	1910	1910	109	170	157	236	260	10 <sup>3</sup> mm <sup>3</sup>	
460UB 82.1	90	22	9760	246	1560	1360	1670	1670	98.7	185	173	289	271	10 <sup>3</sup> mm <sup>3</sup>	
74.6	90	22	8880	245	1420	1230	1510	1510	98.2	166	155	232	242	10 <sup>3</sup> mm <sup>3</sup>	
67.1	90	22	8020	242	1260	1100	1350	1350	98.1	145	136	203	212	10 <sup>3</sup> mm <sup>3</sup>	
410UB 59.7	90	22	7080	219	1030	881	1080	1080	92.6	126	117	175	184	10 <sup>3</sup> mm <sup>3</sup>	
53.7	90	22	6410	216	900	778	955	955	92.4	107	98.6	149	157	10 <sup>3</sup> mm <sup>3</sup>	
360UB 56.7	90	22	6670	194	867	734	903	903	89.9	119	109	163	172	10 <sup>3</sup> mm <sup>3</sup>	
50.7	90	22	5970	192	769	653	801	801	89.3	104	94.8	142	150	10 <sup>3</sup> mm <sup>3</sup>	
44.7	90	22	5300	190	665	568	687	687	89.1	87.3	80.2	119	127	10 <sup>3</sup> mm <sup>3</sup>	
310UB 46.2	90	22	5410	163	631	524	642	642	87.3	99.6	89.7	135	143	10 <sup>3</sup> mm <sup>3</sup>	
40.4	90	22	4760	166	549	457	558	558	86.7	84.8	76.5	115	122	10 <sup>3</sup> mm <sup>3</sup>	
32.0	90	22	3730	163	407	339	405	405	78.7	51.6	46.0	67.4	75.8	10 <sup>3</sup> mm <sup>3</sup>	
250UB 37.3	70	22	4270	142	417	336	418	418	76.9	72.2	64.8	97.3	102	10 <sup>3</sup> mm <sup>3</sup>	
31.4	70	22	3630	138	339	277	343	343	76.6	56.8	51.4	76.8	80.8	10 <sup>3</sup> mm <sup>3</sup>	
25.7	70	18	2980	136	274	227	281	281	65.4	36.7	32.9	49.4	53.4	10 <sup>3</sup> mm <sup>3</sup>	
200UB 29.8	70	22	3460	116	269	212	267	267	71.3	52.0	45.6	68.5	73.4	10 <sup>3</sup> mm <sup>3</sup>	
25.4	70	22	2830	113	221	176	220	221	70.7	41.4	36.5	54.5	58.7	10 <sup>3</sup> mm <sup>3</sup>	
22.3	70	22	2560	113	199	157	189	197	70.7	37.1	32.7	47.7	52.5	10 <sup>3</sup> mm <sup>3</sup>	
180UB 22.2	†														
18.1	†														
16.1	†														
150UB 18.0	†														
14.0	†														

Notes: (1) Gauges and hole diameters are those recommended in "Standardised Structural Connections".  
(2) † indicates flange too small for high strength structural bolts.  
(3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

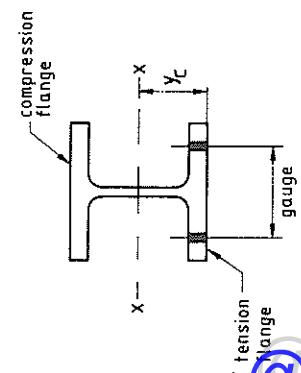
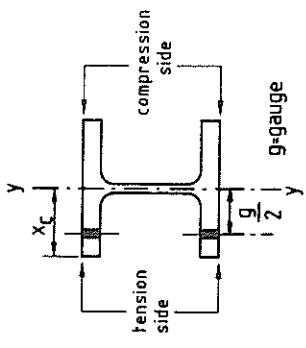


TABLE 3.1-18

**UNIVERSAL COLUMNS  
GRADE 300**

**SECTION PROPERTIES**

**two holes on tension flange**



Designation	Holes Deducted	Diameter	$A_{in}$	About x-axis				About y-axis			
				$y_c$	$Z_x$ (comp)	$Z_x$ (tens)	$S_x$	$x_c$	$Z_y$ (comp)	$Z_y$ (tens)	$S_y$
	mm	mm	mm <sup>2</sup>	mm	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>
310UC158	140	26	18800	164	2370	2370	2680	160	787	740	1110
	137	26	16300	160	2050	2050	2300	159	674	633	949
	118	26	14000	157	1760	1760	1960	158	572	537	806
96.8	140	26	11660	154	1450	1450	1560	1600	465	436	634
250UC 89.5	140	22	10600	130	1100	1100	1230	133	361	334	500
72.9	140	22	8700	127	897	897	986	132	291	269	399
200UC 59.5	140	22	7000	114	569	482	584	109	177	157	235
52.2	140	22	6110	112	500	422	507	108	154	136	204
46.2	140	22	5420	110	440	372	437	108	145	118	175
150UC 37.2	90	22	4230	89.9	264	211	264	82.4	81.6	70.9	106
30.0	90	22	3450	87.7	215	172	212	81.9	65.6	56.9	85.4
23.4	90	22	2680	84.3	160	129	146	81.0	46.5	40.7	57.1
100UC 14.8	60	22	1580	57.3	61.3	42.5	55.7	55.4	18.1	-14.3	21.4
											25.7

Notes: (1) Gauges and hole diameters are those recommended in "Standardised Structural Connections".  
(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

TABLE 3.2-1(A)  
**WELDED BEAMS  
SURFACE AREAS**

Designation	Profile Distance	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face	m <sup>2</sup> /m	m <sup>2</sup> /tonne	m <sup>2</sup> /tonne
1200WB455	4370	4.37	9.61	3870	3.87	8.51	6.55
423	4350	4.35	10.3	3850	3.85	9.10	7.38
392	4340	4.34	11.1	3840	3.84	9.79	7.40
342	3940	3.94	11.5	3540	3.54	10.4	7.52
317	3920	3.92	12.4	3520	3.52	11.1	7.58
278	3710	3.71	13.3	3360	3.36	12.1	7.28
249	3410	3.41	13.7	3130	3.13	12.6	7.21
1000WB322	3620	3.62	11.2	3220	3.22	10.0	7.30
296	3600	3.60	12.1	3200	3.20	10.8	7.30
258	3390	3.39	13.1	3040	3.04	11.8	7.30
215	3170	3.17	14.8	2870	2.87	13.4	7.30
900WB282	3420	3.42	12.1	3020	3.02	10.7	7.30
257	3410	3.41	13.3	3010	3.01	11.7	7.30
218	3200	3.20	14.6	2850	2.85	13.0	7.30
175	2980	2.98	17.0	2680	2.68	15.3	7.30
800WB192	2810	2.81	14.7	2510	2.51	13.1	7.33
168	2700	2.70	16.1	2430	2.42	14.5	7.33
146	2680	2.68	18.4	2410	2.40	16.5	7.33
122	2560	2.56	20.9	2310	2.31	18.9	7.33
700WB173	2510	2.51	14.5	2240	2.24	13.0	6.08
150	2400	2.40	16.0	2150	2.15	14.3	6.54
130	2380	2.38	18.3	2130	2.13	16.3	7.30
115	2360	2.36	20.6	2110	2.11	18.4	8.49

TABLE 3.2-2(A)  
**WELDED COLUMNS  
SURFACE AREAS**

Designation	Profile Distance	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne
500WC440	414	2880	2.88	6.55	2380	2.38	5.41	414	2900	6.99
	383	2880	2.88	7.52	2380	2.38	5.78	383	2980	2.98
	340	2980	2.98	8.77	2480	2.48	6.21	2970	2970	2.97
	290	2970	2.97	10.2	2470	2.47	7.30	267	2960	2.96
	228	2940	2.94	11.1	2460	2.46	8.51	228	2940	12.9
400WC361	328	2380	2.38	6.59	1980	1.98	5.48	328	2400	7.33
	303	2390	2.39	7.88	1990	1.99	6.11	303	2390	7.88
	270	2380	2.38	8.82	1980	1.98	6.56	270	2360	2.36
	181	2340	2.34	11.1	1950	1.96	7.34	181	2340	13.0
	144	2330	2.33	13.0	1940	1.94	9.25	144	2330	16.1
350WC280	2050	2050	2.05	7.33	1930	1.93	10.7	144	1930	1.93
	258	2040	2.04	7.89	1690	1.69	6.54	258	2030	2.03
	230	2020	2.02	8.82	1680	1.68	7.30	230	2020	10.3
	197	197	197	10.3	1670	1.67	8.49	197	1670	16.70

**TABLE 3.2-1(B)**  
**WELDED BEAMS**  
**FIRE ENGINEERING DESIGN**  
**exposed surface area to mass ratio (m<sup>2</sup>/tonne)**

1 = TOTAL PERIMETER, PROFILE-PROTECTED  
 2 = TOTAL PERIMETER, BOX-PROTECTED, NO GAP  
 3 = TOTAL PERIMETER, BOX-PROTECTED, 25mm GAP  
 4 = TOP FLANGE EXCLUDED, PROFILE-PROTECTED  
 5 = TOP FLANGE EXCLUDED, BOX-PROTECTED, NO GAP  
 6 = TOP FLANGE EXCLUDED, BOX-PROTECTED, 25mm GAP

Designation	1	2	3	4	5	6
1200WB455	9.61	7.48	7.92	8.51	6.38	6.60
423	10.3	7.99	8.47	9.10	6.81	7.05
392	11.1	8.59	9.11	9.79	7.32	7.57
342	11.5	9.27	9.86	10.4	8.10	8.39
317	12.4	9.96	10.6	11.1	8.69	9.01
278	13.3	10.9	11.7	12.1	9.67	10.0
249	13.7	11.6	12.4	12.6	10.5	10.9
1000WB392	11.2	8.86	9.48	10.0	7.61	7.92
296	12.1	9.55	10.2	10.8	8.20	8.54
258	13.1	10.5	11.3	11.8	9.19	9.58
215	14.8	12.1	13.0	13.4	10.7	11.2
900WB282	12.1	9.39	10.1	10.7	7.97	8.33
257	13.3	10.2	11.0	11.7	8.69	9.08
218	14.6	11.5	12.5	13.0	9.94	10.4
175	17.0	13.7	14.8	15.3	12.0	12.6
800WB192	14.7	11.7	12.7	13.1	10.1	10.6
168	16.1	12.9	14.1	14.5	11.3	11.9
146	18.4	14.7	16.1	16.5	12.8	13.5
122	20.9	17.0	18.7	18.9	15.0	15.8
700WB173	14.5	11.5	12.6	13.0	9.88	10.5
150	16.0	12.8	14.1	14.3	11.1	11.8
130	18.3	14.6	16.1	16.3	12.7	13.4
115	20.6	16.4	18.2	18.4	14.3	15.1

Note: See page 3-4 for details on cases of fire exposure considered.

**TABLE 3.2-2(B)**  
**WELDED COLUMNS**  
**FIRE ENGINEERING DESIGN**  
**exposed surface area to mass ratio (m<sup>2</sup>/tonne)**

1 = TOTAL PERIMETER, PROFILE-PROTECTED  
 2 = TOTAL PERIMETER, BOX-PROTECTED, NO GAP  
 3 = TOTAL PERIMETER, BOX-PROTECTED, 25mm GAP  
 4 = TOP FLANGE EXCLUDED, PROFILE-PROTECTED  
 5 = TOP FLANGE EXCLUDED, BOX-PROTECTED, NO GAP  
 6 = TOP FLANGE EXCLUDED, BOX-PROTECTED, 25mm GAP

Designation	1	2	3	4	5	6
500WC440	6.55	6.99	4.46	4.91	5.41	3.32
414	7.52	7.57	5.07	5.60	5.21	3.52
383	8.77	5.97	7.30	4.50	3.77	4.03
340	10.2	6.93	8.51	5.21	4.80	5.55
290	11.1	7.49	8.24	5.62	5.99	6.50
267	12.9	8.70	9.58	10.7	6.50	6.94
228						
400WC361	6.59	4.60	5.15	5.48	3.49	3.77
328	7.33	5.06	5.67	6.11	3.84	4.14
303	7.88	5.43	6.09	6.56	4.11	4.44
270	8.82	6.04	6.78	7.34	4.55	4.92
212	11.1	7.55	8.49	9.25	5.66	6.13
181	13.0	8.75	9.86	10.7	6.54	7.09
144	16.1	10.8	12.2	13.4	8.06	8.75
350WC280	7.33	5.03	5.74	6.08	3.78	4.14
258	7.89	5.40	6.17	6.54	4.04	4.43
230	8.82	6.00	6.87	7.30	4.47	4.91
197	10.3	6.91	7.93	8.49	5.14	5.64

Note: See page 3-4 for details on cases of fire exposure considered.

**TABLE 3.2-3(A)**  
**UNIVERSAL BEAMS**  
**SURFACE AREAS**

Designation	Profile Distance	Profile Surface Area	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face	m <sup>2</sup> /m	m <sup>2</sup> /m	m <sup>2</sup> /tonne	m <sup>2</sup> /tonne
310UB 46.2	1250	1.49	24.8	1310	1.31	21.9	24.4	754	0.754
310UB 40.4	1240	1.48	27.4	1300	1.30	24.1	30.0	908	0.908
310UB 32.0	1160	1.36	24.1	1200	1.20	21.1	30.0	899	0.899
310UB 25.7	1360	1.35	26.8	1190	1.19	23.4	23.4	885	0.885
250UB 37.3	1070	1.07	26.6	1180	1.18	26.3	23.4	733	0.733
200UB 29.8	922	0.922	30.7	1080	1.08	23.2	563	0.563	0.464
200UB 25.4	912	0.912	35.9	914	0.914	24.7	25.4	914	0.914
200UB 22.3	910	0.910	40.4	779	0.779	29.0	32.6	779	0.779
180UB 18.2	764	0.764	42.0	665	0.665	30.7	34.5	665	0.665
180UB 16.1	691	0.691	31.2	601	0.601	27.1	36.6	601	0.601
150UB 14.0	685	0.685	37.9	595	0.595	32.9	36.9	595	0.595
150UB 14.0	682	0.682	42.5	592	0.592	36.9	36.9	592	0.592
	584	0.584	32.4	509	0.509	28.3		509	0.509
	576	0.576	41.1	501	0.501	35.8		501	0.501

**TABLE 3.2-4(A)**  
**UNIVERSAL COLUMNS**  
**SURFACE AREAS**

Designation	Profile Distance	Profile Surface Area	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face	mm	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne
310UC 158	1840	1.84	11.6	1820	1.82	13.3	1530	1.53	9.66
	137			1810	1.81	15.3	1510	1.51	11.0
	118			1790	1.79	18.4	1500	1.50	12.7
250UC 89.5	1500	1.50	16.8	1480	1.48	14.8	1480	1.48	15.3
	72.9			1480	1.48	20.3	1240	1.24	13.9
200UC 59.5	1220	1.22	20.2	1190	1.19	22.8	1020	1.02	16.8
	52.2			1180	1.18	25.6	989	0.989	18.9
150UC 37.2	908	0.908	24.4	899	0.899	29.7	746	0.746	24.6
	30.0			885	0.885	37.8	733	0.733	31.3
100UC 14.8	563	0.563	38.0	464	0.464				31.3

**TABLE 3.2-3(B)**  
**UNIVERSAL BEAMS**  
**FIRE ENGINEERING DESIGN**  
**exposed surface area to mass ratio (m<sup>2</sup>/tonne)**

1 = TOTAL PERIMETER, PROFILE-PROTECTED  
 2 = TOTAL PERIMETER, BOX-PROTECTED, NO GAP  
 3 = TOTAL PERIMETER, BOX-PROTECTED, 25mm GAP  
 4 = TOP FLANGE EXCLUDED, PROFILE-PROTECTED  
 5 = TOP FLANGE EXCLUDED, BOX-PROTECTED, NO GAP  
 6 = TOP FLANGE EXCLUDED, BOX-PROTECTED, 25mm GAP

Designation	1	2	3	4	5	6
610UB 25	16.7	13.4	15.0	14.9	11.6	12.4
113	18.3	14.7	16.5	16.3	12.7	13.6
101	20.3	16.3	18.2	18.1	14.0	15.0
530UB 92.4	20.0	16.0	18.2	17.8	13.8	14.8
82.0	22.4	17.9	20.3	19.9	15.3	16.6
460UB 82.1	20.0	15.9	18.3	17.7	13.5	14.8
74.6	21.9	17.3	20.0	19.4	14.8	16.1
67.1	24.2	19.1	22.1	21.4	16.3	17.8
410UB 59.7	24.8	19.5	22.8	21.9	16.5	18.2
53.7	27.4	21.5	25.2	24.1	18.2	20.0
360UB 56.7	24.1	18.7	22.2	21.1	15.6	17.4
50.7	26.8	20.7	24.7	23.4	17.4	19.3
44.7	30.1	23.3	27.7	26.3	19.5	21.7
310UB 46.2	26.8	20.3	24.6	23.2	16.8	18.9
40.4	30.2	22.9	27.8	26.2	18.9	21.4
32.0	36.2	27.9	34.2	31.5	23.3	26.4
250UB 37.3	28.6	21.6	26.9	24.7	17.7	20.3
31.4	33.7	25.3	31.6	29.0	20.6	23.8
25.7	37.5	29.0	36.8	32.6	24.2	28.1
200UB 29.8	30.7	22.7	29.4	26.3	18.3	21.6
25.4	35.9	26.5	34.4	30.7	21.3	25.2
22.3	40.4	29.7	38.6	34.5	23.8	28.3
18.2	42.0	32.6	43.6	36.6	27.2	32.7
180UB 22.2	31.2	24.3	33.3	27.1	20.2	24.7
18.1	37.9	29.3	40.4	32.9	24.3	29.9
16.1	42.5	32.8	45.3	36.9	27.2	33.4
150UB 18.0	32.4	25.5	36.6	28.3	21.4	26.9
14.0	41.1	32.1	46.4	35.8	26.8	33.9

Note: See page 3-4 for details on cases of fire exposure considered.

**TABLE 3.2-4(B)**

**UNIVERSAL COLUMNS**  
**FIRE ENGINEERING DESIGN**  
**exposed surface area to mass ratio (m<sup>2</sup>/tonne)**

1 = TOTAL PERIMETER, PROFILE-PROTECTED  
 2 = TOTAL PERIMETER, BOX-PROTECTED, NO GAP  
 3 = TOTAL PERIMETER, BOX-PROTECTED, 25mm GAP  
 4 = TOP FLANGE EXCLUDED, PROFILE-PROTECTED  
 5 = TOP FLANGE EXCLUDED, BOX-PROTECTED, NO GAP  
 6 = TOP FLANGE EXCLUDED, BOX-PROTECTED, 25mm GAP

Designation	1	2	3	4	5	6
3100UC 158	11.6	8.08	9.34	9.66	6.11	6.74
137	13.3	9.18	10.6	11.0	6.93	7.66
118	15.3	10.5	12.2	12.7	7.94	8.79
96.8	18.4	12.6	14.7	15.3	9.48	10.5
250UC 89.5	16.8	11.5	13.8	13.9	8.68	9.80
72.9	20.3	13.9	16.6	16.8	10.4	11.8
200UC 59.5	20.2	14.0	17.3	16.8	10.6	12.3
52.2	22.8	15.7	19.5	18.9	11.8	13.7
46.2	25.6	17.5	21.9	21.2	13.2	15.3
150UC 37.2	24.4	17.0	22.4	22.4	12.9	15.5
30.0	29.7	20.5	27.1	24.6	15.4	18.7
23.4	37.8	26.0	34.6	31.3	19.5	23.8
100UC 14.8	38.0	26.5	40.0	31.3	19.8	26.5

Note: See page 3-4 for details on cases of fire exposure considered.

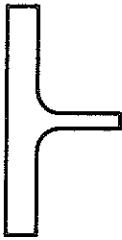


TABLE 3.2-5(A)  
TEES CUT FROM UNIVERSAL BEAMS  
SURFACE AREAS

Designation	Profile Distance	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face			
305BT62.5	1060	1.06	16.9	827	0.827	13.2	
56.5	1050	1.05	18.5	821	0.821	14.5	
50.5	1040	1.04	20.5	816	0.816	16.0	
265BT46.3	937	0.937	20.3	728	0.728	15.7	
41.0	932	0.932	22.7	723	0.723	17.6	
230BT41.1	831	0.831	20.3	640	0.640	15.6	
37.3	826	0.826	22.1	636	0.636	17.0	
33.6	822	0.822	24.5	632	0.632	18.8	
205BT29.9	751	0.751	25.1	573	0.573	19.1	
26.9	747	0.747	27.7	569	0.569	21.1	
180BT28.4	691	0.691	24.3	519	0.519	18.3	
25.4	686	0.686	27.1	515	0.515	20.3	
22.4	682	0.682	30.4	511	0.511	22.8	
155BT23.1	627	0.627	27.0	461	0.461	19.9	
20.2	622	0.622	30.5	457	0.457	22.4	
16.0	583	0.583	36.5	434	0.434	27.2	
125BT18.7	539	0.539	29.0	393	0.393	21.1	
15.7	534	0.534	34.0	388	0.388	24.7	
12.9	484	0.484	37.8	360	0.360	28.2	
100BT14.9	465	0.465	31.1	331	0.331	22.2	
12.7	460	0.460	36.4	327	0.327	25.8	
11.2	458	0.458	40.8	325	0.325	29.0	
9.1	385	0.385	42.4	286	0.286	31.5	
90BT11.1	349	0.349	31.7	259	0.295	23.5	
9.1	345	0.345	38.4	255	0.255	28.4	
8.1	343	0.343	43.0	253	0.253	31.7	
75BT 9.0	296	0.296	33.0	221	0.221	24.7	
7.0	291	0.291	41.8	216	0.216	31.0	

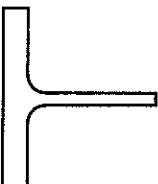
TABLE 3.2-6(A)

TEES CUT FROM UNIVERSAL COLUMNS  
SURFACE AREAS

Designation	Profile Distance	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face	Profile Distance	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face	Profile Surface Area	Profile Distance	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face		
155CT79.0	933	0.933	11.8	622	0.622	7.88	613	0.613	8.96	922	0.922	13.5	605	0.605	10.3
68.5	59.0	59.0	912	912	59.0	59.0	902	902	59.0	59.0	59.0	59.0	59.0	59.0	12.3
125CT44.8	758	0.758	17.0	502	0.502	11.2	494	0.494	13.5	748	0.748	20.5	494	0.494	13.5
36.5															
100CT29.8	608	0.608	20.4	403	0.403	13.5	399	0.399	15.3	603	0.603	23.1	395	0.395	17.1
26.1															
75CT18.6	460	0.460	24.8	306	0.306	16.5	301	0.301	19.9	454	0.454	30.1	295	0.295	25.3
15.0															
50CT 7.4	284	0.284	38.6	185	0.185	25.2									

**TABLE 3.2-5(B)**  
**TEES CUT FROM UNIVERSAL BEAMS**  
**FIRE ENGINEERING DESIGN**  
**exposed surface area to mass ratio (m<sup>2</sup>/tonne)**

1 = TOTAL PERIMETER, PROFILE-PROTECTED  
 2 = TOTAL PERIMETER, BOX-PROTECTED, NO GAP  
 3 = TOTAL PERIMETER, BOX-PROTECTED, 25mm GAP  
 4 = TOP FLANGE EXCLUDED, PROFILE-PROTECTED  
 5 = TOP FLANGE EXCLUDED, BOX-PROTECTED, NO GAP  
 6 = TOP FLANGE EXCLUDED, BOX-PROTECTED, 25mm GAP

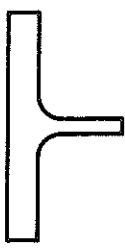


Designation	1	2	3	4	5	6
305BT62.5	16.9	17.1	20.3	13.2	13.4	15.0
56.5	18.5	18.7	22.2	14.5	14.7	16.5
50.5	20.5	20.8	24.7	16.0	16.3	18.2
265BT46.3	20.3	22.9	24.8	15.7	16.0	18.2
41.0	22.7	27.8	27.8	17.6	17.9	20.3
230BT41.1	20.3	22.1	20.5	25.4	15.6	15.8
37.3	37.3	22.4	22.4	27.8	17.0	17.3
33.6	33.6	24.5	24.8	30.7	18.8	19.1
205BT29.9	25.1	25.4	32.1	19.1	19.5	22.8
26.9	27.7	28.1	35.5	21.1	21.5	25.2
180BT28.4	24.3	24.7	31.7	18.3	18.6	22.2
25.4	27.1	27.4	35.3	20.3	20.7	24.6
22.4	30.4	30.9	39.8	22.8	23.2	27.7
155BT23.1	27.0	27.4	36.1	19.9	20.3	24.6
20.2	30.5	31.0	40.8	22.4	22.9	27.8
16.0	36.5	37.2	49.7	27.2	27.9	34.1
125BT18.7	29.0	29.4	40.1	21.1	21.5	26.9
15.7	34.0	34.5	47.3	24.7	25.2	31.6
12.9	37.8	38.6	54.3	28.1	28.9	36.8
100BT14.9	31.1	31.6	45.0	22.2	22.7	29.3
12.7	36.4	37.0	52.8	25.8	26.4	34.4
11.2	40.8	41.5	59.3	29.0	29.6	38.6
9.1	42.4	43.5	65.5	31.5	32.6	43.6
90BT11.1	31.7	32.4	50.5	23.5	24.2	33.3
9.1	38.4	39.2	61.4	28.4	29.2	40.3
8.1	43.0	44.0	69.0	31.7	32.7	45.2
75BT 9.0	33.0	33.8	56.1	24.7	25.4	36.6
7.0	41.8	42.8	71.5	31.0	32.0	46.4

Note: See page 3-4 for details on cases of fire exposure considered.

**TABLE 3.2-6(B)**

**TEES CUT FROM UNIVERSAL COLUMNS**  
**FIRE ENGINEERING DESIGN**  
**exposed surface area to mass ratio (m<sup>2</sup>/tonne)**



1 = TOTAL PERIMETER, PROFILE-PROTECTED  
 2 = TOTAL PERIMETER, BOX-PROTECTED, NO GAP  
 3 = TOTAL PERIMETER, BOX-PROTECTED, 25mm GAP  
 4 = TOP FLANGE EXCLUDED, PROFILE-PROTECTED  
 5 = TOP FLANGE EXCLUDED, BOX-PROTECTED, NO GAP  
 6 = TOP FLANGE EXCLUDED, BOX-PROTECTED, 25mm GAP

Designation	1	2	3	4	5	6
155CT79.0	11.8	12.0	14.5	7.88	8.06	9.33
68.5	13.5	13.7	16.6	8.96	9.17	10.6
59.0	15.5	15.8	19.1	10.3	10.5	12.2
48.4	18.6	18.9	23.0	12.3	12.6	14.7
125CT44.8	17.0	17.3	21.7	11.3	11.5	13.8
36.5	20.5	20.8	26.3	13.5	13.9	16.6
100CT29.8	20.4	20.7	27.4	13.5	13.8	17.2
26.1	23.1	23.5	31.1	15.3	15.7	19.5
23.1	25.9	26.3	34.9	17.1	17.5	21.8
75CT18.6	24.8	25.3	36.1	16.5	16.9	22.3
15.0	30.1	30.6	39.9	20.4	20.4	27.1
11.7	38.3	39.0	56.1	25.3	25.9	34.5
50CT 7.4	38.6	39.8	68.9	25.2	26.3	39.9

Note: See page 3-4 for details on cases of fire exposure considered.

TABLE 3.2-7(A)  
**PARALLEL FLANGE CHANNELS  
SURFACE AREAS**

Designation	Mass per metre	Profile Distance	Profile Surface Area	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face	Profile Surface Area Less 1 Flange Face
	kg/m	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne
380 PFC	55.2	1130	1.13	20.4	1030	1.03	18.6
300 PFC	40.1	932	0.932	23.2	842	0.842	21.0
250 PFC	35.5	834	0.834	23.5	744	0.744	21.0
230 PFC	25.1	737	0.737	29.3	662	0.662	26.3
200 PFC	22.9	678	0.678	29.6	603	0.603	26.3
180 PFC	20.9	638	0.638	30.5	563	0.563	26.9
150 PFC	17.7	579	0.579	32.7	504	0.504	28.5

TABLE 3.2-8(A)  
**TAPER FLANGE CHANNELS  
SURFACE AREAS**

Designation	Mass per metre	Profile Distance	Profile Surface Area	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face	Profile Surface Area Less 1 Flange Face
	kg/m	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne
125 TFC	13.4	480	0.480	35.7	415	0.415	30.9
100 TFC	9.34	374	0.374	40.0	324	0.324	34.6
75 TFC	6.65	286	0.286	43.0	246	0.246	37.0

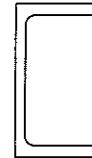
TABLE 3.2-9(A)  
**TAPER FLANGE BEAMS  
SURFACE AREAS**

Designation	Mass per metre	Profile Distance	Profile Surface Area	Profile Surface Area	Profile Distance Less 1 Flange Face	Profile Surface Area Less 1 Flange Face	Profile Surface Area Less 1 Flange Face
	kg/m	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne
125 TFB	13.1	470	0.470	35.7	405	0.405	30.8
100 TFB	7.20	349	0.349	48.5	304	0.304	42.2

TABLE 3.2-7(B)

**PARALLEL FLANGE CHANNELS**  
**FIRE ENGINEERING DESIGN**  
**exposed surface area to mass ratio (m<sup>2</sup>/tonne)**

- 1 = TOTAL PERIMETER, PROFILE-PROTECTED
- 2 = TOTAL PERIMETER, BOX-PROTECTED, NO GAP
- 3 = TOTAL PERIMETER, BOX-PROTECTED, 25mm GAP
- 4 = TOP FLANGE EXCLUDED, PROFILE-PROTECTED
- 5 = TOP FLANGE EXCLUDED, BOX-PROTECTED, NO GAP
- 6 = TOP FLANGE EXCLUDED, BOX-PROTECTED, 25mm GAP



Designation	kg/m	1	2	3	4	5	6
380 PFC	55.2	20.4	17.4	21.0	18.6	15.6	17.4
300 PFC	40.1	23.2	19.5	24.4	21.0	17.2	19.7
250 PFC	35.5	23.5	19.2	24.8	21.0	16.6	19.4
230 PFC	25.1	29.3	24.3	32.2	26.3	21.3	25.3
200 PFC	22.9	29.6	24.0	32.7	26.3	20.7	25.1
180 PFC	20.9	30.5	24.4	34.0	26.9	20.8	25.6
150 PFC	17.7	32.7	25.4	36.7	28.5	21.2	26.8

Note: See page 3-4 for details on cases of fire exposure considered.

TABLE 3.2-8(B)

**TAPER FLANGE CHANNELS**  
**FIRE ENGINEERING DESIGN**  
**exposed surface area to mass ratio (m<sup>2</sup>/tonne)**

- 1 = TOTAL PERIMETER, PROFILE-PROTECTED
- 2 = TOTAL PERIMETER, BOX-PROTECTED, NO GAP
- 3 = TOTAL PERIMETER, BOX-PROTECTED, 25mm GAP
- 4 = TOP FLANGE EXCLUDED, PROFILE-PROTECTED
- 5 = TOP FLANGE EXCLUDED, BOX-PROTECTED, NO GAP
- 6 = TOP FLANGE EXCLUDED, BOX-PROTECTED, 25mm GAP



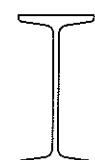
Designation	kg/m	1	2	3	4	5	6
125 TFC	13.4	35.7	28.3	43.2	30.9	23.5	30.9
100 TFC	9.34	40.0	32.1	53.4	34.6	26.7	37.4
75 TFC	6.65	43.0	34.6	64.7	37.0	28.6	43.6

Note: See page 3-4 for details on cases of fire exposure considered.

TABLE 3.2-9(B)

**TAPER FLANGE BEAMS**  
**FIRE ENGINEERING DESIGN**  
**exposed surface area to mass ratio (m<sup>2</sup>/tonne)**

- 1 = TOTAL PERIMETER, PROFILE-PROTECTED
- 2 = TOTAL PERIMETER, BOX-PROTECTED, NO GAP
- 3 = TOTAL PERIMETER, BOX-PROTECTED, 25mm GAP
- 4 = TOP FLANGE EXCLUDED, PROFILE-PROTECTED
- 5 = TOP FLANGE EXCLUDED, BOX-PROTECTED, NO GAP
- 6 = TOP FLANGE EXCLUDED, BOX-PROTECTED, 25mm GAP



Designation	kg/m	1	2	3	4	5	6
125 TFB	13.1	35.7	28.9	44.1	30.8	24.0	31.6
100 TFB	7.20	48.5	40.3	68.1	42.2	34.1	47.9

Note: See page 3-4 for details on cases of fire exposure considered.

TABLE 3.2-10(A)  
**EQUAL ANGLES  
SURFACE AREAS**

Designation	Mass per metre	Profile Distance	Profile Surface Area	Profile Surface Area
	kg/m	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne
200 x 200 x 26EA	76.8	788	0.788	10.3
18EA	60.1	788	0.788	13.1
18EA	54.4	788	0.788	14.5
16EA	48.7	788	0.788	16.2
13EA	40.0	788	0.788	19.7
150 x 150 x 19EA	42.1	590	0.590	14.0
16EA	35.4	590	0.590	16.6
12EA	27.3	590	0.590	21.6
10EA	21.9	590	0.590	27.0
125 x 125 x 16EA	29.1	491	0.491	16.9
12EA	22.5	491	0.491	21.8
10EA	18.0	491	0.491	27.3
8EA	14.9	491	0.491	32.9
100 x 100 x 12EA	17.7	392	0.392	22.1
10EA	14.2	392	0.392	27.6
8EA	11.8	392	0.392	33.3
6EA	9.16	392	0.392	42.8
90 x 90 x 10EA	12.7	352	0.352	27.7
8EA	10.6	352	0.352	33.3
6EA	8.22	352	0.352	42.9
75 x 75 x 10EA	10.5	292	0.292	27.8
8EA	8.73	292	0.292	33.5
6EA	6.81	292	0.292	42.9
5EA	5.27	292	0.292	55.4
65 x 65 x 10EA	9.02	255	0.255	28.3
8EA	7.51	255	0.255	33.9
6EA	5.87	255	0.255	43.4
5EA	4.56	255	0.255	55.9
55 x 55 x 6EA	4.93	215	0.215	43.6
5EA	3.84	215	0.215	56.0
50 x 50 x 8EA	5.68	195	0.195	34.3
6EA	4.46	195	0.195	43.7
5EA	3.48	195	0.195	56.1
3EA	2.31	195	0.195	84.2
45 x 45 x 6EA	3.97	175	0.175	44.2
5EA	3.10	175	0.175	56.6
3EA	2.06	175	0.175	85.1
40 x 40 x 6EA	3.50	155	0.155	44.4
5EA	2.73	155	0.155	56.8
3EA	1.83	155	0.155	84.2
30 x 30 x 6EA	2.56	115	0.115	45.1
5EA	2.01	115	0.115	57.3
3EA	1.35	115	0.115	85.1
25 x 25 x 6EA	2.08	95.3	0.0953	45.7
5EA	1.65	95.3	0.0953	57.7
3EA	1.12	95.3	0.0953	85.2

TABLE 3.2-11(A)  
**UNEQUAL ANGLES  
SURFACE AREAS**

Designation	Mass per metre	Profile Distance	Profile Surface Area	Profile Surface Area
	kg/m	mm	m <sup>2</sup> /m	m <sup>2</sup> /tonne
150 x 100 x 12UA	10UA	18.0	491	491
150 x 90 x 16UA	10UA	27.9	471	471
150 x 90 x 16UA	12UA	21.6	471	471
150 x 90 x 16UA	10UA	17.3	471	471
150 x 90 x 16UA	8UA	14.3	471	471
125 x 75 x 12UA	10UA	14.2	392	392
125 x 75 x 12UA	8UA	11.8	392	392
125 x 75 x 12UA	6UA	9.16	392	392
100 x 75 x 10UA	8UA	12.4	342	342
100 x 75 x 10UA	8UA	10.3	342	342
100 x 75 x 10UA	6UA	7.98	342	342
75 x 50 x 8UA	6UA	7.23	244	244
75 x 50 x 8UA	6UA	5.66	244	244
75 x 50 x 8UA	5UA	4.40	244	244
65 x 50 x 8UA	6UA	6.59	225	225
65 x 50 x 8UA	6UA	5.16	225	225
65 x 50 x 8UA	5UA	4.02	225	225

TABLE 3.2-10(B)

**EQUAL ANGLES****FIRE ENGINEERING DESIGN**  
**Exposed surface area to mass ratio (m<sup>2</sup>/tonne)**

1 = TOTAL PERIMETER PROFILE—PROTECTED  
 2 = TOTAL PERIMETER BOX—PROTECTED, NO GAP  
 3 = TOTAL PERIMETER, BOX—PROTECTED, 25mm GAP  
 4 = TOP FLANGE EXCLUDED, PROFILE—PROTECTED  
 5 = TOP FLANGE EXCLUDED, BOX—PROTECTED NO GAP  
 6 = TOP FLANGE EXCLUDED, BOX—PROTECTED 25mm GAP

Designation	1	2	3	4	5	6
200 x 200 x 26EA	10.3	10.4	13.0	7.66	7.61	9.12
20EA	13.1	13.3	16.6	9.78	9.98	11.6
18EA	14.5	14.7	18.4	10.8	11.0	12.9
16EA	16.2	16.4	20.5	12.1	12.3	14.4
13EA	19.7	20.0	25.0	14.7	15.0	17.5
150 x 150 x 19EA	14.0	14.2	19.0	10.5	10.7	13.1
16EA	16.6	16.9	22.6	12.4	12.7	15.5
12EA	21.6	22.0	29.3	16.1	16.5	20.1
10EA	27.0	27.4	36.5	20.1	20.6	25.2
125 x 125 x 16EA	16.9	17.2	24.0	12.6	12.9	16.3
12EA	21.8	22.2	31.1	16.3	16.7	21.1
10EA	27.3	27.7	38.8	20.3	20.8	26.4
8EA	32.9	33.5	46.9	24.6	25.1	31.8
100 x 100 x 12EA	22.1	22.6	33.8	16.5	16.9	22.1
10EA	27.6	28.1	42.2	20.5	21.1	26.4
8EA	33.3	33.9	50.9	24.8	25.4	33.9
6EA	42.8	43.7	65.5	31.9	32.7	43.7
90 x 90 x 10EA	27.7	28.3	44.0	20.6	21.2	29.0
8EA	33.3	34.1	53.0	24.8	25.6	35.0
6EA	42.9	43.8	68.1	31.9	32.9	45.0
75 x 75 x 10EA	27.8	28.6	47.6	20.7	21.4	30.9
8EA	33.5	34.4	57.3	24.9	25.8	37.2
6EA	42.9	44.1	73.5	31.9	33.1	47.8
5EA	55.4	56.9	94.8	41.2	42.7	61.6
65 x 65 x 10EA	28.3	28.8	51.0	21.1	21.6	32.7
8EA	33.9	34.6	61.2	25.3	26.0	39.3
6EA	43.4	44.3	78.4	32.3	33.2	50.2
5EA	55.9	57.0	101	41.6	42.8	64.7
55 x 55 x 6EA	43.6	44.6	85.2	32.4	33.5	53.8
5EA	56.0	57.3	109	41.7	43.0	69.1
50 x 50 x 8EA	34.3	35.2	70.5	26.5	26.4	44.0
6EA	43.7	44.9	89.7	32.5	33.6	56.1
5EA	56.1	57.6	115	44.7	45.2	71.9
3EA	84.2	86.4	173	62.6	64.8	108
45 x 45 x 6EA	44.2	45.4	95.8	32.8	34.0	59.2
5EA	56.6	58.1	123	42.1	43.6	75.9
3EA	85.1	87.4	184	63.2	65.5	114
40 x 40 x 6EA	44.4	45.8	103	33.0	34.3	62.9
5EA	56.8	58.5	132	42.2	43.9	80.5
3EA	85.1	87.7	197	63.2	65.7	121
30 x 30 x 6EA	45.1	47.0	125	33.4	35.2	74.4
5EA	57.3	59.6	159	42.4	44.7	94.4
3EA	85.1	88.6	236	63.0	66.5	140
25 x 25 x 6EA	45.7	48.0	144	33.7	36.0	84.0
5EA	57.7	60.6	182	42.6	45.4	106
3EA	85.2	89.4	268	62.8	67.0	156

Note: See page 3-4 for details on cases of fire exposure considered.

TABLE 3.2-11(B)

**UNEQUAL ANGLES**  
**FIRE ENGINEERING DESIGN**  
**Exposed surface area to mass ratio (m<sup>2</sup>/tonne)**

1 = TOTAL PERIMETER, PROFILE—PROTECTED  
 2 = TOTAL PERIMETER, BOX—PROTECTED, NO GAP  
 3 = TOTAL PERIMETER, BOX—PROTECTED, 25mm GAP  
 4 = TOP FLANGE EXCLUDED, PROFILE—PROTECTED  
 5 = TOP FLANGE EXCLUDED, BOX—PROTECTED, NO GAP  
 6 = TOP FLANGE EXCLUDED, BOX—PROTECTED, 25mm GAP

Designation	1	2	3	4	5	6
150 x 100 x 12UA	150 x 100 x 12UA	150 x 100 x 10UA	21.8	22.2	31.1	17.4
10UA	10UA	27.3	27.7	38.8	21.7	22.2
150 x 90 x 16UA	150 x 90 x 16UA	150 x 12UA	16.9	17.2	24.4	13.7
12UA	10UA	21.9	22.3	31.5	17.7	18.1
10UA	8UA	27.3	27.8	39.4	22.1	22.6
8UA	8UA	33.0	33.6	47.5	26.7	27.3
125 x 75 x 12UA	125 x 75 x 12UA	125 x 10UA	22.1	22.6	33.8	18.3
10UA	10UA	27.6	28.1	42.2	22.3	22.8
8UA	8UA	33.3	33.9	50.9	26.9	27.6
6UA	6UA	42.8	43.7	65.5	34.6	35.5
100 x 75 x 10UA	100 x 75 x 10UA	100 x 10UA	27.7	28.3	44.5	21.6
8UA	8UA	33.4	34.1	53.6	26.0	26.8
6UA	6UA	42.9	43.8	68.9	33.5	34.4
75 x 50 x 8UA	75 x 50 x 8UA	75 x 6UA	33.8	34.6	62.3	26.9
6UA	6UA	43.2	44.2	79.5	34.4	35.4
5UA	5UA	55.6	56.8	102	44.2	45.5
65 x 50 x 8UA	65 x 50 x 8UA	65 x 6UA	34.1	34.9	65.2	26.5
5UA	5UA	43.5	44.5	83.3	33.9	34.9
56.0	57.3	57.3	57.3	107	43.5	44.8

Note: See page 3-4 for details on cases of fire exposure considered.

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**PART 4 METHODS OF STRUCTURAL ANALYSIS**

	PAGE	
<b>4.1</b>	<b>Methods of Determining Design Action Effects.....</b>	<b>4-2</b>
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<b>4.2.1</b>	<b>Braced Members .....</b>	<b>4-2</b>
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**TABLES****TABLES 4-1 to 4-11**

Elastic Flexural Buckling Loads ( $N_{om}$ ) .....	4-10
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**PART 4****METHODS OF STRUCTURAL ANALYSIS****4.1 Methods of Determining Design Action Effects**

This section provides guidance on calculating design action effects as required by AS 4100. The methods of analysis recognised by AS 4100 are:

- (a) first-order elastic analysis with moment amplification (Clause 4.4.2 of AS 4100),
- (b) second-order elastic analysis (Appendix E of AS 4100),
- (c) plastic analysis with moment amplification (Clause 4.5 of AS 4100), and
- (d) advanced analysis (Appendix D of AS 4100).

These four methods consider the interaction of load and deformation that produce second-order effects. For members subject to bending and axial force, second-order effects (known as  $P-\Delta$  and  $P-\delta$  effects) can increase the design bending moment.

Structural analysis methods (a) and (b) are most commonly used. However (b) can only be effectively used via computer methods. This method, together with methods (c) and (d) are beyond the scope of this publication. Hence, tables are presented which will assist designers with method (a) above.

**4.2 Moment Amplification for First-Order Elastic Analyses**

For a member subjected to combined bending and axial force, the bending moments are *amplified* by the presence of axial force. This occurs to both isolated, statically determinate members, and members in a statically indeterminant frame. A first-order elastic analysis alone does not consider second-order effects, however *moment amplification* accounts for the second-order effects. The moment amplification factor is calculated differently for braced and sway members as shown below.

**4.2.1 Braced Members**

In a braced member the transverse displacement of one end of the member relative to the other is effectively prevented. The moment amplification factor for a braced member is  $\delta_b$ .

If a first-order elastic analysis is carried out then  $\delta_b$  is used to amplify the bending moments between the ends of the member (Clause 4.4.2.2 of AS 4100). If  $\delta_b$  is greater than 1.4, a second-order elastic analysis must be carried out in accordance with Appendix E of AS 4100.

$\delta_b$  is calculated from the flow chart in Figure 4.1. The design bending moment is given by:

$$M^* = M_m^* \quad (\text{for braced members subject to axial tension or with zero axial force})$$

$$M^* = \delta_b M_m^* \quad (\text{for braced members subject to compression})$$

where  $M_m^*$  is the maximum design bending moment calculated using a first-order analysis.

## 4.2.2 Sway Members

In a sway member the transverse displacement of one end of the member relative to the other is not effectively prevented. The moment amplification factor for a sway member is  $\delta_s$ .

The bending moments calculated from a first-order elastic analysis are modified by the moment amplification factor ( $\delta_m$ ) which is the greater of  $\delta_b$  and  $\delta_s$  (Clause 4.4.2.3 of AS 4100). If  $\delta_m$  is greater than 1.4 a second-order elastic analysis must be used in accordance with Appendix E of AS 4100.

$\delta_b$  and  $\delta_s$  are calculated using the flow charts shown in Figures 4.1 and 4.2 and the design bending moment is given by:

$$M^* = \delta_m M_m^*$$

## 4.2.3 Values of $c_m$

The factor for unequal moments ( $c_m$ ) is used in the calculation of  $\delta_b$ . If a braced member is subject *only to end moments* then:

$$c_m = 0.6 - 0.4 \beta_m \leq 1.0 \quad (\text{Clause 4.4.2.2 of AS 4100})$$

where  $\beta_m$  is the ratio of the smaller to the larger bending moment at the ends of the member, taken as positive when the member is bent in reverse curvature.

If the member is subjected to transverse loading,  $\beta_m$  is calculated as follows:

- (a)  $\beta_m = -1.0$  (conservative), (Clause 4.4.2.2(a) of AS 4100)
- (b)  $\beta_m$  is obtained by matching the moment distribution options shown in Figure 4.4.2.2 of AS 4100,
- (c)  $\beta_m$  is based on the midspan deflection. (Clause 4.4.2.2(c) of AS 4100)

## 4.2.4 Elastic Flexural Buckling Loads

Elastic flexural buckling loads ( $N_{om}$ ) are required for the calculation of  $\delta_b$  and  $\delta_m$ . Values of  $N_{om}$  for various effective lengths ( $L_e$ ) are given in Tables 4-1 to 4-11 determined using Clause 4.6.2 of AS 4100 as:

$$N_{om} = \frac{\pi^2 EI}{(k_e L)^2}$$

where  $k_e L = L_e$  = effective length

There are two series of tables. Each (A) series table lists elastic flexural buckling loads for buckling about the  $x$ -axis ( $N_{omx}$ ) and is immediately followed by a (B) series table for buckling about the  $y$ -axis ( $N_{omy}$ ).

$k_e$  is given in Table 6.2 for members with idealised end restraints. For braced or sway members in frames,  $k_e$  depends on the ratio ( $\gamma$ ) of the compression member stiffness to the end restraint stiffness, calculated at each end of the member. Example 2 in Section 4.3 provides a sample calculation of  $k_e$  for a simple unbraced plane frame.

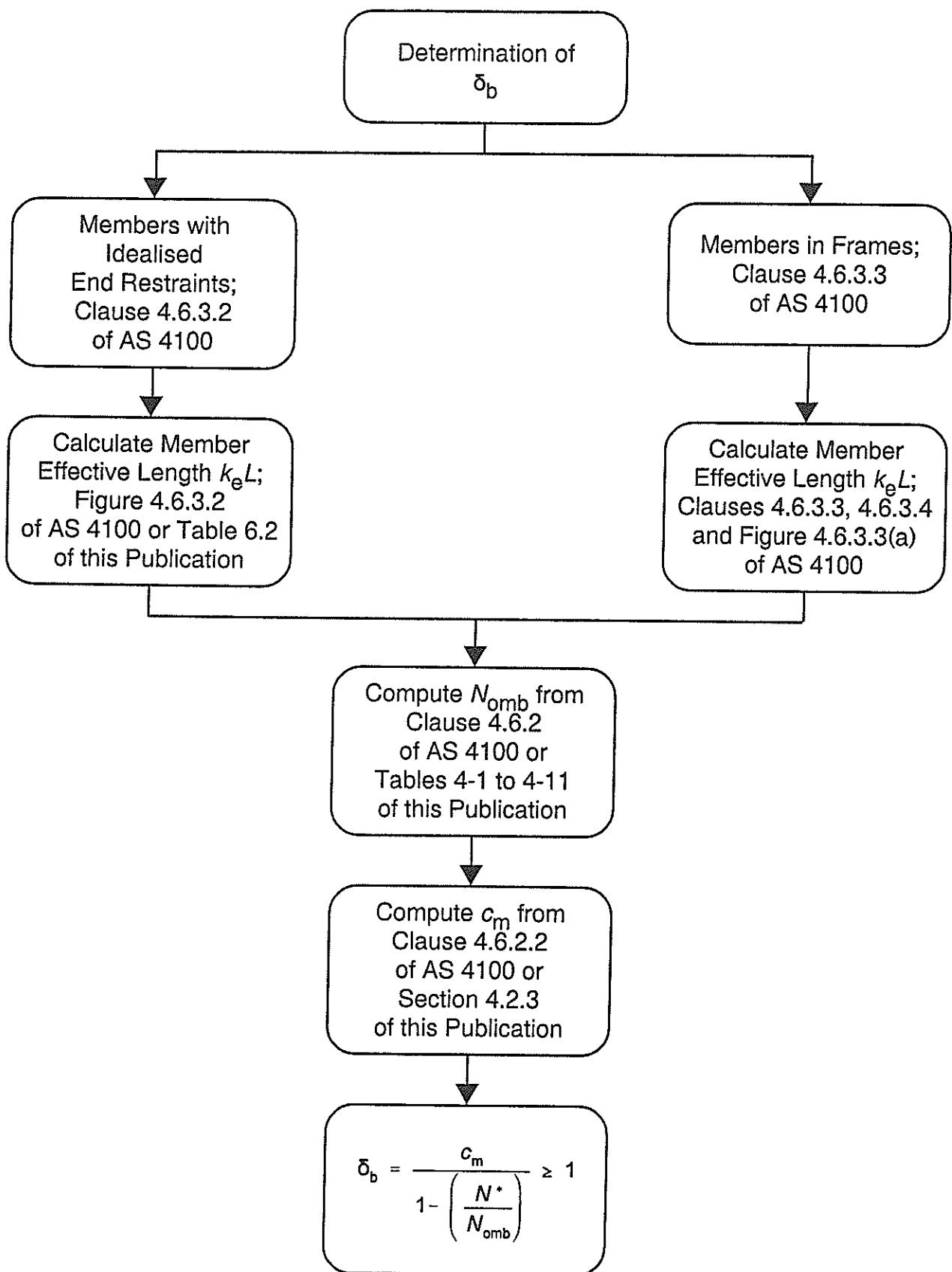
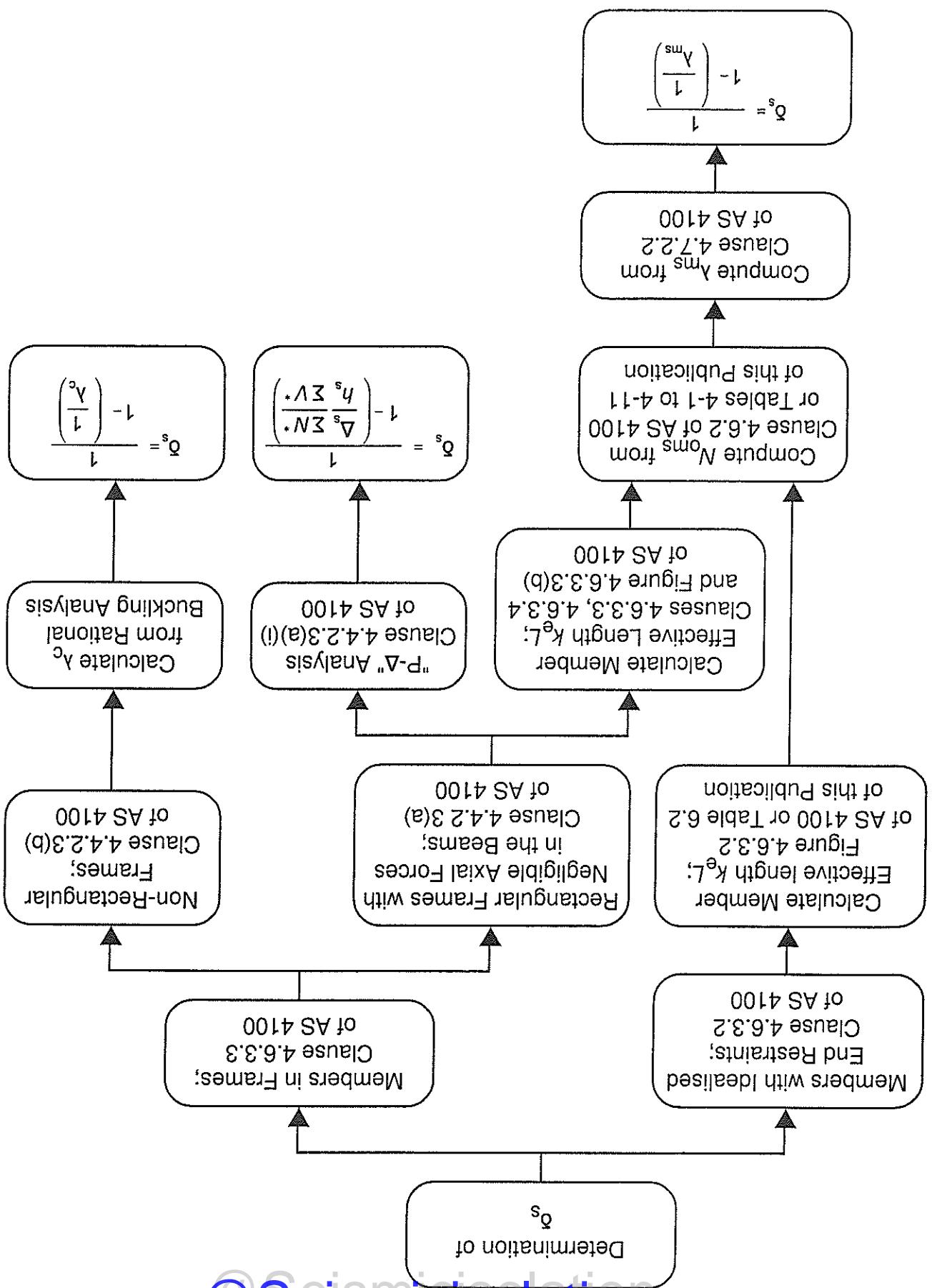


Figure 4.1: Flow Chart for Determination of  $\delta_b$

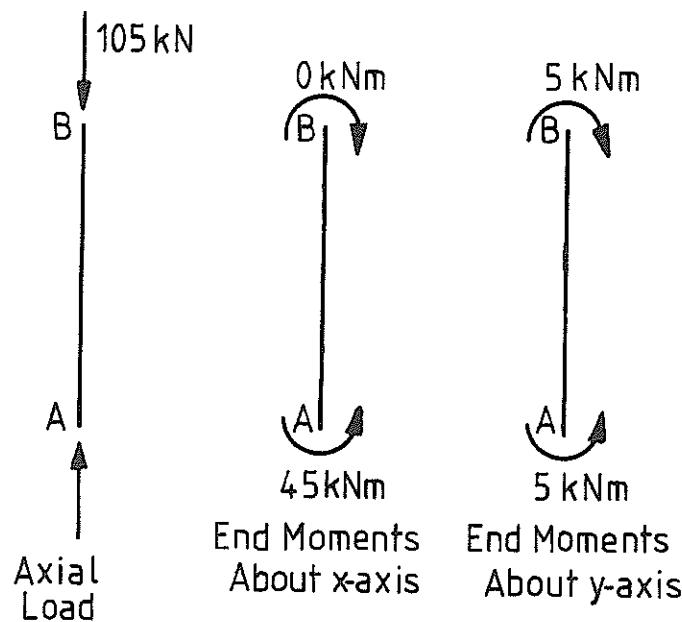
Figure 4.2: Flow Chart for Determination of  $\phi_s$



## 4.3 Examples

### 1. Braced Beam Column

Determine the design action effects for an isolated beam column below. A braced member is subjected to design actions as shown.



#### Design Data:

Section: 200UB29.8 Grade 300 steel

Effective lengths: Flexural buckling (x-axis) = 4.0 m  
Flexural buckling (y-axis) = 4.0 m

#### Solution:

$$N^* = 105 \text{ kN}$$

$$N_{ombx} = 3590 \text{ kN} \quad \text{from Table 4-3(A) for } L_{ex} = 4.0 \text{ m}$$

$$N_{omby} = 476 \text{ kN} \quad \text{from Table 4-3(B) for } L_{ey} = 4.0 \text{ m}$$

$$M_{mx}^* = 45 \text{ kNm} \quad \text{maximum at End A}$$

$$M_{my}^* = 5.0 \text{ kNm} \quad \text{maximum at Ends A and B}$$

$$c_{mx} = 0.60 \quad \text{from Section 4.2.3 for } \beta_{mx} = 0$$

$$c_{my} = 1.00 \quad \text{from Section 4.2.3 for } \beta_{my} = -1.0$$

From Figure 4.1 the moment amplification factor ( $\delta_b$ ) is given by:

$$\delta_b = \frac{c_m}{1 - \left( \frac{N^*}{N_{omb}} \right)}$$

Considering flexural buckling about x-axis:

$$\delta_{bx} = 0.618 (< 1) (\Rightarrow \delta_{bx} = 1)$$

∴ Maximum moment occurs at the ends, i.e. at End A

$$M_x^* = 45 \text{ kNm}$$

Considering flexural buckling about y-axis:

$$\delta_{by} = 1.28$$

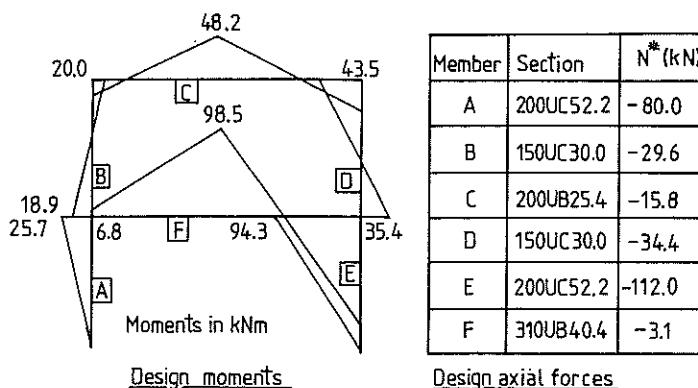
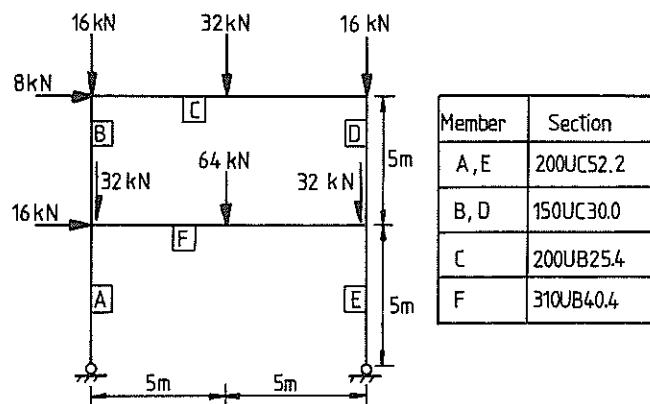
∴ Maximum moment occurs between ends, i.e. in span

$$M_y^* = 1.28 \times 5.0 \\ = 6.40 \text{ kNm}$$

## 2. Unbraced plane frame

Calculate the design action effects using first-order elastic analysis and moment magnification for the columns of the unbraced frame below. This is based on Example 4.5 of *Worked Examples for Steel Structures*, 2nd Edition, M.A. Bradford, R.Q. Bridge & N.S. Trahair, published by AISC 1992.

The design loads on a frame and the results of a first-order elastic analysis are shown below.



### Solution:

- (i) Calculation of elastic flexural buckling loads for the columns:

The braced and sway effective length factors ( $k_{eb}$  and  $k_{es}$ ) are required for the determination of the elastic flexural buckling loads ( $N_{omb}$  and  $N_{oms}$  respectively).

Since the restraining beams are rigidly connected at their far ends to the columns,  $\beta_e = 1.0$  (Table 4.6.3.4 of AS 4100 ).

- a) Upper storey columns (Clause 4.6.3.4 of AS 4100)

$$\gamma = \frac{\sum \left( \frac{I}{L} \right)_c}{\sum \beta_e \left( \frac{I}{L} \right)_b}$$

$$\gamma_T = (17.6 / 5.0) / (1.0 \times 23.6 / 10.0) = 1.49$$

$$\gamma_B = ((17.6 + 52.8) / 5.0) / (1.0 \times 86.4 / 10.0) = 1.63$$

Using Figures 4.6.3.3(b) and (a) of AS 4100,  $k_{es} = 1.47$        $k_{eb} = 0.83$

$$\therefore L_{es} = 1.47 \times 5.0 = 7.35 \text{ m} \quad L_{eb} = 0.83 \times 5.0 = 4.15 \text{ m}$$

From Table 4-4(A) for  $L_e = 8 \text{ m}$ ,  $N_{om} = 543 \text{ kN}$

For  $L_e = 7.35 \text{ m}$ , the elastic buckling loads for the upper storey columns are

$$N_{oms} = 543 \times (8 / 7.35)^2 \quad N_{omb} = 543 \times (8 / 4.15)^2 \\ = 643 \text{ kN} \quad = 2020 \text{ kN}$$

- b) Lower storey columns (Clause 4.6.3.4 of AS 4100)

$$\gamma_T = ((17.6 + 52.8) / 5.0) / (1.0 \times 86.4 / 10.0) = 1.63$$

$$\gamma_B = 10 \text{ (pinned base)}$$

Using Figures 4.6.3.3(b) and (a) of AS 4100,  $k_{es} = 2.1$        $k_{eb} = 0.89$

$$\therefore L_{es} = 2.1 \times 5.0 = 10.5 \text{ m} \quad L_{eb} = 0.89 \times 5.0 = 4.45 \text{ m}$$

From Table 4-4(A) for  $L_e = 10 \text{ m}$ ,  $N_{om} = 1040 \text{ kN}$

For  $L_e = 10.5 \text{ m}$ , the elastic buckling loads for the upper storey columns are

$$N_{oms} = 1040 \times (10 / 10.5)^2 \quad N_{omb} = 1040 \times (10 / 4.45)^2 \\ = 943 \text{ kN} \quad = 5250 \text{ kN}$$

- (ii) Calculation of moment amplification factor  $\delta_b$  (consider each column separately)

From Figure 4.1 the moment amplification factor  $\delta_b$  is given by:

$$\delta_b = \frac{c_m}{1 - \left( \frac{N^*}{N_{omb}} \right)}$$

Column A:

$$c_{mA} = 0.60 \quad (\text{Section 4.2.3 for } \beta_{mA} = 0)$$

$$\therefore \delta_{bA} = \frac{0.60}{1 - \frac{80.0}{5250}} = 0.609 \quad (< 1.0)$$

Column B:

$$c_{mB} = 0.222 \quad (\text{Section 4.2.3 for } \beta_{mB} = 0.95)$$

$$\therefore \delta_{bB} = \frac{0.222}{1 - \frac{29.6}{2020}} = 0.225 \quad (< 1.0)$$

Column D:

$$c_{mD} = 0.274 \quad (\text{Section 4.2.3 for } \beta_{mD} = 0.81)$$

$$\therefore \delta_{bD} = \frac{0.274}{1 - \frac{34.4}{2020}} = 0.278 \quad (< 1.0)$$

Column E:

$$c_{mE} = 0.60 \quad (\text{Section 4.2.3 for } \beta_{mE} = 0)$$

$$\therefore \delta_{bE} = \frac{0.60}{1 - \frac{112}{5250}} = 0.613 \quad (< 1.0)$$

Clause 4.4.2.2 of AS 4100 states that  $\delta_b \geq 1.0$ .

$$\therefore \delta_b = 1.0 \quad \text{for the upper storey}$$

$$\delta_b = 1.0 \quad \text{for the lower storey}$$

(iii) Calculation of sway moment amplification factor  $\delta_s$

From Figure 4.2 for a rectangular frame with negligible axial force in the beams, the sway moment amplification factor  $\delta_s$  for each storey is given by

$$\delta_s = \frac{1}{1 - \left( \frac{1}{\lambda_{ms}} \right)}$$

$$\text{where } \lambda_{ms} = \frac{\sum \left( \frac{N_{oms}}{L} \right)}{\sum \left( \frac{N^*}{L} \right)}$$

a) Upper storey (Clause 4.7.2.2 of AS 4100)

$$\lambda_{ms} = \frac{2 \times 643/5.0}{(29.6 + 34.4)/5.0} = 20.1$$

$$\therefore \delta_s = 1.052 \quad (< 1.4)$$

b) Lower storey (Clause 4.7.2.2 of AS 4100)

$$\lambda_{ms} = \frac{2 \times 943/5.0}{(80.0 + 112)/5.0} = 9.82$$

$$\therefore \delta_s = 1.113 \quad (< 1.4)$$

(iv) Determination of  $\delta_m$

$$\delta_m = \max [\delta_b, \delta_s] = 1.052 \quad \text{for the upper storey}$$

$$\delta_m = \max [\delta_b, \delta_s] = 1.113 \quad \text{for the lower storey}$$

Therefore the design bending moments are:

$$M^* = 43.5 \times 1.052 = 45.8 \text{ kNm} \quad \text{for the upper storey}$$

$$M^* = 94.3 \times 1.113 = 105 \text{ kNm} \quad \text{for the lower storey}$$

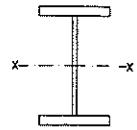


TABLE 4-1(A)  
WELDED BEAMS  
ELASTIC FLEXURAL BUCKLING LOADS  
buckling about x-axis

Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres															
	0	2	4	6	8	10	12	15	18	21	24	27	30	33	36	
1200WB455	∞	7570	1890	841	473	303	210	135	93.4	68.6	52.6	41.5	33.6	27.8	23.4	
	423	∞	6660	1720	762	429	274	191	122	84.7	62.2	47.6	37.6	30.5	25.2	21.2
	392	∞	6160	1540	685	385	247	171	110	76.1	55.9	42.8	33.8	27.4	22.6	19.0
	342	∞	5120	1280	569	320	205	142	91.0	63.2	46.4	35.5	28.1	22.7	18.8	15.8
	317	∞	4570	1140	507	285	183	127	81.2	56.4	41.4	31.7	25.1	20.3	16.8	14.1
	278	∞	3760	939	417	235	150	104	66.8	46.4	34.1	26.1	20.6	16.7	13.8	11.6
249	∞	3150	787	350	197	126	87.5	56.0	38.9	28.6	21.9	17.3	14.0	11.6	9.72	
	1000WB322	∞	3690	923	410	231	148	103	65.6	45.6	33.5	25.6	20.3	16.4	13.6	11.4
	296	∞	3280	820	364	205	131	91.1	58.3	40.5	29.8	22.8	18.0	14.6	12.0	10.1
	258	∞	2680	669	297	167	107	74.4	47.6	33.1	24.3	18.6	14.7	11.9	9.83	8.26
	215	∞	2000	501	223	125	80.2	55.7	35.6	24.7	18.2	13.9	11.0	8.91	7.36	6.19
	900WB282	∞	2830	707	314	177	113	78.6	50.3	34.9	25.6	19.6	15.5	12.6	10.4	8.73
257	∞	2490	623	277	156	99.7	69.3	44.3	30.8	22.6	17.3	13.7	11.1	9.16	7.70	
	218	∞	2010	501	223	125	80.2	55.7	35.6	24.8	18.2	13.9	11.0	8.91	7.37	6.19
	175	∞	1460	365	162	91.3	58.4	40.6	26.0	18.0	13.2	10.1	8.01	6.49	5.36	4.51
	800WB192	∞	1470	367	163	91.8	58.7	40.8	26.1	18.1	13.3	10.2	8.06	6.52	5.39	4.53
168	∞	1230	307	136	76.6	49.0	34.1	21.8	15.1	11.1	8.52	6.73	5.45	4.50	3.78	
	146	∞	1010	252	112	62.9	40.3	28.0	17.9	12.4	9.13	6.99	5.52	4.47	3.70	3.11
	122	∞	775	194	86.1	48.4	31.0	21.5	13.8	9.57	7.03	5.38	4.25	3.44	2.85	2.39
	700WB173	∞	1020	255	113	63.6	40.7	28.3	18.1	12.6	9.23	7.07	5.59	4.52	3.74	3.14
150	∞	842	211	93.6	52.6	33.7	23.4	15.0	10.4	7.64	5.85	4.62	3.74	3.09	2.60	
	130	∞	689	172	76.5	43.1	27.6	19.1	12.2	8.50	6.25	4.78	3.78	3.06	2.53	2.13
	115	∞	569	142	63.3	35.6	22.8	15.8	10.1	7.03	5.16	3.95	3.12	2.53	2.09	1.76

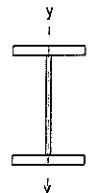


TABLE 4-1(B)  
WELDED BEAMS  
ELASTIC FLEXURAL BUCKLING LOADS  
buckling about y-axis

Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres															
	0	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	6.0	7.0	8.0	9.0	10.0	
1200WB455	∞	1650	731	411	263	183	134	103	81.3	65.8	45.7	33.6	25.7	20.3	16.5	
	423	∞	1480	658	370	237	165	121	92.6	73.1	59.2	41.1	30.2	23.1	18.3	14.8
	392	∞	1320	585	329	211	146	107	82.3	65.0	52.7	36.6	26.9	20.6	16.3	13.2
	342	∞	675	300	169	108	74.9	55.1	42.2	33.3	27.0	18.7	13.8	10.5	8.33	6.75
	317	∞	590	262	148	94.4	65.6	48.2	36.9	29.2	23.6	16.4	12.0	9.22	7.29	5.90
	278	∞	353	157	88.3	56.5	39.3	28.8	22.1	17.5	14.1	9.82	7.21	5.52	4.36	3.53
249	∞	172	76.4	43.0	27.5	19.1	14.0	10.7	8.48	6.87	4.77	3.51	2.68	2.12	1.72	
	1000WB322	∞	674	300	169	108	74.9	55.1	42.2	33.3	27.0	18.7	13.8	10.5	8.33	6.74
	296	∞	590	262	148	94.4	65.6	48.2	36.9	29.1	23.6	16.4	12.0	9.22	7.29	5.90
	258	∞	353	157	88.3	56.5	39.3	28.8	22.1	17.4	14.1	9.81	7.21	5.52	4.36	3.53
	215	∞	178	79.2	44.6	28.5	19.8	14.6	11.1	8.80	7.13	4.95	3.64	2.79	2.20	1.78
	900WB282	∞	674	300	169	108	74.9	55.0	42.1	33.3	27.0	18.7	13.8	10.5	8.32	6.74
257	∞	590	262	147	94.4	65.5	48.1	36.9	29.1	23.6	16.4	12.0	9.22	7.28	5.90	
	218	∞	353	157	88.2	56.5	39.2	28.8	22.1	17.4	14.1	9.80	7.20	5.51	4.36	3.53
	175	∞	178	79.1	44.5	28.5	19.8	14.5	11.1	8.79	7.12	4.94	3.63	2.78	2.20	1.78
	800WB192	∞	249	111	62.2	39.8	27.6	20.3	15.6	12.3	9.95	6.91	5.08	3.89	3.07	2.49
168	∞	171	76.1	42.8	27.4	19.0	14.0	10.7	8.45	6.85	4.75	3.49	2.67	2.11	1.71	
	146	∞	137	60.9	34.2	21.9	15.2	11.2	8.56	6.76	5.48	3.80	2.80	2.14	1.69	1.37
	122	∞	82.4	36.6	20.6	13.2	9.15	6.72	5.15	4.07	3.29	2.29	1.68	1.29	1.02	0.824
	700WB173	∞	192	85.2	47.9	30.7	21.3	15.6	12.0	9.47	7.67	5.32	3.91	3.00	2.37	1.92
150	∞	129	57.2	32.2	20.6	14.3	10.5	8.04	6.35	5.14	3.57	2.62	2.01	1.59	1.29	
	130	∞	103	45.7	25.7	16.5	11.4	8.40	6.43	5.08	4.12	2.86	2.10	1.61	1.27	1.03
	115	∞	82.4	36.6	20.6	13.2	9.15	6.72	5.15	4.07	3.29	2.29	1.68	1.29	1.02	0.824

TABLE 4-2(A)

**WELDED COLUMNS**

**ELASTIC FLEXURAL BUCKLING LOADS**

buckling about x-axis



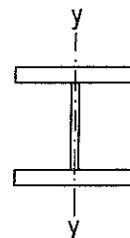
Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres														
	0	2	4	6	8	10	12	15	18	21	24	27	30	33	36
500WC440	∞	1060	266	118	66.5	42.5	29.5	18.9	13.1	9.64	7.38	5.83	4.73	3.91	3.28
414	∞	1040	261	116	65.1	41.7	29.0	18.5	12.9	9.45	7.24	5.72	4.63	3.83	3.22
383	∞	930	233	103	58.2	37.2	25.8	16.5	11.5	8.44	6.46	5.11	4.14	3.42	2.87
340	∞	1010	253	112	63.3	40.5	28.1	18.0	12.5	9.18	7.03	5.55	4.50	3.72	3.12
290	∞	865	216	96.1	54.1	34.6	24.0	15.4	10.7	7.85	6.01	4.75	3.84	3.18	2.67
267	∞	771	193	85.7	48.2	30.9	21.4	13.7	9.52	7.00	5.36	4.23	3.43	2.83	2.38
228	∞	620	155	68.9	38.8	24.8	17.2	11.0	7.66	5.63	4.31	3.40	2.76	2.28	1.91
400WC361	∞	673	168	74.8	42.1	26.9	18.7	12.0	8.31	6.11	4.67	3.69	2.99	2.47	2.08
328	∞	652	163	72.4	40.7	26.1	18.1	11.6	8.05	5.91	4.53	3.58	2.90	2.39	2.01
303	∞	580	145	64.5	36.3	23.2	16.1	10.3	7.16	5.26	4.03	3.18	2.58	2.13	1.79
270	∞	506	127	56.2	31.6	20.2	14.1	9.00	6.25	4.59	3.51	2.78	2.25	1.86	1.56
212	∞	383	95.7	42.5	23.9	15.3	10.6	6.80	4.73	3.47	2.66	2.10	1.70	1.41	1.18
181	∞	306	76.4	34.0	19.1	12.2	8.49	5.44	3.77	2.77	2.12	1.68	1.36	1.12	0.944
144	∞	240	60.0	26.7	15.0	9.60	6.66	4.26	2.96	2.18	1.67	1.32	1.07	0.881	0.740
350WC280	∞	369	92.1	40.9	23.0	14.7	10.2	6.55	4.55	3.34	2.56	2.02	1.64	1.35	1.14
258	∞	326	81.5	36.2	20.4	13.0	9.06	5.80	4.02	2.96	2.26	1.79	1.45	1.20	1.01
230	∞	283	70.7	31.4	17.7	11.3	7.86	5.03	3.49	2.56	1.96	1.55	1.26	1.04	0.873
197	∞	240	59.9	26.6	15.0	9.59	6.66	4.26	2.96	2.17	1.66	1.32	1.07	0.881	0.740

TABLE 4-2(B)

**WELDED COLUMNS**

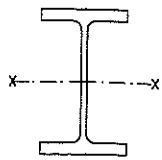
**ELASTIC FLEXURAL BUCKLING LOADS**

buckling about y-axis



Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres														
	0	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	6.0	7.0	8.0	9.0	10.0
500WC440	∞	1650	733	412	264	183	135	103	81.4	66.0	45.8	33.7	25.8	20.4	16.5
414	∞	1650	732	412	264	183	134	103	81.3	65.9	45.8	33.6	25.7	20.3	16.5
383	∞	1480	659	371	237	165	121	92.7	73.2	59.3	41.2	30.3	23.2	18.3	14.8
340	∞	1320	585	329	211	146	108	82.3	65.0	52.7	36.6	26.9	20.6	16.3	13.2
290	∞	1150	512	288	184	128	94.0	72.0	56.9	46.1	32.0	23.5	18.0	14.2	11.5
267	∞	1030	457	257	165	114	84.0	64.3	50.8	41.1	28.6	21.0	16.1	12.7	10.3
228	∞	823	366	206	132	91.5	67.2	51.4	40.6	32.9	22.9	16.8	12.9	10.2	8.23
400WC361	∞	846	376	211	135	94.0	69.1	52.9	41.8	33.8	23.5	17.3	13.2	10.4	8.46
328	∞	843	375	211	135	93.7	68.9	52.7	41.7	33.7	23.4	17.2	13.2	10.4	8.43
303	∞	759	337	190	121	84.4	62.0	47.5	37.5	30.4	21.1	15.5	11.9	9.37	7.59
270	∞	675	300	169	108	75.0	55.1	42.2	33.3	27.0	18.7	13.8	10.5	8.33	6.75
212	∞	527	234	132	84.3	58.5	43.0	32.9	26.0	21.1	14.6	10.8	8.23	6.50	5.27
181	∞	422	187	105	67.5	46.8	34.4	26.3	20.8	16.9	11.7	8.60	6.59	5.20	4.22
144	∞	337	150	84.3	53.9	37.5	27.5	21.1	16.6	13.5	9.36	6.88	5.27	4.16	3.37
350WC280	∞	565	251	141	90.4	62.8	46.1	35.3	27.9	22.6	15.7	11.5	8.83	6.98	5.65
258	∞	509	226	127	81.4	56.5	41.5	31.8	25.1	20.4	14.1	10.4	7.95	6.28	5.09
230	∞	452	201	113	72.3	50.2	36.9	28.3	22.3	18.1	12.6	9.23	7.06	5.58	4.52
197	∞	395	176	98.8	63.2	43.9	32.3	24.7	19.5	15.8	11.0	8.07	6.18	4.88	3.95

TABLE 4-3(A)  
**UNIVERSAL BEAMS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about x-axis**



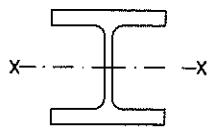
Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres														
	0	2	4	6	8	10	12	15	18	21	24	27	30	33	36
610UB125	∞	487	122	54.1	30.4	19.5	13.5	8.65	6.01	4.41	3.38	2.67	2.16	1.79	1.50
113	∞	432	108	48.0	27.0	17.3	12.0	7.67	5.33	3.91	3.00	2.37	1.92	1.59	1.33
101	∞	376	93.9	41.7	23.5	15.0	10.4	6.68	4.64	3.41	2.61	2.06	1.67	1.38	1.16
530UB 92.4	∞	274	68.4	30.4	17.1	10.9	7.60	4.86	3.38	2.48	1.90	1.50	1.22	1.00	0.844
82.0	∞	236	58.9	26.2	14.7	9.42	6.54	4.19	2.91	2.14	1.64	1.29	1.05	0.865	0.727
460UB 82.1	∞	183	45.9	20.4	11.5	7.34	5.10	3.26	2.26	1.66	1.27	1.01	0.815	0.674	0.566
74.6	∞	165	41.3	18.4	10.3	6.61	4.59	2.94	2.04	1.50	1.15	0.907	0.735	0.607	0.510
67.1	∞	146	36.5	16.2	9.11	5.83	4.05	2.59	1.80	1.32	1.01	0.800	0.648	0.536	0.450
410UB 59.7	∞	107	26.7	11.9	6.67	4.27	2.97	1.90	1.32	0.969	0.742	0.586	0.475	0.392	0.330
53.7	∞	92.7	23.2	10.3	5.79	3.71	2.57	1.65	1.14	0.841	0.644	0.508	0.412	0.340	0.286
360UB 56.7	∞	79.5	19.9	8.83	4.97	3.18	2.21	1.41	0.982	0.721	0.552	0.436	0.353	0.292	0.245
50.7	∞	70.0	17.5	7.78	4.37	2.80	1.94	1.24	0.864	0.635	0.486	0.384	0.311	0.257	0.216
44.7	∞	59.9	15.0	6.65	3.74	2.40	1.66	1.06	0.739	0.543	0.416	0.329	0.266	0.220	0.185
310UB 46.2	∞	49.5	12.4	5.51	3.10	1.98	1.38	0.881	0.612	0.449	0.344	0.272	0.220	0.182	
40.4	∞	42.6	10.7	4.74	2.67	1.71	1.18	0.758	0.527	0.387	0.296	0.234	0.190	0.157	
32.0	∞	31.2	7.79	3.46	1.95	1.25	0.866	0.554	0.385	0.283	0.217	0.171	0.139	0.115	
250UB 37.3	∞	27.5	6.87	3.05	1.72	1.10	0.763	0.488	0.339	0.249	0.191				
31.4	∞	22.0	5.49	2.44	1.37	0.879	0.610	0.391	0.271	0.199	0.153				
25.7	∞	17.5	4.36	1.94	1.09	0.698	0.485	0.310	0.215	0.158	0.121				
200UB 29.8	∞	14.4	3.59	1.60	0.899	0.575	0.399	0.256	0.178	0.130					
25.4	∞	11.6	2.91	1.29	0.727	0.465	0.323	0.207	0.144	0.106					
22.3	∞	10.3	2.59	1.15	0.646	0.414	0.287	0.184	0.128	0.094					
18.2	∞	7.80	1.96	0.867	0.488	0.312	0.217	0.139	0.096	0.071					
180UB 22.2	∞	7.54	1.89	0.898	0.471	0.302	0.210	0.134							
18.1	∞	5.99	1.50	0.665	0.374	0.239	0.166	0.106							
16.1	∞	5.23	1.31	0.581	0.327	0.209	0.145	0.093							
150UB 18.0	∞	4.47	1.12	0.496	0.279	0.179	0.124								
14.0	∞	3.29	0.822	0.365	0.205	0.131	0.091								



**TABLE 4-3(B)**  
**UNIVERSAL BEAMS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about y-axis**

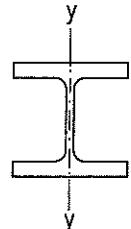
Designation	Elastic Flexural Buckling Loads $N_{\text{om}}$ (MN) Effective Length ( $L_e$ ) in metres														
	0	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	6.0	7.0	8.0	9.0	10.0
610UB125 113 101	∞	77.6	34.5	19.4	12.4	8.62	6.34	4.85	3.83	3.10	2.16	1.58	1.21	0.958	0.776
	∞	67.6	30.1	16.9	10.8	7.51	5.52	4.23	3.34	2.70	1.88	1.38	1.06	0.835	0.676
	∞	57.8	25.7	14.5	9.26	6.43	4.72	3.62	2.86	2.31	1.61	1.18	0.904	0.714	0.578
530UB 92.4 82.0	∞	47.0	20.9	11.7	7.51	5.22	3.83	2.94	2.32	1.88	1.30	0.958	0.734	0.580	0.470
460UB 82.1 74.6 67.1	∞	36.8	16.3	9.19	5.88	4.08	3.00	2.30	1.82	1.47	1.02	0.750	0.574	0.454	0.368
	∞	32.8	14.6	8.20	5.25	3.64	2.68	2.05	1.62	1.31	0.911	0.669	0.512	0.405	0.328
	∞	28.7	12.8	7.18	4.59	3.19	2.34	1.79	1.42	1.15	0.798	0.586	0.449	0.354	0.287
410UB 59.7 53.7	∞	23.8	10.6	5.95	3.81	2.64	1.94	1.49	1.17	0.952	0.661	0.485	0.372	0.294	0.238
	∞	20.3	9.01	5.07	3.24	2.25	1.65	1.27	1.00	0.810	0.563	0.413	0.317	0.250	0.203
360UB 56.7 50.7 44.7	∞	21.8	9.69	5.45	3.49	2.42	1.78	1.36	1.08	0.872	0.606	0.445	0.341	0.269	0.218
	∞	18.9	8.42	4.74	3.03	2.11	1.55	1.18	0.936	0.758	0.526	0.387	0.296	0.234	0.189
	∞	16.0	7.10	4.00	2.56	1.78	1.30	0.999	0.789	0.639	0.444	0.326	0.250	0.197	0.160
310UB 46.2 40.4 32.0	∞	17.8	7.90	4.45	2.84	1.98	1.45	1.11	0.878	0.711	0.494	0.363	0.278	0.220	
	∞	15.1	6.71	3.77	2.41	1.68	1.23	0.943	0.745	0.604	0.419	0.308	0.236	0.186	
	∞	8.72	3.88	2.18	1.40	0.969	0.712	0.545	0.431	0.349	0.242	0.178	0.136	0.108	
250UB 37.3 31.4 25.7	∞	11.2	4.97	2.79	1.79	1.24	0.912	0.698	0.552	0.447	0.310	0.228	0.175		
	∞	8.82	3.92	2.20	1.41	0.908	0.720	0.551	0.435	0.353	0.245	0.180	0.138		
	∞	5.03	2.24	1.26	0.805	0.559	0.411	0.314	0.248	0.201	0.140	0.103	0.079		
200UB 29.8 25.4 22.3 18.2	∞	7.61	3.38	1.90	1.22	0.846	0.621	0.476	0.376	0.304	0.211	0.155			
	∞	6.05	2.69	1.51	0.967	0.672	0.494	0.378	0.299	0.242	0.168	0.123			
	∞	5.42	2.41	1.36	0.868	0.603	0.443	0.339	0.268	0.217	0.151	0.111			
	∞	2.24	0.997	0.561	0.359	0.249	0.183	0.140	0.111	0.090	0.062	0.046			
180UB 22.2 18.1 16.1	∞	2.41	1.07	0.602	0.385	0.268	0.197	0.150	0.119	0.096					
	∞	1.92	0.856	0.481	0.308	0.214	0.157	0.120	0.095	0.077					
	∞	1.68	0.748	0.421	0.269	0.187	0.137	0.105	0.083	0.067					
150UB 18.0 14.0	∞	1.33	0.589	0.332	0.212	0.147	0.108	0.083	0.065						
	∞	0.977	0.434	0.244	0.156	0.109	0.080	0.061	0.048						

TABLE 4-4(A)  
**UNIVERSAL COLUMNS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about x-axis**



Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres													
	0	2	4	6	8	10	12	14	16	18	20	22	24	26
310UC158	∞	191	47.9	21.3	12.0	7.66	5.32	3.91	2.99	2.36	1.91	1.58	1.33	1.13
137	∞	162	40.6	18.0	10.1	6.49	4.51	3.31	2.54	2.00	1.62	1.34	1.13	0.960
118	∞	137	34.2	15.2	8.54	5.47	3.80	2.79	2.14	1.69	1.37	1.13	0.949	0.809
96.8	∞	110	27.5	12.2	6.88	4.40	3.06	2.25	1.72	1.36	1.10	0.910	0.764	0.651
250UC 89.5	∞	70.4	17.6	7.82	4.40	2.82	1.96	1.44	1.10	0.869	0.704	0.582	0.489	0.417
72.9	∞	56.2	14.0	6.24	3.51	2.25	1.56	1.15	0.878	0.694	0.562	0.464	0.390	0.333
200UC 59.5	∞	30.2	7.56	3.36	1.89	1.21	0.840	0.617	0.472	0.373	0.302	0.250	0.210	0.179
52.2	∞	26.1	6.52	2.90	1.63	1.04	0.724	0.532	0.408	0.322	0.261	0.216	0.181	0.154
46.2	∞	22.6	5.66	2.52	1.41	0.906	0.629	0.462	0.354	0.279	0.226	0.187	0.157	0.134
150UC 37.2	∞	10.9	2.73	1.21	0.683	0.437	0.304	0.223	0.171	0.135				
30.0	∞	8.68	2.17	0.965	0.543	0.347	0.241	0.177	0.136	0.107				
23.4	∞	6.23	1.56	0.693	0.390	0.249	0.173	0.127						
100UC 14.8	∞	1.57	0.393	0.175	0.098									

TABLE 4-4(B)  
**UNIVERSAL COLUMNS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about y-axis**



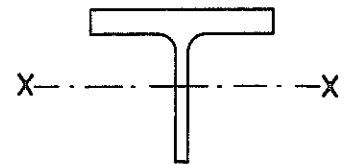
Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres														
	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14
310UC158	∞	248	61.9	27.5	15.5	9.91	6.88	5.05	3.87	3.06	2.48	2.05	1.72	1.47	1.26
137	∞	211	52.7	23.4	13.2	8.43	5.86	4.30	3.29	2.60	2.11	1.74	1.46	1.25	1.08
118	∞	178	44.5	19.8	11.1	7.13	4.95	3.64	2.78	2.20	1.78	1.47	1.24	1.05	0.909
96.8	∞	144	36.0	16.0	8.99	5.75	4.00	2.94	2.25	1.78	1.44	1.19	0.999	0.851	0.734
250UC 89.5	∞	95.6	23.9	10.6	5.97	3.82	2.65	1.95	1.49	1.18	0.956	0.790	0.664	0.565	0.488
72.9	∞	76.6	19.1	8.51	4.79	3.06	2.13	1.56	1.20	0.946	0.766	0.633	0.532	0.453	0.391
200UC 59.5	∞	40.3	10.1	4.48	2.52	1.61	1.12	0.822	0.629	0.497	0.403	0.333	0.280	0.238	0.206
52.2	∞	34.9	8.73	3.88	2.18	1.40	0.971	0.713	0.546	0.431	0.349	0.289	0.243	0.207	0.178
46.2	∞	30.3	7.57	3.37	1.89	1.21	0.842	0.618	0.473	0.374	0.303	0.250	0.210	0.179	0.155
150UC 37.2	∞	13.8	3.46	1.54	0.865	0.553	0.384	0.282	0.216						
30.0	∞	11.1	2.77	1.23	0.693	0.443	0.308	0.226	0.173						
23.4	∞	7.87	1.97	0.874	0.492	0.315	0.218	0.161	0.123						
100UC 14.8	∞	2.24	0.560	0.249	0.140	0.090									



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TABLE 4-5(A)

**TEES CUT FROM UNIVERSAL BEAMS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about x-axis**



Designation	Elastic Flexural Buckling Loads $N_{\text{om}}$ (MN) Effective Lengths ( $L_e$ ) in metres														
	0	1	2	3	4	5	6	7	8	9	10	11	12	14	16
305BT62.5	∞	135	33.7	15.0	8.42	5.39	3.74	2.75	2.11	1.66	1.35	1.11	0.936	0.688	0.526
56.5	∞	123	30.8	13.7	7.70	4.93	3.42	2.51	1.92	1.52	1.23	1.02	0.855	0.628	0.481
50.5	∞	112	28.0	12.4	7.00	4.48	3.11	2.29	1.75	1.38	1.12	0.926	0.778	0.571	0.437
265BT46.3	∞	76.4	19.1	8.49	4.78	3.06	2.12	1.56	1.19	0.944	0.764	0.632	0.531	0.390	0.299
41.0	∞	69.0	17.2	7.67	4.31	2.76	1.92	1.41	1.08	0.852	0.690	0.570	0.479	0.352	0.269
230BT41.1	∞	48.4	12.1	5.38	3.03	1.94	1.34	0.988	0.757	0.598	0.484	0.400	0.336	0.247	0.189
37.3	∞	43.9	11.0	4.88	2.74	1.76	1.22	0.896	0.686	0.542	0.439	0.363	0.305	0.224	0.171
33.6	∞	39.8	9.96	4.43	2.49	1.59	1.11	0.813	0.623	0.492	0.398	0.329	0.277	0.203	0.156
205BT29.9	∞	27.0	6.74	3.00	1.69	1.08	0.749	0.550	0.421	0.333	0.270	0.223	0.187	0.138	
26.9	∞	25.0	6.26	2.78	1.56	1.00	0.695	0.511	0.391	0.309	0.250	0.207	0.174	0.128	
180BT28.4	∞	19.1	4.78	2.12	1.19	0.764	0.531	0.390	0.299	0.236	0.191	0.158	0.133		
25.4	∞	17.1	4.27	1.90	1.07	0.683	0.474	0.348	0.267	0.211	0.171	0.141	0.119		
22.4	∞	15.5	3.86	1.72	0.966	0.618	0.429	0.315	0.241	0.191	0.155	0.128	0.107		
155BT23.1	∞	10.5	2.62	1.16	0.654	0.419	0.291	0.214	0.164	0.129					
20.2	∞	9.26	2.32	1.03	0.579	0.371	0.257	0.189	0.145	0.114					
16.0	∞	7.62	1.91	0.847	0.476	0.305	0.212	0.156	0.119	0.094					
125BT18.7	∞	5.73	1.43	0.637	0.358	0.229	0.159	0.117							
15.7	∞	5.09	1.27	0.565	0.318	0.204	0.141	0.104							
12.9	∞	4.01	1.00	0.445	0.251	0.160	0.111	0.082							
100BT14.9 *	∞	2.94	0.735	0.327	0.184	0.118									
12.7 *	∞	2.55	0.638	0.283	0.159	0.102									
11.2 *	∞	2.20	0.549	0.244	0.137	0.088									
9.1	∞	1.80	0.450	0.200	0.112	0.072									
90BT11.1	∞	1.69	0.423	0.188	0.106	0.068									
9.1	∞	1.35	0.337	0.150	0.084	0.054									
8.1	∞	1.19	0.297	0.132	0.074	0.047									
75BT 9.0	∞	1.05	0.263	0.117	0.066	0.042									
7.0	∞	0.809	0.202	0.090	0.051	0.032									

Note: \* indicates buckling about y-axis for the axis shown in the diagram.

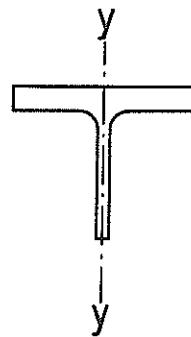


TABLE 4-5(B)  
TEES CUT FROM UNIVERSAL BEAMS  
ELASTIC FLEXURAL BUCKLING LOADS  
buckling about y-axis

Designation	Elastic Flexural Buckling Loads $N_{\text{cm}}$ (MN) Effective Length ( $L_e$ ) in metres														
	0	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	6.0	7.0	8.0	9.0	10.0
305BT62.5	∞	38.8	17.2	9.70	6.21	4.31	3.17	2.43	1.92	1.55	1.08	0.792	0.606	0.479	0.388
56.5	∞	33.8	15.0	8.45	5.41	3.76	2.76	2.11	1.67	1.35	0.939	0.690	0.528	0.417	0.338
50.5	∞	28.9	12.9	7.23	4.63	3.21	2.36	1.81	1.43	1.16	0.803	0.590	0.452	0.357	0.289
265BT46.3	∞	23.5	10.4	5.87	3.76	2.61	1.92	1.47	1.16	0.939	0.652	0.479	0.367	0.290	0.235
41.0	∞	19.9	8.83	4.97	3.18	2.21	1.62	1.24	0.981	0.795	0.552	0.406	0.310	0.245	0.199
230BT41.1	∞	18.4	8.17	4.59	2.94	2.04	1.50	1.15	0.908	0.735	0.511	0.375	0.287	0.227	0.184
37.3	∞	16.4	7.29	4.10	2.62	1.82	1.34	1.02	0.809	0.656	0.455	0.335	0.256	0.202	0.164
33.6	∞	14.4	6.38	3.59	2.30	1.60	1.17	0.897	0.709	0.574	0.399	0.293	0.224	0.177	0.144
205BT25.5	∞	11.9	5.29	2.97	1.90	1.32	0.971	0.743	0.587	0.476	0.330	0.243	0.186	0.147	0.119
26.9	∞	10.1	4.50	2.53	1.62	1.13	0.827	0.633	0.500	0.405	0.281	0.207	0.158	0.125	0.101
180BT28.4	∞	10.9	4.84	2.73	1.74	1.21	0.890	0.681	0.538	0.436	0.303	0.222	0.170	0.135	0.109
25.4	∞	9.47	4.21	2.37	1.52	1.05	0.773	0.592	0.468	0.379	0.263	0.193	0.148	0.117	0.095
22.4	∞	7.99	3.55	2.00	1.28	0.888	0.652	0.499	0.395	0.320	0.222	0.163	0.125	0.099	0.080
155BT23.1	∞	8.89	3.95	2.22	1.42	0.988	0.726	0.556	0.439	0.356	0.247	0.181	0.139	0.110	
20.2	∞	7.55	3.35	1.89	1.21	0.838	0.616	0.472	0.373	0.302	0.210	0.154	0.118	0.093	
16.0	∞	4.36	1.94	1.09	0.698	0.485	0.356	0.273	0.215	0.174	0.121	0.089	0.068	0.054	
125BT18.7	∞	5.59	2.48	1.40	0.894	0.621	0.456	0.349	0.276	0.223	0.155	0.114	0.087		
15.7	∞	4.41	1.96	1.10	0.705	0.490	0.360	0.276	0.218	0.176	0.122	0.090	0.069		
12.9	∞	2.52	1.12	0.629	0.402	0.279	0.205	0.157	0.124	0.101	0.070	0.051	0.039		
100BT14.9*	∞	3.81	1.69	0.951	0.609	0.423	0.311	0.238	0.188	0.152	0.106				
12.7*	∞	3.02	1.34	0.756	0.484	0.336	0.247	0.189	0.149	0.121	0.084				
11.2*	∞	2.71	1.21	0.678	0.434	0.301	0.221	0.170	0.134	0.108	0.075				
9.1	∞	1.12	0.498	0.280	0.179	0.125	0.091	0.070	0.055	0.045	0.031				
90BT11.1	∞	1.20	0.535	0.301	0.193	0.134	0.098								
9.1	∞	0.962	0.428	0.241	0.154	0.107	0.079								
8.1	∞	0.842	0.374	0.210	0.135	0.094	0.069								
75BT 9.0	∞	0.663	0.295	0.166	0.106	0.074	0.054								
7.0	∞	0.488	0.217	0.122	0.078	0.054	0.040								

Note: \* indicates buckling about x-axis for the axis shown in the diagram.

TABLE 4-6(A)  
**TEES CUT FROM UNIVERSAL COLUMNS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about x-axis**

Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres														
	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14
155CT79.0	∞	124	31.0	13.8	7.74	4.95	3.44	2.53	1.93	1.53	1.24	1.02	0.860	0.733	0.632
68.5	∞	105	26.4	11.7	6.59	4.22	2.93	2.15	1.65	1.30	1.05	0.871	0.732	0.624	0.538
59.0	∞	89.1	22.3	9.90	5.57	3.56	2.47	1.82	1.39	1.10	0.891	0.736	0.619	0.527	0.454
48.4	∞	71.9	18.0	7.99	4.49	2.88	2.00	1.47	1.12	0.888	0.719	0.594	0.499	0.426	0.367
125CT44.8	∞	47.8	11.9	5.31	2.99	1.91	1.33	0.975	0.747	0.590	0.478	0.395	0.332	0.283	0.244
36.5	∞	38.3	9.57	4.26	2.39	1.53	1.06	0.782	0.598	0.473	0.383	0.317	0.266	0.227	0.195
100CT29.8	∞	20.1	5.04	2.24	1.26	0.806	0.559	0.411	0.315	0.249	0.201	0.166	0.140		
26.1	∞	17.5	4.37	1.94	1.09	0.699	0.485	0.357	0.273	0.216	0.175	0.144	0.121		
23.1	∞	15.1	3.79	1.68	0.947	0.606	0.421	0.309	0.237	0.187	0.151	0.125	0.105		
75CT18.6	∞	6.92	1.73	0.769	0.432	0.277	0.192	0.141							
15.0	∞	5.54	1.39	0.616	0.346	0.222	0.154	0.113							
11.7	∞	3.93	0.983	0.437	0.246	0.157	0.109	0.080							
50CT 7.4	∞	1.12	0.280	0.124	0.070										

TABLE 4-6(B)  
**buckling about y-axis**

Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Lengths $L_e$ in metres														
	0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	5.5	6.0	6.5	7.0
155CT79.0	∞	118	29.6	13.2	7.40	4.73	3.29	2.42	1.85	1.46	1.18	0.978	0.822	0.700	0.604
68.5	∞	99.9	25.0	11.1	6.24	4.00	2.77	2.04	1.56	1.23	0.999	0.825	0.694	0.591	0.510
59.0	∞	83.2	20.8	9.24	5.20	3.33	2.31	1.70	1.30	1.03	0.832	0.687	0.578	0.492	0.424
48.4	∞	66.5	16.6	7.39	4.16	2.66	1.85	1.36	1.04	0.821	0.665	0.550	0.462	0.394	0.339
125CT44.8	∞	41.0	10.2	4.55	2.56	1.64	1.14	0.836	0.640	0.506	0.410	0.339	0.284	0.242	0.209
36.5	∞	32.1	8.03	3.57	2.01	1.28	0.892	0.655	0.502	0.396	0.321	0.265	0.223	0.190	0.164
100CT29.8	∞	18.6	4.66	2.07	1.16	0.745	0.517	0.380	0.291	0.230	0.186	0.154			
26.1	∞	15.6	3.90	1.73	0.976	0.624	0.434	0.319	0.244	0.193	0.156	0.129			
23.1	∞	13.8	3.45	1.53	0.862	0.551	0.383	0.281	0.215	0.170	0.138	0.114			
75CT18.6	∞	7.18	1.79	0.798	0.449	0.287	0.199	0.147							
15.0	∞	5.58	1.40	0.620	0.349	0.223	0.155	0.114							
11.7	∞	4.64	1.16	0.516	0.290	0.186	0.129	0.095							
50CT 7.4	∞	0.940	0.235	0.104	0.059										

TABLE 4-7(A)  
**TAPER FLANGE BEAMS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about x-axis**

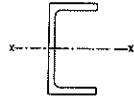
Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Lengths $L_e$ in metres									
	0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0
125 TFB	∞	8.57	2.14	0.952	0.535	0.343	0.238	0.175	0.134	0.106
100 TFB	∞	2.88	0.720	0.320	0.180	0.115				

TABLE 4-7(B)  
**buckling about y-axis**

Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres												
	0	0.25	0.5	0.75	1.0	1.25	1.5	1.75	2.0	2.25	2.5	2.75	3.0
125 TFB	∞	10.6	2.66	1.18	0.665	0.425	0.296	0.217	0.166	0.131	0.106		
100 TFB	∞	2.51	0.628	0.279	0.157	0.100	0.070						

TABLE 4-8(A)

**PARALLEL FLANGE CHANNELS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about x-axis**



Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres													
	0	1	2	3	4	5	6	7	8	9	10	12	14	16
380 PFC	∞	299	74.9	33.3	18.7	12.0	8.32	6.11	4.68	3.70	2.99	2.08	1.53	1.17
300 PFC	∞	143	35.7	15.9	8.93	5.72	3.97	2.92	2.23	1.76	1.43	0.993	0.729	0.558
250 PFC	∞	89.1	22.3	9.90	5.57	3.56	2.47	1.82	1.39	1.10	0.891	0.619	0.455	0.348
230 PFC	∞	52.8	13.2	5.87	3.30	2.11	1.47	1.08	0.825	0.652	0.528	0.367	0.270	0.206
200 PFC	∞	37.7	9.43	4.19	2.36	1.51	1.05	0.770	0.589	0.466	0.377	0.262	0.192	0.147
180 PFC	∞	27.9	6.97	3.10	1.74	1.12	0.775	0.569	0.436	0.344	0.279	0.194	0.142	0.109
150 PFC	∞	16.5	4.12	1.83	1.03	0.658	0.457	0.336	0.257	0.203	0.165	0.114		

TABLE 4-8(B)

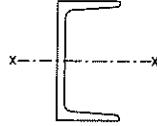
**PARALLEL FLANGE CHANNELS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about y-axis**



Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres														
	0	0.25	0.5	0.75	1.0	1.25	1.5	1.75	2.0	2.25	2.5	3.0	3.5	4.0	4.5
380 PFC	∞	205	51.2	22.7	12.8	8.19	5.69	4.18	3.20	2.53	2.05	1.42	1.04	0.800	0.632
300 PFC	∞	128	31.9	14.2	7.98	5.11	3.55	2.61	2.00	1.58	1.28	0.887	0.652	0.499	0.394
250 PFC	∞	115	28.8	12.8	7.19	4.60	3.20	2.35	1.80	1.42	1.15	0.799	0.587	0.449	0.355
230 PFC	∞	55.6	13.9	6.18	3.48	2.22	1.54	1.13	0.869	0.687	0.556	0.386	0.284	0.217	0.172
200 PFC	∞	52.3	13.1	5.81	3.27	2.09	1.45	1.07	0.817	0.645	0.523	0.363	0.267	0.204	0.161
180 PFC	∞	47.7	11.9	5.30	2.98	1.91	1.32	0.972	0.745	0.588	0.477	0.331	0.243	0.186	0.147
150 PFC	∞	40.6	10.2	4.51	2.54	1.62	1.13	0.829	0.634	0.501	0.406	0.282	0.207	0.159	0.125

TABLE 4-9(A)

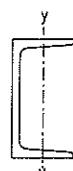
**TAPER FLANGE CHANNELS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about x-axis**



Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres									
	0	1	2	3	4	5	6	7	8	
125 TFC	∞	8.36	2.09	0.929	0.523	0.335	0.232	0.171	0.131	0.103
100 TFC	∞	3.71	0.929	0.413	0.232	0.149	0.103			
75 TFC	∞	1.42	0.356	0.158	0.089					

TABLE 4-9(B)

**TAPER FLANGE CHANNELS**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about y-axis**



Designation	Elastic Flexural Buckling Loads $N_{om}$ (MN) Effective Length ( $L_e$ ) in metres											
	0	0.25	0.5	0.75	1.0	1.25	1.5	1.75	2.0	2.25		
125 TFC	∞	19.5	4.88	2.17	1.22	0.780	0.542	0.398	0.305	0.241	0.195	0.135
100 TFC	∞	8.22	2.05	0.913	0.514	0.329	0.228	0.168	0.128			
75 TFC	∞	3.62	0.904	0.402	0.226	0.145	0.100	0.074				

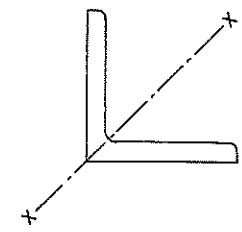
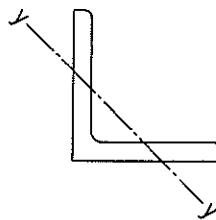


TABLE 4-10(A)  
**EQUAL ANGLES**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about x-axis**

Designation	Elastic Flexural Buckling Loads $N_{\text{om}}$ (MN) for Effective Lengths ( $L_e$ ) in metres										
	0	0.5	1.0	1.5	2.0	2.5	3.0	4.0	5.0	6.0	8.0
200x200x26EA	∞	448	112	49.8	28.0	17.9	12.5	7.01	4.48	3.11	1.75
	20EA	∞	361	90.2	40.1	22.5	14.4	10.0	5.63	3.61	2.50
	18EA	∞	329	82.3	36.6	20.6	13.2	9.15	5.15	3.29	2.29
	16EA	∞	297	74.3	33.0	18.6	11.9	8.25	4.64	2.97	2.06
	13EA	∞	247	61.7	27.4	15.4	9.87	6.35	3.85	2.47	1.71
150x150x19EA	∞	139	34.6	15.4	8.66	5.54	3.85	2.17	1.39	0.962	0.541
	16EA	∞	119	29.7	13.2	7.43	4.76	3.30	1.86	1.19	0.826
	12EA	∞	93.7	23.4	10.4	5.85	3.75	2.60	1.46	0.937	0.650
	10EA	∞	75.9	19.0	8.43	4.74	3.03	2.11	1.19	0.759	0.527
125x125x16EA	∞	66.6	16.6	7.40	4.16	2.66	1.85	1.04	0.666	0.462	0.260
	12EA	∞	52.8	13.2	5.87	3.30	2.11	1.47	0.825	0.528	0.367
	10EA	∞	43.0	10.7	4.78	2.69	1.72	1.19	0.671	0.430	0.298
	8EA	∞	35.9	8.98	3.99	2.24	1.44	0.998	0.561	0.359	0.249
100x100x12EA	∞	26.0	6.50	2.89	1.63	1.04	0.723	0.406	0.260	0.181	
	10EA	∞	21.3	5.33	2.37	1.33	0.853	0.592	0.333	0.213	0.148
	8EA	∞	17.9	4.47	1.99	1.12	0.716	0.497	0.280	0.179	0.124
	6EA	∞	14.1	3.51	1.56	0.878	0.562	0.390	0.220	0.141	0.098
90x 90x10EA	∞	15.3	3.82	1.70	0.954	0.611	0.424	0.238	0.153		
	8EA	∞	12.8	3.21	1.43	0.803	0.514	0.357	0.201	0.128	
	6EA	∞	10.1	2.53	1.12	0.632	0.404	0.281	0.158	0.101	
75x 75x10EA	∞	8.53	2.13	0.947	0.533	0.341	0.237	0.133			
	8EA	∞	7.21	1.80	0.801	0.451	0.288	0.200	0.113		
	6EA	∞	5.70	1.43	0.634	0.356	0.228	0.158	0.089		
	5EA	∞	4.45	1.11	0.494	0.278	0.178	0.124	0.069		
65x 65x10EA	∞	5.46	1.36	0.606	0.341	0.218	0.152				
	8EA	∞	4.65	1.16	0.517	0.291	0.186	0.129			
	6EA	∞	3.72	0.930	0.413	0.232	0.149	0.103			
	5EA	∞	2.93	0.733	0.326	0.183	0.117	0.062			
55x 55x 6EA	∞	2.19	0.548	0.243	0.137						
	5EA	∞	1.74	0.434	0.193	0.109					
50x 50x 8EA	∞	2.00	0.500	0.222	0.125						
	6EA	∞	1.62	0.404	0.180	0.101					
	5EA	∞	1.29	0.321	0.143						
	3EA	∞	0.868	0.217	0.096						
45x 45x 6EA	∞	1.15	0.288	0.128							
	5EA	∞	0.920	0.230	0.102						
	3EA	∞	0.624	0.156	0.069						
40x 40x 6EA	∞	0.787	0.197								
	5EA	∞	0.632	0.158							
	3EA	∞	0.430	0.108							
30x 30x 6EA	∞	0.306	0.076								
	5EA	∞	0.249	0.062							
	3EA	∞	0.172	0.043							
25x 25x 6EA	∞	0.166	0.041								
	5EA	∞	0.137	0.034							
	3EA	∞	0.095	0.024							

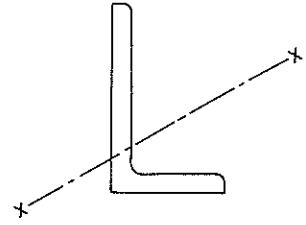
TABLE 4-10(B)

**EQUAL ANGLES**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about y-axis**



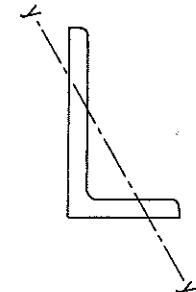
Designation	Elastic Flexural Buckling Loads $N_{\text{om}}$ (MN) Effective Lengths ( $L_e$ ) in metres										
	0	0.25	0.5	0.75	1.0	1.25	1.5	2.0	2.5	3.0	4.0
200x200x26EA	∞	471	118	52.3	29.4	18.8	13.1	7.36	4.71	3.27	1.84
20EA	∞	374	93.6	41.6	23.4	15.0	10.4	5.85	3.74	2.60	1.46
18EA	∞	341	85.3	37.9	21.3	13.6	9.47	5.33	3.41	2.37	1.33
16EA	∞	307	76.8	34.1	19.2	12.3	8.53	4.80	3.07	2.13	1.20
13EA	∞	255	63.8	28.4	16.0	10.2	7.09	3.99	2.55	1.77	0.997
150x150x19EA	∞	145	36.3	16.1	9.07	5.81	4.03	2.27	1.45	1.01	0.567
16EA	∞	123	30.9	13.7	7.71	4.94	3.43	1.93	1.23	0.857	0.482
12EA	∞	96.7	24.2	10.7	6.04	3.87	2.68	1.51	0.967	0.671	0.378
10EA	∞	78.4	19.6	8.71	4.90	3.13	2.18	1.22	0.784	0.544	0.306
125x125x16EA	∞	69.6	17.4	7.73	4.35	2.78	1.93	1.09	0.696	0.483	0.272
12EA	∞	54.5	13.6	6.06	3.41	2.18	1.51	0.852	0.545	0.379	0.213
10EA	∞	44.2	11.1	4.91	2.76	1.77	1.23	0.691	0.442	0.307	0.173
8EA	∞	37.0	9.24	4.11	2.31	1.48	1.03	0.577	0.370	0.257	0.144
100x100x12EA	∞	27.1	6.77	3.01	1.69	1.08	0.752	0.423	0.271	0.188	0.106
10EA	∞	22.0	5.49	2.44	1.37	0.879	0.610	0.343	0.220	0.153	0.086
8EA	∞	18.4	4.60	2.04	1.15	0.735	0.511	0.287	0.184	0.128	0.072
6EA	∞	14.5	3.61	1.61	0.903	0.578	0.402	0.226	0.145	0.100	0.056
90x 90x10EA	∞	15.8	3.95	1.76	0.988	0.632	0.439	0.247	0.158	0.110	
8EA	∞	13.2	3.31	1.47	0.828	0.530	0.368	0.207	0.132	0.092	
6EA	∞	10.4	2.61	1.16	0.652	0.417	0.290	0.163	0.104	0.072	
75x 75x10EA	∞	8.92	2.23	0.991	0.558	0.357	0.248	0.139			
8EA	∞	7.49	1.87	0.832	0.468	0.299	0.208	0.117			
6EA	∞	5.91	1.48	0.657	0.369	0.236	0.164	0.092			
5EA	∞	4.63	1.16	0.515	0.290	0.185	0.129	0.072			
65x 65x10EA	∞	5.78	1.44	0.642	0.361	0.231	0.160				
8EA	∞	4.85	1.21	0.539	0.303	0.194	0.135				
6EA	∞	3.85	0.962	0.427	0.240	0.154	0.107				
5EA	∞	3.03	0.757	0.337	0.189	0.121	0.084				
55x 55x 6EA	∞	2.28	0.571	0.254	0.143						
5EA	∞	1.80	0.451	0.200	0.113						
50x 50x 8EA	∞	2.13	0.533	0.237	0.133						
6EA	∞	1.69	0.423	0.188	0.106						
5EA	∞	1.34	0.335	0.149	0.084						
3EA	∞	0.913	0.228	0.101	0.057						
45x 45x 6EA	∞	1.21	0.303	0.135							
5EA	∞	0.956	0.239	0.106							
3EA	∞	0.650	0.163	0.072							
40x 40x 6EA	∞	0.836	0.209	0.093							
5EA	∞	0.660	0.165	0.073							
3EA	∞	0.450	0.112	0.050							
30x 30x 6EA	∞	0.337	0.084								
5EA	∞	0.265	0.066								
3EA	∞	0.181	0.045								
25x 25x 6EA	∞	0.189	0.047								
5EA	∞	0.148	0.037								
3EA	∞	0.101	0.025								

TABLE 4-11(A)  
**UNEQUAL ANGLES**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about x-axis**



Designation	Elastic Flexural Buckling Loads $N_{\text{om}}$ (MN) Effective Lengths ( $L_e$ ) in metres										
	0	0.5	1.0	1.5	2.0	2.5	3.0	4.0	5.0	6.0	8.0
150x100x12UA 10UA	∞	59.3	14.8	6.59	3.71	2.37	1.65	0.927	0.593	0.412	0.232
	∞	48.2	12.1	5.36	3.01	1.93	1.34	0.753	0.482	0.335	0.188
150x 90x16UA 12UA 10UA 8UA	∞	69.5	17.4	7.72	4.34	2.78	1.93	1.09	0.695	0.482	0.271
	∞	55.0	13.7	6.11	3.44	2.20	1.53	0.859	0.550	0.382	0.215
	∞	44.7	11.2	4.97	2.79	1.79	1.24	0.699	0.447	0.311	0.175
	∞	37.4	9.34	4.15	2.34	1.49	1.04	0.584	0.374	0.259	0.146
125x 75x12UA 10UA 8UA 6UA	∞	30.9	7.72	3.43	1.93	1.24	0.858	0.483	0.309	0.214	0.121
	∞	25.2	6.31	2.80	1.58	1.01	0.701	0.394	0.252	0.175	0.099
	∞	21.2	5.29	2.35	1.32	0.846	0.588	0.331	0.212	0.147	0.083
	∞	16.6	4.15	1.84	1.04	0.664	0.461	0.259	0.166	0.115	0.065
100x 75x10UA 8UA 6UA	∞	14.9	3.72	1.65	0.931	0.596	0.414	0.233	0.149	0.103	
	∞	12.5	3.13	1.39	0.783	0.501	0.348	0.196	0.125	0.087	
	∞	9.87	2.47	1.10	0.617	0.395	0.274	0.154	0.099	0.068	
75x 50x 8UA 6UA 5UA	∞	4.63	1.16	0.514	0.289	0.185	0.129	0.072			
	∞	3.70	0.925	0.411	0.231	0.148	0.103	0.058			
	∞	2.92	0.729	0.324	0.182	0.117	0.081	0.046			
65x 50x 8UA 6UA 5UA	∞	3.32	0.831	0.369	0.208	0.133	0.092				
	∞	2.67	0.667	0.296	0.167	0.107	0.074				
	∞	2.11	0.527	0.234	0.132	0.084	0.059				

TABLE 4-11(B)  
**UNEQUAL ANGLES**  
**ELASTIC FLEXURAL BUCKLING LOADS**  
**buckling about y-axis**



Designation	Elastic Flexural Buckling Loads $N_{\text{om}}$ (MN) Effective Lengths ( $L_e$ ) in metres										
	0	0.25	0.5	0.75	1.0	1.25	1.5	2.0	2.5	3.0	4.0
150x100x12UA 10UA	∞	42.5	10.6	4.73	2.66	1.70	1.18	0.665	0.425	0.295	0.166
	∞	34.6	8.64	3.84	2.16	1.38	0.960	0.540	0.346	0.240	0.135
150x 90x16UA 12UA 10UA 8UA	∞	41.8	10.5	4.64	2.61	1.67	1.16	0.653	0.418	0.290	0.163
	∞	32.9	8.22	3.65	2.06	1.32	0.914	0.514	0.329	0.228	0.128
	∞	26.8	6.69	2.97	1.67	1.07	0.743	0.418	0.268	0.186	0.105
	∞	22.4	5.61	2.49	1.40	0.897	0.623	0.350	0.224	0.156	0.088
125x 75x12UA 10UA 8UA 6UA	∞	18.5	4.62	2.05	1.16	0.739	0.513	0.289	0.185	0.128	
	∞	15.0	3.76	1.67	0.940	0.602	0.418	0.235	0.150	0.104	
	∞	12.6	3.15	1.40	0.789	0.505	0.351	0.197	0.126	0.088	
	∞	9.94	2.49	1.10	0.621	0.398	0.276	0.155	0.099		
100x 75x10UA 8UA 6UA	∞	12.7	3.17	1.41	0.793	0.507	0.352	0.198	0.127		
	∞	10.6	2.66	1.18	0.665	0.425	0.295	0.166	0.106		
	∞	8.39	2.10	0.932	0.524	0.335	0.233	0.131	0.084		
75x 50x 8UA 6UA 5UA	∞	3.34	0.836	0.372	0.209	0.134	0.093				
	∞	2.66	0.666	0.296	0.166	0.106	0.074				
	∞	2.11	0.527	0.234	0.132	0.084	0.058				
65x 50x 8UA 6UA 5UA	∞	2.96	0.739	0.328	0.185	0.118					
	∞	2.35	0.587	0.261	0.147	0.094					
	∞	1.86	0.464	0.206	0.116	0.074					

**PART 5 MEMBERS SUBJECT TO BENDING**

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**TABLES 5.3-1 to 5.3-11**

Design Moment Capacities for Members without Full Lateral Restraint.....	5-40
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**PART 5 MEMBERS SUBJECT TO BENDING****5.1 Maximum Design Loads for Beams with Full Lateral Restraint Subject to Uniformly Distributed Loading**

**NOTE: BEAM SELF WEIGHT:** For Tables 5.1-1 to 5.1-13, the self weight of the beam has NOT been deducted. The designer must include the self weight as part of the dead load when determining the maximum design load  $W_L^*$  or  $W_S^*$ .

Tables 5.1-1 to 5.1-13 give values of the maximum design loads for single-span simply-supported beams with full lateral restraint subject to uniformly distributed loads as shown in Figure 5.1.

**Designers should assess maximum design loads for the strength and serviceability separately as different load combinations apply to these cases (AS 1170).**

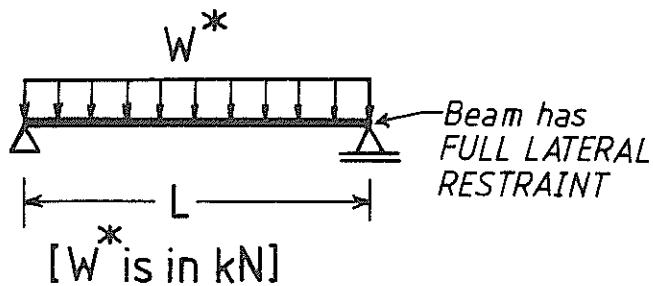


Figure 5.1

Tables 5.1-1 to 5.1-13 also list the maximum segment length for full lateral restraint (FLR) for each section.

For angles subject to bending, reference should be made to Part 8 of this publication.

### 5.1.1 Strength Limit State Design

For the beam configuration in Figure 5.1, the maximum strength limit state design load ( $W_L^*$ ) is the *lesser* of the maximum design load ( $W_{L1}^*$ ) associated with the design section moment capacity ( $\phi M_{sx}$ ) and the maximum design load ( $W_{L2}^*$ ) associated with the design shear capacity ( $\phi V_u$ ).

The designer must ensure that the strength limit state design load ( $W_L^*$ ) is less than or equal to the maximum design load  $W_L^*$ , i.e.

$$W^* \leq W_L^*$$

where  $W_L^* = \min [W_{L1}^*; W_{L2}^*]$

$W_{L1}^*$  and  $W_{L2}^*$  are listed in **bold** within the first row of entries for each section in Tables 5.1-1 to 5.1-13.

For the beam configuration shown in Figure 5.1, the strength of the beam is not controlled by the interaction of bending moment and shear force (Clause 5.12 of AS 4100).

#### 5.1.1.1 $W_{L1}^*$ - based on Design Moment Capacity

The derivation of the design section moment capacity is given in Section 5.2.2.1, and listed in Tables 5.2-1 to 5.2-11.

For a single-span simply-supported beam subject to uniformly distributed loading (see Figure 5.1), the maximum bending moment ( $M_{max}$ ) is given by:

$$M_{max} = \frac{WL}{8}$$

where  $W$  = total load on the beam  
 $L$  = length of the beam

The design moment capacity for the beam in Figure 5.1 is  $\phi M_{sx}$ . Therefore, substituting  $\phi M_{sx}$  for  $M_{max}$ , and rearranging the above equation gives:

$$W_{L1}^* = \frac{8\phi M_{sx}}{L}$$

where  $W_{L1}^*$  is the *Maximum Design Load* based on the design moment capacity of the beam.

### 5.1.1.2 $W_{L2}^*$ - based on Design Shear Capacity

The derivation of the design shear capacity ( $\phi V_v$ ) is given in Section 5.2.2.3 and listed in Tables 5.2-1 to 5.2-11.

For a single-span simply-supported beam subject to uniformly distributed loading (see Figure 5.1), the maximum shear force ( $V_{max}$ ) is given by:

$$V_{max} = \frac{W}{2}$$

Therefore, substituting  $\phi V_v$  for  $V_{max}$  and rearranging the equation gives:

$$W_{L2}^* = 2\phi V_v$$

where  $W_{L2}^*$  is the *Maximum Design Load* based on the design shear capacity of the beam.

## 5.1.2 Serviceability Limit State Design

The value of serviceability load ( $W_S^*$ ) given in the tables is the lesser of the maximum design load ( $W_{L1}^*$ ) which will achieve a **calculated total elastic deflection** of  $L / 250$  (where  $L$  is the span of the beam) and the load at which first yield occurs ( $W_{YL}^*$ ).

### $W_{S1}^*$ - based on a Deflection Limit of $L / 250$ (simply supported beam)

The maximum *elastic* deflection ( $\Delta_{max}$ ) of the beam shown in Figure 5.1 is given by:

$$\Delta_{max} = \frac{5WL^3}{384EI_x}$$

where  $E$  =  $200 \times 10^3$  MPa  
 $I_x$  = second moment of area about the major principal  $x$ -axis

Therefore, substituting  $\Delta_{max} = L / 250$  and rearranging the equation gives the maximum design load for serviceability based on deflection ( $W_{S1}^*$ ):

$$W_{S1}^* = \frac{384EI_x}{1250L^2}$$

For deflection limits other than span / 250, the value of the maximum design load based on another deflection limit ( $W_{S2}^*$ ) may be calculate using the principles outlined above.

## **$W_{YL}^*$ - based on first yield load**

The load at which first yield occurs in the member is given by

$$W_{YL}^* = \frac{8Z_{x\min} f_y}{L}$$

The serviceability limit state maximum design load ( $W_S^*$ ) is given by:

$$W_S^* = \min [W_{S1}^* ; W_{YL}^*]$$

$W_S^*$  is listed in *italics* within the second row for each section in Tables 5.1-1 to 5.1-13. Serviceability loads governed by yielding are shaded.

## **5.1.3 Full Lateral Restraint**

Full lateral restraint may be achieved for a beam by: (a) continuous lateral restraint, or (b) full or partial restraint provided at sufficient locations along the beam. The distance between the locations in (b) is termed the segment length. The maximum value of segment length to maintain the full lateral restraint condition is generally listed under "FLR" in Tables 5.1-1 to 5.1-13.

Formulae for calculating FLR are given in Clause 5.3.2.4 of AS 4100 and Section 5.2.2.2. For the beam configuration shown in Figure 5.1, the ratio  $\beta_m$  is equal to -0.8.

## **5.1.4 Additional Design Checks**

Where loads are transmitted into the webs at supports or at load points, the capacity of the web to resist such forces should be checked in accordance with Section 5.2.2.4, and the values of these web capacities listed in Tables 5.2-1 to 5.2-11.

### 5.1.5 Other Load Conditions

The values given in Tables 5.1-1 to 5.1-13 are for single span, simply supported beams subject to uniformly distributed loads (Figure 5.1). However, the information presented in these tables may be used for beams with full lateral restraint and other loading situations using the equivalent uniform design loads given in Table 5.1 and the following procedure:

- (1) Calculate the equivalent uniformly distributed maximum design load for moment ( $W_{EM}^*$ ) using Table 5.1.
- (2) Based on  $W_{EM}^*$  select a section with an adequate maximum design load ( $W_{L1}^*$ ) associated with the design moment capacity from Tables 5.1-1 to 5.1-13.
- (3) Calculate equivalent uniformly distributed maximum design load for shear ( $W_{EV}^*$ ) using Table 5.1.
- (4) Check that the section selected in (2) has an adequate maximum design load ( $W_{L2}^*$ ) associated with the design shear capacity to resist  $W_{EV}^*$ . If not, select a new section size which can resist  $W_{EV}^*$ .
- (5) Check shear and bending interaction in accordance with Section 5.2.2.3. A check is not necessary if  $V^* < 0.6 \phi V_v$  or  $M^* < 0.75 \phi M_s$ .
- (6) Calculate equivalent uniformly distributed serviceability load ( $W_{ES}^*$ ) from Table 5.1.
- (7) Check that the section selected in (4) has an adequate maximum serviceability design load ( $W_{S1}^*$ ) to resist  $W_{ES}^*$ . If not, select a new section size which can resist  $W_{ES}^*$ .

This procedure is shown in Example 2 of Section 5.1.6.

### 5.1.6 Examples

1. A simply supported beam of 4 metres span is subjected to uniformly distributed loads of:

$$G \text{ (Dead Load)} = 50 \text{ kN} \quad (\text{total load})$$

$$Q \text{ (Live Load)} = 64 \text{ kN} \quad (\text{short term total load})$$

The beam is continuously laterally restrained. The total deflection of the beam under serviceability load must not exceed  $L / 250$ . Select an appropriate Universal Beam section in Grade 300 steel to resist these loadings.

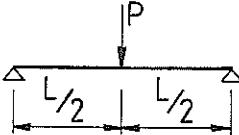
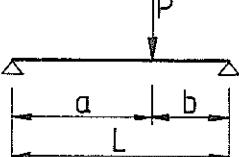
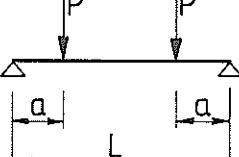
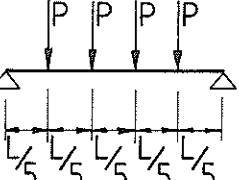
Solution:

- (a) Calculation of maximum design loads:

$$\begin{aligned} \text{Strength limit state} \quad W_L^* &= 1.25G + 1.5Q \\ &= 159 \text{ kN} \end{aligned}$$

$$\begin{aligned} \text{Serviceability limit state} \quad W_S^* &= G + 0.7Q \quad (\text{short term live load}) \\ &= 94.8 \text{ kN} \end{aligned}$$

TABLE 5.1: Table of Equivalent Uniform Design Loads

Loading	Equivalent Strength Maximum Design Loads		Equivalent Serviceability Maximum Design Load $W_{ES}^*$
	Moment $W_{EM}^*$	Shear $W_{EV}^*$	
	$2P$	$P$	$\frac{8P}{5}$
 for $a > b$	$\frac{8abP}{L^2}$	$\frac{2Pa}{L}$	$\frac{8P}{5} \left[ 3\left(\frac{a}{L}\right) - 4\left(\frac{a}{L}\right)^3 \right]$ at midspan
	$\frac{8aP}{L}$	$2P$	$\frac{16P}{5} \left[ 3\left(\frac{a}{L}\right) - 4\left(\frac{a}{L}\right)^3 \right]$
	$4P$	$3P$	$\frac{19P}{5}$
	$\frac{24P}{5}$	$4P$	$\frac{3024P}{625}$

(b) Use of the Tables:

*Strength Limit State* - Select a section from the Tables such that the maximum design loads  $W_{L1}^*$  and  $W_{L2}^*$  are greater than or equal to  $W_L^*$ . It can be seen from Table 5.1-5(2) that for a 250UB25.7 - Grade 300, the **maximum** design loads are:

$$W_{L1}^* = 184 \text{ kN}$$

$$W_{L2}^* = 429 \text{ kN}$$

$$\therefore W_L^* = \min [W_{L1}^*, W_{L2}^*]$$

$$= 184 \text{ kN} \quad (> 159 \text{ kN})$$

Therefore, a 250UB25.7 satisfies the strength limit state.

*Serviceability Limit State* - From Table 5.1-5(2) it can be seen that for a 250UB25.7 - Grade 300, the serviceability load for a deflection limit of  $L/250$  is:

$$W_S^* = 136 \text{ kN} \quad (> 94.8 \text{ kN})$$

2. A beam which is simply supported has a span of 6.0 metres with full lateral restraint. The beam is subjected to nominal central dead and short term live loads of 40 kN and 25 kN respectively. Design a suitable Universal Beam in Grade 300 steel with a limit on deflection of span / 250.

Solution:

- (1) Calculate equivalent uniformly distributed maximum design load for moment ( $W_{EM}^*$ )

From Table 5.1  $W_{EM}^*$  associated with the central dead and live loads is:

$$W_{EM}^* = 2P$$

$$= 2(1.25 \times 40 + 1.5 \times 25)$$

$$= 175 \text{ kN}$$

- (2) Based on  $W_{EM}^*$  select a section with an adequate maximum design load ( $W_{L1}^*$ ) based on design moment capacity

From Table 5.1-5(2), a 310UB32.0 has adequate maximum design load with  $W_{L1}^* = 179 \text{ kN}$ .

- (3) Calculate equivalent uniformly distributed maximum design load for shear ( $W_{EV}^*$ )

From Table 5.1  $W_{EV}^*$  for the central dead and live loads is:

$$W_{EV}^* = P$$

$$= 1.25 \times 40 + 1.5 \times 25$$

$$= 87.5 \text{ kN}$$

- (4) Check that the section selected in Step 2 has an adequate maximum design load ( $W_{L2}^*$ ) based on shear capacity

From Table 5.1-5(2), a 310UB32.0 has adequate maximum design load with  $W_{L2}^* = 566 \text{ kN}$ .

- (5) Check if a shear and bending interaction check is necessary.

$$W_{L2}^* = 566 \text{ kN for a 250UB25.7.} \quad (\text{Table 5.1-5(2)})$$

$$\phi V_v = 283 \text{ kN} \quad (\text{Table 5.2-5})$$

$$0.6 \phi V_v = 0.6 \times 283$$

$$= 170 \text{ kN}$$

$$> 43.8 \text{ kN} \quad (V^* = W_{Ev}^* / 2)$$

Therefore no shear and bending interaction check is necessary.

- (6) Calculate equivalent uniformly distributed serviceability load ( $W_{Es}^*$ )

From Table 5.1  $W_{Es}^*$  for the central dead and live loads is:

$$\begin{aligned} W_{Es}^* &= \frac{8P}{5} \\ &= \frac{8}{5} (40 + 0.7 \times 25) \\ &= 92 \text{ kN} \end{aligned}$$

- (7) From Table 5.1-5(2), a 310UB32.0 has adequate maximum serviceability design load  $W_{S1}^* = 109 \text{ kN.}$

∴ Adopt a 310UB32.0 - Grade 300 section.

Note: In this example the self weight of the beam is not taken into consideration. The calculation should be repeated to include self weight if significant.

## 5.2 Design Section Moment and Web Capacities

### 5.2.1 Scope

Tables 5.2-1 to 5.2-11 contain values of design section moment capacities about the principal x- & y-axes ( $\phi M_{sx}$ ,  $\phi M_{sy}$ ) and the design shear capacity ( $\phi V_v$ ) for shear forces acting in the principal y-axis direction (note that such a shear force is related to bending about the x-axis). Design section moment capacities are given for I- sections with holes in the tension flange ( $\phi M'_{sx}$ ,  $\phi M''_{sx}$ ). Standard bolt hole diameters and gauge lengths are used on the flanges (refer to Tables 3.1-15(1) to 3.1-18 for details). These values provide basic information necessary for checking shear/bending interaction.

Also listed are the maximum segment lengths for full lateral restraint (FLR) to ensure that the maximum design section moment capacity can be achieved for bending about the x-axis. The Tables give values of design web bearing yield capacity per unit length ( $\phi R_{by}/b_{bf}$ ) and design web bearing buckling capacity per unit length ( $\phi R_{bb}/b_b$ ) for all sections except Structural Tees.

### 5.2.2 Method

#### 5.2.2.1 Design Section Moment Capacity

The design section moment capacity ( $\phi M_s$ ) is determined from Clauses 5.1 and 5.2.1 of AS 4100 using

$$\phi M_s = \phi f_y Z_e$$

where  $\phi = 0.9$  (Table 3.4 of AS 4100)

$f_y$  = yield stress used in design (for a section where the web and flange yield stresses ( $f_{yw}$  &  $f_{yt}$ ) are different the *lower* value is used)

$Z_e$  = effective section modulus (Section 3.2.2.2)

Design section moment capacities are listed for bending about both principal axes. For bending about the x-axis, the design member moment capacity ( $\phi M_b$ ) equals the design section moment capacity for members which are fully restrained against flexural-torsional buckling. For bending about the y-axis, flexural-torsional buckling does not occur, and the design member moment capacity equals the design section moment capacity.

For asymmetric sections (Structural Tees, Channels and Angles) bending about the asymmetric axis, the value of the design section moment capacity depends on the direction of the bending moment.

#### 5.2.2.2 Segment Length for Full Lateral Restraint (FLR)

For I- sections and Channels, a segment with full or partial restraints at each end may be considered to have full lateral restraint if its length satisfies Clause 5.3.2.4 of AS 4100, i.e.

$$FLR \leq r_y (K_1 + K_2 \beta_m) \sqrt{\left(\frac{250}{f_y}\right)}$$

where FLR = maximum segment length for full lateral restraint

$K_1$  = 80 (for equal flanged I- sections) or 60 (for equal flanged Channels)

$K_2$  = 50 (for equal flanged I- sections) or 40 (for equal flanged Channels)

$$r_y = \sqrt{\left(\frac{I_y}{A_g}\right)}$$

The FLR values listed in Tables 5.2-1 to 5.2-11 are calculated using  $\beta_m = -1.0$  which is the most conservative case. However  $\beta_m = -0.8$  may be used for segments with transverse loads (as in the case of Tables 5.1-1 to 5.1-13), or  $\beta_m$  may be taken as the ratio of the smaller to larger end moments in the length ( $L$ ) for segments without transverse loads (positive when the segment is bent in reverse curvature).

For Structural Tees cut from Universal Beams the values of maximum segment length have been determined by calculating the maximum effective length for which the design member moment capacity equals the design section moment capacity assuming  $\alpha_m = 1.0$ . For Tees cut from Universal Beams bending about the  $x$ -axis that causes compression in the stem, there is no effective length for which the design member moment capacity equals the design section moment capacity. Structural Tees cut from Universal Columns and some BTs bent about the  $y$ -axis do not buckle laterally and hence no value of effective length is given.

### 5.2.2.3 Design Shear Capacity of a Web

For I-sections and channels the shear stress distribution in the web is approximately uniform and the design shear capacity  $\phi V_v$  can be taken as (Clause 5.11 of AS 4100):

$$\phi V_v = \phi(0.6 f_{yw} A_w) \quad \text{for } \frac{d_1}{t_w} \sqrt{\left(\frac{f_{yw}}{250}\right)} \leq 82$$

$$\phi V_v = \phi(0.6 f_{yw} A_w) \left[ \frac{82}{\left( \frac{d_1}{t_w} \right) \sqrt{\left( \frac{f_{yw}}{250} \right)}} \right]^2 \quad \text{for } \frac{d_1}{t_w} \sqrt{\left( \frac{f_{yw}}{250} \right)} > 82$$

where  $\phi = 0.9$

$d_1$  = clear depth of the web

$A_w$  = area of the web  $= d t_w$  (for hot-rolled sections)

$= d_1 t_w$  (for welded sections)

$f_{yw}$  = yield stress of the web

For Structural Tees the shear stress distribution is non-uniform and the web shear capacity is given by

$$\phi V_v = \min \left[ \phi V_u, \frac{2\phi V_u}{0.9 + \left( \frac{f_{vm}^*}{f_{va}^*} \right)} \right]$$

where  $f_{vm}^*$ ,  $f_{va}^*$  = the maximum and average design shear stresses determined from an elastic analysis.

$\phi V_u$  = the design shear capacity assuming a uniform shear stress distribution

For interaction of shear and bending the design shear capacity in the presence of bending moment ( $\phi V_{vm}$ ) is

$$\phi V_{vm} = \phi V_v \quad \text{for } M^* \leq 0.75 \phi M_s$$

$$\text{or } \phi V_{vm} = \phi V_v \left[ 2.2 - \left( \frac{1.6M^*}{\phi M_s} \right) \right] \quad \text{for } 0.75 \phi M_s \leq M^* \leq \phi M_s$$

Interaction need only be checked if  $V^* \geq 0.6 (\phi V_v)$  and  $M^* \geq 0.75 (\phi M_s)$ .

**Note for Welded Sections:** Clause 9.2 of AS 3679.2 states that the flange-web welded joint for welded sections shall develop the minimum tensile strength of the web (for  $t_w \leq 16$  mm), or the minimum tensile strength of a 16 mm web (for  $t_w > 16$  mm), therefore

$$\begin{aligned}\phi V_{wj} &= \phi f_u t_w && (\text{for } t_w \leq 16 \text{ mm}) \\ &= 16 \phi f_u && (\text{for } t_w > 16 \text{ mm})\end{aligned}$$

where  $\phi = 0.8$  (Table 3.4 of AS 4100)  
 $\phi V_{wj}$  = the design capacity of the welded joint  
 $t_w$  = web thickness

For some Welded Columns the design shear capacity ( $\phi V_v$ ) is governed by the capacity of the welded joint.

The adjacent table lists the design capacity of the welded joints for the range of web thicknesses of Welded Beams and Welded Columns.

Steel Grade (AS 3679.2)	Web Thickness $t_w$	Web Tensile Strength $f_u$	Design Capacity of Welded Joint $\phi V_{wj}$
	mm	MPa	kN/mm
300	10	430	3.44
300	12	430	4.13
300	$\geq 16$	430	5.50
400	10	480	3.84
400	12	480	4.61
400	$\geq 16$	480	6.14

Note:  $\phi V_{wj}$  includes the welds on **both** sides of the web.

#### 5.2.2.4 Design Web Bearing Capacities

The design bearing yield capacity of a web ( $\phi R_{by}$ ) is calculated in accordance with Clause 5.13.3 of AS 4100 by

$$\frac{\phi R_{by}}{b_{bf}} = \phi(1.25 t_w f_y w)$$

where  $b_{bf}$  is shown in Figure 5.1, and  $\phi = 0.9$  (Table 3.4 of AS 4100).

The design bearing buckling capacity ( $\phi R_{bb}$ ) is determined using Clause 5.13.4 of AS 4100. This is equal to the design axial compression capacity of a member with area  $t_w b_b$  and slenderness,  $L_e/r = 2.5 d_1/t_w$  with  $\alpha_b = 0.5$  and  $k_f = 1.0$  (Section 6 of AS 4100).

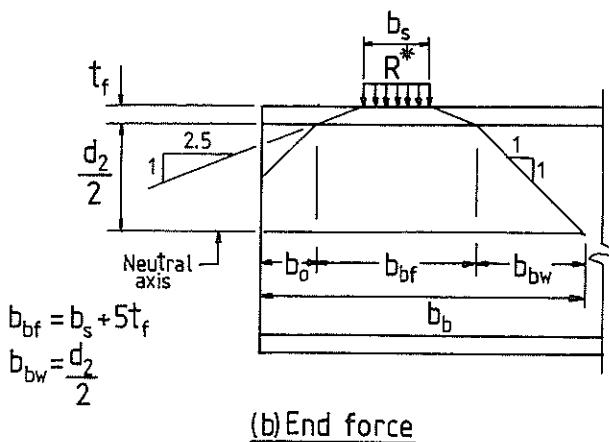
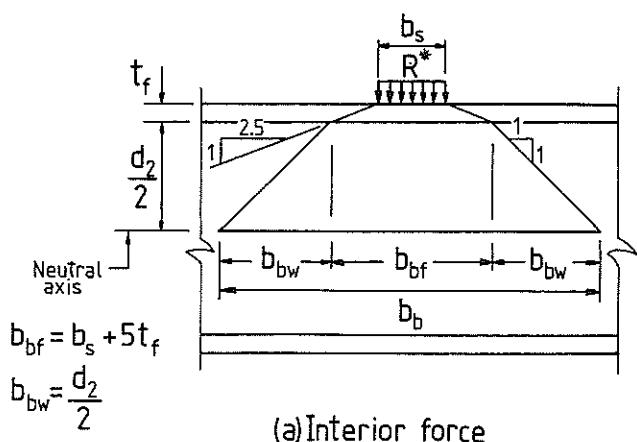
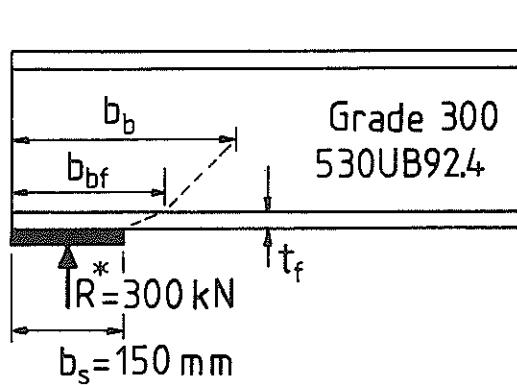


Figure 5.1  $b_{bf}$  and  $b_b$  for Dispersions of Force Through Flange and Web  
 (Reproduced by courtesy of Standards Australia)

### 5.2.3 Example

A 530UB92.4 - Grade 300 steel beam is subjected to an end reaction of  $R^* = 300$  kN. Check the bearing capacity of this section to resist this force.



Solution:

(1) Check shear capacity

$$\begin{aligned} V^* &= R^* = 300 \text{ kN} \\ \phi V_v &= 939 \text{ kN} \quad (\text{Table 5.2-5}) \\ &> V^* \therefore \text{O.K.} \end{aligned}$$

(2) Check bearing capacity

(a) Design bearing yield capacity ( $\phi R_{by}$ )

$$b_{bf} = b_s + 2.5 t_f = 150 + 2.5 \times 15.6 = 189 \text{ mm}$$

$$\frac{\phi R_{bb}}{b_{bf}} = 3.67 \quad (\text{Table 5.2-5})$$

$$\therefore \phi R_{by} = 3.67 \times 189 = 694 \text{ kN}$$

(b) Design bearing buckling capacity ( $\phi R_{bb}$ )

$$b_b = b_{bf} + b_{bw} = 189 + 250.9 = 440 \text{ mm}$$

$$\frac{\phi R_{by}}{b_b} = 0.903 \quad (\text{Table 5.2-5})$$

$$\therefore \phi R_{bb} = 0.903 \times 440 = 397 \text{ kN}$$

Hence  $\phi R_b = \min [\phi R_{bb}, \phi R_{by}] = 397 \text{ kN} > R^* \therefore \text{O.K.}$

## 5.3 Design Moment Capacity for Members Without Full Lateral Restraint

### 5.3.1 Scope

Values of design member moment capacity ( $\phi M_b$ ) are given in Tables 5.3-1 to 5.3-11 for various values of effective length ( $L_e$ ) based on the uniform moment case ( $\alpha_m = 1.0$ ) for members bending about the  $x$ -axis *without full lateral restraint*. Many tables are supplemented by graphs immediately following. The design section moment capacity ( $\phi M_{sx}$ ) is also listed to allow easy calculation of  $\phi M_b$  for other moment distributions, as well as the design shear capacity ( $\phi V_v$ ) for calculation of bending shear interaction.

### 5.3.2 Design Member Moment Capacity

The values of design moment capacity ( $\phi M_b$ ) are determined in accordance with Clause 5.6.1.4 of AS 4100 as:

$$\phi M_b = \phi \alpha_m \alpha_s M_s \leq \phi M_s$$

where  $\phi = 0.9$  (Table 3.4 of AS 4100)

$\alpha_m$  = moment modification factor (Clause 5.6.1.1 of AS 4100)

= 1.0 (**Assumed for all tables and graphs - based on uniform moment case**)

$$\alpha_s = 0.6 \left\{ \sqrt{\left[ \left( \frac{M_s}{M_{oa}} \right)^2 + 3 \right]} - \left( \frac{M_s}{M_{oa}} \right) \right\} \quad (\text{Equation 5.6.1.1(2) of AS 4100})$$

$M_{oa}$  =  $M_o$  - reference buckling moment (Clause 5.6.1.1(a)(iv)(A) of AS 4100)

$$= \sqrt{\left( \frac{\pi^2 EI_y}{L_e^2} \right) \left( GJ + \frac{\pi^2 EI_w}{L_e^2} \right)} \quad (\text{Equation 5.6.1.1(3) of AS 4100})$$

$L_e$  = effective length

For Structural Tees there is an additional term, the monosymmetry section constant ( $\beta_x$ ), in the formula for the reference buckling moment,  $M_o$ , to account for the asymmetry about the  $x$ -axis. For more details refer to Clause 5.6.1.2 of AS 4100.

### 5.3.3 Effective Length

The value of  $\phi M_b$  depends on the effective length ( $L_e$ ) of the flexural member.  $L_e$  is determined by:

$$L_e = k_t k_l k_r L \quad (\text{Clause 5.6.3 of AS 4100})$$

where  $k_t$  = twist restraint factor (Table 5.6.3(1) of AS 4100)

$k_l$  = load height factor (Table 5.6.3(2) of AS 4100)

$k_r$  = lateral rotation restraint factor (Table 5.6.3(3) of AS 4100)

$L$  = length of segment

The article *Design of Unbraced Beams* in the AISC technical journal, "Steel Construction", Vol 27, No 1, February 1993, provides guidance on the restraint conditions provided by many common connections. Reference can also be made to the article *Design of Unbraced Cantilevers*, in "Steel Construction", Vol 27, No 3, August 1993.

### 5.3.4 Other Loading and Restraint Conditions

The design moment capacities presented in these tables can be used for other loading conditions. For these situations the effective length ( $L_e$ ) corresponding to the actual length and restraint conditions must be assessed and the appropriate value of  $\alpha_m$  determined in accordance with Clause 5.6.1.1(a) of AS 4100. The design moment capacity ( $\phi M_b$ ) can then be determined as the lesser of:

$$\phi M_{sx} = \phi Z_{ex} f_y$$

and  $\phi M_b = \phi \alpha_m \alpha_s Z_{ex} f_y$

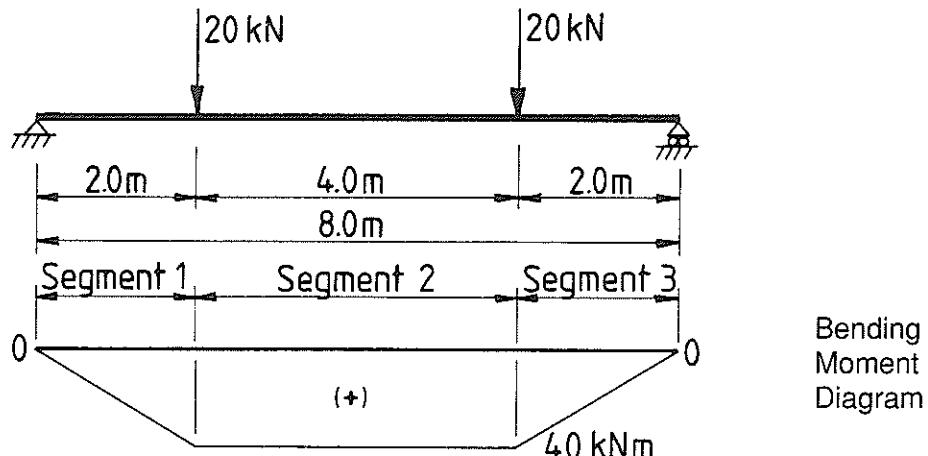
where  $\phi = 0.9$  (Table 3.4 of AS 4100)

$$\phi M_b = \alpha_m \text{ times the value of } \phi M_b (= \phi \alpha_s Z_{ex} f_y) \text{ given in Tables 5.3-1 to 5.3-11}$$

**Tables 5.3-1 to 5.3-11 are based on the most critical moment distribution - i.e. uniform moment over the beam entire segment ( $\alpha_m = 1.0$ ). For other values of  $\alpha_m$ , designers should use the lesser of  $\phi M_{sx}$  and  $\alpha_m(\phi M_b)$  where  $\phi M_b$  is the value given in the appropriate table for the same effective length.**

### 5.3.5 Examples

1. A simply supported beam shown below has two concentrated loads applied to the top flange. Full restraint is provided at the load points and the supports. The calculated design load at each point is 20 kN and includes an allowance for self weight. What size Universal Beam is required to support these loads?



#### Design Data:

$$\text{Design bending moment } M^* = 40 \text{ kNm}$$

$$\text{Design shear force } V^* = 20 \text{ kN}$$

#### Solution:

For beam segment 2:

$$\text{End restraint condition} = \text{FF} \quad (\text{fully restrained at both ends of the segment})$$

$$\text{Twist restraint factor } k_t = 1.0 \quad (\text{Table 5.6.3(1) of AS 4100})$$

$$\text{Load Height Factor } k_f = 1.0 \quad (\text{Table 5.6.3(2) of AS 4100})$$

$$\text{Lateral rotation restraint factor } k_r = 1.0 \quad (\text{Top flange loading at segment end}) \quad (\text{Table 5.6.3(3) of AS 4100}) \text{ (conservative)}$$

$$\therefore \text{Effective length } L_e = k_t k_f k_r L \\ = 1.0 \times 1.0 \times 1.0 \times 4.0 \\ = 4.0 \text{ m}$$

As a uniform bending moment is applied to segment 2,  $\alpha_m = 1.0$  (Table 5.6.1 of AS 4100). Thus alternatives can be read directly from Table 5.3-5 for a uniform bending moment of 40 kNm on segment 2 with an effective length ( $L_e = 4.0$  m).

$$\therefore \text{Choose } 200\text{UB29.8 - Grade 300} \quad \phi M_b = 47.6 \text{ kNm} > M^* \\ \phi V_v = 225 \text{ kN} > V^* \text{ (Note also } 0.6 \phi V_v > V^*)$$

Beam segments 1 and 3 do not have to be checked because they have the same design bending moment (i.e. the maximum segment moment) and end restraints but a shorter effective length compared with the middle segment. Additionally the bending moment distribution is different in the end segments ( $\alpha_m = 1.75$  (Table 5.6.1 of AS 4100)). As the end segments have a smaller effective length and a larger moment modification factor, the design member moment capacity of these segments cannot be less than that of the central (critical) segment.

Designers should also make checks for bearing (for the strength limit state), and deflection.

2. Considering the simply supported beam in Example 1 above, redesign the beam assuming that full restraint is **not** provided at the load points.

Design Data:

$$\text{Design bending moment } M^* = 40 \text{ kNm}$$

$$\text{Design shear force } V^* = 20 \text{ kN}$$

Solution:

For entire beam:

$$\text{End restraint condition} = \text{FF} \quad (\text{fully restrained at both ends of the segment})$$

$$\text{Twist restraint factor } k_t = 1.0 \quad (\text{Table 5.6.3(1) of AS 4100})$$

$$\text{Load Height Factor } k_l = 1.4 \quad (\text{Table 5.6.3(2) of AS 4100})$$

$$\text{Lateral rotation restraint factor } k_r = 1.0 \quad (\text{Table 5.6.3(3) of AS 4100})$$

$$\therefore \text{Effective length } L_e = k_t k_l k_r L \\ = 1.0 \times 1.4 \times 1.0 \times 8.0 \\ = 11.2 \text{ m}$$

$$\text{Moment modification factor } \alpha_m = 1.088 \quad (\text{Table 5.6.1 of AS 4100})$$

$$\text{To satisfy the strength limit state } M^* \leq \phi M_b = \phi \alpha_m \alpha_s M_{sx} \quad (\leq \phi M_{sx})$$

$$\text{This can be rewritten as } M^*/\alpha_m = 40/1.088 = 36.8 \text{ kNm} \\ \leq \phi(1.0)\alpha_s M_{sx}$$

The right hand side is the value of  $\phi M_b$  (based on  $\alpha_m = 1.0$ ) that is found in Tables 5.3-1 to 5.3-11.

To design this beam  $M^*$  (= 40 kNm)  $< \phi M_{sx}$  and  $M^*/\alpha_m$  (= 36.8 kNm)  $< \phi M_b$ .

An appropriate section can then be read directly from the table using an *adjusted* design bending moment of  $M^*/\alpha_m$ .

$$\begin{aligned} \text{For a 310UB46.2 - Grade 300} \quad \phi M_{sx} &= 197 \text{ kNm} \quad (> M^*) \quad (\text{Table 5.3-5}) \\ \phi M_b &= 40.0 \text{ kNm} \quad (\text{Table 5.3-5 for } L_e = 12 \text{ m and } \alpha_m = 1) \\ \therefore \phi M_b &= 1.088 \times 40.0 = 43.5 \text{ kNm} \quad (> M^*) \\ \phi V_v &= 356 \text{ kN} \end{aligned}$$

A shear/bending interaction check is not necessary and a 310UB46.2 Grade 300 section is adequate.

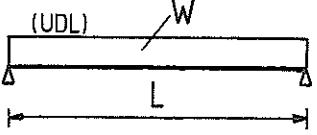
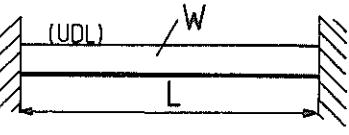
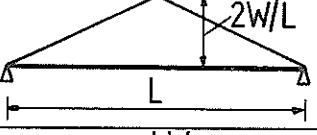
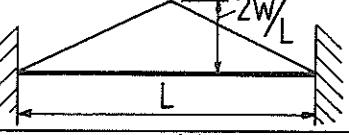
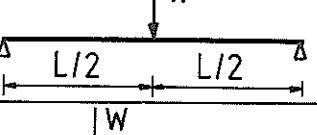
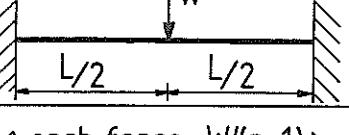
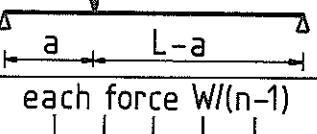
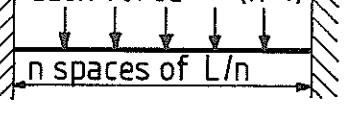
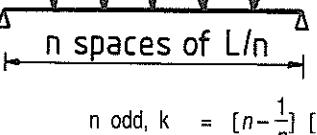
## 5.4 Calculation of Beam Deflections

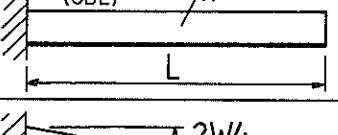
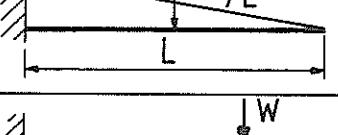
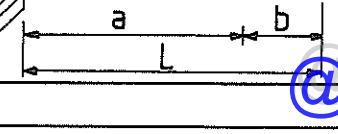
Common methods for calculating the elastic deflection of a beam include:-

- integration of  $M/EI$  diagram;
- moment area;
- slope deflection;
- published solutions for particular cases;
- approximate or numerical methods (e.g. finite elements)

Table 5.3 gives the more commonly used beam deflection formulae. Due to the large range of loading configurations and support conditions considered for beams in design, a comprehensive set of beam deflection formulae is published in the AISC technical journal "Steel Construction", Vol. 26 No. 1, (February 1992).

TABLE 5.3: Beam Deflection Formulae

SIMPLY SUPPORTED BEAMS		BUILT-IN BEAMS	
	$\Delta = \frac{5}{384} \frac{WL^3}{EI}$		$\Delta = \frac{1}{384} \frac{WL^3}{EI}$
	$\Delta = \frac{1}{60} \frac{WL^3}{EI}$		$\Delta = \frac{1.4}{384} \frac{WL^3}{EI}$
	$\Delta = \frac{1}{48} \frac{WL^3}{EI}$		$\Delta = \frac{1}{192} \frac{WL^3}{EI}$
	$\Delta = \frac{WL^3}{48EI} \left[ \frac{3a}{L} - 4\left(\frac{a}{L}\right)^3 \right]$		$\Delta = \frac{k}{192(n-1)} \frac{WL^3}{EI}$
	$\Delta = \frac{k}{192(n-1)} \frac{WL^3}{EI}$	$n \text{ odd, } k = [n - \frac{1}{n}] [1 - \frac{1}{2}(1 - \frac{1}{n^2})]$ $n \text{ even, } k = [3 - \frac{1}{2}(1 + \frac{4}{n^2})] \times n - [2(n - \frac{1}{n})]$	

CANTILEVERS	
	$\Delta = \frac{1}{8} \frac{WL^3}{EI}$
	$\Delta = \frac{1}{15} \frac{WL^3}{EI}$
	$\Delta = \frac{Wa^3}{EI} \frac{1}{3} [1 + \frac{3b}{2a}]$

Where:

$\Delta$  = maximum deflection

$W$  = total load on beam

$L$  = span of beam

$E$  = Young's modulus of elasticity

$I$  = second moment of area of cross-section

[BLANK]

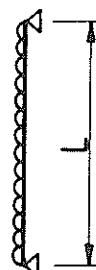


TABLE 5.1-1  
WELDED BEAMS

## MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT bending about x-axis

$W_{L1}^*$ : Maximum Design Load based on Moment  
 $W_{L2}^*$ : Maximum Design Load based on Shear  
 $W_{L3}^*$ : Maximum Design Load is LESSER of  $W_{L1}^*$  and  $W_{L2}^*$   
 $W_s^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield



Designation	W <sub>L</sub> <sup>r</sup> (kN) / W <sub>S</sub> <sup>r</sup> (kN) Span in metres										W <sub>L<sub>2</sub></sub> FLR	
	3	3.5	4	5	6	7	8	9	10	11		
1200WB455	19000	16300	14200	11400	9480	8130	7110	6320	5690	4740	4050	3560
1200WB423	17400	14900	13000	10400	9540	8180	7150	6360	5720	4770	4050	3590
1200WB392	15800	13500	13160	10500	8710	7440	6510	5780	5210	4340	3720	3250
1200WB342	15800	13500	11800	9450	7880	6750	5910	5250	5250	4350	3730	3270
1200WB317	13300	11400	9950	7970	6640	5690	4980	4430	3940	3940	3550	2950
1200WB317	12000	10300	910	7210	6010	5150	4500	4000	3600	3000	2570	2250
1200WB278	10100	8660	7550	7050	5850	5440	4410	3920	3530	2940	2520	2200
1200WB278	9740	8330	7290	5520	4660	4330	3710	3250	3240	2910	2430	2050
1200WB249	8660	7420	6500	5200	4330	4070	3450	3050	2890	2600	2170	1820
1000WB322	9140	6660	6110	4890	4070	3510	3110	2760	2600	2170	1850	1620
1000WB296	11000	9440	8260	6610	5510	4720	4130	3670	3300	2750	2350	2060
1000WB296	10590	8350	8160	6540	5450	4670	4050	3540	3240	2770	2370	2080
1000WB296	9910	8500	7440	5950	4960	4250	3720	3300	2910	2530	2170	1890
1000WB258	9770	8470	7230	5830	4630	4190	3650	3260	2930	2540	2180	1820
1000WB258	8270	7090	6200	4960	4130	3540	3100	2760	2400	2070	1770	1440
1000WB215	8020	6820	6020	5110	4010	3440	3010	2670	2410	2070	1700	1300
1000WB215	6830	5900	5170	4130	3440	2950	2560	2300	2070	1720	1480	1290
900WB282	9160	7850	6870	5500	4580	3930	3440	3050	2750	2260	1950	1650
900WB282	9260	7340	6950	5360	4650	3970	3470	3040	2750	2320	1980	1660
900WB257	8170	7010	6130	4900	4090	3500	3070	2720	2450	2040	1750	1530
900WB218	8240	7080	6180	4540	4120	3530	3050	2750	2470	2160	1850	1610
900WB218	6630	5740	5020	4020	3350	2870	2510	2230	2010	1670	1450	1290
900WB175	5400	4630	4050	3240	2700	2310	2020	1800	1620	1370	1160	1010
800WB192	5260	4510	3950	3160	2630	2250	1970	1750	1560	1320	1090	880
800WB122	5420	4640	4060	3250	2710	2320	2030	1810	1630	1350	1160	1020
800WB168	4600	3940	3450	2760	2300	1970	1720	1530	1380	1150	1020	903
800WB146	4580	3930	3440	2750	2260	1960	1720	1530	1380	1150	1020	903
700WB173	4110	3520	3080	2470	2050	1760	1540	1370	1250	1030	881	771
700WB150	3080	3560	3050	2450	2040	1750	1530	1360	1240	1020	877	773
700WB130	3220	2790	2440	1960	1610	1400	1220	1090	978	815	698	611
700WB130	3170	2720	2360	1900	1590	1350	1140	1060	810	708	606	539
700WB115	4290	3680	3230	2580	2150	1840	1610	1430	1290	1070	855	756
700WB115	3370	3630	3250	2580	2150	1840	1610	1430	1290	1070	855	756
700WB115	3610	3090	2710	2170	1800	1550	1380	1200	1080	880	747	644
700WB115	2559	2090	2550	2150	1750	1540	1350	1200	1050	877	771	685
700WB115	2730	2340	2050	1640	1310	1170	1020	910	819	683	585	410
700WB115	2670	2290	2080	1660	1330	1140	1020	910	819	683	585	410

Notes: (1) FLR<sub>m</sub> segment length for full lateral restraint, based on transverse load case ( $\beta_m = -0.8$ ).  
 (2) Shading indicates serviceability loads governed by yielding.

TABLE 5.1-2  
WELDED BEAMS  
GRADE 400

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
bending about X-axis**

W<sub>L1</sub>: Maximum Design Load based on Moment  
W<sub>L2</sub>: Maximum Design Load based on Shear  
W<sub>T</sub>: Maximum Design Load is LESSER of W<sub>L1</sub> and W<sub>L2</sub>  
W<sub>S</sub>: Serviceability Load based on Deflection Limit of Span/250 or First Yield

X— — — — — X

Designation	W <sub>L1</sub> (kN)/W <sub>S</sub> (kN) Span in metres												W <sub>L2</sub>	FLR
	3	3.5	4	5	6	7	8	9	10	12	14	16		
200WB455	24200	20500	18200	14500	12100	10400	9000	8080	7270	6060	5190	4550	4040	3310
24500	21600	18400	14400	12300	10400	8700	7180	6760	6740	5680	4810	4260	3260	1950
22200	19000	16600	13300	11100	9510	8320	7390	6550	5550	4750	4160	3700	3330	3020
22400	19200	16800	13500	12000	10500	8460	7470	6720	5620	4560	4240	3640	3340	2140
20100	17300	15100	12100	10100	8630	7550	6710	6040	5030	4320	3780	3360	3020	2750
22300	17400	15200	12200	10300	8860	7860	6750	6080	5060	3920	3270	3000	2370	1920
17000	14500	12700	10200	8480	7270	6360	5650	5090	4240	3630	3180	2830	2540	2310
16800	14600	12500	10300	8410	7210	6310	5600	5040	4200	3620	3160	2820	2540	2310
1200WB317	15300	13100	11500	9200	7670	6570	5750	5110	4600	3830	3290	2870	2560	2090
13300	13000	11300	9670	7560	6460	5670	5040	4630	3760	3290	2820	2560	2220	1770
12900	11000	9660	7730	6490	5520	4830	4300	3870	3220	2760	2420	2150	1930	1760
12200WB278	12200	10700	9370	7450	6260	5350	4650	4160	3750	3140	2390	1830	1760	1640
11000	9460	8270	6620	5520	4730	4140	3680	3310	2760	2360	2070	1840	1770	966
10500	8540	8170	7650	6280	5240	4540	3930	3430	3140	2660	2000	1550	1550	6640
1000WB322	14200	12100	10600	8490	7000	6070	5310	4720	4250	3540	3030	2650	2360	1930
14400	12000	10500	8410	7070	6010	5260	4670	4210	3190	2340	1860	1420	1150	1740
12700	10900	9560	7650	6310	5460	4780	4250	3620	3190	2730	2390	2120	1910	1740
12800	10400	9420	7540	6240	5380	4710	4150	3770	3280	2840	2080	1660	1260	1020
10500	9110	7970	6380	5320	4520	3990	3540	3190	3190	2660	2280	1990	1770	1590
1000WB258	10300	8840	7740	6380	5460	4420	3870	3470	3190	2660	2310	1700	1300	1030
1000WB215	8720	7480	6540	5230	4380	3740	3270	2910	2620	2180	1870	1640	1450	1310
8250	7050	6170	5640	4120	3530	3050	2740	2470	2120	1730	1270	975	770	624
11100	9890	8740	6990	5890	4990	4370	3880	3500	2910	2500	2180	1940	1750	1090
11500	10200	8830	7740	6540	5560	4510	4040	3670	3520	2450	1800	1380	1090	880
10400	8910	7730	6360	5460	4520	3950	3450	3120	2660	2230	1950	1730	1560	1450
10500	8580	7640	6360	5310	4540	3970	3490	3100	2660	2230	1950	1730	1560	1450
900WB282	8520	7480	6170	5100	4250	3640	3190	2830	2550	2120	1820	1590	1420	1160
8680	5720	5010	4010	3310	2980	2550	2230	2000	1670	1430	1250	1110	1000	910
8660	5710	5000	4000	3340	2950	2560	2230	1820	1620	1260	928	710	567	327
8780	5810	5050	4070	3390	2910	2540	2260	2030	1700	1450	1270	1020	8250	327
900WB218	85100	7290	6310	5100	4250	3640	3190	2830	2550	2120	1820	1590	1420	1160
8530	7260	5440	4510	3420	2850	2570	2220	2000	1730	1440	1230	1060	877	647
900WB175	5020	5720	5010	4010	3310	2980	2550	2230	1820	1670	1430	1250	1110	1000
800WB192	6780	5810	5050	4070	3390	2910	2540	2260	2030	1700	1450	1270	1020	8250
800WB168	5740	4920	4310	3440	2670	2460	2150	1910	1720	1440	1230	1080	957	564
800WB146	5020	5410	3770	3010	2510	1880	1880	1530	1060	779	596	477	382	317
800WB19	5720	4430	3510	2810	2250	2150	1510	1510	1260	1080	942	837	754	685
800WB122	3960	3390	2970	2380	1980	1700	1480	1320	1190	990	848	742	660	540
800WB16	5740	4920	4310	3440	2670	2460	2150	1910	1720	1440	1230	1080	957	564
800WB146	5020	5410	3770	3010	2510	1880	1880	1530	1060	779	596	477	382	317
700WB150	4640	3980	3480	2810	2250	2150	1510	1510	1260	1080	942	837	754	685
700WB122	3960	3390	2970	2380	1980	1700	1480	1320	1190	990	848	742	660	540
700WB173	5520	4730	4140	3310	2760	2360	2070	1840	1660	1380	1180	1030	928	798
700WB150	4640	3980	3480	2810	2250	2150	1510	1510	1260	1080	942	837	754	685
700WB130	4090	3510	3070	2420	2050	1540	1360	1050	1290	1050	728	535	410	324
700WB115	3460	2970	2390	2080	1730	1480	1300	1150	1060	877	768	682	614	558
700WB115	3460	2970	2390	2080	1730	1480	1300	1150	1040	865	749	649	577	214
700WB115	2330	2900	2540	2030	1690	1450	1110	875	709	492	362	362	2750	1746

Notes: (1) FLR, segment length for full lateral restraint, based on transverse load case ( $I_m = 0.8$ )  
(2) Shading indicates serviceability loads governed by yielding.

**WELDED COLUMNS  
GRADE 300**

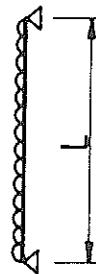
**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
bending about x-axis**

W<sub>L1</sub>: Maximum Design Load based on Moment  
W<sub>L2</sub>: Maximum Design Load based on Shear  
W<sub>L</sub>: Maximum Design Load is LESSER of W<sub>L1</sub> and W<sub>L2</sub>  
W<sub>s</sub>: Serviceability Load based on Deflection Limit of Span/250 or First Yield

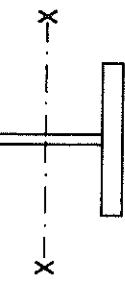
Designation	W <sub>L1</sub> (kN)/W <sub>s</sub> (kN) Span in metres												W <sub>L2</sub>	FLR				
	3	3.5	4	5	6	7	8	9	10	12	14	16						
300WC440	6990	5980	5240	4190	3490	3000	2620	2330	2100	1750	1500	1310	1160	1050	953	4840	4.62	
500WC444	6700	5720	5040	4020	3350	2770	2070	1630	1320	979	675	517	409	331	274	3870	4.75	
500WC344	6770	5810	5080	4060	3390	2980	2540	2260	2030	1690	1450	1270	1130	1020	924	3870	4.69	
500WC363	6572	5650	4930	3940	3250	2650	2030	1600	1300	901	662	507	400	324	268	3870	4.69	
500WC340	6130	5260	4680	3680	3070	2640	2040	1840	1530	1310	1150	1020	920	836	3870	4.69		
500WC340	5977	5119	4470	3580	2860	2360	1870	1430	1160	804	591	453	358	295	3870	4.69		
500WC290	6030	5170	4520	3620	3020	2550	2260	2010	1810	1510	1290	1130	1010	905	823	3400	4.69	
500WC290	5966	5110	4470	3580	2860	2360	1870	1430	1160	804	591	453	358	295	3870	4.69		
500WC290	5080	4360	3810	3050	2540	2180	1910	1690	1530	1270	1090	942	839	715	260	2920	4.75	
500WC290	5172	4420	3860	3190	2590	2200	1680	1330	1080	748	550	421	332	269	693	2920	4.75	
500WC267	4500	3860	3380	2700	2250	1930	1690	1500	1350	1130	965	844	750	675	614	2920	4.68	
500WC228	4578	4320	3630	2800	2200	1960	1500	1190	967	667	490	375	296	240	198	2920	4.38	
500WC340	3750	3220	2820	2250	1880	1610	1410	1250	1130	938	804	704	626	512	2920	4.38		
400WC361	4102	3520	3050	2420	2050	1560	1210	953	772	536	394	302	238	193	160	2920	3.77	
400WC361	5020	4300	3760	3010	2510	1880	1670	1500	1250	1070	941	836	752	684	4230	3.65		
400WC328	4746	4440	3850	3140	2530	2330	1770	1310	1030	838	582	428	327	259	210	173	3.77	
400WC328	4770	4040	3580	2880	2380	2040	1780	1590	1430	1190	1020	894	795	715	650	2860	3.82	
400WC303	4556	3860	3440	2750	2250	1660	1270	1000	812	564	414	317	251	203	168	2270	3.76	
400WC303	4310	3170	3230	2590	2160	1850	1620	1440	1290	1080	924	808	719	647	588	2860	3.77	
400WC270	3769	3570	3140	2500	2010	1470	1130	892	722	502	369	282	223	181	149	2270	3.52	
400WC270	3800	3260	2850	2280	1900	1630	1480	1270	1140	950	814	713	633	570	518	2850	3.77	
400WC212	3739	3170	2770	2220	1750	1250	934	778	630	438	321	246	194	158	130	254	1810	3.52
400WC181	2930	2510	2240	1760	1460	1260	1100	976	879	732	628	549	439	399	399	399	2270	3.76
400WC181	2560	2460	2170	1740	1320	1050	922	819	737	615	527	461	410	369	335	335	2270	3.52
400WC144	1880	1600	1400	1120	931	798	621	559	465	399	349	310	279	254	216	1810	3.52	
350WC280	2349	2120	1530	1190	830	670	467	369	299	207	152	117	92.2	74.7	61.7	553	453	3.38
350WC280	3320	2450	1990	1660	1420	1240	1110	996	830	711	622	553	498	498	498	498	2330	3.38
350WC258	3149	2890	2230	1840	1470	1230	1050	922	717	566	459	319	234	179	142	115	94.8	3.35
350WC258	2980	2560	2240	1790	1490	1280	1120	996	897	747	641	560	498	448	408	408	2330	3.35
350WC230	2869	2440	2130	1520	1130	828	634	501	406	282	207	159	125	101	83.9	369	2080	3.34
350WC230	2630	2250	1970	1580	1310	1130	986	876	788	657	563	493	438	394	358	358	2080	3.38
350WC197	2250	2160	1820	1410	978	719	550	435	352	244	180	109	88	72.7	337	307	1780	3.38
350WC197	2130	1930	1600	1350	1120	964	844	750	675	562	482	422	375	317	274	274	1780	3.38
	2330	1880	1610	1190	829	609	466	368	298	207	152	117	92.1	74.6	61.7	553	453	3.38

Notes: (1) FLR, segment length for full lateral restraint, based on transverse load case ( $\beta_m = -0.8$ ).  
(2) Shading indicates serviceability loads governed by yielding.

**TABLE 5.1-4**  
**WELDED COLUMNS**  
**GRADE 400**  
**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT**  
bending about x-axis



W<sub>L1</sub>: Maximum Design Load based on Moment  
W<sub>L2</sub>: Maximum Design Load based on Shear  
W<sub>s</sub>: Maximum Design Load is LESSER of W<sub>L1</sub> and W<sub>L2</sub>  
W<sub>s</sub>: Serviceability Load based on Deflection Limit of Span/250 or First Yield



Designation	W <sub>L1</sub> (kN) / W <sub>s</sub> (kN) Span in meters												W <sub>L2</sub>	FLR				
	1	3	3.5	4	5	6	7	8	9	10	12	14						
500WC440	8990	7700	6740	5390	4490	3850	3370	3000	2700	2250	1930	1680	1350	1230	6320*	4.07		
500WC414	8520	7150	6150	5170	3680	2700	2070	1630	1320	979	675	517	409	337	274			
500WC383	8710	7460	6530	5230	4350	3730	3270	2900	2610	2180	1870	1630	1450	1310	1190	4980	4.19	
500WC340	8450	7240	6340	5070	3600	2650	2030	1600	1300	907	662	507	400	324	268			
500WC290	7890	6760	5910	4730	3940	3380	2860	2630	2370	1970	1690	1480	1310	1180	1080	4980	4.14	
500WC267	7270	5770	5750	4570	3220	2360	1810	1430	1160	804	597	453	358	290	239			
500WC228	6540	5720	4580	3810	2860	2270	1750	1540	1290	910	1630	1430	1270	1140	1040	4370	4.14	
400WC361	7580	6370	5750	4520	3500	2570	2070	1750	1560	1260	875	643	492	389	315			
400WC270	6400	5490	4800	3840	3200	2740	2400	2130	1920	1600	1370	1200	1070	980	873	3690	4.19	
400WC328	6650	5590	4950	3950	2950	2200	1680	1330	1080	748	550	427	332	269	223			
400WC303	6200	5150	4510	3560	2850	2420	2120	1880	1700	1410	1210	1060	942	848	771	3690	4.13	
400WC220	4430	3800	3320	2660	2210	1900	1660	1480	1330	1110	949	830	738	654	598			
400WC212	5220	4460	3900	3090	2720	2760	2420	2150	1930	1610	1380	1210	1070	967	880	5370*	3.22	
400WC181	5540	4750	4160	3330	2770	2380	2080	1850	1600	1390	1190	1040	924	832	756	3810	3.33	
400WC144	5330	4530	4010	2890	2440	2090	1830	1630	1470	1220	1050	916	814	733	666	3400	3.33	
350WC290	4890	4190	3650	2930	2350	2330	1710	1370	1030	638	552	428	327	259	210	173		
350WC280	6130	5260	4600	3680	3070	2300	2040	1840	1550	1310	1150	1020	920	836	810	3810	3.37	
350WC267	5590	5060	4340	3250	2250	1660	1270	1000	812	564	474	377	317	251	203	168		
350WC220	4220	3760	3260	2380	1820	1420	1130	892	722	502	369	282	223	181	149	3810	3.33	
350WC212	3690	3160	2770	2210	1850	1580	1380	1230	1110	923	791	692	615	554	503	2870	3.31	
350WC181	3040	2600	2260	1820	1300	1140	1010	911	759	650	569	506	455	414	3810	2870	3.13	
350WC144	2200	1880	1650	1320	1100	941	824	732	659	549	471	412	366	329	300	2300	3.13	
350WC280	4270	3660	3280	2560	2130	1830	1600	1420	1280	1070	914	800	711	640	582	2990	2.99	
350WC258	3040	2650	2870	1840	1270	936	717	566	459	319	234	179	142	115	94.8			
350WC230	3840	3290	2880	2310	1920	1650	1440	1280	1150	961	824	721	641	576	524	2990	2.95	
350WC197	3260	2900	2550	2030	1690	1450	1270	1130	1010	845	724	634	563	507	461	2670	2.95	
	3260	2900	2200	1410	978	550	352	244	180	109	88	620	542	482	394	394	2260	2.98
	2830	2480	2170	1450	1190	829	609	466	368	295	117	152	117	92.1	74.6	61.7		

Notes: (1) FLR, segment length for full lateral restraint, based on transverse load case ( $\beta_m = -0.8$ ).  
(2) Shading indicates serviceability loads governed by yielding.  
(3) \* Indicates shear capacity governed by the shear capacity of the weld.

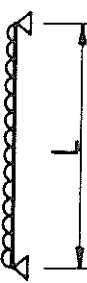
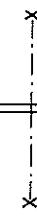


TABLE 5.1-5(1)

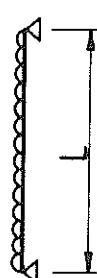
**UNIVERSAL BEAMS  
GRADE 300**
**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
bending about x-axis**
 $W_{L1}^*$ : Maximum Design Load based on Moment $W_{L2}^*$ : Maximum Design Load based on Shear $W_L^*$ : Maximum Design Load is LESSER of  $W_{L1}^*$  and  $W_{L2}^*$  $W_S^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield

Designation	$W_{L1}^*$ (kN) / $W_S^*$ (kN) Span in metres										$W_{L2}^*$	FLR m			
	3	3.5	4	5	6	7	8	9	10	12					
610UB125	2470	2120	1850	1480	1240	1060	927	824	742	618	530	464	412	371	337
610UB113	2410	2060	1710	1440	1200	1032	903	748	606	427	309	237	187	151	125
610UB113	2210	1900	1650	1330	1110	948	829	737	663	553	474	415	369	332	302
610UB101	2350	1840	1610	1250	1020	892	792	663	537	373	274	210	166	134	111
610UB101	2090	1790	1560	1250	1040	894	782	695	626	522	447	391	348	313	284
5530UB 92.4	2020	1730	1550	1240	1016	867	731	577	468	325	239	183	148	117	96.6
5530UB 92.4	1710	1460	1280	1020	853	732	640	569	512	427	366	320	284	256	233
5530UB 82.0	1660	1430	1250	996	862	795	695	532	420	347	236	174	133	105	88.0
5530UB 82.0	1490	1280	1120	933	744	638	558	496	446	372	319	279	248	223	188.0
460UB 82.1	1450	1240	1080	856	725	599	458	362	293	204	150	115	90.5	203	175.0
460UB 82.1	1320	1130	991	753	661	567	446	397	330	283	228	177	148	117	100.6
460UB 74.6	1285	1110	959	725	634	466	357	282	228	159	117	89.2	220	198	158.0
460UB 74.6	1200	1030	897	718	598	513	449	399	359	299	256	224	199	179	147.2
460UB 67.1	1170	1000	873	733	572	420	322	254	206	143	105	80.4	63.5	57.4	144.0
460UB 67.1	1060	912	798	638	532	456	399	355	319	266	228	200	177	160	133.0
410UB 59.7	1045	853	761	585	504	371	284	224	162	126	92.6	70.9	56.0	45.4	37.5
410UB 59.7	864	741	648	519	432	370	324	288	259	216	185	162	144	130	118
410UB 53.7	852	730	629	503	369	271	208	164	133	92.3	67.8	51.9	41.0	33.2	27.5
410UB 53.7	811	695	609	487	405	348	304	270	243	203	174	152	135	122	111
360UB 56.7	795	682	597	462	320	235	180	142	115	80.1	58.9	45.1	35.6	28.8	23.8
360UB 56.7	729	625	547	364	312	273	243	219	182	156	137	121	109	99.4	99.1
360UB 50.7	719	616	539	396	275	202	155	122	99.0	68.7	50.5	38.7	30.6	24.7	14.3
360UB 50.7	646	553	484	387	323	277	242	215	194	161	138	121	108	88.1	88.7
360UB 44.7	636	547	479	349	242	178	136	108	87.1	60.5	44.5	34.0	26.9	21.8	14.1
360UB 44.7	591	507	443	296	253	222	197	177	148	127	111	98.5	88.7	80.6	83.9
	538	504	447	298	207	152	116	92.0	74.6	51.8	38.0	29.1	23.0	18.6	15.4

Notes: (1) FLR, segment length for full lateral restraint, based on transverse load case ( $\beta_m = -0.8$ ).

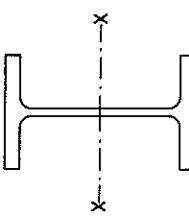
(2) Shading indicates serviceability loads governed by yielding.

(3) Grade 300 refers to BHP Grade 300PLIS™. See Note (1) on page 2-2.



**TABLE 5.1-5(2)**  
**UNIVERSAL BEAMS**  
**GRADE 300**

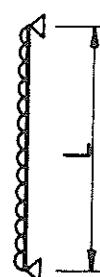
W<sub>1</sub>: Maximum Design Load based on Moment  
 W<sub>2</sub>: Maximum Design Load based on Shear  
 W<sub>L1</sub>: Maximum Design Load is LESSER of W<sub>1</sub> and W<sub>2</sub>  
 W<sub>s</sub>: Serviceability Load based on Deflection Limit of Span/250 or First Yield



Designation	W <sub>L1</sub> (kN) / W <sub>s</sub> (kN) Span in metres												W <sub>L2</sub> kN	FLR m		
	0.5	0.75	1	1.25	1.5	2	3	4	5	6	7	8	10	12	15	
310UB 46.2	3150	2100	1570	1260	1050	787	525	394	315	262	225	197	157	131	105	
310UB 40.4	3146	2090	1570	1260	1050	787	523	386	247	171	126	96.4	61.7	42.8	27.4	
310UB 32.0	2910	1940	1460	1170	972	729	496	364	292	243	208	182	146	121	97.2	64.1
2150B 37.3	2150	1430	1080	860	717	538	358	269	215	179	154	134	108	83.0	53.1	33.6
2240	2230	1450	1120	895	747	560	373	280	249	155	108	79.2	60.7	40.7	27.0	71.7
2500UB 31.4	2500	180	1110	883	742	536	371	274	224	187	160	140	112	93.3	74.7	56.7
2500UB 25.7	1810	1210	911	739	607	456	304	228	182	152	130	114	95.0	69.8	53.5	34.2
1470	1470	991	736	593	604	453	342	177	109	76.0	55.8	42.8	30.0	19.0	12.2	50.7
1450	1450	974	730	594	491	368	245	184	147	123	105	92.0	73.6	61.3	49.1	42.9
2000UB 29.8	1450	970	727	592	485	364	241	176	136	86.9	60.4	44.4	34.0	21.7	15.1	9.66
2000UB 25.4	1440	961	721	597	489	360	242	182	145	121	104	90.9	72.7	60.6	48.5	45.1
2000UB 22.3	1190	796	597	478	398	298	199	149	119	99.5	74.6	65.3	53.5	42.8	28.0	12.4
1050	1050	697	594	475	398	297	161	90.5	57.9	40.2	29.6	22.6	14.5	10.1	6.44	40.7
1050	1050	710	582	523	418	349	261	174	131	105	87.1	74.7	65.3	52.3	43.6	34.8
200UB 18.2	828	552	414	331	276	207	138	104	80.5	57.5	35.8	26.3	20.1	12.9	8.94	5.72
180UB 22.2	818	545	409	327	273	204	108	60.7	38.9	27.0	19.8	15.2	11.2	8.45	27.6	30.8
180UB 18.1	800	600	450	360	300	225	150	112	90.0	75.0	64.3	56.2	45.0	37.5	6.75	4.32
180UB 16.1	637	425	319	255	212	159	106	79.7	53.7	45.5	39.8	31.9	26.6	21.2	12.2	0.722
150UB 18.0	628	418	314	257	209	157	104	72.4	40.7	26.1	18.1	13.3	10.2	6.57	4.52	2.89
150UB 14.0	598	415	311	259	207	156	104	77.8	62.2	51.9	44.5	38.9	31.1	25.9	20.7	32.1
469	313	235	168	156	117	78.2	58.7	61.8	34.8	22.2	15.4	8.69	5.56	3.86	2.47	0.655
455	303	227	152	102	45.5	25.6	16.4	11.4	8.35	6.39	4.09	2.84	1.82	15.6	25.9	0.589

Notes: (1) FLR, segment length for full lateral restraint, based on transverse load case ( $\beta_m = -0.8$ ).  
 (2) Shading indicates serviceability loads governed by yielding.  
 (3) Grade 300 refers to BHP Grade 300 PLUS™. See Note (1) on page 2-2.

**TABLE 5.1-6**  
**UNIVERSAL COLUMNS**  
**GRADE 300**  
**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT**  
bending about x-axis



W<sub>L1</sub>: Maximum Design Load based on Moment  
W<sub>L2</sub>: Maximum Design Load based on Shear  
W<sub>s</sub>: Maximum Design Load is LESSER of W<sub>L1</sub> and W<sub>L2</sub>  
W<sub>v</sub>: Serviceability Load based on Deflection Limit of Span/250 or First Yield

Designation	W <sub>L1</sub> (kN) / W <sub>s</sub> (kN) Span in metres												W <sub>L2</sub>	FLR	
	3	3.5	4	5	6	7	8	9	10	12	14	16			
310UC15.8	1800	1550	1350	1080	901	773	676	601	541	451	386	338	300	270	246
310UC13.7	1776	1520	1330	953	662	463	372	294	238	166	122	99.1	73.6	59.6	49.2
310UC11.8	1550	1330	1160	928	773	663	580	515	464	387	331	290	258	232	211
310UC11.8	1530	1310	1160	803	561	412	316	249	202	140	103	78.9	62.4	50.5	41.7
310UC9.8	1320	1130	987	790	658	564	494	439	395	329	282	247	219	197	180
310UC9.8	1320	1130	987	681	473	347	265	210	170	118	86.8	66.5	52.5	42.6	35.2
310UC9.8	130	965	845	676	563	483	422	375	338	282	241	211	188	169	154
250UC89.5	1760	1523	857	548	381	280	214	169	137	95.2	69.9	53.5	42.3	34.3	28.3
250UC89.5	824	618	495	412	353	309	275	247	206	177	155	137	124	112	94.3
250UC72.9	820	703	548	351	244	179	137	108	87.7	60.9	44.7	34.2	27.1	21.9	18.1
250UC72.9	710	608	532	426	355	304	266	237	213	177	152	133	118	106	96.8
200UC59.5	472	405	437	280	194	143	109	86.4	70.0	48.6	35.7	27.3	21.6	17.5	14.5
200UC52.2	418	307	235	283	236	202	177	157	142	118	101	88.5	78.7	70.8	64.4
200UC46.2	410	352	308	246	205	176	154	137	123	103	88.0	77.0	68.4	61.6	56.0
150UC37.2	361	265	203	130	90.2	66.3	50.7	40.1	32.5	22.5	16.6	12.7	10.0	8.12	6.71
150UC37.2	356	305	267	214	178	153	133	119	107	89.0	76.3	66.7	59.3	53.4	48.5
150UC30.0	313	230	176	173	78.3	57.5	44.0	34.8	28.2	19.6	14.4	11.0	8.70	7.05	5.82
150UC30.0	223	191	167	134	112	95.6	83.6	74.3	66.9	55.8	47.8	41.8	37.2	33.5	30.4
150UC23.4	151	111	85.1	54.5	37.8	27.8	21.3	16.8	13.6	9.45	6.95	5.32	4.20	3.40	2.81
150UC23.4	120	164	144	115	95.8	82.1	71.9	63.9	57.5	47.9	41.1	35.9	31.9	28.7	26.1
100UC14.8	135	116	87.6	67.6	43.2	30.0	22.1	16.9	13.3	10.8	7.51	5.52	4.22	3.94	2.23
100UC14.8	86.2	63.4	48.5	31.0	81.1	67.6	58.0	50.7	45.1	40.6	33.8	29.0	25.4	22.5	20.3
100UC14.8	57.1	48.9	42.8	34.3	28.6	24.5	21.6	15.8	12.1	9.58	7.76	5.39	3.96	3.03	2.40
100UC14.8	21.7	16.0	12.2	7.82	5.43	3.99	3.06	2.41	1.96	1.36	14.3	12.2	9.52	7.79	6.87

Notes: (1) FLR, segment length for full lateral restraint, based on transverse load case ( $\beta_m = -0.8$ ).

(2) Shading indicates serviceability loads governed by yielding.

(3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

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**TEES CUT FROM UNIVERSAL BEAMS  
GRADE 300**

$W_{L1}^*$ : Maximum Design Load based on Moment  
 $W_{L2}^*$ : Maximum Design Load based on Shear  
 $W_{L3}^*$ : Maximum Design Load is LESSER of  $W_{L1}^*$  and  $W_{L2}^*$   
 $W_S^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield

Designation	W <sub>L1</sub> ' (kN) / W <sub>S</sub> ' (kN) Span in metres										W <sub>L2</sub> kN	Effective Length m			
	1	1.25	1.5	1.75	2	2.5	3	3.5	4	5					
305BT62.5	897	718	598	513	449	359	299	256	224	179	150	128	112	1040	2.27
305BT56.5	865	532	443	357	332	266	222	190	166	133	131	85.6	65.5		
305BT55	831	665	554	475	416	333	277	238	208	166	139	119	104	973	2.17
305BT50.5	616	492	477	382	305	246	225	176	154	123	105	78.2	59.9		
305BT50.5	826	661	551	472	413	330	275	235	206	165	138	118	103	975	1.98
265BT46.3	612	409	408	352	305	245	224	175	153	122	96.8	71.1	54.5		
265BT46.3	627	501	418	358	313	251	209	179	157	125	104	89.5	78.3	828	1.94
265BT41.0	463	371	310	265	232	186	155	135	115	95	92.9	66.1	48.6	37.2	
265BT41.0	577	462	385	330	289	231	192	165	144	115	96.2	82.5	72.1	773	1.84
230BT41.1	428	342	265	244	214	171	143	122	107	85.5	59.6	43.8	33.6		
230BT41.1	455	364	303	260	227	182	152	130	114	90.9	75.8	64.9	56.8	693	1.90
230BT37.3	337	269	224	192	168	135	112	92	82	60.3	49.6	41.9	30.8		
230BT37.3	414	331	276	237	207	166	138	118	104	82.8	69.0	59.2	51.8	632	1.85
230BT33.6	307	245	215	175	153	123	102	87.7	76.7	54.6	37.9	27.9	21.3		
230BT33.6	381	305	254	218	190	152	127	109	95.2	76.2	63.5	54.4	47.6	586	1.78
205BT29.9	282	226	169	161	144	123	104	92.1	80.6	70.6	49.6	35.3	25.3		
205BT29.9	283	226	188	162	141	113	94.2	80.8	70.7	56.5	47.1	40.4	35.3	480	1.79
205BT26.9	209	188	140	120	105	83.8	63.8	53.8	52.2	33.6	23.3	17.1	13.1		
205BT26.9	287	229	191	164	143	115	95.6	81.9	71.7	57.3	47.8	41.0	35.8	464	1.61
180BT28.4	212	170	142	121	106	84.9	70.8	60.7	50.7	48.7	31.2	21.6	15.9		
180BT28.4	225	180	150	129	113	90.2	75.1	64.4	56.4	45.1	37.6	32.2	28.2	433	1.83
180BT25.4	162	132	111	95.4	83.5	65.8	55.7	47.7	37.2	23.8	16.5	12.1	9.29		
180BT25.4	203	163	135	116	102	81.3	67.7	58.0	46.0	30.8	25.4	20.0	17.6	392	
180BT22.4	150	120	100	86.0	75.2	62.2	50.2	38.0	33.2	21.3	14.8	10.8	8.30		
180BT22.4	195	156	130	111	97.4	77.9	64.9	55.7	48.7	39.0	32.5	27.8	24.4	367	1.61
148	119	98.9	86.8	74.2	59.3	49.4	39.3	30.1	23.4	13.4	9.82				

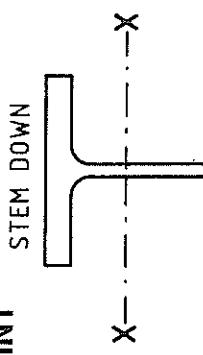
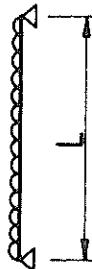
Notes: (1) Shading indicates serviceability load governed by yielding.  
 (2) The Effective Length for Tees is the maximum effective length of a segment for which  $\phi M_b = \phi M_{Sx}$  assuming  $\sigma_m = 1.0$ .  
 (3) Grade 300 refers to BHP Grade 300PLIStM. See Note 11 on page 2-2.

**TABLE 5.1-7(2)**  
**TEES CUT FROM UNIVERSAL BEAMS**  
**GRADE 300**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT**  
**bending about x-axis**

$W_{L1}^*$ : Maximum Design Load based on Moment  
 $W_{L2}^*$ : Maximum Design Load based on Shear  
 $W_L^*$ : Maximum Design Load is LESSER of  $W_{L1}^*$  and  $W_{L2}^*$   
 $W_S^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield

stem down — flange in compression



Designation	$W_{L1}^*/(kN) / W_L^*/(kN)$ Span in metres								$W_{L2}^*$	Effective Length m
	1	1.25	1.5	1.75	2	2.5	3	3.5		
155BT23.1	140	112	93.7	80.3	70.2	56.2	46.8	40.1	35.1	20.1
155BT20.2	134	107	89.5	76.5	62.0	52.3	44.7	36.6	26.6	9.05
155BT16.0	99.4	73.5	68.2	58.4	67.1	53.7	44.7	38.3	33.5	22.4
109	87.1	72.6	62.2	54.4	48.2	43.6	36.3	32.0	23.5	17.5
125BT18.7	85.3	68.3	65.9	48.8	45.7	34.7	26.4	31.1	27.2	18.1
98.8	79.0	65.8	55.4	49.4	39.5	32.9	28.2	19.8	14.8	9.49
73.2	59.5	58.0	41.8	36.6	28.6	19.8	14.6	11.2	7.14	6.59
89.8	71.8	59.8	51.3	44.9	35.9	29.9	25.3	22.4	18.0	14.6
57.7	51.7	44.8	34.4	35.6	25.3	17.6	12.9	9.90	6.34	5.88
125BT12.9	72.3	57.8	48.2	41.3	36.1	28.9	24.1	20.6	18.1	14.5
53.5	42.8	35.7	30.6	26.8	20.0	13.9	10.2	7.80	4.99	3.47
100BT14.9*	62.9	50.3	41.9	35.9	31.4	25.2	21.0	18.0	15.7	12.6
46.6	37.4	34.7	26.6	22.9	22.9	14.7	10.2	7.47	5.72	5.55
100BT12.7*	55.4	44.3	36.9	31.6	27.7	22.2	18.5	15.8	13.8	10.5
41.5	33.2	27.5	21.6	19.9	12.7	8.82	6.48	4.96	3.78	3.23
45.0	36.0	30.0	25.7	22.5	18.0	15.0	12.8	11.2	9.90	10.3
35.6	28.5	23.7	21.3	17.1	10.9	7.59	5.58	4.27	2.73	2.55
40.9	40.9	32.7	27.3	20.5	16.4	13.6	11.7	10.2	8.18	7.88
30.3	24.2	20.2	17.3	14.0	8.96	6.22	4.57	3.50	2.24	1.87
43.2	34.5	28.8	24.7	21.6	17.3	14.4	12.3	10.8	8.64	7.91
32.0	25.6	21.3	17.2	13.2	8.43	5.85	4.30	3.29	2.71	2.27
34.9	28.0	23.3	20.0	17.5	14.0	11.6	9.98	8.74	7.49	6.42
25.9	20.7	17.3	13.7	10.5	6.72	4.67	3.43	2.62	1.68	1.39
31.0	24.8	20.6	17.7	15.5	12.4	10.3	8.85	7.74	6.82	5.84
22.9	18.4	15.3	12.1	9.23	5.91	4.10	3.01	2.31	1.48	1.17
31.7	25.3	21.1	16.1	15.8	12.7	10.6	9.04	7.91	6.33	5.28
23.4	18.8	14.6	10.7	8.19	5.24	3.64	2.67	2.05	1.31	0.910
25.1	20.1	16.7	14.3	12.5	10.0	8.36	7.17	6.27	5.02	4.18
23.6	14.9	8.22	6.29	4.03	2.80	2.05	1.57	1.01	0.699	0.514

Notes: (1) \* indicates bending about minor principal Y axis for the axis shown in the diagram.

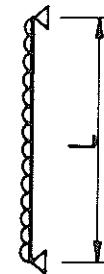
(2) The effective Length for Tees is the maximum effective length of a segment for which  $\phi M_b = \phi M_{sc}$  assuming  $\alpha_m = 1.0$ .

(3)\*\* these sections which are bent about the Y axis do not buckle laterally, and have no requirements for the maximum segment length to achieve the full section capacity.

(4) Shading indicates serviceability load governed by yielding.

(5) Grade 300 refers to BHP Grade 300PLUS™. See Note (i) on page 2-2.

TABLE 5.1-8(1)  
**TEES CUT FROM UNIVERSAL BEAMS  
GRADE 300**



**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT**  
bending about x-axis  
stem up — stem in compression

$W_{L1}^*$ : Maximum Design Load based on Moment  
 $W_{L2}^*$ : Maximum Design Load based on Shear  
 $W_L^*$ : Maximum Design Load is LESSER of  $W_{L1}^*$  and  $W_{L2}^*$   
 $W_S^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield

Designation	$W_{L1}^* / W_S^*$ (kN) / Span in metres								Effective Length m	
	1	1.25	1.5	1.75	2	2.5	3	3.5		
305BT62.5	561	465	388	332	291	233	194	166	116	96.9
	635	532	442	387	332	285	222	190	165	85.6
305BT56.5	477	382	318	273	239	191	159	136	119	95.4
	616	442	411	355	318	265	225	184	154	79.5
305BT50.5	396	317	264	226	198	158	132	113	99.0	113
	612	400	403	350	316	265	225	175	153	78.2
265BT46.3	363	290	242	207	181	145	121	104	90.6	66.0
	464	377	310	265	232	185	155	133	116	96.8
265BT41.0	296	237	197	169	148	118	98.6	84.5	73.9	60.4
	428	342	285	244	214	173	143	122	107	92.5
230BT41.1	316	233	211	181	158	127	105	90.4	79.1	63.3
	347	263	224	192	162	135	112	95.2	84.2	52.7
230BT37.3	262	210	175	150	131	105	87.3	74.9	65.5	41.9
	307	245	205	175	153	123	102	87.7	76.2	30.8
230BT33.6	210	168	140	120	105	84.1	70.1	60.1	54.6	37.4
	352	225	188	161	147	113	94.6	84.6	70.6	23.7
205BT29.9	166	133	111	95.1	83.2	66.6	55.5	47.6	41.6	34.5
	229	169	140	120	105	85.9	63.8	53.8	43.4	23.3
205BT26.9	150	120	100	85.9	75.1	60.1	50.1	42.9	37.6	17.1
	212	132	112	121	105	84.9	70.3	60.7	51.1	30.1
180BT28.4	161	129	108	92.2	80.7	64.6	53.8	46.7	37.2	25.0
	167	134	111	95.4	83.5	68.8	55.7	47.7	41.6	30.0
180BT25.4	136	109	90.8	77.9	68.1	54.5	45.4	38.9	34.1	23.8
	152	120	101	86.6	76.2	60.2	50.2	45.0	33.2	22.7
180BT22.4	114	90.9	75.7	64.9	56.8	45.4	37.9	32.5	28.4	21.3
	146	129	106	84.8	74.2	59.3	39.3	30.1	19.2	16.2

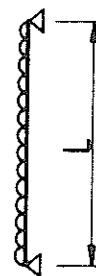
Notes: (1) The effective length for Tees is the maximum effective length of a segment for which  $\phi M_b = \phi M_{sx}$  assuming  $\alpha_m = 1.0$ . For all sections there is no segment length for which the full section section capacity can be attained.

(2) Shading indicates serviceability load governed by yielding.  
(3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

**TABLE 5.1-8(2)**  
**TEES CUT FROM UNIVERSAL BEAMS**  
**GRADE 300**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT**  
**bending about x-axis**

stem up — stem in compression



$W_{L1}^*$ : Maximum Design Load based on Moment

$W_{L2}^*$ : Maximum Design Load based on Shear

$W_L^*$ : Maximum Design Load is LESSER of  $W_{L1}^*$  and  $W_{L2}^*$

$W_S^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield

Designation	$W_L^*$ (kN) / $W_S^*$ (kN) Span in metres								$W_{L2}^*$ kN	Effective Length m
	1	1.25	1.5	1.75	2	2.5	3	3.5		
155BT23.1	99.4	79.6	66.3	56.8	49.7	39.8	33.1	28.4	19.9	16.6
155BT20.2	102	83.2	69.2	55.5	45.2	34.7	26.6	20.4	14.2	12.4
155BT20.2	82.0	65.6	54.7	46.9	41.0	32.8	27.3	20.5	13.0	6.65
155BT16.0	22.4	72.5	62.3	56.3	49.7	39.8	32.0	23.4	16.4	5.09
155BT16.0	57.9	46.3	38.6	33.1	28.9	23.1	19.3	16.5	11.5	10.2
125BT18.7	85.3	68.2	58.9	46.0	42.7	34.7	26.4	19.4	14.5	5.98
125BT18.7	75.0	60.0	50.0	42.9	37.5	30.0	25.0	21.4	18.8	8.27
125BT15.7	72.2	58.5	49.9	33.5	35.6	28.6	19.8	14.6	12.5	4.51
125BT15.7	66.9	53.6	44.6	38.3	33.5	26.8	22.3	19.1	17.2	2.73
125BT12.9	67.1	53.7	44.8	36.4	32.6	25.3	17.6	12.9	10.7	2.46
125BT12.9	44.5	35.6	29.6	25.4	22.2	17.8	14.8	12.7	11.1	0.00
100BT14.9*	55.5	42.8	35.7	31.6	26.8	20.0	13.9	10.2	7.80	3.77
100BT14.9*	52.8	42.3	35.2	30.2	26.4	21.1	17.6	13.2	10.6	0.00
100BT12.7*	46.6	37.3	37.1	26.6	22.9	14.7	10.2	7.47	5.72	***
100BT12.7*	45.4	36.3	30.2	25.9	22.7	18.1	15.1	13.0	11.3	0.00
100BT11.1	45.5	32.2	27.6	23.6	19.9	12.7	8.82	6.48	4.40	3.23
100BT11.1	36.0	28.8	24.0	20.6	18.0	14.4	12.0	10.3	7.41	5.56
100BT 9.1	25.6	22.5	23.7	20.3	17.1	10.9	7.59	5.58	4.27	2.55
100BT 9.1	29.1	23.3	19.4	16.6	14.5	11.6	9.69	8.31	7.23	1.95
90BT11.1	32.3	24.2	20.2	17.3	14.0	8.96	6.22	7.27	5.82	4.85
90BT11.1	38.0	30.4	25.3	21.7	19.0	15.2	12.7	9.07	7.54	4.15
90BT 9.1	32.0	25.5	22.2	17.2	13.2	8.43	5.85	4.30	3.50	3.64
90BT 9.1	28.6	22.8	19.0	16.3	14.3	11.4	9.52	8.16	7.14	1.07
90BT 8.1	25.9	20.7	17.3	13.7	10.5	6.72	4.67	4.67	5.71	4.08
90BT 8.1	21.0	19.2	16.0	13.7	12.0	9.62	8.01	6.87	6.01	0.857
75BT 9.0	22.9	18.4	15.3	12.1	9.23	5.91	4.10	3.07	2.31	0.656
75BT 9.0	29.3	23.4	19.5	16.7	14.6	11.7	9.75	8.36	7.32	3.01
75BT 7.0	23.4	18.8	14.6	10.7	8.19	5.24	3.64	2.67	4.88	1.03
75BT 7.0	21.9	17.5	14.6	12.5	10.9	8.75	7.29	6.25	4.37	0.669
75BT 7.0	18.6	14.3	11.2	8.22	6.29	4.03	2.80	2.05	1.57	0.514

Notes: (1) \* indicates bending about minor principal y-axis for the axis shown in the diagram.

(2) The effective Length for Tees is the maximum effective length of a segment for which  $\phi M_b = \phi M_{ex}$  assuming  $\alpha_m = 1.0$ . \*\*\* these sections which are bent about the y axis do not buckle laterally, and have no requirements for the maximum segment length to achieve the full section capacity. For other sections there is no segment length for which the the full section section capacity can be attained.

(3) Shading indicates serviceability loads governed by yielding.

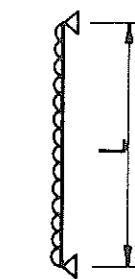


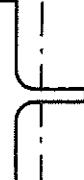
TABLE 5.1-9  
TEES CUT FROM UNIVERSAL COLUMNS  
GRADE 300  
MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
bending about y-axis  
stem down — flange in compression

$W_{L1}^*$ : Maximum Design Load based on Moment

$W_{L2}^*$ : Maximum Design Load based on Shear

$W_L^*$ : Maximum Design Load is LESSER of  $W_{L1}^*$  and  $W_{L2}^*$

$W_s^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield

STEM DOWN  


y—

Designation	$W_{L1}^* / W_s^*$ (kN) Span in metres								$W_{L2}^*$ kN
	1	1.25	1.5	1.75	2	2.5	3	3.5	
165CT79.0	342	274	228	195	171	137	114	97.7	85.5
155CT68.5	253	203	169	145	127	101	84.4	72.7	57.6
155CT76.5	292	234	195	167	146	117	97.3	83.4	73.0
155CT59.0	216	172	142	125	105	85.2	72.1	67.0	48.6
155CT117.0	245	196	164	140	123	98.2	81.8	70.1	49.1
155CT148.4	192	145	121	104	90.9	72.7	60.6	52.0	40.5
155CT144.8	198	158	132	113	98.8	79.1	65.9	56.5	49.4
125CT36.5	158	126	105	86.5	76.8	63.0	52.5	42.3	32.4
125CT44.8	147	117	97.8	83.8	73.3	58.7	48.9	41.9	36.7
109CT26.1	109	86.9	72.4	62.1	51.3	43.5	35.4	26.0	19.9
100CT23.1	122	97.5	81.3	69.6	60.9	48.8	40.6	34.8	26.4
92.3	92.3	73.9	61.6	52.6	46.2	36.9	27.8	20.4	15.6
89.6	89.6	71.6	59.7	51.2	44.8	35.8	29.9	25.6	22.4
65.3	65.3	53.7	44.2	37.9	33.2	23.2	16.7	11.8	9.06
75.5	75.5	60.4	50.3	43.1	37.8	30.2	25.2	21.6	18.9
55.9	55.9	44.7	37.3	32.0	28.0	19.4	13.5	9.92	7.59
65.0	65.0	52.0	43.4	37.2	32.5	26.0	21.7	18.6	13.3
49.9	49.9	36.4	30.4	23.3	23.5	20.0	17.2	11.9	8.76
75CT18.6	45.5	36.4	30.4	26.0	22.8	18.2	15.2	13.0	11.4
75CT15.0	35.7	27.0	22.5	18.2	14.0	8.94	6.21	4.56	3.49
75CT11.7	38.2	30.6	25.5	21.8	19.1	15.3	12.7	10.9	9.55
28.3	28.3	22.6	18.9	14.2	10.9	6.95	4.83	3.55	2.71
24.6	24.6	19.7	16.1	11.8	9.03	5.78	4.01	2.95	2.26
50CT 7.4	10.6	8.51	7.09	6.08	5.32	4.25	3.54	3.04	2.66
	7.32	4.68	3.25	2.39	1.83	1.17	0.813	0.597	0.457

Notes: (1) Structural Tees cut symmetrically from Universal Columns which are bent about y-axis do not buckle laterally and have no requirements for maximum segment length to achieve the full nominal section capacity.

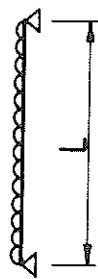
(2) Shading indicates serviceability loads governed by yielding.  
(3) Grade 300 refers to BHP 300PLUS™. See Note (1) on page 2-2.

TABLE 5.1-10

**TEES CUT FROM UNIVERSAL COLUMNS  
GRADE 300**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
bending about y-axis**

stem up — stem in compression

 $W_L^*$ : Maximum Design Load based on Moment $W_L^t$ : Maximum Design Load based on Shear $W_L^s$ : Maximum Design Load is LESSER of  $W_L^*$  and  $W_L^t$  $W_s^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield

Designation	$W_L^s$ (kN) / $W_s^*$ (kN) Span in metres								$W_{L2}^*$ kN
	1	1.25	1.5	1.75	.2	2.5	3	3.5	
15SCT79.0	340	272	227	194	170	136	113	97.1	85.0
15SCT68.5	253	203	175	145	127	103	84.4	72.4	57.6
15SCT73	283	226	188	161	141	113	94.2	80.7	70.6
15SCT59.0	216	173	144	123	108	86.5	72.1	61.3	56.5
15SCT62	229	183	153	131	114	91.6	76.3	65.4	48.6
15SCT48.4	182	145	121	104	97.9	72.7	60.6	52.0	57.2
15SCT48.4	185	148	123	106	92.6	74.1	61.7	52.9	40.5
125CT44.8	138	125	105	80.1	78.8	63.0	52.5	42.3	32.4
140	112	93.2	79.9	69.9	55.9	46.6	39.9	34.9	20.7
109	96.9	86.9	72.4	62.1	54.3	43.4	35.4	26.0	19.9
111	88.9	88.9	74.0	63.5	55.5	44.4	37.0	31.7	22.2
92.3	72.9	61.6	52.6	46.2	36.9	27.8	20.4	15.6	18.5
109CT29.8	86.6	69.3	57.8	49.5	43.3	34.7	28.9	24.8	21.7
100CT26.1	86.3	53.1	44.2	37.2	32.2	23.2	16.7	11.8	17.3
70.3	56.3	46.9	40.2	35.2	32.1	28.1	23.4	20.1	9.06
25.9	24.7	37.3	32.6	26.0	19.4	13.5	9.92	7.59	14.1
61.2	48.9	40.8	34.9	30.6	24.5	20.4	17.5	15.3	17.6
49.9	39.9	33.3	28.5	25.0	17.2	11.9	8.76	6.70	10.2
75CT18.6	45.3	36.2	30.2	25.9	22.6	18.1	15.1	12.9	11.3
75CT15.0	33.7	27.0	22.5	18.2	14.0	8.94	6.21	4.56	3.49
36.1	28.8	24.0	20.6	18.0	14.4	12.0	10.3	9.01	7.21
25.3	22.7	18.9	14.2	10.9	6.95	4.83	3.55	2.71	2.71
30.7	24.6	20.5	17.5	15.3	12.3	10.2	8.77	7.67	6.14
24.6	16.7	16.7	11.8	9.03	5.78	4.01	2.95	2.26	1.44
50CT 7.4	10.6	8.48	7.06	6.05	5.30	4.24	3.53	3.03	2.65
	7.32	4.68	3.25	2.39	1.83	1.17	0.813	0.597	0.457

Notes: (1) Structural Tees cut symmetrically from Universal Columns which are bent about y-axis do not buckle laterally and have no requirements for maximum segment length to achieve the full nominal section capacity.

(2) Shading indicates serviceability loads governed by yielding.

(3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

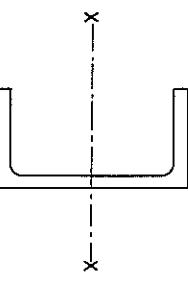


TABLE 5.1-11

**PARALLEL FLANGE CHANNELS  
GRADE 300**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
bending about x-axis**

$W_{t1}^*$ : Maximum Design Load based on Moment

$W_{t2}^*$ : Maximum Design Load based on Shear

$W_L^*$ : Maximum Design Load is LESSER of  $W_{t1}^*$  and  $W_{t2}^*$

$W_s^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield

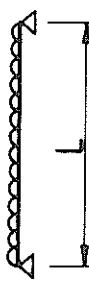
Designation	Mass per metre	$W_{L1}^* (\text{kN}) / W_{L2}^* (\text{kN})$ Span in metres										FLR m									
		1	1.25	1.5	1.75	2	2.5	3	3.5	4	5	6	7	8	9	10					
380 PFC	55.2	1910	1530	1270	1090	954	763	636	545	477	382	318	273	238	212	191	1310	0.803			
300 PFC	40.1	1220	974	812	696	594	475	395	315	259	203	174	146	115	93.2	829	0.719				
250 PFC	35.5	909	727	606	527	472	379	329	295	243	203	174	152	135	122	829	0.719				
230 PFC	25.1	586	593	578	545	495	433	347	283	226	173	111	77.0	56.6	43.3	34.2	691	0.726			
200 PFC	22.9	477	479	447	412	372	319	279	235	195	167	117	97.7	83.7	73.3	65.1	517	0.600			
180 PFC	20.9	392	398	367	355	325	295	262	239	191	159	136	103	65.8	45.7	33.6	25.7	415	0.609		
150 PFC	17.7	377	377	301	251	215	185	155	139	96.5	112	95.8	73.4	46.9	32.6	24.0	14.5	11.7	0.609		
		295	295	228	228	197	169	148	118	98.7	82.0	56.9	41.8	32.0	20.5	14.2	10.5	8.01	5.12	311	0.591

Notes: (1) FLR = segment length for full lateral restraint, based on transverse load case ( $\beta_m = -0.8$ ).

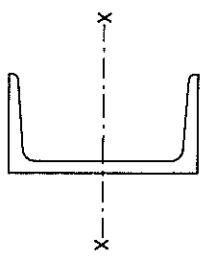
(2) Shading indicates serviceability loads governed by yielding.

(3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

TABLE 5.1-12

**TAPER FLANGE CHANNELS  
GRADE 250**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
bending about x-axis**

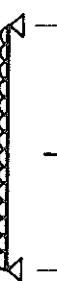
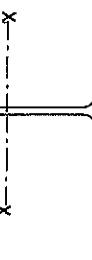
$W_{L1}^*$ : Maximum Design Load based on Moment  
 $W_{L2}^*$ : Maximum Design Load based on Shear  
 $W_L^*$ : Maximum Design Load is LESSER of  $W_{L1}^*$  and  $W_{L2}^*$   
 $W_S^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield



Designation	Mass per metre	$W_{L1}^*(\text{kN}) / W_S^*(\text{kN})$ Span in metres										FLR						
		1	1.25	1.50	1.75	2	2.5	3	3.5	4	5	6	7	8	9	10	FLR	
125 TFC	13.4	149	119	99.0	84.9	74.3	59.4	49.5	42.4	37.1	29.7	24.8	21.2	18.6	16.5	14.9	211	
100 TFC	9.34	82.9	66.3	55.3	47.4	41.4	33.2	27.6	23.7	20.7	16.6	13.8	11.8	10.4	9.07	3.21	2.60	0.522
75 TFC	6.65	43.1	34.5	28.7	24.6	21.6	17.5	12.8	9.44	7.23	4.62	3.21	2.36	1.81	1.43	1.16	0.829	140
		30.0	28.4	19.7	14.5	11.1	7.09	4.92	3.62	2.77	1.77	1.23	0.82	0.692	0.547	0.443	0.319	

Notes: (1) FLR, segment length for full lateral restraint, based on transverse load case ( $\beta_m = -0.8$ ).  
(2) Shading indicates serviceability loads governed by yielding.

TABLE 5.1-13

**TAPER FLANGE BEAMS  
GRADE 250**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
bending about x-axis**


$W_{L1}^*$ : Maximum Design Load based on Moment  
 $W_{L2}^*$ : Maximum Design Load based on Shear  
 $W_L^*$ : Maximum Design Load is LESSER of  $W_{L1}^*$  and  $W_{L2}^*$   
 $W_S^*$ : Serviceability Load based on Deflection Limit of Span/250 or First Yield

Designation	Mass per metre	$W_{L1}^*(\text{kN}) / W_S^*(\text{kN})$ Span in metres										FLR				
		1	1.25	1.5	1.75	2	2.5	3	3.5	4	5	6	7	8	9	10
125 TFB	13.1	150	120	100	85.9	75.1	60.1	42.9	37.6	30.1	25.0	21.5	18.8	16.7	15.0	176
100 TFB	7.20	63.8	51.0	42.5	36.5	66.7	42.7	29.6	21.8	16.7	7.41	5.44	4.17	3.29	2.67	0.556

Notes: (1) FLR, segment length for full lateral restraint, based on transverse load case ( $\beta_m = -0.8$ ).  
(2) Shading indicates serviceability loads governed by yielding.

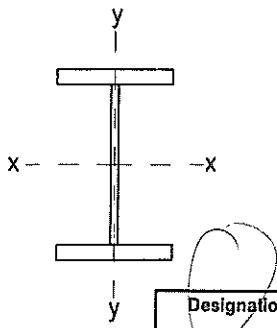


TABLE 5.2-1

**WELDED BEAMS  
GRADE 300**  
**DESIGN SECTION MOMENT AND WEB CAPACITIES**

Designation	Design Section Moment Capacities					Design Web Capacities		
	About x-axis		About y-axis			$\phi V_v$	$\frac{\phi R_{bb}}{b_b}$	$\frac{\phi R_{by}}{b_{bf}}$
	$\phi M'_{sx}$	$\phi M''_{sx}$	FLR	$\phi M_{sy}$	kNm			
	kNm	kNm	kNm	m	kNm	kN	kN/mm	kN/mm
1200WB455	7110	7110	7110	3.40	1260	2900	0.783	5.40
423	6510	6510	6510	3.34	1130	2900	0.783	5.40
392	5910	5910	5910	3.28	1010	2900	0.783	5.40
342	4980	4980	4450	2.51	646	2900	0.783	5.40
317	4500	4500	4050	2.44	565	2900	0.783	5.40
278	3790	3790		2.02	387	2900	0.783	5.40
249	3250	3250		1.49	239	2900	0.783	5.40
1000WB322	4130	4130	3670	2.59	646	2490	1.02	5.40
296	3720	3720	3320	2.52	565	2490	1.02	5.40
258	3100	3100		2.09	387	2490	1.02	5.40
215	2580	2580		1.57	244	2490	1.02	5.40
900WB282	3440	3440	3000	2.76	645	1730	0.566	4.18
257	3070	3070	2700	2.71	565	1730	0.566	4.18
218	2510	2510		2.27	386	1730	0.566	4.18
175	2020	2020		1.74	243	1730	0.566	4.18
800WB192	2030	2030		2.04	318	1190	0.425	3.49
168	1720	1720		1.81	238	1190	0.425	3.49
146	1540	1420		1.67	204	1190	0.425	3.49
122	1220	1130		1.42	135	1190	0.425	3.49
700WB173	1610	1610		1.88	267	1100	0.544	3.49
150	1350	1350		1.66	197	1100	0.544	3.49
130	1210	1110		1.53	169	1100	0.544	3.49
115	1020	944		1.46	134	1100	0.544	3.49

Notes: (1) FLR based on most conservative case ( $\beta_m = -1$ ).  
(2)  $\phi M'_{sx}$  — for sections with two holes on tension flange.  
(3)  $\phi M''_{sx}$  — for sections with four holes on tension flange.

TABLE 5.2-2

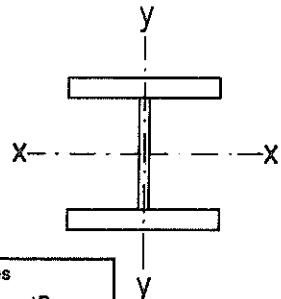
**WELDED BEAMS  
GRADE 400**  
**DESIGN SECTION MOMENT AND WEB CAPACITIES**

Designation	Design Section Moment Capacities					Design Web Capacities		
	About x-axis		About y-axis			$\phi V_v$	$\frac{\phi R_{bb}}{b_b}$	$\frac{\phi R_{by}}{b_{bf}}$
	$\phi M'_{sx}$	$\phi M''_{sx}$	FLR	$\phi M_{sy}$	kNm			
	kNm	kNm	kNm	m	kNm	kN	kN/mm	kN/mm
1200WB455	9090	9090	8190	3.00	1620	3320	0.806	6.84
423	8320	8320	7520	2.95	1460	3320	0.806	6.84
392	7550	7550	6860	2.89	1260	3320	0.806	6.84
342	6360	6020	5660	2.22	830	3320	0.806	6.84
317	5750	5460	5150	2.15	723	3320	0.806	6.84
278	4830	4570		1.78	497	3320	0.806	6.84
249	4140	3880		1.31	308	3320	0.806	6.84
1000WB322	5310	5030	4720	2.28	830	3150	1.06	6.84
296	4780	4540	4270	2.22	723	3150	1.06	6.84
258	3990	3770		1.85	497	3150	1.06	6.84
215	3270	3090		1.40	303	3150	1.06	6.84
900WB282	4370	4090	3780	2.44	830	1820	0.583	5.40
257	3900	3660	3390	2.39	721	1820	0.583	5.40
218	3190	2980		2.00	495	1820	0.583	5.40
175	2500	2320		1.55	302	1820	0.583	5.40
800WB192	2540	2310		1.80	408	1190	0.437	4.50
168	2150	1950		1.59	307	1190	0.437	4.50
146	1880	1710		1.49	258	1190	0.437	4.50
122	1480	1350		1.26	166	1190	0.437	4.50
700WB173	2070	1890		1.66	343	1380	0.562	4.50
150	1740	1580		1.46	253	1380	0.562	4.50
130	1540	1410		1.36	214	1380	0.562	4.50
115	1300	1200		1.30	166	1380	0.562	4.50

Notes: (1) FLR based on most conservative case ( $\beta_m = -1$ ).  
(2)  $\phi M'_{sx}$  — for sections with two holes on tension flange.  
(3)  $\phi M''_{sx}$  — for sections with four holes on tension flange.

TABLE 5.2-3

**WELDED COLUMNS  
GRADE 300**  
**DESIGN SECTION MOMENT AND WEB CAPACITIES**



Designation	Design Section Moment Capacities					Design Web Capacities		
	About x-axis		About y-axis			$\phi V_v$	$\frac{\phi R_{bb}}{b_b}$	$\frac{\phi R_{by}}{b_{bf}}$
	$\phi M_{sx}$	$\phi M'_{sx}$	$\phi M''_{sx}$	FLR	$\phi M_{sy}$			
	kNm	kNm	kNm	m	kNm	kN	kN/mm	kN/mm
500WC440	2620	2620	2620	3.46	1260	2420	9.42	12.6
414	2540	2540	2540	3.56	1260	1940	7.27	10.1
383	2300	2300	2300	3.52	1140	1940	7.27	10.1
340	2260	2260	2260	3.52	1010	1700	5.18	7.87
290	1910	1910	1910	3.56	860	1460	3.97	6.75
267	1690	1690	1690	3.51	747	1460	3.97	6.75
228	1410	1410	1200	3.28	593	1460	3.97	6.75
400WC361	1880	1880	1650	2.74	810	2120	9.59	12.6
328	1790	1790	1550	2.87	808	1480	6.36	8.82
303	1620	1620	1400	2.83	727	1480	6.36	8.82
270	1430	1430	1240	2.83	646	1320	5.55	7.87
212	1100	1100	954	2.82	504	1130	4.43	6.75
181	922	922	781	2.64	408	1130	4.43	6.75
144	698	698	566	2.64	303	907	3.23	5.40
350WC280	1240	1240		2.54	618	1160	6.61	8.82
258	1120	1120		2.51	557	1160	6.61	8.82
230	986	986		2.51	495	1040	5.81	7.87
197	844	844		2.53	433	891	4.74	6.75

Notes: (1) FLR based on most conservative case ( $\beta_m = -1$ ).  
(2)  $\phi M_{sx}$  — for sections with two holes on tension flange.  
(3)  $\phi M''_{sx}$  — for sections with four holes on tension flange.

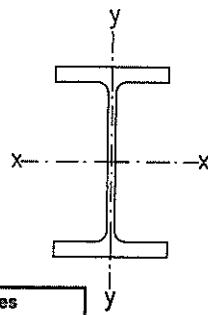
TABLE 5.2-4

**WELDED COLUMNS  
GRADE 400**  
**DESIGN SECTION MOMENT AND WEB CAPACITIES**

Designation	Design Section Moment Capacities					Design Web Capacities		
	About x-axis		About y-axis			$\phi V_v$	$\frac{\phi R_{bb}}{b_b}$	$\frac{\phi R_{by}}{b_{bf}}$
	$\phi M_{sx}$	$\phi M'_{sx}$	$\phi M''_{sx}$	FLR	$\phi M_{sy}$			
	kNm	kNm	kNm	m	kNm	kN	kN/mm	kN/mm
500WC440	3370	3370	3040	3.05	1620	3010*	11.9	16.2
414	3270	3270	2930	3.14	1620	2490	9.10	13.0
383	2960	2960	2660	3.10	1460	2490	9.10	13.0
340	2860	2860	2540	3.11	1270	2190	6.35	10.1
290	2400	2400	2090	3.14	1070	1850	4.68	8.55
267	2120	2120	1830	3.10	928	1850	4.68	8.55
228	1660	1530	1390	2.92	717	1850	4.68	8.55
400WC361	2420	2280	2120	2.41	1040	2690*	12.1	16.2
328	2300	2160	1990	2.53	1040	1910	7.97	11.3
303	2080	1950	1800	2.50	935	1910	7.97	11.3
270	1830	1720	1590	2.49	831	1700	6.91	10.1
212	1380	1290	1180	2.49	631	1440	5.36	8.55
181	1140	1040	945	2.34	499	1440	5.36	8.55
144	824	741	657	2.34	367	1150	3.82	6.84
350WC280	1600	1480		2.24	795	1500	8.34	11.3
258	1440	1340		2.21	716	1500	8.34	11.3
230	1270	1180		2.21	636	1340	7.30	10.1
197	1080	1000		2.23	556	1130	5.82	8.55

Notes: (1) FLR based on most conservative case ( $\beta_m = -1$ ).  
(2)  $\phi M_{sx}$  — for sections with two holes on tension flange.  
(3)  $\phi M''_{sx}$  — for sections with four holes on tension flange.  
(4) \* indicates shear capacity governed by the shear capacity of the weld.

TABLE 5.2-5  
**UNIVERSAL BEAMS  
GRADE 300**  
**DESIGN SECTION MOMENT AND WEB CAPACITIES**

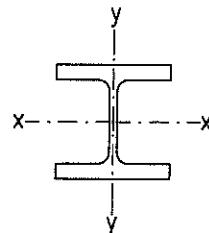


Designation	Design Section Moment Capacities				Design Web Capacities		
	About x-axis		About y-axis		$\phi V_v$	$\frac{\phi R_{bb}}{b_b}$	$\frac{\phi R_{by}}{b_{bf}}$
	$\phi M_{bx}$	$\phi M'_{sx}$	FLR	$\phi M_{sy}$			
	kNm	kNm	m	kNm	kN	kN/mm	kN/mm
610UB125	927	927	1.41	130	1180	1.07	4.02
113	829	829	1.38	114	1100	0.921	3.78
101	782	782	1.30	104	1100	0.810	3.82
530UB 92.4	640	589	1.23	92.2	939	0.903	3.67
82.0	558	515	1.20	78.0	876	0.773	3.46
460UB 82.1	496	450	1.16	79.0	788	1.06	3.56
74.6	449	407	1.14	70.8	719	0.861	3.28
67.1	399	363	1.13	62.0	667	0.724	3.06
410UB 59.7	324	291	1.09	54.9	548	0.698	2.81
53.7	304	275	1.02	49.8	529	0.654	2.74
360UB 56.7	273	244	1.07	52.0	496	0.907	2.88
50.7	242	216	1.05	45.5	449	0.725	2.63
44.7	222	198	0.997	40.4	420	0.630	2.48
310UB 46.2	197	173	1.07	44.0	356	0.740	2.41
40.4	182	161	1.02	40.0	320	0.588	2.20
32.0	134	117	0.873	25.0	283	0.456	1.98
250UB 37.3	140	120	0.915	33.5	283	0.857	2.30
31.4	114	98.8	0.885	26.3	265	0.769	2.20
25.7	92.0	80.8	0.741	17.8	214	0.484	1.80
200UB 29.8	90.0	76.9	0.842	24.9	225	1.06	2.27
25.4	74.6	63.3	0.816	19.8	204	0.897	2.09
22.3	65.3	54.5	0.821	17.4	174	0.650	1.80
18.2	51.8	†	0.587	9.92	154	0.522	1.62
180UB 22.2	56.2	†	0.551	11.7	186	1.12	2.16
18.1	45.2	†	0.546	9.36	151	0.788	1.80
16.1	39.8	†	0.542	8.19	135	0.630	1.62
150UB 18.0	38.9	†	0.454	7.74	161	1.24	2.16
14.0	29.3	†	0.441	5.70	130	0.912	1.80

Notes:

- (1) FLR based on most conservative case ( $\beta_m = -1$ ).
- (2)  $\phi M'_{sx}$  — for sections with two holes on tension flange.
- (3) † indicates flange too small for high strength structural bolts.
- (4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

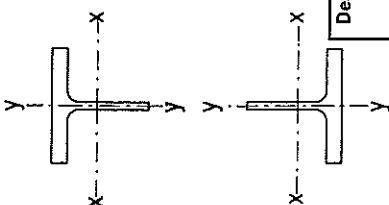
TABLE 5.2-6  
**UNIVERSAL COLUMNS  
GRADE 300**  
**DESIGN SECTION MOMENT AND WEB CAPACITIES**



Designation	Design Section Moment Capacities				Design Web Capacities		
	About x-axis		About y-axis		$\phi V_v$	$\frac{\phi R_{bb}}{b_b}$	$\frac{\phi R_{by}}{b_{bf}}$
	$\phi M_{bx}$	$\phi M'_{sx}$	FLR	$\phi M_{sy}$			
	kNm	kNm	m	kNm	kN	kN/mm	kN/mm
310UC158	676	676	2.24	305	832	3.47	5.30
137	580	580	2.22	261	717	2.90	4.66
118	494	494	2.20	222	606	2.32	4.02
96.8	422	422	2.10	187	527	1.76	3.56
250UC 89.5	309	309	1.85	143	472	2.24	3.78
72.9	266	266	1.77	123	377	1.62	3.10
200UC 59.5	177	158	1.42	80.6	337	2.08	3.35
52.2	154	137	1.41	70.3	285	1.66	2.88
46.2	133	118	1.40	60.3	257	1.43	2.63
150UC 37.2	83.6	71.2	1.05	36.9	226	1.91	2.92
30.0	71.9	61.2	1.01	31.7	180	1.42	2.38
23.4	50.7	41.9	0.969	21.2	161	1.26	2.20
100UC 14.8	21.4	16.1	0.650	9.91	83.8	1.19	1.80

Notes:

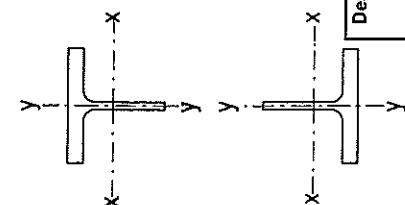
- (1) FLR based on most conservative case ( $\beta_m = -1$ ).
- (2)  $\phi M'_{sx}$  — for sections with two holes on tension flange.
- (3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 5.2-7  
TEES CUT FROM UNIVERSAL BEAMS  
GRADE 300**

**DESIGN SECTION MOMENT AND WEB CAPACITIES**

Designation	Design Section Moment Capacities				Design Shear Capacity $\phi V_y$ kN	
	About x-axis		About y-axis			
	Stem Down	Stem Up	Effective Length	$\phi M_{x,s}$		
$\phi M_{x,t}$ kNm	m	kNm	m	kNm		
305BT62.5 56.5 50.5	112 104 103	2.27 2.17 1.98	72.7 59.6 49.5	0.00 0.00 0.00	64.9 56.8 52.1	
265BT46.3 41.0	78.3 72.1	1.94 1.84	45.3 37.0	0.00 0.00	46.1 39.0	
230BT41.1 37.3 33.6	56.8 51.8 47.6	1.90 1.85 1.78	39.5 32.7 26.3	0.00 0.00 0.00	34.6 35.4 31.0	
205BT29.9 26.9	35.3 35.8	1.79 1.61	20.8 18.8	0.00 0.00	27.4 24.9	
180BT28.4 25.4 22.4	28.2 25.4 24.4	1.83 1.76 1.61	20.2 17.0 14.2	0.00 0.00 0.00	26.0 22.7 20.2	
155BT23.1 20.2 16.0	17.6 16.8 13.6	1.96 1.76 1.47	12.4 10.2 7.23	0.00 0.00 0.00	154 139 123	
125BT18.7 15.7 12.9	12.3 11.2 9.03	1.69 1.49 1.28	9.38 8.37 5.56	0.00 0.00 0.00	16.7 13.2 8.88	
100BT14.9* 12.7* 11.2*	7.86 6.92 5.62	*** *** ***	6.60 5.67 4.50	*** *** ***	12.4 9.90 8.68	
90BT11.1 9.1 8.1	5.40 5.11 3.92	1.10 1.03 3.87	4.75 3.64 3.01	0.00 0.00 0.00	5.85 4.68 4.09	
75BT 9.0 7.0	3.96 3.14	0.920 0.801	3.66 2.73	0.00 0.00	3.87 2.85	
					69.7 56.2	



**TABLE 5.2-8  
TEES CUT FROM UNIVERSAL COLUMNS  
GRADE 300**

**DESIGN SECTION MOMENT AND WEB CAPACITIES**

Designation	Design Section Moment Capacities				Design Shear Capacity $\phi V_y$ kN	
	About y-axis		About x-axis			
	Stem Down	Stem Up	Effective Length	$\phi M_{y,t}$		
$\phi M_{y,t}$ kNm	m	kNm	m	kNm		
155CT79.0 68.5	42.7	42.5	42.7	42.5	357	
155CT79.0 68.5	36.5	35.3	36.5	35.3	308	
155CT79.0 68.5	30.7	28.6	30.7	28.6	260	
155CT79.0 68.5	24.7	23.1	24.7	23.1	226	
125CT44.8 36.5	18.3	17.5	18.3	17.5	202	
125CT44.8 36.5	15.2	13.9	15.2	13.9	161	
100CT29.8 26.1	11.2	10.8	11.2	10.8	144	
100CT29.8 26.1	9.44	8.79	9.44	8.79	122	
100CT29.8 26.1	8.13	7.64	8.13	7.64	110	
75CT18.6 15.0	5.69	5.66	5.69	5.66	96.9	
75CT18.6 15.0	4.78	4.51	4.78	4.51	76.8	
75CT18.6 15.0	3.53	3.84	3.53	3.84	68.9	
50CT 7.4 7.4	1.33	1.32	1.33	1.32	4.95	
					35.4	

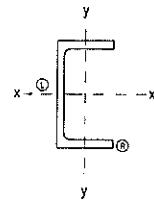
Notes:

- (1) Stem Down and  $\phi M_{x,t}$  is for bending about the x-axis which causes compression in the flange.
- (2) Stem Up and  $\phi M_{x,t}$  is for bending about the x-axis which causes compression in the stem.
- (3) \* indicates x- and y-axes are interchanged from that shown on the diagram.
- (4) The Effective Length for Tees is the maximum effective length of a segment for which  $\phi M_b = \phi M_{x,t}$  assuming  $a_m = 1.0$ .
- (5) \*\*\* indicates that bending is about y-axis and there is no maximum segment length required to achieve the full section moment capacity.
- (6) For other sections bending about the x-axis (stem up) there is no unrestrained segment length for which the full section moment capacity can be achieved.
- (7) Grade 300 refers to BHIP Grade 300PLUS™. See Note (1) on page 2-2.

Notes:

- (1) Stem Down and  $\phi M_{x,y}$  is for bending about the y-axis which causes compression in the flange.
- (2) Stem Up and  $\phi M_{x,y}$  is for bending about the y-axis which causes compression in the stem.
- (3) For all sections bending about the y-axis there is no maximum segment length required to achieve the full section moment capacity.
- (4) Grade 300 refers to BHIP Grade 300PLUS™. See Note (1) on page 2-2.

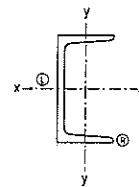
TABLE 5.2-9  
**PARALLEL FLANGE CHANNELS  
GRADE 300**  
**DESIGN SECTION MOMENT AND WEB CAPACITIES**



Designation	Mass per metre	Design Section Moment Capacities				Design Web Capacities		
		About x-axis		About y-axis		$\phi V_v$	$\frac{\phi R_{bb}}{b_b}$	$\frac{\phi R_{by}}{b_{bl}}$
		$\phi M_{bx}$	FLR	$\phi M_{syR}$	$\phi M_{syL}$			
kg/m		kNm	m	kNm	kNm	kN	kN/mm	kN/mm
380 PFC	55.2	238	0.574	33.8	28.9	657	1.44	3.60
300 PFC	40.1	152	0.514	26.1	22.2	415	1.19	2.88
250 PFC	35.5	114	0.518	24.0	24.0	346	1.45	2.88
230 PFC	25.1	73.3	0.428	13.6	12.2	258	1.03	2.34
200 PFC	22.9	59.7	0.435	13.2	12.6	207	1.02	2.16
180 PFC	20.9	49.0	0.435	12.1	12.1	187	1.12	2.16
150 PFC	17.7	37.0	0.422	11.1	11.1	156	1.27	2.16

Notes: (1) FLR based on most conservative case ( $\beta_m = -1$ ).  
(2)  $\phi M_{syR}$  — For bending about the y-axis that causes compression in the toe R.  
(3)  $\phi M_{syL}$  — For bending about the y-axis that causes compression in the web L.  
(4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

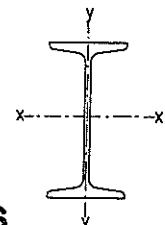
TABLE 5.2-10  
**TAPER FLANGE CHANNELS  
GRADE 250**  
**DESIGN SECTION MOMENT AND WEB CAPACITIES**



Designation	Mass per metre	Design Section Moment Capacities				Design Web Capacities		
		About x-axis		About y-axis		$\phi V_v$	$\frac{\phi R_{bb}}{b_b}$	$\frac{\phi R_{by}}{b_{bl}}$
		$\phi M_{ax}$	FLR	$\phi M_{syR}$	$\phi M_{syL}$			
kg/m		kNm	m	kNm	kNm	kN	kN/mm	kN/mm
125 TFC	13.4	18.6	0.373	4.72	4.72	105	1.16	1.75
100 TFC	9.34	10.4	0.290	2.64	2.64	70.2	0.990	1.46
75 TFC	6.65	5.39	0.228	1.46	1.46	52.7	1.06	1.46

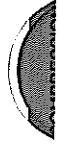
Notes: (1) FLR based on most conservative case ( $\beta_m = -1$ ).  
(2)  $\phi M_{syR}$  — For bending about the y-axis that causes compression in the toe R.  
(3)  $\phi M_{syL}$  — For bending about the y-axis that causes compression in the web L.

TABLE 5.2-11  
**TAPER FLANGE BEAMS  
GRADE 250**  
**DESIGN SECTION MOMENT AND WEB CAPACITIES**



Designation	Mass per metre	Design Section Moment Capacities				Design Web Capacities		
		About x-axis		About y-axis		$\phi V_v$	$\frac{\phi R_{bb}}{b_b}$	$\frac{\phi R_{by}}{b_{bl}}$
		$\phi M_{ax}$	FLR	$\phi M_{sy}$				
kg/m		kNm	m	kNm		kN	kN/mm	kN/mm
125 TFB	13.1	18.8	0.417	3.64		87.8	0.909	1.46
100 TFB	7.20	8.03	0.274	1.24		56.2	0.772	1.17

Note: FLR based on most conservative case ( $\beta_m = -1$ ).

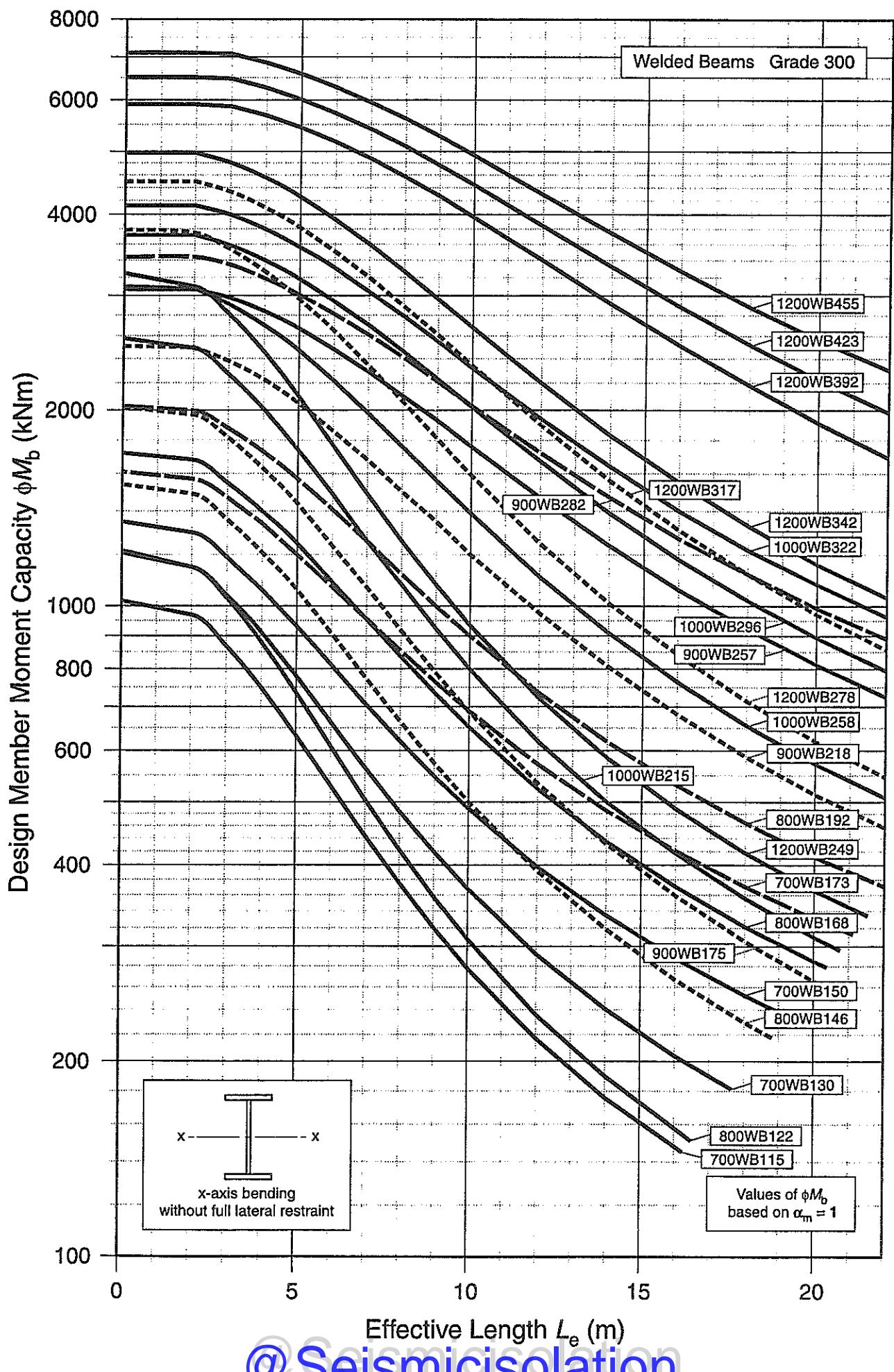


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**TABLE 5.3-1**  
**WELDED BEAMS**  
**GRADE 300**  
**DESIGN MOMENT CAPACITIES FOR MEMBERS WITHOUT FULL LATERAL RESTRAINT**  
**bending about x-axis**

Designation	$\phi M_{sx}$	$\phi V_r$	Design Member Moment Capacities, $\phi M_b$ (kNm)									
			Effective Length (L_e) in metres	9	8	7	6	5	4	3	2	1
1200WB455	7110	2900	7110	7080	6860	6590	6280	5980	5610	5270	4930	3740
423	6510	2900	6510	6480	6270	6010	5720	5410	5090	4760	4440	3840
382	5910	2900	5910	5870	5680	5440	5170	4880	4570	4270	3960	3400
342	4980	2900	4980	4810	4560	4260	3930	3600	3270	2960	2680	2200
317	4500	2900	4500	4340	4100	3820	3510	3200	2890	2610	2340	1900
278	3790	2900	3750	3540	3270	2960	2650	2340	2060	1810	1590	1250
249	3250	2900	3100	2810	2460	2100	1770	1490	1260	1080	934	724
1000WB222	4130	2490	4130	4000	3800	3560	3310	3040	2790	2550	2320	1940
296	3720	2490	3720	3590	3400	3180	2940	2700	2460	2230	2020	1670
258	3100	2490	3080	2910	2700	2470	2220	1980	1760	1560	1390	1180
215	2580	2490	2490	2270	2010	1740	1490	1280	1080	924	800	620
900WB282	3440	1730	3440	3350	3190	3010	2810	2610	2410	2210	2030	1720
257	3070	1730	3070	2980	2840	2670	2480	2280	2100	1930	1760	1470
218	2510	1730	2510	2560	2380	2230	2050	1860	1680	1500	1350	1200
175	2020	1730	1970	1820	1630	1440	1240	1070	917	791	688	535
800WB192	2030	1190	2000	1880	1730	1570	1410	1280	1120	1000	900	737
168	1720	1190	1680	1550	1400	1250	1090	955	836	736	652	524
146	1540	1190	1490	1360	1210	1060	907	775	665	574	500	392
122	1220	1190	1150	1030	880	737	610	505	423	368	308	236
700WB173	1610	1100	1570	1470	1340	1200	1070	956	853	765	690	572
150	1350	1100	1300	1190	932	812	708	621	548	489	398	335
130	1210	1100	1150	1040	911	781	664	565	484	420	368	292
115	1020	970	868	750	634	531	445	376	321	278	217	176

Note: Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).  
For other moment distributions use the appropriate value of  $\alpha_m$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m \phi M_b$  and  $\phi M_{sx}$  given above.



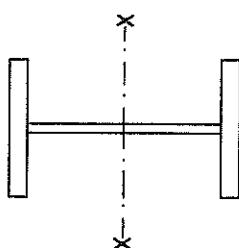


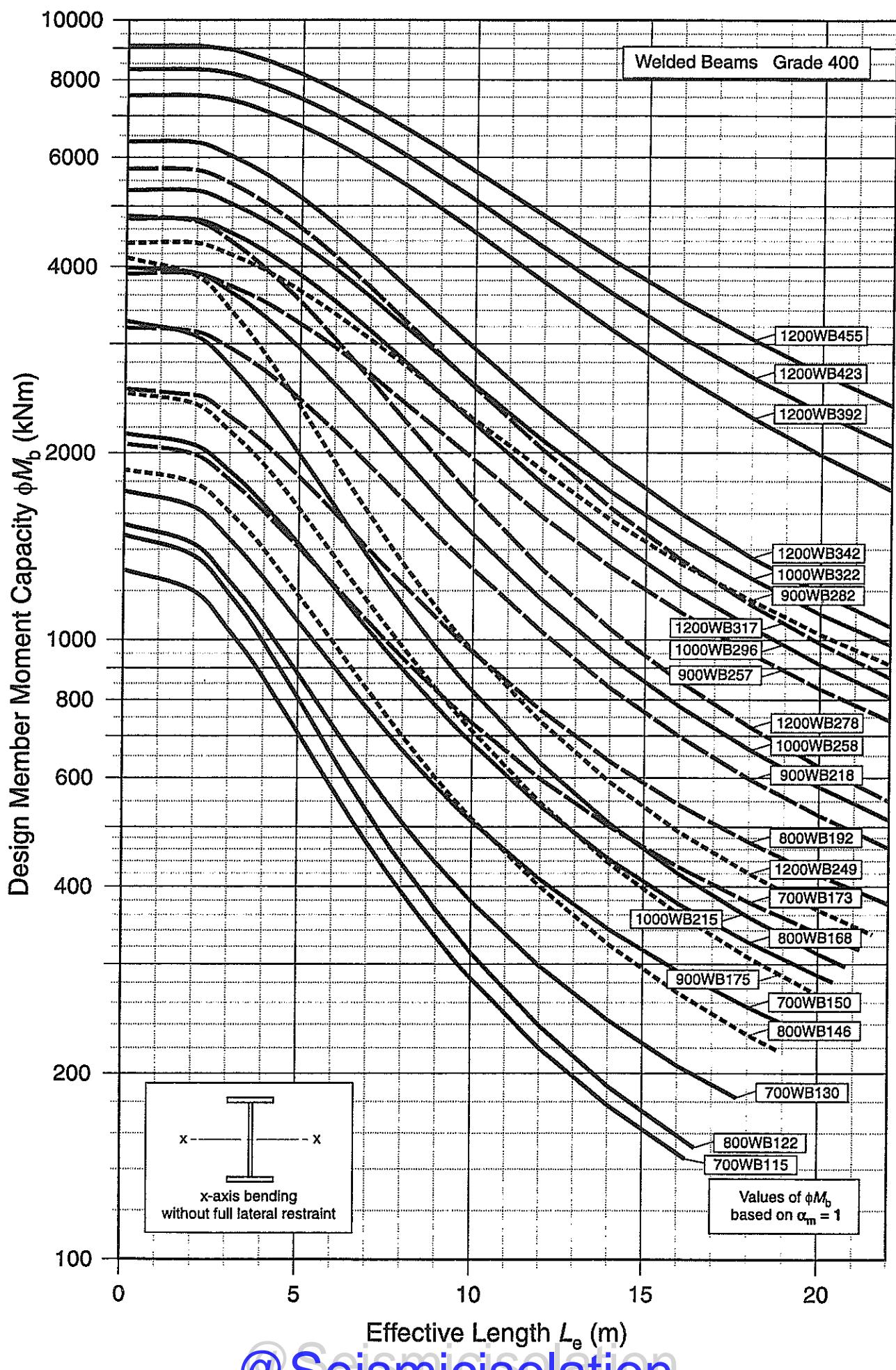
TABLE 5.3-2

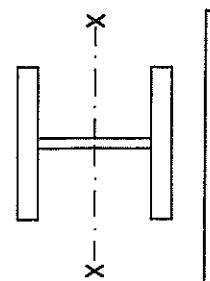
**WELDED BEAMS  
GRADE 400**

**DESIGN MOMENT CAPACITIES FOR MEMBERS WITHOUT FULL LATERAL RESTRAINT  
bending about X-axis**

Designation	$\phi M_{ax}$ kNm	$\phi V_r$ kN	Design Member Moment Capacities, $\phi M_s$ (kNm)														
			2	3	4	5	6	7	8	9	10	12	14	16	18	20	22
1200WB455	9090	3320	9090	8950	8590	8160	7680	7180	6660	6160	5670	4810	4090	3510	3050	2680	2380
423	8320	3320	8320	8180	7840	7440	6990	6510	6030	5550	5100	4280	3610	3070	2650	2320	2050
392	7550	3320	7550	7410	7100	6720	6300	5850	5400	4950	4530	3770	3150	2660	2280	1980	1740
342	6360	3320	6340	6020	5620	5150	4660	4180	3720	3310	2940	2350	1920	1600	1360	1190	1050
317	5750	3320	5720	5430	5040	4610	4150	3700	3270	2890	2550	2020	1630	1350	1140	987	867
278	4830	3320	4720	4390	3960	3510	3050	2630	2260	1950	1690	1300	1040	857	724	626	550
249	4140	3320	3870	3400	2880	2380	1940	1600	1330	1120	961	737	592	492	421	367	326
1400WB322	5310	3150	5300	5040	4720	4350	3960	3570	3200	2870	2570	2090	1730	1460	1260	1100	981
296	4780	3150	4760	4530	4220	3870	3510	3150	2810	2500	2230	1780	1460	1220	1050	912	807
268	3990	3150	3910	3640	3310	2940	2580	2250	1950	1690	1480	1160	938	781	666	580	513
215	3270	3150	3090	2760	2370	1990	1650	1360	1140	964	827	633	507	420	358	312	276
900WB282	4370	1820	4370	4180	3940	3650	3350	3050	2770	2500	2260	1870	1560	1330	1160	1020	911
257	3900	1820	3900	3720	3500	3230	2960	2680	2410	2170	1950	1580	1310	1110	952	833	740
218	3190	1820	3140	2850	2710	2440	2170	1910	1680	1470	1300	1030	836	699	598	522	462
175	2600	1820	2400	2170	1910	1630	1370	1150	974	828	713	547	437	362	308	268	236
800WB192	2540	1190	2480	2290	2070	1830	1610	1400	1230	1080	956	769	638	543	473	418	375
168	2150	1190	2050	1870	1650	1430	1220	1040	897	778	682	540	444	376	326	288	257
146	1880	1190	1790	1610	1480	1180	992	830	700	597	516	400	323	270	231	202	180
122	1480	1190	1370	993	807	651	530	437	367	313	239	191	159	136	118	105	90
700WB173	2070	1380	1990	1810	1610	1410	1230	1070	935	825	734	597	501	431	378	337	303
150	1740	1380	1640	1460	1260	1070	910	775	666	550	511	411	342	293	256	227	205
130	1540	1380	1430	1250	1060	882	728	606	510	437	379	298	244	206	179	158	141
115	1300	1380	1200	1040	870	710	577	472	393	332	285	220	178	149	128	112	100

Note: Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).  
For other moment distributions use the appropriate value of  $\alpha_m$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m \phi M_b$  and  $\phi M_{sx}$  given above.

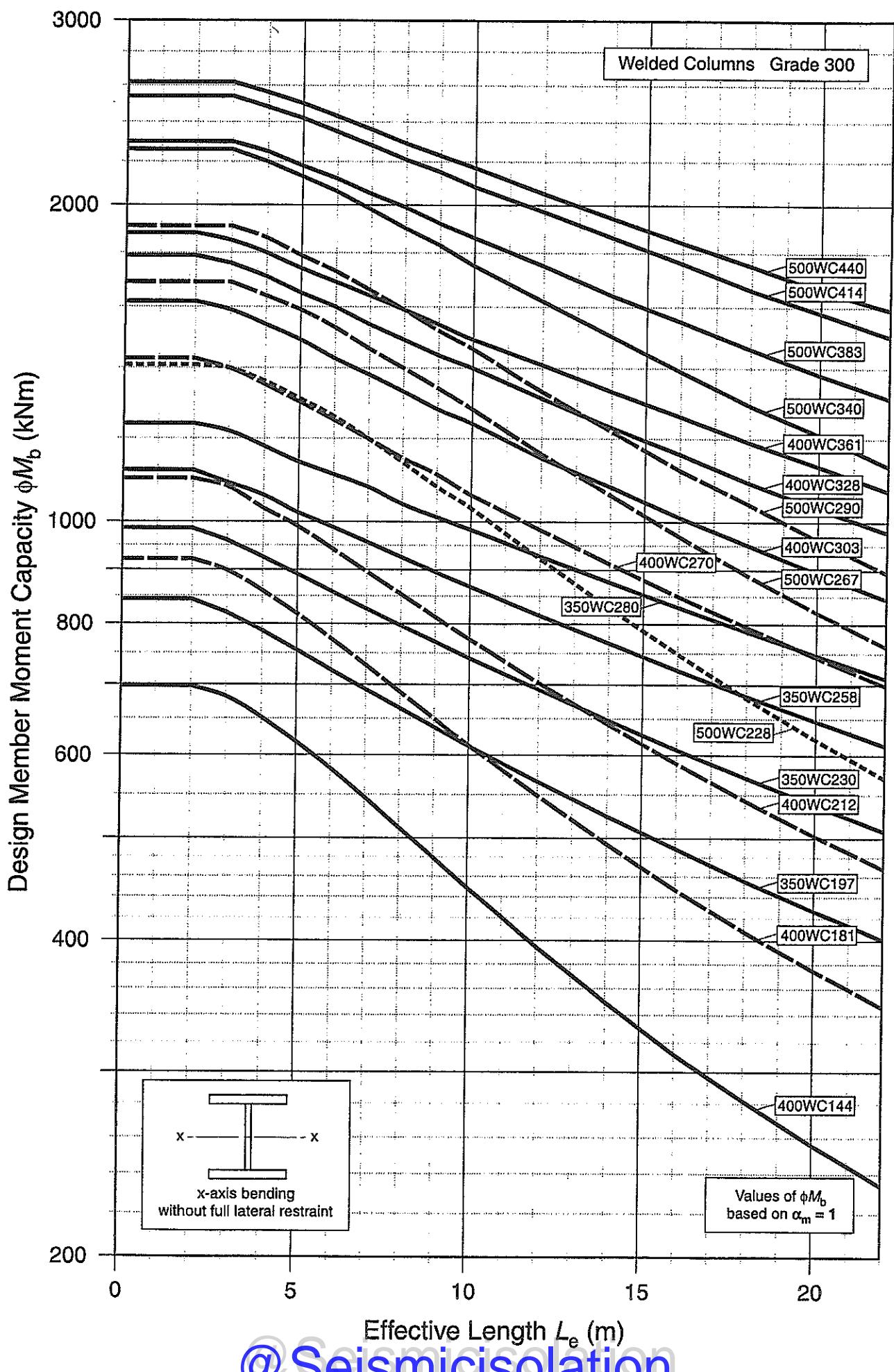


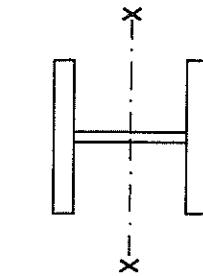


**TABLE 5.3-3**  
**WELDED COLUMNS**  
**GRADE 300**  
**DESIGN MOMENT CAPACITIES FOR MEMBERS WITHOUT FULL LATERAL RESTRAINT**  
**bending about x-axis**

Designation	$\phi M_{sx}$ kNm	$\phi V_s$ kN	Design Member Moment Capacities, $\phi M_b$ (kNm) Effective Length ( $L_e$ ) in metres																							
			2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22			
500WC440	2620	2420	2620	2560	2500	2430	2360	2290	2230	2170	2050	1940	1840	1750	1660	1590	1660	1750	1840	1940	1840	1750	1660			
414	2540	1940	2540	2540	2480	2420	2350	2280	2210	2150	2080	1970	1860	1760	1660	1580	1500	1660	1760	1860	1970	1860	1760	1660		
383	2300	1940	2300	2300	2250	2180	2120	2050	1990	1920	1860	1750	1640	1550	1460	1380	1310	1460	1550	1640	1550	1460	1380	1310		
340	2260	1700	2260	2260	2200	2130	2060	1980	1900	1830	1750	1620	1500	1390	1290	1210	1130	1290	1350	1290	1210	1130	1290	1350		
290	1910	1460	1910	1910	1860	1790	1730	1660	1590	1520	1460	1330	1220	1120	1040	962	895	895	962	1040	1120	1220	1330	1460		
267	1690	1460	1690	1690	1640	1590	1530	1460	1400	1340	1280	1160	1060	969	890	821	761	761	890	969	1060	1160	1280	1340		
228	1410	1460	1410	1410	1360	1310	1260	1200	1140	1080	1030	923	829	749	680	621	570	570	680	749	829	923	1030	1140		
400WC361	1880	2120	1880	1850	1800	1740	1690	1640	1590	1540	1490	1440	1390	1330	1280	1230	1180	1130	1180	1230	1280	1330	1390	1440		
328	1790	1480	1790	1760	1710	1650	1600	1540	1490	1430	1380	1330	1280	1240	1190	1150	1100	1060	1010	951	895	845	795	744		
303	1620	1480	1620	1590	1540	1490	1430	1350	1300	1250	1200	1150	1110	1060	983	913	850	795	744	699	647	593	543	498		
270	1430	1320	1430	1430	1400	1350	1300	1250	1200	1150	1110	1060	1030	990	897	812	773	703	642	589	543	503	468	426		
212	1100	1130	1100	1100	1080	1030	990	943	900	854	812	773	731	689	650	613	549	494	447	408	375	346	317	282		
181	922	1130	922	922	899	860	818	774	731	689	650	613	571	547	512	480	449	395	350	312	282	256	234	208	182	
144	698	907	698	698	662	618	583	547	512	480	449	408	375	346	317	282	256	234	208	182	156	134	112	90	68	
350WC280	1240	1160	1240	1220	1180	1140	1110	1080	1040	1010	983	928	877	830	787	747	710	673	623	571	525	489	456	427	401	
258	1120	1160	1120	1090	1060	1020	989	957	926	896	868	835	797	769	742	693	648	607	567	525	489	456	427	401	375	
230	986	1040	986	960	926	892	859	827	797	769	733	693	665	638	612	566	525	489	456	427	401	375	346	317	282	
197	844	891	844	844	820	788	755	723	693	665	638	612	566	525	489	456	427	401	375	346	317	282	256	234	208	182

Note: Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).  
For other moment distributions use the appropriate value of  $\alpha_m$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m \phi M_b$  and  $\phi M_{sx}$  given above.





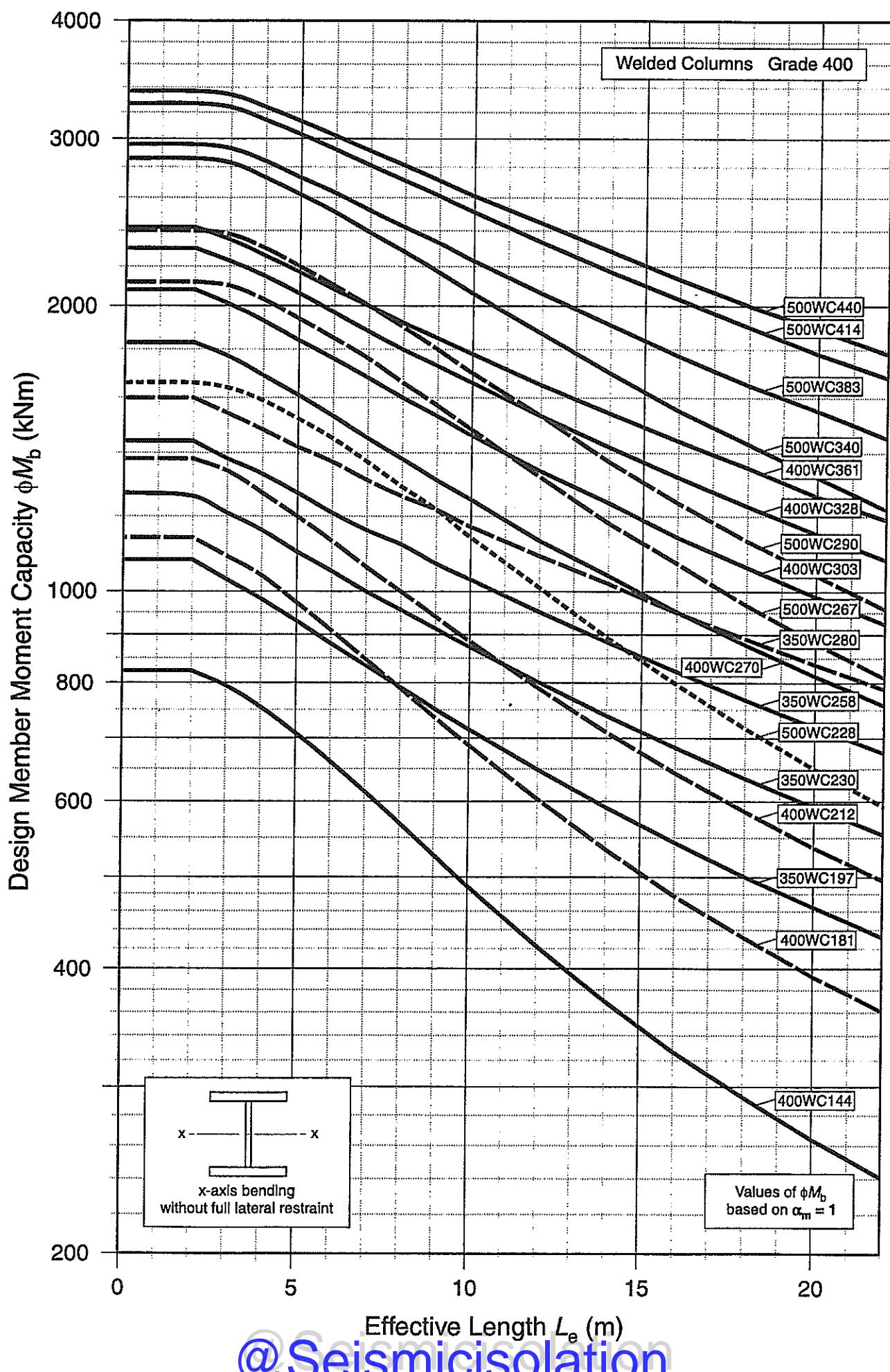
**TABLE 5.3-4**  
**WELDED COLUMNS**  
**GRADE 400**  
**DESIGN MOMENT CAPACITIES FOR MEMBERS WITHOUT FULL LATERAL RESTRAINT**  
**bending about x-axis**

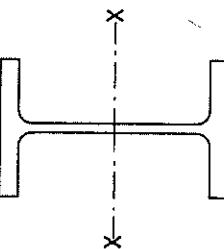
Designation	$\phi M_{s,x}$ kNm	$\phi V_v$ kN	Design Member Moment Capacities, $\phi M_b$ (kNm) Effective Length ( $L_e$ ) in metres									
			6	7	8	9	10	12	14	16	18	20
500WC440	3370	3010*	3370	3340	3240	3130	3020	2910	2810	2710	2610	2440
414	3270	2490	3270	3240	3140	3030	2920	2810	2710	2610	2510	2280
383	2960	2490	2960	2930	2840	2730	2630	2520	2420	2330	2230	2030
340	2860	2190	2860	2830	2730	2620	2510	2390	2280	2170	2060	1870
290	2400	1850	2400	2380	2300	2200	2100	2000	1900	1800	1700	1550
267	2120	1850	2120	2100	2030	1940	1850	1760	1660	1570	1480	1370
228	1660	1850	1660	1640	1590	1520	1450	1370	1280	1220	1140	1010
400WC361	2420	2690*	2420	2350	2260	2170	2080	2000	1920	1850	1780	1650
328	2300	1910	2300	2280	2150	2060	1970	1880	1800	1730	1660	1530
303	2080	1910	2080	2050	1930	1840	1760	1680	1600	1530	1460	1340
270	1830	1700	1830	1770	1690	1610	1530	1450	1380	1310	1250	1130
212	1380	1440	1380	1340	1270	1200	1130	1060	1000	941	886	790
181	1140	1440	1140	1090	1040	974	910	848	790	737	688	604
144	824	1150	824	795	755	709	662	615	570	528	489	423
350WC280	1600	1500	1600	1540	1480	1420	1370	1310	1260	1220	1170	1090
258	1440	1500	1440	1380	1330	1270	1210	1160	1120	1070	1030	952
230	1270	1340	1260	1210	1160	1100	1050	1000	956	914	874	802
197	1080	1130	1080	1030	982	931	881	835	792	752	715	649

Notes: (1) Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).

(2) \* indicates shear capacity governed by shear capacity of the weld.

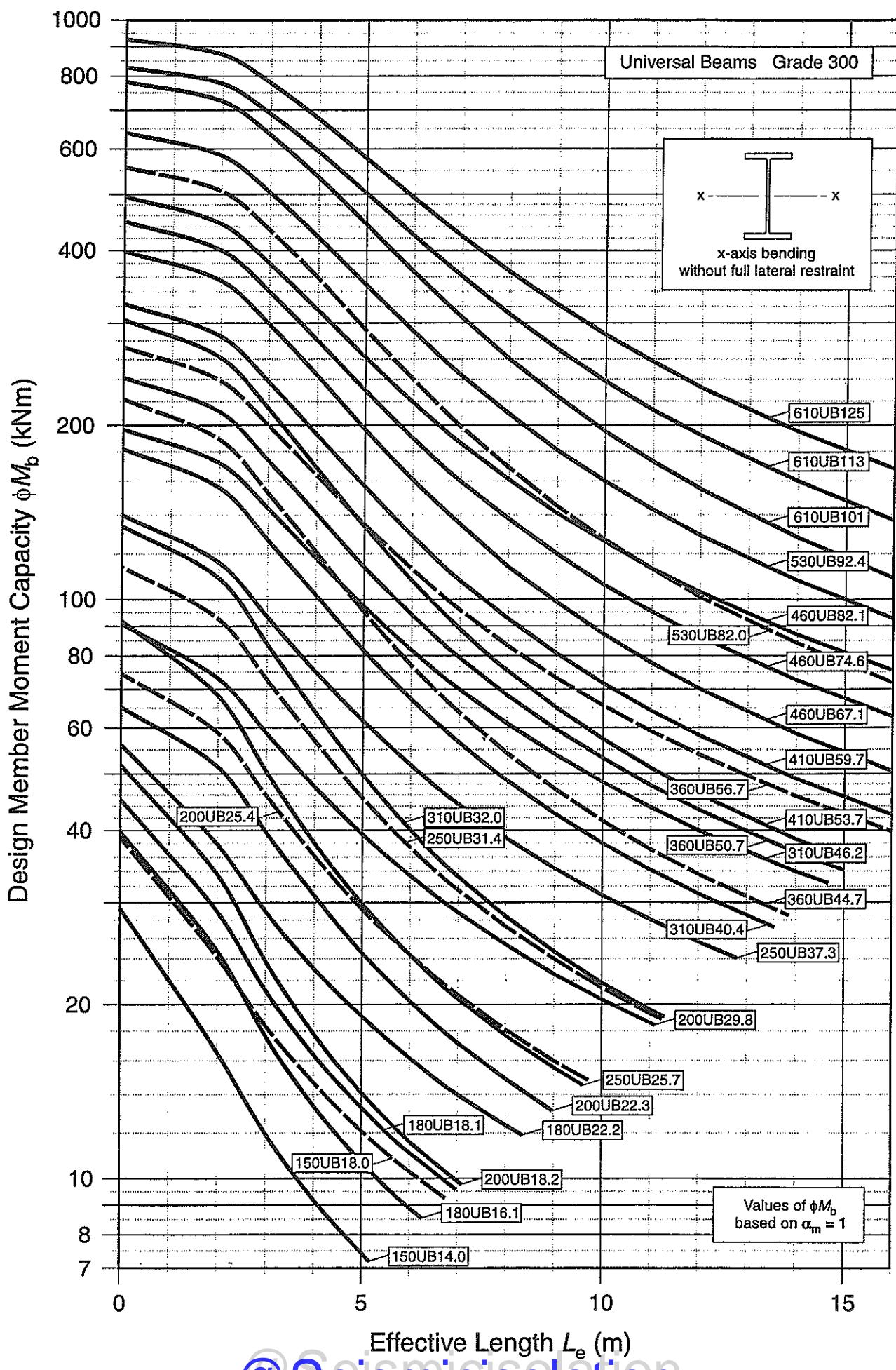
For other moment distributions use the appropriate value of  $\alpha_m$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m \phi M_b$  and  $\phi M_{b,ax}$  given above.

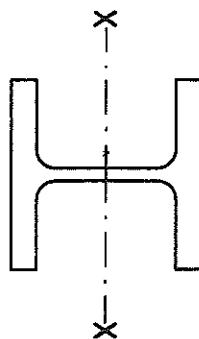




Designation	$\phi M_{sx}$ kNm	$\phi V_u$ kN	Design Member Moment Capacities, $\phi M_b$ (kNm)											
			6	7	8	9	10	11	12	13	14	15	16	
610UB125 113 101	927 829 782	1180 1100 1100	872 777 689	778 634 535	675 502 444	577 424 367	492 361 307	423 310 260	367 322 224	286 212 195	257 192 173	232 195 155	195 160 128	168 160 109
530UB 92.4 82.0	640 558	939 876	584 504	422	349	290	244	209	181 145	160 127	143 113	129 101	108 84.2	92.7 71.9
460UB 74.6 67.1	496 449 399	788 719 667	445 340 355	380 280 299	316 230 244	262 190 197	219 160 161	186 138 135	161 120 114	141 106 99.1	126 103 87.2	113 95.3 77.8	103 86.4 70.2	87.1 72.7 58.7
410UB 59.7 53.7	324 364	548 529	285 282	238 214	193 169	157	129	108	92.8 75.5	81.0 65.3	71.7 57.4	58.3 51.2	49.1 46.2	42.5 38.7
360UB 56.7 50.7 44.7	273 242 222	496 449 420	239 211 189	200 174 153	164 141 121	135 114 95.4	113 94.3 77.1	96.1 79.5 64.0	83.3 68.4 54.3	73.4 59.8 47.1	65.6 53.2 41.5	59.2 47.8 37.1	54.0 43.4 33.6	45.8 36.7 28.2
310UB 46.2 40.4 32.0	197 182 134	356 320 283	172 156 109	144 127 84.1	118 102 64.1	97.5 81.9 49.9	81.9 67.4 40.1	70.1 56.7 33.3	61.1 48.8 28.4	48.4 42.7 24.7	43.8 38.0 21.8	40.0 34.2 19.6	34.0 31.1 17.8	29.7 26.3 15.0
250UB 37.3 31.4 25.7	140 114 92.0	283 265 214	116 92.7 68.3	93.6 73.0 50.6	75.3 57.1 38.1	61.8 45.5 29.9	51.8 37.4 24.4	44.4 31.6 20.5	38.8 27.3 17.7	30.9 24.0 17.2	28.1 21.4 13.9	26.7 19.3 12.6	21.9 17.6 11.5	19.2 14.9 13.0
200UB 29.8 25.4 22.3 18.2	90.9 74.6 65.3 51.8	225 204 174 154	73.2 58.9 46.0 33.6	58.9 46.0 36.2 23.8	39.4 29.2 24.4 17.8	33.4 29.2 24.4 14.1	28.9 29.2 20.8 11.6	25.4 24.4 20.8 9.91	22.6 18.1 16.0 8.62	20.4 14.4 13.1 7.63	18.6 13.0 11.7 6.84	17.0 13.0 10.6 6.21	14.6 10.2 9.68 5.68	12.8 8.90 8.25 4.85
180UB 22.2 18.1 16.1	56.2 45.2 39.8	186 151 135	37.9 29.0 24.8	29.0 21.2 17.7	23.1 16.4 13.4	19.1 13.3 10.7	16.2 11.1 8.91	14.0 9.56 7.62	12.4 8.37 6.66	9.99 7.45 5.91	9.11 6.71 5.31	8.37 6.10 4.82	7.19 4.80 4.42	6.31 4.20 3.31
150UB 18.0 14.0	38.9 29.3	161 130	24.2 16.6	18.4 12.0	14.7 9.20	12.1 7.45	10.3 6.24	8.94 5.37	7.89 4.71	7.05 4.19	6.37 3.78	5.81 3.44	4.59 3.15	4.03 2.70

Notes: (1) Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).  
 For other moment distributions use the appropriate value of  $\alpha_m$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m \phi M_b$  and  $\phi M_{Max}$  given above.  
 (2) Grade 300 refers to BHP Grade 300PLUSTM. See Note (1) on page 2-2.





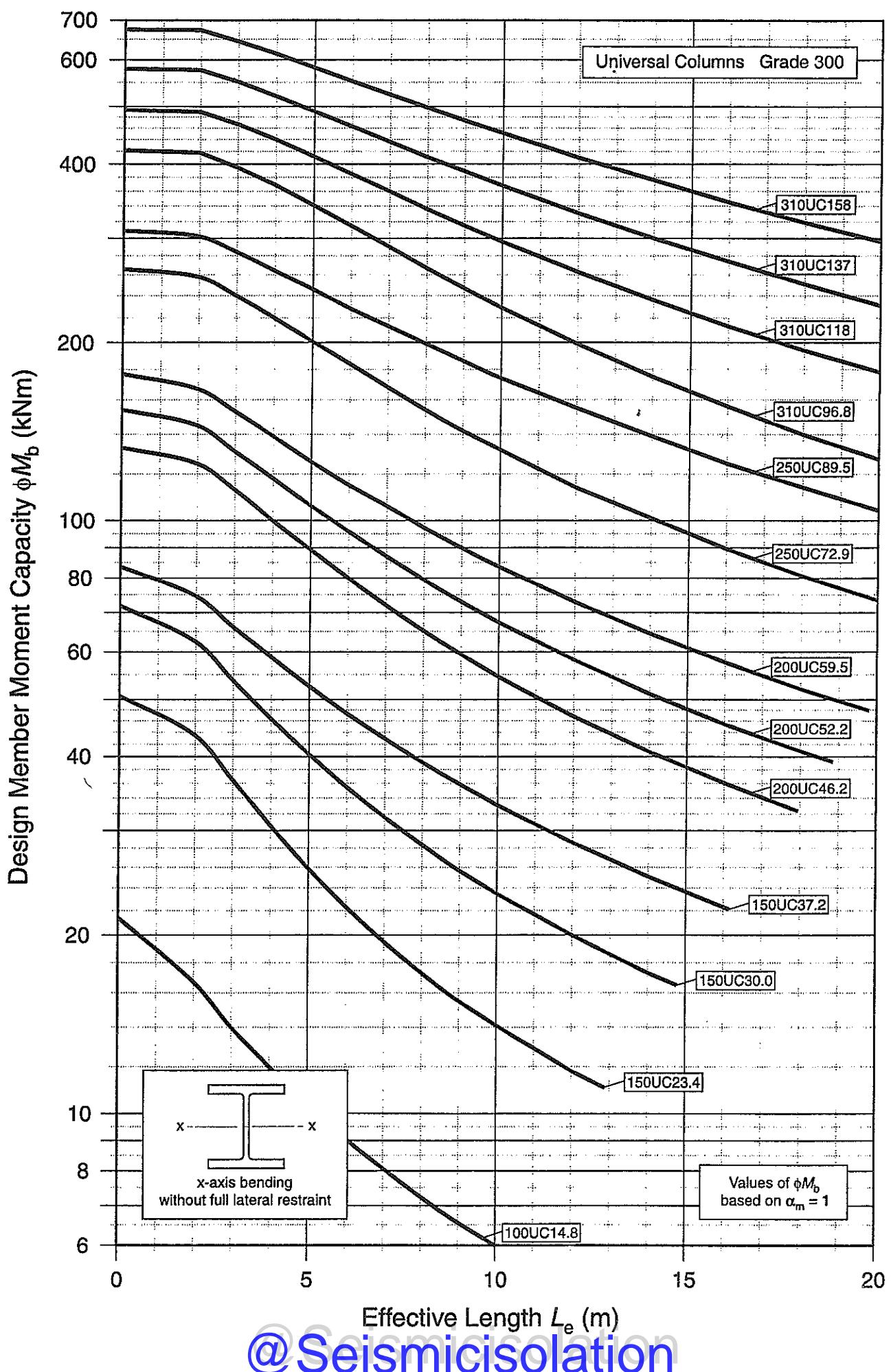
**TABLE 5.3-6**  
**UNIVERSAL COLUMNS**  
**GRADE 300**  
**DESIGN MOMENT CAPACITIES FOR MEMBERS WITHOUT FULL LATERAL RESTRAINT**  
**bending about x-axis**

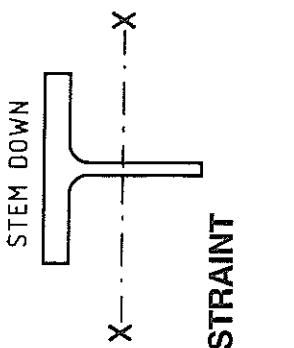
Designation	$\phi M_{ax}$	$\phi V_r$	Design Member Moment Capacities, $\phi M_b$ (kNm)									
			5	6	7	8	9	10	12	14	16	18
	kNm	kN										
340UC158	676	832	674	645	614	582	552	524	498	473	451	410
137	580	717	577	551	521	491	463	436	411	389	368	331
118	494	606	490	467	440	412	385	360	336	315	296	263
96.8	422	527	418	395	369	341	315	290	267.	247	229	199
250UC 89.5	309	472	302	284	264	246	228	213	199	186	174	155
72.9	266	377	258	240	220	201	184	168.	154	142	132	114
200UC 59.5	177	337	167	153	139	126	115	106	97.3	90.0	83.6	73.0
52.2	154	285	145	131	118	106	95.9	87.1	79.5	73.0	67.4	58.2
46.2	133	257	125	113	100	89.4	80.0	72.0	65.2	59.5	54.6	46.8
150UC 37.2	83.6	226	74.6	66.1	58.8	52.6	47.3	42.9	39.1	35.9	33.1	28.6
30.0	71.9	180	62.5	53.8	46.4	40.4	35.5	31.6	28.4	25.7	23.5	20.0
23.4	50.7	161	43.5	36.5	30.6	25.9	22.3	19.5	17.3	15.5	14.1	11.8
100UC 14.8	21.4	83.8	16.7	14.0	12.0	10.4	9.09	8.08	7.25	6.56	5.99	5.09

Notes: (1) Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).

For other moment distributions use the appropriate value of  $\alpha_m$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m \phi M_b$  and  $\phi M_{sx}$  given above.

(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.




  
**TABLE 5.3-7**  
**TEES CUT FROM UNIVERSAL BEAMS**  
**GRADE 300**  
**DESIGN MOMENT CAPACITIES FOR MEMBERS WITHOUT FULL LATERAL RESTRAINT**  
**bending about x- axis**  
stem down — flange in compression

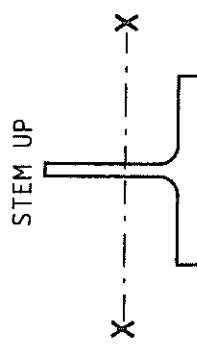
Designation	$\phi M_{sx}$ kNm	$\phi V_v$ kN	Design Member Moment Capacities, $\phi M_b$ (kNm) Effective Length ( $L_e$ ) in metres									
			1	2	3	4	5	6	7	8	10	12
30SBT62.5	112	520	112	112	106	102	97.4	93.4	89.6	82.3	75.7	69.8
56.5	104	486	104	101	96.9	92.6	88.4	84.3	80.3	72.9	66.3	60.5
50.5	103	488	103	98.9	94.1	89.0	84.0	79.1	74.5	66.1	58.9	52.7
26SBT46.3	78.3	414	78.3	78.2	75.1	71.6	68.1	64.6	61.3	58.1	52.3	47.2
41.0	72.1	387	72.1	71.7	68.4	64.8	61.0	57.4	53.9	50.6	44.7	39.7
230BT41.1	56.8	346	56.8	56.6	54.4	52.1	49.8	47.5	45.3	43.2	39.4	36.0
37.3	51.8	316	51.8	51.5	49.4	47.1	44.8	42.5	40.4	38.3	34.6	31.4
33.6	47.6	293	47.6	47.2	45.0	42.7	40.3	38.0	35.9	33.8	30.1	27.0
205BT29.9	35.3	240	35.3	35.1	33.6	32.0	30.4	28.8	27.4	26.0	23.5	21.2
26.9	35.8	232	35.8	35.2	33.3	31.3	29.3	27.4	25.7	24.0	21.1	18.7
180BT28.4	28.2	217	28.2	28.0	26.9	25.8	24.7	23.6	22.6	21.6	19.8	18.2
25.4	25.4	196	25.4	25.2	24.1	23.0	21.9	20.8	19.8	18.8	17.1	15.5
22.4	24.4	184	24.4	23.9	22.7	21.4	20.1	18.9	17.8	16.7	14.8	13.2
155BT23.1	17.6	154	17.6	17.5	16.9	16.3	15.8	15.2	14.6	14.1	13.1	12.2
20.2	16.8	139	16.8	16.6	16.0	15.3	14.6	13.9	13.3	12.7	11.6	10.6
16.0	13.6	123	13.6	13.3	12.5	11.7	11.0	10.3	9.66	9.07	8.01	7.13
125BT18.7	12.3	123	12.3	12.2	11.7	11.3	10.8	10.4	9.99	9.60	8.87	8.21
15.7	11.2	115	11.2	11.0	10.4	9.88	9.36	8.87	8.40	7.97	7.18	6.50
12.9	9.03	92.5	9.03	8.67	8.14	7.63	7.14	6.69	6.27	5.88	5.21	4.64
100BT14.9*	7.86	97.4	7.86	7.86	7.86	7.86	7.86	7.86	7.86	7.86	7.86	7.86
12.7*	6.92	88.2	6.92	6.92	6.92	6.92	6.92	6.92	6.92	6.92	6.92	6.92
11.2*	5.62	75.2	5.62	5.62	5.62	5.62	5.62	5.62	5.62	5.62	5.62	5.62
9.1	5.11	66.3	5.11	4.79	4.45	4.13	3.83	3.56	3.31	3.09	2.71	2.40
90BT11.1	5.40	80.4	5.15	4.88	4.62	4.38	4.16	3.94	3.75	3.39	3.08	2.81
9.1	4.37	65.3	4.37	4.11	3.85	3.61	3.38	3.17	2.98	2.80	2.49	2.01
8.1	3.87	58.0	3.87	3.61	3.36	3.12	2.90	2.70	2.52	2.36	2.07	1.65
75BT 9.0	3.96	69.7	3.94	3.70	3.48	3.27	3.08	2.90	2.73	2.58	2.31	2.08
7.0	3.14	56.2	3.09	2.85	2.62	2.41	2.23	2.06	1.91	1.77	1.54	1.36

Notes: (1) \* indicates bending about minor principal y-axis, for the axis shown in the diagram. These sections cannot buckle laterally when bending about the y-axis.

(2) Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).

For other moment distributions use the appropriate value of  $\alpha_m(\phi M_b)$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m(\phi M_b)$  &  $\phi M_{sx}$  given above.

(3) Grade 300 refers to BHP Grade 300 PLUS™. See Note (1) on page 2-2.



**TABLE 5.3-8**  
**TEES CUT FROM UNIVERSAL BEAMS**  
**GRADE 300**

**DESIGN MOMENT CAPACITIES FOR MEMBERS WITHOUT FULL LATERAL RESTRAINT**  
**bending about x-axis**

stem up — stem in compression

Designation	$\phi M_{sx}$ kNm	$\phi V_v$	Design Member Moment Capacities, $\phi M_b$ (kNm) Effective Length ( $L_e$ ) in metres											
			1	2	3	4	5	6	7	8	10			
305BT62.5 56.5 50.5	72.7 59.6 49.5	520 486 488	64.0 51.5 41.3	63.1 49.8 39.9	61.8 48.7 39.0	60.4 47.5 38.0	58.9 46.2 37.0	57.4 45.0 36.0	55.9 43.8 35.0	54.4 41.5 33.0	51.6 39.3 31.2	48.9 39.3 31.2	46.3 37.2 29.5	44.0 35.3 27.9
265BT46.3 41.0	45.3 37.0	414 387	39.3 31.0	38.7 30.5	37.8 29.8	36.8 29.0	35.7 28.1	34.7 27.3	33.7 26.4	32.7 25.6	30.7 24.0	28.9 22.5	27.3 22.5	25.8 20.0
230BT41.1 37.3 33.6	39.5 32.7 26.3	346 316 293	35.4 28.9 22.8	34.7 28.4 22.4	33.7 27.6 21.8	32.7 26.8 21.2	31.7 26.0 20.5	30.7 25.2 19.9	29.7 24.4 19.3	28.8 23.6 18.7	27.0 22.1 17.5	25.4 20.8 16.4	23.8 19.8 15.4	22.5 18.4 14.5
205BT29.9 26.9	20.8 18.8	240 232	18.7 16.2	18.4 15.9	17.9 15.5	17.4 15.0	16.9 14.5	16.4 14.0	15.9 13.5	15.4 13.0	14.5 12.2	13.7 11.4	12.9 10.6	12.2 9.99
180BT28.4 25.4 22.4	20.2 17.0 14.2	217 196 184	18.6 15.4 12.4	18.2 15.0 12.1	17.7 14.6 11.8	17.2 14.2 11.4	16.6 13.7 11.0	16.1 13.3 10.6	15.6 12.8 10.2	15.1 12.4 9.86	14.2 11.6 9.18	13.4 10.9 8.56	12.6 10.2 8.00	11.9 9.61 7.49
155BT23.1 20.2 16.0	12.4 10.2 7.23	154 139 123	11.8 9.58 6.53	11.3 9.39 6.38	11.0 9.15 6.18	10.8 8.91 5.98	10.5 8.67 5.78	10.2 8.42 5.58	9.93 8.19 5.39	9.43 7.96 5.21	8.95 7.52 4.86	8.50 7.11 4.55	8.09 6.73 4.26	8.09 6.38 4.00
125BT18.7 15.7 12.9	9.38 8.37 5.56	123 115 92.5	8.96 7.66 5.12	8.74 7.42 4.95	8.49 7.15 4.77	8.24 6.87 4.58	7.99 6.61 4.40	7.75 6.35 4.22	7.51 6.10 4.06	7.29 5.86 3.90	6.86 5.43 3.60	6.46 5.03 3.34	6.10 4.68 3.10	5.76 4.36 2.89
100BT14.9* 12.7 11.2* 9.1	6.60 5.67 4.50 3.64	97.4 88.2 75.2 66.3	6.60 5.67 4.50 3.56	6.60 5.67 4.50 3.19	6.60 5.67 4.50 3.03	6.60 5.67 4.50 2.87	6.60 5.67 4.50 2.72	6.60 5.67 4.50 2.59	6.60 5.67 4.50 2.46	6.60 5.67 4.50 2.33	6.60 5.67 4.50 2.12	6.60 5.67 4.50 1.93	6.60 5.67 4.50 1.77	6.60 5.67 4.50 1.62
90BT11.1	4.75 3.57 3.01	80.4 65.3 58.0	4.55 3.36 2.79	4.15 3.19 2.65	3.96 3.03 2.50	3.78 2.87 2.36	3.60 2.73 2.24	3.44 2.59 2.12	3.29 2.46 2.00	3.01 2.34 1.90	2.77 2.12 1.72	2.55 1.93 1.56	2.36 1.77 1.42	2.36 1.93 1.42
75BT 9.0	3.66 2.73	69.7 56.2	3.49 2.52	3.30 2.35	3.11 2.19	2.94 2.04	2.78 1.90	2.63 1.77	2.49 1.66	2.36 1.56	2.13 1.38	1.93 1.23	1.76 1.11	1.62 1.00

Notes: (1) \* Indicates bending about minor principal y-axis, for the axis shown in the diagram. These sections cannot buckle laterally when bending about the y-axis.

(2) Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).

For other moment distributions use the appropriate value of  $\alpha_m$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m(\phi M_b)$  &  $\phi M_{sx}$  given above.

(3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

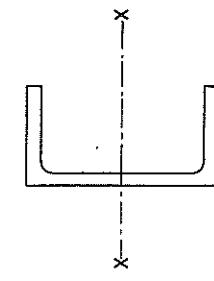


TABLE 5.3-9  
**PARALLEL FLANGE CHANNELS**  
**GRADE 300**  
**DESIGN MOMENT CAPACITIES FOR MEMBERS WITHOUT FULL LATERAL RESTRAINT**  
 bending about x-axis

Designation	Mass per metre	Design Member Moment Capacities, $\phi M_b$ (kNm)														
		$\phi M_{bx}$	$\phi V_y$	Effective Length ( $L_e$ ) in metres	3.5	4.0	4.5									
380 PFC	55.2	238	657	230	212	192	173	156	140	127	115	106	97.2	89.9	78.0	68.8
300 PFC	40.1	152	415	144	131	117	105	93.8	84.4	76.4	69.7	63.9	58.9	54.6	47.5	42.0
250 PFC	35.5	114	346	108	98.6	89.2	80.7	73.1	66.6	61.0	56.1	51.8	48.1	44.9	39.4	35.1
280 PFC	25.1	73.3	258	67.0	59.1	51.6	45.2	39.9	35.5	31.9	28.9	26.4	24.2	22.4	19.4	17.1
200 PFC	22.9	59.7	207	54.8	48.8	43.3	38.5	34.4	31.0	28.1	25.7	23.6	21.8	20.3	17.7	15.7
180 PFC	20.9	49.0	187	45.1	40.3	35.9	32.0	28.8	26.0	23.7	21.7	20.0	18.5	17.2	15.1	13.4
150 PFC	17.7	37.0	156	33.8	30.2	26.9	24.0	21.6	19.6	17.8	16.3	15.1	14.0	13.0	11.4	10.1

Notes: (1) Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).

(2) For other moment distributions use the appropriate value of  $\alpha_m$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m \phi M_b$  &  $\phi M_s$  given above.

(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

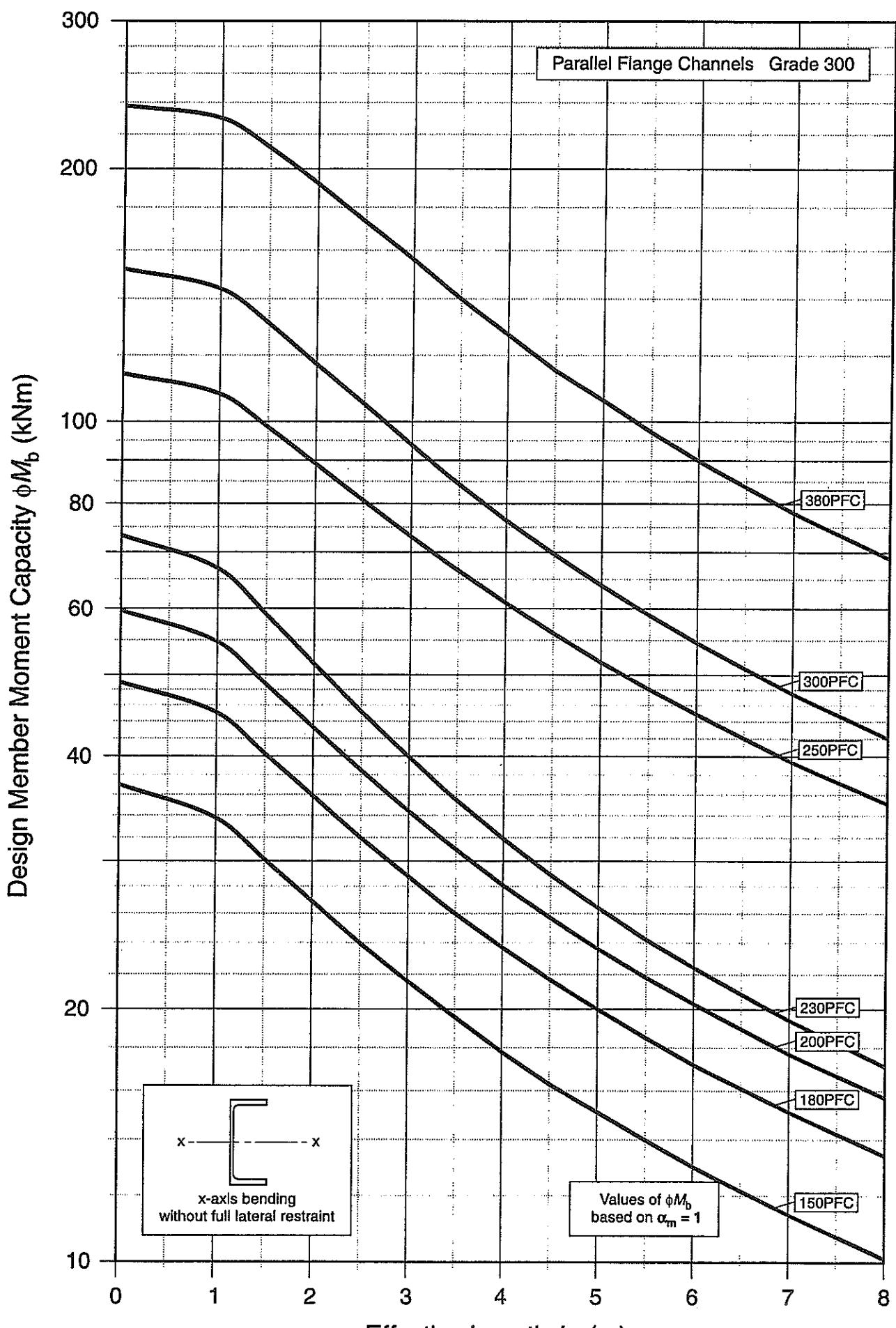
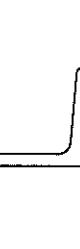


TABLE 5.3-10

**TAPER FLANGE CHANNELS  
GRADE 250**

**DESIGN MOMENT CAPACITIES FOR MEMBERS WITHOUT FULL LATERAL RESTRAINT  
bending about x-axis**



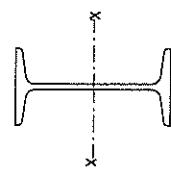
Designation	Mass per metre	$\phi M_{sx}$	$\phi V_v$	Design Member Moment Capacities, $\phi M_b$ (kNm)							
				Effective Length ( $L_e$ ) in metres	3.0	3.5	4.0	4.5	5.0	5.5	6.0
125 TFC	13.4	18.6	105	16.8	15.1	13.6	12.3	11.2	10.2	9.39	8.66
100 TFC	9.34	10.4	70.2	8.96	7.94	7.08	6.35	5.74	5.22	4.77	4.39
75 TFC	6.65	5.39	52.7	4.54	4.03	3.60	3.24	2.93	2.66	2.44	2.24
											2.07
											1.92
											1.79
											1.57
											1.40

Note: Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).  
For other moment distributions use the appropriate value of  $\alpha_m$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m \phi M_b$  &  $\phi M_s$  given above.

TABLE 5.3-11

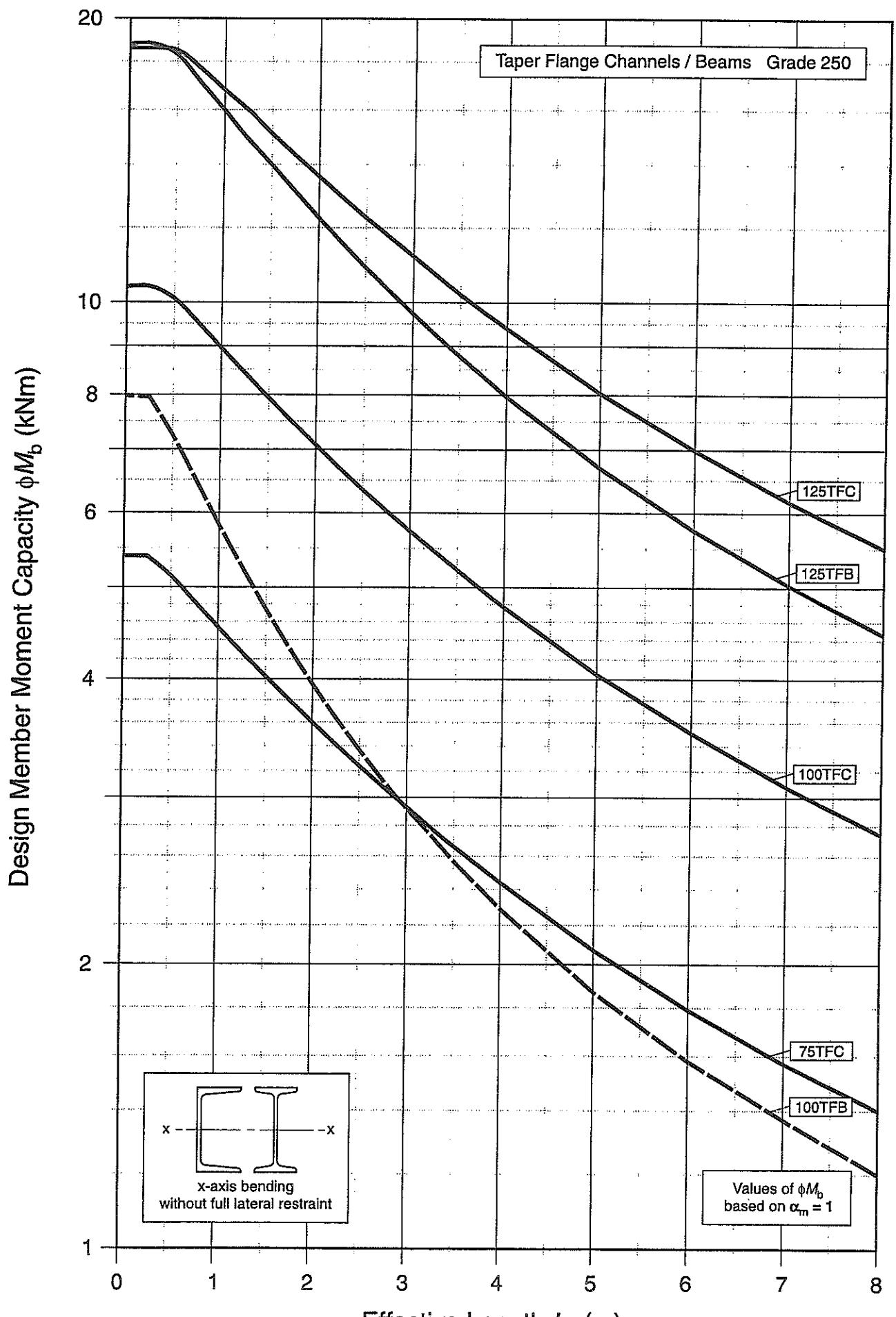
**TAPER FLANGE BEAMS  
GRADE 250**

**DESIGN MOMENT CAPACITIES FOR MEMBERS WITHOUT FULL LATERAL RESTRAINT  
bending about x-axis**



Designation	Mass per metre	$\phi M_{sx}$	$\phi V_v$	Design Member Moment Capacities, $\phi M_b$ (kNm)							
				Effective Length ( $L_e$ ) in metres	2.0	2.5	3.0	3.5	4.0	4.5	5.0
125TFB	13.1	18.8	87.8	18.3	17.1	16.0	14.9	14.0	13.1	12.3	10.9
100TFB	7.20	7.98	56.2	7.25	6.50	5.82	5.24	4.74	4.32	3.95	3.37

Note: Values of  $\phi M_b$  based on  $\alpha_m = 1$  (uniform moment over entire segment).  
For other moment distributions use the appropriate value of  $\alpha_m$  obtained from AS 4100 Table 5.6.1 or 5.6.2 and use the minimum of  $\alpha_m \phi M_b$  &  $\phi M_s$  given above.



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## PART 6 MEMBERS SUBJECT TO AXIAL COMPRESSION

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6.1 Scope .....	6-2
6.2 Design Section Capacity in Axial Compression .....	6-2
6.3 Design Member Capacity in Axial Compression .....	6-2
6.4 Effective Length.....	6-4
6.5 Example .....	6-5

### TABLES

#### TABLES 6-1 to 6-13

Design Member Capacities in Axial Compression ( $\phi N_c$ ) .....	6-6
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COMPRESSION

TENSILE

**PART 6 MEMBERS SUBJECT TO AXIAL COMPRESSION****6.1 General**

Values of the design member capacity in compression ( $\phi N_c$ ) for buckling about both principal axes, for a range of effective lengths ( $L_e$ ) are given in Tables 6-1 to 6-13. The capacities are determined from Section 6 of AS 4100. Many tables are supplemented by graphs of  $\phi N_c$  versus  $L_e$  placed consecutively after the tables for each corresponding grade and section. All loads are assumed to be applied through the centroid of the section. The column capacity is associated with flexural or flexural-torsional buckling.

The tables in this section have been grouped into two series:

- the (A) series for the member buckling about the  $x$ -axis, and
- the (B) series for the member buckling about the  $y$ -axis.

The (A) series tables and graphs are immediately followed by the (B) series of tables and graphs.

**6.2 Design Section Capacity in Axial Compression**

The design section capacity in compression ( $\phi N_s$ ) is obtained from Clause 6.2 of AS 4100 and is given by:

$$\phi N_s = \phi k_f A_n f_y$$

where  $\phi = 0.9$  (Table 3.4 of AS 4100)

$k_f$  = form factor (see Section 3.2.2.3)

$A_n$  = net area of the cross-section

=  $A_g$  assuming no penetrations or holes

$f_y$  = yield stress (for sections where the flange and web yield stresses ( $f_{yf}$  &  $f_{yw}$ ) differ, the **lower** value applied to the entire cross-section in the above equation for  $\phi N_s$ )

The design *section* capacity considers the behaviour of the cross-section only (as in a stub column test), and is affected by the element slenderness of each plate element in the cross-section. The form factor ( $k_f$ ) represents the proportion of the section that is effective in axial compression due to local buckling. The design *member* capacity in compression (Section 6.3) accounts for (amongst other factors) overall member buckling considering the effective length of the member.

**6.3 Design Member Capacity in Axial Compression**

The design member capacity in compression ( $\phi N_c$ ) is obtained from Clause 6.3 of AS 4100 and is given by:

$$\phi N_c = \phi \alpha_c N_s \leq \phi N_s$$

where  $\phi = 0.9$  (Table 3.4 of AS 4100)

$\alpha_c$  = member slenderness reduction factor

The member slenderness reduction factor ( $\alpha_c$ ) depends on the modified member slenderness ( $\lambda_n$ ) and the member section constant ( $\alpha_b$ ). From Clause 6.3.3 of AS 4100

$$\alpha_c = \xi \left\{ 1 - \sqrt{\left[ 1 - \left( \frac{90}{\xi \lambda} \right)^2 \right]} \right\}$$

$$\text{where } \xi = \frac{\left( \frac{\lambda}{90} \right)^2 + 1 + \eta}{2 \left( \frac{\lambda}{90} \right)^2}$$

$$\lambda = \lambda_n + \alpha_a \alpha_b$$

$$\lambda_n = \left( \frac{L_e}{r} \right) \sqrt{(k_f)} \sqrt{\left( \frac{f_y}{250} \right)}$$

$$\alpha_a = \frac{2100 (\lambda_n - 13.5)}{\lambda_n^2 - 15.3 \lambda_n + 2050}$$

$$\eta = 0.00326 (\lambda - 13.5) \geq 0$$

$L_e$  = effective length of a compression member

$r$  = radius of gyration about the axis of buckling

For routine design the above equations need not be used. AS 4100 Table 6.3.3(3) should be consulted to obtain the value of  $\alpha_c$  directly from  $\lambda_n$  and  $\alpha_b$ .

Note that the design member capacity equals the design section capacity ( $\phi N_c = \phi N_s$ ) when the effective length is zero ( $L_e = 0$ ).

Table 6.1 below lists values  $\alpha_b$  for the sections considered in this publication.

**TABLE 6.1**

Section	Member section constant $\alpha_b$	
	$k_f = 1.0$	$k_f < 1.0$
WB, WC	0	0.5
UB, UC, TFB	0	0
Channels	0.5	1.0
Structural Tees	0.5	1.0
Angles	0.5	1.0

## 6.4 Effective Length

The values of  $\phi N_c$  depend on the *effective length* ( $L_e$ ) of the member. The effective length depends on the rotational and translational restraints at the ends of the member and is determined using the following formula:

$$L_e = k_e L$$

The member effective length factor ( $k_e$ ) (Clause 6.3.2 of AS 4100) can be determined using Clause 4.6.3 of AS 4100 or by a rational frame buckling analysis (Clause 4.7 of AS 4100).

$k_e$  is given in Table 6.2 for members with idealised end restraints. For braced or sway members in frames,  $k_e$  depends on the ratio ( $\gamma$ ) of the compression member stiffness to the end restraint stiffness, calculated at each end of the member. Example 2 of Section 4.3 provides a sample calculation of  $k_e$  for a simple unbraced plane frame.

**TABLE 6.2: Effective Length Factors for Members for Idealised Conditions of End Restraint**

	Braced Member			Sway Member		
	Buckled Shape	Buckled Shape	Buckled Shape	Buckled Shape	Buckled Shape	Buckled Shape
Buckled Shape						
Effective length factor ( $k_e$ )	0.7	0.85	1.0	1.2	2.2	2.2
Symbols for end restraint conditions	 	= Rotation fixed, translation fixed = Rotation free, translation fixed		 	= Rotation fixed, translation free = Rotation free, translation free	

## 6.5 Example

Design a Universal Column, with a length of 5.8 m, in Grade 300 steel to resist a design axial force,  $N^* = 850$  kN. Assume that for x-axis buckling both ends are pinned (rotation free, translation fixed), while for y-axis buckling one end is pinned and the other end is rotationally and translationally fixed.

### Design Data

$$N^* = 850 \text{ kN}$$

### Solution

#### (i) Determine effective lengths

For x-axis buckling  $k_e = 1.0$  (Table 6.2)

$$\therefore L_{ex} = k_e L = 1 \times 5.8 = 5.8 \text{ m} \approx 6.0 \text{ m}$$

For y-axis buckling  $k_e = 0.85$  (Table 6.2)

$$\therefore L_{ey} = k_e L = 0.85 \times 5.8 = 4.93 \text{ m} \approx 5.0 \text{ m}$$

#### (ii) Select a member

For buckling about the x-axis, the smallest member is

$$200UC46.2 \quad \phi N_{cx} = 1140 \text{ kN} \quad (L_{ex} = 6.0 \text{ m}) \quad (\text{Table 6-6(A)})$$

$$> N^*$$

For buckling about the y-axis

$$200UC46.2 \quad \phi N_{cy} = 786 \text{ kN} \quad (L_{ey} = 5.0 \text{ m}) \quad (\text{Table 6-6(B)})$$

$$< N^* \quad \text{which is inadequate}$$

Select new section based on y-axis buckling

$$200UC52.2 \quad \phi N_{cy} = 900 \text{ kN} \quad (L_{ey} = 5.0 \text{ m}) \quad (\text{Table 6-6(B)})$$

$$> N^*$$

Check new section for buckling about x-axis

$$200UC52.2 \quad \phi N_{cx} = 1300 \text{ kN} \quad (L_{ex} = 6.0 \text{ m}) \quad (\text{Table 6-6(A)})$$

$$> N^*$$

$\therefore$  Adopt a 200UC52.2 Grade 300 steel member.

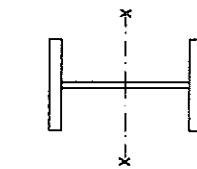


TABLE 6-1(A)

**WELDED BEAMS  
GRADE 300**

**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION  
buckling about x-axis**

Designation	$\phi N_s$ (kN) ( $L_e = 0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN) Effective Length ( $L_e$ ) in metres												
		2	4	6	8	10	12	15	18	21	24	27	30	33
1200WB455	12200	12200	12200	12100	11900	11700	11300	11000	10600	10200	9810	9390	8950	8490
423	11200	11200	11200	11100	10900	10700	10400	10000	9700	9350	8980	8550	8180	7760
392	10200	10200	10200	10100	9910	9720	9430	9130	8820	8490	8150	7790	7420	7030
342	8580	8580	8580	8580	8580	8580	8580	8580	8580	8580	7930	7670	7410	6840
317	7780	7780	7780	7780	7780	7780	7780	7780	7780	7780	7440	7170	6700	6450
278	6540	6540	6540	6540	6540	6540	6540	6540	6540	6540	6220	5830	5420	5000
249	5600	5600	5600	5600	5600	5600	5600	5600	5600	5600	5310	5140	4800	4430
1000WB322	8580	8580	8580	8580	8390	8190	8000	7700	7390	7070	6720	6350	5970	5570
296	7780	7780	7780	7780	7590	7420	7240	6960	6680	6380	6060	5720	5370	5010
258	6540	6540	6540	6540	6380	6230	6070	5840	5600	5340	5070	4780	4470	4170
215	5450	5450	5450	5450	5280	5150	5020	4810	4590	4360	4110	3850	3590	3320
900WB282	7650	7650	7650	7610	7420	7230	7050	6780	6450	6130	5780	5420	5040	4670
257	6840	6840	6840	6800	6630	6470	6300	6040	5760	5470	5160	4830	4490	4150
218	5610	5610	5610	5570	5430	5290	5150	4940	4710	4470	4210	3930	3630	3370
175	4480	4480	4480	4440	4320	4200	4080	3900	3710	3500	3280	3050	2830	2580
800WB192	5070	5070	4990	4850	4710	4570	4380	4110	3850	3580	3300	3020	2740	2490
168	4300	4300	4230	4110	3990	3870	3680	3480	3260	3020	2780	2540	2310	2090
146	3830	3830	3830	3760	3650	3540	3420	3240	3050	2840	2620	2400	2180	1770
122	3020	3020	3020	2960	2870	2780	2690	2550	2390	2230	2050	1870	1700	1530
700WB173	4710	4710	4580	4430	4280	4120	3870	3600	3300	3000	2700	2410	2150	1920
150	3980	3980	3980	3740	3610	3470	3260	3020	2770	2510	2260	2010	1790	1600
130	3560	3560	3560	3440	3320	3200	3070	2870	2640	2410	2160	1930	1710	1510
115	3020	3020	2920	2810	2710	2600	2420	2230	2020	1810	1610	1430	1260	1120

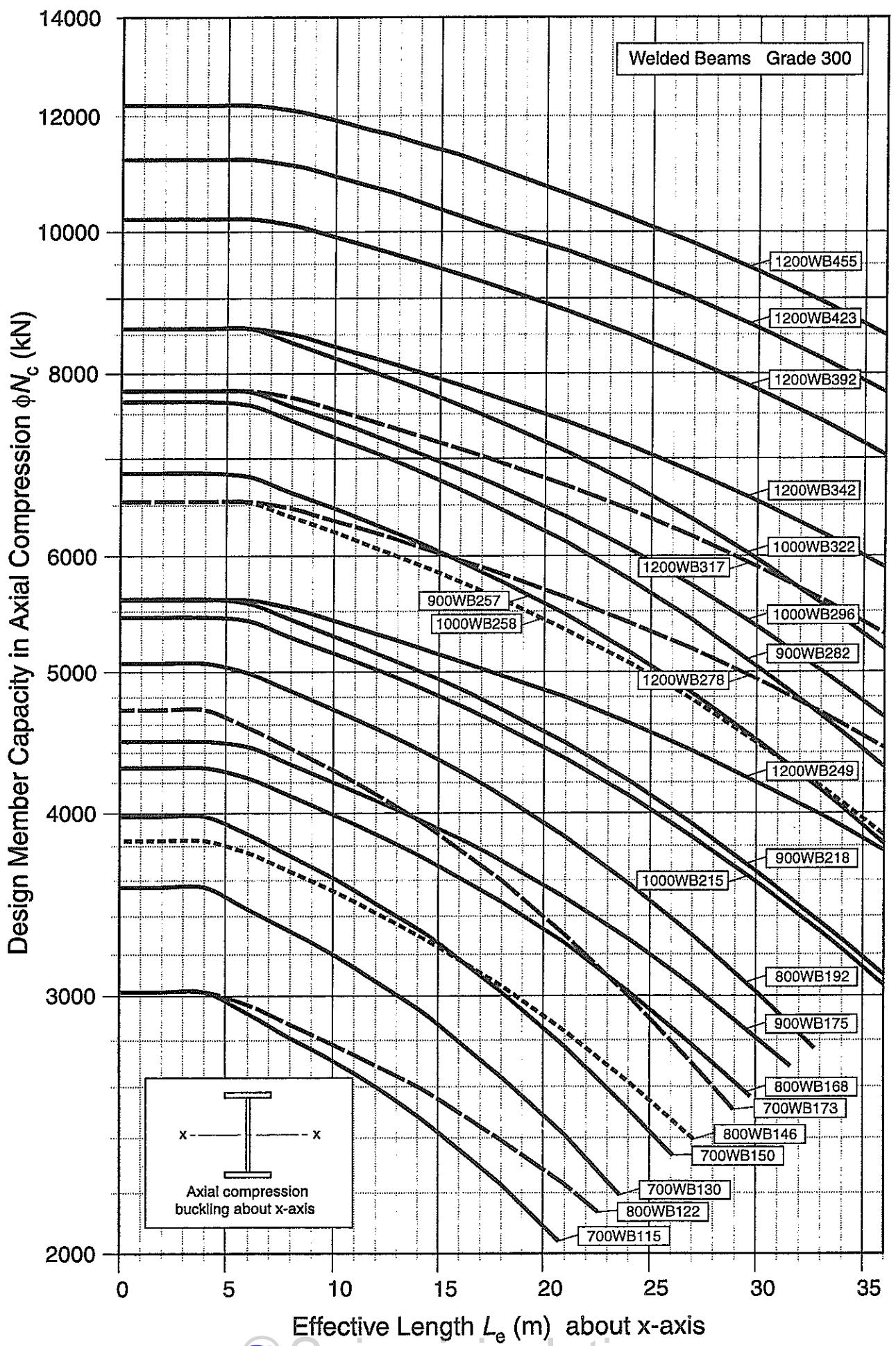
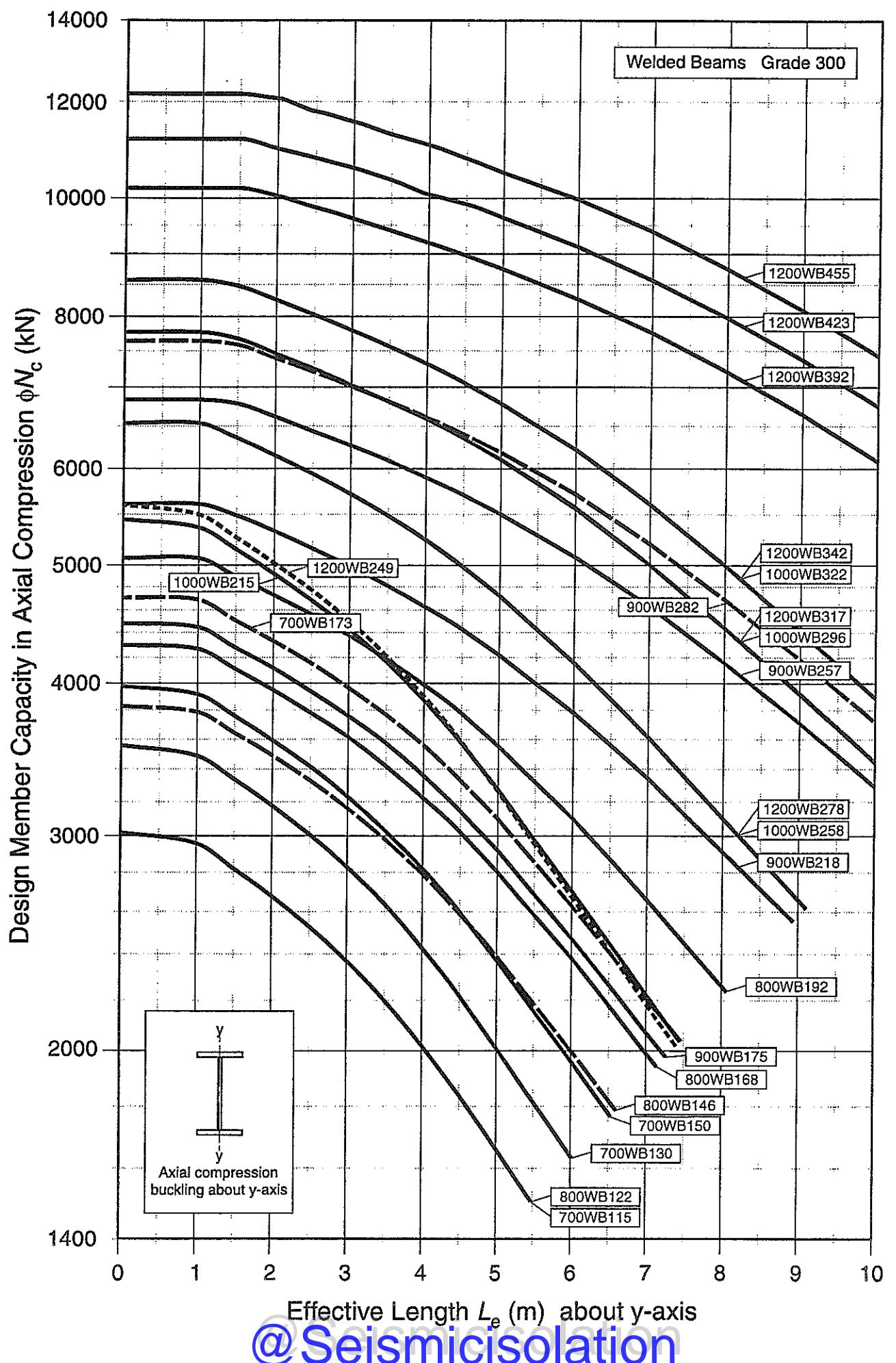




TABLE 6-1(B)

**WELDED BEAMS  
GRADE 300**
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION  
buckling about y-axis**

Designation	$\phi N_c$ (kN) ( $I_{e=0}$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN) Effective Length ( $L_e$ ) in metres												
		1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	6.0	7.0	8.0	9.0
1200WB455	12200 423	12200 11200	12100 11000	11800 10800	11600 10600	11300 10400	11100 10100	10800 9800	10500 9640	9980 9130	9390 8570	8750 7980	8090 7370	7420 6750
392	10200 342	10200 8880	10000 8830	9620 8260	9410 8030	9200 7800	9100 7560	8980 7320	8750 7060	8270 6790	7760 6220	7210 5610	6650 5000	6080 4420
317	7780 278	7780 6540	7470 6150	7260 5940	7040 5720	6820 5490	6600 5250	6360 4990	6110 4720	5580 4160	5010 3610	4450 3100	3930 2660	3450 2280
249	5800 1000WB392	5800 296	5800 7780	58260 7680	58260 7470	58030 7260	57800 7040	5760 6820	57320 6600	57060 6360	5670 6110	5610 5010	4450 3100	3930 2660
5450	5370 900WB282	5370 7650	5370 7590	5370 7400	5370 7210	5370 7020	5370 6820	5370 6620	5370 6410	5370 6190	5370 5710	5370 5510	4450 4160	3930 3100
215	5370 900WB282	5370 7650	5370 7590	5370 7400	5370 7210	5370 7020	5370 6820	5370 6620	5370 6410	5370 6190	5370 5710	5370 5510	4450 4160	3930 3100
175	4450 800WB192	4450 5070	4450 4900	4450 4730	4450 4560	4450 4380	4450 4190	4450 3930	4450 3780	4450 3550	4450 3100	4450 2660	4450 2260	3450 3190
4480	4450 800WB192	4450 5070	4450 4900	4450 4730	4450 4560	4450 4380	4450 4190	4450 3930	4450 3780	4450 3550	4450 3100	4450 2660	4450 2260	3450 3190
5610	5610 4270	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
4480	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 2920	4450 2720	4450 2520	4450 2320	4450 2120	3450 3190
5610	5610 4270	5610 4110	5610 3950	5610 3780	5610 3610	5610 3420	5610 3220	5610 3020	5610 2820	5610 2620	5610 2420	5610 2220	5610 2020	3450 3190
175	4450 4280	4450 4280	4450 4120	4450 3940	4450 3760	4450 3570	4450 3360	4450 3140	4450 29					



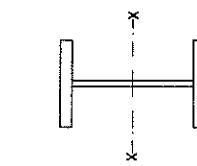
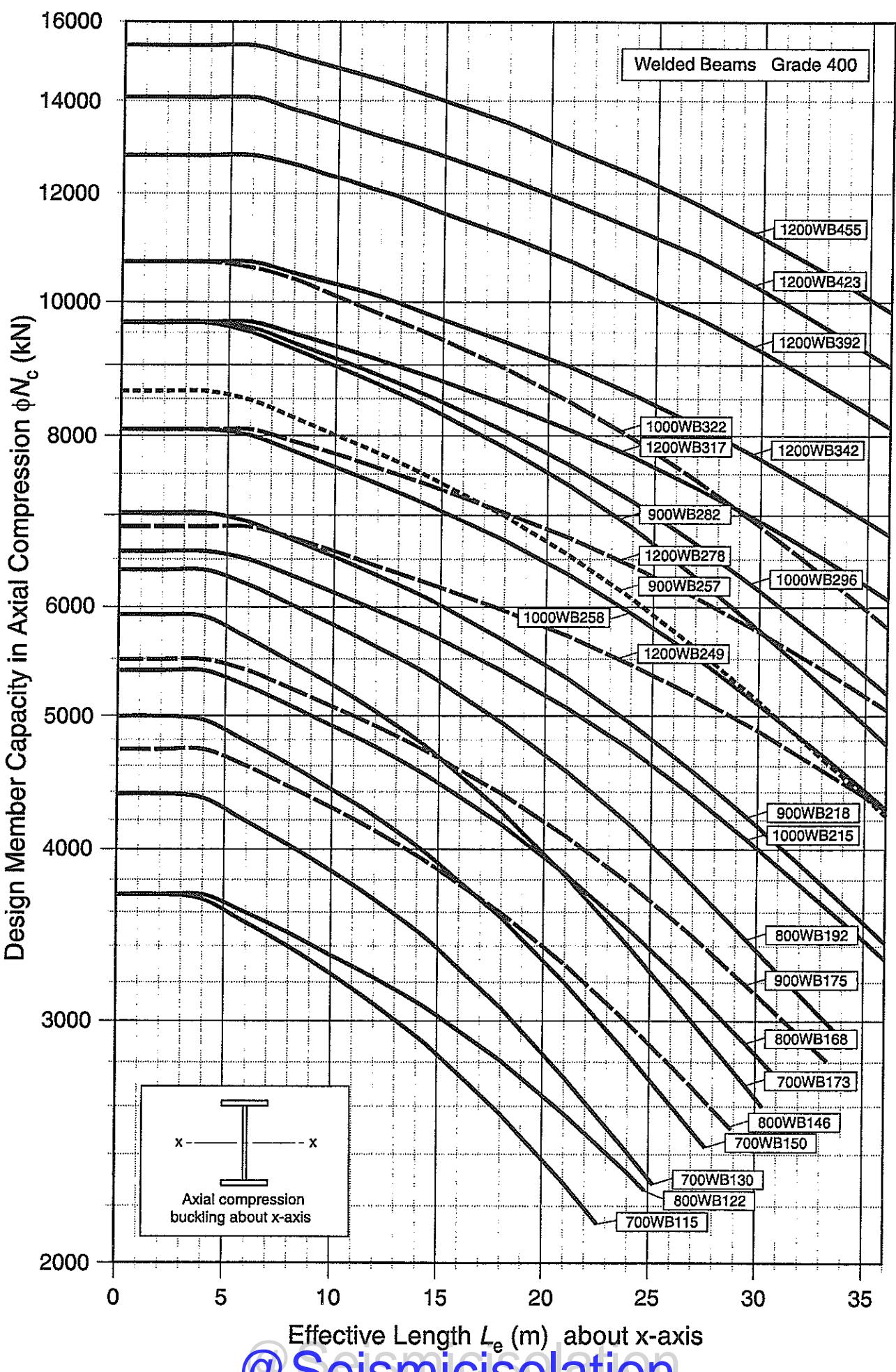


TABLE 6-2(A)

**WELDED BEAMS  
GRADE 400**
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION  
buckling about x-axis**

Designation	$\phi N_s$ (kN) ( $L_{e=0}$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN) Effective Length ( $L_e$ ) in metres													
		2	4	6	8	10	12	15	18	21	24	27	30	33	36
1200WB455	15400 423	15400 14100	15400 14100	15100 13800	14800 13500	14500 13200	14000 12800	13500 11200	12900 11300	12400 10800	11800 10200	11100 9580	10500 9580	9830 8970	
1200 392	12800 342	12800 10700	12800 10700	12600 10500	12300 10300	12000 10100	11600 9710	11200 9350	10700 8970	10200 8560	9740 8140	9210 7690	8660 7280	8110 6770	
1000 317	9680 278	9680 8090	9680 8090	9680 8090	9490 9090	9290 7930	9080 7760	8760 7580	8430 7310	8080 7030	7720 6740	7330 6430	6930 6100	6510 5760	6080 5410
6870 249	6870 6870	6870 6870	6870 6740	6590 6430	6590 6280	6590 5970	6590 5690	6590 5580	6280 5380	5720 5450	5720 5170	4880 4570	4570 4270	4570 4270	
1000WB322	10700 296	10700 9680	10700 9680	10600 9590	10400 9340	10100 9100	9810 8850	9390 8460	8940 8060	8460 7620	7960 7160	7420 6670	6870 6170	6330 5670	5800 5190
8090 258	8090 6590	8090 6590	8090 6590	8010 6550	7800 6330	7590 6150	7380 5970	7050 5690	6710 5580	6340 5380	5940 4730	5530 4730	5100 4370	4690 4010	4280 3650
900WB282	9660 257	9660 8620	9660 8620	9510 8490	9250 8250	9080 8010	8710 7770	8280 7390	7840 6690	7360 6550	6850 6090	6310 5610	5780 5130	5260 4660	4770 4230
7030 218	7030 5500	7030 5500	6920 5400	6720 5240	6530 5080	6330 4920	6020 4660	5880 4390	5630 4090	5330 3780	4940 3780	4550 3460	4160 3460	3780 3140	3420 2840
5500 175	5500 3710	5500 3710	5400 3710	5260 3600	4920 3480	4750 3350	4470 3280	4170 3030	3840 2810	3500 2570	3170 2330	2840 2330	2400 2090	2140 1860	2270 1660
800WB192	6390 168	6390 5400	6390 5400	6230 5260	6030 5090	5830 4920	5620 4750	5300 4470	4940 4170	4560 3840	4170 3500	3770 3170	3380 2840	3030 2400	2710 2140
5400 146	4730 3710	4730 3710	4600 3710	4440 3600	4290 3480	4130 3350	3870 3280	3600 3030	3300 2810	2990 2570	2690 2330	2690 2330	2400 1860	2270 1660	2270 1480
3710 122	3710 3710	3710 3710	3600 3600	3480 3480	3350 3350	3280 3280	3030 2810	2810 2570	2570 2330	2330 2090	2330 2090	2330 2090	2330 1860	2330 1660	2330 1480
700WB173	5930 150	5930 5000	5930 4970	5700 4790	5480 4610	5270 4420	5040 4230	4670 3910	4260 3570	3830 3200	3400 2840	3000 2410	2640 2110	2320 1840	2050 1610
4390 130	4390 3710	4390 3710	4360 3710	4190 3680	4030 3440	3860 3250	3680 3090	3390 2840	3070 2570	2730 2290	2410 2010	2110 1760	1930 1530	1700 1340	1420 1180

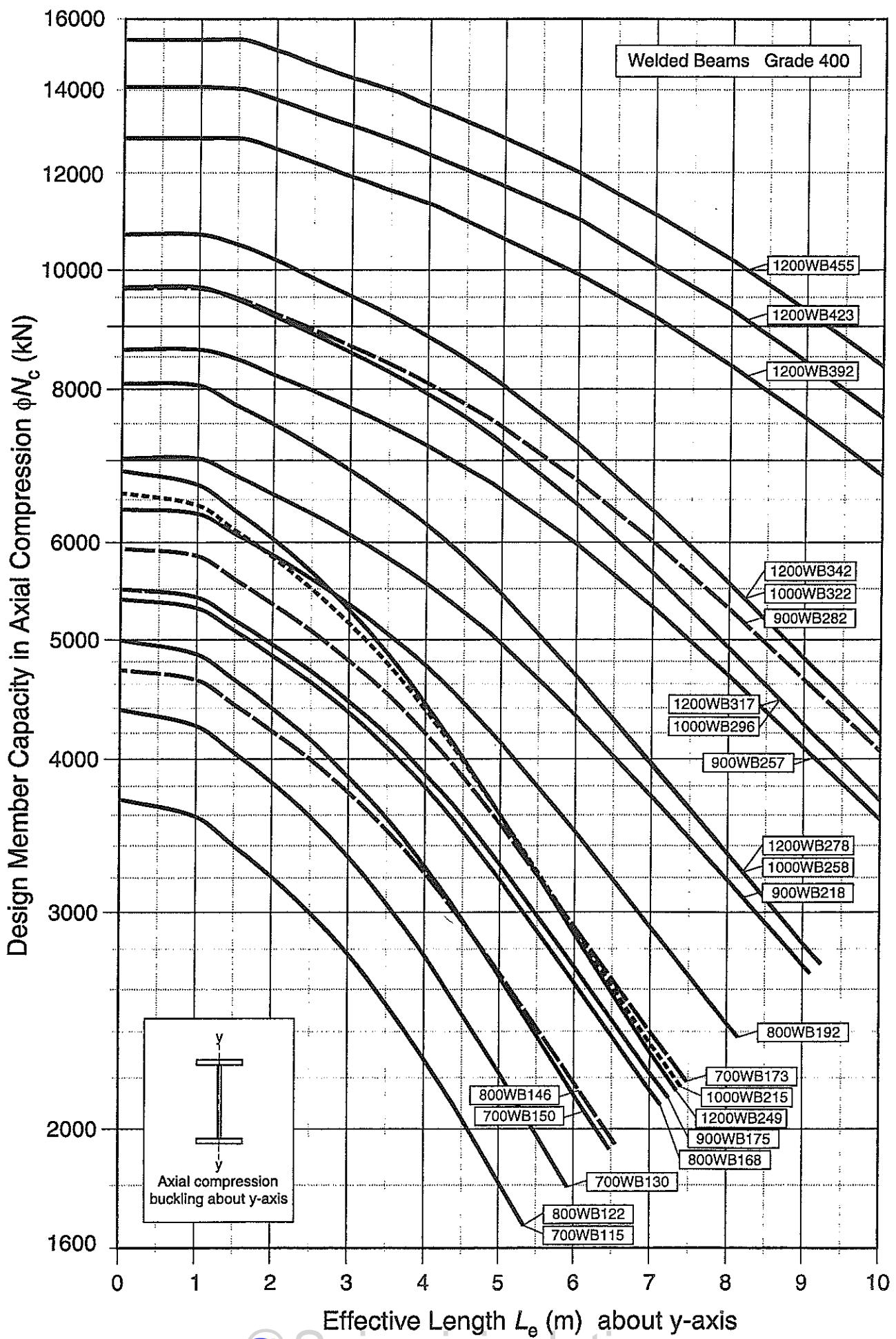


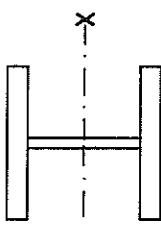


**WELDED BEAMS  
GRADE 400**

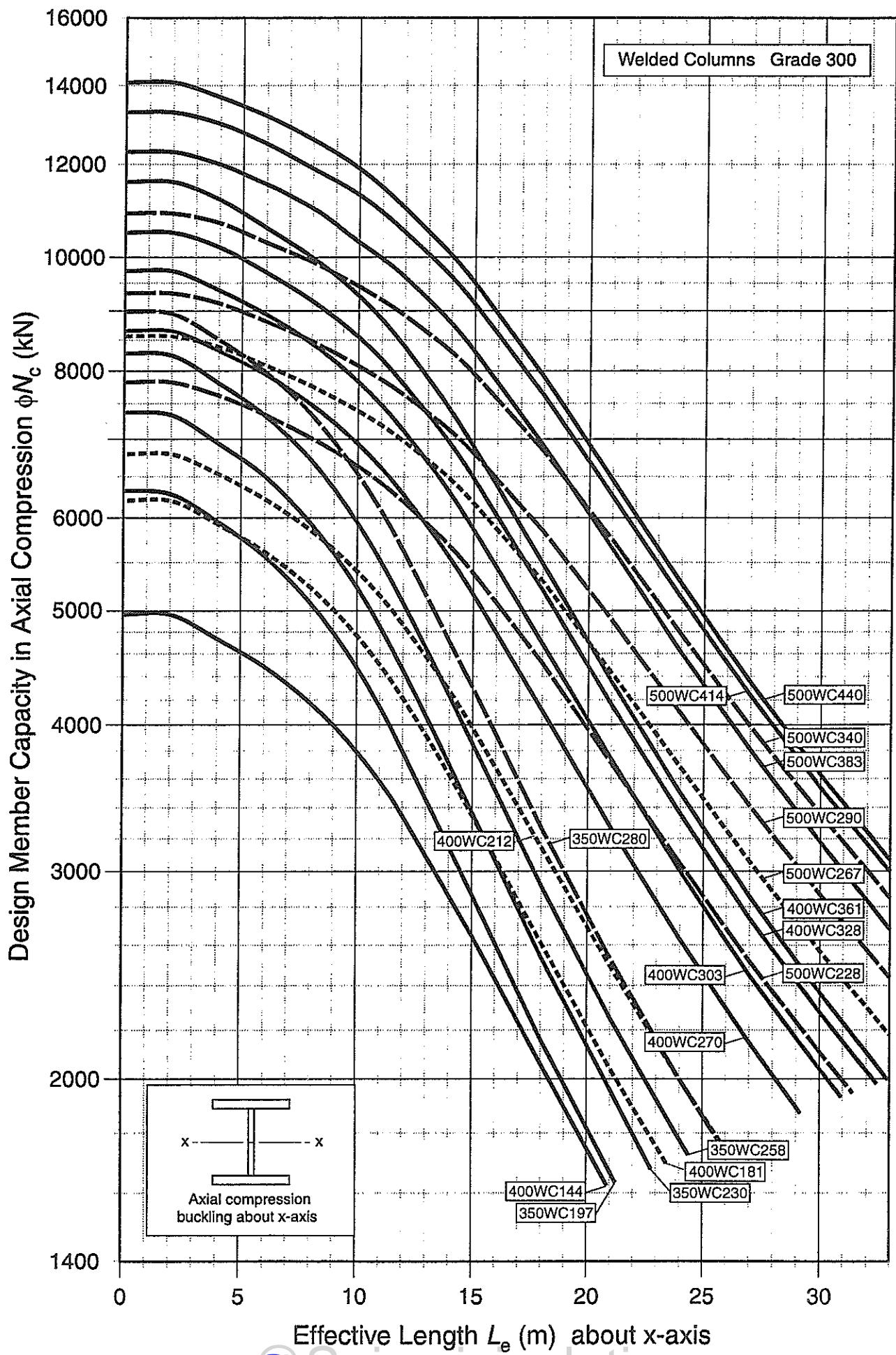
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION  
buckling about y-axis**

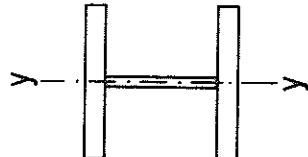
Designation	$\phi N_u$ (kN) ( $L_e=0$ )	Design Load Capacities for Axial Compression, $\phi N_c$ (kN)													
		1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	6.0	7.0	8.0	9.0	10.0
1200WB55	15400	15400	15400	15000	14700	14300	14000	13600	13200	12800	12000	11100	10200	9260	8350
423	14100	14100	14100	13700	13400	13100	12800	12400	12000	11700	11000	10100	9290	8420	7580
392	12800	12800	12800	12500	12200	11900	11600	11300	10900	10600	9910	9160	8360	7570	6800
342	10700	10700	10500	10200	9850	9520	9190	8830	8460	8060	7230	6370	5560	4830	4190
317	9680	9680	9460	9170	8880	8570	8260	7930	7590	7220	6450	5670	4930	4270	3700
278	8090	8090	7770	7490	7190	6880	6550	6210	5840	5450	4680	3970	3350	2830	2420
249	6870	6870	6370	6040	5680	5290	4880	4440	4010	3600	2880	2310	1880	1550	1300
100WB322	10700	10700	10500	10200	9850	9520	9190	8830	8460	8060	7230	6370	5560	4830	4190
296	9680	9680	9460	9170	8880	8570	8260	7930	7590	7220	6450	5670	4930	4270	3700
258	8090	8090	8060	7770	7490	7190	6880	6550	6210	5840	5450	4680	3960	3350	2830
215	6590	6590	6440	6140	5840	5510	5160	4790	4390	3990	3600	2910	2350	1920	1590
900WB282	9660	9490	9220	8950	8670	8390	8090	7780	7450	7060	6370	5670	5000	4440	4060
257	8620	8620	8470	8220	7980	7730	7470	7200	6910	6620	5980	5320	4680	4090	3570
218	7030	7030	6810	6570	6340	6090	5830	5560	5270	4970	4340	3730	3190	2720	2340
175	5500	5420	5190	4960	4720	4460	4190	3890	3590	3280	2710	2220	1840	1530	1290
800WB192	6390	6340	6100	5860	5610	5350	5060	4770	4450	4130	3490	2920	2440	2050	1740
168	5400	5310	5090	4860	4620	4370	4090	3800	3490	3190	2630	2150	1780	1480	1250
146	4730	4640	4430	4220	4000	3760	3500	3230	2950	2680	2180	1770	1450	1200	1010
122	3710	3590	3400	3210	3000	2780	2530	2280	2040	1810	1430	1140	922	757	631
700WB173	5930	5850	5600	5350	5090	4810	4520	4200	3870	3540	2920	2400	1980	1650	1390
150	5000	4870	4640	4400	4150	3870	3580	3270	2960	2660	2130	1720	1400	1150	966
130	4390	4260	4050	3830	3590	3330	3050	2770	2480	2220	1760	1410	1140	938	783
115	3710	3590	3400	3210	3000	2780	2530	2280	2040	1810	1430	1140	921	757	631




  
**TABLE 6-3(A)**  
**WELDED COLUMNS**  
**GRADE 300**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about x-axis**

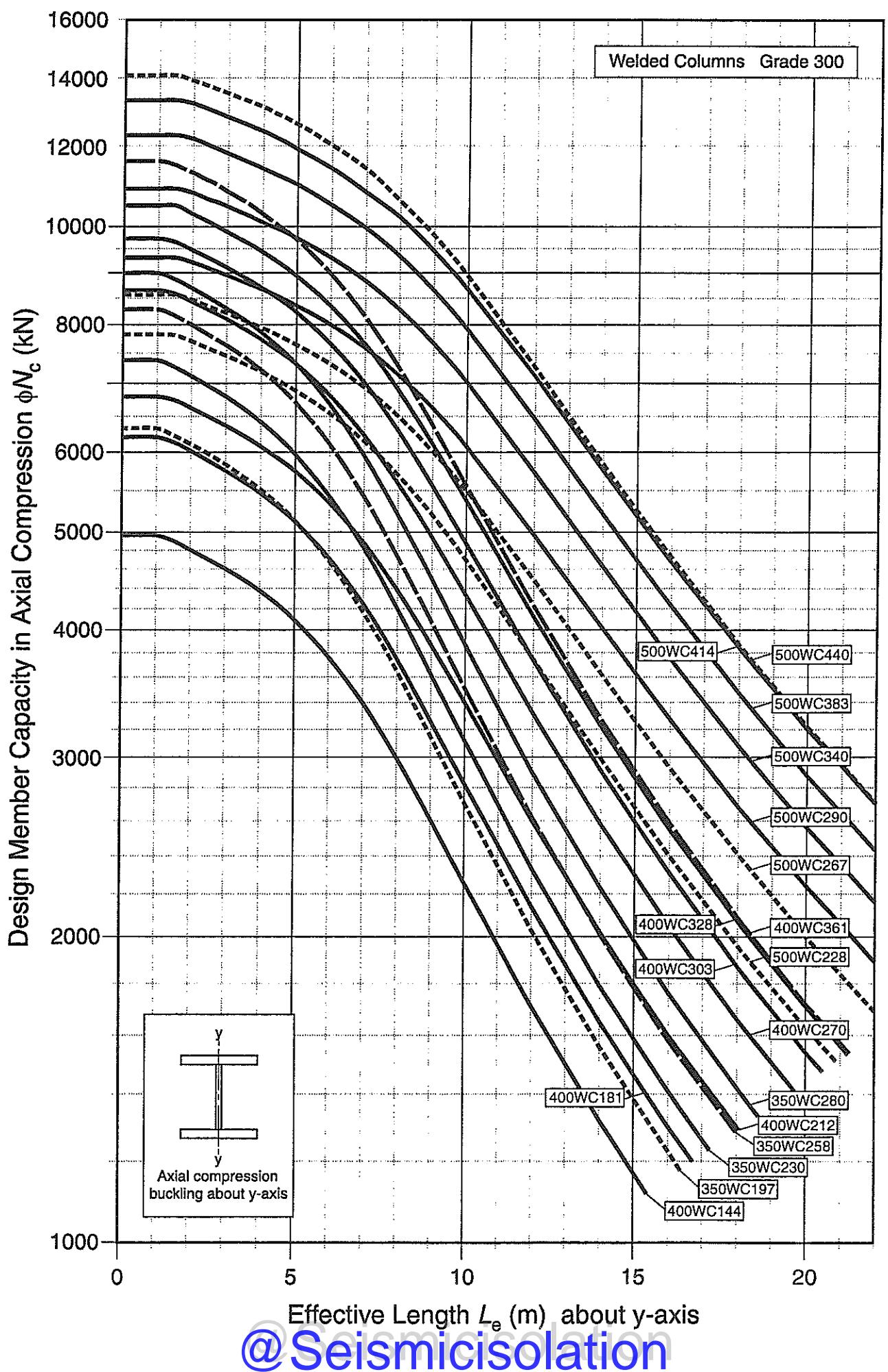
Designation	$\phi N_s$ (kN) ( $L_a=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)											
		2	4	6	8	10	12	15	18	21	24	27	30
500WC440	14100	14100	13700	13200	12800	11900	11000	9510	7910	6460	5280	4350	3630
414	13300	13300	13000	12500	11900	11300	10500	9120	7630	6260	5130	4240	3540
383	12300	12300	12000	11500	11000	10300	9610	8310	6910	5650	4610	3810	3000
340	10900	10900	10700	10300	9910	9450	8920	7950	6840	5750	4780	3990	3180
290	9320	9320	9140	8820	8480	8080	7630	6800	5850	4910	4090	3410	2850
267	8570	8570	8390	8090	7770	7400	6970	6180	5360	4430	3680	3060	2440
228	7830	7830	7630	7340	7020	6640	6190	5390	4520	3710	3050	2520	2180
400WC361	11600	11600	11200	10600	10000	9280	8390	6880	5490	4360	3500	2860	2370
328	10500	10500	10200	9710	9180	8550	7780	6480	5210	4160	3360	2740	1990
303	9730	9730	9370	8940	8440	7830	7100	5870	4690	3740	3000	2450	1920
270	8660	8660	8330	7950	7490	6940	6280	5170	4120	3270	2630	2150	1710
212	6800	6800	6540	6230	5860	5410	4870	3980	3150	2490	2000	1630	1500
181	6210	6210	5930	5620	5240	4770	4220	3350	2610	2040	1630	1320	1130
144	4970	4970	4740	4490	4180	3800	3350	2650	2050	1610	1280	1040	858
350WC280	9000	8960	8510	7990	7550	6540	5630	4310	3270	2530	2000	1620	1340
258	8290	8250	7820	7350	6720	5950	5080	3860	2920	2250	1780	1440	1120
230	7380	7340	6950	6510	5940	5240	4460	3370	2340	1960	1550	1250	991
197	6330	6290	5960	5570	5080	4480	3800	2870	2160	1670	1310	1060	861

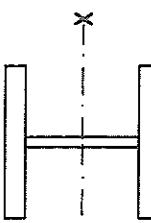




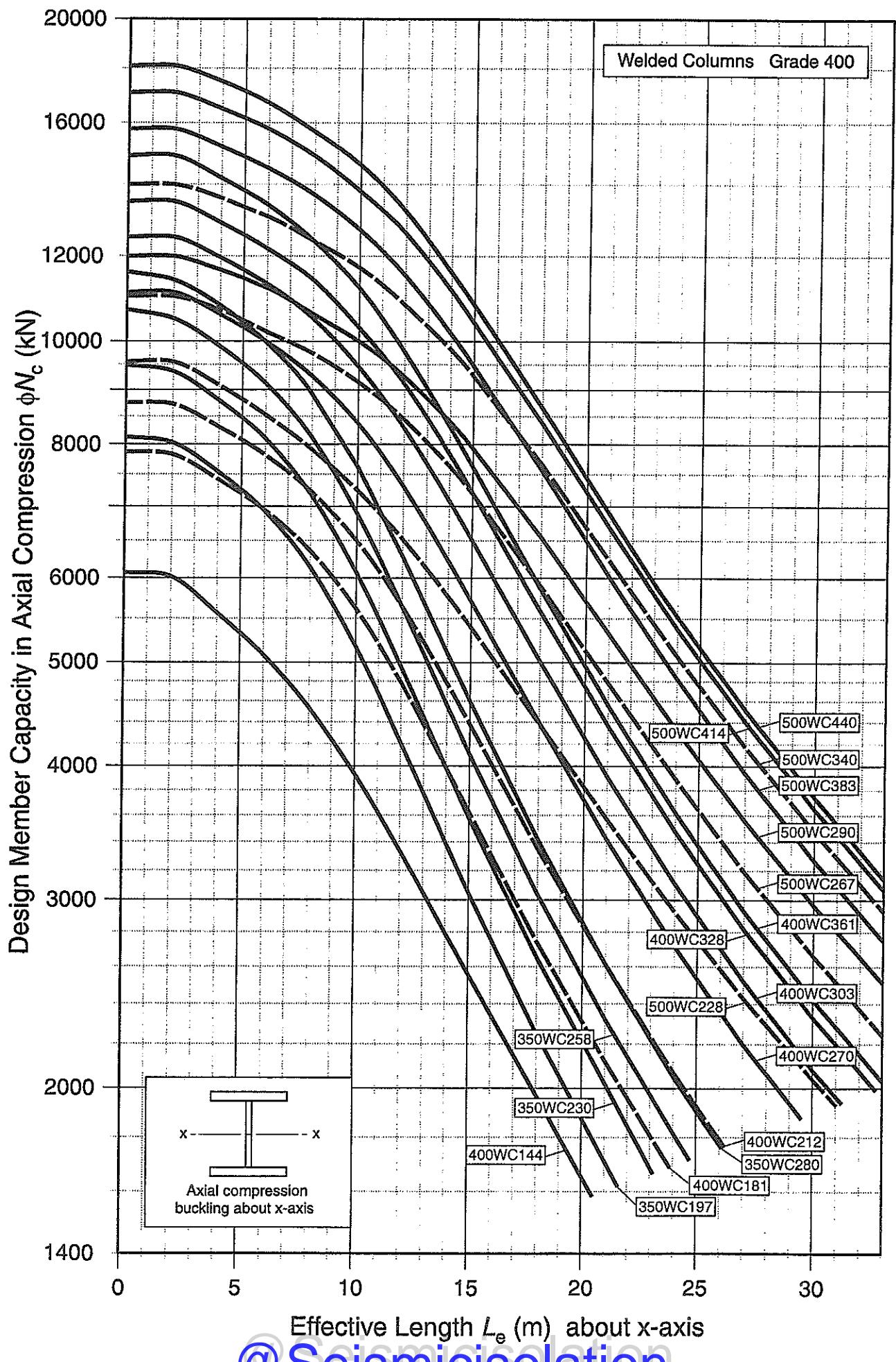
**TABLE 6-3(B)**  
**WELDED COLUMNS**  
**GRADE 300**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about y-axis**

Designation	$\phi N_c$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN) Effective Length ( $L_e$ ) in metres																
		1	2	3	4	5	6	7	8	9	10	12	14	16	18	20	22	
500WC440		14100	13900	13500	13100	12800	12000	11400	10600	8940	7260	5840	4730	3870	3220	2710		
414		13300	13300	13200	12800	12400	11900	11400	10800	8660	7110	5750	4670	3840	3200	2700		
383		12300	12300	12200	11800	11400	11000	10500	9960	9340	7910	6460	5210	4230	3470	2880	2450	
340		10900	10900	10800	10500	10100	9740	9320	8840	8280	7020	5730	4630	3750	3080	2560	2160	
290		9320	9220	8950	8570	8350	8000	7590	7130	6070	4970	4020	3270	2680	2240	1880		
267		8570	8470	8220	7950	7650	7320	6940	6500	5500	4490	3620	2930	2410	2000	1690		
228		7830	7710	7460	7190	6890	6550	6150	5760	4700	3750	2990	2400	1960	1630	1370		
400WC361		11600	11300	10800	10300	9700	8980	8150	7260	5560	4230	3270	2590	2090	1720	1440		
328		10500	10300	9880	9450	8940	8350	7660	6890	5380	4130	3220	2550	2070	1710	1430		
303		9730	9730	9480	9110	8700	8230	7660	7010	6290	4880	3740	2910	2310	1870	1540		
270		8660	8660	8430	8110	7740	7320	6820	6230	5590	4340	3320	2580	2050	1660	1370		
212		6800	6800	6630	6370	6080	5750	5350	4890	4380	3400	2600	2020	1600	1300	1070		
181		6210	6210	6020	5760	5470	5130	4720	4250	3750	2830	2140	1650	1300	1050	895		
144		4970	4970	4810	4610	4380	4100	3770	3400	3000	2260	1710	1320	1040	839	691		
350WC280		9000	8890	8300	7860	7320	6680	5950	5200	3870	2900	2230	1760	1420	1160	973		
258		8290	8290	8000	7640	7220	6710	6110	5430	4730	3510	2620	2010	1580	1280	1050		
230		7380	7380	7120	6800	6420	5970	5430	4830	4200	3120	2330	1790	1410	1130	932		
197		6330	6330	6110	5840	5520	5140	4690	4170	3650	2710	2030	1560	1230	990	814		
																681		



  
**TABLE 6-4(A)**  
**WELDED COLUMNS**  
**GRADE 400**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about x-axis**

Designation	$\phi N_s$ (kN)	Design Member Capacities in Axial Compression, $\phi N_c$ (kN) Effective Length ( $l_{e0}$ ) in metres											
		2	4	6	8	10	12	15	18	21	24	27	
500WC440	18100 414	18100 17100	17500 16500	16700 15800	15700 14500	14600 13700	13200 12700	10800 9470	8650 7560	6870 6010	5520 4830	4510 3940	3740 3270
414	17100	16500	15800	15200	14500	13700	12700	10800	9280	7660	6220	5070	3650
383	15800	15200	14000	13600	13100	12400	11700	10800	9260	7930	6550	5320	3940
340	14000	13600	12800	12000	11600	11200	10600	10000	8440	7190	5900	4780	3480
290	12800	12000	11000	10700	10200	9740	9150	8440	7190	5900	4380	3560	2970
267	11000	9570	9100	8530	7920	7250	6520	5400	4390	3750	3190	2660	2240
228	9570	9100	14900	14200	13400	12400	11200	9760	7620	5860	4560	3620	2440
400WC361	14900	14200	13600	12900	12200	11400	10300	9120	7210	5590	4370	3290	2420
328	13600	12900	12500	11900	11300	10500	9460	8290	6510	5020	3910	3480	2330
303	12500	11900	11100	10600	9990	9270	8370	7310	5710	4400	3420	2520	1980
270	11100	8730	8310	7820	7230	6500	5650	4380	3350	2610	2070	1670	1750
212	8730	7830	7420	6950	6360	5620	4790	3630	2740	2120	1670	1380	1520
181	7830	7420	6670	6020	5570	5090	4540	3940	3340	2560	1970	1550	1110
144	6670	6020	11600	11400	10800	9970	8920	7630	6290	4600	3420	2610	1830
350WC280	11600	11400	10500	9900	9130	8130	6900	5650	4110	3040	2320	1650	1130
258	10500	9900	9370	8800	8100	7180	6070	4950	3580	2650	2020	1470	1010
230	9490	8130	8030	7540	6930	6140	5180	4210	3050	2250	1710	1340	1050
197													874



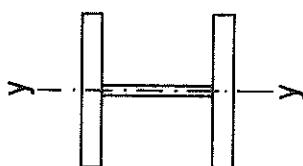


TABLE 6-4(B)

**WELDED COLUMNS  
GRADE 400**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about y-axis**

Designation	$\phi N_s$ (kN) ( $L_{\text{eff}} = 0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)														
		1	2	3	4	5	6	7	8	9	10	12	14	16	18	20
500WC440	18100	18100	17800	17200	16500	15700	14800	13700	12500	10000	7840	6160	4910	3990	3300	2770
414	17100	17100	16800	16200	15600	14900	14100	13100	12100	9780	7710	6080	4870	3960	3280	2760
383	15800	15800	15500	15000	14400	13700	13000	12100	11100	8900	6990	5500	4400	3580	2960	2490
340	14000	14000	13700	13300	12800	12200	11500	10700	9800	7900	6200	4890	3910	3180	2630	2210
290	12000	12000	11800	11400	10900	10400	9870	9210	8460	6850	5390	4260	3410	2770	2290	1930
267	11000	11000	10800	10400	10000	9560	9020	8390	7690	6190	4850	3820	3050	2480	2050	1730
228	9570	9570	9240	8760	8250	7700	7100	6460	5810	4590	3610	2870	2320	1900	1580	1340
400WC361	14900	14900	14300	13600	12800	11900	10700	9400	8120	5940	4410	3370	2650	2130	1750	1460
328	13500	13500	13100	12500	11800	11000	10000	8930	7790	5790	4340	3330	2620	2110	1740	1450
303	12500	12500	12100	11500	10500	10100	9180	8150	7090	5250	3920	3010	2370	1910	1570	1310
270	11100	11100	10700	10200	9680	8990	8170	7250	6300	4660	3480	2670	2100	1690	1390	1160
212	8750	8750	8430	8050	7600	7060	6410	5680	4940	3650	2720	2090	1640	1320	1090	909
181	7870	7870	7540	7170	6720	6180	5530	4820	4130	3000	2220	1690	1330	1070	877	732
144	6070	6070	5710	5320	4890	4420	3900	3400	2930	2170	1640	1270	1010	821	679	570
350WC280	11600	11600	11000	10500	9750	8870	7840	6750	5720	4100	3010	2290	1790	1440	1180	986
258	10700	10700	10200	9620	8950	8130	7160	6140	5190	3700	2720	2070	1620	1300	1060	889
230	9480	9480	9040	8560	7960	7230	6360	5460	4610	3290	2420	1840	1440	1150	946	790
197	8130	8130	7760	7350	6850	6230	5500	4730	4010	2870	2110	1600	1250	1010	827	690

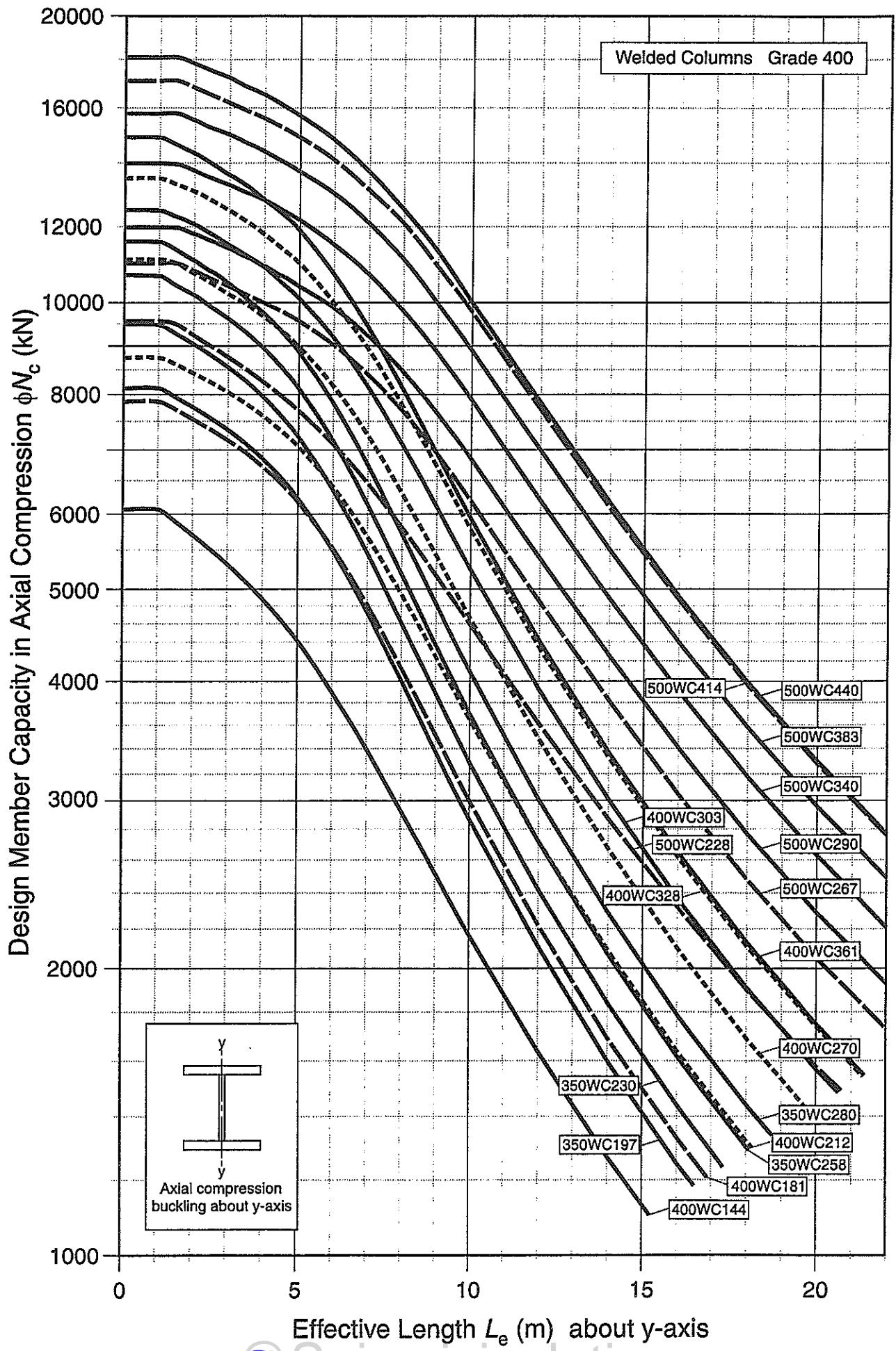
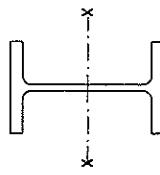


TABLE 6-5(A)

**UNIVERSAL BEAMS  
GRADE 300**

**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**

buckling about x-axis



Designation	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)												
		2	4	6	8	10	12	15	18	21	24	27	30	33
610UB 125	3820	3820	3870	3650	3430	3290	3040	2740	2410	2080	1780	1520	1310	1130
	113	3370	3340	3240	3140	3030	2910	2690	2420	2130	1840	1570	1350	1000
	101	3110	3080	2980	2890	2780	2660	2450	2190	1910	1640	1390	1190	878
530UB 92.4	2980	2960	2900	2800	2690	2570	2420	2160	1850	1560	1290	1080	908	771
	82.0	2560	2510	2420	2320	2220	2090	1860	1600	1340	1120	930	782	664
460UB 82.1	2770	2770	2860	2560	2430	2280	2090	1760	1430	1150	933	765	636	536
	74.6	2440	2440	2360	2150	2010	1850	1570	1280	1030	837	687	572	411
	67.1	2130	2130	2070	1980	1880	1770	1620	1380	1130	909	738	606	425
410UB 59.7	1940	1940	1860	1770	1660	1530	1380	1120	884	698	560	456	377	317
	53.7	1810	1810	1730	1640	1540	1410	1250	1000	783	615	491	399	330
360UB 56.7	1950	1940	1840	1730	1590	1420	1220	930	707	547	433	350	288	241
	50.7	1680	1680	1550	1500	1380	1230	1060	814	620	480	380	307	253
	44.7	1530	1530	1450	1350	1240	1100	936	710	537	414	327	264	218
310UB 46.2	1590	1570	1480	1360	1220	1040	852	622	461	362	277	223	183	153
	40.4	1430	1410	1320	1220	1080	915	746	546	399	305	239	192	132
	32.0	1070	1060	985	914	807	679	551	397	293	223	175	141	116
250UB 37.3	1370	1330	1230	1090	997	700	538	372	269	203	158	127	104	86.4
	31.4	1150	1120	1030	904	738	570	435	300	217	163	127	102	83.1
	25.7	883	870	799	704	578	449	344	237	172	129	101	80.6	66.0
200UB 29.8	1100	1050	998	767	569	411	304	204	146	109	84.7	67.6	55.2	45.9
	25.4	930	889	787	637	467	336	247	166	118	88.6	68.7	54.8	44.7
	22.3	826	790	699	566	415	298	220	148	105	78.8	61.1	48.7	39.8
180UB 22.2	813	764	650	483	329	229	166	110	78.1	58.3	45.1	35.9	29.3	20.5
	18.1	663	623	527	388	263	182	132	87.5	62.1	46.3	35.8	28.5	23.2
	16.1	589	552	466	341	231	160	115	76.6	54.3	40.5	31.3	24.9	20.3
150UB 18.0	661	609	486	323	208	141	101	66.5	47.0	34.9	27.0	21.5	17.5	14.5
	14.0	574	471	371	242	154	104	74.6	49.1	34.6	25.8	19.9	15.8	12.9

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

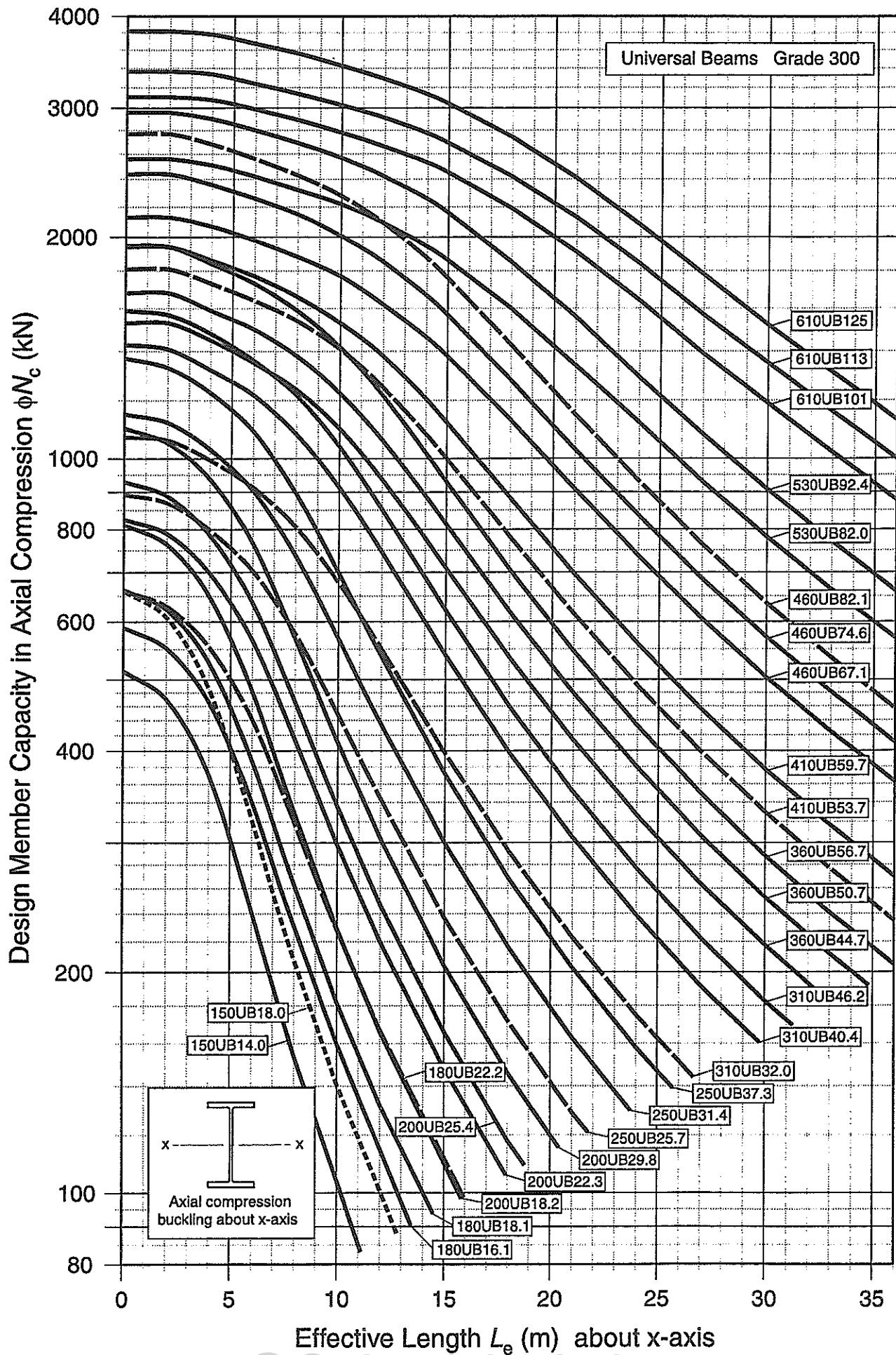




TABLE 6-5(B)

**UNIVERSAL BEAMS  
GRADE 300**
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION  
buckling about y-axis**

Designation	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)													
		1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	6.0	7.0	8.0	9.0	10.0
610UB125	3820	3730	3590	3430	3250	3040	2790	2550	2240	1970	1520	1180	938	760	628
113	3370	3290	3170	3030	2870	2680	2450	2210	1960	1720	1320	1030	819	663	547
101	3110	3030	2910	2770	2610	2420	2200	1970	1730	1510	1150	892	707	571	471
530UB 92.4	2960	2860	2780	2590	2410	2200	1970	1720	1490	1280	963	740	583	470	387
82.0	2560	2470	2360	2280	2080	1890	1680	1470	1270	1090	818	628	494	398	328
460UB 82.1	2770	2650	2520	2380	2170	1940	1690	1450	1230	1050	776	591	463	373	306
74.6	2440	2340	2220	2080	1920	1720	1500	1280	1090	932	690	526	413	332	273
67.1	2130	2050	1950	1830	1680	1500	1310	1120	957	816	604	461	362	291	239
410UB 59.7	1940	1850	1750	1630	1490	1320	1130	961	812	689	507	385	302	242	199
53.7	1810	1720	1620	1500	1380	1180	1000	843	707	597	437	331	259	208	170
360UB 56.7	1950	1850	1750	1620	1460	1270	1080	906	760	642	470	356	279	223	183
50.7	1680	1600	1510	1400	1260	1100	936	786	660	557	408	309	242	194	159
44.7	1530	1450	1360	1260	1120	967	814	678	566	476	347	263	205	165	135
310UB 46.2	1590	1510	1420	1320	1190	1040	880	739	620	523	383	290	227	182	149
40.4	1430	1350	1270	1170	1050	907	764	638	533	449	327	248	194	155	127
32.0	1070	1000	929	833	715	591	481	392	323	269	194	146	114	91.0	74.4
250UB 37.3	1370	1280	1180	1060	913	755	615	502	413	345	249	187	146	116	95.3
31.4	1150	1070	989	880	747	612	494	401	329	274	197	148	115	92.2	75.4
25.7	893	810	726	615	491	383	301	240	195	161	115	86.1	66.8	53.3	43.5
200UB 29.8	1100	1020	929	815	679	547	437	332	288	239	172	129	100	80.0	65.3
25.4	930	854	777	675	555	443	352	283	231	191	137	103	79.8	63.7	52.0
22.3	826	759	691	601	496	396	315	253	207	171	123	92.1	71.5	57.1	46.6
18.2	661	566	467	350	254	188	144	113	90.8	74.6	52.8	39.3	30.4	24.2	19.7
180UB 22.2	813	682	544	394	281	206	157	123	98.4	80.7	57.0	42.4	32.7	26.0	21.2
18.1	663	554	440	317	225	165	125	98.1	78.8	64.6	45.6	33.9	26.2	20.8	17.0
16.1	588	491	388	278	198	145	110	85.9	69.0	56.5	39.9	29.7	22.9	18.2	14.8
150UB 18.0	661	511	361	239	164	118	88.9	69.2	55.3	45.3	31.9	23.6	18.2	14.5	11.8
14.0	514	391	271	178	122	87.4	65.7	51.1	40.9	33.4	23.5	17.4	13.4	10.7	8.68

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

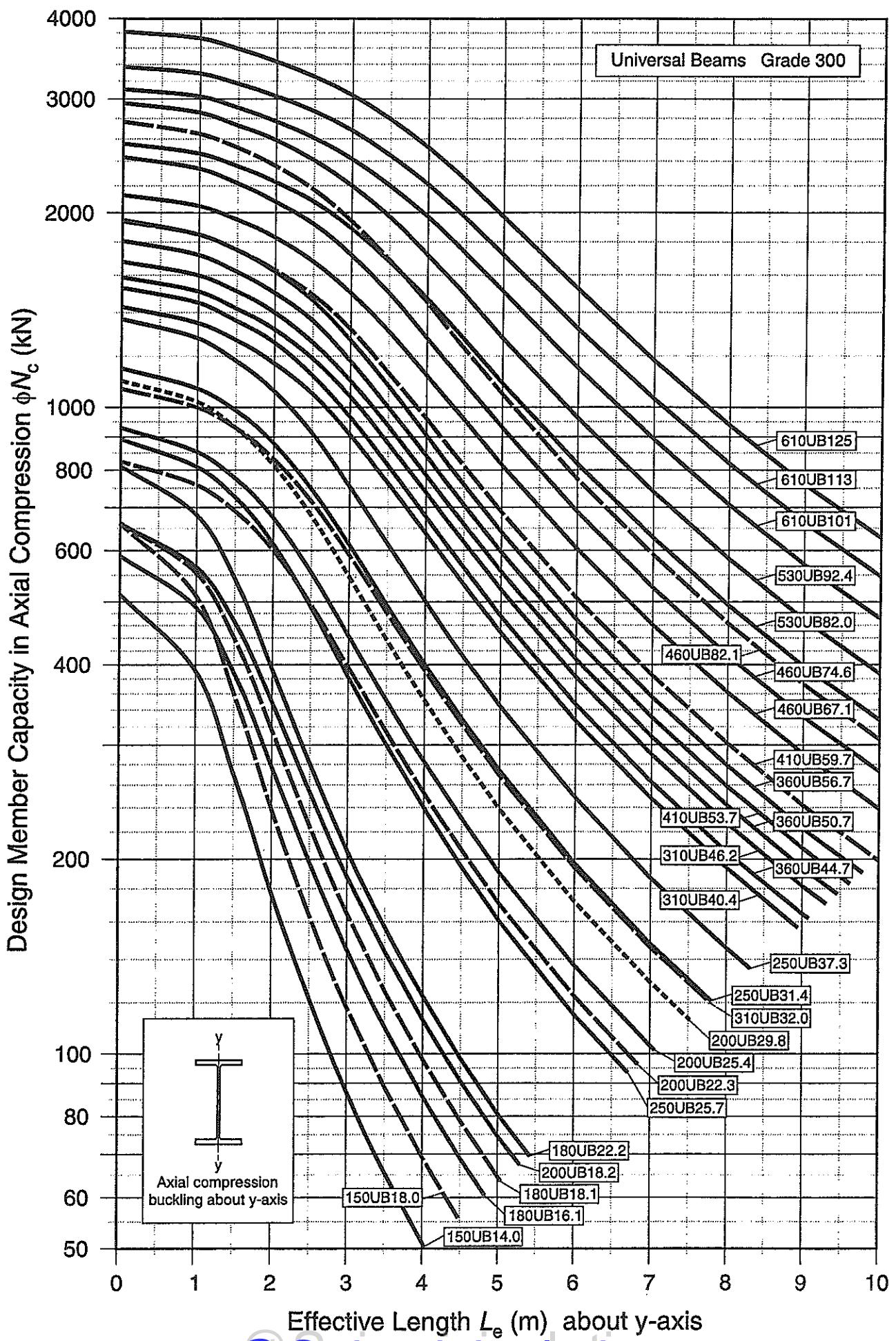
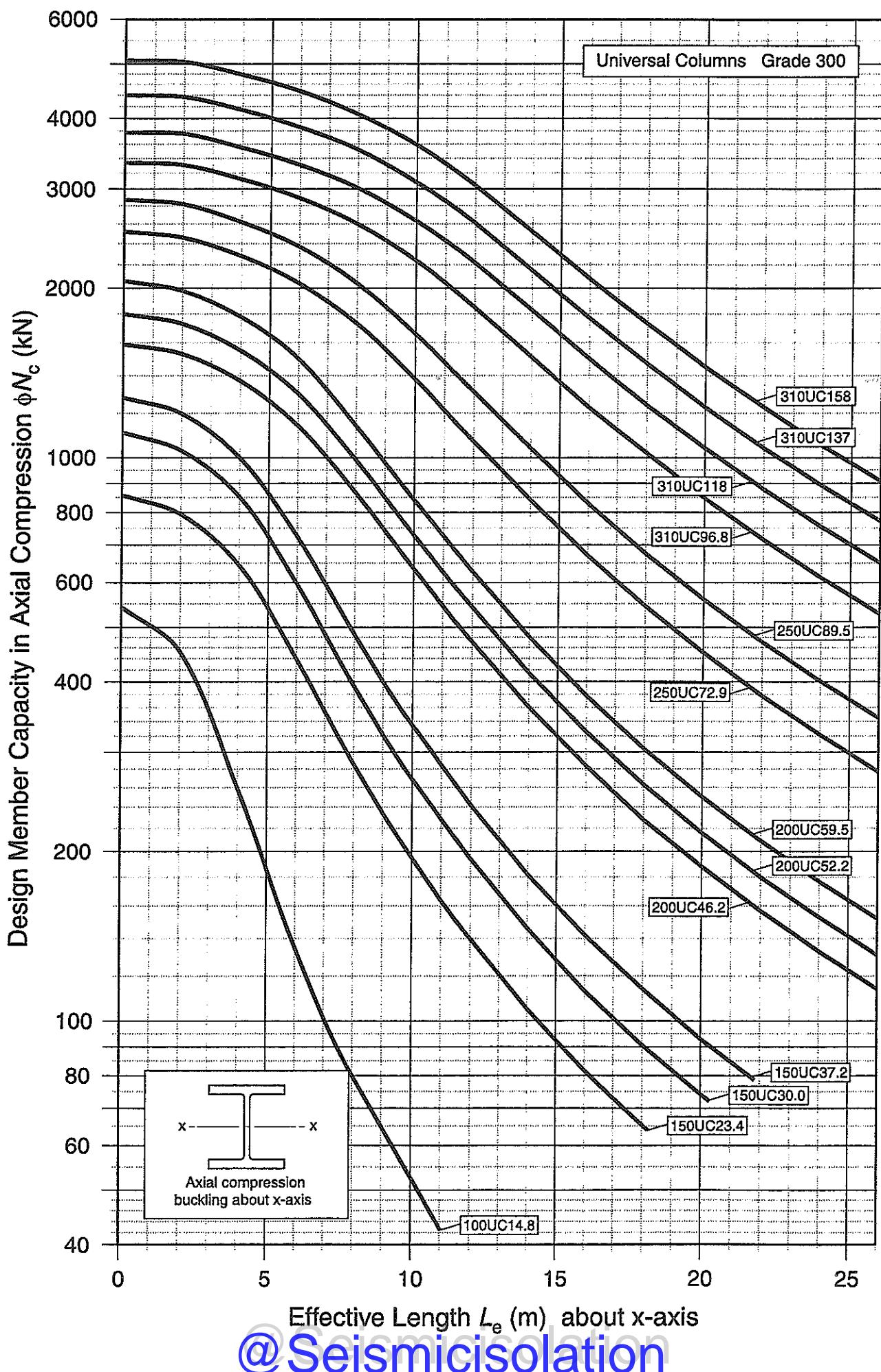


TABLE 6-6(A)  
**UNIVERSAL COLUMNS  
GRADE 300**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about x-axis**

Designation	$\phi N_c$ (kN) ( $L_e = 0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)											
		2	4	6	8	10	12	14	16	18	20	22	24
310UC158	5070	5040	4780	4470	4070	3590	3040	2520	2080	1730	1450	1230	1050
137	4440	4370	4140	3860	3540	3080	2610	2150	1770	1470	1230	1040	909
118	3780	3760	3550	3310	3010	2630	2220	1830	1500	1240	1040	880	772
96.8	3340	3310	3120	2890	2600	2240	1850	1510	1230	1020	848	716	651
250UC 89.5	2870	2820	2370	2040	1660	1310	1040	830	676	560	471	401	345
72.9	2520	2460	2380	2040	1730	1380	1070	842	671	545	451	378	277
200UC 59.5	2060	1980	1500	1140	842	628	481	378	304	250	209	177	152
52.2	1800	1730	1550	1300	932	729	543	415	326	263	216	180	141
46.2	1560	1530	1370	1140	888	636	472	361	284	228	188	157	114
150UC 37.2	1280	1200	1000	725	486	335	242	182	142	114	93.0	77.5	65.5
30.0	1110	1030	853	597	393	269	194	146	113	90.7	74.2	61.7	52.2
23.4	859	795	645	440	266	195	140	105	81.8	65.3	53.4	44.4	37.6
100UC 14.8	543	454	259	135	80.1	52.7	37.2	27.7	21.4	17.0	13.8	11.5	9.69
													8.28

Note: Grade 300 refers to BHPS Grade 300PLUS™. See Note (1) on page 2-2.



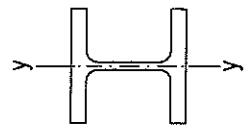


TABLE 6-6(B)

**UNIVERSAL COLUMNS  
GRADE 300**

**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION  
buckling about y-axis**

Designation	$\phi N_s$ (kN) ( $I_{e=0}$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)												
		1	2	3	4	5	6	7	8	9	10	11	12	13
310UC158	5070	4840	4590	4280	3890	3440	2960	2510	2120	1780	1530	1320	1150	1000
	4400	4200	3970	3700	3360	2960	2540	2150	1810	1520	1310	1130	978	856
	3780	3610	3410	3170	2870	2520	2160	1820	1540	1300	1110	954	828	724
	3340	3170	2980	2750	2470	2140	1810	1510	1260	1070	906	778	674	589
250UC 89.5	2870	2840	2680	2490	2240	1930	1600	1310	1070	881	735	621	531	458
	72.9	2520	2490	2340	2150	1920	1630	1330	1070	872	716	596	502	399
200UC 59.5	2060	2000	1840	1620	1330	1030	793	616	489	396	327	274	232	322
	52.2	1800	1750	1610	1420	1160	900	689	535	425	344	283	237	174
	46.2	1590	1550	1420	1250	1020	786	600	466	369	299	246	206	151
150UC 37.2	1280	1210	1060	821	581	410	299	227	177	142	116	97.1	82.2	70.5
	30.0	1110	1050	903	686	476	333	242	183	143	114	93.7	78.1	61.1
	23.4	859	807	685	507	345	239	173	131	102	81.5	66.7	55.6	49.1
100UC 14.8	543	477	323	183	111	73.6	52.2	38.9	30.1	24.0	19.6	16.2	13.7	10.1

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

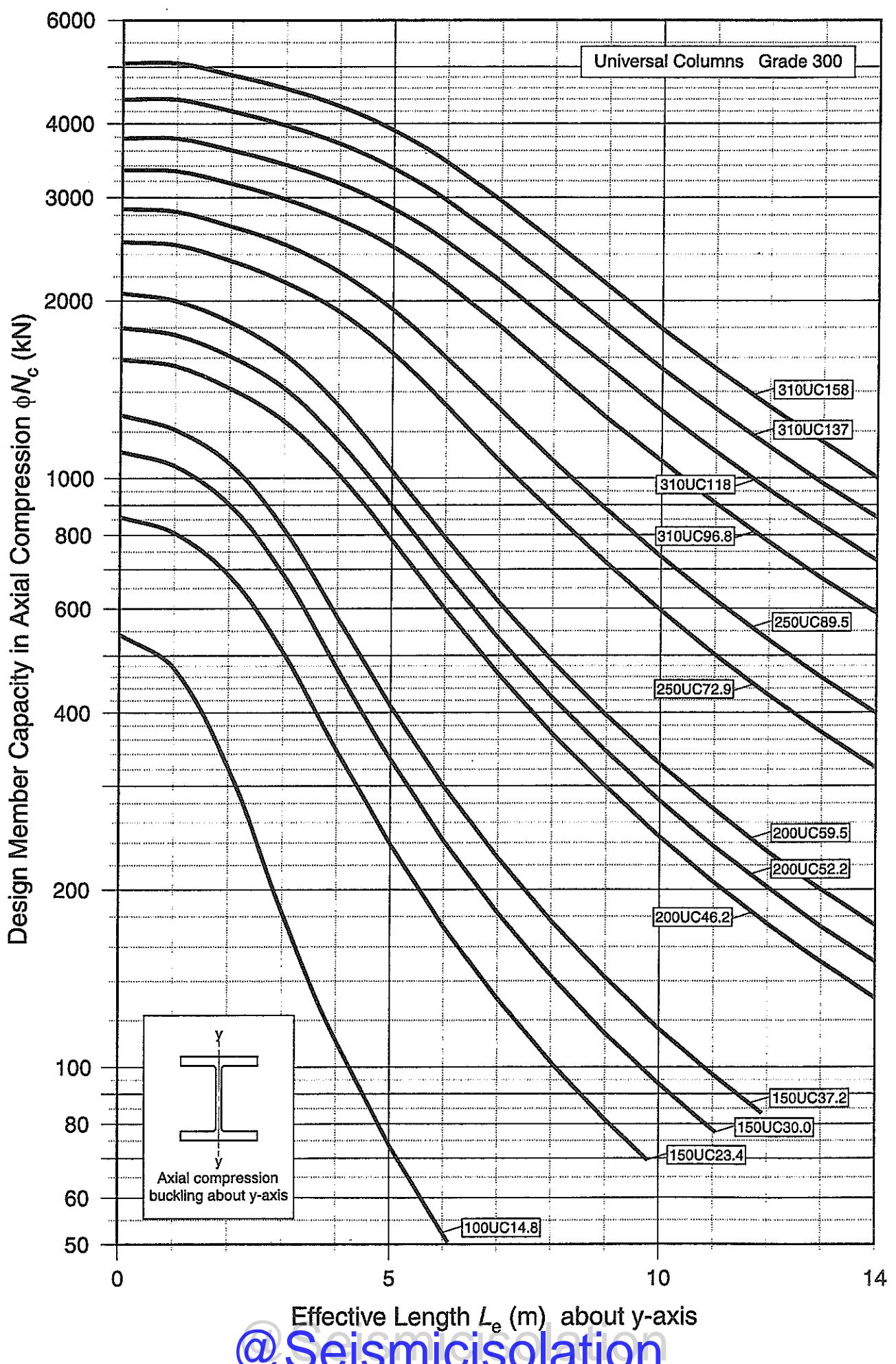
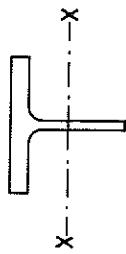


TABLE 6-7(A)

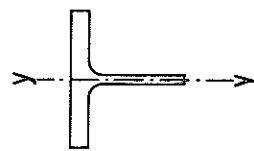
**TEES CUT FROM UNIVERSAL BEAMS  
GRADE 300**

**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION  
buckling about x-axis**



Designation	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)												
		1	2	3	4	5	6	7	8	9	10	12	14	16
305BT62.5	1690	1690	1610	1490	1360	1230	1110	992	883	784	697	553	444	362
56.5	1490	1490	1420	1320	1210	1110	1010	990	887	792	705	627	499	402
50.5	1380	1380	1310	1210	1100	989	876	768	670	583	508	444	374	328
265BT46.3	1310	1310	1220	1100	957	861	765	674	590	516	450	394	343	271
41.0	1130	1130	1050	957	861	765	674	590	516	450	394	306	242	195
230BT41.1	1230	1210	1090	962	833	711	602	508	431	367	315	237	184	146
37.3	1090	1080	968	855	742	636	539	456	387	330	284	214	166	132
33.6	951	945	852	755	657	564	481	408	347	297	255	193	150	119
205BT29.9	870	851	751	647	545	453	375	311	259	218	186	138	106	83.6
26.9	810	792	699	602	507	421	348	289	241	203	172	128	98.3	77.6
190BT28.4	871	833	713	589	475	379	304	245	201	167	140	103	78.0	61.1
25.4	756	725	622	516	418	335	269	218	178	148	125	91.3	69.5	54.5
22.4	688	659	565	468	379	304	243	197	162	134	113	82.7	62.9	49.3
155BT23.1	721	667	543	421	320	243	188	148	119	97.8	81.4	58.7	44.2	34.4
20.2	652	602	488	378	286	217	167	132	106	86.8	72.2	52.1	39.2	30.5
16.0	487	454	373	293	225	173	134	106	85.8	70.4	58.7	42.4	32.0	25.0
125BT18.7	635	559	419	298	210	153	114	88.2	69.9	56.6	46.8	33.3	24.9	19.3
15.7	523	464	353	255	182	133	100	77.4	61.5	49.9	41.2	29.4	22.0	17.1
12.9	405	361	275	199	143	104	78.6	60.9	48.3	39.2	32.4	23.2	17.3	13.5
100BT14.9*	542	443	294	188	124	86.5	63.3	48.1	37.7	30.3	24.8	17.6	13.1	10.1
12.7*	446	367	248	160	106	74.4	54.5	41.5	32.5	26.2	21.5	15.2	11.3	8.74
11.2*	380	313	212	137	91.2	63.9	46.8	35.6	28.0	22.5	18.5	13.1	9.73	7.52
9.1	297	247	169	110	73.9	51.9	38.1	29.1	22.8	18.4	15.1	10.7	7.96	6.15
90BT11.1	406	337	217	127	79.3	53.6	38.4	28.8	22.4	17.9	14.6	10.3	7.62	5.87
9.1	319	248	154	-	93.1	59.9	41.2	29.8	22.5	17.6	14.1	11.5	8.14	6.04
8.1	274	214	133	-	81.2	52.4	36.1	26.2	19.8	15.4	12.4	10.1	7.15	5.31
75BT 9.0	329	261	151	83.4	51.1	34.1	24.3	18.2	14.1	11.3	9.18	6.44	4.77	3.67
7.0	266	202	116	64.2	39.3	26.3	18.7	14.0	10.8	8.65	7.06	4.95	3.66	2.82

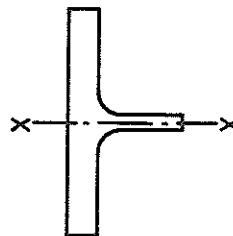
Notes: (1) \* indicates buckling about y-axis for the axis shown in the diagram.  
(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 6-7(B)**  
**TEES CUT FROM UNIVERSAL BEAMS**  
**GRADE 300**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about y-axis**

Designation	$\phi N_c$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN) Effective Length ( $L_e$ ) in metres													
		1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	6.0	7.0	8.0	9.0	10.0
305BT62.5	1690	1620	1510	1390	1280	1160	1050	941	844	755	607	492	404	336	283
56.5	1490	1430	1330	1230	1120	1020	920	826	740	662	531	430	353	293	247
50.5	1380	1310	1220	1120	1020	919	824	737	656	585	466	376	307	255	214
265BT46.3	1310	1240	1140	1030	931	830	736	650	574	507	398	318	258	213	178
41.0	1130	1060	977	887	797	711	629	555	489	432	339	270	219	180	151
230BT41.1	1230	1140	1040	930	825	726	635	554	483	423	328	259	209	171	142
37.3	1090	1010	918	824	732	644	564	492	430	376	292	231	186	152	127
33.6	951	884	804	722	642	565	494	431	373	324	282	217	171	133	111
205BT29.9	870	801	724	646	568	496	431	383	330	285	247	189	148	118	96.5
26.9	810	739	664	588	513	445	383	330	285	247	203	159	127	104	80.1
190BT28.4	871	795	714	632	552	478	412	355	306	266	203	177	138	111	90.3
25.4	756	690	620	549	480	415	358	308	266	231	199	151	118	94.3	76.8
22.4	688	623	557	489	425	365	313	268	230	199	151	118	94.3	76.8	63.7
155BT23.1	721	657	590	521	455	393	338	291	251	218	166	130	104	84.9	70.4
20.2	652	591	528	464	402	346	296	253	218	188	143	112	89.1	72.6	60.2
16.0	487	429	374	321	271	227	191	160	136	116	87.1	67.2	53.2	43.1	35.6
125BT18.7	636	557	486	416	350	293	246	207	175	150	112	86.3	68.3	55.3	45.6
15.7	523	456	396	337	283	236	197	165	140	119	88.9	68.5	54.2	43.8	36.1
12.9	405	338	284	233	189	153	125	103	85.7	72.3	53.2	40.5	31.8	25.6	21.1
100BT14.9 *	542	461	393	327	269	220	181	151	126	107	79.0	60.5	47.6	38.4	31.6
12.7 *	446	377	320	266	217	178	146	121	101	85.5	63.1	48.2	38.0	30.6	25.2
11.2 *	380	324	277	231	190	156	129	107	89.6	75.9	56.2	43.0	33.9	27.4	22.5
9.1	297	226	176	135	103	79.8	63.1	50.8	41.7	34.7	25.1	18.9	14.7	11.8	9.64
90BT11.1	405	317	244	177	129	96.6	74.5	58.9	47.6	39.3	28.0	20.9	16.2	12.9	10.5
9.1	319	229	172	127	94.9	72.4	56.6	45.2	36.8	30.6	21.9	16.5	12.8	10.2	8.35
8.1	274	198	149	119	82.5	63.0	49.3	39.4	32.2	26.7	19.2	14.4	11.2	8.94	7.30
75BT 9.0	329	233	162	110	77.0	56.4	42.9	33.7	27.1	22.2	15.7	11.7	9.04	7.19	5.86
7.0	256	178	122	81.8	57.2	41.8	31.8	24.9	20.0	16.4	11.6	8.63	6.67	5.31	4.32

Notes: (1) \* Indicates buckling about x-axis for the axis shown in the diagram.  
(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

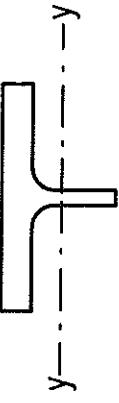


**TABLE 6-8(A)**  
**TEES CUT FROM UNIVERSAL COLUMNS**  
**GRADE 300**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about x-axis**

Designation	$\phi N_s$ (kN) ( $L_e = 0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)											
		1	2	3	4	5	6	7	8	9	10	11	12
155CT79.0	2530	2360	2190	1990	1770	1550	1320	1130	962	825	711	618	541
68.5	2200	2050	1890	1720	1530	1330	1140	967	824	705	608	528	477
59.0	1890	1760	1620	1470	1310	1130	968	822	699	598	516	447	407
48.4	1670	1660	1540	1420	1280	1120	959	811	684	579	493	423	345
125CT44.8	1430	1410	1300	1170	1020	867	718	592	489	409	345	294	253
36.5	1260	1230	1130	1010	872	729	597	488	401	333	280	239	220
100CT29.8	1030	987	874	743	597	465	362	286	230	188	157	132	113
26.1	897	863	764	648	520	405	315	249	200	164	136	115	97.4
23.1	795	763	674	570	456	354	275	217	174	142	118	99.7	84.5
75CT18.6	637	589	488	368	263	189	141	108	85.4	69.0	56.8	47.6	34.7
15.0	554	509	416	307	216	155	114	87.6	69.0	55.7	45.8	38.3	30.1
11.7	428	390	314	227	157	111	82.2	62.7	49.3	39.7	32.7	27.3	27.9
50CT 7.4	270	225	144	84.1	52.6	35.5	25.4	19.1	14.8	11.9	9.69	8.06	6.81
													5.83
													5.04

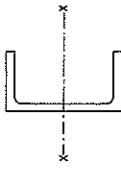
Note: Grade 300 refers to BHP Grade 300PLU™. See Note (1) on page 2-2.

**TABLE 6-8(B)**  
**TEES CUT FROM UNIVERSAL COLUMNS**  
**GRADE 300**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about y-axis**



Designation	$\phi N_c$ (kN) $(L_e = 0)$	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)													
		0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	5.5	6.0	6.5	7.0
155CT79.0	2530	2530	2360	2170	1970	1750	1510	1290	1100	932	797	686	596	521	459
68.5	2200	2190	2040	1880	1700	1500	1300	1100	934	793	677	582	505	441	388
59.0	1890	1880	1750	1610	1450	1280	1100	930	786	666	568	488	423	369	325
48.4	1670	1660	1530	1400	1250	1090	922	774	648	546	484	397	343	299	263
125CT744.8	1430	1400	1280	1140	974	805	654	532	435	361	303	257	221	192	168
36.5	1260	1220	1110	972	819	666	534	429	350	289	241	205	175	152	133
100CT29.8	1030	983	865	726	574	442	342	269	216	176	146	123	105	90.6	78.9
26.1	897	857	751	626	491	376	290	227	182	148	123	104	88.3	76.2	66.3
23.1	795	759	665	554	435	332	256	201	161	131	109	91.5	78.0	67.3	58.6
75CT18.6	637	591	492	374	269	195	146	112	88.3	71.4	58.8	49.3	41.8	36.0	31.2
15.0	554	509	417	308	217	155	115	88.1	69.4	56.0	46.1	38.6	32.7	28.1	24.4
11.7	428	396	328	247	176	127	94.6	72.6	57.3	46.3	38.1	31.9	27.1	23.3	20.2
50CT 7.4	270	218	131	73.3	45.1	30.3	21.6	16.2	12.6	10.0	8.18	6.80	5.74	4.91	4.25

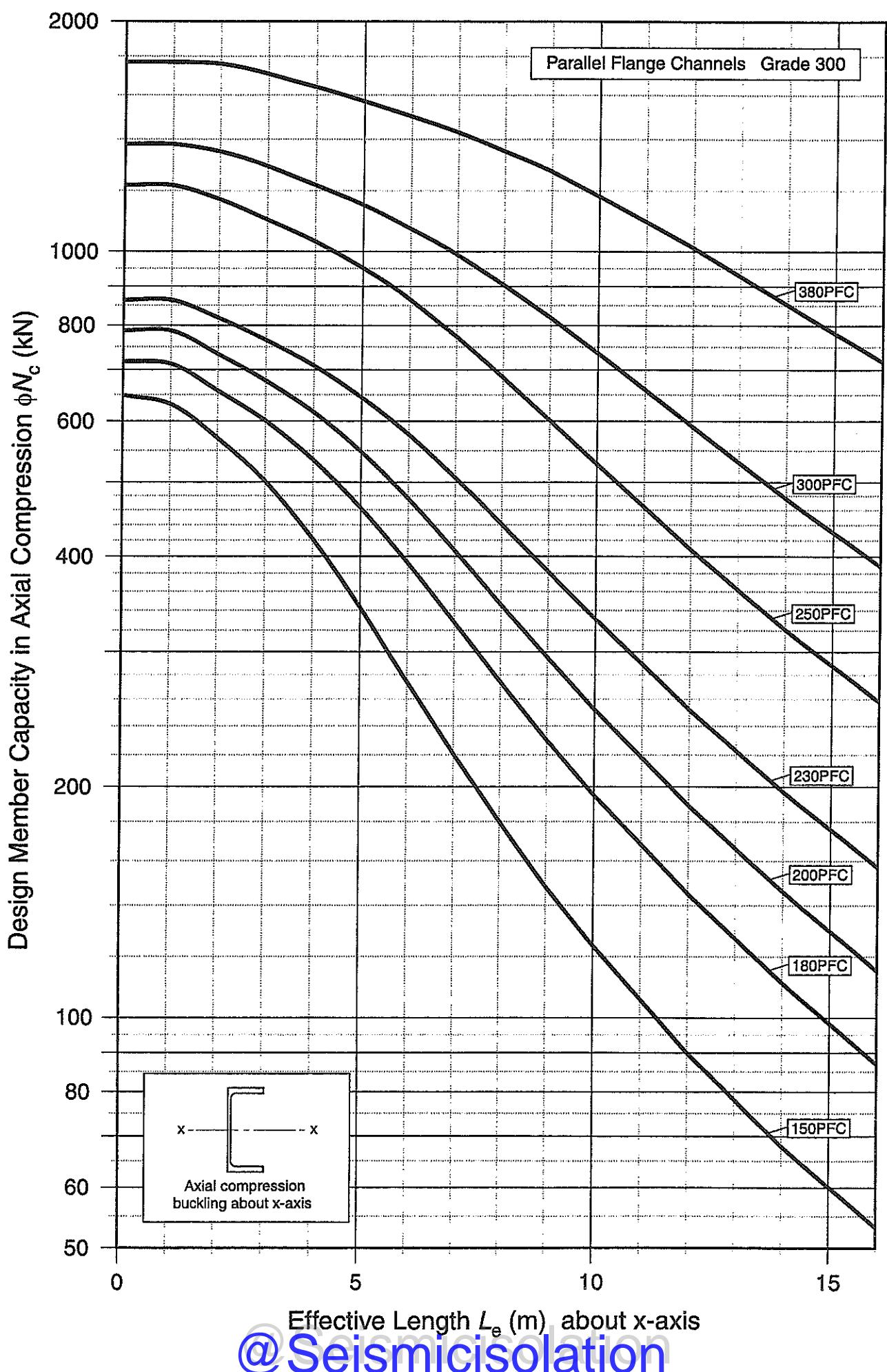
Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

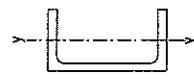


**TABLE 6-9(A)**  
**PARALLEL FLANGE CHANNELS**  
**GRADE 300**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about x-axis**

Designation	Mass per metre kg/m	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)											
			1	2	3	4	5	6	7	8	9	10	12	14
380 PFC	55.2	1770	1760	1700	1640	1570	1500	1430	1350	1270	1180	1010	851	717
300 PFC	40.1	1380	1350	1280	1220	1150	1070	990	904	819	736	591	476	388
250 PFC	35.5	1220	1170	1100	1030	961	865	774	685	602	528	408	321	258
230 PFC	25.1	864	819	766	709	645	577	507	441	382	331	252	197	157
200 PFC	22.9	788	788	734	678	617	548	476	407	346	295	252	189	146
180 PFC	20.9	718	713	658	601	535	463	392	328	274	230	195	145	111
150 PFC	17.7	649	632	571	502	422	343	274	221	180	148	124	90.0	68.0
													53.2	

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.





**TABLE 6-9(B)**  
**PARALLEL FLANGE CHANNELS**  
**GRADE 300**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
buckling about y-axis

Designation	Mass per metre	$\phi N_c$ (kN) ( $L_a=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN) Effective Length ( $L_a$ ) in metres													
			0.25	0.5	0.75	1.0	1.25	1.5	1.75	2.0	2.25	2.5	3.0	3.5		
380 PFC	55.2	1770	1770	1740	1660	1580	1500	1410	1310	1210	1100	1000	815	662	543	378
300 PFC	40.1	1380	1380	1340	1270	1200	1130	1040	955	864	775	691	548	438	355	243
250 PFC	35.5	1220	1220	1190	1130	1060	999	927	851	771	692	618	491	393	318	219
230 PFC	25.1	864	864	822	770	715	654	587	519	454	395	343	263	205	164	110
200 PFC	22.9	788	788	750	704	655	600	541	480	421	367	320	245	192	153	103
180 PFC	20.9	718	718	684	642	597	547	493	437	384	334	292	224	175	140	94.4
150 PFC	17.7	649	649	616	577	534	488	437	385	336	291	253	193	151	120	80.9

Note: Grade 300 refers to BHP Grade 300PILUS™. See Note (1) on page 2-2.

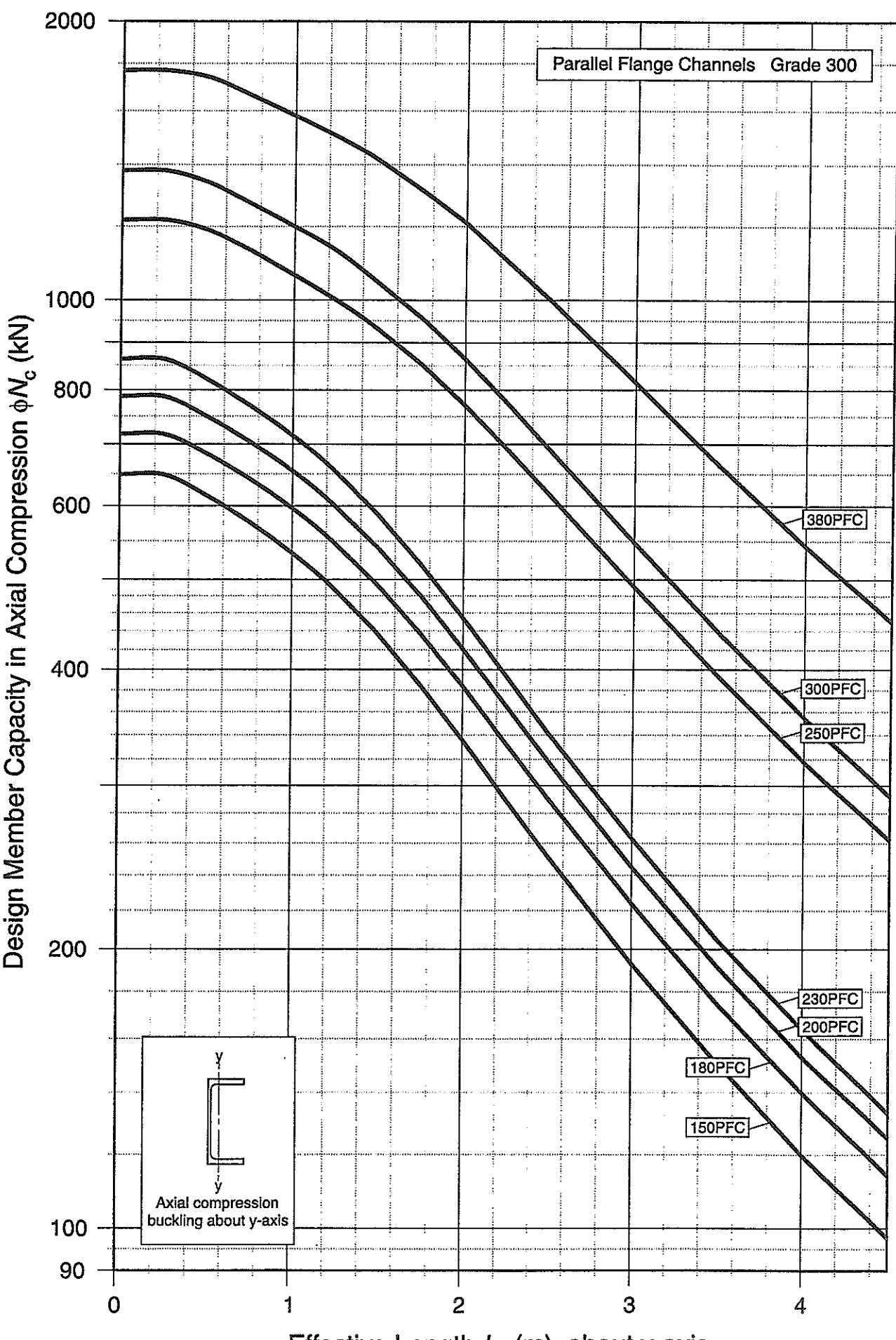
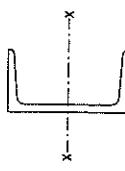


TABLE 6-10(A)

**TAPER FLANGE CHANNELS  
GRADE 250**

**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION  
buckling about x-axis**

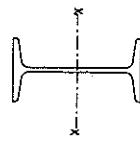


Designation	Mass per metre	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression $\phi N_c$ (kN)									
			1	2	3	4	5	6	7	8	9	10
125 TFC	13.4	400	386	344	295	240	189	148	117	94.6	77.5	64.6
100 TFC	9.34	279	262	223	176	131	96.8	73.0	56.5	44.8	36.4	30.0
75 TFC	6.65	198	177	135	90.8	60.4	42.1	30.7	23.3	18.2	14.6	12.0

TABLE 6-11(A)

**TAPER FLANGE BEAMS  
GRADE 250**

**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION  
buckling about x-axis**



Designation	Mass per metre	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression $\phi N_c$ (kN)									
			1	2	3	4	5	6	7	8	9	10
125 TFB	13.1	392	383	354	317	266	212	164	129	103	83.3	68.8
100 TFB	7.20	214	206	183	151	113	81.9	60.6	46.2	36.3	29.2	23.9

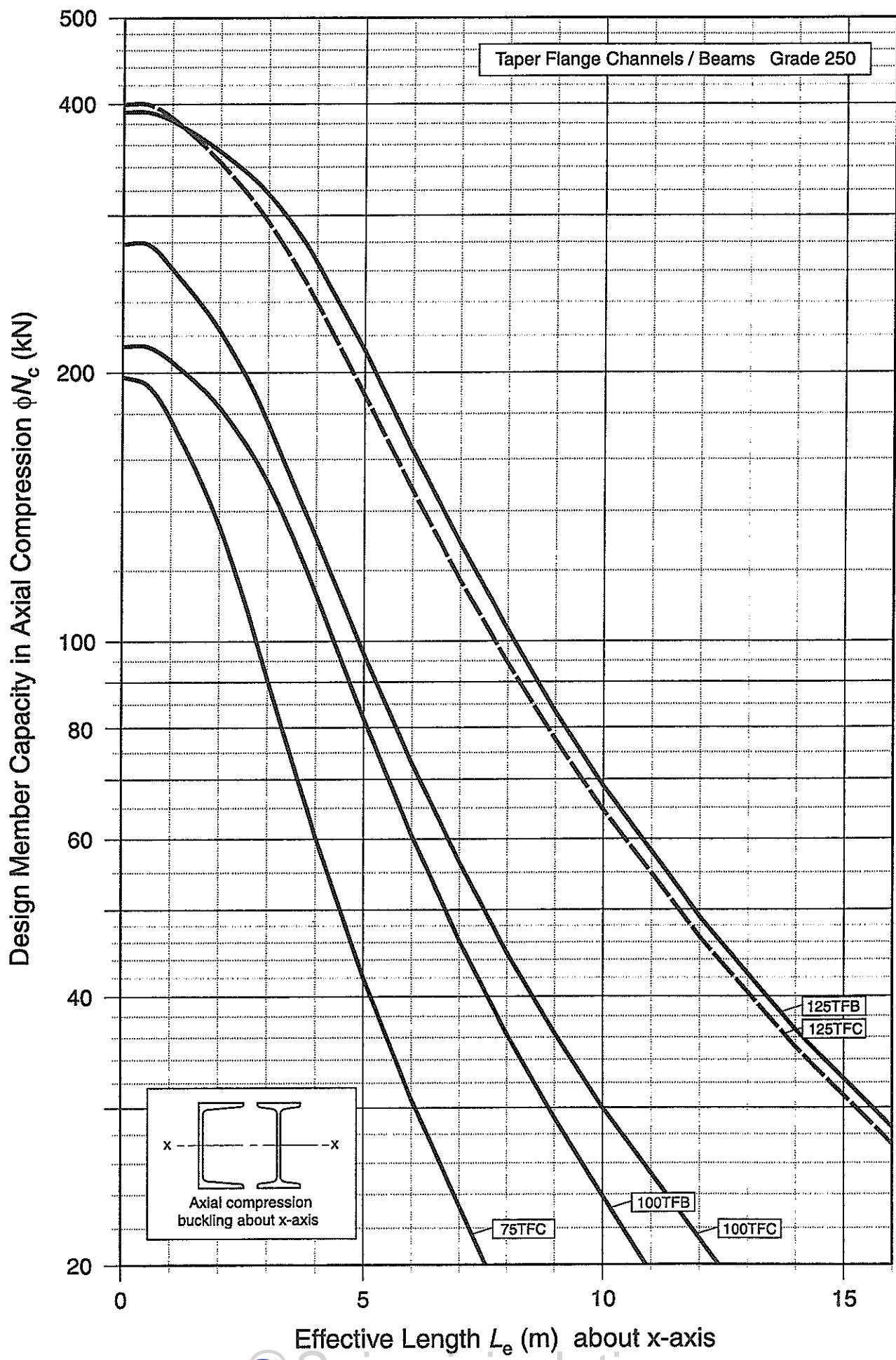




TABLE 6-10(B)

**TAPER FLANGE CHANNELS  
GRADE 250**

**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**

buckling about y-axis

Designation	Mass per metre kg/m	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression $\phi N_c$ (kN) Effective Length ( $L_e$ ) in metres					
			1.0	1.25	1.5	1.75	2.0	2.25
125 TFC	13.4	400	374	346	315	280	244	209
100 TFC	9.34	279	274	249	222	191	159	130
75 TFC	6.65	198	190	167	140	111	85.7	66.3



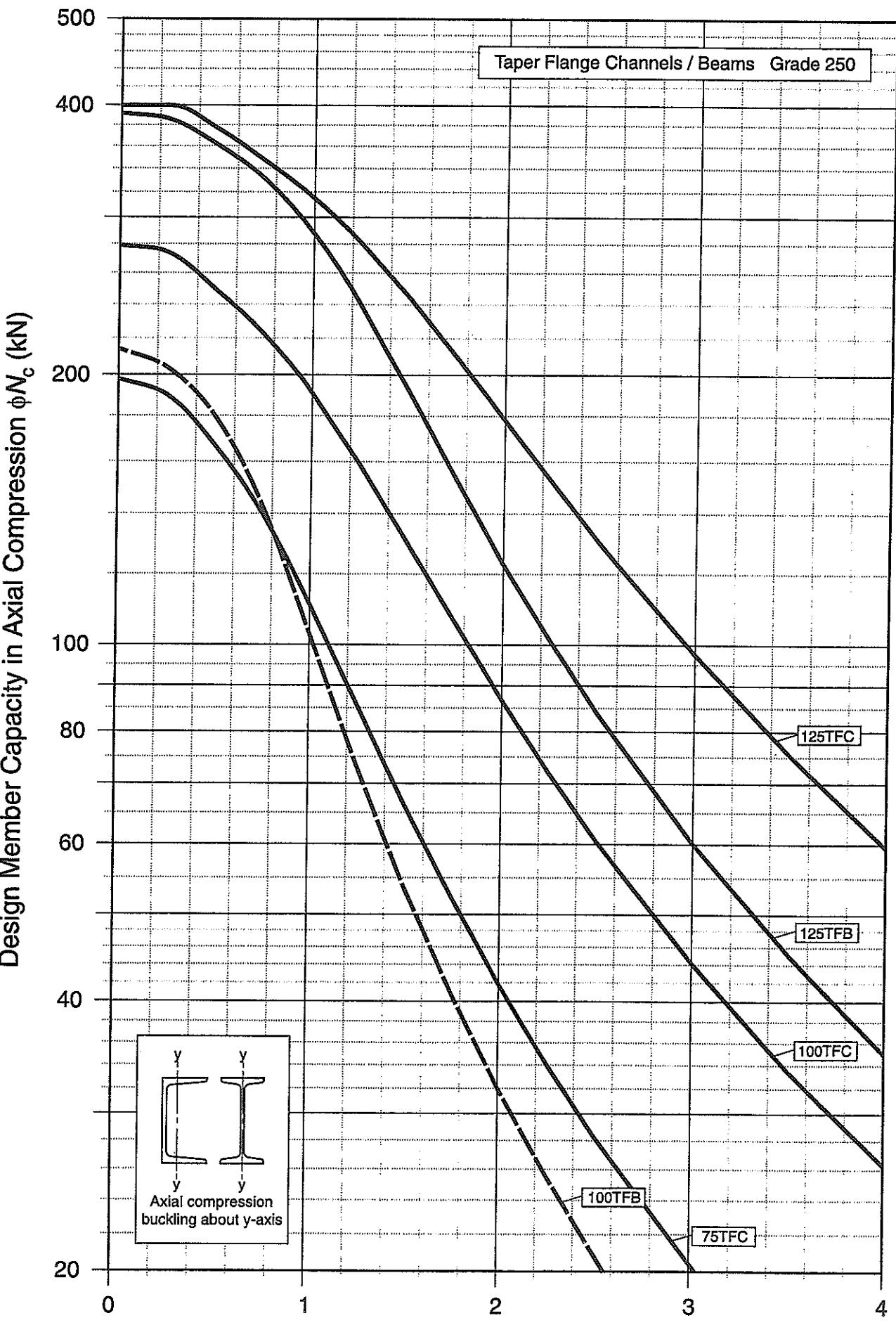
TABLE 6-11(B)

**TAPER FLANGE BEAMS  
GRADE 250**

**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**

buckling about y-axis

Designation	Mass per metre kg/m	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression $\phi N_c$ (kN) Effective Length ( $L_e$ ) in metres					
			1.0	1.25	1.5	1.75	2.0	2.25
125 TFB	13.1	392	386	361	330	288	239	192
100 TFB	7.20	214	204	180	143	103	73.4	53.8



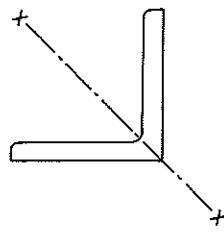
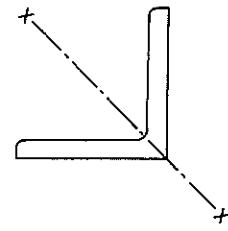


TABLE 6-12(A)-1  
**EQUAL ANGLES  
GRADE 300**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
 buckling about x-axis

Designation	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)					
		0.5	1.0	1.5	2.0	2.5	3.0
200x200x26EA	2820	2820	2800	2690	2580	2480	2360
20EA	2210	2210	2190	2110	2030	1950	1860
18EA	2000	2000	1990	1910	1840	1760	1690
16EA	1790	1790	1780	1710	1650	1580	1510
13EA	1470	1470	1460	1410	1350	1300	1240
150x150x19EA	1540	1540	1500	1420	1340	1250	1160
16EA	1300	1300	1260	1200	1130	1060	981
12EA	1000	1000	973	924	874	819	760
10EA	769	769	741	692	641	589	538
125x125x16EA	1070	1070	1010	949	879	802	718
12EA	826	826	785	735	682	624	560
10EA	661	661	629	590	548	501	451
8EA	516	516	485	445	404	363	323

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 6-12(A)-2**  
**EQUAL ANGLES**  
**GRADE 250**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about x-axis**

Designation	$\phi N_u$ (kN) ( $L_e$ , 0)	Design Member Capacities in Axial Compression, $\phi N_c$ (kN) Effective Length ( $L_e$ ) in metres									
		0.5	1.0	1.5	2.0	2.5	3.0	4.0	5.0	6.0	8.0
100x100x12EA	529	529	494	457	416	371	323	236	173	130	79.2
10EA	424	424	397	368	335	300	262	192	141	106	64.8
8EA	352	352	329	305	279	249	218	161	118	88.7	54.3
6EA	273	273	256	237	217	194	170	126	92.4	69.5	42.6
90x 90x10EA	380	377	349	319	286	248	211	148	106	78.7	47.5
8EA	315	313	290	265	238	207	176	124	89.1	66.1	39.9
6EA	245	244	226	207	185	162	138	97.5	70.0	51.9	31.4
75x 75x10EA	313	306	278	246	209	172	139	91.6	63.5	46.2	27.4
8EA	260	255	231	205	175	144	116	77.2	53.6	39.0	23.1
6EA	203	199	180	160	137	113	91.7	60.8	42.3	30.8	18.3
5EA	157	154	140	124	106	87.9	71.3	47.4	32.9	24.0	14.2
65x 65x10EA	269	259	230	196	159	124	97.3	62.0	42.3	30.5	17.9
8EA	224	213	181	149	119	94.5	75.3	49.5	34.4	25.1	14.9
6EA	175	169	151	130	106	83.4	65.5	41.9	28.7	20.7	12.1
5EA	136	131	117	101	82.6	65.3	51.4	33.0	22.6	16.3	9.57
55x 55x 6EA	147	139	120	97.2	73.9	55.4	42.1	26.1	17.5	12.5	7.29
5EA	114	106	86.9	68.0	52.0	39.8	30.9	19.7	13.4	9.70	5.70
50x 50x 8EA	169	158	132	102	73.7	53.7	40.1	24.5	16.3	11.6	6.72
6EA	133	124	104	80.9	59.0	43.1	32.3	19.7	13.2	9.38	5.43
5EA	104	94.5	75.0	56.6	42.0	31.4	24.0	15.0	10.2	7.31	4.27
3EA	69.0	64.5	54.6	42.6	31.3	23.0	17.2	10.5	7.05	5.02	2.91
45x 45x 6EA	118	108	88.3	64.6	45.2	32.3	23.9	14.4	9.54	6.77	3.90
5EA	92.3	84.8	69.3	51.0	35.9	25.7	19.0	11.5	7.61	5.40	3.12
3EA	61.4	56.5	46.3	34.3	24.2	17.3	12.8	7.75	5.15	3.66	2.11
40x 40x 6EA	104	93.4	72.2	49.3	33.1	23.1	16.9	10.0	6.62	4.68	2.69
5EA	81.5	73.2	56.9	39.1	26.4	17.9	12.5	9.17	5.47	3.61	2.16
3EA	54.4	49.0	38.2	26.4	17.9	12.5	9.17	5.47	3.61	2.55	1.47
30x 30x 6EA	76.2	63.0	40.0	23.1	14.4	9.72	6.97	4.06	2.65	1.86	1.06
5EA	60.0	46.5	28.6	17.3	11.1	7.62	5.52	3.25	2.13	1.50	0.861
3EA	40.4	33.7	21.9	12.8	8.04	5.44	3.90	2.28	1.49	1.05	0.597
25x 25x 6EA	62.1	47.4	25.3	13.6	8.20	5.45	3.88	2.24	1.45	1.02	0.580
5EA	49.2	37.9	20.6	11.1	6.74	4.49	3.19	1.84	1.20	0.840	0.478
3EA	33.3	25.9	14.2	7.72	4.69	3.13	2.22	1.29	0.836	0.586	0.334

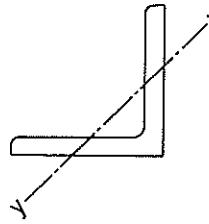


TABLE 6-12(B)-1  
**EQUAL ANGLES**  
**GRADE 300**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about y-axis**

Designation	$\phi N_e$ (kN)	Design Member Capacities in Axial Compression, $\phi N_e$ (kN)					
		( $L_e=0$ )	0.25	0.5	0.75	1.0	1.25
200x200x26EA	2820	2820	2800	2700	2600	2490	2380
20EA	2210	2210	2200	2120	2040	1950	1870
18EA	2000	2000	1990	1920	1850	1770	1690
16EA	1790	1790	1780	1720	1650	1580	1520
13EA	1470	1470	1460	1410	1360	1300	1250
150x150x19EA	1540	1540	1500	1420	1350	1260	1170
16EA	1300	1300	1260	1200	1140	1070	990
12EA	1000	1000	975	927	877	824	766
10EA	769	769	742	694	644	594	543
125x125x16EA	1070	1070	1020	954	886	811	729
12EA	826	826	786	738	686	628	566
10EA	661	661	630	591	550	505	455
8EA	516	516	486	447	406	366	326

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

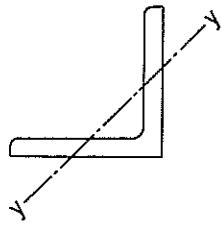


TABLE 6-12(B)-2

**EQUAL ANGLES  
GRADE 250**
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION  
buckling about y-axis**

Designation	$\phi N_s$ (kN)	Design Member Capacities in Axial Compression, $\phi N_c$ (kN) Effective Length ( $L_e$ ) in metres									
		0.25	0.5	0.75	1.0	1.25	1.5	2.0	2.5	3.0	4.0
100x100x12EA	52.9	529	495	459	420	376	329	243	178	134	82.1
10EA	42.4	424	398	369	337	302	265	196	144	109	66.5
8EA	35.2	352	330	306	280	251	221	163	120	90.6	55.6
6EA	27.3	273	256	238	218	196	172	128	94.4	71.1	43.7
90x 90x10EA	38.0	378	350	321	288	252	215	152	109	81.1	49.0
8EA	31.5	313	291	267	239	209	179	127	97.3	67.8	41.0
6EA	24.5	244	226	208	187	164	140	99.6	71.7	53.3	32.3
75x 75x10EA	31.3	307	279	248	213	176	143	94.9	66.0	48.1	28.6
8EA	26.0	255	232	207	177	147	119	79.5	55.3	40.4	24.0
6EA	20.3	199	181	161	139	115	93.7	62.6	43.6	31.8	18.9
5EA	15.7	154	141	125	108	89.7	73.2	48.9	34.1	24.9	14.8
65x 65x10EA	26.9	260	232	199	163	129	101	65.0	44.5	32.1	18.9
8EA	22.4	214	183	151	122	96.9	77.4	51.2	35.7	26.1	15.5
6EA	17.5	169	151	131	107	85.1	67.0	43.1	29.5	21.3	12.5
5EA	13.6	132	118	102	83.8	66.6	52.6	33.9	23.2	16.8	9.87
55x 55x 6EA	14.7	139	121	98.6	75.7	57.0	43.5	27.0	18.2	13.0	7.59
5EA	11.4	107	87.7	69.0	53.1	40.8	31.7	20.3	13.9	10.0	5.90
50x 50x 8EA	16.9	158	134	105	76.9	56.4	42.4	25.9	17.3	12.3	7.15
6EA	13.3	124	95.8	82.5	60.8	44.7	33.6	20.5	13.7	9.79	5.68
5EA	10.4	94.8	75.8	57.7	43.0	32.3	24.8	15.6	10.6	7.59	4.44
3EA	6.9.0	64.8	55.1	43.5	32.3	23.8	18.0	11.0	7.38	5.27	3.06
45x 45x 6EA	11.8	109	89.4	66.3	46.8	33.6	24.9	15.0	9.99	7.10	4.10
5EA	9.2.3	85.0	69.9	52.1	36.8	26.5	19.6	11.9	7.88	5.60	3.23
3EA	6.1.4	56.7	46.8	35.0	24.9	17.9	13.3	8.05	5.35	3.80	2.20
40x 40x 6EA	10.4	93.9	73.6	51.1	34.6	24.3	17.8	10.6	7.00	4.96	2.85
5EA	81.5	73.5	57.7	40.2	27.2	19.1	14.0	8.37	5.53	3.91	2.25
3EA	54.4	49.2	38.8	27.1	18.5	13.0	9.53	5.70	3.76	2.66	1.33
30x 30x 6EA	76.2	63.9	42.1	24.9	15.6	10.6	7.61	4.44	2.90	2.04	1.17
5EA	60.0	47.1	29.5	18.1	11.7	8.04	5.83	3.45	2.26	1.60	0.915
3EA	40.4	34.0	22.5	13.3	8.40	5.69	4.09	2.39	1.56	1.10	0.627
25x 25x 6EA	62.1	48.8	27.6	15.1	9.24	6.17	4.39	2.54	1.66	1.16	0.661
5EA	49.2	38.6	21.7	11.9	7.23	4.82	3.44	1.99	1.29	0.907	0.517
3EA	33.3	26.2	14.8	8.07	4.92	3.29	2.34	1.36	0.881	0.618	0.352

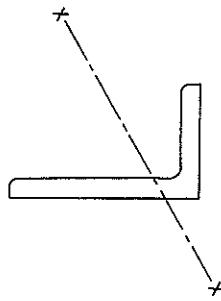


TABLE 6-13(A)

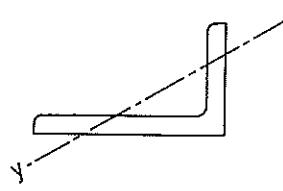
**UNEQUAL ANGLES  
GRADE 300 & 250**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about x-axis**

Designation	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)					
		0.5	1.0	1.5	2.0	2.5	3.0
150x100x12UA 10UA	826	826	790	744	695	641	582
150x100x12UA 644	644	644	609	561	512	462	414
150x 90x16UA 12UA	1020	1020	976	917	854	784	708
150x 90x16UA 10UA	791	791	755	710	662	609	552
150x 90x16UA 8UA	617	617	582	535	487	439	392
125x 75x12UA 10UA	529	529	499	466	430	390	347
125x 75x12UA 8UA	424	424	401	375	346	315	280
125x 75x12UA 6UA	352	352	333	311	288	261	233
100x 75x10UA 8UA	369	369	339	310	278	242	205
100x 75x10UA 6UA	306	306	304	282	258	231	201
75x 50x 8UA 6UA	215	206	176	145	116	92.7	74.1
75x 50x 8UA 5UA	169	163	146	126	103	81.9	64.5
65x 50x 8UA 6UA	197	184	153	122	94.6	73.2	57.3
65x 50x 8UA 5UA	154	147	129	107	84.1	64.3	49.5
	120	113	94.0	75.3	58.8	45.8	35.9

Notes: (1) For 150x90 angles and above: Grade 300.

(2) For 125x75 angles and below: Grade 250.

(3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 6-13(B)**  
**UNEQUAL ANGLES**  
**GRADE 300 & 250**  
**DESIGN MEMBER CAPACITIES IN AXIAL COMPRESSION**  
**buckling about y-axis**

Designation	$\phi N_s$ (kN) ( $L_e=0$ )	Design Member Capacities in Axial Compression, $\phi N_c$ (kN)					
		0.25	0.5	0.75	1.0	1.25	1.5
150x100x12UA 10UA	826	826	773	718	656	588	515
10UA	644	644	592	534	476	418	364
150x 90x16UA 12UA	1020	1020	942	862	774	673	573
10UA	791	787	729	688	600	524	447
10UA 8UA	617	614	555	493	431	371	317
453	453	413	371	328	286	247	183
125x 75x12UA 10UA	529	522	480	435	383	327	272
8UA	424	419	386	350	309	264	220
6UA	352	348	320	290	257	220	184
238	237	213	189	164	141	120	86.7
100x 75x10UA 8UA	369	364	334	302	266	226	188
306	302	278	251	221	188	157	108
238	235	216	196	173	148	123	84.6
75x 50x 8UA 6UA	215	201	165	129	99.2	76.0	59.1
169	160	139	114	87.6	66.1	50.5	31.4
5UA	131	125	108	89.1	68.8	52.1	39.8
65x 50x 8UA 6UA	197	182	149	117	88.9	67.9	52.7
154	146	126	103	78.5	59.0	44.9	33.5
5UA	120	111	91.5	71.8	55.1	42.2	32.8

Notes: (1) For 150x90 angles and above; Grade 300.

(2) For 125x75 angles and below; Grade 250.

(3) Grade 300 refers to BHP Grade 300 PLUS™. See Note (1) on page 2-2.

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## PART 7

## MEMBERS SUBJECT TO AXIAL TENSION

	PAGE
7.1 General.....	7-2
7.2 Design Section Capacity in Axial Tension.....	7-2
7.3 Example .....	7-2

## TABLES

### TABLES 7-1 to 7-24

Design Section Capacities in Axial Tension ( $\phi N_t$ ) .....	7-4
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**PART 7****MEMBERS SUBJECT TO AXIAL TENSION****7.1 General**

Tables 7-1 to 7-24 give values of design section capacity in axial tension. Section 7 of AS 4100 is used to determine these values. The tables list the design section capacity in tension for a variety of standardised bolted and welded connections.

**Note:** This chapter considers only connections with standardised detailing parameters summarised in Section 10 of this publication.

**7.2 Design Section Capacity in Axial Tension**

The design section capacity in axial tension ( $\phi N_t$ ) has been determined from Clause 7.2 of AS 4100 and taken as the *lesser* of:

$$\begin{aligned}\phi N_t &= \phi A_g f_y && \text{(Yielding of the gross section)} \\ \phi N_t &= \phi (0.85) k_t A_n f_u && \text{(Fracture of the net section at a connection)}\end{aligned}$$

where  $\phi = 0.9$  (Table 3.4 of AS 4100)

$f_y$  = yield stress used in design (*For sections where the flange and web yield stresses ( $f_{yf}$  &  $f_{yw}$ ) differ, the lower of the two is applied to the entire cross-section.*)

$f_u$  = ultimate tensile strength used in design

$A_g$  = gross area of the cross-section

$A_n$  = net area of the cross-section (accounting for any fastener holes in the section)

$k_t$  = a correction factor to account for the distribution of forces at a connection (shown in Table 7.1)

**Note:** For staggered bolt holes (not considered in these Tables) designers should consult Clause 9.1.10 of AS 4100 to determine the deduction to the gross area due to the holes.

**7.3 Example**

- Design an appropriate Equal Angle section for a design axial tensile force,  $N^* = 1300$  kN, assuming an eccentrically bolted connection through one leg of the angle.

Solution:

Select a suitable member from Tables 7-22(1) and 7-22(2). The alternatives are:

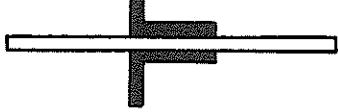
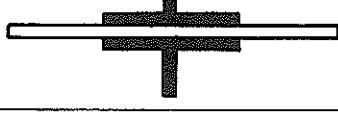
150 x 150 x 19 EA - Grade 300 (42.1 kg/m)  $\phi N_t = 1350 > N^*$

200 x 200 x 13 EA - Grade 300 (40.0 kg/m)  $\phi N_t = 1370 > N^*$

In each case there is a single line of 22 mm holes (20 mm bolts) in one leg of the angle.

Choose a 200 x 200 x 13 EA - Grade 300 section as it is more economical based on mass.

TABLE 7.1: Correction Factor ( $k_t$ )

Configuration Case	Correction Factor ( $k_t$ )
	0.75 for Unequal Angles connected by the Short Leg 0.85 Otherwise
	0.75 for Unequal Angles connected by the Short Leg 0.85 Otherwise
	0.85
	0.90
	0.75 <sup>†</sup>
	0.85*
	1.0
	1.0
	1.0
Other end connection providing uniform force distribution	1.0 <sup>#</sup>

Notes: \* Such connections for Channels and I- sections must satisfy Clause 7.3.2(b) of AS 4100.  
 # These connections must satisfy Clause 7.3.1 of AS 4100.  
 † This configuration not considered in Section 7 of AS 4100.

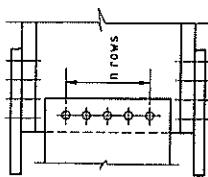


TABLE 7-1

**WELDED BEAMS  
GRADE 300**
**DESIGN SECTION CAPACITIES IN AXIAL TENSION  
with end connections to FLANGE and to WEB**

Designation	Welded No Holes	Hole Dia.	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)											
			Bolted - Two Holes in Each Flange, N in Web						Bolted - Four Holes in Each Flange (for $b_f \geq 400\text{mm}$ ), N in Web					
			N =											
N = 0	mm	5	6	7	8	9	10	11	12	13	14	15		
1200WB455 455*	14600 14600	26					14600 14600	14600 14600	14600 14600	14600 14600	14600 14600	14600 14600	14600 14600	14600 14600
423	13600 13600	26					13600 13600	13600 13600	13600 13600	13600 13600	13600 13600	13600 13600	13600 13600	13600 13600
423*	13600 13600	26					13600 13600	13600 13600	13600 13600	13600 13600	13600 13600	13600 13600	13600 13600	13600 13600
392	12600 12600	26					12600 12600	12600 12600	12600 12600	12600 12600	12600 12600	12600 12600	12600 12600	12600 12600
392*	12600 11000	26					12600 11000	12600 11000	12600 11000	12600 11000	12600 11000	12600 11000	12600 11000	12600 11000
342	11000 11000	26					11000 10800	11000 10800	11000 10800	11000 10800	11000 10800	11000 10800	11000 10800	11000 10800
342*	11000 10200	26					10800 10200	10800 10200	10800 10200	10800 10200	10800 10200	10800 10200	10800 10200	10800 10200
317	10200 10200	26					10200 9980	10200 9980	10200 9980	10200 9980	10200 9980	10200 9980	10200 9980	10200 9980
317*	10200 8900	26					9980 8930	9980 8930	9980 8930	9980 8930	9980 8930	9980 8930	9980 8930	9980 8930
278	8900 7900	26					7980 7980	7980 7980	7980 7980	7980 7980	7980 7980	7980 7980	7980 7980	7980 7980
249	7900	26												
1000WB322	10300 10300	26					10300 10200	10300 10200	10300 10200	10300 10200	10300 10200	10300 10200	10300 10200	10300 10200
322*	10300 9520	26					9520 9410	9520 9410	9520 9410	9520 9410	9520 9410	9520 9410	9520 9410	9520 9410
296	9520 9520	26					9270 8280	9270 8280	9270 8280	9270 8280	9270 8280	9270 8280	9270 8280	9270 8280
296*	9520 8280	26					7220 7220	7220 7080	7220 7080	7220 7080	7220 7080	7220 7080	7220 7080	7220 7080
258	8280 7390	26												
215	7390	26												
900WB282	9050 9050	26					9050 8910	9050 8810	9050 8700	9050 8600	9050 8500	9050 8500	9050 8500	9050 8500
282*	9050 8250	26					8250 8130	8250 8030	8250 7920	8250 7820	8250 7720	8250 7720	8250 7720	8250 7720
257	8250 7010	26					8130 7010	8130 7010	8130 7010	8130 7010	8130 7010	8130 7010	8130 7010	8130 7010
257*	8250 6030	26					5840 5840	5840 5730	5840 5730	5840 5630	5840 5630	5840 5630	5840 5630	5840 5630
218	7010 6030	26												
175	6030	26												
800WB192	6150 5380	26					6150 5380	6150 5380	6150 5380	6150 5380	6150 5380	6150 5380	6150 5380	6150 5380
168	5380	26												
146	5020 4210	26					4920 4070	4920 3990	4920 3990	4920 3990	4920 3990	4920 3990	4920 3990	4920 3990
122	4210	26												
700WB173	5540 4810	26					5540 4810	5540 4810	5540 4810	5540 4810	5540 4810	5540 4810	5540 4810	5540 4810
150	5020 4480	26					4920 4260	4920 4260	4920 4260	4920 4260	4920 4260	4920 4260	4920 4260	4920 4260
130	4480 3940	26					3830 3740	3830 3740	3830 3740	3830 3740	3830 3740	3830 3740	3830 3740	3830 3740
115	3940	26												

**N < N<sub>min</sub>**

- Notes: (1) \* Indicates four holes in each flange.  
 (2) N > N<sub>max</sub> denotes that this number of bolts usually cannot be used in the web.  
 (3) N < N<sub>min</sub> denotes that this number of bolts is not usually used in practical connections.

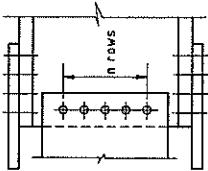
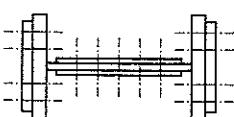


TABLE 7-2  
**WELDED BEAMS**  
**GRADE 400**  
**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
with end connections to FLANGE and to WEB



Designation	Welded No Holes	Hole Dia.	Design Section Capacity in Axial Tension, $\phi N_i$ (kN)										
			Bolted - Two Holes in Each Flange, N in Web					Bolted - Four Holes in Each Flange (for $b_f \geq 400\text{mm}$ ), N in Web					
			5	6	7	8	9	10	11	12	13	14	
1200WB455	18800 455*	26	18200	18100	17900	17800	17600	17400	17200	16100	15900	15700	
423	18800 423	26	16700	16500	16400	16200	16000	15800	15600	15400	15200	15000	14800
423*	17500 392	26	16900	16700	16600	16400	16300	16100	15900	15700	15500	15300	15100
392*	16200 342	26	15500	15400	15300	15200	15100	14900	14800	14700	14600	14500	14400
342	16200 342*	26	14400	14200	14100	14100	14100	14000	13900	13700	13600	13500	13400
342*	14100 317	26	13200	13100	12900	12800	12600	12500	12400	12300	12200	12100	12000
317	13100 278	26	12000	11900	11700	11600	11400	11200	11000	10800	10600	10400	10200
278	11500 249	26	11000	10900	10800	10700	10600	10500	10400	10300	10100	9900	9700
249	10300 1000WB322	26	9150	8990	8840	8690	8540	8380	8230	8080	7930	7760	7450
1000WB322	13500 322*	26	12600	12400	12300	12100	12000	11900	11800	11700	11600	11500	11400
322*	13500 296	26	11400	11200	11100	10900	10800	10700	10600	10500	10400	10300	10200
296	12200 296*	26	11600	11400	11300	11100	11000	10900	10800	10700	10600	10500	10400
296*	12200 258	26	10500	10400	10200	10000	9800	9600	9400	9200	9000	8800	8600
258	10600 215	26	9890	9740	9580	9430	9280	9130	8980	8830	8680	8530	8380
215	9360 900WB282	26	8060	7910	7760	7610	7460	7310	7160	7010	6860	6710	6560
900WB282	11600 282*	26	11200	11100	10900	10800	10700	10600	10500	10400	10300	10200	10100
282*	11600 257	26	9940	9830	9710	9600	9490	9380	9270	9160	9050	8940	8830
257	10500 257*	26	10100	10000	9910	9800	9690	9580	9470	9360	9250	9140	9030
257*	10600 218	26	9070	8960	8850	8730	8620	8510	8400	8290	8180	8070	7960
218	9010 175	26	8460	8340	8230	8120	8010	7900	7790	7680	7570	7460	7350
175	7630 800WB192	26	6630	6520	6400	6290	6170	6060	5950	5840	5730	5620	5510
800WB192	7910 168	26	11200	11100	10900	10800	10700	10600	10500	10400	10300	10200	10100
168	6920 146	26	9940	9830	9710	9600	9490	9380	9270	9160	9050	8940	8830
146	6360 122	26	10100	10000	9910	9800	9690	9580	9470	9360	9250	9140	9030
122	5340 700WB173	26	9070	8960	8850	8730	8620	8510	8400	8290	8180	8070	7960
700WB173	7130 150	26	6530	6440	6340	6250	6160	6060	5960	5860	5760	5660	5560
150	6190 130	26	5580	5490	5390	5300	5210	5120	5030	4940	4850	4760	4670
130	5680 115	26	4850	4760	4660	4570	4480	4390	4300	4210	4120	4030	3940
115	4990 122	26	4270	4180	4080	3990	3900	3810	3720	3630	3540	3450	3360

**N > N<sub>max</sub>**

**N < N<sub>min</sub>**

- Notes: (1) \* indicates Four Holes in Each Flange.  
 (2) N > N<sub>max</sub> denotes that this number of bolts usually cannot be used in the web.  
 (3) N < N<sub>min</sub> denotes that this number of bolts is not usually used in practical connections.



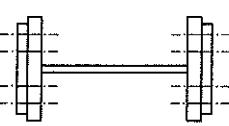


TABLE 7-3  
**WELDED BEAMS  
GRADE 300**  
**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
with end connections to FLANGE only

Designation	Design Section Capacity in Axial Tension, $\phi N_i$ (kN)		
	Welded No Holes	Bolted — N Holes/Flange	N =
	mm	2	4
1000WB322	10300	26	10300
296	9520	26	9520
258	8280	26	8280
215	7390	26	7390
900WB282	9050	26	9050
257	8250	26	8250
218	7010	26	7010
175	6030	26	5660
800WB192	6150	26	6010
168	5380	26	5240
146	5020	26	4820
122	4210	26	3900
700WB173	5540	26	5340
150	4810	26	4610
130	4480	26	4060
115	3940	26	3630

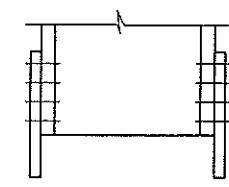


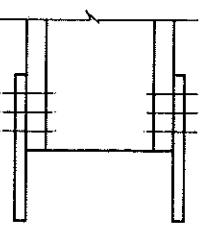
TABLE 7-4

**WELDED BEAMS  
GRADE 400**  
**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
With end connections to FLANGE only

Designation	Design Section Capacity in Axial Tension, $\phi N_i$ (kN)		
	Welded No Holes	Bolted — N Holes/Flange	N =
	mm	Hole Dia.	N =
1200WB455	18100	26	16800
423	16800	26	15700
392	15600	26	14500
342	13600	26	14500
317	12600	26	12500
278	11100	26	11700
249	9380	26	10200
	249	—	—
1000WB322	12800	26	11700
296	11800	26	10900
258	10300	26	9440
215	8540	26	7890
900WB282	11200	26	10200
257	10200	26	9300
218	8860	26	8390
175	6970	26	—
800WB192	7620	26	6710
168	6660	26	5850
146	5810	26	5160
122	4870	26	4350
700WB173	6870	26	5960
150	5980	26	5150
130	5180	26	4530
115	4560	26	4040

[BLANK]

COMBINED



**TABLE 7-5  
WELDED COLUMNS  
GRADE 300**

**DESIGN SECTION CAPACITIES IN AXIAL TENSION  
with end connections to FLANGE and to WEB**

Designation	Welded No Holes	Design Section Capacity in Axial Tension, $\phi N_1$ (kN)				
		Bolted - Two Holes in Each Flange, N in Web				
		Hole Dia.	N = 0	1	2	3
500WC440	14100	26	14100	14100	14100	14100
440*	14100	26	14100	14100	14100	14000
414	13300	26	13300	13300	13300	13300
414*	13300	26	13300	13300	13300	13300
383	12300	26	12300	12300	12300	12300
383*	12300	26	12300	12300	12300	12300
340	10900	26	10900	10900	10900	10900
340*	10900	26	10900	10900	10900	10900
290	9320	26	9320	9320	9320	9320
290*	9320	26	9320	9320	9320	9320
267	8570	26	8570	8570	8570	8570
267*	8570	26	8570	8570	8570	8570
228	7830	26	7830	7830	7830	7830
228*	7830	26	7830	7830	7830	7830
400WC361	11600	26	11600	11600	11600	11600
361*	11600	26	11600	11600	11600	11600
328	10500	26	10500	10500	10500	10500
328*	10500	26	10500	10500	10500	10500
303	9730	26	9730	9730	9730	9730
303*	9730	26	9730	9730	9730	9730
270	8660	26	8660	8660	8660	8660
270*	8660	26	8660	8660	8660	8660
212	6800	26	6800	6800	6800	6800
212*	6800	26	6800	6800	6800	6800
181	6210	26	6210	6210	6210	6210
181*	6210	26	6030	5860	5680	5510
144	4970	26	4970	4970	4960	4960
144*	4970	26	4820	4680	4550	4410
350WC280	9000	26	9000	9000	9000	9000
258	8290	26	8290	8290	8290	8290
230	7380	26	7380	7380	7380	7380
197	6330	26	6330	6330	6330	6330

Notes: (1) \* indicates four holes in each flange.  
(2) N > N<sub>max</sub> denotes that this number of bolts usually cannot be used in the web.  
(3) N < N<sub>min</sub> denotes that this number of bolts is not usually used in practical connections.

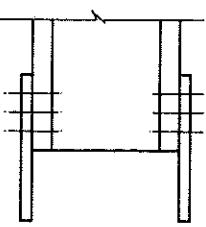


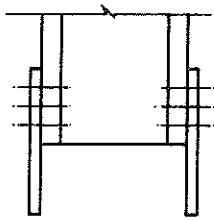
TABLE 7-6

**WELDED COLUMNS  
GRADE 300**

**DESIGN SECTION CAPACITIES IN AXIAL TENSION  
With end connections to FLANGE only**

Designation	Design Section Capacity in Axial Tension, $\phi N_1$ (kN)		
	Bolted — N Holes/Flange		N =
	Welded No Holes	Hole Dia.	
500WC440	14100	26	14100
414	13300	26	13300
383	12300	26	12300
383*	12300	26	12300
340	10900	26	10900
340*	10900	26	10900
290	9320	26	9320
290*	9320	26	9320
267	8570	26	8570
267*	8570	26	8570
228	7830	26	7830
228*	7830	26	7830
500WC440	14100	26	14100
414	13300	26	13300
383	12300	26	12300
383*	12300	26	12300
340	10900	26	10900
340*	10900	26	10900
290	9320	26	9320
290*	9320	26	9320
267	8570	26	8570
267*	8570	26	8570
228	7830	26	7830
228*	7830	26	7830
400WC361	11600	26	11600
361*	11600	26	11600
328	10500	26	10500
328*	10500	26	10500
303	9730	26	9730
303*	9730	26	9730
270	8660	26	8660
270*	8660	26	8660
212	6800	26	6800
212*	6800	26	6800
181	6210	26	6210
181*	6210	26	6030
144	4970	26	4970
144*	4970	26	4820
350WC280	9000	26	9000
258	8290	26	8290
230	7380	26	7380
197	6330	26	6330





**TABLE 7-7**  
**WELDED COLUMNS**  
**GRADE 400**

**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
with end connections to FLANGE and to WEB

Designation	Welded No Holes	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)				
		Bolted - Two Holes in Each Flange, N in Web		Bolted - Four Holes in Each Flange (for $b_f \geq 400\text{mm}$ ), N in Web		
N = 0	Hole Dia.	1	2	3	4	5
500WC440	18100	26	18100	17500	17100	16700
440 *	18100	26	16400	16000	15600	15600
414 *	17100	26	17100	16800	16300	16300
414 *	17100	26	15700	15400	15100	14800
383 *	15800	26	15800	15600	15300	15000
383 *	15800	26	14600	14300	13900	13600
340 *	14000	26	14000	13900	13700	13500
340 *	14000	26	13000	12700	12500	12200
290 *	12000	26	12000	11900	11800	11600
290 *	12000	26	11100	10900	10700	10500
267 *	11000	26	11000	11000	10800	10600
267 *	11000	26	10200	10000	9810	9620
228 *	9920	26	9500	9310	9120	8930
228 *	9920	26	8740	8550	8360	8170
400WC361	14900	26	14900	14600	14200	13800
361 *	14900	26	13500	13100	12700	12300
328	13500	26	13500	13000	12800	12500
328 *	13500	26	12000	11800	11500	11200
303 *	12500	26	12500	12300	12000	11700
303 *	12500	26	11200	10900	10600	10400
270	11100	26	11100	10900	10700	10400
270 *	11100	26	9930	9690	9450	9210
212 *	8750	26	8750	8580	8390	8200
212 *	8750	26	7810	7620	7430	7240
181	7870	26	7490	7300	7110	6920
181 *	7870	26	6730	6540	6350	6150
144 *	6290	26	5990	5840	5690	5530
144 *	6290	26	5380	5230	5080	4920
350WC280	11600	26	11300	11000	10800	9900
258	10700	26	10400	10200	9050	8810
230	9450	26	9290	7960	7770	7570
197	8130	26	—	—	—	—

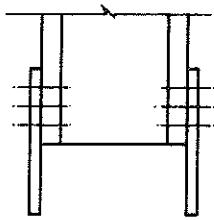
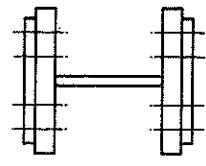
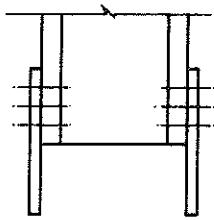
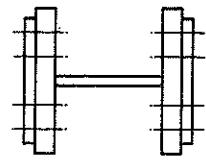
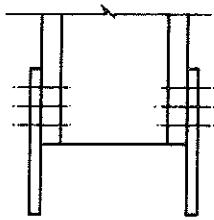
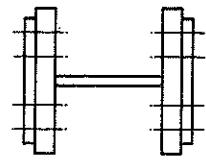
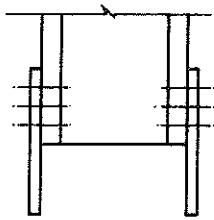
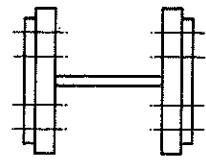
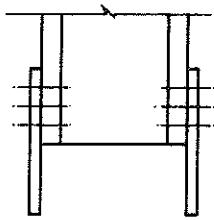
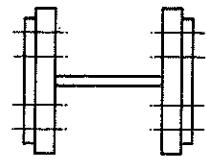
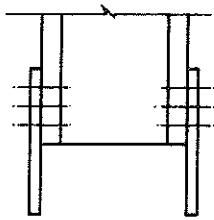
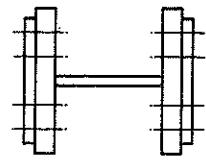
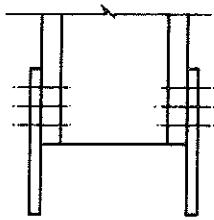
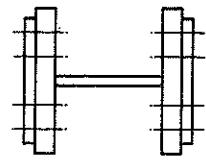
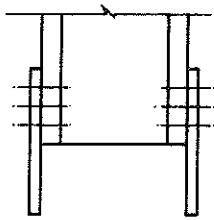
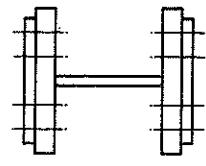
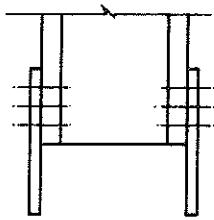
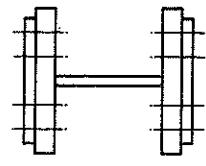
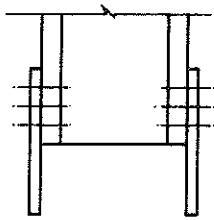
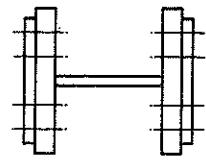
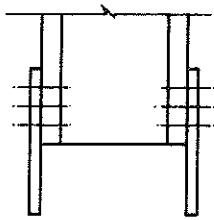
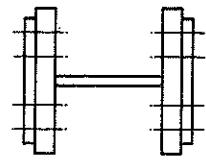
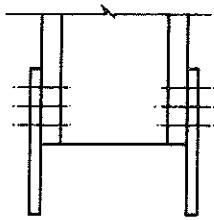
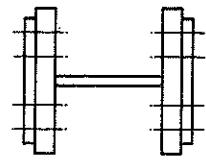
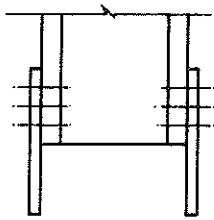
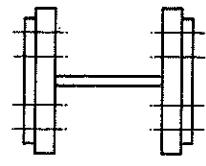
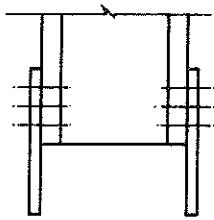
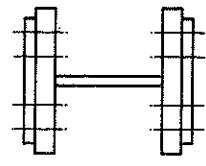
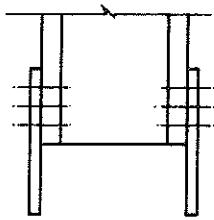
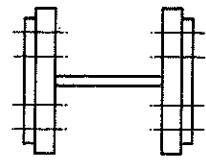
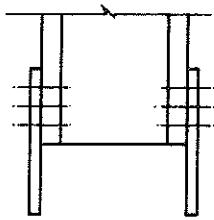
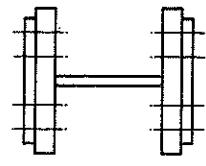
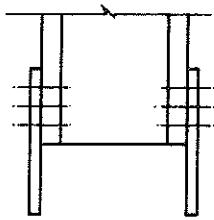
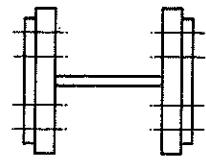
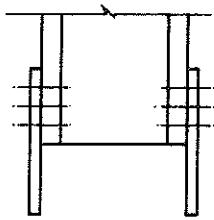
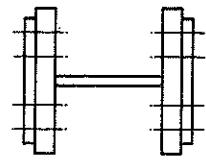
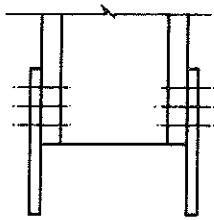
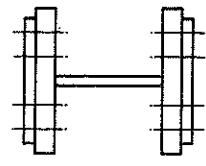
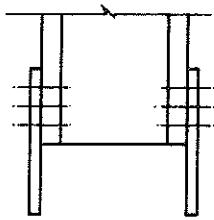
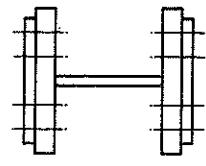
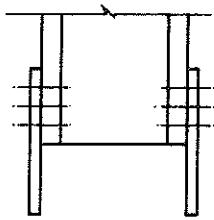
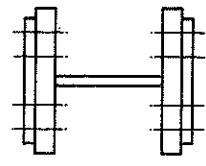
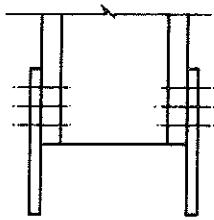
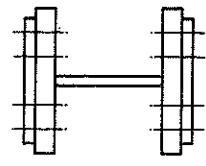
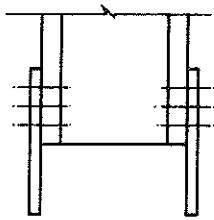
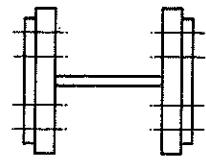
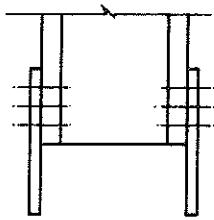
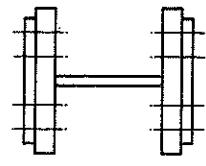
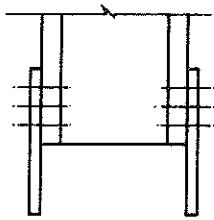
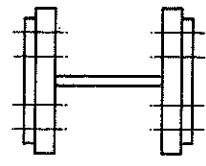
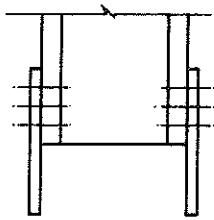
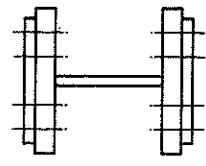
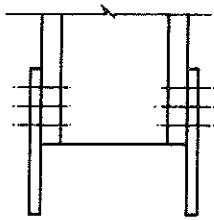
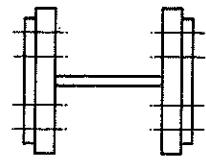
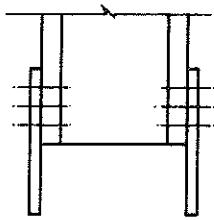
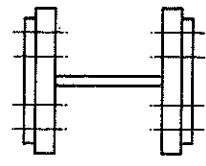
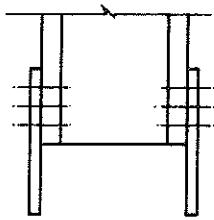
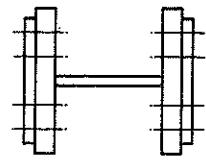
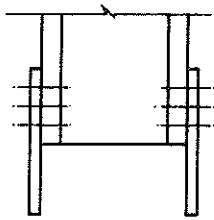
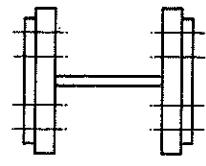
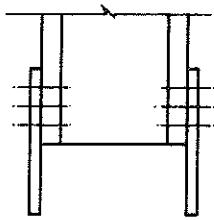
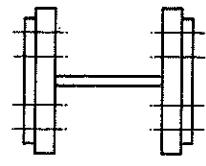
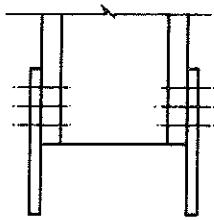
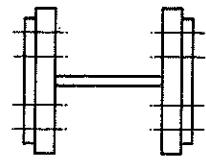
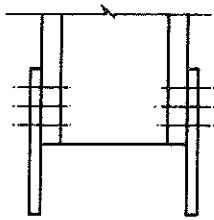
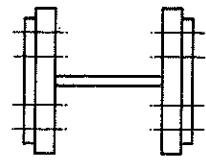
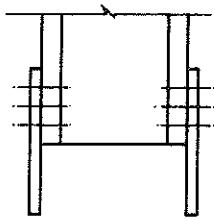
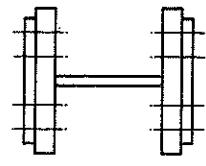
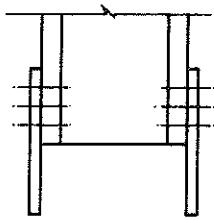
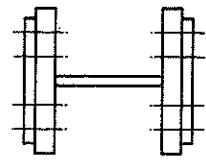
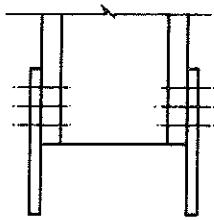
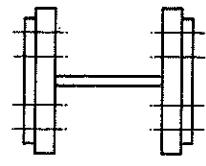
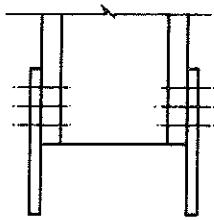
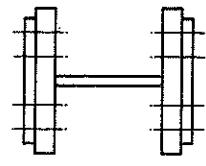
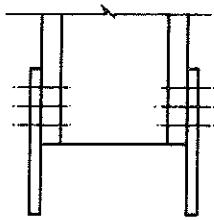
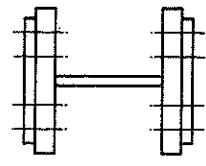
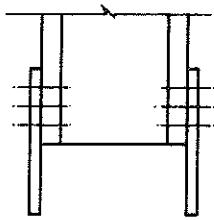
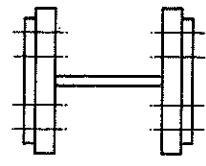
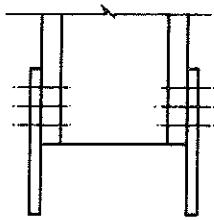
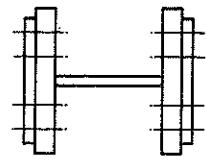
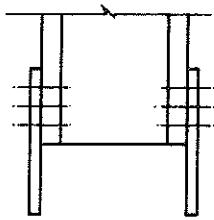
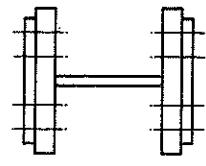
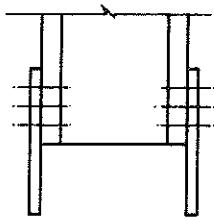
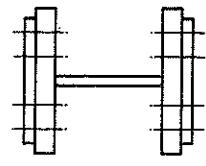
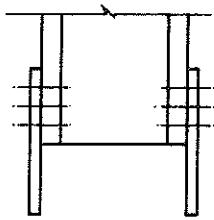
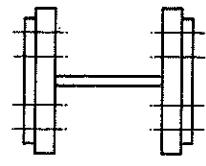
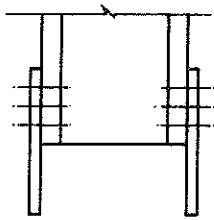
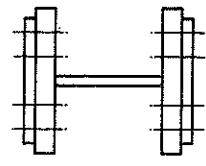
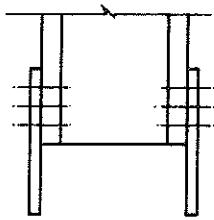
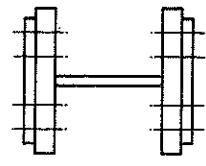
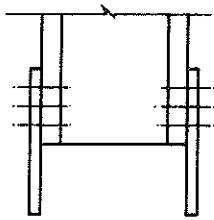
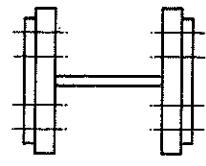
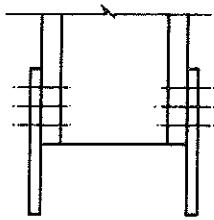
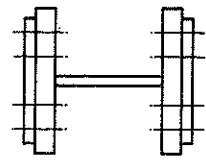
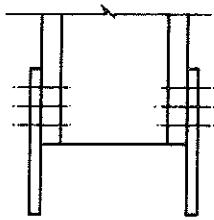
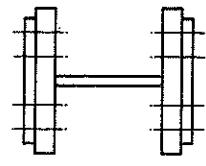
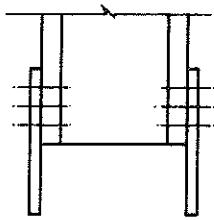
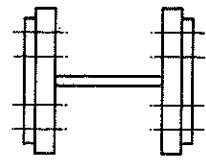
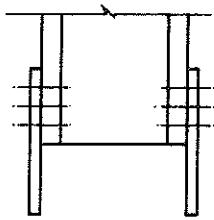
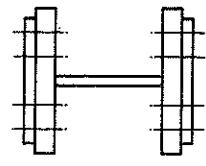
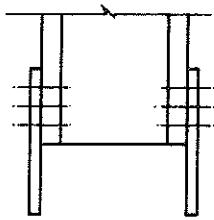
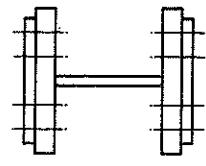
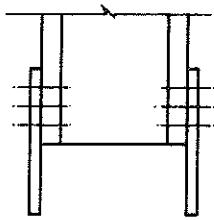
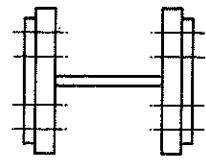
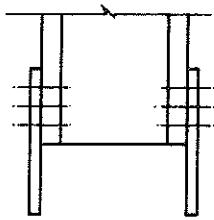
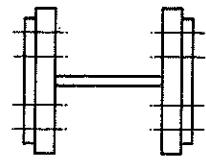
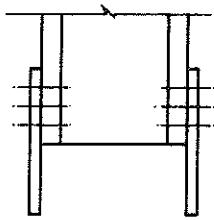
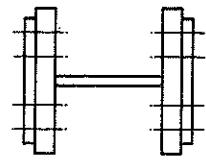
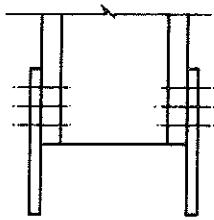
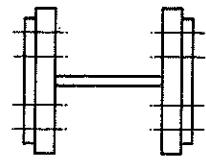
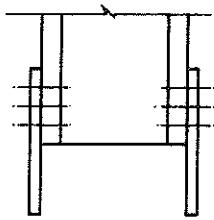
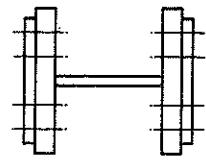
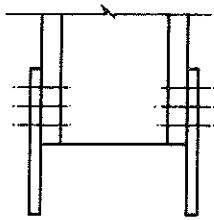
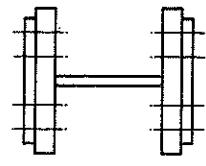
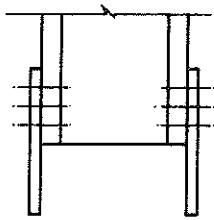
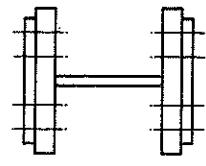
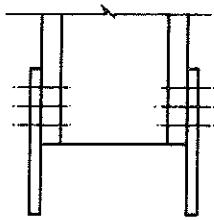
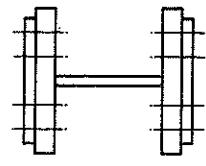
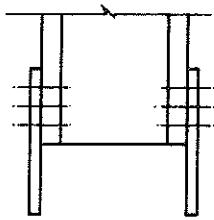
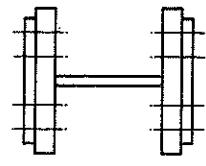
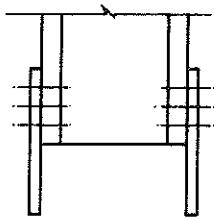
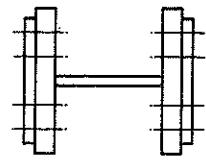
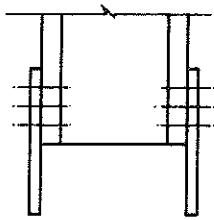
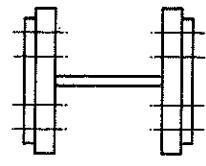
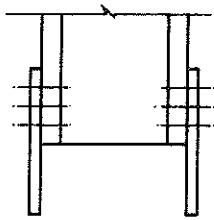
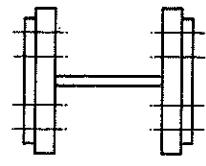
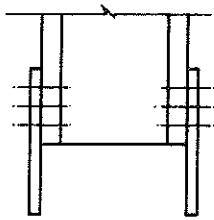
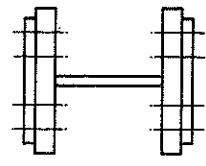
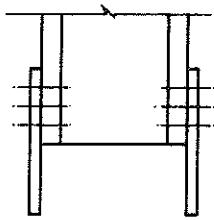
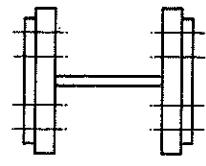
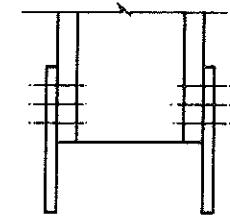
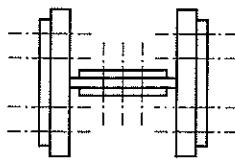
**TABLE 7-8**

**WELDED COLUMNS**  
**GRADE 400**

**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
With end connections to FLANGE only

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)		
	Boiled - N Holes/Flange	Welded - N Holes/Flange	N =
N = 0	mm	mm	mm
400WC440	17500	16500	26
414	15200	15200	26
383	14100	14100	26
340	12500	12500	26
290	11600	11600	26
267	10600	10600	26
228	9800	9800	26
228 *	8400	8400	26
500WC440	14900	14900	26
414 *	13900	13900	26
383	12900	12900	26
340 *	11400	11400	26
303	10600	10600	26
270	9800	9800	26
270 *	7750	7750	26
400WC361	14400	14400	26
414	13200	13200	26
383	12000	12000	26
340	11200	11200	26
303	10400	10400	26
270	9600	9600	26
270 *	7570	7570	26
350WC280	11100	11100	26
258	10300	10300	26
230	9140	9140	26
197	7830	7830	26

- Notes: (1) \* indicates four holes in each flange.  
(2) N > N<sub>max</sub> denotes that this number of bolts usually cannot be used in the web.  
(3) N < N<sub>min</sub> denotes that this number of bolts is not usually used in practical connections.



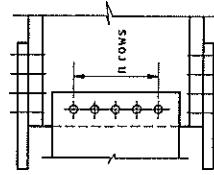
**TABLE 7-9  
UNIVERSAL BEAMS  
GRADE 300**

**DESIGN SECTION CAPACITIES IN AXIAL TENSION  
with end connections to FLANGE and to WEB**

TABLE 7-9

**UNIVERSAL BEAMS  
GRADE 300**

**DESIGN SECTION CAPACITIES IN AXIAL TENSION  
with end connections to FLANGE and to WEB**



Design Section Capacity in Axial Tension,  $\phi N_i$  (kN)

Bolted - Two Holes in Each Flange, N in Web

N =

Designation	Welded No Holes	Hole Dia.	Design Section Capacity in Axial Tension, $\phi N_i$ (kN)						
			1	2	3	4	5	6	7
N = 0	mm	mm							
610UB125	4020	22							
113	3650	22	4020	4020	4020	4020	4020	4020	4020
101	3510	22	3650	3650	3650	3650	3650	3650	3650
530UB 92.4	3190	22	3510	3510	3510	3510	3510	3510	3510
82.0	2840	22	3190	3190	3190	3190	3190	3190	3190
460UB 82.1	2830	22	2840	2840	2840	2840	2840	2840	2840
74.6	2570	22	2830	2830	2830	2830	2830	2830	2830
67.1	2320	22	2570	2570	2570	2570	2570	2570	2570
410UB 59.7	2060	22	2320	2320	2320	2320	2320	2320	2320
53.7	1980	22	2060	2060	2060	2060	2060	2060	2060
360UB 56.7	1960	22	1940	1940	1940	1940	1940	1940	1940
50.7	1750	22	1960	1960	1960	1960	1960	1960	1960
44.7	1650	22	1750	1750	1750	1750	1750	1750	1750
310UB 46.2	1600	22	1590	1590	1590	1590	1590	1590	1590
40.4	1500	22	1410	1410	1410	1410	1410	1410	1410
32.0	1180	22	1100	1100	1100	1100	1100	1100	1100
250UB 37.3	1370	22	1230	1230	1230	1230	1230	1230	1230
31.4	1150	22	1050	1050	1050	1050	1050	1050	1050
25.7	941	18	845	845	845	845	845	845	845
200UB 29.8	1100	22	956	956	956	956	956	956	956
25.4	930	22	814	814	814	814	814	814	814
22.3	826	22	771	771	771	771	771	771	771
18.2	668	†	684	684	684	684	684	684	684
180UB 22.2	813	†							
18.1	663	†							
16.1	589	†							
150UB 18.0	661	†							
14.0	514	†							

**N > N<sub>max</sub>**

- (1) N > N<sub>max</sub> denotes that this number of bolts usually cannot be used in the web.
- (2) N < N<sub>min</sub> denotes that this number of bolts is not usually used in practical connections.
- (3) † indicates flange too small for high strength structural bolts.
- (4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

**TABLE 7-10  
UNIVERSAL BEAMS  
GRADE 300**

**DESIGN SECTION CAPACITIES IN AXIAL TENSION  
with end connections to FLANGE only**

TABLE 7-10

**UNIVERSAL BEAMS  
GRADE 300**

**DESIGN SECTION CAPACITIES IN AXIAL TENSION  
with end connections to FLANGE only**

Designation	Design Section Capacity in Axial Tension, $\phi N_i$ (kN)						
	Bolted - N Holes/Flange			Bolted - N Holes/Flange			
	Welded No Holes	Hole Dia.	N = 0	N = 0	Hole Dia.	N =	
610UB125	4020	22	4020	4020	3650	3650	4020
113	3650	22	3650	3650	3510	3510	3650
101	3510	22	3510	3510	3510	3510	3510
530UB 92.4	3190	22	3190	3190	2840	2840	3190
82.0	2840	22	2840	2840	2790	2790	2840
460UB 82.1	2830	22	2830	2830	2570	2570	2830
74.6	2570	22	2570	2570	2320	2320	2570
67.1	2320	22	2320	2320	2260	2260	2320
410UB 59.7	2060	22	2060	2060	1960	1960	2060
53.7	1980	22	1980	1980	1770	1770	1980
360UB 56.7	1960	22	1960	1960	1680	1680	1960
50.7	1750	22	1750	1750	1540	1540	1750
44.7	1650	22	1650	1650	1490	1490	1650
310UB 46.2	1600	22	1600	1600	1500	1500	1600
40.4	1500	22	1500	1500	1360	1360	1500
32.0	1180	22	1180	1180	1100	1100	1180
250UB 37.3	1370	22	1230	1230	1050	1050	1370
31.4	1150	22	1050	1050	845	845	1150
25.7	941	18	845	845	815	815	941
200UB 29.8	1100	22	956	956	771	771	1090
25.4	930	22	814	814	721	721	821
22.3	826	22					924
18.2	668	†					924
180UB 22.2	813	†					807
18.1	663	†					659
16.1	589	†					585
150UB 18.0	661	†					657
14.0	514	†					511

Notes: (1) † indicates flange too small for high strength structural bolts.  
(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 7-11  
UNIVERSAL COLUMNS  
GRADE 300**

**DESIGN SECTION CAPACITIES IN AXIAL TENSION  
with end connections to FLANGE and to WEB**

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)				
	Bolted — Two Holes in Each Flange, N in Web				
	Welded No Holes	Hole Dia. mm	N = 0	2	3
310UC158	5070	26	5070	5070	5070
137	4400	26	4400	4400	4400
118	3780	26	3780	3780	3780
96.8	3340	26	3340	3340	3340
250UC 89.5	2870	22	2870	2870	2870
72.9	2520	22	2520	2520	2520
200UC 59.5	2060	22	2060	2010	1940
52.2	1800	22	1800	1750	1690
46.2	1590	22	1590	1550	1500
150UC 37.2	1280	22	1190	1130	—
30.0	1110	22	972	923	—
23.4	859	22	757	712	—
100UC 14.8	543	22	391	—	—

Notes: (1) — indicates that  $N > N_{max}$ , i.e. this number of bolts usually cannot be used in the web.  
 (2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

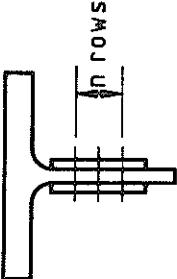


**TABLE 7-12  
UNIVERSAL COLUMNS  
GRADE 300**

**DESIGN SECTION CAPACITIES IN AXIAL TENSION  
with end connections to FLANGE only**

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)				
	Welded No Holes		Bolted — N Holes/Flange Hole Dia. mm		
	N = 0	N = 2	N = 2		
310UC158	5070	5070	5070	26	5020
137	4400	4400	4400	26	4350
118	3780	3780	3780	26	3740
96.8	3340	3340	3340	26	3080
250UC 89.5	2870	2870	2870	22	2820
72.9	2520	2520	2520	22	2310
200UC 59.5	2060	2060	2060	22	1820
52.2	1800	1800	1800	22	1590
46.2	1590	1590	1590	22	1410
150UC 37.2	1280	1190	1130	22	1060
30.0	1110	972	923	22	868
23.4	859	757	712	22	682
100UC 14.8	543	391	—	22	364

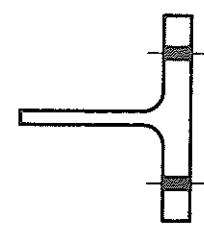
Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 7-13**  
**TEES CUT FROM UNIVERSAL BEAMS  
GRADE 300**  
**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
**with end connections to WEB only**

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)					
	Welded — No Holes		Bolted — N Holes in Web		Bolted — N Holes/Flange	
	N = 0	Hole Dia. mm	1	2	3	N =
305BT62.5	2010	22	1950	1880	1810	2010
56.5	1820	22	1760	1700	1640	1820
50.5	1640	22	1580	1520	1460	1750
265BT46.3	1490	22	1430	1380	1320	1590
41.0	1320	22	1270	1220	1160	1420
230BT41.1	1320	22	1260	1210	—	1410
37.3	1200	22	1150	1100	—	1280
33.6	1080	22	1030	986	—	1160
205BT29.9	962	22	919	876	—	1160
26.9	867	22	826	783	—	958
180BT28.4	912	22	868	—	—	1050
25.4	815	22	775	—	—	958
22.4	721	22	682	—	—	958
155BT23.1	747	22	710	—	—	958
20.2	656	22	622	—	—	958
16.0	514	22	483	—	—	958
125BT18.7	598	22	563	—	—	958
15.7	505	22	471	—	—	958
12.9	411	22	383	—	—	958
100BT14.9	481	22	446	—	—	958
12.7	406	22	374	—	—	958
11.2	361	22	333	—	—	958
9.1	291	22	266	—	—	958
90BT11.1	355	18	327	—	—	958
9.1	289	18	267	—	—	958
8.1	257	18	236	—	—	958
75BT 9.0	288	18	261	—	—	958
7.0	224	18	201	—	—	958

Notes: (1) — indicates that  $N > N_{max}$ , i.e. this number of bolts usually cannot be used in the web.  
(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 7-14**  
**TEES CUT FROM UNIVERSAL BEAMS  
GRADE 300**  
**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
**with end connections to FLANGE only**

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)					
	Welded — No Holes		N = 0		Bolted — N Holes/Flange	
	N = 0	Hole Dia. mm	N = 0	Hole Dia. mm	N =	Hole Dia. mm
305BT62.5	2010	22	1950	1880	1810	2010
56.5	1820	22	1760	1700	1640	1820
50.5	1640	22	1580	1520	1460	1750
265BT46.3	1490	22	1430	1380	1320	1590
41.0	1320	22	1270	1220	1160	1420
230BT41.1	1320	22	1260	1210	—	1410
37.3	1200	22	1150	1100	—	1280
33.6	1080	22	1030	986	—	1160
205BT29.9	962	22	919	876	—	958
26.9	867	22	826	783	—	958
180BT28.4	912	22	868	—	—	958
25.4	815	22	775	—	—	958
22.4	721	22	682	—	—	958
155BT23.1	747	22	710	—	—	958
20.2	656	22	622	—	—	958
16.0	514	22	483	—	—	958
125BT18.7	598	22	563	—	—	958
15.7	505	22	471	—	—	958
12.9	411	22	383	—	—	958
100BT14.9	481	22	446	—	—	958
12.7	406	22	374	—	—	958
11.2	361	22	333	—	—	958
9.1	291	22	266	—	—	958
90BT11.1	355	18	327	—	—	958
9.1	289	18	267	—	—	958
8.1	257	18	236	—	—	958
75BT 9.0	288	18	261	—	—	958
7.0	224	18	201	—	—	958

Notes: (1) — indicates flange too small for high strength structural bolts.  
(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

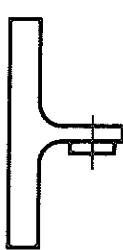


TABLE 7-15

**TEES CUT FROM UNIVERSAL COLUMNS  
GRADE 300**  
**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
**with end connections to WEB only**

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)		
	Welded No Holes	Bolted — N Holes in Web	N =
	Hole Dia.		
	mm		
		1	
155CT79.0	2530	26	2430
68.5	2200	26	2110
59.0	1890	26	1810
48.4	1560	26	1490
125CT44.8	1430	22	1380
36.5	1170	22	1130
100CT29.8	960	22	908
26.1	859	22	795
23.1	744	22	703
75CT18.6	596	22	551
15.0	486	22	449
11.7	375	22	341
50CT 7.4	237	22	209

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

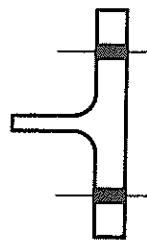


TABLE 7-16

**TEES CUT FROM UNIVERSAL COLUMNS  
GRADE 300**  
**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
**with end connections to FLANGE only**

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)		
	Welded No Holes	Bolted — N Holes/Flange	N =
	N = 0	mm	
	Hole Dia.	Hole Dia.	
	mm	mm	
		2	
155CT79.0	2530	26	2260
68.5	2200	26	1960
59.0	1890	26	1680
48.4	1560	26	1390
125CT44.8	1430	22	1250
36.5	1170	22	1030
100CT29.8	960	26	773
26.1	859	26	674
23.1	744	26	598
75CT18.6	596	22	408
15.0	486	22	332
11.7	375	22	269
50CT 7.4	237	22	97.5

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

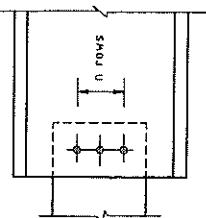


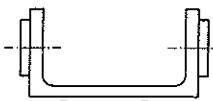
TABLE 7-17

## PARALLEL FLANGE CHANNELS GRADE 300

**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
with end connections to WEB only

Designation	Mass per metre	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)			
		Welded No Holes	Bolted - N Holes in Web	N =	
		mm	1	2	3
380 PFC	55.2	1770	22	1770	1770
300 PFC	40.1	1380	22	1380	1310
250 PFC	35.5	1220	22	1220	1190
230 PFC	25.1	864	22	864	834
200 PFC	22.9	788	22	788	759
180 PFC	20.9	718	22	718	—
150 PFC	17.7	645	18	614	—

Notes: (1) indicates that  $N > N_{max}$ , i.e. this number of bolts usually cannot be used in the web.  
(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



## PARALLEL FLANGE CHANNELS GRADE 300

**DESIGN SECTION CAPACITIES IN AXIAL TENSION**

**with end connections to FLANGE only**

Designation	Mass per metre	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)			
		Welded No Holes	Bolted - N Holes/Flange	N =	
		mm	1		
380 PFC	55.2	1770	22	1770	
300 PFC	40.1	1380	22	1280	
250 PFC	35.5	1220	22	1100	
230 PFC	25.1	884	22	765	
200 PFC	22.9	788	22	684	
180 PFC	20.9	718	22	623	
150 PFC	17.7	645	18	547	

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

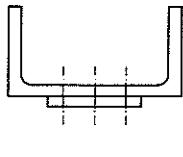


TABLE 7-19

## TAPER FLANGE CHANNELS GRADE 250

**DESIGN SECTION CAPACITIES IN AXIAL TENSION**

**with End Connections to WEB only**

Designation	Mass per metre	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)			
		Welded No Holes	Bolted - N Holes in Web	N =	
		mm	1	2	3
125 TFC	13.4	400	18	400	—
100 TFC	9.34	279	18	279	—
75 TFC	6.65	198	18	198	—

Note: — indicates that  $N > N_{max}$ , i.e. this number of bolts usually cannot be used in the web.

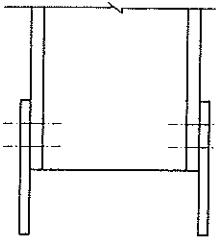


TABLE 7-20

## TAPER FLANGE CHANNELS GRADE 250

**DESIGN SECTION CAPACITIES IN AXIAL TENSION**

**with end connections to FLANGE only**

Designation	Mass per metre	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)			
		Welded No Holes	Bolted - N Holes/Flange	N =	Hole Dia.
		mm	1		
125 TFC	13.4	400	18	400	—
100 TFC	9.34	279	18	279	—
75 TFC	6.65	198	18	198	—

Note: ↑ Flange too small for high strength bolts.

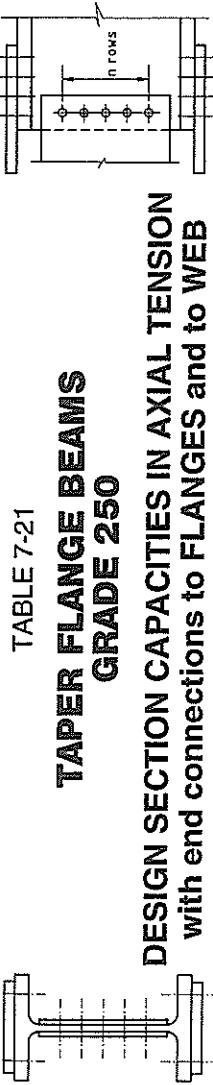


TABLE 7-21

## TAPER FLANGE BEAMS GRADE 250

**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
with end connections to FLANGES and to WEB

Designation	Mass per metre	kg/m	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)				
			Welded No Holes	Bolted - Two Holes in Each Flange, N in Web	Hole Dia.	N = 0	1
125 TFB	13.1	392	†	—	—	—	—
100 TFB	7.20	215	†	—	—	—	—

Notes: (1) — indicates that  $N > N_{\text{flange}}$ , i.e., this number of bolts usually cannot be used in the web.  
(2) † Flange too small for high strength structural bolts.



## EQUAL ANGLES GRADE 300

**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
one leg attached

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)				
	Welded No Holes	Bolted - N Holes in Leg	Hole Dia.	N =	
N = 0	mm	1	2		
200 x 200 x 25EA	2470	22	2470	2470	—
20EA	1930	22	1930	1930	—
18EA	1750	22	1750	1750	—
16EA	1670	22	1670	1570	—
13EA	1370	22	1370	1290	—
150 x 150 x 19EA	1350	22	1350	1300	104
16EA	1220	22	1190	1090	81.5
12EA	940	22	921	845	54.4
10EA	797	22	737	677	—
125 x 125 x 16EA	1000	18	980	899	76.2
12EA	774	18	758	697	60.0
10EA	657	18	608	559	40.4
8EA	544	18	503	463	—

Note: Grade 300 refers to BHP Grade 300 PLUS™. See Note (1) on page 2-2.

TABLE 7-22(2)

## EQUAL ANGLES GRADE 250

### DESIGN SECTION CAPACITIES IN AXIAL TENSION one leg attached

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)				
	Welded No Holes	Bolted - N Holes in Leg	Hole Dia.	N =	
N = 0	mm	1	2		
100 x 100 x 10EA	529	18	529	—	
10EA	424	18	424	—	
8EA	352	18	352	—	
6EA	273	18	273	—	
90 x 90 x 10EA	380	18	380	—	
8EA	315	18	315	—	
6EA	245	18	245	—	
75 x 75 x 10EA	313	18	311	—	
8EA	260	18	259	—	
6EA	203	18	202	—	
5EA	157	18	157	—	
65 x 65 x 10EA	269	18	261	—	
8EA	224	18	218	—	
6EA	175	18	171	—	
5EA	136	18	133	—	
55 x 55 x 6EA	147	18	139	—	
5EA	114	18	108	—	
50 x 50 x 8EA	169	18	155	—	
6EA	133	18	123	—	
5EA	104	18	96.0	—	
3EA	69.0	18	64.2	—	
45 x 45 x 6EA	118	—	—	—	—
5EA	92.3	—	—	—	—
3EA	61.4	—	—	—	—
40 x 40 x 6EA	104	—	—	—	—
5EA	81.5	—	—	—	—
3EA	54.4	—	—	—	—
30 x 30 x 6EA	76.2	—	—	—	—
5EA	60.0	—	—	—	—
3EA	40.4	—	—	—	—
25 x 25 x 6EA	62.1	—	—	—	—
5EA	49.2	—	—	—	—
3EA	33.3	—	—	—	—

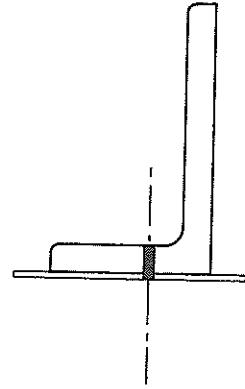


TABLE 7-23

**UNEQUAL ANGLES  
GRADE 300 & 250**  
**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
**long leg attached**

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)		
	Welded No Holes	Bolted - N Holes in Leg Hole Dia.	N =
150 x 75 x 10UA	—	—	—
150 x 100 x 12UA	774 657	22 22	745 597
150 x 90 x 16UA	959 742 630 519	18 18 18 18	935 724 581 479
125 x 75 x 12UA	529 424 352 273	18 18 18 18	529 424 352 273
100 x 75 x 10UA	369 306 238	18 18 18	369 306 238
75 x 50 x 8UA	215 169 131	18 18 18	208 163 127
65 x 50 x 8UA	197 154 120	18 18 18	187 147 114

Notes: (1) For 150 x 90 angles and above: Grade 300.  
 (2) For 125 x 75 angles and below: Grade 250.  
 (3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

TABLE 7-24

**UNEQUAL ANGLES  
GRADE 300 & 250**  
**DESIGN SECTION CAPACITIES IN AXIAL TENSION**  
**short leg attached**

Designation	Design Section Capacity in Axial Tension, $\phi N_t$ (kN)		
	Welded No Holes	Bolted - N Holes in Leg Hole Dia.	N =
150 x 100 x 12UA	—	—	—
150 x 90 x 16UA	10UA 10UA 10UA 8UA	10UA 12UA 10UA 8UA	724 579
125 x 75 x 12UA	10UA 8UA 6UA	10UA 8UA 6UA	529 424 352
100 x 75 x 10UA	8UA 6UA	8UA 6UA	369 306
75 x 50 x 8UA	6UA 5UA	6UA 5UA	238 197
65 x 50 x 8UA	5UA	5UA	114

Notes: (1) For 150 x 90 angles and above: Grade 300.  
 (2) For 125 x 75 angles and below: Grade 250.  
 (3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

(1) For 150 x 90 angles and above: Grade 300.  
 (2) For 125 x 75 angles and below: Grade 250.  
 (3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

**PART 8 MEMBERS SUBJECT TO COMBINED ACTIONS**

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*Tables 8.1-1 to 8.1-13 provide the information required to design members for combined actions. All relevant section capacities in bending, compression, tension and shear are given as well as reduced section moment capacities. These tables also provide reference to the appropriate tables in Sections 5 and 6 to determine design member capacities in bending and axial compression.*

**PART 8 MEMBERS SUBJECT TO COMBINED ACTIONS****8.1 Scope**

This part of the Tables contains the interaction formulae which are used to design members subject to combined actions in accordance with Section 8 of AS 4100. Tables 8.1-1 to 8.1-11 list design section capacities, including the effects of combined actions.

Sections 8.6, 8.7 and 8.8 present methods for calculating maximum design loads for angles as beams and as struts eccentrically loaded in trusses. Tables 8.2-1 to 8.2-12 and 8.3-1 to 8.3-6 list these maximum design loads.

**8.2 Design for Combined Actions**

Sections 8.3 and 8.4 give the formulae for combined bending and axial compression and combined bending and axial tension respectively. Each section describes the method for uniaxial bending about the major principal  $x$ -axis, for uniaxial bending about the minor principal  $y$ -axis, and for biaxial bending. Section 8.5 gives the interaction formulae for biaxial bending without axial forces. In every case both the section capacity and the member capacity must be checked.

*Note: The equations for section capacities listed in this section include the changes in Amendment 2 of AS 4100.*

**For all cases of combined bending and axial force the designer should first ensure that the appropriate design axial capacity is greater than the design axial force (i.e.  $\phi N \geq N^*$ ).**

**8.3 Combined Bending and Axial Compression**

In this section:

$$\phi = 0.9 \text{ (Table 3.4 of AS 4100)}$$

$\phi M_{sx}$  = design section moment capacity for bending about the major principal  $x$ -axis

$\phi M_{sy}$  = design section moment capacity for bending about the minor principal  $y$ -axis

$N^*$  = design axial compressive force

$\phi N_s$  = design section capacity in compression

$\phi N_{cx}$  = design member capacity in compression, buckling about the  $x$ -axis

$\phi N_{cy}$  = design member capacity in compression, buckling about the  $y$ -axis

**8.3.1 Compression and Uniaxial Bending - about the major principal  $x$ -axis**

For a member subject to uniaxial bending about the major principal  $x$ -axis and axial compression, the following condition must be satisfied:

$$M_x^* \leq \min [\phi M_{rx} ; \phi M_{ix} ; \phi M_{ox}]$$

where  $M_x^*$  = design bending moment about the major principal  $x$ -axis

$\phi M_{rx}$  = design section moment capacity ( $\phi M_s$ ) for bending about the major principal  $x$ -axis reduced by axial force (see Section 8.3.1.1)

$\phi M_{ix}$  = design in-plane member moment capacity ( $\phi M_i$ ) for bending about the major principal  $x$ -axis (see Section 8.3.1.2(a))

$\phi M_{ox}$  = design out-of-plane member moment capacity ( $\phi M_o$ ) for bending about the major principal  $x$ -axis (see Section 8.3.1.2(b))

### 8.3.1.1 Section Capacity

The value of  $\phi M_{rx}$  must be determined at all points along the member and the minimum value used to satisfy Section 8.3.1.

$$\phi M_{rx} = \phi M_{sx} \left( 1 - \frac{N^*}{\phi N_s} \right) \quad (\text{Clause 8.3.2 of AS 4100})$$

Alternatively, for doubly symmetric I- sections *compact about the x-axis* with  $k_f = 1.0$  subject to bending and compression

$$\phi M_{rx} = 1.18 \phi M_{sx} \left( 1 - \frac{N^*}{\phi N_s} \right) \leq \phi M_{sx} \quad (\text{Clause 8.3.2 of AS 4100})$$

For doubly symmetric I- sections *compact about the x-axis* with  $k_f < 1.0$  subject to bending and compression

$$\phi M_{rx} = \phi M_{sx} \left( 1 - \frac{N^*}{\phi N_s} \right) \left[ 1 + 0.18 \left( \frac{82 - \lambda_w}{82 - \lambda_{wy}} \right) \right] \leq \phi M_{sx} \quad (\text{Clause 8.3.2 of AS 4100})$$

where  $\lambda_w$  = the element slenderness of the web (Clause 6.2.3 of AS 4100)

$$= \frac{d_1}{t_w} \sqrt{\frac{f_y}{250}} \quad (\text{where } f_y = \min [ f_{y1}; f_{yw} ])$$

$\lambda_{wy}$  = the web yield slenderness limit (Table 6.2.4 of AS 4100)  
 = 45 for the hot-rolled I- sections considered in this publication.  
 = 35 for the welded I- sections considered in this publication.

For doubly symmetric I- sections, Tables 8.1-1 to 8.1-6, list  $\phi M_{sx}$ ,  $\phi M_{rx}$  (comp), and  $\phi M_{rx}$  (tens). Designers should calculate  $n = N^*/\phi N_s$ , and use it to calculate the value of  $\phi M_{rx}$ , and ensure that it is **less** than the design section capacity  $\phi M_{sx}$ . For other sections (tees and channels) the reduced section moment capacity is calculated by using the first of the equations given above.

### 8.3.1.2 Member Capacity

This section only applies to members analysed using an elastic method of analysis. Where there is sufficient restraint to prevent lateral buckling, only the in-plane requirements of Sections 8.3.1.1 and 8.3.1.2 need to be satisfied. If there is insufficient restraint to prevent lateral buckling, then both the in-plane and out-of-plane requirements of Sections 8.3.1.1 and 8.3.1.2 need to be satisfied.

#### (a) In-plane capacity

$$\phi M_{ix} = \phi M_{sx} \left( 1 - \frac{N^*}{\phi N_{cx}} \right) \quad (\text{Clause 8.4.2.2 of AS 4100})$$

For braced and sway members, the above value of  $\phi N_{cx}$  is to be calculated using an effective length factor ( $k_{ex}$ ) equal to 1.0 (i.e.  $L_{ex} = L$ ), unless a lower value of  $k_{ex}$  has been calculated for a braced member, provided that  $N^* \leq \phi N_{cx}$  where the value of  $\phi N_{cx}$  in this inequality is calculated using the correct value of  $k_{ex}$ .

(b) Out-of-plane capacity

$$\phi M_{ox} = \phi M_{bx} \left( 1 - \frac{N^*}{\phi N_{cy}} \right) \quad (\text{Clause 8.4.4.1 of AS 4100})$$

where  $\phi M_{bx}$  = design member moment capacity for bending about the major principal x-axis

For doubly symmetric compact I- sections with  $k_f = 1.0$ , alternatives for calculating  $\phi M_{ix}$  and  $\phi M_{ox}$  are presented in AS 4100 Clauses 8.4.2.2 and 8.4.4.1. This is beyond the scope of this publication.

### 8.3.2 Compression and Uniaxial Bending - about the minor principal y-axis

For a member subject to uniaxial bending about the minor principal y-axis and axial compression, the following condition must be satisfied:

$$M_y^* \leq \min [\phi M_{ry}; \phi M_{iy}]$$

where  $\phi = 0.9$  (Table 3.4 of AS 4100)

$M_y^*$  = design bending moment about the minor principal y-axis

$\phi M_{ry}$  = design section moment capacity ( $\phi M_s$ ) about the minor principal y-axis reduced by axial force (see Section 8.3.2.1)

$\phi M_{iy}$  = nominal in-plane member moment capacity ( $\phi M_i$ ) about the minor principal y-axis (see Section 8.3.2.2)

#### 8.3.2.1 Section Capacity

The value of  $\phi M_{ry}$  must be determined at all points along the member and the minimum value is used to satisfy Section 8.3.2.

$$\phi M_{ry} = \phi M_{sy} \left( 1 - \frac{N^*}{\phi N_s} \right) \quad (\text{Clause 8.3.3 of AS 4100})$$

Alternatively, for doubly symmetric I- sections *compact about the y-axis* subject to bending and compression

$$\phi M_{ry} = 1.19 \phi M_{sy} \left[ 1 - \left( \frac{N^*}{\phi N_s} \right)^2 \right] \leq \phi M_{sy} \quad (\text{Clause 8.3.3 of AS 4100})$$

For doubly symmetric I- sections, Tables 8.1-1 to 8.1-6, list  $\phi M_{sy}$  and  $\phi M_{ry}$ . Designers should calculate  $n = N^*/\phi N_s$ , and use it to calculate the value of  $\phi M_{ry}$ , and ensure that it is **less** than the design section capacity  $\phi M_{sy}$ . For other sections (tees and channels) the reduced section moment capacity is calculated by using the first of the equations given above.

#### 8.3.2.2 Member Capacity

This section applies only to members analysed using an elastic method of analysis. For bending about the minor principal y-axis only the in-plane requirements need to be satisfied.

### In-plane capacity

$$\phi M_{ly} = \phi M_{sy} \left( 1 - \frac{N^*}{\phi N_{cy}} \right) \quad (\text{Clause 8.4.2.2 of AS 4100})$$

For braced and sway members, the above value of  $\phi N_{cy}$  is to be calculated using an effective length factor ( $k_{ey}$ ) equal to 1.0 (i.e.  $L_{ey} = L$ ), unless a lower value of  $k_{ey}$  has been calculated for a braced member, provided that  $N^* \leq \phi N_{cy}$  where the value of  $\phi N_{cy}$  in this inequality is calculated using the correct value of  $k_{ey}$ .

## 8.3.3 Compression and Biaxial Bending

For a member subject to biaxial bending and axial compression, both the conditions defined in Sections 8.3.3.1 and 8.3.3.2 must be satisfied.

### 8.3.3.1 Section Capacity

$$\frac{N^*}{\phi N_s} + \frac{M_x^*}{\phi M_{sx}} + \frac{M_y^*}{\phi M_{sy}} \leq 1 \quad (\text{Clause 8.3.4 of AS 4100})$$

Alternatively for doubly symmetric I- sections *compact about both x- and y-axes*

$$\left( \frac{M_x^*}{\phi M_{rx}} \right)^{\gamma} + \left( \frac{M_y^*}{\phi M_{ry}} \right)^{\gamma} \leq 1 \quad (\text{Clause 8.3.4 of AS 4100})$$

where  $\gamma = 1.4 + \left( \frac{N^*}{\phi N_s} \right) \leq 2.0$

and  $\phi M_{rx}$  and  $\phi M_{ry}$  are calculated using the alternatives presented in Sections 8.3.1.1 & 8.3.2.1.

### 8.3.3.2 Member Capacity

$$\left( \frac{M_x^*}{\phi M_{cx}} \right)^{1.4} + \left( \frac{M_y^*}{\phi M_{ly}} \right)^{1.4} \leq 1 \quad (\text{Clause 8.4.5.1 of AS 4100})$$

where  $\phi M_{cx} = \text{lesser of } \phi M_{ix} \text{ and } \phi M_{ox}$  (see Section 8.3.1.2)

## 8.4 Combined Bending and Axial Tension

In this section:

$\phi = 0.9$  (Table 3.4 of AS 4100)

$N^*$  = design axial tensile force

$\phi N_t$  = design section capacity in axial tension

### 8.4.1 Tension & Uniaxial Bending - about the major principal x-axis

For a member subject to uniaxial bending about the major principal x-axis and axial tension, the following condition must be satisfied:

$$M_x^* \leq \min [\phi M_{rx}; \phi M_{ox}]$$

#### 8.4.1.1 Section Capacity

The value of  $\phi M_{rx}$  must be determined at all points along the member and the minimum value is used to satisfy Section 8.4.1.

$$\phi M_{rx} = \phi M_{sx} \left( 1 - \frac{N^*}{\phi N_t} \right) \quad (\text{Clause 8.3.2 of AS 4100})$$

Alternatively, for doubly symmetric I- sections *compact about the x-axis* subject to bending and tension

$$\phi M_{rx} = 1.18 \phi M_{sx} \left( 1 - \frac{N^*}{\phi N_t} \right) \leq \phi M_{sx} \quad (\text{Clause 8.3.2 of AS 4100})$$

*For doubly symmetric I- sections, Tables 8.1-1 to 8.1-6, list  $\phi M_{sx}$  and  $\phi M_{rx}$  (tens). Designers should calculate  $n = N^*/\phi N_t$ , and use it to calculate the value of  $\phi M_{rx}$ , and ensure that it is less than the design section capacity  $\phi M_{sx}$ . For other sections (tees and channels) the reduced section moment capacity is calculated by using the first of the equations given above.*

#### 8.4.1.2 Member Capacity

This section only applies to members analysed using an elastic method of analysis. Only the out-of-plane capacity needs to be considered.

##### Out-of-plane capacity

$$\phi M_{ox} = \phi M_{bx} \left( 1 + \frac{N^*}{\phi N_t} \right) \leq \phi M_{rx} \quad (\text{Clause 8.4.4.2 of AS 4100})$$

#### 8.4.2 Tension and Uniaxial Bending – about the minor principal y-axis

For a member subject to uniaxial bending about the minor principal y-axis and axial tension, the following condition must be satisfied:

$$M_y^* \leq \phi M_{ry}$$

#### 8.4.2.1 Section Capacity

The value of  $\phi M_{ry}$  must be determined at all points along the member and the minimum value is used to satisfy Section 8.4.2.

$$\phi M_{ry} = \phi M_{sy} \left( 1 - \frac{N^*}{\phi N_s} \right) \quad (\text{Clause 8.3.3 of AS 4100})$$

Alternatively for doubly symmetric I- sections *compact about the y-axis* subject to bending and tension

$$\phi M_{ry} = 1.19 \phi M_{sy} \left[ 1 - \left( \frac{N^*}{\phi N_t} \right)^2 \right] \leq \phi M_{sy} \quad (\text{Clause 8.3.3 of AS 4100})$$

*For doubly symmetric I- sections, Tables 8.1-1 to 8.1-6, list  $\phi M_{sy}$  and  $\phi M_{ry}$ . Designers should calculate  $n = N^*/\phi N_t$ , and use it to calculate the value of  $\phi M_{ry}$ , and ensure that it is less than the design section capacity  $\phi M_{sy}$ . For other sections (tees and channels) the reduced section moment capacity is calculated by using the first of the equations given above.*

### 8.4.3 Tension and Biaxial Bending

For a member subject to biaxial bending and axial tension, both the conditions defined in Sections 8.4.3.1 and 8.4.3.2 must be satisfied.

#### 8.4.3.1 Section Capacity

$$\frac{N^*}{\phi N_t} + \frac{M_x^*}{\phi M_{sx}} + \frac{M_y^*}{\phi M_{sy}} \leq 1 \quad (\text{Clause 8.3.4 of AS 4100})$$

Alternatively, for doubly symmetric I- sections *compact about both x- and y-axes*

$$\left( \frac{M_x^*}{\phi M_{rx}} \right)^\gamma + \left( \frac{M_y^*}{\phi M_{ry}} \right)^\gamma \leq 1 \quad (\text{Clause 8.3.4 of AS 4100})$$

where  $\gamma = 1.4 + \left( \frac{N^*}{\phi N_t} \right) \leq 2.0$

and  $\phi M_{rx}$  and  $\phi M_{ry}$  are calculated using the alternatives presented in Sections 8.4.1.1 & 8.4.2.1.

#### 8.4.3.2 Member Capacity

$$\left( \frac{M_x^*}{\phi M_{tx}} \right)^{1.4} + \left( \frac{M_y^*}{\phi M_{sy}} \right)^{1.4} \leq 1 \quad (\text{Clause 8.4.5.2 of AS 4100})$$

where  $\phi M_{tx} = \min [\phi M_{rx}, \phi M_{ox}]$  (see Sections 8.4.1.1 and 8.4.1.2).

## 8.5 Biaxial Bending

For a member subject to biaxial bending without any axial force, both the conditions defined in Sections 8.5.1 and 8.5.2 must be satisfied.

#### 8.5.1 Section Capacity

$$\frac{M_x^*}{\phi M_{sx}} + \frac{M_y^*}{\phi M_{sy}} \leq 1 \quad (\text{Clause 8.3.4 of AS 4100})$$

Alternatively, for doubly symmetric I- sections *compact about both x- and y-axes*

$$\left( \frac{M_x^*}{\phi M_{sx}} \right)^{1.4} + \left( \frac{M_y^*}{\phi M_{sy}} \right)^{1.4} \leq 1 \quad (\text{Clause 8.3.4 of AS 4100})$$

#### 8.5.2 Member Capacity

$$\left( \frac{M_x^*}{\phi M_{bx}} \right)^{1.4} + \left( \frac{M_y^*}{\phi M_{sy}} \right)^{1.4} \leq 1 \quad (\text{Clause 8.4.5 of AS 4100})$$

## 8.6 Example

Considering further Example 1 of Section 4.3, the adequacy of the member under the calculated design action effects is now checked as required by Clauses 8.3 and 8.4 of AS 4100.

### Design Data:

Section:	200UB29.8 Grade 300 steel
Effective lengths:	Flexural buckling (x-axis) = 4.0 m
	Flexural buckling (y-axis) = 4.0 m
	Lateral buckling = 4.0 m
Design action effects:	$N^* = 105 \text{ kN}$ $M_x^* = 45 \text{ kNm}$ $M_y^* = 6.40 \text{ kNm}$

Solution: The example involves biaxial bending and axial compression as described in Section 8.3.3 of these Tables.

### (i) Section Capacity Check (Section 8.3.3.1)

From Table 8.1-5 obtain:

$$\begin{aligned}\phi N_s &= 1100 \text{ kN} > N^* \\ \phi M_{sx} &= 90.9 \text{ kNm} \\ \phi M_{sy} &= 24.9 \text{ kNm}\end{aligned}$$

$$\text{Now } \frac{N^*}{\phi N_s} = \frac{105}{1100} = 0.0955$$

Using Table 8.1-5

$$\begin{aligned}\phi M_{rx} (\text{comp}) &= 107 (1-0.0955) = 96.8 \text{ kNm} > \phi M_{sx} \\ \therefore \phi M_{rx} &= \phi M_{sx} = 90.9 \text{ kNm} \\ \phi M_{ry} &= 29.6 (1-0.0955^2) = 29.3 \text{ kNm} > \phi M_{sy} \\ \therefore \phi M_{ry} &= \phi M_{sy} = 24.9 \text{ kNm}\end{aligned}$$

$$\text{Now } \gamma = 1.4 + \left( \frac{N^*}{\phi N_s} \right)^{\frac{1}{4}} = 1.496 < 2.0$$

$$\text{Then } \left( \frac{M_x^*}{\phi M_{rx}} \right)^{\gamma} + \left( \frac{M_y^*}{\phi M_{ry}} \right)^{\gamma} = \left( \frac{45.0}{90.9} \right)^{1.496} + \left( \frac{6.40}{24.9} \right)^{1.496} = 0.480 (< 1.0)$$

The above interaction equation was used as the section is *compact about both x- and y-axes*.

### (ii) Member Capacity Check (Section 8.3.3.2)

$$\left( \frac{M_x^*}{\phi M_{cx}} \right)^{1.4} + \left( \frac{M_y^*}{\phi M_{cy}} \right)^{1.4} \leq 1$$

From the Tables obtain:

$$\begin{aligned}\phi N_{cx} &= 938 \text{ kN} & (\text{Table 6-5(A)}) \\ \phi N_{cy} &= 352 \text{ kN} & (\text{Table 6-5(B)}) \\ \phi M_{bx} &= 47.6 \text{ kNm} & (\text{Table 5.3-5}) (\text{ based on } \alpha_m = 1.0) \\ \phi M_{sy} &= 24.9 \text{ kNm} & (\text{Table 8.1-5})\end{aligned}$$

The moment distribution for x-axis bending is not uniform, but the above value of  $\phi M_{bx}$  is based on the uniform moment case. From Table 5.6.1 of AS 4100,  $\alpha_m = 1.75$ .

$$\begin{aligned}\therefore \phi M_{bx} &= \min [\alpha_m(\phi M_{bx}), \phi M_{sx}] \\ &= \min [1.75 \times 47.6, 90.9] = \min [83.3, 90.9] \\ &= 83.3 \text{ kNm}\end{aligned}$$

Calculate in-plane and out-of-plane capacities:

$$\begin{aligned}\text{a)} \quad \phi M_{ix} &= \phi M_{sx} \left(1 - \frac{N^*}{\phi N_{cx}}\right) \\ &= 90.9 \left(1 - \frac{105}{938}\right) \\ &= 80.7 \text{ kNm}\end{aligned}$$

$$\begin{aligned}\text{b)} \quad \phi M_{ox} &= \phi M_{bx} \left(1 - \frac{N^*}{\phi N_{cy}}\right) \\ &= 83.3 \left(1 - \frac{105}{352}\right) \\ &= 58.4 \text{ kNm}\end{aligned}$$

$$\begin{aligned}\therefore \phi M_{cx} &= \min [\phi M_{ix}, \phi M_{ox}] \\ &= 58.4 \text{ kNm}\end{aligned}$$

$$\begin{aligned}\phi M_{iy} &= \phi M_{sy} \left(1 - \frac{N^*}{\phi N_{cy}}\right) \\ &= 24.9 \left(1 - \frac{105}{352}\right) \\ &= 17.5 \text{ kNm}\end{aligned}$$

$$\begin{aligned}\text{Thus, } \left(\frac{M_x^*}{\phi M_{cx}}\right)^{1.4} + \left(\frac{M_y^*}{\phi M_{iy}}\right)^{1.4} &= \left(\frac{45}{58.4}\right)^{1.4} + \left(\frac{6.40}{17.5}\right)^{1.4} \\ &= 0.939 \quad (< 1.0 \therefore \text{O.K.})\end{aligned}$$

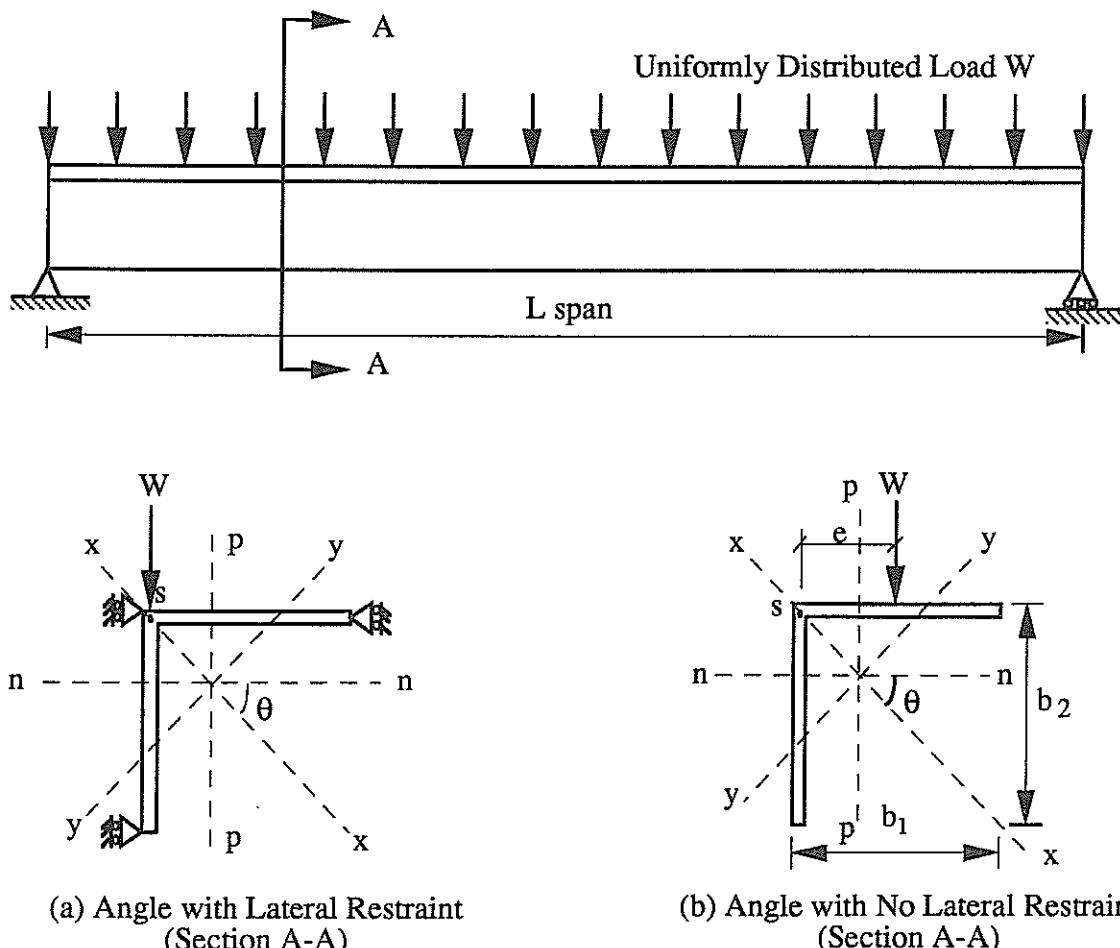
## 8.7 Maximum Design Loads for Angles Subject to Bending

### 8.7.1 General

Tables 8.2-1 to 8.2-12 give maximum design loads for strength ( $W_L^*$ ) and serviceability ( $W_{S1}^*$ ,  $W_{S2}^*$ ) for simply supported angles subject to uniformly distributed transverse loads. **Designers should assess the maximum design loads for strength and serviceability separately as different load factors apply to these cases as specified in AS 1170.**

Two situations are considered as shown below. Case (a) refers to angles which are *continuously restrained against twisting and constrained to deflect in the loading plane*. Case (b) is for angles *unrestrained against twisting and deflection in any plane*. These cases are considered, in principle only, in Clause 5.7 of AS 4100.

For case (a) a first-order elastic analysis is suitable for determining the design action effects. However for the unrestrained case, case (b), the design action effects are dependent on the deformed shape of the member and a second-order analysis is required.



- Notes:
- (1) s - shear centre
  - (2) eccentricity  $e = b_1/2$
  - (3) The angle is torsionally restrained at the support in both cases

Figure 8.1: Schematic Representation of Angle Configurations

## 8.7.2 Angles with Continuous Lateral Restraint

Tables 8.2-1 to 8.2-6 give maximum design loads for angles with full lateral restraint. The maximum design load for strength ( $W_L^*$ ) is the *lesser* of the maximum design loads associated with either biaxial bending or biaxial shear. The serviceability load ( $W_{S1}^*$ ) is the lesser of the load required to reach the deflection limit ( $L/250$ ) and the yield load. Similarly the serviceability load ( $W_{S2}^*$ ) is the lesser of the load required to reach the deflection limit ( $L/500$ ) and the yield load.

It is assumed that the beams are simply supported with a uniformly distributed load applied along the horizontal leg of the angle. This loading ensures there are no torsional effects. Note that the direction of loading is important.

To constrain the member to bend in the loading plane (a non-principal plane), the restraint must apply a significant force ( $W_{rest}$ ) at right angles to the external load ( $W$ ). These two forces result in bending about both principal axes of the angle. The maximum design load for strength is determined by considering the biaxial bending section capacity of the angle, or the biaxial shear capacity. Similarly the maximum design serviceability load is calculated by considering the deflection caused by biaxial bending (though this deflection is constrained to be in the loading plane).

## 8.7.3 Angles without Continuous Lateral Restraint

Tables 8.2-7 to 8.2-12 give maximum design loads for angles without continuous lateral and torsional restraint. The maximum design load for strength ( $W_{S1}^*$ ) is the lesser of the maximum design loads concerned with either biaxial bending, or combined biaxial shear and torsion. The serviceability load ( $W_{S1}^*$ ) is the lesser of the load required to reach the deflection limit ( $L/250$ ) and the yield load (either axial or shear yielding). Similarly the serviceability load ( $W_{S2}^*$ ) is the lesser of the load required to reach the deflection limit ( $L/500$ ) and the yield load.

It is assumed that the beams are simply supported with a uniformly distributed load applied eccentric to the shear centre through the horizontal leg of the angle (Figure 8.1). The angle is torsionally restrained at the supports only.

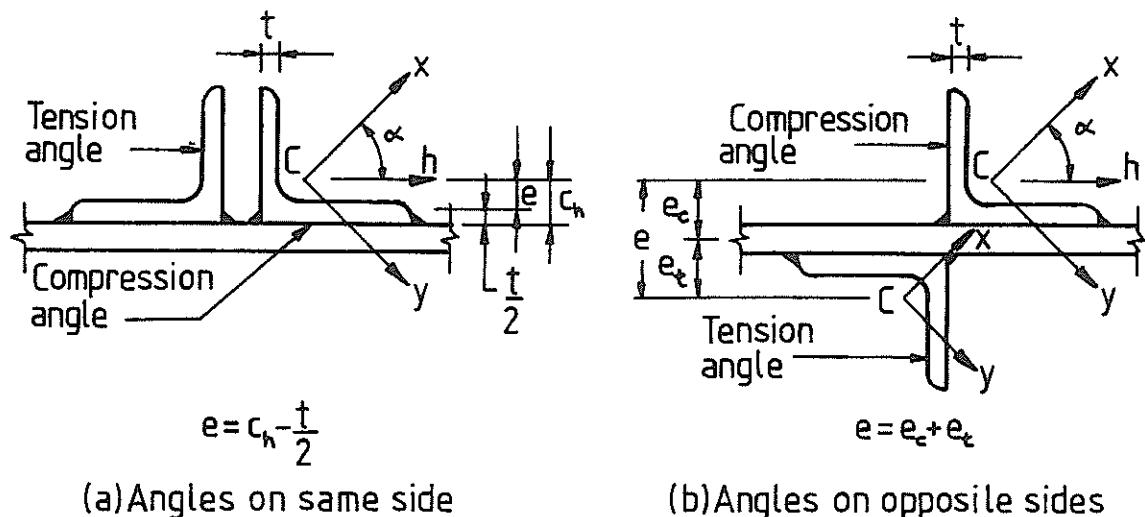
A second-order analysis is required to determine the design action effects and deflection.

More details on both cases can be found in the article *Design of Angles to AS 4100 - 1990* in the AISC technical journal, "Steel Construction", Vol 25, No 2, May 1991.

## 8.8 Eccentrically Loaded Single Angles in Trusses

Maximum design axial loads for single angles eccentrically loaded in trusses are given in Tables 8.3-1 to 8.3-6. These tables apply only to angles subject to axial force where there is eccentricity of the applied load due to the nature of the connection of the angle to the gusset plate in the truss.

Two cases are considered and are illustrated in Figure 8.2.



**Figure 8.2: Single Angles Loaded Through One Leg**

(Reproduced by courtesy of Standards Australia)

The maximum design loads are calculated using Clause 8.4.6 of AS 4100. It is assumed that the thickness of the gusset plate is 20 mm if the angle leg thickness is greater than or equal to 16 mm, and 10 mm if the angle thickness is less than 16 mm.

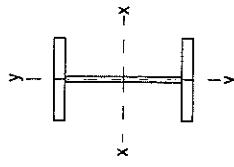


TABLE 8.1-1  
WELDED BEAMS  
GRADE 300  
DESIGN SECTION CAPACITIES

Designation	Design Section Axial Capacities		Design Section Moment Capacities				Design Shear Capacity $\phi V_s$ kN	
	$\phi N_s$	$\phi N_t$	About x-axis		About y-axis			
			$\phi M_{sx}$	$\phi M_{tx}$ (Comp)	$\phi M_{sy}$ (tens)	$\phi M_{ty}$		
	kN	kN	kNm	kNm	kNm	kNm		
1200WB455	12200	14600	7110	7330 (1-n)	8390 (1-n)	1260	1500 (1-n <sup>2</sup> )	
423	11200	13600	6510	6710 (1-n)	7680 (1-n)	1130	1350 (1-n <sup>2</sup> )	
392	10200	12600	5910	6090 (1-n)	6970 (1-n)	1010	1010 (1-n <sup>2</sup> )	
342	8580	11000	4980	5130 (1-n)	5880 (1-n)	646	769 (1-n <sup>2</sup> )	
317	7780	10200	4500	4640 (1-n)	5320 (1-n)	565	673 (1-n <sup>2</sup> )	
278	6540	8930	3790	3900 (1-n)	4470 (1-n)	387	460 (1-n <sup>2</sup> )	
249	5600	7980	3250	3350 (1-n)	3930 (1-n)	239	285 (1-n <sup>2</sup> )	
1000WB322	8580	10300	4130	4420 (1-n)	4870 (1-n)	646	768 (1-n <sup>2</sup> )	
296	7780	9520	3720	3980 (1-n)	4390 (1-n)	565	672 (1-n <sup>2</sup> )	
215	6540	8280	3100	3320 (1-n)	3660 (1-n)	387	460 (1-n <sup>2</sup> )	
5450	7390	2580	2740	2740 (1-n)	3050 (1-n)	244	290 (1-n <sup>2</sup> )	
900WB252	7650	9050	3440	3520 (1-n)	4050 (1-n)	645	768 (1-n <sup>2</sup> )	
257	6840	8250	3070	3140 (1-n)	3620 (1-n)	565	672 (1-n <sup>2</sup> )	
218	5610	7010	2510	2670 (1-n)	2860 (1-n)	386	460 (1-n <sup>2</sup> )	
175	4480	6030	2020	2050 (1-n)	2390 (1-n)	243	290 (1-n <sup>2</sup> )	
800WB192	5070	6150	2030	2040 (1-n)	2400 (1-n)	318	378 (1-n <sup>2</sup> )	
168	4300	5380	1720	1730 (1-n)	2030 (1-n)	238	284 (1-n <sup>2</sup> )	
146	3830	5020	1540	1540 (1-n)	1540 (1-n)	204	243 (1-n <sup>2</sup> )	
122	3020	4210	1220	1220 (1-n)	1220 (1-n)	135	135 (1-n)	
700WB173	4710	5540	1610	1680 (1-n)	1900 (1-n)	267	318 (1-n <sup>2</sup> )	
150	3980	4810	1350	1420 (1-n)	1600 (1-n)	197	234 (1-n <sup>2</sup> )	
130	3560	4480	1210	1260 (1-n)	1430 (1-n)	169	201 (1-n <sup>2</sup> )	
115	3020	3940	1020	1060 (1-n)	1210 (1-n)	134	134 (1-n)	

Notes: (1)  $\phi M_{rx}$  (comp) refers to the design section moment capacity reduced by compression (where  $n = N^*/\phi N_s$ ) and must be less than or equal to  $\phi M_{sx}$ .

(2)  $\phi M_{rx}$  (tens) refers to the design section moment capacity reduced by tension (where  $n = N^*/\phi N_t$ ) and must be less than or equal to  $\phi M_{tx}$ .

(3)  $\phi M_{ry}$  refers to the design section moment capacity reduced by axial force (where  $n = N^*/\phi N_t$  or  $N^*/\phi N_s$ ) and must be less than or equal to  $\phi M_{sy}$ .

(4) The above values of  $\phi N_t$  are based on sections with no holes and  $k_t = 1$ . For other values of  $\phi N_t$  see pages 7-4 and 7-6.

(5) For the design member moment capacity  $\phi M_b$  see page 5-40.

(6) For the design member capacity in compression (x-axis)  $\phi N_{bx}$  see page 6-6.

(7) For the design member capacity in compression (y-axis)  $\phi N_{by}$  see page 6-8.

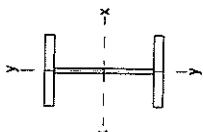


TABLE 8.1-2  
**WELDED BEAMS  
GRADE 400**  
**DESIGN SECTION CAPACITIES**

Designation	Design Section Axial Capacities		Design Section Moment Capacities About x-axis				Design Section Moment Capacities About y-axis				Design Shear Capacity $\phi V_y$ kN
	$\phi N_s$ kN	$\phi N_t$ kN	$\phi M_{sx}$ kNm	$\phi M_{tx}$ (comp) kNm	$\phi M_{sy}$ (tens) kNm	$\phi M_{ty}$ kNm	$\phi M_{ry}$ kNm	$\phi M_{ry}$ kNm	$\phi M_{ry}$ kNm		
1200WB455	15400 423	18800 14100	9090 8320	9090 (1-n) 8320 (1-n)	9090 (1-n) 8320 (1-n)	1620 1460	1930 (1-n <sup>2</sup> ) 1460 (1-n)	1930 (1-n <sup>2</sup> ) 1460 (1-n)	1930 (1-n <sup>2</sup> ) 1460 (1-n)	3320	
12800 352	16200 10700	7550 6360	7550 6360	7550 (1-n) 6360 (1-n)	7550 (1-n) 6360 (1-n)	1260 830	1260 (1-n) 830	1260 (1-n) 830	1260 (1-n) 830	3320	
14100 342	14100 9680	6360 5750	6360 5750	6360 (1-n) 5750 (1-n)	6360 (1-n) 5750 (1-n)	723 723	723 (1-n) 723	723 (1-n) 723	723 (1-n) 723	3320	
13100 317	13100 8090	5750 4830	5750 4830	5750 (1-n) 4830 (1-n)	5750 (1-n) 4830 (1-n)	497 497	497 (1-n) 497	497 (1-n) 497	497 (1-n) 497	3320	
11500 278	11500 8090	4830 4140	4830 4140	4830 (1-n) 4140 (1-n)	4830 (1-n) 4140 (1-n)	308 308	366 (1-n <sup>2</sup> ) 366 (1-n <sup>2</sup> )	366 (1-n <sup>2</sup> ) 366 (1-n <sup>2</sup> )	366 (1-n <sup>2</sup> ) 366 (1-n <sup>2</sup> )	3320	
10300 249	10300 6870	5310 4140	5310 4140	5310 (1-n) 4140 (1-n)	5310 (1-n) 4140 (1-n)	830 723	830 723	830 723	830 723	3320	
13300 286	12200 8090	4780 3990	4780 3990	4960 (1-n) 4140 (1-n)	4960 (1-n) 4140 (1-n)	5640 4700	5640 (1-n) 4700 (1-n)	5640 (1-n) 4700 (1-n)	5640 (1-n) 4700 (1-n)	3150	
10600 215	10600 6590	3990 3270	3990 3270	3990 (1-n) 3270 (1-n)	3990 (1-n) 3270 (1-n)	4700 3860	4700 (1-n) 3860 (1-n)	4700 (1-n) 3860 (1-n)	4700 (1-n) 3860 (1-n)	3150	
11600 257	11600 8620	4370 3990	4370 3990	4370 (1-n) 3990 (1-n)	4370 (1-n) 3990 (1-n)	830 721	830 721	830 721	830 721	3150	
9010 218	9010 7030	3190 2500	3190 2500	3190 (1-n) 2500 (1-n)	3190 (1-n) 2500 (1-n)	3190 2500	3190 (1-n) 2500 (1-n)	3190 (1-n) 2500 (1-n)	3190 (1-n) 2500 (1-n)	3150	
7630 175	7630 5500	2500 2500	2500 2500	2500 (1-n) 2500 (1-n)	2500 (1-n) 2500 (1-n)	302 302	302 (1-n) 302 (1-n)	302 (1-n) 302 (1-n)	302 (1-n) 302 (1-n)	3150	
6390 168	7910 5400	2540 2150	2540 2150	2540 (1-n) 2150 (1-n)	2540 (1-n) 2150 (1-n)	408 307	408 307	408 307	408 307	1820	
6360 146	6360 4790	1880 1880	1880 1880	1880 (1-n) 1880 (1-n)	1880 (1-n) 1880 (1-n)	258 180	258 (1-n) 180	258 (1-n) 180	258 (1-n) 180	1820	
5340 122	5340 3710	1480 1480	1480 1480	1480 (1-n) 1480 (1-n)	1480 (1-n) 1480 (1-n)	166 166	166 (1-n) 166	166 (1-n) 166	166 (1-n) 166	1820	
7130 150	7130 5000	2070 1740	2070 1740	2090 (1-n) 1760 (1-n)	2090 (1-n) 1760 (1-n)	2440 2050	2440 (1-n) 2050 (1-n)	2440 (1-n) 2050 (1-n)	2440 (1-n) 2050 (1-n)	1190	
5680 130	5680 4390	1540 1540	1540 1540	1540 (1-n) 1540 (1-n)	1540 (1-n) 1540 (1-n)	253 1810	253 (1-n) 1810 (1-n)	253 (1-n) 1810 (1-n)	253 (1-n) 1810 (1-n)	1190	
4990 115	4990 3710	1300 1300	1300 1300	1300 (1-n) 1300 (1-n)	1300 (1-n) 1300 (1-n)	166 166	166 (1-n) 166	166 (1-n) 166	166 (1-n) 166	1190	

Notes: (1)  $\phi M_{rx}$  (comp) refers to the design section moment capacity reduced by compression (where  $n = N^f / \phi N_s$ ) and must be less than or equal to  $\phi M_{sx}$ .

(2)  $\phi M_{tx}$  (tens) refers to the design section moment capacity reduced by tension (where  $n = N^* / \phi N_t$ ) and must be less than or equal to  $\phi M_{sy}$ .

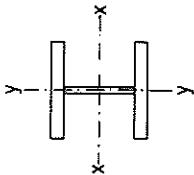
(3)  $\phi M_{ry}$  refers to the design section moment capacity reduced by axial force (where  $n = N^* / \phi N_t$  or  $N^* / \phi N_s$ ) and must be less than or equal to  $\phi M_{gy}$ .

(4) The above values of  $\phi N_t$  are based on sections with no holes and  $k_t = 1$ . For other values of  $\phi N_t$  see pages 7-5 and 7-6.

(5) For the design member moment capacity  $\phi M_b$  see page 5-42.

(6) For the design member capacity in compression (x-axis)  $\phi N_{cx}$  see page 6-10.

(7) For the design member capacity in compression (y-axis)  $\phi N_{cy}$  see page 6-12.


  
**TABLE 8.1-3**  
**WELDED COLUMNS**  
**GRADE 300**  
**DESIGN SECTION CAPACITIES**

Designation	Design Section Axial Capacities		Design Section Moment Capacities						Design Shear Capacity $\phi V_y$ kN	
			About x-axis			About y-axis				
	$\phi N_s$	$\phi N_t$	$\phi M_{sx}$	$\phi M_{tx}$ (comp)	$\phi M_{sy}$	$\phi M_{ty}$	$\phi M_{xy}$			
	kN	kN	kNm	kNm	kNm	kNm	kNm			
500WC440	14100	14100	2620	3090 (1-n)	3090 (1-n)	1260	1500 (1-n <sup>2</sup> )	2420		
414	13390	13300	2540	3000 (1-n)	3000 (1-n)	1260	1500 (1-n <sup>2</sup> )	1940		
383	12300	12300	2300	2710 (1-n)	2710 (1-n)	1140	1380 (1-n <sup>2</sup> )	1940		
340	10900	10900	2250	2670 (1-n)	2670 (1-n)	1010	1200 (1-n <sup>2</sup> )	1700		
290	9320	9320	1910	1910 (1-n)	1910 (1-n)	860	880 (1-n)	1460		
267	8570	8570	1690	1690 (1-n)	1690 (1-n)	747	747 (1-n)	1460		
228	7830	7830	1410	1410 (1-n)	1410 (1-n)	593	593 (1-n)	1460		
400WC361	11600	11600	1880	2220 (1-n)	2220 (1-n)	810	964 (1-n <sup>2</sup> )	2120		
328	10500	10500	1790	2110 (1-n)	2110 (1-n)	808	961 (1-n <sup>2</sup> )	1480		
303	9730	9730	1620	1910 (1-n)	1910 (1-n)	727	805 (1-n <sup>2</sup> )	1480		
270	8660	8660	1430	1680 (1-n)	1680 (1-n)	646	769 (1-n <sup>2</sup> )	1320		
212	6800	6800	1100	1100 (1-n)	1100 (1-n)	504	504 (1-n)	1130		
181	6210	6210	922	922 (1-n)	922 (1-n)	408	408 (1-n)	1130		
144	4970	4970	698	698 (1-n)	698 (1-n)	303	303 (1-n)	907		
350WC280	9000	9000	1240	1470 (1-n)	1470 (1-n)	618	736 (1-n <sup>2</sup> )	1160		
258	8290	8290	1120	1320 (1-n)	1320 (1-n)	557	663 (1-n <sup>2</sup> )	1160		
230	7380	7380	986	1160 (1-n)	1160 (1-n)	495	589 (1-n <sup>2</sup> )	1040		
197	6330	6330	844	995 (1-n)	995 (1-n)	433	515 (1-n <sup>2</sup> )	891		

Notes: (1)  $\phi M_{sx}$  (comp) refers to the design section moment capacity reduced by compression (where  $n = N^*/\phi N_s$ ) and must be less than or equal to  $\phi M_{sx}$ .

(2)  $\phi M_{tx}$  (tens) refers to the design section moment capacity reduced by tension (where  $n = N^*/\phi N_t$ ) and must be less than or equal to  $\phi M_{tx}$ .

(3)  $\phi M_{sy}$  refers to the design section moment capacity reduced by axial force (where  $n = N^*/\phi N_t$  or  $N^*/\phi N_s$ ) and must be less than or equal to  $\phi M_{sy}$ .

(4) The above values of  $\phi N_s$  are based on sections with no holes and  $k_t = 1$ . For other values of  $\phi N_s$  see page 7-8.

(5) For the design member moment capacity  $\phi M_b$  see page 5-44.

(6) For the design member capacity in compression (x-axis)  $\phi N_{cx}$  see page 6-14.

(7) For the design member capacity in compression (y-axis)  $\phi N_{cy}$  see page 6-16.

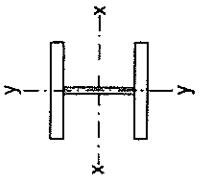


TABLE 8.1-4  
WELDED COLUMNS  
GRADE 400  
DESIGN SECTION CAPACITIES

Designation	Design Section Axial Capacities		Design Section Moment Capacities				Design Shear Capacity $\phi V_y$ kN	
	$\phi N_s$	$\phi N_t$	About x-axis		About y-axis			
			$\phi M_{sx}$ kNm	$\phi M_{tx}$ (comp) kNm	$\phi M_{sy}$ kNm	$\phi M_{ty}$ kNm		
500WC440	18100	18100	3370	3880 (1-n)	3980 (1-n)	1620	1930 (1-n <sup>2</sup> )	
414	17100	17100	3270	3850 (1-n)	3850 (1-n)	1620	1930 (1-n <sup>2</sup> )	
383	15800	15800	2960	3490 (1-n)	3490 (1-n)	1460	1740 (1-n <sup>2</sup> )	
340	14000	14000	2860	2860 (1-n)	2860 (1-n)	1270	1270 (1-n)	
290	12000	12000	2400	2400 (1-n)	2400 (1-n)	1070	1070 (1-n)	
267	11000	11000	2120	2120 (1-n)	2120 (1-n)	928	928 (1-n)	
228	9570	9920	1660	1660 (1-n)	1660 (1-n)	717	717 (1-n)	
400WC361	14900	14900	2420	2850 (1-n)	2850 (1-n)	1040	1240 (1-n <sup>2</sup> )	
328	13500	13500	2300	2710 (1-n)	2710 (1-n)	1040	1240 (1-n <sup>2</sup> )	
303	12500	12500	2050	2450 (1-n)	2450 (1-n)	935	1110 (1-n <sup>2</sup> )	
270	11100	11100	1880	2160 (1-n)	2160 (1-n)	831	983 (1-n <sup>2</sup> )	
212	8750	8750	1380	1380 (1-n)	1380 (1-n)	631	631 (1-n)	
181	7870	7870	1140	1140 (1-n)	1140 (1-n)	499	499 (1-n)	
144	6070	6290	824	824 (1-n)	824 (1-n)	367	367 (1-n)	
350WC280	11600	11600	1600	1890 (1-n)	1890 (1-n)	795	946 (1-n <sup>2</sup> )	
258	10700	10700	1440	1700 (1-n)	1700 (1-n)	716	852 (1-n <sup>2</sup> )	
230	9490	9490	1270	1500 (1-n)	1500 (1-n)	636	757 (1-n <sup>2</sup> )	
197	8130	8130	1050	1280 (1-n)	1280 (1-n)	556	662 (1-n <sup>2</sup> )	

Notes: (1)  $\phi M_{rx}$  (comp) refers to the design section moment capacity reduced by compression (where  $n = N^*/\phi N_s$ ) and must be less than or equal to  $\phi M_{sx}$ .

(2)  $\phi M_{tx}$  (tens) refers to the design section moment capacity reduced by tension (where  $n = N^*/\phi N_t$ ) and must be less than or equal to  $\phi M_{sy}$ .

(3)  $\phi M_{ry}$  refers to the design section moment capacity reduced by axial force (where  $n = N^*/\phi N_t$  or  $N^*/\phi N_s$ ) and must be less than or equal to  $\phi M_{sy}$ .

(4) The above values of  $\phi N_t$  are based on sections with no holes and  $k_t = 1$ . For other values of  $\phi N_t$  see page 7-9.

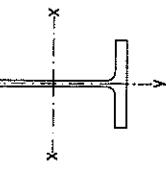
(5) For the design member moment capacity  $\phi M_s$  see page 5-46.

(6) For the design member capacity in compression (x-axis)  $\phi N_{cx}$  see page 6-18.

(7) For the design member capacity in compression (y-axis)  $\phi N_{cy}$  see page 6-20.

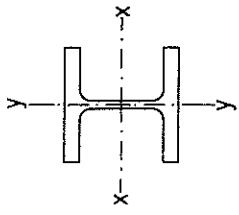
(8) \* indicates shear capacity governed by the shear capacity of the weld.

TABLE 8.1-5  
**UNIVERSAL BEAMS  
GRADE 300**  
**DESIGN SECTION CAPACITIES**



Designation	Design Section Axial Capacities		Design Section Moment Capacities				Design Shear Capacity $\phi V_v$ kN	
			About x-axis		About y-axis			
	$\phi N_u$ kN	$\phi N_t$ kN	$\phi M_{rx}$ (comp) kNm	$\phi M_{rx}$ (tens) kNm	$\phi M_{ry}$ kNm	$\phi M_{sy}$ kNm		
610UB125 113 101	3820 3370 3110	4020 3650 3510	927 829 782	1070 (1-n) 942 (1-n) 869 (1-n)	1090 (1-n) 979 (1-n) 923 (1-n)	130 114 104	154 (1-n) 135 (1-n) 124 (1-n)	1180 1100 1100
530UB 92.4 82.0	2960 2560	3190 2840	640 558	728 (1-n) 625 (1-n)	755 (1-n) 658 (1-n)	92.2 78.0	110 (1-n) 92.9 (1-n)	939 876
460UB 82.1 74.6 67.1	2770 2440 2130	2830 2570 2320	496 449 399	579 (1-n) 515 (1-n) 451 (1-n)	585 (1-n) 529 (1-n) 471 (1-n)	79.0 70.8 62.0	94.0 (1-n) 84.3 (1-n) 73.8 (1-n)	788 719 667
410UB 59.7 53.7	1940 1810	2060 1980	324 304	369 (1-n) 342 (1-n)	382 (1-n) 359 (1-n)	54.8 49.8	65.3 (1-n) 59.3 (1-n)	548 529
360UB 56.7 50.7 44.7	1950 1680 1530	1960 1750 1650	273 242 222	322 (1-n) 280 (1-n) 222 (1-n)	323 (1-n) 286 (1-n) 222 (1-n)	52.0 45.5 40.4	61.9 (1-n) 54.1 (1-n) 40.4 (1-n)	496 449 420
310UB 46.2 40.4 32.0	1590 1430 1070	1600 1500 1180	197 182 134	231 (1-n) 208 (1-n) 134 (1-n)	232 (1-n) 215 (1-n) 134 (1-n)	44.0 40.0 25.0	52.3 (1-n) 47.6 (1-n) 25.0 (1-n)	356 320 283
250UB 37.3 31.4 25.7	1370 1150 893	1370 1150 941	140 114 92.0	165 (1-n) 114 (1-n) 105 (1-n)	165 (1-n) 114 (1-n) 109 (1-n)	33.5 26.3 17.8	39.9 (1-n) 26.3 (1-n) 21.1 (1-n)	283 265 214
200UB 29.8 25.4 22.3 18.2	1100 930 826 661	1100 930 826 668	90.0 74.6 65.3 51.8	107 (1-n) 74.6 (1-n) 65.3 (1-n) 60.8 (1-n)	107 (1-n) 74.6 (1-n) 65.3 (1-n) 61.1 (1-n)	24.9 19.8 17.4 9.92	29.6 (1-n) 19.8 (1-n) 17.4 (1-n) 11.8 (1-n)	225 204 174 154
180UB 22.2	813	813	56.2	66.4 (1-n)	66.4 (1-n)	11.7	13.9 (1-n)	186
18.1 16.1	663 589	663 589	45.2 39.8	53.4 (1-n) 47.0 (1-n)	53.4 (1-n) 47.0 (1-n)	9.36 8.19	11.1 (1-n) 9.75 (1-n)	151 135
150UB 18.0	661 514	661 514	38.9 29.3	45.9 (1-n) 34.6 (1-n)	45.9 (1-n) 34.6 (1-n)	7.74 5.70	9.21 (1-n) 6.73 (1-n)	161 130

Notes: (1)  $\phi M_{rx}$  (comp) refers to the design section moment capacity reduced by compression (where  $n = N^*/\phi N_u$ ) and must be less than or equal to  $\phi M_{sx}$ .  
(2)  $\phi M_{rx}$  (tens) refers to the design section moment capacity reduced by tension (where  $n = N^*/\phi N_t$ ) and must be less than or equal to  $\phi M_{sx}$ .  
(3)  $\phi M_{ry}$  refers to the design section moment capacity reduced by axial force (where  $n = N^*/\phi N_u$  or  $N^*/\phi N_t$ ) and must be less than or equal to  $\phi M_{sy}$ .  
(4) The above values of  $\phi N_u$  are based on sections with no holes and  $k_1 = 1$ . For other values of  $\phi N_u$  see page 7-10.  
(5) For the design member moment capacity  $\phi M_b$  see page 5-48.  
(6) For the design member capacity in compression (x-axis)  $\phi N_{cx}$  see page 6-22.  
(7) For the design member capacity in compression (y-axis)  $\phi N_{cy}$  see page 6-24.  
(8) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 8.1-6**  
**UNIVERSAL COLUMNS**  
**GRADE 300**  
**DESIGN SECTION CAPACITIES**

Designation	Design Section Axial Capacities		Design Section Moment Capacities				Design Shear Capacity $\phi V_y$ kN
	$\phi N_s$	$\phi N_t$	About x-axis		About y-axis		
	kN	kN	$\phi M_{sx}$	$\phi M_{tx}$ (comp)	$\phi M_{ry}$ (tens)	$\phi M_{sy}$	
310UC158	5070	5070	676	798 (1-n)	305	363 (1-n <sup>2</sup> )	832
137	4400	4400	580	684 (1-n)	261	311 (1-n <sup>2</sup> )	717
118	3780	3780	494	582 (1-n)	222	264 (1-n <sup>2</sup> )	606
96.8	3340	3340	422	422 (1-n)	187	187 (1-n)	527
250UC 89.5	2870	2870	309	365 (1-n)	365 (1-n)	170 (1-n <sup>2</sup> )	472
72.9	2520	2520	266	266 (1-n)	266 (1-n)	123 (1-n)	377
200UC 59.5	2060	2060	177	209 (1-n)	209 (1-n)	80.6	96.0 (1-n <sup>2</sup> )
52.2	1800	1800	154	182 (1-n)	182 (1-n)	70.3	337
46.2	1590	1590	133	133 (1-n)	133 (1-n)	60.3	285
156UC 37.2	1280	1280	83.6	98.7 (1-n)	98.7 (1-n)	36.9	43.9 (1-n <sup>2</sup> )
30.0	1110	1110	71.9	84.8 (1-n)	84.8 (1-n)	31.7	37.7 (1-n <sup>2</sup> )
23.4	859	859	50.7	50.7 (1-n)	50.7 (1-n)	21.2	21.2 (1-n)
100UC 14.8	543	543	21.4	25.3 (1-n)	25.3 (1-n)	9.91	11.8 (1-n <sup>2</sup> )
							83.8

Notes: (1)  $\phi M_{tx}$  (comp) refers to the design section moment capacity reduced by compression (where  $n = N^*/\phi N_s$ ) and must be less than or equal to  $\phi M_{sx}$ .

(2)  $\phi M_{tx}$  (tens) refers to the design section moment capacity reduced by tension (where  $n = N^*/\phi N_t$ ) and must be less than or equal to  $\phi M_{sx}$ .

(3)  $\phi M_{ry}$  refers to the design section moment capacity reduced by axial force (where  $n = N^*/\phi N_t$  or  $N^*/\phi N_s$ ) and must be less than or equal to  $\phi M_{sy}$ .

(4) The above values of  $\phi N_i$  are based on sections with no holes and  $k_i = 1$ . For other values of  $\phi N_i$  see page 7-11.

(5) For the design member moment capacity  $\phi M_b$  see page 5-50.

(6) For the design member capacity in compression (x-axis)  $\phi N_{sx}$  see page 6-26.

(7) For the design member capacity in compression (y-axis)  $\phi N_{sy}$  see page 6-28.

(8) Grade 300 refers to BHP Grade 300 PLUS™. See Note (1) on page 2-2.

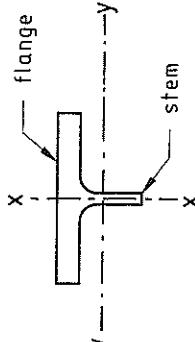


TABLE 8.1-7

## TEES CUT FROM UNIVERSAL BEAMS GRADE 300

### DESIGN SECTION CAPACITIES

Designation	Design Section Axial Capacities		Design Section Moment Capacities				Design Shear Capacity $\phi V_v$
	$\phi N_s$	$\phi N_t$	$\phi M_{sx}$	$\phi M_{sy}$	$\phi M_{tx}$	$\phi M_{ty}$	
	kN	kN	kNm	kNm	kNm	kNm	
305BT62.5	1690	2010	112	72.7	64.9	520	
56.5	1490	1820	104	59.6	56.8	486	
50.5	1380	1750	103	49.5	52.1	488	
265BT46.3	1310	1590	78.3	45.3	46.1	414	
41.0	1130	1420	72.1	37.0	39.0	387	
230BT41.1	1230	1410	56.8	39.5	346	346	
37.3	1090	1280	51.8	32.7	35.4	316	
33.6	951	1160	47.6	26.3	31.0	293	
205BT29.9	870	1030	35.3	20.8	27.4	240	
26.9	810	989	35.8	18.8	24.9	232	
180BT28.4	870	976	28.2	20.2	26.0	217	
25.4	756	872	25.4	17.0	22.7	19.6	
22.4	688	822	24.4	14.2	20.2	18.4	
155BT23.1	721	799	17.6	12.4	22.0	154	
20.2	652	748	16.8	10.2	20.0	139	
16.0	487	586	13.6	7.23	12.5	123	
125BT18.7	632	682	12.3	9.38	16.7	123	
15.7	523	576	11.2	8.37	13.2	115	
12.9	405	469	9.03	5.56	8.88	92.5	
100BT14.9 *	549	549	7.86	6.60	12.4	97.4	
12.7 *	446	464	6.92	5.67	9.50	88.2	
11.2 *	380	412	5.62	4.50	8.68	75.2	
9.1	297	332	5.11	3.64	4.96	66.3	
90BT11.1	405	405	5.40	4.75	5.85	80.4	
9.1	319	330	4.37	3.57	4.68	65.3	
8.1	274	293	3.87	3.01	4.09	58.0	
75BT 9.0	329	329	4.96	3.66	3.87	69.7	
7.0	256	256	3.14	2.73	2.85	56.2	

Notes: (1) \* indicates x- and y-axes are interchanged from that shown on the diagram.

(2)  $\phi M_{sx}$  refers to bending about the x-axis that causes compression in the flange.

(3)  $\phi M_{sy}$  refers to bending about the y-axis that causes compression in the stem.

(4) For all sections  $\phi M_{tx} = \phi M_{sx} (1-\eta)$  where  $\eta = N^*/\phi N_s$  or  $N^*/\phi N_t$ .

(5) The above values of  $\phi N_s$  are based on sections with no holes and  $k_1 = 1$ . For other values of  $\phi N_s$  see page 7-13.

(6) For tees bending about the y-axis the design member moment capacity,  $\phi M_{sy}$ , equals the design section moment capacity,  $\phi M_{sy}$ .

(7) For the design member capacity in compression (x-axis)  $\phi N_{ex}$  see page 6-32.

(8) For the design member capacity in compression (y-axis)  $\phi N_{ey}$  see page 6-33.

(9) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

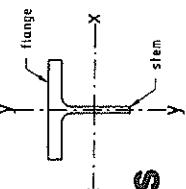


TABLE 8.1-8

## TEES CUT FROM UNIVERSAL COLUMNS GRADE 300

### DESIGN SECTION CAPACITIES

Designation	Design Section Axial Capacities		Design Section Moment Capacities				Design Shear Capacity $\phi V_v$
	$\phi N_s$	$\phi N_t$	$\phi M_{sx}$	$\phi M_{sy}$	$\phi M_{tx}$	$\phi M_{ty}$	
	kN	kN	kNm	kNm	kNm	kNm	
305BT62.5	1690	2010	112	72.7	64.9	520	
56.5	1490	1820	104	59.6	56.8	486	
50.5	1380	1750	103	49.5	52.1	488	
265BT46.3	1310	1590	78.3	45.3	46.1	414	
41.0	1130	1420	72.1	37.0	39.0	387	
230BT41.1	1230	1410	56.8	39.5	346	346	
37.3	1090	1280	51.8	32.7	35.4	316	
33.6	951	1160	47.6	26.3	31.0	293	
205BT29.9	870	1030	35.3	20.8	27.4	240	
26.9	810	989	35.8	18.8	24.9	232	
180BT28.4	870	976	28.2	20.2	26.0	217	
25.4	756	872	25.4	17.0	22.7	19.6	
22.4	688	822	24.4	14.2	20.2	18.4	
155BT23.1	721	799	17.6	12.4	22.0	154	
20.2	652	748	16.8	10.2	20.0	139	
16.0	487	586	13.6	7.23	12.5	123	
125BT18.7	632	682	12.3	9.38	16.7	123	
15.7	523	576	11.2	8.37	13.2	115	
12.9	405	469	9.03	5.56	8.88	92.5	
100BT14.9 *	549	549	7.86	6.60	12.4	97.4	
12.7 *	446	464	6.92	5.67	9.50	88.2	
11.2 *	380	412	5.62	4.50	8.68	75.2	
9.1	297	332	5.11	3.64	4.96	66.3	
90BT11.1	405	405	5.40	4.75	5.85	80.4	
9.1	319	330	4.37	3.57	4.68	65.3	
8.1	274	293	3.87	3.01	4.09	58.0	
75BT 9.0	329	329	4.96	3.66	3.87	69.7	
7.0	256	256	3.14	2.73	2.85	56.2	

Notes: (1)  $\phi M_{sy}$  refers to bending about the y-axis that causes compression in the flange.

(2)  $\phi M_{sy}$  refers to bending about the y-axis that causes compression in the stem.

(3) For all sections  $\phi M_{tx} = \phi M_{sx} (1-\eta)$  where  $\eta = N^*/\phi N_s$  or  $N^*/\phi N_t$ .

(4) For all sections  $\phi M_{ty} = \phi M_{sy} (1-\eta)$  where  $\eta = N^*/\phi N_s$  or  $N^*/\phi N_t$ .

(5) The above values of  $\phi N_s$  are based on sections with no holes and  $k_1 = 1$ . For other values of  $\phi N_s$  see page 7-13.

(6) For tees bending about the y-axis the design member moment capacity,  $\phi M_{sy}$ , equals the design section moment capacity,  $\phi M_{sy}$ .

(7) For the design member capacity in compression (x-axis)  $\phi N_{ex}$  see page 6-32.

(8) For the design member capacity in compression (y-axis)  $\phi N_{ey}$  see page 6-33.

(9) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

TABLE 8.1-9

PARALLEL FLANGE CHANNELS GRADE 300 DESIGN SECTION CAPACITIES						
Designation	Mass per metre	Design Section Axial Capacities			Design Shear Capacity	Design Section Moment Capacities About x-axis
		$\phi N_s$	$\phi N_t$	$\phi M_{sx}$		
	kg/m	kN	kN	kNm	kN	
380 PFC	55.2	1770	238	28.9	657	125 TFC
300 PFC	40.1	1380	152	22.2	415	100 TFC
210 PFC	35.5	1220	114	24.0	346	75 TFC
230 PFC	26.1	864	73.3	12.2	13.6	258
210 PFC	22.9	788	788	59.7	12.6	207
180 PFC	20.9	718	718	49.0	12.1	187
150 PFC	17.7	649	649	37.0	11.1	156

NOTES: (1)  $\phi M_{syL}$  refers to bending about the y-axis that causes compression in the web marked L.  
(2)  $\phi M_{syR}$  refers to bending about the y-axis that causes compression in the flange marked R.  
(3) For all sections  $\phi M_{sx} = \phi M_{sx}(1-n)$  where  $n = N^*/\phi N_s$  or  $N^*/\phi N_t$ .  
(4) For all sections  $\phi M_{ry} = \phi M_{sy}(1-n)$  where  $n = N^*/\phi N_s$  or  $N^*/\phi N_t$ .  
(5) The above values of  $\phi N_t$  are based on sections with no holes and  $k_t = 1$ . For other values of  $\phi N_t$  see page 7-14.  
(6) For the design member moment capacity  $\phi M_b$  see page 5-56.  
(7) For the design member capacity in compression (x-axis)  $\phi N_{cx}$  see page 6-38.  
(8) For the design member capacity in compression (y-axis)  $\phi N_{cy}$  see page 6-40.  
(9) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

TABLE 8.1-10

### TAPER FLANGE CHANNELS GRADE 250 DESIGN SECTION CAPACITIES



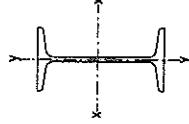
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Designation	Mass per metre	Design Section Axial Capacities			Design Shear Capacity	Design Section Moment Capacities About x-axis
		$\phi N_s$	$\phi N_t$	$\phi M_{sx}$		
	kg/m	kN	kN	kNm	kN	
125 TFB	13.1	392	392	18.8	22.2 (1-n)	22.2 (1-n)
100 TFB	7.20	214	214	7.98	9.41 (1-n)	9.41 (1-n)

NOTES: (1)  $\phi M_{syL}$  refers to the design section moment capacity reduced by compression (where  $n = N^*/\phi N_s$ ) and must be less than or equal to  $\phi M_{sx}$ .  
(2)  $\phi M_{syR}$  refers to the design section moment capacity reduced by tension (where  $n = N^*/\phi N_t$ ) and must be less than or equal to  $\phi M_{sx}$ .  
(3)  $\phi M_{ry}$  refers to the design section moment capacity reduced by axial force (where  $n = N^*/\phi N_s$  or  $N^*/\phi N_t$ ) and must be less than or equal to  $\phi M_{sy}$ .  
(4) The above values of  $\phi N_t$  are based on sections with no holes and  $k_t = 1$ . For other values of  $\phi N_t$  see page 7-15.  
(5) For the design member moment capacity  $\phi M_b$  see page 5-56.  
(6) For the design member capacity in compression (x-axis)  $\phi N_{cx}$  see page 6-38.  
(7) For the design member capacity in compression (y-axis)  $\phi N_{cy}$  see page 6-40.

TABLE 8.1-11

### TAPER FLANGE BEAMS GRADE 250 DESIGN SECTION CAPACITIES



Designation	Mass per metre	Design Section Axial Capacities			Design Shear Capacity	Design Section Moment Capacities About y-axis
		$\phi N_s$	$\phi N_t$	$\phi M_{sx}$		
	kg/m	kN	kN	kNm	kNm	
125 TFB	13.1	392	392	18.8	22.2 (1-n)	22.2 (1-n)
100 TFB	7.20	214	214	7.98	9.41 (1-n)	9.41 (1-n)

NOTES: (1)  $\phi M_{rx}(\text{comp})$  refers to the design section moment capacity reduced by compression (where  $n = N^*/\phi N_s$ ) and must be less than or equal to  $\phi M_{sx}$ .  
(2)  $\phi M_{rx}(\text{lens})$  refers to the design section moment capacity reduced by tension (where  $n = N^*/\phi N_t$ ) and must be less than or equal to  $\phi M_{sx}$ .  
(3)  $\phi M_{ry}$  refers to the design section moment capacity reduced by axial force (where  $n = N^*/\phi N_s$  or  $N^*/\phi N_t$ ) and must be less than or equal to  $\phi M_{sy}$ .  
(4) The above values of  $\phi N_t$  are based on sections with no holes and  $k_t = 1$ . For other values of  $\phi N_t$  see page 7-15.  
(5) For the design member moment capacity  $\phi M_b$  see page 5-56.  
(6) For the design member capacity in compression (x-axis)  $\phi N_{cx}$  see page 6-38.  
(7) For the design member capacity in compression (y-axis)  $\phi N_{cy}$  see page 6-40.

TABLE 8.1-12(1)  
**EQUAL ANGLES  
GRADE 300**  
**DESIGN SECTION CAPACITIES**

Designation	Design Section Axial Capacities $\phi N_s$	Design Section Moment Capacities About x-axis      About y-axis			
		Load A $\phi M_{sx}$	Load B $\phi M_{sy}$	Load C $\phi M_{ry}$	Load D $\phi M_{rx}$
200 x 200 x 16EA	2470	152	67.3	74.8	380
200 x 200 x 20EA	1930	121	55.0	61.7	315
18EA	1750	108	49.5	57.0	245
16EA	1670	99.7	46.5	55.8	6EA
13EA	1370	76.9	36.7	47.5	260
150 x 150 x 19EA	1350	62.6	27.8	30.9	313
16EA	1220	57.1	25.8	28.9	203
12EA	940	41.9	19.5	23.4	5EA
10EA	769	32.8	15.7	20.8	157
125 x 125 x 16EA	1000	38.6	17.1	19.0	269
12EA	774	29.8	13.6	15.5	224
10EA	661	24.0	11.2	13.8	8EA
8EA	516	18.5	8.84	11.8	175

Notes: (1) The values of  $\phi M_{sx}$  and  $\phi M_{sy}$  depend on the direction of the bending moment. The appropriate value is based on the direction of the load (A, B or D) as shown in the diagram.  
 (2) For all sections  $\phi M_{tx} = \phi M_{sx} (1-n)$  where  $n = N^*/\phi N_s$  or  $N^*/\phi N_c$ .  
 (3) For all sections  $\phi M_{ry} = \phi M_{sy} (1-n)$  where  $n = N^*/\phi N_s$  or  $N^*/\phi N_c$ .  
 (4) The above values of  $\phi N_s$  are based on sections with no holes and  $k_t = 0.85$ .  
 (5) For other values of  $\phi N_s$  see page 7-15.  
 (6) For the design member capacity in compression (x-axis)  $\phi N_{ex}$  see page 6-42.  
 (7) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

TABLE 8.1-12(2)

**EQUAL ANGLES  
GRADE 250**  
**DESIGN SECTION CAPACITIES**

Designation	Design Section Axial Capacities $\phi N_s$	Design Section Moment Capacities About x-axis      About y-axis			
		Load A $\phi M_{sx}$	Load B $\phi M_{sy}$	Load C $\phi M_{ry}$	Load D $\phi M_{rx}$
100 x 100 x 12EA	529	529	16.4	7.29	8.10
100 x 100 x 10EA	424	424	13.2	6.03	6.80
100 x 100 x 8EA	352	352	10.5	4.91	5.83
100 x 100 x 6EA	273	273	7.55	3.63	4.71
90 x 90 x 10EA	380	380	10.7	4.83	5.37
90 x 90 x 8EA	315	315	8.64	4.00	4.62
90 x 90 x 6EA	245	245	6.29	3.01	3.75
75 x 75 x 10EA	313	313	7.15	3.19	3.55
75 x 75 x 8EA	260	260	6.04	2.76	3.07
75 x 75 x 6EA	203	203	4.51	2.13	2.51
75 x 75 x 5EA	157	157	3.21	1.58	2.04
65 x 65 x 10EA	269	269	5.28	2.32	2.57
65 x 65 x 8EA	224	224	4.50	2.01	2.23
65 x 65 x 6EA	175	175	3.52	1.62	1.84
65 x 65 x 5EA	136	136	2.58	1.22	1.50
50 x 50 x 8EA	147	147	2.50	1.44	1.26
50 x 50 x 6EA	114	114	1.89	0.891	1.04
50 x 50 x 5EA	119	119	2.51	1.10	1.22
50 x 50 x 3EA	133	133	2.03	0.917	1.02
50 x 50 x 3EA	104	104	1.58	0.738	0.839
45 x 45 x 6EA	118	118	1.61	0.716	0.796
45 x 45 x 5EA	92.3	92.3	1.29	0.590	0.656
45 x 45 x 3EA	61.4	61.4	0.776	0.378	0.472
40 x 40 x 6EA	104	104	1.24	0.545	0.606
40 x 40 x 5EA	81.5	81.5	0.993	0.452	0.502
40 x 40 x 3EA	54.4	54.4	0.626	0.303	0.364
30 x 30 x 6EA	76.2	76.2	0.641	0.277	0.308
30 x 30 x 5EA	60.0	60.0	0.522	0.232	0.267
30 x 30 x 3EA	40.4	40.4	0.359	0.171	0.190
25 x 25 x 6EA	62.1	62.1	0.417	0.180	0.200
25 x 25 x 5EA	49.2	49.2	0.344	0.150	0.167
25 x 25 x 3EA	33.3	33.3	0.240	0.112	0.125

Notes: (1) The values of  $\phi M_{sx}$  and  $\phi M_{sy}$  depend on the direction of the bending moment. The appropriate value is based on the direction of the load (A, B or D) as shown in the diagram.

(2) For all sections  $\phi M_{tx} = \phi M_{sx} (1-n)$  where  $n = N^*/\phi N_s$  or  $N^*/\phi N_c$ .

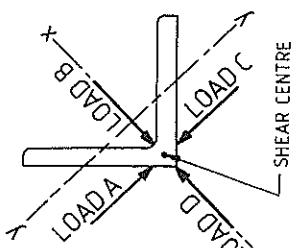
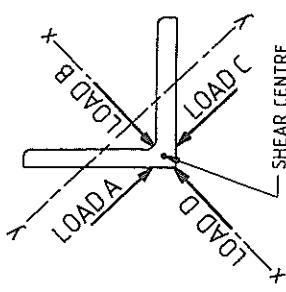
(3) For all sections  $\phi M_{ry} = \phi M_{sy} (1-n)$  where  $n = N^*/\phi N_s$  or  $N^*/\phi N_c$ .

(4) The above values of  $\phi N_s$  are based on sections with no holes and  $k_t = 0.85$  (one leg attached). For other values of  $\phi N_s$  see page 7-15.

(5) For the design member capacity in compression (x-axis)  $\phi N_{ex}$  see page 6-42.

(6) For the design member capacity in compression (y-axis)  $\phi N_{ey}$  see page 6-43.

(7) For other values of  $\phi N_s$  see page 6-45.



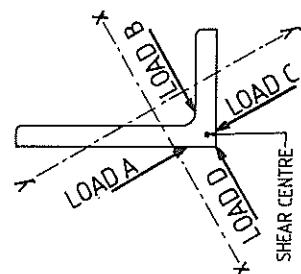


TABLE 8.1-13  
**UNEQUAL ANGLES  
GRADE 300 & 250  
DESIGN SECTION CAPACITIES**

Designation	Design Section Axial Capacities $\phi N_s$ kN	Design Section Moment Capacities			
		About x-axis		About y-axis	
		Load A $\phi M_{sx}$	Load C $\phi M_{sx}$	Load B $\phi M_{sy}$	Load D $\phi M_{sy}$
150 x 100 x 12UA	774	724	27.6	29.8	9.54
10UA	644	579	21.6	23.5	7.48
150 x 90 x 16UA	959	897	35.6	35.8	10.7
12UA	742	693	26.0	28.1	7.78
10UA	617	556	20.3	23.6	6.10
8UA	451	458	15.3	17.4	4.58
125 x 75 x 12UA	529	529	16.3	16.5	4.89
10UA	424	424	12.4	13.4	3.73
8UA	352	352	9.70	11.2	2.91
6UA	238	273	6.88	7.59	2.01
100 x 75 x 10UA	369	369	9.43	9.57	3.82
8UA	306	306	7.51	8.02	3.04
6UA	238	238	5.38	5.47	2.18
75 x 50 x 8UA	215	215	4.05	4.05	1.41
6UA	169	169	3.03	3.21	1.05
5UA	131	131	2.17	2.39	0.758
65 x 50 x 8UA	197	197	3.29	3.29	1.37
6UA	154	154	2.57	2.62	1.07
5UA	120	120	1.88	1.96	0.784
					0.958

Notes: (1) For 150 x 90 angles and above: Grade 300.

(2) For 125 x 75 angles and below: Grade 250.

(3) The values of  $\phi M_{sx}$  and  $\phi M_{sy}$  depend on the direction of the bending moment. The appropriate value is based on the direction of the load (A, B, C or D) as shown in the diagram.

(4) For all sections  $\phi M_{rx} = \phi M_{sx} (1-n)$  where  $n = N^*/\phi N_s$  or  $N^*/\phi N_s$ .

(5) For all sections  $\phi M_{ry} = \phi M_{sy} (1-n)$  where  $n = N^*/\phi N_s$  or  $N^*/\phi N_s$ .

(6) The above values of  $\phi N_s$  are based on sections with no holes and  $k = 0.75$  (short leg attached). For other values of  $\phi N_s$  see page 7-16.

(7) For the design member capacity in compression (x-axis)  $\phi N_{cx}$  see page 6-46.

(8) For the design member capacity in compression (y-axis)  $\phi N_{cy}$  see page 6-47.

(9) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

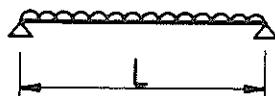
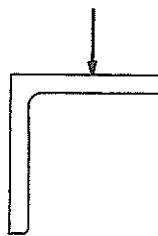


TABLE 8.2-1(1)

**EQUAL ANGLES  
GRADE 300**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
vertical leg down**
 $W_t^*$  Maximum Design Load based on Moment or Shear $W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield $W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass Per m	$W_t^* \text{ (kN)}/W_{S1}^* \text{ (kN)}/W_{S2}^* \text{ (kN)}$ Span in metres									
		1	2	3	4	5	6	7	8	9	10
200 x 200 x 26EA	76.8	681 571	340 285	227 190	170 138	136 88.1	113 61.2	97.2 45.0	85.1 34.4	75.6 27.2	68.1 22.0
20EA	60.1	548 451	274 225	183 160	137 110	110 70.7	91.3 49.1	78.3 36.1	68.5 27.6	60.9 21.8	54.8 17.7
18EA	54.4	490 406	245 205	163 136	123 101	98.1 64.5	81.7 44.8	70.0 32.9	61.3 25.2	54.5 19.9	49.0 16.1
16EA	48.7	457 393	228 197	152 131	114 90.9	91.3 58.2	76.1 40.4	65.2 29.7	57.1 22.7	50.7 18.0	45.7 14.5
13EA	40.0	355 322	177 162	118 106	88.7 75.5	71.0 48.3	59.2 33.6	50.7 24.7	44.4 18.9	39.4 14.9	35.5 12.1
					151	67.1	37.7	24.2	16.8	12.3	9.44
									7.46		6.04
150 x 150 x 19EA	42.1	281 235	140 117	93.6 75.6	70.2 42.5	56.2 27.2	46.8 18.9	40.1 13.9	35.1 10.6	31.2 8.40	28.1 6.80
16EA	35.4	259 213	129 106	86.2 64.7	64.7 36.4	51.7 23.3	43.1 16.2	37.0 11.9	32.3 9.1	28.7 7.19	25.9 5.83
12EA	27.3	192 165	95.9 82.6	64.0 50.9	48.0 28.6	38.4 18.3	32.0 12.7	27.4 9.36	24.0 7.16	21.3 5.66	19.2 4.58
10EA	21.9	152 141	75.9 70.7	50.6 41.3	37.9 23.2	30.3 14.9	25.3 10.3	21.7 7.58	19.0 5.8	16.9 4.58	15.2 3.71
					46.4	20.6	11.6	7.43	5.16	3.79	2.9
									2.29		1.86
125 x 125 x 16EA	29.1	173 145	86.7 72.4	57.8 36.3	43.4 20.4	34.7 13.1	28.9 9.07	24.8 6.67	21.7 5.1	19.3 4.03	
12EA	22.5	135 113	67.7 56.3	45.1 28.7	33.9 16.2	27.1 10.3	22.6 7.18	19.3 5.28	16.9 4.04	15.0 3.19	
10EA	18.0	110 98.7	55.0 48.3	36.6 23.4	27.5 13.1	22.0 8.41	18.3 5.84	15.7 4.29	13.7 3.28	12.2 2.60	
8EA	14.9	85.6 80.2	42.8 40.1	28.5 19.5	21.4 11.0	17.1 7.03	14.3 4.88	12.2 3.59	10.7 2.74	9.51 2.17	
					80.2	22.0	9.76	5.49	3.51	2.44	1.79
									1.37		1.08

Notes: (1) Shading indicates serviceability load governed by yielding.

(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

**FULL LATERAL  
RESTRAINT**

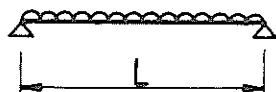
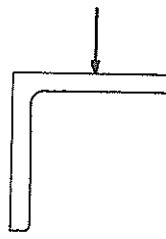


TABLE 8.2-1(2)

**EQUAL ANGLES  
GRADE 250**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
vertical leg down**
 $W_L^*$  Maximum Design Load based on Moment or Shear $W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield $W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass Per m	$W_L^*$ (kN)/ $W_{S1}^*$ (kN)/ $W_{S2}^*$ (kN) Span in metres									
		1	2	3	4	5	6	7	8	9	10
100 x 100 x 12EA	17.7	73.6 61.0 61.0	36.8 30.5 15.9	24.5 14.2 7.08	18.4 5.10 3.99	14.7 3.54 2.55	12.3 2.60 1.77	10.5 1.30			
	14.2	60.0 49.2 49.2	30.0 24.0 13.0	20.0 11.6 5.79	15.0 6.52 3.26	12.0 4.17 2.09	10.0 2.90 1.45	8.57 2.13 1.06			
	11.8	48.3 40.9 40.9	24.1 20.4 10.9	16.1 9.72 4.86	12.1 5.47 2.73	9.66 3.50 1.75	8.05 2.43 1.21				
	9.16	35.0 31.8 31.8	17.5 15.9 8.59	11.7 7.64 3.82	8.74 6.99 2.15	6.99 5.83 1.37	5.83 1.91 0.950				
90 x 90 x 10EA	12.7	48.3 39.4 37.4	24.2 18.7 9.35	16.1 8.31 4.75	12.1 4.67 2.34	9.66 2.99 1.50					
	10.6	39.5 32.8 31.4	19.8 15.7 7.86	13.2 6.98 3.49	9.88 3.93 1.96	7.90 2.51 1.26					
	8.22	29.1 25.5 24.7	14.5 12.4 6.19	9.69 5.50 2.75	7.26 3.09 1.55	5.81 1.98 0.990					
75 x 75 x 10EA	10.5	32.2 26.1 20.9	16.1 10.5 5.23	10.7 4.65 2.33	8.04 2.62 1.31						
	8.73	27.5 22.8 17.7	13.7 8.83 4.42	9.15 3.93 1.96	6.87 2.21 1.10						
	6.81	20.7 17.1 14.0	10.4 6.98 3.49	6.92 3.10 1.55	5.19 1.75 0.873						
	5.27	15.0 13.1 10.9	7.49 5.45 2.73	4.99 2.42 1.21	3.74 1.36 0.681						
65 x 65 x 10EA	9.02	23.5 20.0 13.4	11.8 6.71 3.36	7.85 2.98 1.49							
	7.51	20.3 16.8 11.4	10.1 5.70 2.85	6.75 2.54 1.27							
	5.87	16.0 13.2 9.11	8.02 4.55 2.28	5.35 2.02 1.01							
	4.56	11.9 10.3 7.18	5.94 3.59 1.79	3.96 1.60 0.798							
55 x 55 x 6EA	4.93	11.4 9.27 5.37	5.68 2.69 1.34	3.78 1.19 0.597							
	3.84	8.70 7.24 4.26	4.35 2.13 1.06	2.90 0.946 0.473							
50 x 50 x 8EA	5.68	11.2 9.58 4.93 9.18	5.60 2.46 1.23 4.59								
	4.46	7.67 3.97 7.23 5.92	1.98 0.992 3.62 1.58								
	3.48	3.15 4.36 4.36	0.788 2.18 1.07								
	2.31	2.13	0.533								

FULL LATERAL  
RESTRAINT

Notes: (1) Shading indicates serviceability load governed by yielding.  
(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

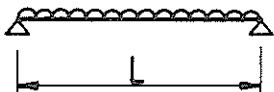
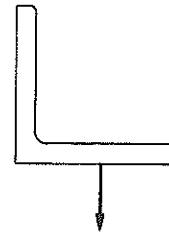


TABLE 8.2-2(1)

**EQUAL ANGLES  
GRADE 300**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
vertical leg up**
 $W_L^*$  Maximum Design Load based on Moment or Shear $W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield $W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass Per m	$W_L^*$ (kN)/ $W_{S1}^*$ (kN)/ $W_{S2}^*$ (kN)									
		Span in metres									
mm mm	kg/m	1	2	3	4	5	6	7	8	9	10
200 x 200 x 26EA	76.8	681	340	227	170	136	113	97.2	85.1	75.6	68.1
		571	285	190	138	88.1	61.2	45.0	34.4	27.2	22.0
		571	275	122	68.8	44.1	30.6	22.5	17.2	13.6	11.0
20EA	60.1	550	275	183	138	110	91.7	78.6	68.8	61.1	55.0
		451	225	150	110	70.7	49.1	36.1	27.6	21.8	17.7
		451	221	98.2	55.2	35.3	24.5	18.0	13.8	10.9	8.84
18EA	54.4	497	248	166	124	99.3	82.8	70.9	62.1	55.2	49.7
		409	205	136	101	64.5	44.8	32.9	25.2	19.9	16.1
		409	202	89.6	50.4	32.3	22.4	16.5	12.6	9.96	8.07
16EA	48.7	469	235	156	117	93.8	78.2	67.0	58.6	52.1	46.9
		398	197	131	90.9	58.2	40.4	29.7	22.7	18.0	14.5
		393	182	80.8	45.5	29.1	20.2	14.8	11.4	8.98	7.27
13EA	40.0	373	187	124	93.4	74.7	62.2	53.3	46.7	41.5	37.3
		324	162	108	75.5	48.3	33.6	24.7	18.9	14.9	12.1
		324	151	67.1	37.7	24.2	16.8	12.3	9.44	7.46	6.04
150 x 150 x 19EA	42.1	281	140	93.6	70.2	56.2	46.8	40.1	35.1	31.2	28.1
		235	117	75.6	42.5	27.2	18.9	13.9	10.6	8.40	6.80
		235	85.1	37.8	21.3	13.6	9.45	6.94	5.32	4.20	3.40
16EA	35.4	259	130	86.4	64.8	51.9	43.2	37.0	32.4	28.8	25.9
		213	106	64.7	36.4	23.3	16.2	11.9	9.10	7.19	5.83
		213	72.8	32.4	18.2	11.7	8.09	5.95	4.55	3.60	2.91
12EA	27.3	197	98.6	65.7	49.3	39.4	32.9	28.2	24.6	21.9	19.7
		166	92.5	50.9	28.6	18.3	12.7	9.36	7.16	5.66	4.58
		166	57.3	25.5	14.3	9.17	6.37	4.68	3.58	2.83	2.29
10EA	21.9	161	80.4	53.6	40.2	32.2	26.8	23.0	20.1	17.9	16.1
		141	70.7	41.3	23.2	14.9	10.3	7.58	5.80	4.58	3.71
		141	46.4	20.6	11.6	7.43	5.16	3.79	2.90	2.29	1.86
125 x 125 x 16EA	29.1	173	86.7	57.8	43.4	34.7	28.9	24.8	21.7	19.3	17.3
		145	72.4	36.3	20.4	13.1	9.07	6.67	5.10	4.03	3.27
		145	40.8	18.1	10.2	6.53	4.54	3.33	2.55	2.02	1.63
12EA	22.5	137	68.4	45.6	34.2	27.4	22.8	19.5	17.1	15.2	13.7
		113	56.3	28.7	16.2	10.3	7.18	5.28	4.04	3.19	2.59
		113	32.3	14.4	8.08	5.17	3.59	2.64	2.02	1.60	1.29
10EA	18.0	114	57.0	38.0	28.5	22.8	19.0	16.3	14.2	12.7	11.4
		96.7	48.3	23.4	13.1	8.41	5.84	4.29	3.28	2.60	2.10
		96.7	26.3	11.7	6.57	4.20	2.92	2.14	1.64	1.30	1.05
8EA	14.9	90.9	45.5	30.3	22.7	18.2	15.2	13.0	11.4	10.1	9.09
		80.2	40.1	19.5	11.0	7.03	4.88	3.59	2.74	2.17	1.76
		80.2	22.0	9.76	5.49	3.51	2.44	1.79	1.37	1.08	0.878

Notes: (1) Shading indicates serviceability load governed by yielding.

(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

**FULL LATERAL  
RESTRAINT**

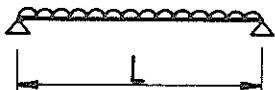
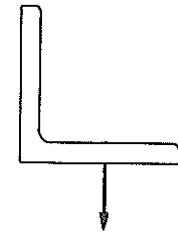


TABLE 8.2-2(2)

**EQUAL ANGLES  
GRADE 250**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
vertical leg up**
 $W_t^*$  Maximum Design Load based on Moment or Shear $W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield $W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass Per m	$W_t^* \text{ (kN)}/W_{S1}^*(\text{kN})/W_{S2}^*(\text{kN})$ Span in metres									
		1	2	3	4	5	6	7	8	9	
100 x 100 x 12EA	17.7	73.6 61.0 61.0 60.3 49.2 49.2 49.4 40.9 36.8 31.8 31.8	36.8 30.5 15.9 20.1 21.6 13.0 24.7 20.4 18.4 15.9 8.59	24.5 14.2 7.08 15.1 11.6 5.79 16.5 9.72 12.3 7.64 3.82	18.4 7.97 3.99 12.1 6.52 3.26 12.3 5.47 9.21 4.30 2.15	14.7 5.10 2.55 10.1 4.17 2.09 9.88 3.50 7.37 2.75 1.37	12.3 3.54 1.77 10.1 2.90 1.45 8.23 2.43 1.21 0.818	10.5 2.60 1.30 8.62 2.13 1.06	9.20 1.99 1.00 7.54 1.63 0.818		
10EA	14.2										
8EA	11.8										
6EA	9.16										
90 x 90 x 10EA	12.7	48.3 39.4 37.4 40.0 32.8 31.4 30.2 29.5 24.7	24.2 18.7 9.35 20.0 15.7 7.86 15.1 12.4 6.19	16.1 8.31 4.15 13.3 6.98 3.49 10.1 5.50 2.75	12.1 4.67 2.34 10.0 3.93 1.96 7.56 3.09 1.55	9.66 2.99 1.50 8.01 2.51 1.26 6.04 1.98 0.990	8.05 2.08 1.04 6.67 1.75 0.870				
8EA	10.6										
6EA	8.22										
75 x 75 x 10EA	10.5	32.2 26.7 20.9 27.5 23.3 17.7 21.2 14.0 15.7 13.2	16.1 10.5 5.23 13.7 8.83 4.42 10.6 6.98 7.86 5.45	10.7 4.65 2.33 9.15 3.93 1.96 7.06 3.10 5.24 2.42	8.04 2.62 1.31 6.87 2.21 1.10 5.29 1.75 3.93 1.36	6.43 1.67 0.84 5.49 1.41 0.710 0.873					
8EA	8.73										
6EA	6.81										
5EA	5.27										
65 x 65 x 10EA	9.02	23.5 20.0 13.4 20.3 16.8 11.4 16.2 9.11 12.3 0.3	11.8 6.71 3.36 10.1 5.70 2.85 8.08 3.49 6.14 3.59	7.85 2.98 1.49 6.75 2.54 1.27 5.39 0.873 4.09 1.60							
8EA	7.51										
6EA	5.87										
5EA	4.56										
55 x 55 x 6EA	4.93	11.4 9.27 5.37 8.84 7.24 4.26	5.68 2.69 1.34 4.42 2.13 1.06	3.78 1.19 0.897 2.95 0.946 0.473							
5EA	3.84										
50 x 50 x 8EA	5.68	11.2 9.58 4.93 9.18 7.57 3.97 7.29 5.92 3.15 4.59 3.92	5.60 2.46 1.23 4.59 1.98 0.992 3.65 1.58 0.788 2.29 1.07 0.533								
6EA	4.46										
5EA	3.48										
3EA	2.31										

**FULL LATERAL  
RESTRAINT**

Note: Shading indicates serviceability load governed by yielding.

TABLE 8.2-3

**UNEQUAL ANGLES  
GRADE 300 & 250**
**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
long leg down**
W<sub>L</sub><sup>\*</sup> Maximum Design Load based on Moment or ShearW<sub>S1</sub><sup>\*</sup>Serviceability Load based on Deflection Limit of Span/250 or First YieldW<sub>S2</sub><sup>\*</sup>Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass Per m	W <sub>L</sub> <sup>*</sup> (kN)/W <sub>S1</sub> <sup>*</sup> (kN)/W <sub>S2</sub> <sup>*</sup> (kN) Span in metres							
		1	2	3	4	5	6	7	8
150 x 100 x 12UA	22.5	184	92.0	61.4	46.0	36.8	30.7	26.3	23.0
		166	77.6	44.5	25.0	16.0	11.1	8.18	6.26
		156	50.1	22.3	12.5	8.01	5.57	4.09	3.13
	18.0	147	73.7	49.1	36.9	29.5	24.6	21.1	18.4
		133	66.4	36.1	20.3	13.0	9.03	6.63	5.08
		133	40.6	18.1	10.2	6.50	4.51	3.32	2.54
150 x 90 x 16UA	27.9	234	117	77.9	58.4	46.8	39.0	33.4	29.2
		196	98.1	54.4	30.6	19.6	13.6	9.99	7.65
		196	61.2	27.2	15.3	9.79	6.80	5.00	3.82
	21.6	183	91.4	61.0	45.7	36.6	30.5	26.1	22.9
		152	76.2	42.9	24.1	15.5	10.7	7.88	6.04
		152	48.3	21.5	12.1	7.73	5.37	3.94	3.02
	17.3	154	76.8	51.2	38.4	30.7	25.6	21.9	19.2
		131	65.3	34.8	19.6	12.5	8.71	6.40	4.90
		131	39.2	17.4	9.80	6.27	4.36	3.20	2.45
	14.3	115	57.5	38.3	28.8	23.0	19.2	16.4	14.4
		108	54.1	29.1	16.4	10.5	7.27	5.34	4.09
		108	32.7	14.5	8.18	5.24	3.64	2.67	2.05
125 x 75 x 12UA	17.7	108	53.9	35.9	26.9	21.5	18.0		
		90.1	45.0	24.2	13.6	8.70	6.04		
		90.1	27.2	12.1	6.79	4.35	3.02		
	14.2	67.2	43.6	29.1	21.8	17.4	14.5		
		72.5	36.3	19.7	11.1	7.90	4.92		
		72.5	22.2	9.84	5.54	3.54	2.46		
	11.8	72.6	36.3	24.2	18.1	14.5	12.1		
		60.2	30.1	16.5	9.27	5.93	4.12		
		60.2	18.5	8.24	4.64	2.97	2.06		
	9.16	50.2	25.1	16.7	12.6	10.0	8.37		
		46.7	23.4	12.9	7.27	4.65	3.23		
		46.7	14.5	6.46	3.64	2.33	1.62		
100 x 75 x 10UA	12.4	55.5	27.8	18.5	13.9	11.1			
		47.1	23.5	10.5	5.93	3.80			
		47.1	11.9	5.27	2.97	1.90			
	10.3	46.5	23.2	15.5	11.6	9.30			
		39.2	19.6	8.86	4.98	3.19			
		39.2	9.97	4.43	2.49	1.59			
	7.98	32.6	16.3	10.9	8.16	6.53			
		30.5	15.2	6.97	3.92	2.51			
		30.5	7.84	3.48	1.96	1.25			
75 x 50 x 8UA	7.23	25.1	12.6	8.37					
		21.3	7.85	3.49					
		15.7	3.93	1.74					
	5.66	19.9	9.94	6.63					
		16.7	6.26	2.78					
		12.5	3.13	1.39					
	4.40	14.9	7.46	4.97					
		13.0	4.93	2.19					
		9.86	2.47	1.10					
65 x 50 x 8UA	6.59	18.8	9.40	6.26					
		16.1	5.23	2.32					
		10.5	2.62	1.16					
	5.16	15.0	7.49	4.99					
		12.7	4.18	1.86					
		8.36	2.09	0.929					
	4.02	11.3	5.66	3.77					
		9.86	3.30	1.47					
		6.60	1.65	0.734					

FULL LATERAL  
RESTRAINT

- Notes: (1) Shading indicates serviceability load governed by yielding.  
(2) For 150 x 90 angles and above: Grade 300.  
(3) For 125 x 75 angles and below: Grade 250.  
(4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

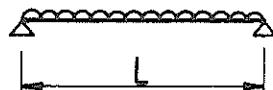
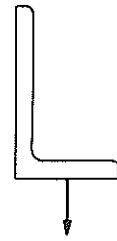


TABLE 8.2-4

**UNEQUAL ANGLES  
GRADE 300 & 250**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
long leg up**
 $W_L^*$  Maximum Design Load based on Moment or Shear $W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield $W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass Per m	$W_L^*/(kN)/W_{S1}^*(kN)/W_{S2}^*(kN)$ Span in metres							
		1	2	3	4	5	6	7	8
150 x 100 x 12UA	22.5	170 155 155	85.1 77.6 50.1	56.8 44.5 22.3	42.6 25.0 12.5	34.1 16.0 8.01	28.4 11.1 5.57	24.3 8.18 4.09	21.3 6.26 3.13
	10UA	18.0	133 133 133	66.5 65.4 40.6	44.3 36.1 18.1	33.2 20.3 10.2	26.6 13.0 6.50	22.2 9.03 4.51	19.0 6.63 3.32
									2.54
150 x 90 x 16UA	27.9	232 196 196 169 152 152 132 131 131 99.1 106	116 98.1 61.2 84.6 78.2 48.3 66.0 65.9 39.2 49.6 54.1 32.7	77.4 54.4 27.2 56.4 42.9 21.5 44.0 34.8 17.4 33.0 29.1 14.5	58.1 30.6 15.3 42.3 24.1 12.1 33.0 19.6 9.80 24.8 16.4 8.18	46.5 19.6 9.79 33.8 15.5 12.1 26.4 12.5 6.27 19.8 10.5 5.24	38.7 13.6 6.80 28.2 10.7 7.73 22.0 8.71 4.36 16.5 7.27 3.64	33.2 9.99 5.00 24.2 7.88 5.37 18.9 6.40 3.20 14.2 5.34 2.67	29.0 7.65 3.82 21.1 6.04 3.02 16.5 4.90 2.45 12.4 4.09 2.05
	12UA	21.6	169 152 152 132	84.6 78.2 48.3 66.0	56.4 42.9 21.5 44.0	42.3 24.1 12.1 33.0	33.8 15.5 7.73 26.4	28.2 10.7 5.37 22.0	24.2 7.88 3.94 18.9
		17.3	132 131 131	66.0 39.2 39.2	44.0 33.0 33.0	33.0 17.4 9.80	26.4 12.5 6.27	22.0 8.71 4.36	16.5 6.40 3.20
	8UA	14.3	99.1 106 106	49.6 54.1 54.1	33.0 29.1 29.1	24.8 16.4 14.5	19.8 10.5 8.18	16.5 7.27 5.24	14.2 12.4 4.09
125 x 75 x 12UA	17.7	106 90.1 90.1 81.0 72.5 72.5 63.0 60.2 60.2 43.3 46.7	53.2 45.0 27.2 40.5 36.9 22.2 31.5 30.1 18.5 21.7 28.1	35.4 24.2 12.1 27.0 19.7 9.84 21.0 16.5 8.24 14.4	26.6 13.6 6.79 20.2 11.1 5.54 15.8 9.27 4.64 10.8	21.3 8.70 4.35 16.2 7.09 3.54 12.6 5.93 2.97 8.67	17.7 6.04 3.02 13.5 4.92 2.46 10.5 4.12 2.06 7.22		
	10UA	14.2	81.0 72.5 72.5 63.0	40.5 36.9 22.2 31.5	27.0 19.7 9.84 21.0	20.2 11.1 5.54 15.8	16.2 11.1 3.54 12.6	13.5 7.09 4.92 10.5	
		11.8	63.0 60.2 60.2 43.3	31.5 30.1 18.5 21.7	21.0 16.5 8.24 14.4	15.8 9.27 4.64 10.8	12.6 5.93 2.97 8.67	10.5 4.12 2.06 7.22	
	6UA	9.16	43.3 46.7 46.7 46.7	21.7 28.1 28.1 14.5	14.4 12.9 12.9 6.46	10.8 7.27 7.27 3.64	7.22 4.65 3.23 2.33	7.22 3.23 3.23 1.62	
100 x 75 x 10UA	12.4	54.9 47.1 47.1 43.5 39.2 39.2 31.1 30.5 30.5	27.3 20.5 11.9 21.8 19.6 9.97 15.6 15.2 7.84	18.2 10.5 5.27 14.5 8.86 4.43 10.4 6.97 3.48	13.7 5.93 2.97 10.9 4.98 2.49 7.78 3.92 1.96	10.9 3.80 1.90 8.71 3.19 1.59 6.23 2.51 1.25			
	8UA	10.3	43.5 39.2 39.2 31.1	21.8 19.6 9.97 15.6	14.5 8.86 4.43 10.4	10.9 4.98 2.49 7.78	8.71 3.19 1.59 6.23		
		7.98	30.5 30.5	15.2 7.84	6.97 3.48	3.92 1.96	2.51 1.25		
	6UA	7.23	25.1 21.3 15.7 18.8 16.7 12.5 13.4 13.0 9.86	12.6 7.85 3.93 9.38 6.26 3.13 6.71 4.93 2.47	8.37 3.49 1.74 6.25 2.78 1.39 4.48 2.19 1.10				
75 x 50 x 8UA	5.66	18.8 16.1 10.5 14.7 12.7 10.7 9.89 6.60	9.40 5.23 2.62 7.33 4.18 2.09 3.30 1.65	6.26 3.22 1.76 4.89 1.86 0.929 1.47 0.734	FULL LATERAL RESTRANT				
	5UA	4.40	13.4 13.0 9.86	6.71 4.93 2.19	4.48 2.19 1.10				
	6UA	6.59	18.8 16.1 10.5 14.7 12.7 8.36 10.7 9.89	9.40 5.23 2.62 7.33 4.18 2.09 5.35 3.30	6.26 3.22 1.76 4.89 1.86 0.929 3.57 1.47				
	5UA	4.02	10.7 9.89	5.35 3.30	3.57 1.47				

Notes: (1) Shading indicates serviceability load governed by yielding.

(2) For 150 x 90 angles and above: Grade 300.

(3) For 125 x 75 angles and below: Grade 250.

(4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

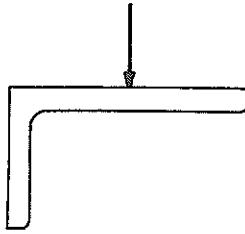
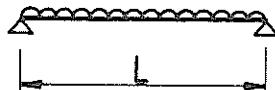


TABLE 8.2-5

# **UNEQUAL ANGLES**

## **GRADE 300 & 250**

## **MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT short leg down**

W<sub>t</sub>\* Maximum Design Load based on Moment or Shear

$W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield

W<sub>s2</sub>\*Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation		Mass Per m	W <sub>L</sub> <sup>+</sup> (kN)/W <sub>S1</sub> <sup>+</sup> (kN)/W <sub>S2</sub> <sup>+</sup> (kN) Span in metres							
			1	2	3	4	5	6	7	8
150 x 100 x 12UA	22.5	81.7	40.9	27.2	20.4	16.3	13.6	11.7	10.2	
		74.1	35.9	16.0	8.98	5.75	3.99	2.93	2.24	
10UA	18.0	71.8	18.0	7.98	4.49	2.87	2.00	1.47	1.12	
		67.4	33.7	22.5	16.9	13.5	11.2	9.63	8.43	
150 x 90 x 16UA	27.9	86.8	43.4	28.9	21.7	17.4	14.5	12.4	10.8	
		76.7	33.1	14.7	8.26	5.29	3.67	2.70	2.07	
12UA	21.6	66.1	16.5	7.35	4.13	2.64	1.84	1.35	1.03	
		66.4	33.2	22.1	16.6	13.3	11.1	9.49	8.30	
10UA	17.3	60.0	26.4	11.7	6.60	4.23	2.93	2.16	1.65	
		52.8	13.2	5.87	3.30	2.11	1.47	1.08	0.825	
8UA	14.3	55.0	27.5	18.3	13.8	11.0	9.17			
		51.6	21.6	9.61	5.40	3.46	2.40			
125 x 75 x 12UA	17.7	29.4	7.36	3.27	1.84	1.18				
		40.0	20.0	13.3	10.0	8.00				
10UA	14.2	31.8	15.9	10.6	7.94	6.35				
		28.5	12.1	5.38	3.03	1.94				
8UA	11.8	24.2	6.06	2.69	1.51	0.969				
		25.8	12.9	8.59	6.44	5.16				
6UA	9.16	23.7	10.2	4.54	2.55	1.63				
		20.4	5.10	2.27	1.28	0.816				
100 x 75 x 10UA	12.4	19.0	9.51	6.34	4.75	3.80				
		18.1	8.05	3.58	2.01	1.29				
8UA	10.3	16.1	4.02	1.79	1.01	0.644				
		31.8	15.9	10.6	7.95	6.36				
6UA	7.98	22.8	11.4	5.07	2.85	1.83				
		26.0	13.0	8.68	6.51	5.21				
75 x 50 x 8UA	7.23	23.1	9.62	4.27	2.40	1.54				
		19.2	4.81	2.14	1.20	0.769				
6UA	5.66	19.5	9.73	6.49	4.87	3.89				
		23.0	7.59	3.38	1.90	1.22				
5UA	4.40	15.2	3.80	1.69	0.949	0.608				
		11.5	5.73	3.82						
6UA	5.66	10.1	2.78	1.24						
		5.56	1.39	0.618						
5UA	4.40	8.89	4.45	2.96						
		7.08	2.23	0.993						
6UA	5.16	4.47	1.12	0.496						
		6.70	3.35	2.23						
5UA	4.02	6.23	1.77	0.787						
		3.54	0.885	0.393						
65 x 50 x 8UA	6.59	11.3	5.67	3.78						
		9.91	2.67	1.19						
6UA	5.16	5.34	1.33	0.593						
		8.98	4.49	2.99						
5UA	4.02	7.04	2.15	0.954						
		4.29	1.07	0.477						
6UA	4.02	6.81	3.41	2.27						
		8.13	1.70	0.757						
5UA	4.02	3.40	0.851	0.378						

FULL LATERAL  
RESTRAINT

Notes: (1) Shading indicates serviceability load governed by yielding.

(2) For 150 x 90 angles and above: Grade 300.

(2) For 150 x 90 angles and above: Grade 300.  
(3) For 125 x 75 angles and below: Grade 250.

(4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

# FULL LATERAL RESTRAINT

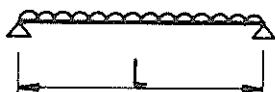
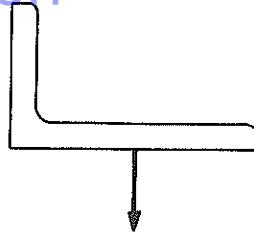


TABLE 8.2-6

**UNEQUAL ANGLES  
GRADE 300 & 250**

**MAXIMUM DESIGN LOADS FOR BEAMS WITH FULL LATERAL RESTRAINT  
short leg up**
W<sub>L</sub>\* Maximum Design Load based on Moment or ShearW<sub>S1</sub>\* Serviceability Load based on Deflection Limit of Span/250 or First YieldW<sub>S2</sub>\* Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass Per m	W <sub>L</sub> * (kN)/W <sub>S1</sub> *(kN)/W <sub>S2</sub> *(kN) Span in metres							
		1	2	3	4	5	6	7	
150 x 100 x 12UA	22.5	81.2 74.1 71.8 64.0 58.7	40.6 35.9 18.0 32.0 29.3	27.1 16.0 7.98 21.3 13.0	20.3 8.98 4.49 16.0 7.33	16.2 5.75 2.87 12.8 4.69	13.5 3.99 2.00 10.7 3.26	11.6 2.93 1.47 9.15 2.39	
	10UA	18.0	64.0 58.7	32.0 14.7	21.3 6.52	16.0 3.67	12.8 2.35	10.7 1.63	
		27.9	86.7 76.7 66.1 65.6 60.0 52.8 52.9 51.6 43.2 39.6 32.9	43.3 33.1 16.5 32.8 26.4 13.2 26.5 21.6 10.8 19.8 18.1	28.9 14.7 7.35 21.9 11.7 5.87 17.6 9.61 4.80 13.2 8.06	21.7 8.26 4.13 16.4 6.60 3.30 13.2 5.40 2.70 9.90 4.54	17.3 5.29 2.64 13.1 4.23 2.11 10.6 3.46 1.73 7.92 2.90	14.4 3.67 1.84 10.9 2.93 1.47 8.82 2.40 1.20 6.60 2.02	12.4 2.70 1.35 9.37 2.16 1.08 7.56 1.76 0.882 5.66 1.48
		21.6	65.6 60.0 52.8 52.9 51.6 43.2 39.6 32.9	32.8 26.4 13.2 26.5 21.6 10.8 19.8 18.1	21.9 11.7 5.87 17.6 9.61 4.80 13.2 8.06	16.4 6.60 3.30 13.2 5.40 2.70 10.6 4.54	13.1 4.23 2.11 10.6 3.46 2.27 8.82 2.40	10.9 2.93 1.47 8.82 2.40 1.45 7.56 1.76	9.37 2.16 1.08 7.56 1.76 1.48 0.882 5.66
		17.3	52.9 51.6 43.2 39.6 32.9	26.5 21.6 10.8 19.8 18.1	17.6 9.61 4.80 13.2 8.06	13.2 5.40 2.70 9.90 4.54	10.6 3.46 1.73 7.92 2.90	8.82 2.40 1.20 6.60 2.02	7.56 1.76 0.882 5.66 1.48
	8UA	14.3	39.6 32.9 24.2 25.2 23.7 20.4 17.3 18.3 15.2	19.8 18.1 6.06 12.6 10.2 5.10 8.66 9.13 7.59	13.2 8.06 2.69 8.41 4.54 2.27 5.77 6.09 3.38	10.6 4.54 1.51 6.30 2.55 1.28 4.33 2.14 1.90	8.82 2.40 0.969 5.04 1.63 0.816 3.46 1.20 0.644	7.56 1.76 0.969 5.04 1.63 0.816 3.46 1.48	0.882 5.66 1.48
		17.7	39.9 35.2 29.4 31.4 28.5 24.2 25.2 23.7 17.3	20.0 14.7 7.36 15.7 12.1 6.06 12.6 10.2 8.66	13.3 6.54 3.27 10.5 5.38 2.69 8.41 4.54 5.77	9.98 3.68 1.84 7.85 3.03 1.51 6.30 2.55 4.33	7.99 2.36 1.18 6.28 1.94 0.969 5.04 1.63 3.46		
		14.2	31.4 28.5 24.2 25.2 23.7 20.4 17.3 18.3 15.2	15.7 12.1 6.06 12.6 10.2 5.10 8.66 9.13 7.59	10.5 5.38 2.69 8.41 4.54 2.27 5.77 6.09 3.38	7.85 3.03 1.51 6.30 2.55 1.28 4.33 2.14 1.90	6.28 1.94 0.969 5.04 1.63 0.816 3.46 1.20 0.644		
		11.8	24.2 25.2 23.7 20.4 17.3 18.3 15.2	12.6 10.2 8.66 5.10 8.66 9.13 7.59	8.41 4.54 2.69 2.27 5.77 6.09 3.80	6.30 2.55 1.51 1.28 4.33 5.04 0.949	5.04 1.63 0.816 3.46 1.20 0.644		
		9.16	20.4 17.3 18.3 15.2	5.10 8.66 9.13 7.59	2.27 5.77 6.09 3.80	1.28 4.33 5.04 0.949			
100 x 75 x 10UA	12.4	31.8 27.8 22.8 26.1 23.1	16.9 11.4 5.70 13.0 9.62	10.6 5.07 2.54 8.69 4.27	7.95 2.85 1.43 6.52 2.40				
	8UA	10.3	22.8 26.1 19.2 18.3 18.0	13.0 9.62 4.81 9.13 7.59	8.69 6.52 2.14 6.09 4.54	6.52 2.40 1.20 4.56 3.46			
		7.98	19.2 18.3 18.0 15.2	4.81 9.13 6.09 3.80	2.14 6.09 4.56 0.949	1.20 4.56 3.46 0.949			
		7.23	11.5 10.1 5.56 8.85 7.99 4.47 6.47 6.23 3.54	5.73 2.78 1.39 4.42 2.23 1.12 3.23 1.77 0.885	3.82 1.24 0.618 2.95 0.993 0.496 2.16 0.787 0.393				
	6UA	5.66	5.56 8.85 7.99 4.47 6.47 6.23 3.54	1.39 4.42 2.23 1.12 3.23 1.77 0.885	0.618 2.95 0.993 0.496 2.16 0.787 0.393				
		4.40	4.47 6.47 6.23 3.54	1.12 3.23 2.16 0.885	0.496 2.16 0.787 0.393				
		7.23	11.5 10.1 5.56 8.85 7.99 4.47 6.47 6.23 3.54	5.73 2.78 1.39 4.42 2.23 1.12 3.23 1.77 0.885	3.82 1.24 0.618 2.95 0.993 0.496 2.16 0.787 0.393				
		6.59	11.3 9.94 5.34 8.99 7.84 4.29 6.67 6.13 3.40	5.67 2.67 1.33 4.49 2.15 1.07 3.33 1.70 0.851	3.78 1.19 0.593 3.00 0.954 0.477 2.22 0.757 0.378				
		5.16	5.34 8.99 7.84 4.29 6.67 6.13 3.40	1.33 4.49 2.15 1.07 3.33 1.70 0.851	0.593 3.00 0.954 0.477 2.22 0.757 0.378				
	5UA	4.02	4.29 6.67 6.13 3.40	1.07 3.33 2.22 0.851	0.477 2.22 0.757 0.378				
		3.54	3.54	0.885	0.393				
		3.02	3.02	0.885	0.378				
<b>FULL LATERAL RESTRAINT</b>									

Notes: (1) Shading indicates serviceability load governed by yielding.

(2) For 150 x 90 angles and above: Grade 300.

(3) For 125 x 75 angles and below: Grade 250.

(4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

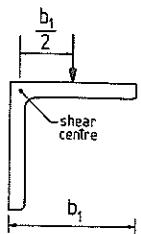
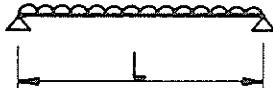


TABLE 8.2-7(1)  
**EQUAL ANGLES  
GRADE 300**

**MAXIMUM DESIGN LOADS FOR BEAMS WITHOUT FULL LATERAL RESTRAINT  
leg down**

$W_L^*$  Maximum Design Load based on Moment or Shear/Torsion  
 $W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield  
 $W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass per metre	$W_L^*/(kN)/W_{S1}^*/(kN)/W_{S2}^*/(kN)$ Span in metres									
		1	2	3	4	5	6	7	8	9	10
200 x 200 x 26EA	76.8	212 212 212 212 133 133 133 109 109 109 94.2 94.2 64.0	209 209 173 173 131 131 131 108 108 108 93.5 93.5 63.6	173 173 78.2 68.2 128 128 61.5 106 99.2 55.6 91.6 62.5	130 87.3 44.3 68.2 35.0 22.5 15.7 76.3 63.5 31.7 88.4 28.3	104 56.3 28.5 44.0 35.0 22.5 15.7 76.3 63.5 20.4 73.1 18.3	86.3 39.3 19.9 30.8 22.5 15.7 11.6 54.4 47.5 14.3 60.8 18.3	73.9 29.0 14.6 22.7 11.6 8.88 11.6 52.2 46.3 10.5 52.0 9.43	64.6 22.2 11.2 17.5 8.88 7.03 8.88 46.3 41.6 8.07 45.5 7.24	57.3 17.6 8.87 13.9 7.03 5.70 13.9 42.2 41.6 6.39 40.4 5.73	51.5 14.3 7.19 11.2 5.70 5.18 10.2 37.9 41.6 6.39 36.2 4.65
20EA	60.1	133 133 133 109 109 94.2 94.2 64.0	131 131 131 108 108 93.5 93.5 63.6	128 128 61.5 106 99.2 55.6 49.5 62.5	105 83.9 69.8 95.6 61.4 39.8 28.3 60.8	59.7 52.2 46.3 47.5 27.8 20.6 42.7 58.5	52.2 46.3 41.6 42.2 15.8 12.6 37.4 49.9	46.3 41.6 41.6 42.2 12.6 10.2 33.2 42.7	46.3 41.6 41.6 42.2 12.6 10.2 29.9 47.2	41.6 37.9 37.9 37.9 10.2 5.70 29.9 3.83	
18EA	54.4	109 109 94.2 94.2 64.0	108 108 93.5 93.5 63.6	106 99.2 91.6 49.5 62.5	95.6 61.4 54.5 28.3 60.8	76.3 39.8 35.4 18.3 58.5	63.5 27.8 24.8 12.8 49.9	54.4 52.2 45.5 9.43 42.7	47.5 42.2 40.4 7.24 37.4	42.2 37.9 40.4 5.73 33.2	37.9 5.70 36.2 4.65 29.9
16EA	48.7	94.2 94.2 64.0	93.5 93.5 63.6	91.6 91.6 62.5	88.4 54.5 49.5	73.1 35.4 28.3	60.8 24.8 18.3	52.0 18.4 9.43	45.5 14.1 7.24	40.4 11.2 5.73	36.2 9.12 4.65
13EA	40.0	64.0 64.0 64.0	63.6 63.6 63.6	62.5 62.5 40.2	60.8 43.8 23.1	58.5 28.6 14.9	49.9 20.1 10.5	42.7 14.9 7.75	37.4 11.5 5.96	33.2 9.14 4.72	29.9 7.44 3.83
150 x 150 x 19EA	42.1	114 114 114 87.6 87.6 87.6 52.9 52.9 36.5 36.5 36.5	107 85.9 54.0 65.8 77.8 45.5 20.5 51.9 51.9 34.8 35.9 35.9 27.4	71.3 47.8 24.3 13.7 40.2 11.6 14.7 49.7 30.5 15.9 34.7 35.9 35.9 12.6	53.4 27.1 13.7 8.83 22.9 11.6 14.7 38.4 17.5 9.02 32.5 26.0 23.8 7.18	42.7 17.5 8.83 39.3 10.3 7.48 10.3 30.6 11.3 5.81 26.0 21.7 13.7 4.65	35.5 12.2 6.14 32.7 7.58 5.21 3.84 25.5 7.91 4.05 21.8 19.0 6.26 3.25	30.4 8.97 4.52 28.0 5.82 3.84 2.94 21.8 5.84 2.99 18.6 16.0 4.64 2.40	26.5 6.88 3.46 24.4 5.82 2.94 2.33 19.0 4.49 2.29 18.6 16.0 3.57 1.84	23.5 5.44 2.74 21.6 4.60 2.33 1.89 16.8 3.56 1.81 16.0 13.9 2.84 1.46	21.1 4.42 2.22 19.4 3.74 1.89 14.8 2.89 1.47 12.2 2.31 1.18
16EA	35.4	87.6 87.6 87.6 52.9 52.9 34.8 36.5 36.5 36.5	85.5 65.8 49.2 20.5 15.9 15.9 34.7 35.9 35.9 27.4	77.8 40.2 22.9 11.6 11.6 9.02 32.5 26.0 21.7 12.6	39.3 32.7 28.0 10.3 11.3 5.81 4.05 21.7 18.6 7.18	32.7 28.0 24.4 10.3 11.3 5.81 4.05 21.7 18.6 7.18	24.4 28.0 21.6 7.58 7.91 4.05 2.99 18.6 16.0 4.64	24.4 21.6 19.4 5.82 5.84 4.05 2.29 18.6 16.0 3.57	21.6 21.6 19.4 4.60 4.49 3.57 1.81 16.0 13.9 2.84	21.6 19.4 19.4 3.74 3.56 3.57 1.47 12.2 12.2 2.31	19.4 2.22 1.89 14.8 3.56 3.57 1.47 12.2 12.2 2.31
12EA	27.3	52.9 52.9 52.9 36.5 36.5 36.5	51.9 51.9 51.9 35.9 35.9 35.9	49.7 38.4 30.6 15.9 34.7 23.8	38.4 30.6 25.5 9.02 32.5 13.7	30.6 25.5 21.8 5.81 26.0 7.18	25.5 21.8 21.8 5.81 21.7 4.65	21.8 19.0 19.0 4.05 18.6 3.25	16.0 13.9 13.9 2.29 18.6 2.40	16.0 13.9 13.9 1.81 16.0 1.84	14.8 14.8 14.8 1.81 12.2 1.46
10EA	21.9	36.5 36.5 36.5	35.9 35.9 35.9	34.7 34.7 23.8	32.5 22.3 17.8	26.0 17.8 14.8	21.7 17.8 12.6	18.6 14.8 12.6	16.0 12.6 10.7	13.9 10.7 9.25	12.2 8.14 8.14
8EA	14.9	35.5 35.5 35.5 24.6 24.6 24.6	34.4 30.6 16.0 24.0 24.0 13.1	29.8 14.0 7.29 22.8 22.8 5.98	22.3 8.03 4.14 18.4 18.4 3.42	17.8 5.19 2.66 14.7 14.7 2.21	17.3 5.19 1.86 12.3 12.3 1.54	14.8 3.63 1.86 10.3 10.3 1.54	12.9 2.68 1.37 8.73 8.73 1.14	11.3 2.06 1.05 7.56 7.56 0.872	9.91 1.65 0.831 6.63 6.63 0.690
125 x 125 x 16EA	29.1	83.9 83.9 83.9 51.2 51.2 35.5 35.5 24.6 24.6	65.9 51.1 26.0 49.3 34.9 30.6 16.0 24.0 13.1	43.9 23.1 11.7 34.9 26.1 14.0 7.29 22.8 5.98	32.9 13.1 6.61 26.1 20.8 8.03 4.14 18.4 5.98	26.2 8.41 4.24 20.8 17.3 5.19 4.14 14.7 4.25	21.8 5.86 2.95 17.3 14.8 5.19 2.66 14.7 2.98	18.6 4.31 2.17 17.3 14.8 3.63 1.86 12.3 2.98	16.2 3.31 1.66 10.3 12.9 2.68 1.37 10.3 2.20	14.4 2.62 1.32 1.03 11.3 1.63 1.05 8.73	12.9 2.12 1.07 0.834 9.91 1.33 0.831 6.63
12EA	22.5	51.2 51.2 51.2 35.5 35.5 24.6 24.6	49.3 39.0 20.2 34.4 30.6 16.0 24.0	34.9 17.7 9.10 29.8 14.0 7.29 22.8	26.1 10.1 5.15 22.3 14.0 7.29 18.4	20.8 6.51 3.31 17.8 8.03 4.14 18.4	17.3 4.54 2.31 14.8 5.19 2.66 14.7	14.8 3.35 1.70 12.9 5.19 1.86 14.7	12.9 2.57 1.30 11.3 12.9 1.37 10.3	11.3 2.04 1.03 9.91 11.3 1.05 8.73	9.91 1.65 0.834 8.14 9.91 1.33 0.831 6.63
10EA	18.0	35.5 35.5 35.5 24.6 24.6 24.6	34.4 30.6 16.0 24.0 24.0 13.1	29.8 14.0 7.29 22.8 22.8 5.98	22.3 14.0 7.29 18.4 18.4 3.42	17.8 5.19 2.66 14.7 14.7 2.21	17.8 3.63 1.86 12.3 12.3 1.54	14.8 2.68 1.37 10.3 10.3 1.14	12.6 2.06 1.05 8.73 8.73 0.872	10.7 1.63 0.831 7.56 7.56 0.690	8.14 1.33 0.831 6.63 6.63 0.560

Notes: (1) Shading indicates serviceability load governed by yielding.

(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

WITHOUT  
FULL LATERAL  
RESTRAINT

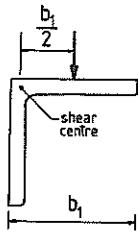
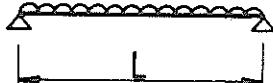


TABLE 8.2-7(2)  
EQUAL ANGLES  
GRADE 250

**MAXIMUM DESIGN LOADS FOR BEAMS WITHOUT FULL LATERAL RESTRAINT**  
**leg down**

$W_L^*$  Maximum Design Load based on Moment or Shear/Torsion

$W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield

$W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass per metre	$W_L^*/W_{S1}^*/W_{S2}^*$ (kN) / Span in metres							
		1	2	3	4	5	6	7	8
100 x 100 x 12EA	17.7	42.3 42.3 39.6	28.0 20.0 10.2	18.7 9.02 4.57	14.0 5.11 2.58	11.1 3.28 1.65	9.25 2.28 1.15	7.90 1.68 0.846	6.88 1.29 0.648
10EA	14.2	27.7 27.7 27.7	23.1 16.0 8.21	15.4 7.22 3.69	11.5 4.10 2.09	9.15 2.64 1.34	7.59 1.84 0.932	6.48 1.36 0.686	5.59 1.04 0.526
8EA	11.8	19.3 18.3 18.3 18.3	18.4 13.0 6.79	12.8 5.94 3.06	9.56 3.38 1.73	7.63 2.18 1.12	6.33 1.52 0.777	5.34 1.12 0.572	4.53 0.863 0.439
6EA	9.16	11.8 11.8 11.8	11.4 9.79 5.19	9.90 4.51 2.36	7.41 2.59 1.35	5.93 1.68 0.867	4.88 4.05 0.605	4.05 0.867 0.446	3.44 0.667 0.342
90 x 90 x 10EA	12.7	27.1 27.1 23.1	18.4 11.7 5.95	12.2 5.26 2.67	9.15 2.98 1.51	7.30 1.92 0.966	6.05 1.33 0.672	5.16 0.980 0.494	4.45 0.751 0.379
8EA	10.6	18.9 18.9 18.9 18.9	15.5 9.58 4.94	10.3 4.34 2.22	7.68 2.47 1.26	6.11 1.59 0.807	5.07 1.11 0.562	4.26 0.816 0.413	3.62 0.626 0.317
6EA	8.22	11.7 11.7 11.7	11.0 7.28 3.81	8.01 3.33 1.73	5.99 1.90 0.980	4.78 1.23 0.630	3.89 0.858 0.439	3.22 0.634 0.323	2.73 0.487 0.248
75 x 75 x 10EA	10.5	24.6 20.1 13.3	12.3 6.69 3.39	8.17 3.00 1.51	6.11 1.69 0.853	4.87 1.09 0.547	4.03 0.756 0.380	3.44 0.556 0.279	
8EA	8.73	18.1 16.8 11.1	10.5 5.56 2.83	6.98 2.50 1.27	5.21 1.42 0.715	4.14 0.908 0.458	3.43 0.632 0.319		
6EA	6.81	11.2 11.2 8.54	8.29 4.29 2.21	5.51 1.94 0.993	4.12 1.10 0.561	3.27 0.709 0.360	2.63 0.494 0.251		
5EA	5.27	6.88 6.88 6.88	6.35 3.25 1.70	4.26 1.48 0.769	3.19 0.846 0.436	2.48 0.546 0.280			
65 x 65 x 10EA	9.02	18.0 14.6 8.66	8.98 4.35 2.19	5.97 1.95 0.979	4.46 1.10 0.552				
8EA	7.51	15.5 12.4 7.25	7.72 3.64 1.84	5.12 1.63 0.823	3.83 0.922 0.464				
6EA	5.87	10.9 9.76 5.67	6.20 2.84 1.45	4.11 1.28 0.650	3.06 0.724 0.367				
5EA	4.56	6.69 6.69 4.36	4.84 2.18 1.13	3.21 0.988 0.507	2.40 0.562 0.287				
55 x 55 x 6EA	4.93	8.69 6.68 3.42 6.39 5.14 2.66	4.33 1.71 0.868 3.43 1.33 0.681	2.87 0.768 0.387 2.28 0.599 0.305					
5EA	3.84								
50 x 50 x 8EA	5.68	8.58 6.37 3.22 7.04 5.01 2.55 5.65 3.88 2.00 2.85 2.49 1.31	4.28 1.61 0.812 3.50 1.28 0.645 2.81 0.998 0.508 1.88 0.655 0.340	2.84 0.720 0.362 2.32 0.572 0.288					
6EA	4.46								
5EA	3.48								
3EA	2.31								

WITHOUT  
FULL LATERAL  
RESTRAINT

Note: Shading indicates serviceability load governed by yielding.

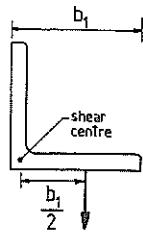
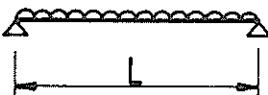


TABLE 8.2-8(1)  
**EQUAL ANGLES  
GRADE 300**

**MAXIMUM DESIGN LOADS FOR BEAMS WITHOUT FULL LATERAL RESTRAINT  
leg up**

$W_L^*$  Maximum Design Load based on Moment or Shear/Torsion

$W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield

$W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass per metre	$W_L^* \text{ (kN)}/W_{S1}^* \text{ (kN)}/W_{S2}^* \text{ (kN)}$ Span in metres									
		1	2	3	4	5	6	7	8	9	10
200 x 200 x 26EA	76.8	207 207	204 184	178 81.5	134 45.8	107 29.3	89.0 20.3	76.2 14.9	66.7 11.4	59.2 8.99	53.3 7.28
20EA	60.1	130 130	129 119	126 66.0	109 36.9	87.5 23.5	72.9 16.3	62.4 11.9	54.6 9.12	48.5 7.20	43.6 5.83
18EA	54.4	108 108	107 103	104 103	98.8 70.3	79.0 44.4	65.8 30.5	56.4 22.3	49.3 17.0	43.7 13.4	39.3 10.8
16EA	48.7	93.0 93.0	92.3 92.3	90.3 90.3	86.7 64.8	74.8 40.7	62.2 27.9	53.3 20.3	46.5 15.4	41.2 12.1	36.9 9.80
13EA	40.0	63.5 63.5	63.0 63.0	61.9 61.9	59.8 57.2	56.6 35.3	49.8 24.0	42.6 17.4	37.2 13.2	32.1 10.3	28.0 8.30
		63.5 63.5	63.0 63.0	47.7 47.7	26.2 16.6	11.4 8.34		6.36 6.36	5.00 5.00		4.04
150 x 150 x 19EA	42.1	111 111	108 97.6	73.5 51.1	55.1 28.6	44.1 18.2	36.7 12.6	31.4 9.24	27.5 7.06	24.4 5.57	21.9 4.51
16EA	35.4	131 85.9	56.7 83.7	25.1 68.7	14.1 51.5	9.01 41.2	6.25 34.3	4.69 29.3	3.51 25.6	2.77 22.7	2.24 20.2
12EA	27.3	85.9 85.9	48.9 48.9	21.6 12.1	24.7 7.71	15.7 5.34	10.8 3.92	7.93 3.92	6.05 3.00	4.77 2.37	3.86 1.92
10EA	21.9	52.3 52.3	51.2 51.2	48.7 36.2	39.3 19.9	31.3 12.6	26.1 8.65	22.2 6.31	19.0 4.81	16.3 3.79	14.2 3.06
		52.3 36.2	39.5 35.6	17.2 34.1	9.62 31.5	6.12 25.7	4.23 21.0	3.10 7.22	2.37 5.24	1.87 3.98	1.51 3.12
		36.2 36.2	35.6 34.6	31.6 31.6	16.9 10.6	10.6 7.95	5.05 3.48	2.54 1.94		1.53 1.53	1.23
125 x 125 x 16EA	29.1	81.9 81.9	68.2 54.3	45.4 24.4	34.1 13.7	27.2 8.71	22.7 6.03	19.4 4.42	16.9 3.38	15.0 2.67	13.4 2.16
12EA	22.5	50.4 50.4	48.4 42.8	36.2 19.6	27.1 10.9	21.7 6.94	18.0 4.79	15.4 3.51	13.1 2.36	11.3 1.73	9.78 1.08
10EA	18.0	50.4 35.2	21.7 33.9	9.56 30.3	5.35 22.7	3.41 18.0	2.36 14.6	1.73 12.0	1.33 9.97	1.05 8.44	0.847 7.26
8EA	14.9	35.2 35.2	18.0 23.7	16.5 22.0	9.07 18.2	5.73 14.2	3.95 11.1	2.88 8.99	2.20 7.42	1.73 6.25	1.40 5.34
		24.4 24.4	23.7 23.7	14.5 15.6	7.86 6.73	4.92 3.73	3.37 2.37	2.45 1.63	1.86 1.20	1.47 0.912	1.18 0.719
		24.4 24.4	15.6 15.6								0.581

Notes: (1) Shading indicates serviceability load governed by yielding.

(2) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

WITHOUT  
FULL LATERAL  
RESTRAINT

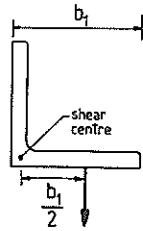
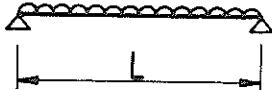


TABLE 8.2-8(2)  
**EQUAL ANGLES  
GRADE 250**

**MAXIMUM DESIGN LOADS FOR BEAMS WITHOUT FULL LATERAL RESTRAINT  
leg up**

$W_L^*$  Maximum Design Load based on Moment or Shear/Torsion

$W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield

$W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass per metre	$W_L^*/(kN)/W_{S1}^*/(kN)/W_{S2}^*/(kN)$ Span in metres								
		1	2	3	4	5	6	7	8	
100 x 100 x 12EA	17.7	41.2 41.2 41.2 41.2 27.3 27.3 27.3 19.1 19.1 11.8 11.8 11.8 11.8	29.0 21.6 10.6 18.0 8.71 3.84 18.1 15.6 7.41 11.2 9.87 5.56 6.04	19.3 9.49 4.68 7.85 3.84 2.15 13.1 6.71 3.25 11.2 7.36 5.63 2.61	14.5 5.31 2.63 4.37 2.78 1.37 9.82 3.72 1.82 9.87 7.36 5.63 1.45	11.6 3.39 1.68 2.78 1.92 1.37 7.82 2.36 1.16 1.90 1.90 1.31 0.922	9.62 2.35 1.17 1.92 1.41 1.19 6.34 1.63 0.801 4.41 4.41 0.637	8.23 1.72 0.856 1.41 1.08 0.698 5.19 1.19 0.587 3.56 3.56 0.466	7.18 1.32 0.655 5.64 4.33 0.534 4.33 0.908 0.449 2.93 2.93 0.356	
90 x 90 x 10EA	12.7	26.6 26.6 25.1 18.7 18.7 18.7 11.5 11.5 6EA	19.2 12.7 6.21 16.0 10.9 5.27 10.8 9.10 4.25	12.8 5.58 2.75 10.6 4.74 2.32 8.08 3.87 1.86	9.57 3.12 1.54 7.96 2.64 1.30 6.02 2.13 1.04	7.64 1.99 0.984 6.34 5.14 0.829 4.62 1.35 0.659	6.35 1.37 0.682 5.14 4.21 0.574 3.61 0.928 0.456	5.36 1.01 0.501 0.383 0.650 0.421 2.91 0.678 0.334	4.52 0.770 0.352 0.650 0.322 2.40 0.518	0.770 0.383 0.281 0.255
75 x 75 x 10EA	10.5	25.0 20.4 13.9 17.8 17.8 11.9 11.1 11.1 5EA	12.6 7.03 3.47 11.0 5.98 2.93 8.50 4.86 9.63	8.43 3.10 1.54 7.29 2.63 1.30 5.65 2.11 2.35	6.31 1.74 0.864 5.46 4.35 0.728 4.22 1.18 1.03	5.04 1.11 0.552 4.35 3.54 0.465 3.23 0.749 0.579	4.19 0.769 0.383 0.649 0.323 0.323 2.54 0.518 0.370	3.57 0.565 0.281 0.256	0.565 0.281	
65 x 65 x 10EA	9.02	18.4 18.4 8.94 16.0 16.0 7.60 10.7 10.7 5EA	9.18 4.50 2.23 7.98 5.31 3.82 6.44 4.28 3.09	6.12 1.99 0.990 3.97 1.69 0.837 4.28 3.20 1.36	4.59 1.12 0.556 3.97 0.945 0.470 3.20 0.757 0.668					
55 x 55 x 6EA	4.93	9.02 7.07 3.59 6.28 6.28 5.00	4.50 1.80 0.889 3.53 2.34 1.45	3.00 0.794 0.394 2.34 0.636 0.313						
50 x 50 x 8EA	5.68	8.74 6.65 3.29 7.26 5.39 2.64 5.85 4.39 2.12 3EA	4.36 1.65 0.821 3.62 1.33 0.657 2.92 1.06 0.524 2.81 1.85 0.756 1.51	2.91 0.731 0.364 2.41 0.586 0.291 1.06 0.605 0.297						

Note: Shading indicates serviceability load governed by yielding.

**WITHOUT  
FULL LATERAL  
RESTRAINT**

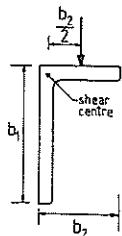


TABLE 8.2-9

**UNEQUAL ANGLES  
GRADE 300 & 250**
**MAXIMUM DESIGN LOADS FOR BEAMS WITHOUT FULL LATERAL RESTRAINT  
long leg down**

$W_L^*$  Maximum Design Load based on Moment or Shear/Torsion  
 $W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield  
 $W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass per metre	$W_L^*/(kN)/W_{S1}^*(kN)/W_{S2}^*(kN)$ Span in metres							
		1	2	3	4	5	6	7	8
150 x 100 x 12UA	22.5	59.7	53.5	35.4	26.3	20.8	17.0	13.9	11.6
		59.7	48.0	26.3	15.1	9.81	6.87	5.08	3.91
10UA	18.0	59.7	30.4	13.9	7.92	5.12	3.57	2.63	2.02
		42.3	40.0	28.4	21.0	16.4	12.9	10.4	8.64
150 x 90 x 16UA	27.9	96.2	66.3	43.9	32.6	25.8	21.2	17.8	14.9
		96.2	66.7	34.1	19.5	12.6	8.80	6.49	4.99
12UA	21.6	96.2	39.1	17.7	10.1	6.48	4.51	3.32	2.55
		61.4	50.1	33.1	24.4	19.2	15.3	12.4	10.3
10UA	17.3	61.4	45.4	25.4	14.6	9.49	6.65	4.92	3.79
		61.4	29.5	13.5	7.70	4.97	3.48	2.56	1.97
8UA	14.3	43.8	40.5	26.8	19.7	14.9	11.5	9.24	7.60
		43.8	36.8	19.4	11.3	7.37	5.18	3.85	2.97
125 x 75 x 12UA	17.7	49.6	30.4	20.1	14.9	11.7	9.60	7.81	6.50
		49.6	27.0	15.0	8.58	5.54	3.87	2.86	2.19
10UA	14.2	49.6	17.3	7.83	4.44	2.86	1.99	1.47	1.12
		33.7	23.9	15.7	11.6	9.04	7.08	5.71	4.70
8UA	11.8	33.7	21.7	11.7	6.71	4.35	3.04	2.25	1.73
		33.7	13.6	6.20	3.53	2.28	1.59	1.17	0.900
6UA	9.16	23.9	19.3	12.7	9.27	6.95	5.38	4.31	3.54
		23.9	17.9	9.33	5.39	3.51	2.47	1.83	1.41
100 x 75 x 10UA	12.4	29.5	17.8	11.8	8.73	6.90	5.69	4.66	3.88
		29.5	14.5	6.56	3.73	2.40	1.68	1.24	0.948
8UA	10.3	28.7	7.50	3.37	1.91	1.23	0.854	0.628	0.482
		21.0	14.6	9.65	7.14	5.64	4.46	3.61	3.00
6UA	7.98	21.0	11.7	5.36	3.06	1.98	1.38	1.02	0.783
		21.0	6.16	2.79	1.58	1.02	0.710	0.523	0.401
75 x 50 x 8UA	7.20	13.1	10.6	6.98	5.17	3.96	3.10	2.50	2.07
		13.1	8.70	4.04	2.32	1.51	1.06	0.781	0.600
		13.1	4.69	2.14	1.22	0.789	0.551	0.406	0.312
6UA	5.63	15.2	7.51	4.93	3.63	2.76	2.15	1.73	1.42
		15.2	4.97	2.24	1.27	0.816	0.568	0.418	0.321
5UA	4.37	9.93	2.56	1.15	0.647	0.415	0.289	0.212	0.163
		11.7	5.77	3.77	2.68	1.96	1.51	1.21	
5UA		10.8	3.81	1.73	0.963	0.634	0.442	0.326	
		7.64	1.99	0.897	0.507	0.326	0.227	0.167	
65 x 50 x 8UA	6.59	7.77	4.28	2.75	1.87	1.36	1.04		
		7.77	2.86	1.31	0.750	0.485	0.339		
		5.76	1.53	0.692	0.393	0.253	0.177		
		12.5	6.20	4.09	3.02	2.39			
		10.7	3.36	1.51	0.850	0.546			
		6.70	1.71	0.762	0.430	0.275			
		9.77	4.83	3.17	2.34				
		8.44	2.60	1.17	0.665				
		5.21	1.34	0.600	0.339				
		7.13	3.64	2.38	1.66				
		6.51	1.98	0.901	0.513				
		3.98	1.04	0.467	0.264				

**WITHOUT**  
**FULL LATERAL**  
**RESTRAINT**

Notes: (1) For 150 x 90 angles and above: Grade 300.  
 (2) For 125 x 75 angles and below: Grade 250.  
 (3) Shading indicates serviceability load governed by yielding.  
 (4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

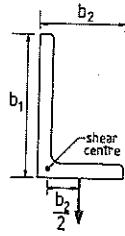
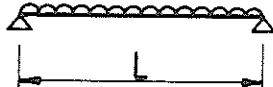


TABLE 8.2-10

**UNEQUAL ANGLES  
GRADE 300 & 250**
**MAXIMUM DESIGN LOADS FOR BEAMS WITHOUT FULL LATERAL RESTRAINT  
long leg up**
 $W_L^*$  Maximum Design Load based on Moment or Shear/Torsion $W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield $W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass per metre	$W_L^* \text{ (kN)}/W_{S1}^* \text{ (kN)}/W_{S2}^* \text{ (kN)}$ Span in metres							
		1	2	3	4	5	6	7	8
150 x 100 x 12UA	22.5	60.1	56.8	37.8	28.2	22.5	18.1	14.7	12.1
		60.1	56.8	32.6	17.8	11.2	7.72	5.64	4.29
10UA	18.0	60.1	35.4	15.4	8.58	5.45	3.77	2.76	2.11
		42.3	40.4	30.2	23.0	17.4	13.4	10.7	8.76
150 x 90 x 16UA	27.9	99.4	72.5	48.3	36.0	28.7	23.8	19.5	16.2
		99.4	50.9	38.9	21.6	13.7	9.46	6.92	5.28
12UA	21.6	99.4	42.8	18.9	10.6	6.73	4.66	3.42	2.61
		62.3	54.2	36.0	26.9	21.2	16.5	13.3	10.9
10UA	17.3	62.3	48.4	31.9	17.4	11.0	7.53	5.50	4.18
		62.3	34.6	15.0	8.38	5.32	3.68	2.69	2.05
8UA	14.3	44.1	41.7	29.5	21.6	15.8	12.1	9.63	7.81
		44.1	41.7	27.8	14.8	9.21	6.28	4.55	3.45
8UA	14.3	44.1	29.5	12.6	6.93	4.38	3.02	2.20	1.68
		30.9	29.5	23.5	16.2	11.6	8.83	6.94	5.59
8UA	14.3	30.9	29.5	23.5	13.3	8.10	5.45	3.92	2.95
		30.9	26.5	10.9	5.95	3.73	2.55	1.86	1.41
125 x 75 x 12UA	17.7	50.9	33.2	22.0	16.5	13.1	10.5	8.49	7.02
		50.9	28.1	17.2	9.53	6.05	4.17	3.05	2.33
10UA	14.2	50.9	19.0	8.34	4.66	2.97	2.06	1.51	1.15
		34.1	25.8	17.1	12.8	9.77	7.59	6.07	4.97
8UA	11.8	34.1	23.0	14.5	7.91	4.98	3.43	2.50	1.91
		34.1	15.8	6.86	3.82	2.43	1.68	1.23	0.938
6UA	9.16	24.1	20.7	13.7	10.1	7.39	5.68	4.50	3.65
		24.1	19.4	12.7	6.85	4.28	2.92	2.12	1.62
6UA	9.16	24.1	13.7	5.87	3.24	2.05	1.42	1.03	0.799
		15.0	14.2	10.1	6.85	4.94	3.74	2.93	2.36
100 x 75 x 10UA	12.4	15.0	14.2	10.1	5.86	3.57	2.41	1.73	1.31
		15.0	11.8	4.85	2.64	1.66	1.13	0.826	0.629
8UA	10.3	29.6	18.9	12.6	9.40	7.50	6.04	4.89	4.05
		29.6	16.0	7.24	4.02	2.56	1.77	1.29	0.989
6UA	7.98	29.6	8.03	3.53	1.98	1.26	0.875	0.642	0.491
		20.9	15.3	10.2	7.59	5.88	4.59	3.69	3.04
5UA	4.37	20.9	14.5	6.19	3.42	2.17	1.50	1.09	0.833
		20.9	6.82	2.99	1.67	1.06	0.735	0.539	0.412
5UA	4.37	13.1	11.3	7.50	5.49	4.04	3.10	2.47	2.01
		13.1	10.7	5.12	2.79	1.75	1.20	0.874	0.666
75 x 50 x 8UA	7.20	13.1	5.57	2.40	1.34	0.847	0.584	0.427	0.326
		16.3	8.13	5.38	4.01	2.97	2.29	1.83	1.49
6UA	5.63	16.3	5.46	2.40	1.34	0.853	0.590	0.433	0.331
		10.9	2.67	1.18	0.662	0.423	0.293	0.215	0.165
5UA	4.37	12.4	6.18	4.09	2.83	2.06	1.57	1.24	
		11.0	4.47	1.94	1.07	0.682	0.471	0.345	
5UA	4.37	8.85	2.15	0.944	0.528	0.337	0.233	0.171	
		7.82	4.58	2.89	1.93	1.38	1.04		
5UA	4.37	7.82	3.71	1.57	0.865	0.547	0.377		
		7.38	1.73	0.756	0.421	0.267	0.185		
65 x 50 x 8UA	6.59	13.0	6.51	4.33	3.23	2.51			
		11.0	3.55	1.57	0.877	0.560			
6UA	5.16	7.07	1.75	0.776	0.436	0.279			
		10.3	5.14	3.40	2.45				
5UA	4.02	8.73	2.87	1.26	0.702				
		5.70	1.40	0.619	0.347				
5UA	4.02	7.11	3.84	2.51	1.69				
		6.92	2.34	1.01	0.561				
		4.65	1.12	0.493	0.275				

**WITHOUT  
FULL LATERAL  
RESTRAINT**

- Notes: (1) For 150 x 90 angles and above: Grade 300.  
(2) For 125 x 75 angles and below: Grade 250.  
(3) Shading indicates serviceability load governed by yielding.  
(4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

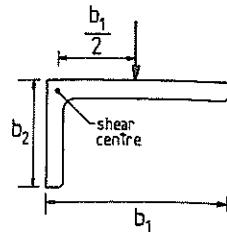
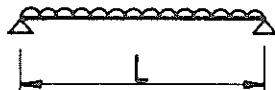


TABLE 8.2-11

**UNEQUAL ANGLES  
GRADE 300 & 250**
**MAXIMUM DESIGN LOADS FOR BEAMS WITHOUT FULL LATERAL RESTRAINT  
short leg down**
 $W_L^*$  Maximum Design Load based on Moment or Shear/Torsion $W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield $W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass per metre	$W_L^*/(kN)/W_{S1}^*/(kN)/W_{S2}^*/(kN)$ Span in metres								
		1	2	3	4	5	6	7	8	
150 x 100 x 12UA	22.5	40.6 40.6 40.6 28.5 28.5 26.5	38.5 23.0 11.6 26.0 18.4 9.39	25.6 10.3 5.21 22.0 8.31 4.21	19.2 5.84 2.94 16.5 4.71 2.38	15.4 3.75 1.88 13.2 3.03 1.53	12.8 2.61 1.31 11.0 2.11 1.06	11.0 1.92 0.963 9.45 1.55 0.781	9.63 1.47 0.738 8.28 1.19 0.599	
	18.0									
150 x 90 x 16UA	27.9	64.9 63.3 43.6 39.9 39.9 34.1 27.9 27.9	41.0 22.0 11.1 31.9 17.2 8.70 27.3 13.9	27.3 9.85 4.94 21.3 7.73 3.89 18.2 6.25	20.5 5.55 2.78 15.9 4.36 2.19 13.7 3.53	16.4 3.56 1.78 12.8 2.80 1.40 11.0 2.27	13.7 2.47 1.24 10.6 1.95 0.976 9.14 1.58	11.7 1.82 0.909 9.12 1.43 0.717 7.84 1.16	10.3 1.39 0.696 7.98 1.10 0.550 6.88 0.890	
	21.6									
10UA	17.3	27.9 27.9 27.9 19.4 19.4 19.4	27.3 8.70 13.9 7.04 19.2 11.5	18.2 3.89 6.25 3.15 11.4 5.19	13.7 2.19 3.53 1.78 11.4 2.94	11.0 1.40 2.27 1.14 9.11 1.89	9.14 0.976 0.793 7.60 6.52 1.32	7.84 0.717 0.583 5.72 0.969 0.743	6.88 0.550 0.447 5.72 0.743 0.374	
	14.3									
125 x 75 x 12UA	17.7	33.1 29.1 19.4 21.8 21.8 15.7 15.3 15.3 13.0 9.41 9.41	18.9 9.75 4.90 15.2 7.90 3.98 12.6 6.58 3.33 9.27 5.10 2.60	12.6 4.36 2.19 10.1 3.54 1.78 8.42 2.95 1.49 6.54 2.30 1.16	9.44 2.46 1.23 7.61 6.09 1.00 6.32 4.22 0.838 4.91 0.836 0.657	7.55 1.57 0.789 6.09 5.07 0.642 5.06 4.22 0.537 3.93 0.836 0.421	6.29 1.09 0.547 5.07 4.35 0.446 5.06 3.62 0.547 3.28 0.582 0.293	5.40 0.804 0.402 4.35 3.81 0.654 0.501 0.251	4.72 0.616 0.308 3.81 0.547 0.251	
	14.2									
8UA	11.8	15.3 15.3 13.0 9.41 9.41	12.6 6.58 3.33 9.27 5.10	8.42 2.95 1.49 6.54 2.30	6.32 1.67 0.838 4.91 1.30	5.06 1.07 0.537 3.93 0.836	4.22 0.744 0.374 3.28 0.582	3.62 0.547 0.275	3.62 0.547 0.275	
	9.16									
6UA	7.98	9.52 9.52 9.34	9.16 4.70 2.40	6.11 2.12 1.08	4.59 1.20 0.608	3.68 0.772 0.390				
100 x 75 x 10UA	12.4	21.3 21.3 14.5 15.2 15.2 6.07 12.1 9.52 9.52	14.3 7.30 3.69 11.8 11.8 2.73 3.08 9.16 4.70	9.51 3.27 1.65 7.89 5.92 1.54 1.38 6.11 2.12	7.13 1.85 0.928 5.92 4.73 0.777 0.498 4.59 1.20	5.70 1.18 0.595 4.73 3.68 0.772				
	10.3									
8UA	7.98	12.1 9.52 9.52	3.08 4.70 2.40	1.38 2.12 1.08	0.777 0.327 0.258	0.498 0.184				
75 x 50 x 8UA	7.20	10.6 7.27 3.67 8.34 5.74 2.91 5.37 4.47 2.28	5.30 1.84 0.923 4.17 1.46 0.734 3.25 1.14 0.578	3.53 0.820 0.411 2.78 0.651 0.327 2.17 0.512 0.258	2.65 0.462 0.231 2.09 0.367 0.184	2.12 0.296 0.148				
	5.63									
6UA	4.37									
5UA	4.37									
65 x 50 x 8UA	6.59	10.1 6.91 3.49 8.01 5.44 2.76 5.34 4.22	5.06 1.75 0.878 4.00 1.38 0.697 3.11 1.08							
	5.16									
6UA	4.02									
5UA	4.02									

**WITHOUT  
FULL LATERAL  
RESTRAINT**

- Notes: (1) For 150 x 90 angles and above: Grade 300.  
 (2) For 125 x 75 angles and below: Grade 250.  
 (3) Shading indicates serviceability load governed by yielding.  
 (4) Grade 300 refers to BHP Grade 300 PLUA™. See Note (1) on page 2-2.

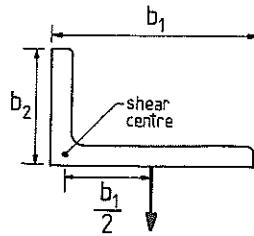
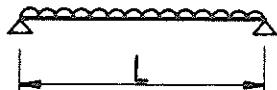


TABLE 8.2-12

**UNEQUAL ANGLES  
GRADE 300 & 250**
**MAXIMUM DESIGN LOADS FOR BEAMS WITHOUT FULL LATERAL RESTRAINT  
short leg up**
 $W_L^*$  Maximum Design Load based on Moment or Shear/Torsion $W_{S1}^*$  Serviceability Load based on Deflection Limit of Span/250 or First Yield $W_{S2}^*$  Serviceability Load based on Deflection Limit of Span/500 or First Yield

Designation	Mass per metre	$W_L^*/(kN)/W_{S1}^*/(kN)/W_{S2}^*/(kN)$ Span in metres							
		1	2	3	4	5	6	7	8
150 x 100 x 12UA	22.5	40.4 40.4 40.4 28.4 28.4	36.7 24.4 12.0 27.6 9.84	24.5 10.7 5.31 19.3 4.35	18.3 6.01 2.98 14.5 2.44	14.5 3.75 1.88 11.3 1.53	12.2 2.66 1.32 9.64 1.08	10.5 1.95 0.971 8.25 0.792	9.15 1.49 0.743 7.19 0.606
		10UA	18.0						
150 x 90 x 16UA	27.9	64.3 44.5 39.7 35.4 27.8 27.8 19.3	40.9 22.5 11.2 30.1 17.9 8.87 18.0	27.3 9.99 4.98 20.1 7.93 3.94 12.0	20.5 5.62 2.80 15.1 4.45 2.21 8.99	16.3 3.56 1.78 11.9 2.80 1.40 7.06	13.6 2.49 1.25 10.0 1.97 0.982 5.98	11.7 1.83 0.915 8.60 1.45 0.722 5.12	10.2 1.40 0.700 7.52 1.11 0.552 4.40
		12UA	21.6						
10UA	17.3	39.7 35.4 27.8 27.8 19.3	30.1 8.87 23.9 7.27 18.0	15.9 3.94 15.9 3.22 12.0	11.9 2.21 1.40 1.81 8.99	9.39 1.40 9.39 1.14 7.06	7.94 0.982 0.722 0.802 5.98	6.80 0.722 0.552 0.450 5.12	5.93 0.905 0.450 4.40 0.758
		8UA	14.3						
125 x 75 x 12UA	17.7	32.8 29.3 19.8 21.7 21.7 16.2 15.2 15.2 13.8 9.36	18.8 9.98 4.96 14.4 8.19 4.06 11.4 6.94 3.06 7.57	12.5 4.42 2.20 9.61 3.62 1.80 7.57 5.68 1.71 5.68	9.38 2.48 1.24 7.21 2.03 1.01 1.01 4.48 1.07 4.48	7.47 1.57 0.789 5.72 1.28 0.642 0.642 3.78 0.758 3.78	6.25 1.10 0.551 4.80 0.901 0.449 0.449 0.556 0.377 0.556	5.36 0.810 0.405 4.80 0.661 0.330 0.330 3.23 0.277 3.23	4.69 0.620 0.310 3.60 0.506 0.252 0.252
		10UA	14.2						
8UA	11.8	21.7 16.2 15.2 15.2 13.8 9.36	8.19 4.06 11.4 6.94 3.06 7.85	3.62 1.80 7.57 5.68 1.71 5.24	2.03 1.80 1.01 1.07 0.850 3.93	1.28 0.642 0.642 0.537 0.537 3.93	0.901 0.449 0.449 0.377 0.377 3.08	0.661 0.330 0.330 0.277 0.277 2.61	0.506 0.252 0.252 0.252 0.252 0.600
		6UA	9.16						
100 x 75 x 10UA	12.4	21.3 21.3 15.1 15.1 15.1 12.8 9.51 9.51	14.3 7.62 3.77 11.6 6.46 3.18 8.24 5.21 2.53	9.53 3.36 1.67 7.70 2.84 1.41 5.49 2.27 1.11	7.15 1.89 0.938 5.77 1.59 0.789 4.12 1.27 0.624	5.64 1.18 0.595 4.52 0.990 0.498 3.21 0.773 0.421	5.36 0.810 0.405 3.60 0.661 0.556 0.277 0.277 0.298	4.69 0.620 0.310 3.60 0.506 0.252 0.252 0.252 0.252	
		8UA	10.3						
6UA	7.98	15.1 12.8 9.51 9.51	11.6 3.18 8.24 5.21	7.70 1.41 5.49 2.27	5.77 0.789 4.12 1.27	4.52 0.498 3.21 0.773	4.80 0.990 0.498 0.773	4.80 0.990 0.498 0.773	
		6UA	7.98						
75 x 50 x 8UA	7.20	10.7 7.52 3.73 8.06 6.07 2.99 5.32 4.91 2.39	5.33 1.87 0.931 4.03 1.50 0.744 2.92 1.20 0.591	3.55 0.829 0.413 2.68 0.664 0.330 1.95 0.529 0.262	2.66 0.466 0.232 2.01 0.372 0.186	2.12 0.296 0.148	2.12 0.296 0.148	2.12 0.296 0.148	
		6UA	5.63						
5UA	4.37	8.06 6.07 2.99 5.32 4.91 2.39	4.03 1.50 0.744 2.92 1.20 0.591	2.68 0.664 0.330 1.95 0.529 0.262	2.01 0.372 0.186	2.01 0.372 0.186	2.01 0.372 0.186	2.01 0.372 0.186	
		5UA	4.37						
65 x 50 x 8UA	6.59	10.2 7.17 3.55 8.02 5.79 2.84 5.30 4.69 2.27	5.10 1.78 0.886 4.01 1.43 0.708 2.96 1.14 0.562	shear centre					
		6UA	5.16						
5UA	4.02	5.30 4.69 2.27	2.96 1.14 0.562						
		5UA	4.02						

**WITHOUT  
FULL LATERAL  
RESTRAINT**

- Notes: (1) For 150 x 90 angles and above: Grade 300.  
 (2) For 125 x 75 angles and below: Grade 250.  
 (3) Shading indicates serviceability load governed by yielding.  
 (4) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

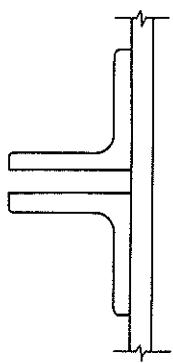


TABLE 8.3-1(1)

**EQUAL ANGLES  
GRADE 300**

**MAXIMUM DESIGN LOADS FOR ECCENTRICALLY LOADED SINGLE ANGLES IN TRUSSES**  
angles on the same side of the truss chord

Designation	Maximum Design Loads (kN)																	
	Length in metres																	
	0.25	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	5.5	6.0	7.0	8.0	9.0	10	11
200 x 200 x 26EA	903	903	891	863	835	806	776	743	709	672	635	598	562	494	433	381	336	297
20EA	717	717	701	677	652	627	601	574	546	517	487	458	430	377	331	291	256	227
18EA	646	646	629	606	583	559	535	510	485	459	432	406	381	334	293	257	227	201
16EA	610	609	588	564	539	515	490	465	440	414	388	364	340	296	259	227	200	177
13EA	482	479	460	438	416	396	375	354	334	313	283	274	256	223	195	171	151	134
150 x 150 x 19EA	496	479	458	436	413	388	361	334	307	282	259	237	200	169	145	125	108	90.8
16EA	452	451	431	409	387	364	340	314	289	264	241	220	201	169	143	122	105	90.8
12EA	342	338	321	302	284	266	247	227	208	190	174	159	145	122	103	88.1	76.0	66.1
10EA	269	263	245	226	208	191	174	159	145	132	121	110	101	85.2	72.6	62.4	54.2	47.4
125 x 125 x 16EA	367	366	347	327	306	282	257	232	209	187	168	151	136	112	92.7	77.8	66.2	56.8
12EA	285	282	265	248	231	212	193	174	156	140	125	113	101	83.3	69.2	58.3	49.6	42.7
10EA	237	231	215	198	182	166	149	133	119	106	95.2	85.4	76.9	63.1	52.5	44.3	37.8	32.6
8EA	180	175	159	144	130	117	105	93.7	83.9	75.3	67.7	61.1	55.4	45.9	38.5	32.8	28.2	24.5

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

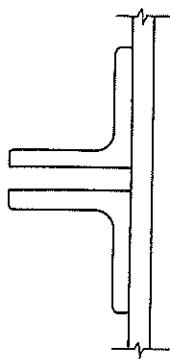


TABLE 8.3-1(2)

**EQUAL ANGLES  
GRADE 250**
**MAXIMUM DESIGN LOADS FOR ECCENTRICALLY LOADED SINGLE ANGLES IN TRUSSES**  
 angles on the same side of the truss chord

Designation	Maximum Design Loads (kN)									
	Length in metres									
	0.25	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
100 x 100 x 12EA	194	192	180	168	154	139	124	109	96.2	84.9
10EA	157	154	144	133	121	109	96.8	85.3	75.2	66.3
8EA	129	125	116	106	96.5	86.4	76.5	67.3	59.3	52.3
6EA	94.9	91.5	83.5	75.7	68.1	60.5	53.4	46.9	41.3	36.5
90 x 90 x 10EA	141	138	128	117	105	92.8	80.9	70.3	61.1	53.3
8EA	116	113	104	94.5	84.6	74.4	64.8	56.2	48.8	42.6
6EA	87.3	84.0	76.2	68.6	60.9	53.3	46.3	40.1	34.9	30.5
75 x 75 x 10EA	115	111	102	91.3	79.3	67.4	57.0	48.2	41.0	35.1
8EA	96.8	93.1	84.7	75.4	65.2	55.3	46.6	39.4	33.5	28.7
6EA	74.2	70.9	63.6	56.1	48.2	40.8	34.4	29.1	24.7	21.2
5EA	54.7	51.7	45.6	39.7	33.8	28.5	24.0	20.3	17.3	14.9
65 x 65 x 10EA	97.6	94.0	85.0	74.1	62.2	51.4	43.4	35.2	29.5	25.0
8EA	82.4	78.1	68.4	58.3	48.7	40.4	33.6	28.1	23.7	20.1
6EA	64.6	61.3	54.4	46.8	39.0	32.1	26.4	22.0	18.4	15.6
5EA	48.5	45.6	39.9	33.9	28.1	23.1	19.1	15.9	13.3	11.4
55 x 55 x 6EA	54.0	50.9	44.2	36.5	29.1	23.1	18.6	15.1	12.5	10.4
5EA	41.5	38.3	31.9	25.8	20.6	16.5	13.3	10.9	9.09	7.65
50 x 50 x 8EA	60.8	57.4	49.5	39.9	31.1	24.2	19.2	15.4	12.6	10.4
6EA	48.4	45.4	38.8	31.0	24.1	18.8	14.9	12.0	9.80	8.15
5EA	37.7	34.6	28.3	22.3	17.4	13.7	10.9	8.84	7.28	6.08
3EA	23.3	21.3	17.3	13.5	10.4	8.16	6.50	5.28	4.36	3.66
45 x 45 x 6EA	42.5	39.7	33.1	25.5	19.3	14.7	11.5	9.15	7.42	6.13
5EA	33.5	31.1	25.5	19.6	14.7	11.3	8.79	7.00	5.69	4.71
3EA	21.1	19.2	15.3	11.6	8.72	6.68	5.24	4.21	3.44	2.87
40 x 40 x 6EA	37.0	34.3	27.5	20.3	14.9	11.1	8.52	6.70	5.39	4.42
5EA	29.3	26.9	21.3	15.7	11.4	8.56	6.58	5.18	4.17	3.43
3EA	19.0	17.1	13.2	9.61	7.02	5.26	4.06	3.22	2.61	2.15
30 x 30 x 6EA	26.1	23.5	16.4	10.8	7.32	5.21	3.87	2.97	2.35	1.90
5EA	20.5	17.8	12.2	8.15	5.61	4.03	3.01	2.33	1.85	1.50
3EA	14.1	12.4	8.45	5.51	3.75	2.68	2.00	1.54	1.23	0.997
25 x 25 x 6EA	20.8	18.0	11.2	6.84	4.46	3.10	2.26	1.72	1.35	1.08
5EA	16.5	14.3	8.86	5.43	3.55	2.47	1.81	1.38	1.08	0.870
3EA	11.4	9.63	5.90	3.60	2.36	1.65	1.21	0.923	0.726	0.586

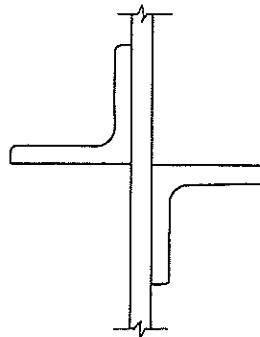


TABLE 8.3-2(1)

**EQUAL ANGLES  
GRADE 300**
**MAXIMUM DESIGN LOADS FOR ECCENTRICALLY LOADED SINGLE ANGLES IN TRUSSES**  
 angles on opposite sides of the truss chord

Designation	Maximum Design Loads (kN) Length in metres										
	0.25	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0
200 x 200 x 26EA	399	395	384	374	363	352	341	329	317	305	293
20EA	331	324	313	303	293	282	272	261	251	240	229
18EA	302	294	283	273	263	253	243	233	223	213	204
16EA	288	287	277	265	254	243	233	222	212	202	192
13EA	246	243	233	221	211	200	190	180	171	162	153
150 x 150 x 19EA	212	212	205	198	190	182	174	166	157	149	140
16EA	216	215	206	197	188	178	169	159	149	140	131
12EA	168	166	157	149	140	132	124	116	108	101	93.8
10EA	134	131	121	112	104	96.2	88.8	82.0	75.8	70.1	64.9
125 x 125 x 16EA	167	167	159	151	143	135	126	118	109	101	93.9
12EA	136	134	126	119	112	104	96.7	89.4	82.5	76.0	70.0
10EA	115	111	103	95.9	88.7	81.7	74.9	68.5	62.6	57.2	52.4
8EA	88.3	85.0	77.6	70.7	64.3	58.5	53.1	48.3	44.0	40.2	36.8

Note: Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

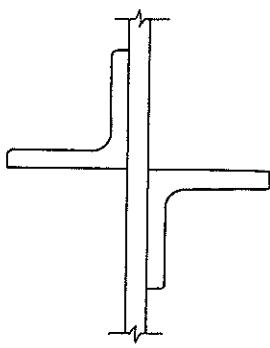


TABLE 8.3-2(2)

**EQUAL ANGLES  
GRADE 250**

**MAXIMUM DESIGN LOADS FOR ECCENTRICALLY LOADED SINGLE ANGLES IN TRUSSES**  
angles on opposite sides of the truss chord

Designation	Maximum Design Loads (kN) Length in metres										
	0.25	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0
100 x 100 x 12EA	87.1	86.2	81.6	77.0	72.1	67.0	61.8	56.7	52.0	47.5	43.5
10EA	73.2	71.7	67.1	62.7	58.2	53.7	49.1	44.8	40.8	37.2	33.9
8EA	61.0	59.1	54.8	50.6	46.6	42.6	38.7	35.1	31.9	28.9	24.0
6EA	45.4	43.5	39.6	36.0	32.7	29.5	26.6	23.9	21.6	19.5	17.7
90 x 90 x 10EA	65.7	62.3	58.2	54.2	50.0	45.6	41.4	37.4	33.8	30.6	27.7
8EA	53.9	52.1	48.2	44.4	40.6	36.8	33.2	29.8	26.9	24.2	21.9
6EA	41.1	39.3	35.7	32.4	29.2	26.1	23.3	20.9	18.7	16.8	15.1
75 x 75 x 10EA	48.8	47.6	44.3	40.8	37.1	33.3	29.7	26.5	23.6	21.1	18.9
8EA	42.6	41.1	37.8	34.5	31.0	27.6	24.5	21.7	19.3	17.2	15.3
6EA	33.6	32.0	29.0	26.0	23.1	20.3	17.9	15.7	13.9	12.4	11.0
5EA	24.9	23.5	20.8	18.3	16.0	13.9	12.1	10.6	9.34	8.28	7.38
65 x 65 x 10EA	39.5	38.4	35.5	32.4	29.0	25.6	22.6	19.9	17.5	15.5	13.8
8EA	34.7	33.2	30.1	26.9	23.8	20.9	18.4	16.1	14.2	12.6	11.2
6EA	28.2	26.8	24.1	21.4	18.8	16.3	14.1	12.3	10.8	9.49	8.39
5EA	21.5	20.3	17.8	15.5	13.4	11.5	9.92	8.60	7.50	6.60	5.84
55 x 55 x 6EA	22.4	21.2	18.9	16.5	14.1	12.1	10.3	8.85	7.65	6.65	5.83
5EA	17.7	16.5	14.2	12.1	10.2	8.65	7.36	6.31	5.45	4.75	4.16
50 x 50 x 8EA	23.1	20.0	17.5	15.0	12.8	10.9	9.32	8.03	6.96	6.07	5.33
6EA	19.3	18.3	16.2	14.0	11.8	9.99	8.45	7.20	6.18	5.34	4.65
5EA	15.6	14.5	12.4	10.5	8.74	7.32	6.17	5.25	4.50	3.89	3.40
3EA	9.77	8.90	7.34	5.99	4.88	4.02	3.36	2.84	2.44	2.11	1.85
45 x 45 x 6EA	16.3	15.4	13.5	11.5	9.60	8.00	6.70	5.66	4.82	4.14	3.59
5EA	13.4	12.5	10.7	8.95	7.36	6.08	5.06	4.25	3.61	3.10	2.68
3EA	8.63	7.85	6.42	5.16	4.16	3.39	2.81	2.36	2.00	1.73	1.50
40 x 40 x 6EA	13.5	12.7	11.0	9.18	7.54	6.20	5.13	4.29	3.62	3.09	2.66
5EA	11.2	10.4	8.81	7.20	5.83	4.75	3.91	3.25	2.74	2.34	2.01
3EA	7.50	6.80	5.49	4.34	3.44	2.77	2.27	1.88	1.59	1.36	1.18
30 x 30 x 6EA	8.24	7.71	6.39	5.06	3.98	3.15	2.53	2.06	1.71	1.43	1.22
5EA	6.90	6.31	5.07	3.96	3.09	2.44	1.95	1.59	1.32	1.11	0.940
3EA	5.04	4.52	3.48	2.62	1.99	1.55	1.24	1.00	0.830	0.698	0.584
25 x 25 x 6EA	5.92	5.49	4.38	3.35	2.56	1.98	1.56	1.25	1.03	0.852	0.718
5EA	5.01	4.59	3.57	2.69	2.03	1.56	1.23	0.987	0.807	0.670	0.565
3EA	3.71	3.29	2.44	1.78	1.32	1.01	0.789	0.693	0.518	0.432	0.365

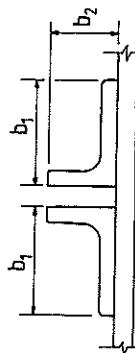


TABLE 8.3-3

**UNEQUAL ANGLES  
GRADE 300 & 250**

**MAXIMUM DESIGN LOADS FOR ECCENTRICALLY LOADED SINGLE ANGLES IN TRUSSES**

angles on same side of the truss chord — long leg attached

Designation	Maximum Design Loads (kN)									
	Length in metres									
	0.25	0.5	0.75	1.0	1.25	1.5	1.75	2.0	2.5	3.0
150 x 100 x 12UA	314	308	297	286	275	262	249	235	205	177
10UA	263	255	243	231	218	206	193	181	157	135
150 x 90 x 16UA	404	394	379	363	346	326	305	282	239	200
12UA	308	299	287	274	261	246	230	214	181	152
10UA	257	247	234	220	206	191	177	164	138	117
8UA	201	192	182	172	161	150	139	129	110	98.3
125 x 75 x 12UA	222	215	205	195	184	171	158	144	119	97.7
10UA	176	170	162	154	145	135	124	114	93.9	77.4
8UA	145	139	132	125	118	110	101	92.6	76.7	63.3
6UA	105	99.8	94.0	87.9	81.9	75.8	69.8	64.1	53.7	45.0
100 x 75 x 10UA	148	143	137	131	124	116	108	99.6	83.5	69.6
8UA	122	118	113	107	101	94.9	88.2	81.3	68.2	56.9
6UA	93.7	90.0	85.8	81.5	76.9	72.0	66.8	61.6	51.7	43.2
75 x 50 x 8UA	87.3	80.7	73.3	65.5	57.8	50.6	44.2	38.5	29.6	23.2
6UA	67.7	63.4	58.6	53.2	47.2	41.3	35.9	31.2	23.8	18.5
5UA	51.9	48.4	44.7	40.5	35.9	31.5	27.4	23.8	18.2	14.2
65 x 50 x 8UA	77.7	72.4	66.1	59.5	52.9	46.6	40.9	35.8	27.8	21.8
6UA	60.7	57.0	52.9	48.3	43.2	38.0	33.2	29.0	22.3	17.4
5UA	46.5	42.8	38.9	34.9	31.0	27.3	24.0	21.1	16.4	13.0

Notes: (1) For 150x30 angles and above: Grade 300.

(2) For 125x75 angles and below: Grade 250.

(3) Grade 300 refers to BHP Grade 300-PLUS™. See Note (1) on page 2-2.

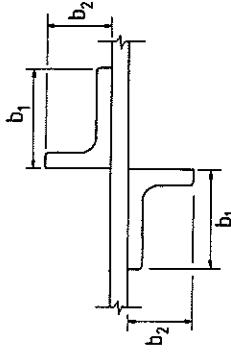


TABLE 8.3-4

**UNEQUAL ANGLES  
GRADE 300 & 250**

**MAXIMUM DESIGN LOADS FOR ECCENTRICALLY LOADED SINGLE ANGLES IN TRUSSES**

angles on opposite sides of the truss chord - long leg attached

Designation	Maximum Design Loads (kN) Length in metres																
	0.25	0.5	0.75	1.0	1.25	1.5	1.75	2.0	2.5	3.0	3.5	4.0	4.5	5.0	5.5	6.0	6.5
150 x 100 x 12UA	136	134	130	126	122	118	114	109	99.7	90.4	81.7	73.7	66.5	60.1	54.4	49.4	67.7
10UA	119	116	111	107	102	98.0	93.5	89.1	80.6	72.5	65.2	58.6	52.8	47.6	43.0	39.0	35.5
150 x 90 x 16UA	156	154	149	145	140	135	129	124	112	100	89.8	80.3	71.8	64.4	57.9	52.2	47.3
12UA	127	124	120	116	111	107	102	97.4	87.6	78.3	69.7	62.1	55.5	49.7	44.6	40.2	36.3
10UA	111	107	103	98.2	93.6	88.9	84.3	79.7	71.0	63.0	55.9	49.7	44.2	39.5	35.5	31.9	28.9
8UA	91.6	88.1	84.2	80.3	78.4	72.6	68.7	65.0	57.8	51.3	45.5	40.4	36.0	32.1	28.8	26.0	23.5
125 x 75 x 12UA	85.0	83.3	80.6	77.7	74.7	71.5	68.0	64.5	57.4	50.7	44.8	39.6	35.1	31.2	27.8	24.9	22.4
10UA	70.9	68.9	66.4	63.8	61.1	58.3	55.3	52.2	46.3	40.8	35.9	31.6	28.0	24.9	22.2	19.8	17.8
8UA	60.3	58.2	55.9	53.6	51.1	48.6	46.0	43.4	38.3	33.6	29.5	26.0	22.9	20.4	18.1	16.2	14.6
6UA	46.7	44.6	42.5	40.4	38.3	36.2	34.1	32.0	28.2	24.8	21.8	19.3	17.1	15.2	12.5	12.1	10.9
100 x 75 x 10UA	61.6	60.3	58.3	56.3	54.1	51.8	49.4	46.9	41.9	37.2	32.9	29.2	25.9	23.1	20.7	18.5	16.7
8UA	52.4	50.9	49.0	47.2	45.2	43.2	41.1	38.9	34.6	30.6	27.0	23.9	21.2	18.9	16.9	15.1	13.6
6UA	41.6	40.0	38.4	36.8	35.1	33.4	31.6	29.9	26.4	23.3	20.5	18.1	16.0	14.3	12.7	11.4	10.3
70 x 50 x 8UA	31.8	30.2	28.5	26.7	24.8	22.9	21.1	19.4	16.4	13.8	11.7	10.0	8.61	7.47	6.52	5.74	5.08
6UA	25.8	24.5	23.1	21.7	20.1	18.5	17.0	15.5	13.0	10.9	9.18	7.81	6.71	5.81	5.07	4.46	3.95
5UA	20.5	19.3	18.1	16.9	15.6	14.3	13.1	11.9	9.90	8.28	6.98	5.94	5.10	4.42	3.86	3.40	3.01
65 x 50 x 8UA	29.0	27.8	26.3	24.7	23.1	21.4	19.8	18.2	15.5	13.1	11.2	9.56	8.25	7.16	6.26	5.52	4.89
6UA	23.7	22.6	21.4	20.1	18.7	17.3	15.9	14.6	12.2	10.3	8.71	7.43	6.39	5.54	4.85	4.26	3.78
5UA	18.8	17.6	16.5	15.3	14.1	12.9	11.9	10.9	9.10	7.66	6.49	5.55	4.78	4.15	3.64	3.21	2.85

Notes: (1) For 150 x 90 angles and above: Grade 300.  
(2) For 125 x 75 angles and below: Grade 250.  
(3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

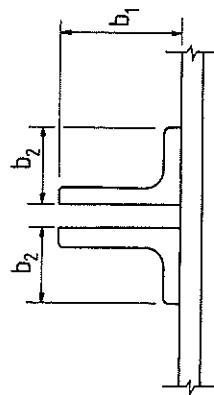


TABLE 8.3-5

**UNEQUAL ANGLES  
GRADE 300 & 250**

**MAXIMUM DESIGN LOADS FOR ECCENTRICALLY LOADED SINGLE ANGLES IN TRUSSES**

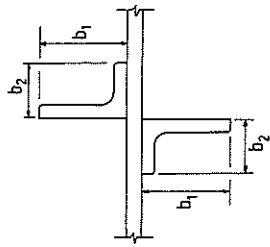
angles on the same side of the truss chord — short leg attached

Designation	Maximum Design Loads (kN) Length in metres																
	0.25	0.5	0.75	1.0	1.25	1.5	1.75	2.0	2.5	3.0	3.5	4.0	4.5	5.0	5.5	6.0	6.5
150 x 100 x 12UA	233	230	225	218	212	206	200	194	182	170	158	146	135	124	114	105	96.9
10UA	192	188	176	170	164	158	152	140	129	119	109	100	91.8	84.5	77.8	71.8	
150 x 90 x 16UA	278	276	270	264	257	244	238	224	210	196	182	169	156	144	133	123	
12UA	214	211	206	199	194	188	182	176	165	154	143	132	121	112	103	94.8	
10UA	180	175	169	163	156	150	144	138	127	116	106	97.4	89.2	81.8	75.2	69.2	
8UA	138	134	130	124	119	115	110	105	96.7	88.6	81.2	74.4	68.3	62.7	57.7	53.2	
125 x 75 x 12UA	153	151	147	143	139	135	131	127	119	110	101	92.9	85.0	77.7	71.1	65.1	
10UA	123	120	116	113	109	105	102	98.1	91.0	83.8	76.8	70.2	64.0	58.4	53.3	48.8	
8UA	102	98.7	95.1	91.6	88.1	84.8	81.5	78.3	72.0	65.9	60.1	54.7	49.7	45.2	41.3	37.7	
6UA	72.2	69.9	67.2	64.3	61.6	58.9	56.3	53.8	49.0	44.6	40.6	37.0	33.7	30.8	28.2	25.9	
100 x 75 x 10UA	117	115	112	108	104	101	96.9	92.8	84.4	75.9	67.7	60.4	53.8	48.0	43.0	38.6	
8UA	97.5	95.2	91.8	88.5	85.2	81.9	78.5	75.0	67.9	60.8	54.1	48.1	42.9	38.3	34.3	30.8	
6UA	72.9	70.8	68.1	65.5	62.9	60.3	57.7	55.1	49.7	44.5	39.6	35.3	31.5	28.1	25.2	22.7	
75 x 50 x 8UA	64.8	62.3	59.2	56.1	53.0	49.8	46.7	43.6	37.8	32.7	28.3	24.6	21.4	18.8	16.6	14.7	
6UA	50.5	48.3	46.0	43.6	41.3	38.9	36.5	34.0	29.3	25.2	21.7	18.7	16.3	14.2	12.5	11.1	
5UA	38.5	36.5	34.5	32.6	30.6	28.7	26.8	24.9	21.4	18.3	15.7	13.6	11.8	10.4	9.13	8.11	
65 x 50 x 8UA	63.2	60.4	57.2	53.7	50.2	46.6	43.0	39.6	33.4	28.2	23.8	20.3	17.4	15.0	13.1	11.5	
6UA	49.5	47.2	44.8	42.4	39.8	37.1	34.2	31.5	26.4	22.0	18.5	15.7	13.4	11.6	10.1	8.84	
5UA	37.8	35.6	33.3	31.0	28.7	26.4	24.3	22.3	18.7	15.7	13.3	11.3	9.74	8.44	7.38	6.49	

Notes: (1) For 150 x 90 angles and above: Grade 300.

(2) For 125 x 75 angles and below: Grade 250.

(3) Grade 300 refers to BHG Grade 300PLUS™. See Note (1) on page 2-2.



**TABLE 8.3-6**  
**UNEQUAL ANGLES**  
**GRADE 300 & 250**  
**MAXIMUM DESIGN LOADS FOR ECCENTRICALLY LOADED SINGLE ANGLES IN TRUSSES**  
angles on opposite sides of the truss chord — short leg attached

Designation	Maximum Design Loads (kN) Length in metres																
	0.25	0.5	0.75	1.0	1.25	1.5	1.75	2.0	2.5	3.0	3.5	4.0	4.5	5.0	5.5	6.0	6.5
150 x 100 x 12UA 10UA	113	112	109	106	103	100	97.3	94.6	89.2	83.9	78.8	73.9	69.2	64.7	60.6	56.7	53.2
150 x 90 x 16UA 12UA	131	130	127	124	121	118	116	113	107	102	96.0	90.5	85.2	80.2	75.4	70.9	66.7
10UA	104	102	99.4	96.4	93.6	90.8	88.1	85.4	80.3	75.3	70.5	65.9	61.6	57.6	53.8	50.4	47.2
8UA	89.5	86.6	83.4	80.2	77.1	74.1	71.2	68.4	63.2	58.4	53.9	49.9	46.2	42.8	39.8	37.1	34.6
125 x 75 x 12UA 10UA	71.8	70.9	69.1	67.2	65.4	63.6	61.9	60.1	56.7	53.2	49.9	46.6	43.5	40.6	37.9	35.4	33.1
8UA	58.9	57.5	55.7	53.9	52.2	50.4	48.8	47.2	44.0	41.0	38.0	35.3	32.7	30.4	28.2	26.3	24.5
6UA	49.6	47.9	46.1	44.3	42.7	41.0	39.5	37.9	35.1	32.3	29.8	27.5	25.3	23.4	21.7	20.1	18.7
100 x 75 x 10UA 8UA	53.9	53.0	51.5	50.0	48.5	47.0	45.5	43.9	40.8	37.7	34.7	31.9	29.3	26.9	24.8	22.8	21.1
6UA	45.8	44.6	43.1	41.6	40.2	38.7	37.3	35.9	33.1	30.4	27.8	25.4	23.2	21.3	19.5	18.0	16.5
70 x 50 x 8UA 6UA	28.4	27.4	26.2	25.1	24.0	22.9	21.8	20.7	18.7	16.8	15.1	13.6	12.2	11.1	10.0	9.12	8.32
5UA	22.7	21.7	20.7	19.7	18.7	17.8	16.9	16.0	14.2	12.6	11.3	10.1	9.01	8.11	7.33	6.65	6.05
65 x 50 x 8UA 6UA	26.5	25.6	24.6	23.5	22.4	21.3	20.2	19.1	17.0	15.1	13.4	11.9	10.6	9.48	8.51	7.67	6.93
5UA	21.5	20.5	19.6	18.7	17.8	16.8	15.9	14.9	13.1	11.5	10.2	8.98	7.96	7.09	6.35	5.71	5.16
	16.8	15.9	14.9	14.1	13.2	12.4	11.6	10.8	9.47	8.28	7.27	6.42	5.69	5.07	4.54	4.09	3.70

Notes: (1) For 150 x 90 angles and above: Grade 300.  
(2) For 125 x 75 angles and below: Grade 250.  
(3) Grade 300 refers to BHP Grade 300PLUS™. See Note (1) on page 2-2.

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**PART 9****CONNECTIONS – BOLTS/WELDS/  
STANDARDISED STRUCTURAL CONNECTIONS**

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**PART 9****CONNECTIONS – BOLTS/WELDS/  
STANDARDISED STRUCTURAL CONNECTIONS****9.1 Bolts****9.1.1 AS 4100 Requirements**

The general requirements and definitions for bolted connections are set out in Clause 9.1 and 9.2, of AS 4100. Clause 9.3 of AS 4100 sets out the requirements for the design of bolts. Clause 9.4 of AS 4100 should be used for assessing the strength of a bolt group. Design detail requirements for bolts are given in Clause 9.6 of AS 4100.

**9.1.2 Bolt Types and Bolting Categories**

*The system of bolting category designation identifies the bolt being used by using its strength grade designation (4.6 or 8.8) and identifies the installation procedure by a supplementary letter (S – snug; T – full tensioning to AS 4100). For 8.8/T categories, the type of joint is identified by an additional letter (F – friction type joint; B – bearing type joint). See Table 9.1.2 for a summary of bolt types and bolting procedures.*

Category 4.6/S refers to commercial bolts of Strength Grade 4.6 conforming to AS 1111, tightened using a standard wrench to a "snug tight" condition.

Category 8.8/S refers to any bolt of Strength Grade 8.8, tightened using a standard wrench to a "snug tight" condition in the same way as for category 4.6/S. Essentially, these bolts are used as higher grade commercial bolts in order to increase the capacity of certain connection types. In practice, they will normally be high strength structural bolts of Grade 8.8 to AS 1252.

Categories 8.8/TF and 8.8/TB (or 8.8/T when referring generally to both types) refer specifically to high strength structural bolts of Strength Grade 8.8 conforming to AS 1252, *fully tensioned in a controlled manner to the requirements of AS 4100 (Clause 15.2)*.

For additional data on dimensions and masses of Commercial and High Strength Structural bolts, nuts and washers refer to Part 10 : Detailing Parameters of this publication. Further relevant information on bolt types, bolting categories and other aspects of bolting can be found in "Bolting of Steel Structures", 3rd Edition, AISc (see Ref.[1] in Section 9.4).

**9.1.3 Design Capacities of Commonly Used Bolts**

Two symbols are incorporated into the bolting category designations 4.6/S, 8.8/S, 8.8/TB. They are:-

**N** : bolt in shear with threads included in the shear plane (eg 8.8 N/S)

**X** : bolt in shear with threads excluded from the shear plane (eg 8.8 X/S)

For bolts, the following tables of design capacity have been derived using the following expressions:

$$N_{lf} = A_s f_{lf}$$

$$V_{fn} = 0.62 f_{lf} k_r A_c \quad (k_r = 1.0 \text{ Clause 9.3.2.1 of AS 4100})$$

$$V_{fx} = 0.62 f_{lf} k_r A_o \quad (k_r = 1.0 \text{ Clause 9.3.2.1 of AS 4100})$$

$$V_{sf} = \mu n_{ei} N_{li} k_h \quad (\text{see 9.1.3(c) for } \mu, n_{ei}, N_{li}, k_h \text{ used})$$

and where applicable, for the ply in bearing

$$V_b = 3.2d_i t_p f_{up} \quad (\text{local bearing failure})$$

$$V_b = a_e t_p f_{up} \quad (\text{end plate tearout failure})$$

Note: The appropriate design capacity factor,  $\phi$  (from Table 3.4 and Clause 3.5.5 of AS 4100), is included in the respective design capacity table.

**TABLE 9.1.2: Bolt Types and Bolting Categories**

Bolting Category	Details of bolt used					Method of Tensioning/ Remarks
	Strength Grade	Minimum Tensile Strength (MPa)	Minimum Yield Strength (MPa)	Name	Australian Standard	
4.6/S	4.6	400	240	Commercial	AS 1111	Use <u>Snug</u> tightened. Least costly and most commonly available is Grade 4.6 bolt.
8.8/S	8.8	830	660	High Strength Commercial	AS 1252	Bolts used are <u>Snug</u> tightened. The high strength structural has a large bolt head and nut because it is designed to withstand full tensioning (see 8.8/T category description). However, it can also be used in a snug tight condition.
8.8/TF	8.8	830	660	High Strength Structural Bolt – Fully Tensioned Friction TypeJoint	AS 1252	In both applications, bolts are fully <u>Tensioned</u> to the requirements of AS 4100. Cost of tensioning is an important consideration in the use of these bolting categories.
8.8/TB	8.8	830	660	High Strength Structural Bolt – Fully Tensioned Bearing Type Joint	AS 1252	

## 9.1.3(a) Design Capacities of Commonly Used Bolts – Strength Limit State

COMMERCIAL BOLTS –  
4.6/S BOLTING CATEGORY

GRADE 4.6

TABLE 9.1.3(a): Design Capacities  
( $f_{ut} = 400$  MPa)

Bolt Size	Axial Tension $\phi N_{tf}$	Shear Values (Single Shear)	
		Threads included in Shear Plane – N $\phi V_{fn}$	Threads excluded from Shear Plane – X $\phi V_{fx}$
M12	27.0	15.1	22.4
M16	50.2	28.6	39.9
M20	78.4	44.6	62.3
M24	113	64.3	89.7
M30	180	103	140
M36	261	151	202
$\phi = 0.8$		$\phi = 0.8$	
		4.6N/S	4.6X/S

**Important Note on 4.6/S Bolting Category**

Values for the threads excluded case are provided for the sake of completeness.

However, in practical structural bolting situations it is never worthwhile considering 4.6X/S category – 8.8N/S is always more economic.

Note: Bearing/Plate Tearout Design Capacity – For all reasonable combinations of ply thickness, bolt diameter and end distance, the design capacity for a ply in bearing ( $\phi V_b$ ) exceeds both  $\phi V_{fn}$  and  $\phi V_{fx}$ .

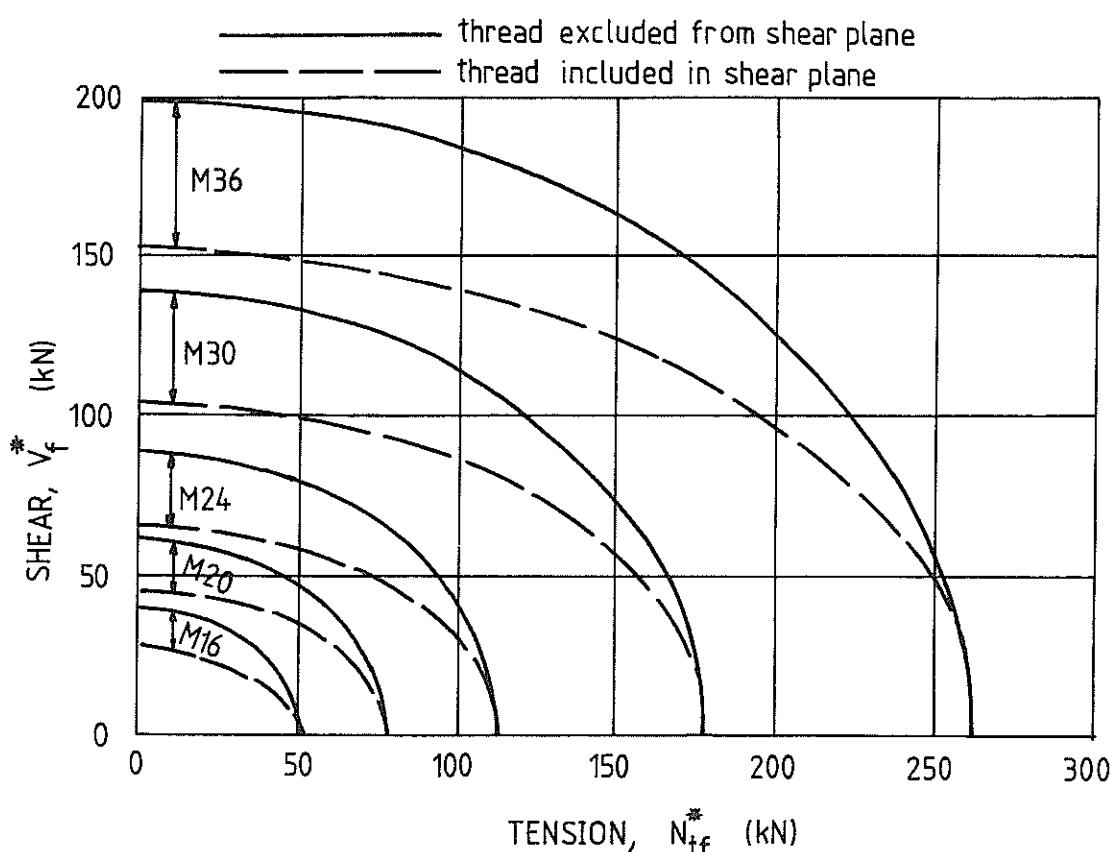


Figure 9.1.3(a): Shear – Tension Interaction Diagram

### 9.1.3(b) Design Capacities of Commonly Used Bolts – Strength Limit State

HIGH STRENGTH STRUCTURAL BOLTS  
8.8/S, 8.8/TB, 8.8/TF BOLTING CATEGORIES

GRADE 8.8

TABLE 9.1.3(b): Design Capacities  
( $f_{ut} = 830 \text{ MPa}$ )

Bolt Size	Axial Tension	Single Shear		Plate Tearout in kN								Bearing in kN							
		Threads included in Shear Plane	Threads excluded from Shear Plane	$\phi V_b$ for $t_p$ & $a_e$ of:								$\phi V_b$ for $t_p$							
				$t_p = 6$	$t_p = 8$	$t_p = 10$	$t_p = 12$	6	8	10									
		$\phi N_{tf}$	$\phi V_{fn}$	$\phi V_{fx}$															
		kN	kN	kN	35	40	45	35	40	45	35	40	45	35					
M16		104	59.3	82.7										122	162	203			
M20		163	92.6	129	83	95	107	111	127	143	139	158	178	166	190	124	152	203	253
M24		234	133	186													182	243	304
M30		373	214	291													228	304	380
M36		541	313	419													274	355	456
	$\phi = 0.8$			$\phi = 0.8$												$\phi = 0.9$			
				8.8N/S	8.8X/S											$f_{up} = 440 \text{ MPa}$		$f_{up} = 440 \text{ MPa}$	

Note: The above table lists the design capacity of a ply in bearing for Grade 300 ( $f_{up} = 440 \text{ MPa}$ ) steel only. For listings and guidance on design capacities for ply failure in other grades of steel refer to Section 9.1.4.

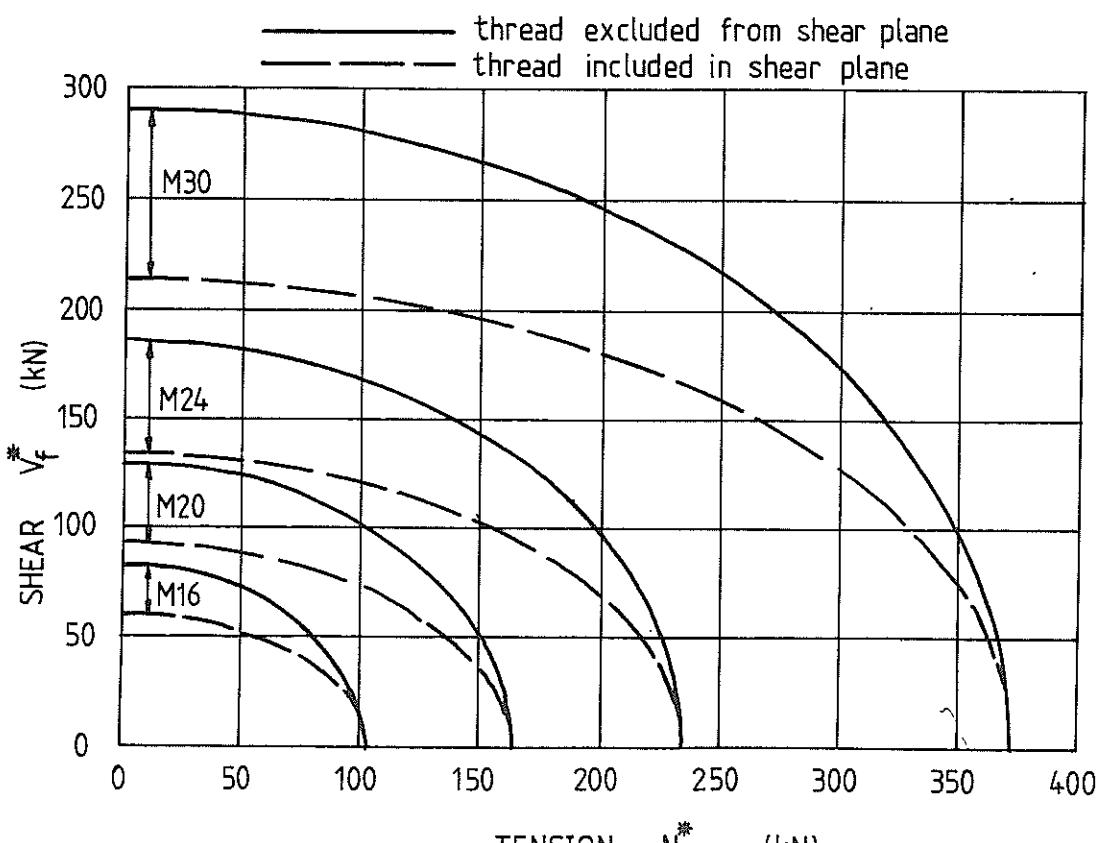


Figure 9.1.3(b): Shear-Tension Interaction Diagram

### 9.1.3(c) Design Capacities of Commonly Used Bolts – Serviceability Limit State

HIGH STRENGTH STRUCTURAL BOLTS  
8.8/TF BOLTING CATEGORIES

GRADE 8.8

TABLE 9.1.3(c): Design Capacities

Slip factor,  $\mu = 0.35$

Number of effective interfaces,  $n_{ei} = 1$

Capacity factor,  $\phi = 0.7$  – for bolt serviceability limit state  
(Clause 3.5.5 of AS 4100)

Bolt Size	Bolt Tension at Installation, $N_{ti}$	Axial Tension $\phi N_{tf}$	Design Capacity in Shear, $\phi V_{sf}$ , for		
			$k_h = 1$	$k_h = 0.85$	$k_h = 0.7$
			kN	kN	kN
M16	95	66.5	23.3	19.8	16.3
M20	145	101	35.5	30.2	24.9
M24	210	147	51.5	43.7	36.0
M30	335	234	82.1	69.8	57.5
M36	490	343	120	102	84.1

Note:  $N_{ti}$  is given in Clause 15.2.5.1 of AS 4100

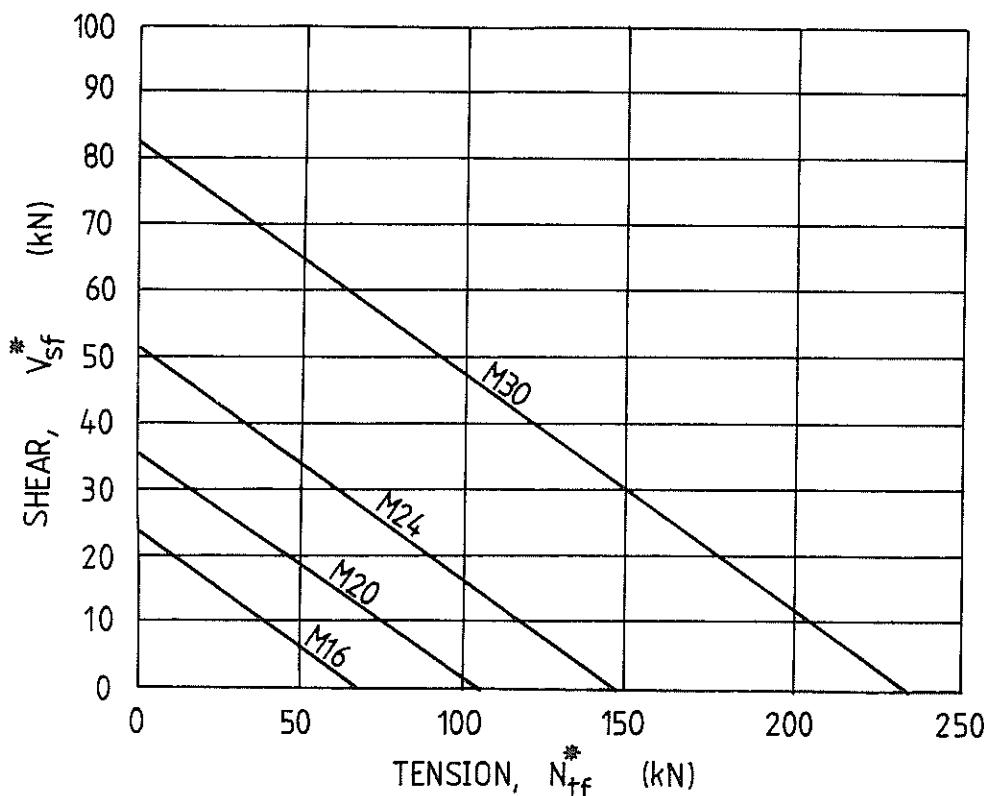


Figure 9.1.3(c): Shear – Tension Interaction Diagram

$k_h = 1.0$

#### 9.1.4 Minimum Edge Distance In Direction of a Component Force / Ply in Bearing

For a bolt bearing on a ply the design bearing capacity for the ply,  $\phi V_b$ , is the *lesser* of the design bearing capacity due to plate tearout (see eqn. 9.1.4(a)) and the design bearing capacity due to ply local bearing failure (see eqn. 9.1.4(b)).

Table 9.1.4 lists the design bearing capacity of a ply,  $\phi V_b$ , derived from the minimum edge distance,  $a_e$ , and is based on the plate tearout criteria of Eqn. 9.3.2.4(2) of AS 4100, i.e.:

$$\phi V_b = \phi a_e t_p f_{up} \quad - \text{eqn. 9.1.4(a)}$$

where  $a_e$  = minimum distance from the edge of a hole to the edge of a ply in the direction of the component force plus half the bolt diameter

The edge of the ply should be deemed to include the edge of an adjacent fastener hole.

The above edge distance provision is intended to apply to the simple situations in connections as shown in Fig. 9.1.4-1(a) as well as more complicated situations, e.g. Fig. 9.1.4-1(b) where the edge distance and end distances are not directly related to the direction of the applied force as those in Fig 9.1.4-1(a).

Consider the bolt group in an angle cleat connection as shown in Fig. 9.1.4-2. The bottom bolt in the connection applies a resultant force ( $V_{fb}^*$ ) to the web of the beam at an angle  $\theta_1$ . The resultant force ( $V_{fb}^*$ ) and the angle ( $\theta_1$ ) can be calculated using conventional methods based on a 'linear' method analysis and taking account of eccentricity (Ref.[2] in Section 9.4).

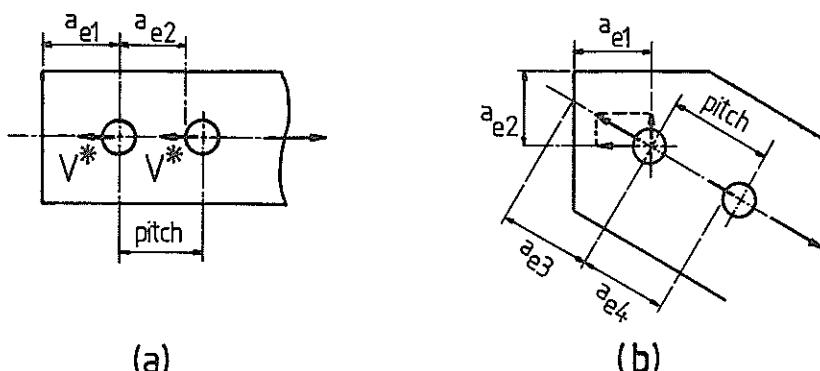


Figure 9.1.4-1

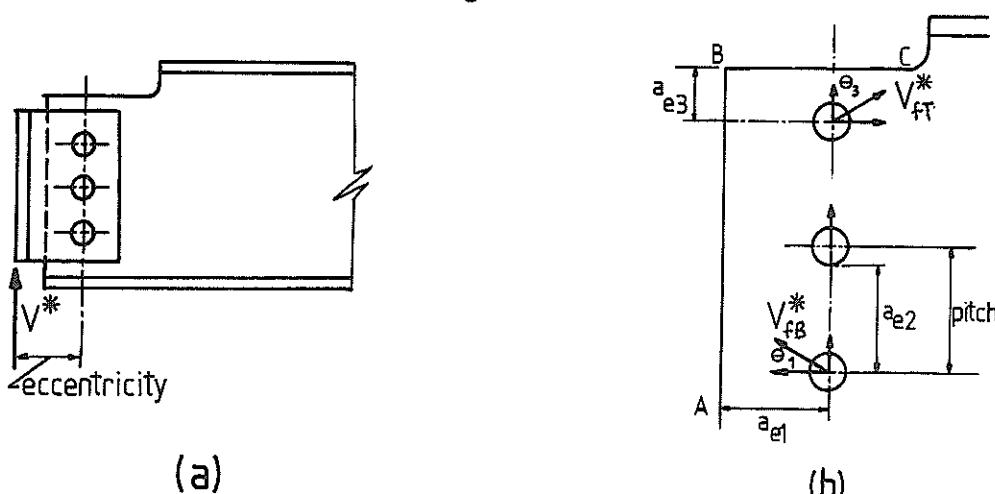


Figure 9.1.4-2

## DESIGN BEARING CAPACITY

I <sub>p</sub>	Form	Grade	f <sub>up</sub>	Design Bearing Capacity, $\phi V_b$ (kN)									
				a <sub>s</sub> (mm)									
mm			MPa	25	30	35	40	45	50	55	60	65	70
6	P	400	480	64.8	77.8	90.7	104	117	130	143	156	168	181
		350	450	60.8	72.9	85.0	97.2	109	122	134	146	158	170
		300	430	58.0	69.7	81.3	92.9	104	116	128	139	151	163
	S	250	410	55.3	66.4	77.5	88.6	99.6	111	122	133	144	155
		350	480	64.8	77.8	90.7	104	117	130	143	156	168	181
		300	440	59.4	71.3	83.2	95.0	107	119	131	143	154	166
8	P	250	410	55.3	66.4	77.5	88.6	99.6	111	122	133	144	155
		400	480	86.4	104	121	138	156	173	190	207	225	242
		350	450	81.0	97.2	113	130	146	162	178	194	211	227
		300	430	77.4	92.9	108	124	139	155	170	186	201	217
	S	250	410	73.8	88.6	103	118	133	148	162	177	192	207
		350	480	86.4	104	121	138	156	173	190	207	225	242
		300	440	79.2	95.0	111	127	143	158	174	190	206	222
		250	410	73.8	88.6	103	118	133	148	162	177	192	207
10	P	400	480	108	130	151	173	194	216	238	259	281	302
		350	450	101	122	142	162	182	203	223	243	263	284
		300	430	96.8	116	136	155	174	194	213	232	252	271
	S	250	410	92.3	111	129	148	166	185	203	221	240	258
		350	480	108	130	151	173	194	216	238	259	281	302
		300	440	99.0	119	139	158	178	198	218	238	257	277
12	P	250	410	92.3	111	129	148	166	185	203	221	240	258
		400	480	130	156	181	207	233	259	285	311	337	363
		350	450	122	146	170	194	219	243	267	292	316	340
		300	430	116	139	163	186	209	232	255	279	302	325
	S	250	410	111	133	155	177	199	221	244	266	288	310
		350	480	130	156	181	207	233	259	285	311	337	363
		300	440	119	143	166	190	214	238	261	285	309	333
		250	410	111	133	155	177	199	221	244	266	288	310
16	P	400	480	173	207	242	277	311	346	380	415	449	484
		350	450	162	194	227	259	292	324	356	389	421	454
		300	430	155	186	217	248	279	310	341	372	403	433
	S	250	410	148	177	207	236	266	295	325	354	384	413
		350	480	173	207	242	277	311	346	380	415	449	484
		300	440	158	190	222	253	285	317	348	380	412	444
20	P	250	410	148	177	207	236	266	295	325	354	384	413
		400	480	216	259	302	346	389	432	475	518	562	605
		350	450	203	243	284	324	365	405	446	486	527	567
	S	300	430	194	232	271	310	348	387	426	464	503	542
		250	410	185	221	258	295	332	369	408	443	480	517
		350	480	216	259	302	346	389	432	475	518	562	605
24	P	300	440	198	238	277	317	356	396	436	475	515	554
		250	410	185	221	258	295	332	369	406	443	480	517
		400	480	259	311	363	415	467	518	570	622	674	726
		350	450	243	292	340	389	437	486	535	583	632	680
	S	300	430	232	279	325	372	418	464	511	557	604	650
		250	410	221	266	310	354	399	443	487	531	576	620
25	P	350	480	259	311	363	415	467	518	570	622	674	726
		300	450	231	277	323	369	415	461	507	554	600	646
		250	410	221	266	310	354	399	443	487	531	576	620
	S	350	480	270	324	378	432	486	540	594	648	702	756
		300	440	248	297	347	396	446	495	545	594	644	693
		250	410	231	277	323	369	415	461	507	554	600	646
28	P	400	480	302	363	423	484	544	605	665	726	786	847
		350	450	284	340	397	454	510	567	624	680	737	794
		300	430	271	325	379	433	488	542	596	650	704	759
	S	250	410	258	310	362	413	465	517	568	620	672	723
		350	480	302	363	423	484	544	605	665	726	786	847
		300	440	277	333	388	444	499	554	610	665	721	776
32	P	400	480	346	415	484	553	622	691	760	829	899	968
		350	450	324	389	454	518	583	648	713	778	842	907
		300	430	310	372	433	495	557	619	681	743	805	867
	S	250	410	295	354	413	472	531	590	649	709	768	827
		350	480	346	415	484	553	622	691	760	829	899	968
		300	440	317	380	444	507	570	634	697	760	824	887
36	P	400	480	389	467	544	622	700	778	855	933	1010	1090
		350	450	365	437	510	583	656	729	802	875	948	1020
		300	430	348	418	488	557	627	697	766	836	906	975
	S	250	410	332	399	465	531	598	664	731	797	863	930
		350	480	389	467	544	622	700	778	855	933	1010	1090
		300	440	356	428	499	570	642	713	784	855	927	998
40	P	400	480	432	518	605	691	778	864	950	1040	1120	1210
		350	450	405	486	567	648	729	810	891	972	1050	1130
		300	430	387	464	542	619	697	774	851	929	1010	1080
	S	250	410	369	443	517	590	664	738	812	886	959	1030
		350	480	432	518	605	691	778	864	950	1040	1120	1210
		300	440	396	475	554	634	713	792	871	950	1030	1110
40	S	250	410	369	443	517	590	664	738	812	886	959	1030

Notes:

(1) Check also for local bearing failure criteria.

(2) For intermediate values of  $a_0$  use linear interpolation.

(3) For the "Form" column of the table, P = Plate; S = Section.

(4) Grade 300 for sections refers to EN 10025-1:2004.

Edge distance  $a_{e1}$  is determined in the following way:–

- (i) the minimum distance from edge A-B, to the centre of the fastener is the distance along the line perpendicular to the edge and through the centre of the fastener;
- (ii) the component of  $V_{fb}^*$  in the direction of the closest edge is  $V_{fb}^* \cos\theta_1$ . Thus,

$$V_{fb}^* \cos\theta_1 \leq \phi a_{e1} f_{up} t_p \quad \text{or} \quad a_{e1} \geq \frac{V_{fb}^* \cos\theta_1}{\phi f_{up} t_p}$$

Similarly, the end distance  $a_{e2}$  would be required to satisfy

$$V_{fb}^* \sin\theta_1 \leq \phi a_{e2} f_{up} t_p \quad \text{or} \quad a_{e2} \geq \frac{V_{fb}^* \sin\theta_1}{\phi f_{up} t_p}$$

The top bolt in the connection would be treated in the following manner:–

- (i) for edge B-C, the component of force towards the closest edge is  $V_{ft}^* \cos\theta_3$ , so that

$$V_{ft}^* \cos\theta_3 \leq \phi a_{e3} f_{up} t_p \quad \text{or} \quad a_{e3} \geq \frac{V_{ft}^* \cos\theta_3}{\phi f_{up} t_p}$$

- (ii) for edge A-B, the component of force in the direction perpendicular to the edge A-B is away from the edge and is not considered.

A check should also be done on the possibility of ply local bearing failure, refer to Eqn. 9.3.2.4(1) of AS 4100, i.e.:–

$$\phi V_b = \phi 3.2 d t_p f_{up}$$

– eqn. 9.1.4(b)

The method above would be used for this check.

***The design bearing capacity of a ply,  $\phi V_b$ , is the lesser of eqns 9.1.4(a) and 9.1.4(b).***

The design bearing force on a ply at a bolt,  $V_b^*$ , must satisfy the following:

$$V_b^* \leq \phi V_b \quad \text{where } \phi = 0.9 \text{ (Table 3.4 of AS 4100).}$$

## 9.1.5 Design Details for Bolts

Consideration must also be given to the Code requirements for design details for bolts (Clause 9.6 of AS 4100) which prescribes minimum/maximum pitch and minimum/maximum edge distance. Table 9.1.5 lists the minimum edge distance from the centre of a fastener to the edge of a plate or the flange of a rolled section.

**TABLE 9.1.5: AS 4100 – Minimum Edge Distances**

Nominal Diameter of Fastener	Sheared or Hand Flame Cut Edge	Rolled Plate; Machine Flame Cut, Sawn or Planed Edge		Rolled Edge of a Rolled Section
		mm	mm	
12	21	18	15	
16	28	24	20	
20	35	30	25	
24	42	36	30	
30	53	45	38	
36	63	54	45	

## 9.1.6 Strength Limit State Assessment of a Bolt Group

For the assessment of the strength of a bolt group in compliance with AS 4100 see Ref.[2] of Section 9.4.

## 9.2 Welds

### 9.2.1 AS 4100 Requirements

The general requirements for welded connections are set out in Clause 9.1 of AS 4100. Clause 9.7 of AS 4100 sets out the requirements for the design of welds. Clause 9.8 of AS 4100 should be used for assessing the strength of a weld group.

### 9.2.2 Weld Quality

Complete Penetration Butt Welds

**GP** (general purpose)  $\phi = 0.6$  (Table 3.4 of AS 4100)

Category GP may be selected where the weld is essentially statically loaded and is not loaded above 66.7% of the design capacity of a SP weld.

**SP** (structural purpose)  $\phi = 0.9$  (Table 3.4 of AS 4100)

Category SP shall be selected where a GP quality weld is not appropriate.

The cut-off value of 66.7% for this weld type is due to the ratio of GP to SP capacity factors ( $\phi$ ), i.e.:

$$0.6/0.9 \times 100 = 66.7\%$$

Fillet Weld / Incomplete Penetration Butt Weld / Plug or Slot Weld / Weld Group

**GP** (general purpose)  $\phi = 0.6$  (Table 3.4 of AS 4100)

Category GP may be selected where the weld is essentially statically loaded and is not loaded above 75% of the design capacity of a SP weld.

**SP** (structural purpose)  $\phi = 0.8$  (Table 3.4 of AS 4100)

Category SP shall be selected where a GP quality weld is not appropriate.

The cut-off value of 75% for these weld types is due to the ratio of GP to SP capacity factors ( $\phi$ ), i.e.:

$$0.6/0.8 \times 100 = 75\%$$

### 9.2.3 Strength Limit State Assessment of Butt Welds

- (a) *Complete penetration butt welds, category SP:* Where a category SP complete penetration butt weld is used, no detailed analysis of the weld strength is required. Due to this, the design capacity of a category SP, complete penetration butt weld, is considered as being equal to the nominal capacity of the weaker part of the parts being joined, multiplied by the appropriate capacity factor,  $\phi (=0.9)$ .

For a category GP complete penetration butt weld, the designer must be satisfied that this weld can properly transmit the imposed loads in the strength limit state condition by taking into account the increased defects permitted in the weld. Again, the design capacity is equal to the nominal capacity of the weaker part multiplied by the appropriate capacity factor,  $\phi (=0.6)$

The design throat thickness for a complete penetration butt weld shall be the size of the weld.

- (b) *Incomplete penetration butt weld:* The design capacity of an incomplete-penetration butt weld shall be calculated as for a fillet weld using the design throat thickness determined in accordance with Clause 9.7.2.3(b) of AS 4100. Following is a summary of this clause for prequalified preparations as specified in AS 1554.1 :

Joint Type	$\theta$ or $t_t$	Manual metal arc	Submerged arc	Flux-cored arc	Gas-shielded metal-arc
<u>Single-V butt weld</u> 	$\theta$ $t_t$	45,60 45:d-3 60:d	60 d	50,60 d-3	50,60 d-3
<u>Double-V butt weld</u> 	$\theta$ $t_t$	45,60 45:d_3+d_4-6	60 d_3+d_4	50,60 d_3+d_4-6	50,60 d_3+d_4-6

NOTE: 1)  $t_t$ =design throat thickness.

2) For other types of butt welds see Table 4.4(B), AS 1554.1

TABLE 9.2.3

Clauses 9.7.2.3(b)(ii) and 9.7.2.3(b)(iii) of AS 4100 should be referred to for non-prequalified preparations for incomplete penetration butt welds.

The effective length of a butt weld is taken as the length of the continuous full size weld. The effective area of a butt weld is calculated from the product of the effective length and the design throat thickness.

## 9.2.4 Strength Limit State Assessment of Fillet Welds

In the design of fillet welds using AS 4100, for

- the size of a fillet weld ( $t_w$ , or  $t_{w1}, t_{w2}$ ) refer to Clauses 9.7.3.1, 9.7.3.2 and 9.7.3.3 of AS 4100;
- the calculation of *design throat thickness* ( $t_t$ ) refer to Clause 9.7.3.4 of AS 4100;
- the calculation of *effective length* refer to Clause 9.7.3.5 of AS 4100.

**Design Capacities of Fillet Welds:** A fillet weld subject to a design force per unit length of weld,  $V_w^*$ , shall satisfy:

$$V_w^* \leq \phi V_w$$

where  $V_w^*$  = the vectorial sum of the design forces per unit length on the effective area of the weld

$V_w$  = nominal capacity of a fillet weld per unit length

=  $0.6 f_{uw} t_t k_r$

$\phi$  = capacity factor (Table 3.4 of AS 4100 or Section 9.2.2 of these tables)

and

$f_{uw}$  = nominal tensile strength of the weld metal (Table 9.7.3.10(1) of AS 4100)

$t_t$  = design throat thickness

$k_r$  = reduction factor for a welded lap connection (Table 9.7.3.10(2) of AS 4100)

The effective area of a fillet weld is the product of the effective length and the design throat thickness.

Tables 9.2.4-1 and 9.2.4-2 lists the design capacity,  $\phi V_w$ , of an equal leg fillet weld for varying weld size ( $t_w$ ) and weld category (SP or GP). These values are derived from the design capacity side of the above strength limit state inequality, so that

$$\phi V_w = \phi 0.6 f_{uw} t_t k_r$$

where the reduction factor to account for the length of a welded lap connection ( $k_r$ ) is taken as unity (Table 9.7.3.10(2) of AS 4100).

Notation used in Tables 9.2.4-1 and 9.2.4-2:

- 1)  $t_t$  = design throat thickness =  $t_w / \sqrt{2}$ ;  $t_w$  = leg size
- 2)  $f_{uw}$  = nominal tensile strength of the weld metal.

**Table 9.2.4-1: Design Capacities of Equal Leg Fillet Welds**  
Category SP,  $\phi = 0.8$

Weld Size (mm)		Design Capacity per unit length of weld, $\phi v_w$ (kN/mm)	
$t_w$	$t_t$	E41XX/W40X	E48XX/W50X
3	2.12	0.417	0.489
4	2.83	0.557	0.652
5	3.54	0.696	0.815
6	4.24	0.835	0.978
8	5.66	1.11	1.30
10	7.07	1.39	1.63
12	8.49	1.67	1.96
		$f_{uw} = 410 \text{ MPa}$	$f_{uw} = 480 \text{ MPa}$

**Table 9.2.4-2: Design Capacities of Equal Leg Fillet Welds**  
Category GP,  $\phi = 0.6$

Weld Size (mm)		Design Capacity per unit length of weld, $\phi v_w$ (kN/mm)	
$t_w$	$t_t$	E41XX/W40X	E48XX/W50X
3	2.12	0.313	0.367
4	2.83	0.417	0.489
5	3.54	0.522	0.611
6	4.24	0.626	0.733
8	5.66	0.835	0.978
10	7.07	1.04	1.22
12	8.49	1.25	1.47
		$f_{uw} = 410 \text{ MPa}$	$f_{uw} = 480 \text{ MPa}$

Remarks on (equal) fillet weld leg sizes,  $t_w$ :

- 1) for  $t_w = 3\text{-}5 \text{ mm}$  : Used for a minimum size fillet weld (Table 9.7.3.2 of AS 4100)
- 2) for  $t_w = 6\text{-}8 \text{ mm}$  : Sizes preferred for standard connections – single pass welds.
- 3) for  $t_w = 10\text{-}12 \text{ mm}$  : Not recommended for all cases – cannot be guaranteed as single pass welds. Check with fabricator before specifying.

## 9.2.5 Strength Limit State Assessment of a Weld Group

For the assessment of the strength of a fillet weld group in compliance with AS 4100 see Ref.[2] of Section 9.4.

## 9.3 Standardised Structural Connections

This Section provides a brief summary only; full details can be found in the references listed in Section 9.4.

### 9.3.1 Standard Components

The components used in any connection are selected from a range of standard flat bars and angles. Using these standard components, it has been possible to develop a standardised connection detail and design capacity tables for each connection type. This has very real advantages, since it enables the designer to adopt a rational approach to connection selection and design.

### 9.3.2 Standardised Structural Connections

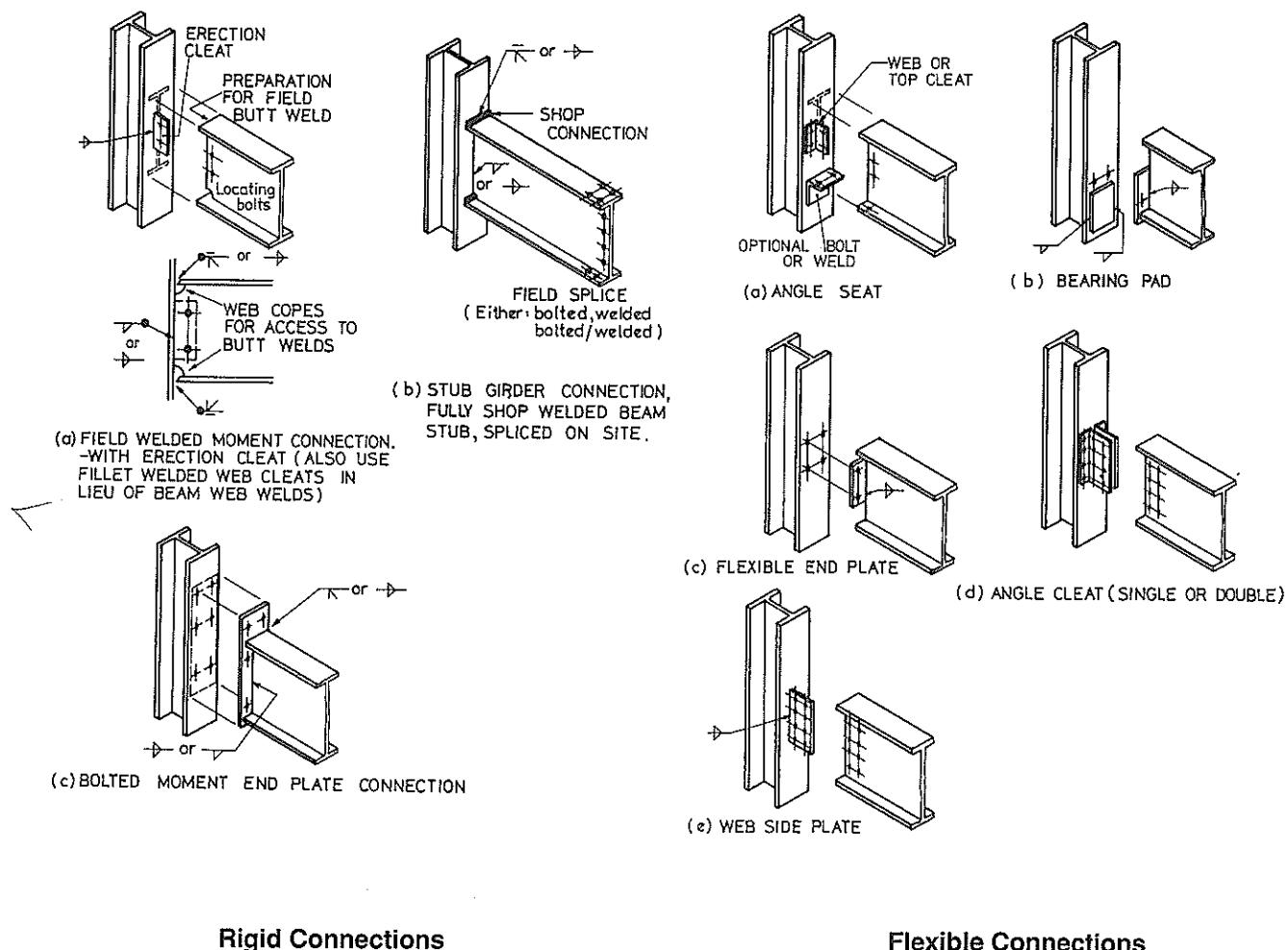


Figure 9.3.2

### 9.3.3 Standard Parameters

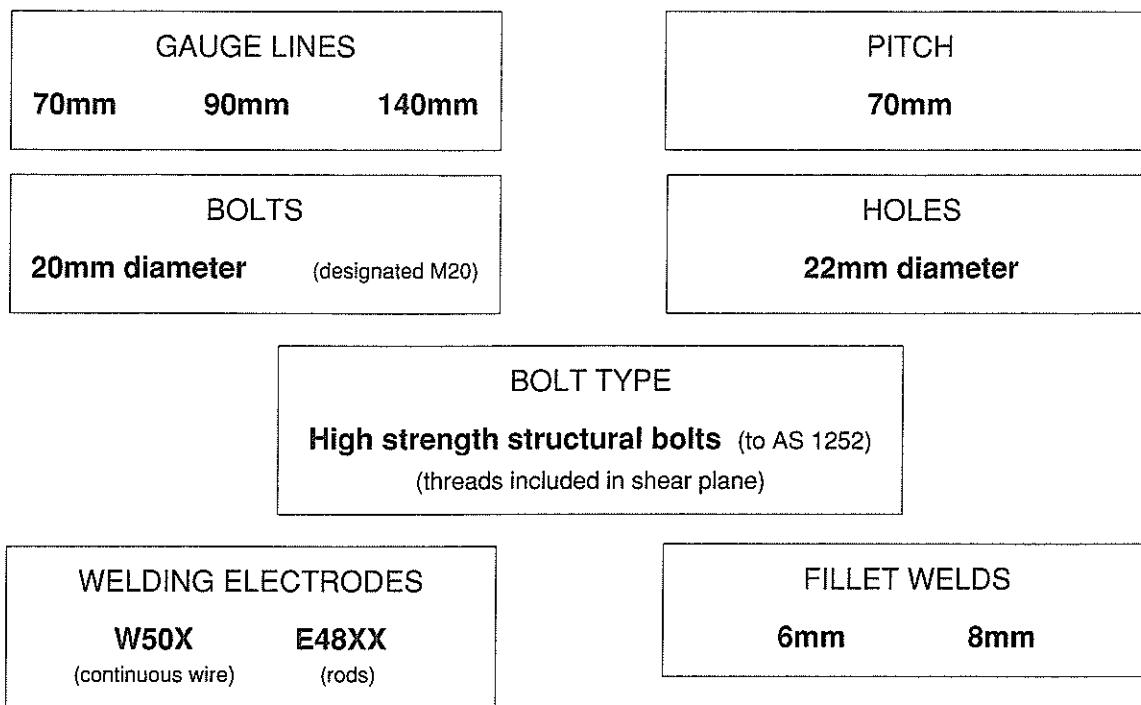
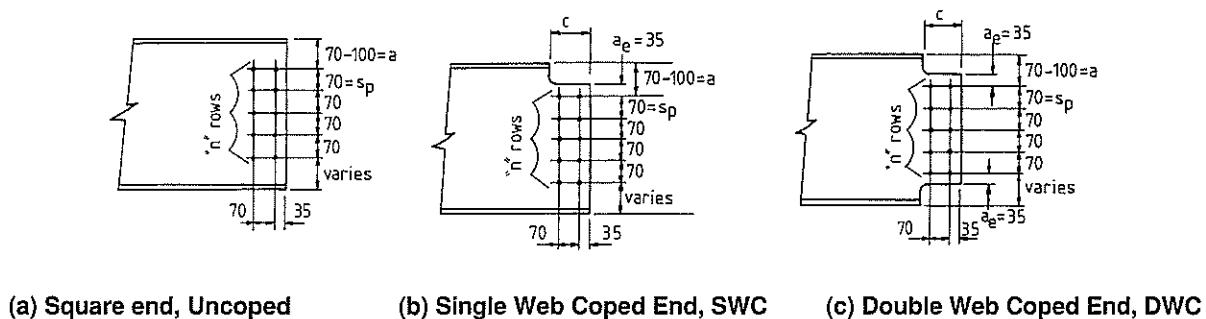


Figure 9.3.3-1: Standard Parameters

#### Bolting Layout for Supported Members



Note: All beam end preparations may have a single line of bolts in lieu of the two lines shown above.

#### Bolting Layouts

Figure 9.3.3-2: Standard End Preparations

## 9.4 References

- [1] A. Firkins & T.J. Hogan, "Bolting of Steel Structures" – 3rd Ed., *Australian Institute of Steel Construction*, 1991.
- [2] T.J. Hogan & I.R. Thomas, "Design of Structural Connections", 4th Ed., *Australian Institute of Steel Construction*, 1994.
- [3] "Standardised Structural Connections", 3rd Ed., *Australian Institute of Steel Construction*, 1985.
- [4] "Design Capacity Tables for Structural Steel", 1st Ed., *Australian Institute of Steel Construction*, 1991.

Suggested reference:

- AS-4100 Supplement 1 – 1990 "Steel Structures – Commentary (Supplement to AS 4100-1990)", *Standards Australia*, 1990. Specific reference to Sections C9, C14 and C15.

**PART 10 DETAILING PARAMETERS**

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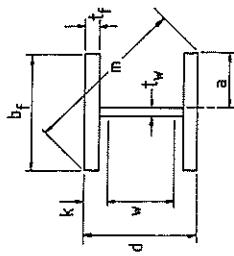


TABLE 10.1-1  
**WELDED BEAMS**  
**RATIONALISED DIMENSIONS FOR DETAILING**

Designation	Depth of Section d	Flange		Web		Dimensions		
		Width b <sub>f</sub>	Thickness t <sub>f</sub>	t <sub>w</sub>	$\frac{t_w}{2}$	a	w	k
kg/m	mm	mm	mm	mm	mm	mm	mm	mm
1200WB455	1200	500	40	16	8	242	1104	48
423	1192	500	36	16	8	242	1104	44
392	1184	500	32	16	8	242	1104	40
342	1184	400	32	16	8	192	1104	40
317	1176	400	28	16	8	192	1104	36
278	1170	350	25	16	8	167	1104	33
249	1170	275	25	16	8	130	1104	33
1000WB322	1024	400	32	16	8	192	944	40
296	1016	400	28	16	8	192	944	36
258	1010	350	25	16	8	167	944	33
215	1000	300	20	16	8	142	944	28
900WB282	924	400	32	12	6	194	848	38
257	916	400	28	12	6	194	848	34
218	910	350	25	12	6	169	848	31
175	900	300	20	12	6	144	848	26
800WB192	816	300	28	10	5	145	748	34
168	810	275	25	10	5	133	748	31
146	800	275	20	10	5	133	748	26
122	792	250	16	10	5	120	748	22
700WB173	716	275	28	10	5	133	648	34
150	710	250	25	10	5	120	648	31
130	700	250	20	10	5	120	648	26
115	692	250	16	10	5	120	648	22

Note: Dimensions may not add correctly due to rounding.

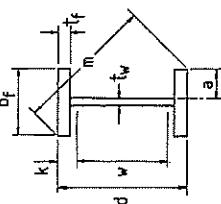


TABLE 10.1-2  
**WELDED COLUMNS**  
**RATIONALISED DIMENSIONS FOR DETAILING**

Designation	Depth of Section d	Flange		Web		Dimensions		
		Width b <sub>f</sub>	Thickness t <sub>f</sub>	t <sub>w</sub>	$\frac{t_w}{2}$	a	w	k
kg/m	mm	mm	mm	mm	mm	mm	mm	mm
500WC440	480	500	40	40	20	230	384	48
414	480	500	40	32	16	234	384	48
383	472	500	36	32	16	234	384	44
340	514	500	32	25	13	238	434	40
290	506	500	28	20	10	240	434	36
267	500	500	26	20	10	240	434	33
228	490	500	20	20	10	240	434	28
400WC361	430	400	40	40	20	180	334	48
328	430	400	40	28	14	186	334	48
303	422	400	36	28	14	186	334	44
270	414	400	32	25	13	188	334	40
212	400	400	26	20	10	190	334	33
181	390	400	20	20	10	190	334	28
144	382	400	16	16	8	192	334	24
350WC280	365	350	40	28	14	161	259	48
347	350	36	28	14	14	161	259	44
230	339	350	32	25	13	163	259	40
197	331	350	28	20	10	165	259	36

Note: Dimensions may not add correctly due to rounding.

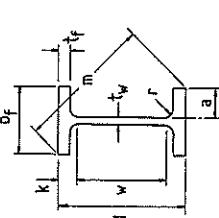


TABLE 10.1-3  
UNIVERSAL BEAMS  
RATIONALISED DIMENSIONS FOR DETAILING

Designation	Depth of Section $d$	Flange Width $b_f$	Flange Thickness $t_f$	Web Thickness $t_w$	Dimensions		
	mm	mm	mm	mm	a	w	k
610UB 25	612	229	20	12	6	109	544
610UB 113	607	228	17	11	6	108	544
602	602	228	15	11	5	109	544
530UB 92.4	533	209	16	10	5	99	474
522.0	528	209	13	10	5	100	474
460UB 82.1	460	191	16	10	5	91	406
457	457	190	15	9	5	90	406
67.1	454	190	13	9	4	91	406
4110UB 59.7	406	178	13	8	4	85	358
53.7	403	178	11	8	4	85	358
360UB 56.7	359	172	13	8	4	82	310
50.7	356	171	12	7	4	82	310
44.7	352	171	10	7	3	82	310
3110UB 46.2	307	166	12	7	3	80	261
40.4	304	165	10	6	3	79	261
32.0	298	149	8	6	3	72	256
25.7	248	124	8	5	3	60	208
200UB 37.3	256	146	11	6	3	70	217
31.4	252	146	9	6	3	70	217
25.7	248	124	8	5	2	47	162
180UB 29.8	207	134	10	6	3	64	170
25.4	203	133	8	6	3	64	170
22.3	202	133	7	5	2	64	170
18.2	198	99	7	5	2	60	208
180UB 22.2	179	90	10	6	3	64	170
18.1	175	90	8	5	3	64	170
16.1	173	90	7	5	2	64	170
150UB 18.0	155	75	10	6	3	35	120
14.0	150	75	7	5	3	35	120

Note: Dimensions may not add correctly due to rounding.

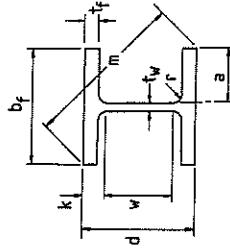


TABLE 10.1-4  
UNIVERSAL COLUMNS  
RATIONALISED DIMENSIONS FOR DETAILING

Designation	Depth of Section $d$	Flange Width $b_f$		Flange Thickness $t_f$		Web Thickness $t_w$		Dimensions
		kg/m	mm	kg/m	mm	kg/m	mm	
310UC 158	327	311	25	16	8	148	244	42
137	321	309	22	14	7	148	244	38
118	315	307	19	12	6	148	244	445
96.8	308	305	15	10	5	148	244	35
250UC 89.5	260	256	17	11	5	123	197	32
		72.9	254	14	9	123	197	43
200UC 59.5	210	205	14	9	5	98	159	28
		206	204	13	8	98	159	359
52.2	206	204	11	7	4	98	159	11
46.2	203	203	11	7	4	98	159	22
150UC 37.2	162	154	12	8	4	73	121	227
		30.0	158	9	7	3	73	9
23.4	152	152	7	6	3	73	121	220
100UC 14.8	97	99	7	5	3	47	63	16
		277	277	11	11	333	13	215

Note: Dimensions may not add correctly due to rounding.

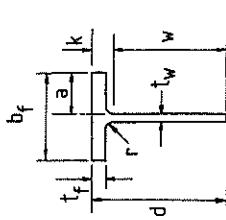


TABLE 10.1-5  
TEES CUT FROM UNIVERSAL BEAMS  
RATIONALISED DIMENSIONS FOR DETAILING

Designation	Cut from Universal Beam Section	Depth of Section $d$	Flange			Web			Dimensions		
			$b_f$	Width $t_f$	Thickness $\frac{t_w}{2}$	$b_f$	Width $t_f$	Thickness $\frac{t_w}{2}$	a	w	k
305BT62.5	610UB125	305	229	20	12	6	109	271	34	14	14
305.5	56.5	303	228	17	11	6	108	271	31	14	14
50.5	50.5	300	228	15	11	5	109	271	29	14	14
265BT46.3	530UB 92.4	266	209	16	10	5	99	236	30	14	14
41.0	82.0	263	209	13	10	5	100	236	27	14	14
230BT41.1	460UB 82.1	229	191	16	10	5	91	202	27	11	11
37.3	74.6	228	190	15	9	5	90	202	26	11	11
33.6	67.1	226	190	13	9	4	91	202,	24	11	11
205BT29.9	410UB 59.7	202	178	13	8	4	85	178	24	11	11
26.9	53.7	200	178	11	8	4	85	178	22	11	11
180BT28.4	360UB 56.7	178	172	13	8	4	82	154	12	8	8
25.4	50.7	177	171	12	7	4	82	154	11	7	7
22.4	44.7	175	171	10	7	3	82	154	11	7	7
155BT23.1	310UB 46.2	153	166	12	7	3	80	129	23	11	11
20.2	40.4	151	165	10	6	3	79	129	22	11	11
16.0	32.0	148	149	8	6	3	72	127	21	13	13
125BT8.7	250UB 37.3	127	146	11	6	3	70	107	20	9	9
15.7	31.4	125	146	9	6	3	60	103	20	12	12
12.0	25.7	123	124	8	5	3	60	103	20	12	12
100BT14.9	200UB 29.8	103	134	10	6	3	64	84	19	9	9
12.7	25.4	101	133	8	6	3	64	84	17	9	9
11.2	22.3	100	133	7	5	3	64	84	16	9	9
9.1	18.2	98	99	7	5	2	47	80	18	11	11
90BT11.1	180UB 22.2	89	90	10	6	3	42	70	19	9	9
9.1	18.1	87	90	8	5	3	43	70	17	9	9
8.1	16.1	86	90	7	5	2	43	70	16	9	9
75BT 9.0	150UB 18.0	77	75	10	6	3	35	59	18	8	8
7.0	14.0	74	75	7	6	3	35	59	15	8	8

Notes: (1) A 1 mm cutting allowance has been provided off each split tee.  
(2) Dimensions may not add correctly due to rounding.

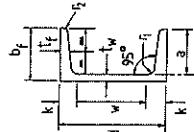


TABLE 10.1-7  
**PARALLEL FLANGE CHANNELS**  
RATIONALISED DIMENSIONS FOR DETAILING

Designation	Mass per m	Depth of Section d	Flange			Web			Dimensions			
			Width b_f	Thickness t_f	mm	Width t_w	Thickness t_f	mm	a	w	k	r
380 PFC	55.2	380	100	18	10	90	10	317	32	14		
300 PFC	40.1	300	90	16	8	82	82	240	30	14		
250 PFC	35.5	250	90	15	8	82	136	27	12			
230 PFC	25.1	230	75	12	7	89	182	24	12			
200 PFC	22.9	200	75	12	6	69	152	24	12			
180 PFC	20.9	180	75	11	6	69	134	23	12			
150 PFC	17.7	150	75	10	6	69	111	20	10			

Note: Dimensions may not add correctly due to rounding.

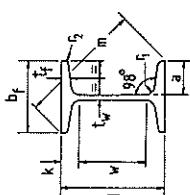


TABLE 10.1-8  
**TAPER FLANGE CHANNELS**  
RATIONALISED DIMENSIONS FOR DETAILING

Designation	Mass per m	Depth of Section d	Flange			Web			Dimensions			mm		
			Width b_f	Thickness t_f	mm	Width t_w	Thickness t_f	mm	a	w	k	r <sub>1</sub>	r <sub>2</sub>	mm
125 TFC	13.4	125	65	8	6	59	93	16	8	4				
100 TFC	9.34	100	50	8	5	45	69	16	8	4				
75 TFC	6.65	75	40	7	5	35	46	15	8	4				

Note: Dimensions may not add correctly due to rounding.

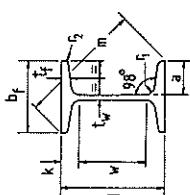
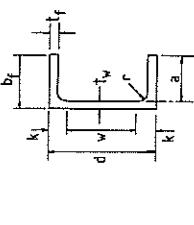


TABLE 10.1-9  
**TAPER FLANGE BEAMS**  
RATIONALISED DIMENSIONS FOR DETAILING

Designation	Mass per m	Depth of Section d	Flange			Web			Dimensions			mm		
			Width b_f	Thickness t_f	mm	Width t_w	Thickness t_f	mm	a	w	k	r <sub>1</sub>	r <sub>2</sub>	mm
125 TFB	13.1	125	65	9	5	3	30	92	17	14.1	8	4		
100 TFB	7.20	100	45	6	4	2	21	74	13	11.0	7	3		

Note: Dimensions may not add correctly due to rounding.



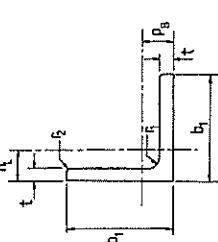


TABLE 10.1-10  
**EQUAL ANGLES**  
RATIONALISED DIMENSIONS FOR DETAILING

Designation	Mass per m	Dimensions			Centre of area $p_a = n_L$	Designation	Leg Size $b_1 \times b_1$	Ration'd Thick-ness	Dimensions			Centre of area $p_a = n_L$			
		Leg Size $b_1 \times b_1$	Actual Thickness						Ration'd Thick-ness	Mass per m	kg/m				
			1	$r_1$	$r_2$					mm	mm	mm			
200 x 200 x 26EA	76.8	26.0	18	5	59	65 x 65 x 10EA	8EA	9.02	9.5	6	3	20	150 x 100 x 12UA		
20EA	60.1	20.0	18	5	57	6EA	7.51	7.8	6	3	19	9.5	10UA		
18EA	54.4	18.0	18	5	56	6EA	5.87	6.0	6	3	18	18.0	10UA		
16EA	48.7	16.0	18	5	55	5EA	4.56	4.6	6	3	18	150 x 100 x 16UA			
13EA	40.0	13.0	18	5	54	55 x 55 x 6EA	4.93	6.0	6	3	16	12UA	10UA		
150 x 150 x 19EA	42.1	19.0	13	5	44	5EA	3.84	4.6	6	3	15	8UA	14.3		
16EA	35.4	15.8	13	5	43	50 x 50 x 8EA	5.68	7.8	6	3	15	125 x 75 x 12UA			
12EA	27.3	12.0	13	5	42	6EA	4.46	6.0	6	3	15	17.7	10UA		
10EA	21.9	9.5	13	5	41	5EA	3.48	4.6	6	3	14	14.2	8UA		
125 x 125 x 16EA	29.1	15.8	10	5	37	3EA	2.91	3.0	6	3	13	11.8	6UA		
12EA	22.5	12.0	10	5	35	45 x 45 x 6EA	3.97	6.0	5	3	13	9.16	9UA		
10EA	18.0	9.5	10	5	34	5EA	3.10	4.6	5	3	13	12.4	8UA		
8EA	14.9	7.8	10	5	34	3EA	2.06	3.0	5	3	12	10.3	6UA		
100 x 100 x 12EA	17.7	12.0	8	5	29	40 x 40 x 6EA	3.50	6.0	5	3	12	7.98	5UA		
10EA	14.2	9.5	8	5	28	5EA	2.73	4.6	5	3	11	5.66	6UA		
8EA	11.8	7.8	8	5	28	3EA	1.83	3.0	5	3	11	4.40	5UA		
6EA	9.2	6.0	8	5	27										
90 x 90 x 10EA	12.7	9.5	8	5	26	30 x 30 x 6EA	2.56	6.0	5	3	10	7.23	8UA		
8EA	10.6	7.8	8	5	25	5EA	2.01	4.6	5	3	9	7.8	6UA		
6EA	8.22	6.0	8	5	24	3EA	1.35	3.0	5	3	8	6.0	5UA		
75x 75 x 10EA	10.5	9.5	8	5	22	25 x 25 x 6EA	2.08	6.0	5	3	8	6.59	8UA		
8EA	8.73	7.8	8	5	21	5EA	1.65	4.6	5	3	8	5.16	6UA		
6EA	6.81	6.0	8	5	21	3EA	1.12	3.0	5	3	7	4.6	5UA		
5EA	5.27	4.6	8	5	20										

Note: Dimensions may not add correctly due to rounding.

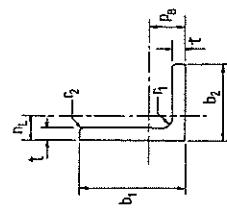
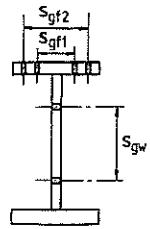


TABLE 10.1-11  
**UNEQUAL ANGLES**  
RATIONALISED DIMENSIONS FOR DETAILING

Designation	Leg Size $b_1 \times b_2$	Ration'd Thick-ness	Dimensions			Centre of area $p_a = n_L$	
			Leg Size $b_1 \times b_2$	Actual Thickness			Ration'd Thick-ness
				1	$r_1$	$r_2$	
150 x 100 x 12UA	150 x 100 x 12UA	12.0	12.0	10	5	49	24
10UA	10UA	9.5	10.0	10	5	48	23
8UA	8UA	8.0	8.5	10	5	50	20
6UA	6UA	6.5	7.0	10	5	49	20
5UA	5UA	5.0	5.5	10	5	51	21
4UA	4UA	4.0	4.5	10	5	52	23
3UA	3UA	3.0	3.5	10	5	50	20
2UA	2UA	2.0	2.5	10	5	51	21
1UA	1UA	1.0	1.5	10	5	52	23
0.5UA	0.5UA	0.5	0.5	10	5	53	24



### GAUGE LINES FOR WELDED SECTIONS

TABLE 10.2-1(A)

Section	M20				M24			
	Flange	$s_{gf1}$	Flange	$s_{gf2}$	Flange	$s_{gf1}$	Flange	$s_{gf2}$
<b>WELDED BEAMS</b>								
1200WB455-392	140	90	280	420	140	90	280	
1200WB342-278	140	90	280		140	90	280	
1200WB249	140	90			140	90		
1000WB322-258	140	90	280		140	90	280	
1000WB215	140	90			140	90		
900WB282,218	140	90	280		140	90	280	
900WB175	140	90			140	90		
800WB	140	90			140	90		
700WB	140	90			140	90		
<b>WELDED COLUMNS</b>								
500WC	140		280	420	140		280	
400WC	140		280		140		280	
350WC	140				140			
Preference	1	2	1	2	1	2	1	2

Note: All Dimensions are in mm.

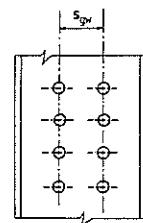


TABLE 10.2-1(B)

Section	Web $s_{gw}$					
	M20			M24		
<b>WELDED BEAMS</b>						
1200WB	140	90	70	140	90	70
1000WB	140	90	70	140	90	70
900WB	140	90	70	140	90	70
800WB	140	90	70	140	90	70
700WB	140	90	70	140	90	70
<b>WELDED COLUMNS</b>						
500WC	140	90	70	140	90	70
400WC	140	90	70	140	90	70
350WC	140	90	70	140	90	70
Preference	1	2	3	1	2	3

Note: All Dimensions are in mm.

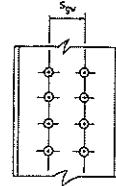
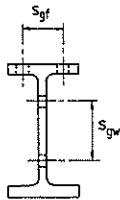


TABLE 10.2-2  
**GAUGE LINES FOR UNIVERSAL SECTIONS**

Section	Flange $s_{gf}$			Web $s_{gw}$					
	M20	M24		M20			M24		
<b>UNIVERSAL BEAMS</b>									
610UB	140	90		140	90	70	140	90	70
530UB	140	90		140	90	70	140	90	70
460UB	90	140		90	70	140	90	70	140
410UB	90	70		90	70	140	90	70	140
360UB, 310UB	90	70		90	70	140	90	70	140
310UB32.0	70			90	70	140			
250UB	70	90		70	90	140	70	90	140
250UB25.7*	70			70	90				
200UB	70			70	90		70	90	
200UB18.2*	50			70	90				
180UB	b			70	90		70	90	
150UB	b			70			70		
<b>UNIVERSAL COLUMNS</b>									
310UC	140	90		140	90		90	70	140
250UC	140	90		140	90		90	70	140
200UC	140	90		140	90		90	70	
150UC	90	70		90			70		
100UC	60			b			c		
Preference	1	2		1	2	3	1	2	3

Notes: \* Gauge listed for 250UB25.7 and 200 UB18.2 are for M16 bolts.

b — indicates that the flange will not accommodate this size of bolt.

c — indicates that the web will not accommodate two lines of bolts with a gauge of 50mm or more.

All Dimensions are in mm.

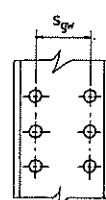
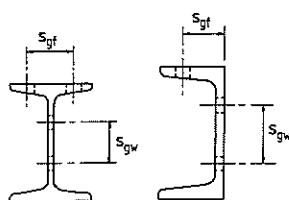


TABLE 10.2-3  
**GAUGE LINES FOR TAPER FLANGE BEAMS AND CHANNELS**

Section	Flange $s_{gf}$			Web $s_{gw}$					
	M16	M20	M24	M16			M20		M24
<b>TAPER FLANGE BEAMS</b>									
125 x 65	b			50			50		c
100 x 45	b			c			c		c
<b>PARALLEL FLANGE CHANNELS</b>									
380 x 100	55	55	55	140	90	70	140	90	70
300 x 90	55	55	b	140	90	70	140	90	70
250 x 90	55	55	b	140	90	70	140	90	70
230 x 75	45	45	b	140	90	70	90	70	70
200 x 75	45	45	b	90	70		90	70	70
180 x 75	45	45	b	70	90		70	90	70
150 x 75	45	45	b	70			65		55
<b>TAPER FLANGE CHANNELS</b>									
125 x 65	35	b	b	50			c		c
100 x 50	b	b	b	c			c		c
75 x 40	b	b	b	c			c		c
Preference	1	1	1	1	2	3	1	2	3

Notes: b — indicates that the flange will not accommodate this size of bolt.

c — indicates that the web will not accommodate two lines of bolts with a guage of 50mm or more.

All Dimensions are in mm.

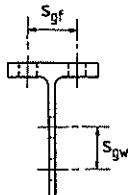
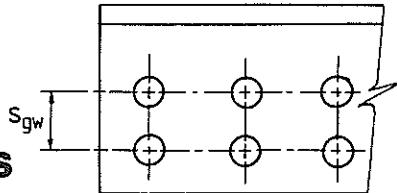


TABLE 10.2-4

**GAUGE LINES FOR STRUCTURAL TEES  
cut from Universal Sections**


Section	Flange $s_{gf}$				Web $s_{gw}$			
	M20		M24		M20		M24	
<b>TEES from Universal Beams</b>								
305BT	140	90	140	90	140	90	70	140
265BT	140	90	140	90	140	90	70	140
230BT	90	140	90		90	70	140	140
205BT	90	70	90		90	70	140	140
180BT	90	70	90		90	70	140	140
155BT	90	70	90		70			
155BT 16.0		70			70			
125BT	70	90			50		c	
125BT 12.9*	70				50			
100BT	70				c		c	
100BT 9.1*	50				c			
90BT	b				c		c	
75BT	b				c		c	
<b>TEES from Universal Columns</b>								
155CT	140	90	140	90	70		60	
125CT	140	90	140	90	50		c	
100CT	140	90	140	90	c		c	
75CT	90	70	90		c		c	
Preference	1	2	1	2	1	2	3	1
								3

Notes:  
\* Gauges listed for 125BT12.9 and 100BT 9.1 are for M16 bolts.  
b — indicates that the flange will not accommodate this size of bolt.  
c — indicates that the web will not accommodate two lines of bolts with a gauge of 50mm or more.  
All Dimensions are in mm.

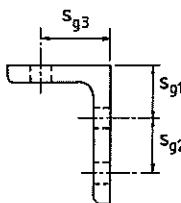
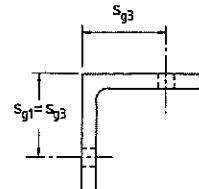


TABLE 10.2-5

**GAUGE LINES FOR ANGLES**


Nominal leg length	$s_{g1}$	$s_{g2}$	$s_{g3}$	Bolt
200	75	75	120	M24
150	55	55	90	M20
125	45	50	75	M20

Nominal leg length	$s_{g3}$	Bolt
100	55	M20
90	55	M20
75	45	M20
65	35	M16
55	35	M16
50	30	M16

## NOTES TO ALL TABLES OF GAUGE LINES:

- The gauges given are suitable for general use in member detailing. When angles are used as components in connections, gauge lines may be varied from the values given above in order to suit a particular connection. See Part 9 for a summary of AISC Standardised Structural Connections and standard components.
- The bolt diameters listed are the maximum that can be accommodated on the thickest angles of each leg length, using either —
  - (a) high strength structural bolts with washers to AS 1252; or
  - (b) commercial bolts with 'large series' washers to AS 1237.
For thinner legs and commercial bolts with 'normal series' washers, it may be possible to accommodate a larger bolt diameter.

TABLE 10.3-1

**DIMENSIONS OF COMMERCIAL BOLTS  
(AS 1111, AS 1112, AS 1237)**

Nom. dia.	Thread pitch	BOLT						NUT			WASHER		
		Thread run-out max.	Shank dia. nom.	Width across flats max.	Width across corners nom.	Height of head ave.	Areas		Width across flats AD	Width across corners shank AD	Height of normal nuts ave.	Outside dia. max.	Nominal thickness
							core	tensile stress $A_s$					
M12	1.75	8.75	12	18	21	8	76.2	84.3	113	18	21	11	24
M16	2.0	10	16	24	28	10	144	157	201	24	28	15	30
M20	2.5	12.5	20	30	35	13	225	245	314	30	35	18	37
M24	3.0	15	24	36	42	15	324	353	452	36	42	21	44
M30	3.5	17.5	30	46	53	19	519	561	706	46	53	25	56
M36	4.0	20	36	55	63	23	759	817	1016	55	63	30	66
													5

Note: All dimensions in mm or  $\text{mm}^2$ .
**DIMENSIONS OF HIGH STRENGTH STRUCTURAL BOLTS  
(AS 1252)**

Nom. dia.	Thread pitch	BOLT						NUT			WASHER		
		Thread run-out max.	Shank dia. nom.	Width across flats max.	Width across corners nom.	Height of head ave.	Areas		Width across flats $A_b$	Width across corners shank $A_b$	Height of normal nuts ave.	Outside dia. max.	Nominal thickness
							core	tensile stress $A_s$					
M16	2.0	6.0	16	27	31	10	144	157	201	27	31	17	34
M20	2.5	7.5	20	32	37	13	225	245	314	32	37	21	39
M24	3.0	9.0	24	41	47	15	324	353	452	41	47	25	50
M30	3.5	10.5	30	50	58	19	519	561	706	50	58	31	60
M36	4.0	12.0	36	60	69	23	759	817	1016	60	69	37	72
													4

Note: All dimensions in mm or  $\text{mm}^2$ .

**TABLE 10.4-1  
MASSES OF BOLTS  
COMMERCIAL BOLTS**

approximate masses in kilograms per 1000

Length under head in mm	Nominal Size of Bolt					Length under head in mm	Nominal Size of Bolt
	M12	M16	M20	M24	M30		
40	64.1	129	214			40	152
45	68.5	137	227			45	160
50	72.9	144	239	377		50	168
55	77.3	153	251	395		55	176
60	81.7	160	264	412		60	184
65	86.1	168	276	429		65	192
70	90.5	176	288	447		70	199
75	95.0	184	300	464		75	207
80	100	192	313	481		80	215
90	109	207	337	516	930	90	231
100	118	223	362	550	986	100	231
110	127	239	387	585	1042	110	231
120	136	255	411	620	1098	120	231
130	145	270	436	654	1154	130	231
140	154	286	460	689	1210	140	231
150	163	302	485	723	1256	150	231
160				758	1322	160	231
170					1378	170	
180					1434	180	
190					1480	190	
200					2089	200	
Approximate mass in kg of 1000 nuts	15.9	32.9	59.8	104	209	352	Approximate mass in kg of 1000 nuts
							55.7
							95.3
							194

**TABLE 10.4-2**

**MASSES OF BOLTS  
HIGH STRENGTH  
STRUCTURAL BOLTS**

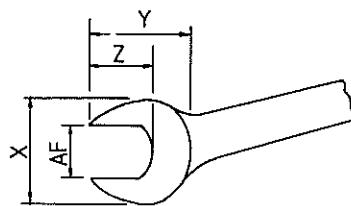
approximate masses in kilograms per 1000

Length under head in mm	Nominal Size of Bolt					Length under head in mm	Nominal Size of Bolt
	M16	M20	M24	M30	M36		
40	40					45	152
45	45					50	160
50	50					55	168
55	55					60	176
60	60					65	184
65	65					70	192
70	70					75	199
75	75					80	207
80	80					85	215
90	90					90	223
100	100					100	231
110	110					110	231
120	120					120	231
130	130					130	231
140	140					140	231
150	150					150	231
160	160					160	231
170						170	
180						180	
190						190	
200						200	
Approximate mass in kg of 1000 nuts	15.9	32.9	59.8	104	209	352	Approximate mass in kg of 1000 nuts
							55.7
							95.3
							194

Source: "Metric Practice for Structural Steelwork", 3rd Edn., Publication No. 5/79, British Constructional Steelwork Association.

## DIMENSIONS OF WRENCHES

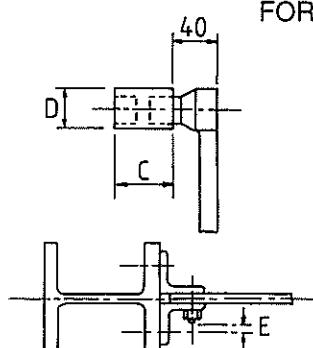
DIMENSIONS OF OPEN ENDED WRENCHES  
FOR DETERMINING ERECTION CLEARANCES  
4.6/S and 8.8/S PROCEDURES



AF = dimension across flats to suit bolt.

Bolt Size	Clearance		
	X	Y	Z
16	52	45	28
20	65	56	35
24	78	67	41
30	99	85	53
36	118	102	63

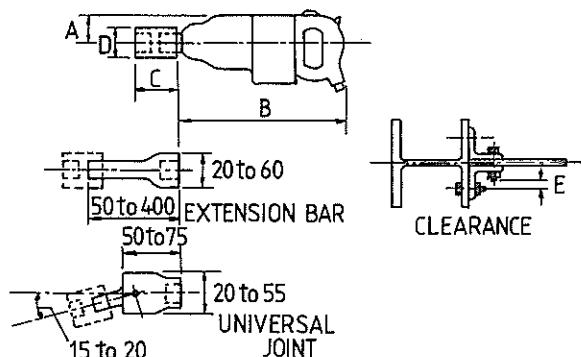
DIMENSIONS OF SOCKETS – HAND WRENCHES  
FOR DETERMINING ERECTION CLEARANCES  
8.8/TF AND 8.8/TB PROCEDURES



Bolt Size	Normal Sockets *		Clearance E
	C	D	
16	50	38	25
20	60	45	30
24	80	57	35

CLEARANCE

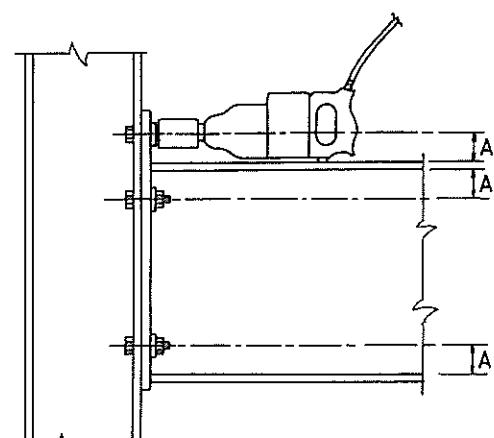
DIMENSIONS OF SOCKETS – IMPACT WRENCHES  
FOR DETERMINING ERECTION CLEARANCES  
8.8/TF AND 8.8/TB PROCEDURES



Larger sizes (M30, M36) of the high strength structural bolt should be treated with caution, especially when full tensioning to the requirements of AS 4100 Clause 15.2.5, since on-site-tensioning can be difficult and requires special equipment to achieve the minimum bolt tensions specified in AS 4100

	Capacity	B	A
Normal Wrenches	to 24	to 450 some to 600	54
Heavy Wrenches			65

Normal Sockets *			Clearance E
Bolt Size	C	D	
16	50	38	25
20	60	45	30
24	80	57	35
30	90	70	40
36	100	80	45



\* Deep length sockets are also available with greater length but same diameter as above. Bolt diameters above M24 cannot be tensioned with a hand wrench.

**PART 11 FLOOR PLATES**

	PAGE
<b>11.1 Details .....</b>	<b>11-2</b>
<b>11.2 Design Formulae.....</b>	<b>11-2</b>
<b>11.3 Maximum Design Loads .....</b>	<b>11-5</b>
11.3.1 Plate Properties .....	11-5
11.3.2 General Notes on Tables 11.3-1 to 11.3-14.....	11-5
11.3.3 Strength Limit State .....	11-6
11.3.4 Serviceability Limit State .....	11-6

**TABLES**

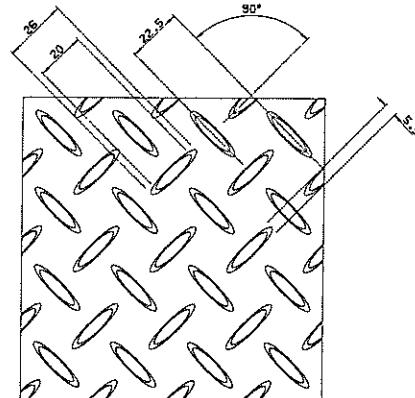
<b>TABLE 11.2</b>	
Design Formulae .....	11-3
<b>TABLES 11.3-1 to 11.3-14</b>	
Maximum Design Loads .....	11-7

**PART 11 FLOOR PLATES****11.1 Details**

Floor plate is characterised by a raised angular pattern (see Pattern Details below) rolled on to one surface. The pattern facilitates cleaning and draining while retaining the required non-slip characteristics. The nominal thickness of floor plate is exclusive of the raised pattern (see note on 'Mass of Floor Plate' below).

***Pattern Details*****Pattern Notes:**

1. All dimensions are in millimetres and are approximate.
2. Pattern projections are approximately 1.5 mm in height.



BHP Steel floor plate pattern

***Floor Plates – Preferred Width, Thickness and Length Combinations*****Preferred Length in metres**

Preferred Width (mm)	Preferred Thickness (mm)					
	3	5	6	8	10	12
1200	6	6	6	–	–	–
1500	–	6	6	6	–	–
1800	–	–	6	6	6	6

TABLE 11.1

**Mass of Floor Plate**

When calculating the design mass of floor plate, add 2.0 kg/m<sup>2</sup> to the mass of plain plate of the same dimensions.

**11.2 Design Formulae**

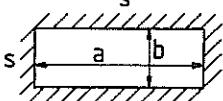
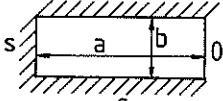
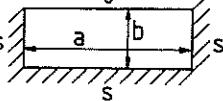
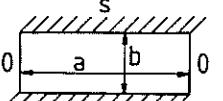
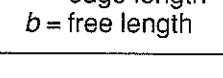
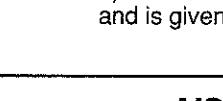
Table 11.2 gives the design formulae for the *Maximum Design Bending Moment*,  $M_m^*$ , and the *Maximum Deflection*,  $\Delta$ , of plates with various support conditions. These formulae have been referenced from:

- *Theory of Plates and Shells*, Timoshenko, S. and Woinowsky-Krieger, S., McGraw-Hill, 2nd Edition, 1959.
- *Roark's Formulas for Stress and Strain*, Young, W.C., McGraw-Hill, 6th Edition, 1989.

**Note:**

- 1) The self weight of the plate has not been deducted from these formulae.
- 2) For highly concentrated loads the designer must also check the transverse shear design actions which have not been tabulated.

TABLE 11.2

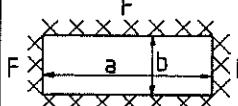
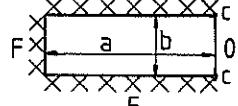
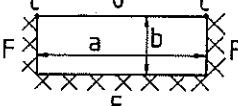
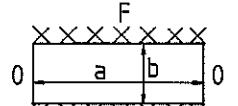
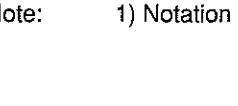
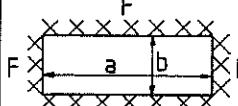
Floor Plate Shape	Loading	Maximum Design Bending Moment, $M_m^*$ Maximum Design Deflection, $\Delta^*$																																	
 $t$ = thickness $a$ = long side $b$ = short side	1. Uniform, $q^*$	At centre: $M_m^* = \beta q^* b^2 \quad \Delta^* = \alpha \frac{q^* b^4}{E t^3}$ <table border="1"> <tr><td><math>\%_b</math></td><td>1.0</td><td>1.2</td><td>1.4</td><td>1.6</td><td>1.8</td><td>2.0</td><td>3.0</td><td>4.0</td><td>5.0</td><td><math>\infty</math></td></tr> <tr><td><math>\alpha</math></td><td>.0443</td><td>.0616</td><td>.0770</td><td>.0906</td><td>.102</td><td>.111</td><td>.134</td><td>.140</td><td>.143</td><td>.142</td></tr> <tr><td><math>\beta</math></td><td>.0479</td><td>.0627</td><td>.0775</td><td>.0862</td><td>.0948</td><td>.102</td><td>.119</td><td>.124</td><td>.125</td><td>.125</td></tr> </table>	$\%_b$	1.0	1.2	1.4	1.6	1.8	2.0	3.0	4.0	5.0	$\infty$	$\alpha$	.0443	.0616	.0770	.0906	.102	.111	.134	.140	.143	.142	$\beta$	.0479	.0627	.0775	.0862	.0948	.102	.119	.124	.125	.125
		$\%_b$	1.0	1.2	1.4	1.6	1.8	2.0	3.0	4.0	5.0	$\infty$																							
$\alpha$	.0443	.0616	.0770	.0906	.102	.111	.134	.140	.143	.142																									
$\beta$	.0479	.0627	.0775	.0862	.0948	.102	.119	.124	.125	.125																									
(see Note 2 below for a description of $r_0'$ )																																			
 $t$ = thickness $a$ = long side $b$ = short side	2. Central concentrated $P^*$ , (modelled as a uniform load over a small concentric circle of radius $r_0'$ )	At centre: $M_m^* = \frac{P^*}{4\pi} [1.3 \log_e \left( \frac{2b}{\pi r_0'} \right) + \beta]$ $\Delta^* = \alpha \frac{P^* b^2}{E t^3}$ <table border="1"> <tr><td><math>\%_b</math></td><td>1.0</td><td>1.2</td><td>1.4</td><td>1.6</td><td>1.8</td><td>2.0</td><td><math>\infty</math></td></tr> <tr><td><math>\alpha</math></td><td>.127</td><td>.148</td><td>.162</td><td>.172</td><td>.177</td><td>.181</td><td>.185</td></tr> <tr><td><math>\beta</math></td><td>.435</td><td>.650</td><td>.789</td><td>.875</td><td>.927</td><td>.958</td><td>1.00</td></tr> </table>	$\%_b$	1.0	1.2	1.4	1.6	1.8	2.0	$\infty$	$\alpha$	.127	.148	.162	.172	.177	.181	.185	$\beta$	.435	.650	.789	.875	.927	.958	1.00									
		$\%_b$	1.0	1.2	1.4	1.6	1.8	2.0	$\infty$																										
$\alpha$	.127	.148	.162	.172	.177	.181	.185																												
$\beta$	.435	.650	.789	.875	.927	.958	1.00																												
(see Note 2 below for a description of $r_0'$ )																																			
 $t$ = thickness $a$ = long side $b$ = short side	3. Uniform, $q^*$	At centre of free edge: $M_m^* = \beta q^* b^2 \quad \Delta^* = \alpha \frac{q^* b^4}{E t^3}$ <table border="1"> <tr><td><math>\%_b</math></td><td>1.0</td><td>1.1</td><td>1.2</td><td>1.3</td><td>1.4</td><td>1.5</td><td>2.0</td><td>3.0</td><td><math>\infty</math></td></tr> <tr><td><math>\alpha</math></td><td>.140</td><td>.146</td><td>.151</td><td>.155</td><td>.157</td><td>.160</td><td>.165</td><td>.166</td><td>.166</td></tr> <tr><td><math>\beta</math></td><td>.112</td><td>.117</td><td>.121</td><td>.124</td><td>.126</td><td>.128</td><td>.132</td><td>.133</td><td>.133</td></tr> </table>	$\%_b$	1.0	1.1	1.2	1.3	1.4	1.5	2.0	3.0	$\infty$	$\alpha$	.140	.146	.151	.155	.157	.160	.165	.166	.166	$\beta$	.112	.117	.121	.124	.126	.128	.132	.133	.133			
		$\%_b$	1.0	1.1	1.2	1.3	1.4	1.5	2.0	3.0	$\infty$																								
$\alpha$	.140	.146	.151	.155	.157	.160	.165	.166	.166																										
$\beta$	.112	.117	.121	.124	.126	.128	.132	.133	.133																										
No solution readily available.																																			
 $t$ = thickness $a$ = long side $b$ = short side	5. Uniform, $q^*$	At centre of free edge: $M_m^* = \beta q^* a^2 \quad \Delta^* = \alpha \frac{q^* a^4}{E t^3}$ <table border="1"> <tr><td><math>\%_b</math></td><td>1.0</td><td>1.1</td><td>1.2</td><td>1.3</td><td>1.4</td><td>1.5</td><td>2.0</td></tr> <tr><td><math>\alpha</math></td><td>.140</td><td>.135</td><td>.126</td><td>.119</td><td>.112</td><td>.106</td><td>.0775</td></tr> <tr><td><math>\beta</math></td><td>.112</td><td>.107</td><td>.100</td><td>.094</td><td>.088</td><td>.083</td><td>.060</td></tr> </table>	$\%_b$	1.0	1.1	1.2	1.3	1.4	1.5	2.0	$\alpha$	.140	.135	.126	.119	.112	.106	.0775	$\beta$	.112	.107	.100	.094	.088	.083	.060									
		$\%_b$	1.0	1.1	1.2	1.3	1.4	1.5	2.0																										
$\alpha$	.140	.135	.126	.119	.112	.106	.0775																												
$\beta$	.112	.107	.100	.094	.088	.083	.060																												
No solution readily available.																																			
 $t$ = thickness $a$ = simply supported edge length $b$ = free length	7. Uniform, $q^*$	At centre of free edge: $M_m^* = \beta q^* b^2 \quad \Delta^* = \alpha \frac{q^* b^4}{E t^3}$ <table border="1"> <tr><td><math>\%_b</math></td><td>0.5</td><td>1.0</td><td>2.0</td><td><math>\infty</math></td></tr> <tr><td><math>\alpha</math></td><td>.158</td><td>.165</td><td>.166</td><td>.166</td></tr> <tr><td><math>\beta</math></td><td>.126</td><td>.132</td><td>.133</td><td>.133</td></tr> </table>	$\%_b$	0.5	1.0	2.0	$\infty$	$\alpha$	.158	.165	.166	.166	$\beta$	.126	.132	.133	.133																		
		$\%_b$	0.5	1.0	2.0	$\infty$																													
$\alpha$	.158	.165	.166	.166																															
$\beta$	.126	.132	.133	.133																															
Note as $\%_b \rightarrow 0$ then $\alpha \rightarrow 0.156$ and $\beta \rightarrow 0.125$																																			
 $t$ = thickness $a$ = simply supported edge length $b$ = free length	8. Central concentrated, $P^*$	No solution readily available.																																	

Note: 1) Notation for Support Conditions: //s – simple support along edge.

o – unsupported, free edge.

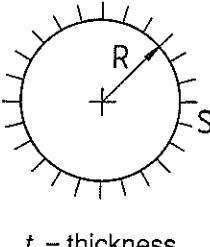
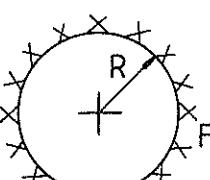
2) For concentrated loads,  $r_0'$  is the equivalent radius of contact for a load concentrated on a very small area and is given by  $r_0' = \sqrt{(1.67t^2 + l^2)}$ , 0.675 if  $r_0' < 0.5$  and  $r_0' = r_0$  if  $r_0' > 0.5$  ( $r_0$  is the radius of the load area).

TABLE 11.2 (cont'd)

Floor Plate Shape	Loading	Maximum Design Bending Moment, $M_m^*$ Maximum Design Deflection, $\Delta^*$																								
 $t$ = thickness $a$ = long side $b$ = short side	9. Uniform, $q^*$	<p>At centre of long edge: <math>M_m^* = \beta q^* b^2</math></p> <p>At centre of plate: <math>\Delta^* = \alpha \frac{q^* b^4}{Et^3}</math></p> <table border="1"> <thead> <tr> <th><math>\frac{a}{b}</math></th><th>1.0</th><th>1.2</th><th>1.4</th><th>1.6</th><th>1.8</th><th>2.0</th><th><math>\infty</math></th></tr> </thead> <tbody> <tr> <td><math>\alpha</math></td><td>.0138</td><td>.0188</td><td>.0226</td><td>.0251</td><td>.0268</td><td>.0277</td><td>.0284</td></tr> <tr> <td><math>\beta</math></td><td>.0513</td><td>.0639</td><td>.0726</td><td>.0780</td><td>.0812</td><td>.0829</td><td>.0833</td></tr> </tbody> </table>	$\frac{a}{b}$	1.0	1.2	1.4	1.6	1.8	2.0	$\infty$	$\alpha$	.0138	.0188	.0226	.0251	.0268	.0277	.0284	$\beta$	.0513	.0639	.0726	.0780	.0812	.0829	.0833
$\frac{a}{b}$	1.0	1.2	1.4	1.6	1.8	2.0	$\infty$																			
$\alpha$	.0138	.0188	.0226	.0251	.0268	.0277	.0284																			
$\beta$	.0513	.0639	.0726	.0780	.0812	.0829	.0833																			
 $t$ = thickness $a$ = long side $b$ = short side	10. Central concentrated, $P^*$	<p>At centre of long edge: <math>M_m^* = \beta P^*</math></p> <p>At centre of plate: <math>\Delta^* = \alpha \frac{P^* b^2}{Et^3}</math></p> <table border="1"> <thead> <tr> <th><math>\frac{a}{b}</math></th><th>1.0</th><th>1.2</th><th>1.4</th><th>1.6</th><th>1.8</th><th>2.0</th><th><math>\infty</math></th></tr> </thead> <tbody> <tr> <td><math>\alpha</math></td><td>.0612</td><td>.0706</td><td>.0755</td><td>.0777</td><td>.0786</td><td>.0788</td><td>.0792</td></tr> <tr> <td><math>\beta</math></td><td>.126</td><td>.149</td><td>.160</td><td>.165</td><td>.167</td><td>.167</td><td>.168</td></tr> </tbody> </table>	$\frac{a}{b}$	1.0	1.2	1.4	1.6	1.8	2.0	$\infty$	$\alpha$	.0612	.0706	.0755	.0777	.0786	.0788	.0792	$\beta$	.126	.149	.160	.165	.167	.167	.168
$\frac{a}{b}$	1.0	1.2	1.4	1.6	1.8	2.0	$\infty$																			
$\alpha$	.0612	.0706	.0755	.0777	.0786	.0788	.0792																			
$\beta$	.126	.149	.160	.165	.167	.167	.168																			
 $t$ = thickness $a$ = long side $b$ = short side	11. Uniform, $q^*$	<p>At point 'C': <math>M_m^* = \beta q^* b^2</math></p> <p>At centre of free edge: <math>\Delta^* = \alpha \frac{q^* b^4}{Et^3}</math></p> <table border="1"> <thead> <tr> <th><math>\frac{a}{b}</math></th><th>1.0</th><th>1.25</th><th>1.50</th></tr> </thead> <tbody> <tr> <td><math>\alpha</math></td><td>.0364</td><td>.0377</td><td>.0366</td></tr> <tr> <td><math>\beta</math></td><td>.0853</td><td>.0867</td><td>.0842</td></tr> </tbody> </table>	$\frac{a}{b}$	1.0	1.25	1.50	$\alpha$	.0364	.0377	.0366	$\beta$	.0853	.0867	.0842												
$\frac{a}{b}$	1.0	1.25	1.50																							
$\alpha$	.0364	.0377	.0366																							
$\beta$	.0853	.0867	.0842																							
 $t$ = thickness $a$ = long side $b$ = short side	12. Central concentrated, $P^*$	No solution readily available.																								
 $t$ = thickness $a$ = long side $b$ = short side	13. Uniform, $q^*$	<p>At point 'C': <math>M_m^* = \beta q^* a^2</math></p> <p>At centre of free edge: <math>\Delta^* = \alpha \frac{q^* a^4}{Et^3}</math></p> <table border="1"> <thead> <tr> <th><math>\frac{a}{b}</math></th><th>1.00</th><th>1.11</th><th>1.25</th><th>1.43</th><th>1.67</th></tr> </thead> <tbody> <tr> <td><math>\alpha</math></td><td>.0364</td><td>.0353</td><td>.0336</td><td>.0319</td><td>.0296</td></tr> <tr> <td><math>\beta</math></td><td>.0853</td><td>.0836</td><td>.0812</td><td>.0782</td><td>.0745</td></tr> </tbody> </table>	$\frac{a}{b}$	1.00	1.11	1.25	1.43	1.67	$\alpha$	.0364	.0353	.0336	.0319	.0296	$\beta$	.0853	.0836	.0812	.0782	.0745						
$\frac{a}{b}$	1.00	1.11	1.25	1.43	1.67																					
$\alpha$	.0364	.0353	.0336	.0319	.0296																					
$\beta$	.0853	.0836	.0812	.0782	.0745																					
	14. Central concentrated, $P^*$	No solution readily available.																								
 $t$ = thickness $a$ = long side $b$ = short side	15. Uniform, $q^*$	<p>Approximate bending moment and deflection distribution to that of a plate bent to a cylindrical surface.</p> <p>Along fixed edge: <math>M_m^* = q^* \frac{b^2}{12}</math></p> <p>At centre of free edge: <math>\Delta^* = \frac{q^* b^4}{6400 \times 10^3 t^3}</math></p>																								
	16. Central concentrated, $P^*$	No solution readily available.																								

Note: 1) Notation for Support Conditions:  
 XXXF – fixed support along edge.  
 O – unsupported, free edge.

TABLE 11.2 (cont'd)

Floor Plate Shape	Loading	Maximum Design Bending Moment, $M_m^*$ Maximum Design Deflection, $\Delta^*$
 $t = \text{thickness}$	17. Uniform, $q^*$	At centre of plate: $M_m^* = 0.206 q^* R^2$ $\Delta^* = 0.695 \frac{q^* R^4}{E t^3}$
	18. Central concentrated, $P^*$	At centre of plate: $M_m^* = \frac{P^*}{6} [1.30 (0.485 \log_e \left(\frac{R}{t}\right) + 0.52) + 0.48]$ $\Delta^* = 0.550 \frac{P^* R^2}{E t^3}$
 $t = \text{thickness}$	19. Uniform, $q^*$	At plate circumference: $M_m^* = 0.125 q^* R^2 \quad (\text{in radial direction})$ At centre of plate: $\Delta^* = 0.171 \frac{q^* R^4}{E t^3}$
	20. Central concentrated, $P^*$	At plate circumference: $M_m^* = \frac{P^*}{6} [1.30 (0.485 \log_e \left(\frac{R}{t}\right) + 0.52)]$ At centre of plate: $\Delta^* = 0.220 \frac{P^* R^2}{E t^3}$

Note: 1) Notation for Support Conditions:    // / S – Simple support around circumference  
XXXF – Fixed support around circumference.

## 11.3 Maximum Design Loads

### 11.3.1 Plate Properties

The following design capacity tables have been determined from the following **plate material criteria**:

- Grade 250 Plate to AS 3678
- Modulus of Elasticity,  $E = 200 \times 10^3 \text{ MPa}$

### 11.3.2 General Notes on Tables 11.3-1 to 11.3-14

A check should be made on the plate strength and serviceability limit states. Usually, the design of floor plates in two-way bending will be governed by the serviceability limit state.

The notation used in these Tables are:

- $D_{sv}$  deflection factor ( $= \Delta^*/q^*$  or  $\Delta^*/P^*$ ) for serviceability limit state
- $P^*$  design central concentrated load for strength or serviceability limit state
- $P_{st}^*$  maximum design load for strength limit state
- $q^*$  design uniformly distributed load for strength or serviceability limit state
- $q_{st}^*$  maximum design uniformly distributed load for strength limit state

$\Delta_m^*$	maximum design deflection due to serviceability design loads ( $q^*$ or $P^*$ )
$\Delta_{ml}$	maximum design deflection limit for serviceability limit state
$\phi$	capacity factor (=0.9)

The designer must include plate self weight multiplied by the appropriate load factor when determining the plate design loads (i.e.  $P^*$  and  $q^*$ ). Note that the design loads  $P^*$  and  $q^*$  are different for the strength and serviceability limit states.

### 11.3.3 Strength Limit State

No specific clauses are given for floor plates in AS 4100 but some guidance is given in AS 4100 Supplement 1-1990. For the strength limit state, floor plates may be designed as compact sections with full lateral restraint, ie.  $Z_e = 1.5Z$ . The plate design moment capacity,  $\phi M_s$ , is determined by

$$\phi M_s = \phi f_y Z_e$$

Maximum design loads ( $q_{st}^*$  and  $P_{st}^*$ ) for the various load and support situations have been determined from  $\phi M_s$  and the elastic relationship between load and moment given in Section 11.2. The maximum design loads are given in Tables 11.3-1 to 11.3-14. When using these tables, the following procedure should be used.

- (i) assess the strength limit state *design load* ( $q^*$  or  $P^*$ );
- (ii) determine the *maximum design load* ( $q_{st}^*$  or  $P_{st}^*$  – whichever is applicable) from Tables 11.3-1 to 11.3-14;
- (iii) the following strength limit state inequality must be satisfied –

$$q^* \leq q_{st}^* \quad \text{or} \quad P^* \leq P_{st}^*$$

If this is not satisfied, a change in one of the plate or loading parameters is required and steps (i) to (iii) repeated. The above inequality would be on the conservative side if an analysis by a failure criterion (Yield Line, Von Mises, etc) was also undertaken.

### 11.3.4 Serviceability Limit State

When using Tables 11.3-1 to 11.3-14 the following method should be used when examining the serviceability limit state:

- (i) determine the serviceability limit state *design load* ( $q^*$  or  $P^*$ );
- (ii) assess the maximum design deflection limit ( $\Delta_{ml}$ ) for the serviceability limit state;
- (iii) either, calculate the *maximum design deflection* ( $\Delta_m^*$ ) from the relevant design formulae of Section 9.2 above, or determine the *deflection factor* ( $D_{sv}$ ) from Tables 11.3-1 to 11.3-14, and multiply by  $q_{sv}^*$  or  $P_{sv}^*$  (whichever is applicable) to get the maximum design deflection ( $\Delta_m^*$ ), i.e.

$$\Delta_m^* = D_{sv} \times (q^* \text{ or } P^*)$$

- (iv) the following inequality must be satisfied –

$$\Delta_m^* \leq \Delta_{ml}$$

If this is not satisfied, a change in one of the plate or loading parameters is required and steps (i) to (iv) repeated.

*Note: The designer must ensure that there is no plate yielding under serviceability loads.*

**FLOOR PLATES  
GRADE 250**

**uniformly distributed load**

TABLE 11.3-1

**MAXIMUM DESIGN LOADS FOR  
PLATES SIMPLY SUPPORTED ON FOUR SIDES**

central concentrated load

TABLE 11.3-2

		Uniform Load Over Whole Floor Plate						Concentrated Load at Centre of Plate					
Thickness t mm	Dimension f <sub>y</sub> MPa	Maximum Design Load, q <sub>s</sub> (kPa) Deflection factor D <sub>s</sub> (mm/kN-a)						Maximum Design Load, P <sub>s</sub> (kN) Deflection factor D <sub>s</sub> (mm/kN) for Dimension a (mm)					
		600	800	1000	1200	1600	2000	2400	600	800	1000	1200	1600
5	280	600	91.3	60.3	49.1	42.9	38.6	36.3	35.3	5	280	600	5.28
	280	800	0.230	0.373	0.489	0.575	0.655	0.705	0.726	5	280	600	4.88
	280	1000	0.726	51.4	37.1	30.1	24.1	22.3	20.7	800	1.83	2.27	2.50
	280	1200	1.77	32.9	1.07	1.37	1.82	2.01	2.20	1000	3.25	5.28	4.78
	280	132	0.133	0.216	0.283	0.353	0.379	0.408	0.420	1200	5.08	5.92	5.28
	280	800	0.420	74.0	53.4	43.3	34.7	32.1	29.8	6	280	600	7.61
6	280	1000	47.3	0.621	0.795	1.05	1.16	1.27	1.37	800	1.06	1.31	1.45
	280	1200	1.03	36.2	26.3	22.2	20.8	20.8	20.8	1000	1.88	2.54	2.24
	280	132	32.9	1.43	2.10	2.57	2.78	2.78	2.78	1200	2.94	3.43	2.94
	280	800	0.133	0.216	0.283	0.353	0.379	0.408	0.420	6	280	600	7.61
	280	1000	0.420	74.0	53.4	43.3	34.7	32.1	29.8	800	1.06	1.31	1.45
	280	1200	2.13	32.9	21.7	17.7	15.4	15.4	15.4	6	280	600	7.61
8	280	132	154	126	110	98.8	92.8	90.3	90.3	8	280	600	13.5
	280	800	0.0561	132	94.9	77.0	61.8	57.0	52.9	800	0.446	0.553	12.1
	280	1000	0.177	0.262	0.335	0.444	0.490	0.536	0.586	1000	0.794	0.947	13.5
	280	1200	0.453	84.2	64.3	46.8	39.5	37.1	37.1	1200	1.24	1.45	12.8
	280	132	0.0287	224	182	159	143	135	131	10	260	600	19.6
	280	800	0.0166	275	198	161	112	99.6	82.7	800	0.229	0.283	17.5
10	280	1000	0.0907	0.134	0.172	0.227	0.251	0.274	0.274	1000	0.406	0.485	19.6
	280	1200	0.222	122	93.3	67.9	57.4	53.8	53.8	1200	0.635	0.740	19.6
	280	132	0.0287	339	224	182	159	143	131	10	260	600	19.6
	280	800	0.0166	275	198	161	112	99.6	82.7	800	0.229	0.283	17.5
	280	1000	0.0907	0.134	0.172	0.227	0.251	0.274	0.274	1000	0.406	0.485	19.6
	280	1200	0.222	122	93.3	67.9	57.4	53.8	53.8	1200	0.635	0.740	19.6
12	280	132	0.0287	322	263	229	206	194	189	12	260	600	28.3
	280	800	0.0166	275	198	161	112	99.6	82.7	800	0.132	0.164	25.2
	280	1000	0.0907	0.0525	0.0776	0.0993	0.132	0.145	0.159	1000	0.235	0.281	28.3
	280	1200	0.222	122	93.3	67.9	57.4	53.8	53.8	1200	0.367	0.428	28.3
	280	132	0.0287	322	263	229	206	194	189	12	260	600	28.3
	280	800	0.0166	275	198	161	112	99.6	82.7	800	0.132	0.164	25.2

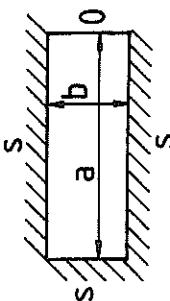
Note: Grade 250 Steel Plate to AS 3678.

		Concentrated Load at Centre of Plate						Maximum Design Load, P <sub>s</sub> (kN) Deflection factor D <sub>s</sub> (mm/kN) for Dimension a (mm)					
Thickness t mm	Dimension f <sub>y</sub> MPa	Concentrated Load at Centre of Plate						Maximum Design Load, P <sub>s</sub> (kN) Deflection factor D <sub>s</sub> (mm/kN) for Dimension a (mm)					
		600	800	1000	1200	1600	2000	600	800	1000	1200	1600	2400
5	280	600	91.3	60.3	49.1	42.9	38.6	36.3	35.3	5	280	600	5.28
	280	800	0.230	0.373	0.489	0.575	0.655	0.705	0.726	5	280	600	4.88
	280	1000	0.726	51.4	37.1	30.1	24.1	22.3	20.7	800	1.88	2.54	2.24
	280	1200	1.77	32.9	1.07	1.37	1.82	2.01	2.20	1000	2.94	3.43	2.94
	280	132	2.13	22.8	15.1	12.3	10.7	10.7	10.7	1200	5.08	5.92	6.88
	280	800	0.133	0.216	0.283	0.353	0.379	0.408	0.420	6	280	600	7.61
6	280	1000	0.420	74.0	53.4	43.3	34.7	32.1	29.8	800	1.06	1.31	1.45
	280	1200	1.03	36.2	26.3	22.2	20.8	20.8	20.8	1000	1.88	2.54	2.24
	280	132	2.13	32.9	21.7	17.7	15.4	15.4	15.4	1200	2.94	3.43	2.94
	280	800	0.133	0.216	0.283	0.353	0.379	0.408	0.420	6	280	600	7.61
	280	1000	0.420	74.0	53.4	43.3	34.7	32.1	29.8	800	1.06	1.31	1.45
	280	1200	2.13	32.9	21.7	17.7	15.4	15.4	15.4	6	280	600	7.61
8	280	132	154	126	110	98.8	92.8	90.3	90.3	8	280	600	13.5
	280	800	0.0561	132	94.9	77.0	61.8	57.0	52.9	800	0.446	0.553	12.1
	280	1000	0.177	0.262	0.335	0.444	0.490	0.536	0.586	1000	0.794	0.947	13.5
	280	1200	0.453	84.2	64.3	46.8	39.5	37.1	37.1	1200	1.24	1.45	12.8
	280	132	0.0287	224	182	159	143	135	131	10	260	600	19.6
	280	800	0.0166	275	198	161	112	99.6	82.7	800	0.229	0.283	17.5
10	280	1000	0.0907	0.134	0.172	0.227	0.251	0.274	0.274	1000	0.406	0.485	19.6
	280	1200	0.222	122	93.3	67.9	57.4	53.8	53.8	1200	0.635	0.740	19.6
	280	132	0.0287	339	224	182	159	143	131	10	260	600	19.6
	280	800	0.0166	275	198	161	112	99.6	82.7	800	0.229	0.283	17.5
	280	1000	0.0907	0.134	0.172	0.227	0.251	0.274	0.274	1000	0.406	0.485	19.6
	280	1200	0.222	122	93.3	67.9	57.4	53.8	53.8	1200	0.635	0.740	19.6
12	280	132	0.0287	322	263	229	206	194	189	12	260	600	28.3
	280	800	0.0166	275	198	161	112	99.6	82.7	800	0.132	0.164	25.2
	280	1000	0.0907	0.0525	0.0776	0.0993	0.132	0.145	0.159	1000	0.235	0.281	28.3
	280	1200	0.222	122	93.3	67.9	57.4	53.8	53.8	1200	0.367	0.428	28.3
	280	132	0.0287	322	263	229	206	194	189	12	260	600	28.3
	280	800	0.0166	275	198	161	112	99.6	82.7	800	0.132	0.164	25.2

Notes: (1) The values listed in this table are based on the formula in Loading configuration 2 on page 11-3. The ratio of b (= the length of the short side of the plate), to r' (= the equivalent radius of contact) in this equation is taken as 20, ie, b/r' = 20.

(2) Grade 250 Steel Plate to AS 3678.

DCT/02/V1-1994



**FLOOR PLATES  
GRADE 250**

**MAXIMUM DESIGN LOADS FOR PLATES  
SIMPLY SUPPORTED ON THREE SIDES, FREE ON ONE SIDE**  
uniformly distributed load

TABLE 11.3-3

Uniform Load Over Whole Floor Plate — Short Side Free				Maximum Design Load, $q_{ds}$ (kPa) Deflection Factor $D_{sv}$ (mm/kPa)				Uniform Load Over Whole Floor Plate — Long Side Free			
Thickness $t$	Dimension $t_y$	Dimension $a$ (mm)	Dimension $b$ (mm)	Thickness $t$	Dimension $t_y$	Dimension $a$ (mm)	Dimension $b$ (mm)	Thickness $t$	Dimension $t_y$	Dimension $a$ (mm)	Dimension $b$ (mm)
mm	MPa	mm	mm	mm	MPa	mm	mm	mm	MPa	mm	mm
5	280	600	39.1	35.1	33.8	33.1	33.0	32.9	280	600	39.1
			0.726	0.807	0.838	0.855	0.859	0.861	0.726	600	0.726
			22.0	20.1	19.2	19.6	18.6	18.5	1.91	22.0	1.91
			2.29	2.51	2.62	2.70	2.71	2.72	2.29	4.90	4.90
			14.1	13.0	12.2	11.9	11.9	11.9	14.1	10.9	10.9
			5.60	6.04	6.44	6.60	6.62	6.62	5.60	10.5	10.5
			11.6	9.77	8.77	8.46	8.29	8.29	1200	1200	1200
			11.6	12.9	13.4	13.4	13.7	13.7			
6	280	600	56.3	50.5	48.7	47.7	47.4	47.4	280	600	56.3
			0.420	0.467	0.485	0.495	0.497	0.498	0.420	600	0.420
			31.6	31.6	28.9	27.7	26.8	26.7	31.6	800	31.6
			1.33	1.33	1.45	1.52	1.56	1.57	1.33	1000	1.33
			1000	20.3	18.7	17.6	17.2	17.1	1000	1000	20.3
			1200	3.24	3.50	3.73	3.82	3.83	1200	1200	3.24
				14.1	12.6	12.2	11.9	11.9			
				6.72	7.47	7.47	7.76	7.92			
8	280	600	100	89.8	86.6	84.8	84.4	84.2	280	600	100
			0.177	0.197	0.205	0.209	0.210	0.210	0.177	600	0.177
			56.3	51.4	49.2	47.7	47.5	47.4	800	800	56.3
			0.560	0.612	0.640	0.660	0.662	0.664	0.560	1000	0.560
			1000	36.0	33.3	31.3	30.5	30.5	1000	1000	36.0
			1200	1.37	1.47	1.57	1.61	1.62	1200	1200	1.37
				25.9	22.5	21.6	21.2	21.2			
					2.84	3.15	3.27	3.34			
10	260	600	145	130	126	123	122	122	260	600	145
			0.0907	0.101	0.105	0.107	0.107	0.108	0.0907	600	0.0907
			800	81.6	74.6	71.4	69.2	69.0	800	800	800
			1000	0.287	0.313	0.328	0.338	0.339	1000	1000	0.287
			1200	52.2	48.3	45.4	44.3	44.2	1200	1200	52.2
			1600	0.700	0.755	0.805	0.825	0.827	1600	1600	0.700
				36.3	32.6	31.4	31.4	30.8			
				1.45	1.61	1.68	1.71	1.71			
					20.4	18.7	17.9	17.9			
						4.59	5.01	5.24			
12	260	600	209	188	181	177	176	176	260	600	209
			0.0525	0.0584	0.0606	0.0619	0.0621	0.0622	0.0525	600	0.0525
			800	118	107	103	99.7	99.3	800	800	118
			1000	0.166	0.181	0.190	0.196	0.196	1000	1000	0.166
			1200	75.2	69.6	65.4	63.8	63.6	1200	1200	75.2
			1600	0.405	0.437	0.466	0.477	0.479	1600	1600	0.405
				52.2	46.9	45.2	44.3	44.3			
					0.840	0.934	0.970	0.990			
						29.4	26.9	26.7			
						2.65	2.90	3.03			

TABLE 11.3-4

Thickness $t$	Dimension $t_y$	Dimension $a$ (mm)	Dimension $b$ (mm)	Uniform Load Over Whole Floor Plate — Long Side Free	Maximum Design Load, $q_{ds}$ (kPa) Deflection Factor $D_{sv}$ (mm/kPa)	for Dimension $a$ (mm)
5	280	600	39.1	35.1	33.8	33.0
			0.726	0.807	0.838	0.855
			22.0	20.1	19.2	18.6
			2.29	2.51	2.62	2.70
			14.1	13.0	12.2	11.9
			5.60	6.04	6.44	6.60
			11.6	9.77	8.77	8.46
				1200	1200	1200
6	280	600	56.3	50.5	48.7	47.4
			0.420	0.467	0.485	0.495
			31.6	31.6	28.9	27.7
			1.33	1.33	1.45	1.52
			1000	20.3	18.7	17.6
			1200	3.24	3.50	3.73
8	280	600	100	89.8	86.6	84.8
			0.177	0.197	0.205	0.210
			56.3	51.4	49.2	47.7
			0.560	0.612	0.640	0.660
			1000	36.0	33.3	31.3
			1200	1.37	1.47	1.57
10	260	600	145	130	126	123
			0.0907	0.101	0.105	0.107
			800	81.6	74.6	71.4
			1000	0.287	0.313	0.328
			1200	52.2	48.3	45.4
			1600	0.700	0.755	0.805
12	260	600	209	188	181	177
			0.0525	0.0584	0.0606	0.0619
			800	118	107	103
			1000	0.166	0.181	0.190
			1200	75.2	69.6	65.4
			1600	0.405	0.437	0.466

Note: Grade 250 Steel Plate to AS 3678.

**FLOOR PLATES  
GRADE 250**  
**MAXIMUM DESIGN LOADS FOR  
PLATES FIXED ON FOUR SIDES**

uniformly distributed load

TABLE 11.3-5

Uniform Load Over Whole Floor Plate				Maximum Design Load, $q_{\text{d}}$ (kPa) Deflection factor $D_{\text{sv}}$ (mm/kPa)								Concentrated Load at Centre of Plate									
Thickness $t$	Dimension $f_y$	Dimension		mm	MPa	600	800	1000	1200	1600	2000	2400	5	280	600	800	1000	1200	1600	2000	2400
		mm	mm																		
5	280	600	85.3	62.8	55.3	52.8	52.5	52.5	52.5	52.5	52.5	52.5	5	280	600	12.5	10.1	9.51	9.43	9.38	9.38
		800	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0		0.881	0.881	1.06	1.12	1.13	1.14	1.14	1.14
		1000	39.7	39.7	39.7	39.7	39.7	39.7	39.7	39.7	39.7	39.7		0.907	0.907	12.5	10.4	9.69	9.43	9.38	9.38
		1200	30.7	30.7	30.7	30.7	30.7	30.7	30.7	30.7	30.7	30.7		1.57	1.57	1.84	1.96	2.02	2.03	2.03	2.03
6	280	600	90.4	79.7	76.0	75.6	75.6	75.6	75.6	75.6	75.6	75.6	6	280	600	18.0	14.5	14.5	13.7	13.5	13.5
		800	69.1	53.6	47.1	42.7	42.5	42.5	42.5	42.5	42.5	42.5		0.510	0.510	18.0	14.9	14.0	13.6	13.5	13.5
		1000	44.2	44.2	44.2	44.2	44.2	44.2	44.2	44.2	44.2	44.2		0.907	0.907	1.06	1.13	1.13	1.17	1.17	1.17
		1200	30.7	30.7	30.7	30.7	30.7	30.7	30.7	30.7	30.7	30.7		1.000	1.000	18.0	15.2	13.7	13.6	13.5	13.5
8	280	600	21.8	161	142	135	134	134	134	134	134	134	8	280	600	32.0	25.8	24.3	24.1	24.0	24.0
		800	0.0175	0.0270	0.0325	0.0351	0.0359	0.0359	0.0359	0.0359	0.0359	0.0359		0.215	0.215	0.260	0.274	0.277	0.278	0.278	0.278
		1000	0.0552	0.0552	0.0790	0.0954	0.1111	0.1111	0.1111	0.1111	0.1111	0.1111		0.383	0.383	32.0	26.6	24.8	24.1	24.0	24.0
		1200	0.135	0.135	0.184	0.245	0.271	0.277	0.277	0.277	0.277	0.277		1.000	1.000	1000	32.0	27.1	24.4	24.1	24.0
10	260	600	317	233	206	196	195	195	195	195	195	195	10	260	600	46.4	37.4	35.3	35.0	34.8	34.8
		800	178	138	121	110	110	110	110	110	110	110		0.110	0.110	0.133	0.140	0.142	0.143	0.143	0.143
		1000	114	91.5	91.5	75.0	75.6	75.6	75.6	75.6	75.6	75.6		0.196	0.196	0.230	0.245	0.245	0.253	0.253	0.253
		1200	0.0690	0.0690	0.0940	0.125	0.139	0.142	0.142	0.142	0.142	0.142		0.306	0.306	46.4	39.3	35.5	35.0	34.8	34.8
		1600	0.143	0.143	0.221	0.266	0.287	0.287	0.287	0.287	0.287	0.287		1.200	1.200	1200	46.4	37.4	35.3	35.0	34.9
12	260	600	456	336	296	282	281	281	281	281	281	281	12	260	600	66.9	53.9	50.8	50.4	50.1	50.1
		800	257	200	0.0080	0.0096	0.0104	0.0107	0.0107	0.0107	0.0107	0.0107		0.0638	0.0638	0.0769	0.0812	0.0821	0.0825	0.0825	0.0825
		1000	164	132	0.0234	0.0233	0.0404	0.0488	0.0567	0.0582	0.0582	0.0582		0.131	0.131	0.133	0.142	0.142	0.147	0.147	0.147
		1200	0.0399	0.0399	0.0544	0.0726	0.0802	0.0822	0.0822	0.0822	0.0822	0.0822		0.114	0.114	66.9	56.5	51.1	50.4	50.1	50.1
		1600	64.1	64.1	0.0828	0.128	0.166	0.166	0.166	0.166	0.166	0.166		0.262	0.262	0.282	0.295	0.295	0.295	0.295	0.295

Note: Grade 250 Steel Plate to AS 3678.

Note: Grade 250 Steel Plate to AS 3678.

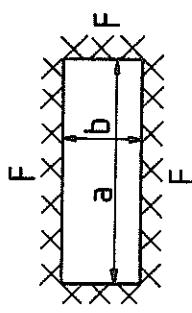
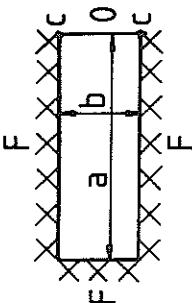


TABLE 11.3-6

central concentrated load

**FLOOR PLATES  
GRADE 250**
**MAXIMUM DESIGN LOADS FOR  
PLATES FIXED ON THREE SIDES, FREE ON ONE SIDE  
uniformly distributed load**

TABLE 11.3-7



Uniform Load Over Whole Floor Plate — Short Side Free

Thickness <i>t</i> mm	Dimension <i>t<sub>y</sub></i> mm	Maximum Design Load, <i>q<sub>fs</sub></i> (kPa) Deflection factor <i>D<sub>sv</sub></i> (mm/kPa) for Dimension <i>a</i> (mm)			
		600	800	1000	1200
5	280	600	51.3	52.2	51.3
	800	0.169	0.194	28.9	29.2
	1000	0.596	0.618	18.5	18.8
	1200	1.46	1.50	12.8	13.1
6	280	600	73.9	75.2	73.9
	800	0.109	0.112	41.5	42.4
	1000	0.345	0.357	26.6	27.0
	1200	0.843	0.867	18.5	18.8
8	280	600	131	134	131
	800	0.0461	0.0472	73.9	75.4
	1000	0.146	0.151	47.3	48.0
	1200	0.355	0.366	32.8	33.4
10	260	600	191	194	191
	800	0.0236	0.0242	107	109
	1000	0.0745	0.0772	68.6	69.7
	1200	0.182	0.187	47.6	48.5
12	260	600	274	279	274
	800	0.0136	0.0140	154	157
	1000	0.0431	0.0447	98.8	100
	1200	0.105	0.108	68.6	69.8
1600	1600	0.218	0.224	0.218	0.224
	1600	0.690	0.715	38.6	39.4
	1600	0.690	0.715	39.1	39.4
	1600	0.690	0.715	0.694	0.694

Note: Grade 250 Steel Plate to AS 3678.

TABLE 11.3-8

Uniform Load Over Whole Floor Plate — Long Side Free				Uniform Load Over Whole Floor Plate — Long Side Free			
Thickness <i>t</i> mm	Dimension <i>t<sub>y</sub></i> mm	Maximum Design Load, <i>q<sub>fs</sub></i> (kPa) Deflection factor <i>D<sub>sv</sub></i> (mm/kPa) for Dimension <i>a</i> (mm)		Maximum Design Load, <i>q<sub>fs</sub></i> (kPa) Deflection factor <i>D<sub>sv</sub></i> (mm/kPa) for Dimension <i>a</i> (mm)		Maximum Design Load, <i>q<sub>fs</sub></i> (kPa) Deflection factor <i>D<sub>sv</sub></i> (mm/kPa) for Dimension <i>a</i> (mm)	
		5	280	5	280	600	800
5	280	600	51.3	52.2	51.3	30.8	21.1
	800	0.169	0.194	28.9	29.2	28.9	19.4
	1000	0.596	0.618	18.5	18.8	0.596	1.34
	1200	1.46	1.50	12.8	13.1	18.5	13.3
				3.02	3.10	1.46	2.84
6	280	600	73.9	75.2	73.9	44.4	30.4
	800	0.109	0.112	41.5	42.4	41.5	27.9
	1000	0.345	0.357	26.6	27.0	0.345	20.4
	1200	0.843	0.867	18.5	18.8	1000	1.50
				1.75	1.79	26.6	19.2
8	280	600	131	134	131	78.9	54.1
	800	0.0461	0.0472	73.9	75.4	0.0461	0.0466
	1000	0.146	0.151	47.3	48.0	800	0.146
	1200	0.355	0.366	32.8	33.4	1000	0.355
				0.737	0.756	1200	0.737
10	260	600	191	194	191	115	78.5
	800	0.0236	0.0242	107	109	0.0236	0.0236
	1000	0.0745	0.0772	68.6	69.7	0.0745	0.0745
	1200	0.182	0.187	47.6	48.5	1000	0.182
	1600	0.377	0.387	26.8	27.3	1200	0.377
				1.24	1.24	1600	1.24
12	260	600	274	279	274	165	113
	800	0.0136	0.0140	154	157	0.0136	0.0136
	1000	0.0431	0.0447	98.8	100	0.0431	0.0431
	1200	0.105	0.108	68.6	69.8	1000	0.105
	1600	0.218	0.224	38.6	39.4	1200	0.218
				0.715	0.715	1600	0.715

Note: Grade 250 Steel Plate to AS 3678.

**FLOOR PLATES  
GRADE 250**

**MAXIMUM DESIGN LOADS FOR  
PLATES FIXED ON TWO SIDES,  
FREE ON TWO SIDES  
uniformly distributed load**

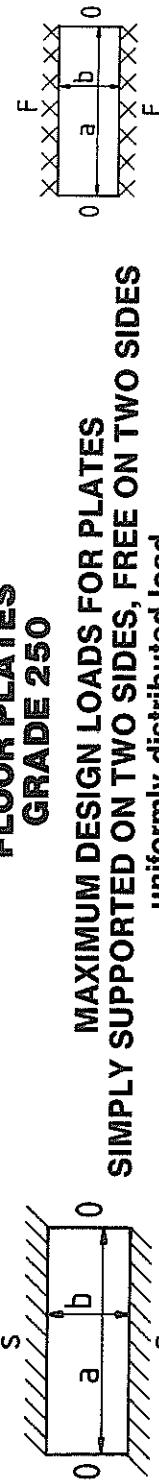


TABLE 11.3-9  
**MAXIMUM DESIGN LOADS FOR PLATES  
SIMPLY SUPPORTED ON TWO SIDES, FREE ON TWO SIDES  
uniformly distributed load**

Uniform Load Over Whole Floor Plate					
Thickness t mm	Dimension t <sub>y</sub> mm	Maximum Design Load, q <sub>u</sub> (kPa) Deflection factor D <sub>sv</sub> (mm/kPa) for Dimension a (mm)			
		600	800	1000	1200
5	280	33.1	33.0	32.9	32.9
	800	0.855	0.857	0.859	0.861
	1000		18.6	18.6	18.5
	1200		2.70	2.71	2.72
6	280	47.6	47.5	47.4	47.4
	800	0.495	0.496	0.497	0.498
	1000		1.56	1.57	1.57
	1200		17.2	17.2	17.1
8	280	84.8	84.6	84.4	84.2
	800	0.209	0.209	0.210	0.210
	1000		47.7	47.6	47.4
	1200		0.660	0.661	0.662
10	260	123	122	122	122
	800	0.107	0.107	0.107	0.108
	1000		69.2	69.1	69.0
	1200		0.338	0.338	0.339
	1600		44.3	44.3	44.3
12	260	177	176	176	176
	800	0.0619	0.0620	0.0621	0.0622
	1000		99.7	99.5	99.3
	1200		0.196	0.196	0.196
	1600		63.8	63.7	63.5

TABLE 11.3-10

Uniform Load Over Whole Floor Plate					
Thickness t mm	Dimension t <sub>y</sub> mm	Maximum Design Load q <sub>u</sub> (kPa)		Deflection factor D <sub>sv</sub> (mm/kPa)	
		280	600	280	600
5	280	32.9	32.9	32.9	32.5
	800	0.861	0.861	0.861	0.162
	1000	18.5	18.5	18.5	29.5
	1200	2.72	2.72	2.72	0.512
6	280	32.9	32.9	32.9	18.9
	800	0.861	0.861	0.861	1.25
	1000	18.5	18.5	18.5	13.1
	1200	2.72	2.72	2.72	2.59
8	280	600	600	600	75.6
	800	0.0938	0.0938	0.0938	42.5
	1000	0.296	0.296	0.296	27.2
	1200	0.723	0.723	0.723	18.9
10	260	600	600	600	1.50
	800	0.0396	0.0396	0.0396	134
	1000	0.125	0.125	0.125	75.6
	1200	0.305	0.305	0.305	33.6
12	260	600	600	600	1.02
	800	0.0203	0.0203	0.0203	281
	1000	0.0640	0.0640	0.0640	110
	1200	0.156	0.156	0.156	70.2
	1600	0.324	0.324	0.324	48.8
					27.4

Note: Grade 250 Steel Plate to AS 3678.

Note: Grade 250 Steel Plate to AS 3678.

## FLOOR PLATES GRADE 250

### MAXIMUM DESIGN LOADS FOR CIRCULAR PLATES SIMPLY SUPPORTED AROUND CIRCUMFERENCE uniformly distributed load

TABLE 11.3-11

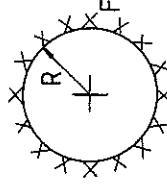
		Uniform Load Over Whole Floor Plate						
Thickness <i>t</i>	<i>f<sub>y</sub></i>	Maximum Design Load, <i>q<sub>ax</sub></i> (kPa)			Concentrated Load at Centre of Plate			
		Deflection factor <i>D<sub>w</sub></i> (mm/kPa)	for Radius (mm)	mm	MPa	600	800	1000
5	280	21.2	11.9	7.65	5.31	2.99	1.91	1.33
		3.60	11.4	27.8	57.6	182	445	922
6	280	30.6	17.2	11.0	7.65	4.30	2.75	1.91
		2.09	6.59	16.1	33.4	105	257	534
8	280	54.4	30.6	19.6	13.6	7.65	4.89	3.40
		0.880	2.78	6.79	14.1	44.5	109	225
10	260	78.9	44.4	28.4	19.7	11.1	7.10	4.93
		0.450	1.42	3.47	7.21	22.8	55.6	115
12	260	114	63.9	40.9	28.4	16.0	10.2	7.10
		0.261	0.824	2.01	4.17	13.2	32.2	66.7

Note: Grade 250 Steel Plate to AS 3678.

TABLE 11.3-12

		Concentrated Load at Centre of Plate						
Thickness <i>t</i>	<i>f<sub>y</sub></i>	Maximum Design Load, <i>P<sub>ax</sub></i> (kN)			Deflection factor <i>D<sub>w</sub></i> (mm/kN)			
		mm	MPa	600	800	1000	1200	1600
5	280	280	2.26	2.17	2.10	2.05	1.97	1.92
		7.92	14.1	22.0	31.7	56.3	88.0	127
6	280	280	3.35	3.21	3.11	3.03	2.91	2.82
		4.58	8.15	12.7	18.3	32.6	50.9	73.3
8	280	280	6.24	5.96	5.76	5.61	5.38	5.22
		1.93	3.44	5.37	7.73	13.8	21.5	30.9
10	260	260	9.39	8.96	8.65	8.41	8.06	7.81
		0.990	1.76	2.75	3.96	7.04	11.0	15.8
12	260	260	14.0	13.3	12.8	12.5	11.9	11.5
		0.573	1.02	1.59	2.29	4.07	6.37	9.17

Note: Grade 250 Steel Plate to AS 3678.



FLOOR PLATES  
GRADE 250  
MAXIMUM DESIGN LOADS FOR CIRCULAR  
PLATES FIXED AROUND CIRCUMFERENCE  
central concentrated load

TABLE 11.3-14

		Concentrated Load Over Whole Floor Plate						
Thickness <i>t</i>	<i>f<sub>y</sub></i>	Maximum Design Load, <i>P<sub>ax</sub></i> (kN)			Deflection factor <i>D<sub>w</sub></i> (mm/kN)			
		mm	MPa	600	800	1000	1200	1600
5	280	280	2.56	2.44	2.35	2.29	2.19	2.12
		3.17	5.63	8.80	12.7	22.5	35.2	50.7
6	280	280	3.80	3.62	3.49	3.39	3.24	3.14
		1.83	3.26	5.09	7.33	13.0	20.4	29.3
8	280	280	7.12	6.76	6.50	6.31	6.02	5.82
		0.773	1.38	2.15	3.09	5.50	8.59	12.4
10	260	260	10.8	10.2	9.81	9.50	9.06	8.74
		0.396	0.704	1.10	1.58	2.82	4.40	6.34
12	260	260	16.1	15.2	14.6	14.1	13.4	12.6
		0.229	0.407	0.637	0.917	1.63	2.55	3.67

Note: Grade 250 Steel Plate to AS 3678.

FLOOR PLATES  
GRADE 250  
MAXIMUM DESIGN LOADS FOR CIRCULAR  
PLATES SIMPLY SUPPORTED AROUND CIRCUMFERENCE  
uniformly distributed load

TABLE 11.3-13

		Uniform Load Over Whole Floor Plate						
Thickness <i>t</i>	<i>f<sub>y</sub></i>	Maximum Design Load, <i>q<sub>ax</sub></i> (kPa)			Concentrated Load at Centre of Plate			
		mm	MPa	600	800	1000	1200	1600
5	280	19.7	12.6	8.75	4.92	3.15	2.19	1.19
		0.886	2.80	6.84	14.2	44.8	109	227
6	280	28.3	18.1	12.6	7.09	4.54	3.15	1.75
		0.513	1.62	3.96	8.21	25.9	63.3	131
8	280	50.4	32.3	22.4	12.6	8.06	5.60	3.11
		0.216	0.684	1.67	3.46	10.9	26.7	55.4
10	260	73.1	46.8	32.5	18.3	11.7	8.13	4.06
		0.111	0.350	0.855	1.77	5.60	13.7	28.4
12	260	105	67.4	46.8	26.3	16.8	11.7	5.66
		0.064	0.203	0.495	1.03	3.24	7.92	16.4

Note: Grade 250 Steel Plate to AS 3678.



**PART 12 RAILS**

	PAGE
Dimensions and Properties .....	12-2

**TABLES**

**TABLE 12-1**

Dimensions and Properties .....	12-2
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References:

"Hot Rolled and Structural Products – 1994 Edition", BHP Steel, 1994.

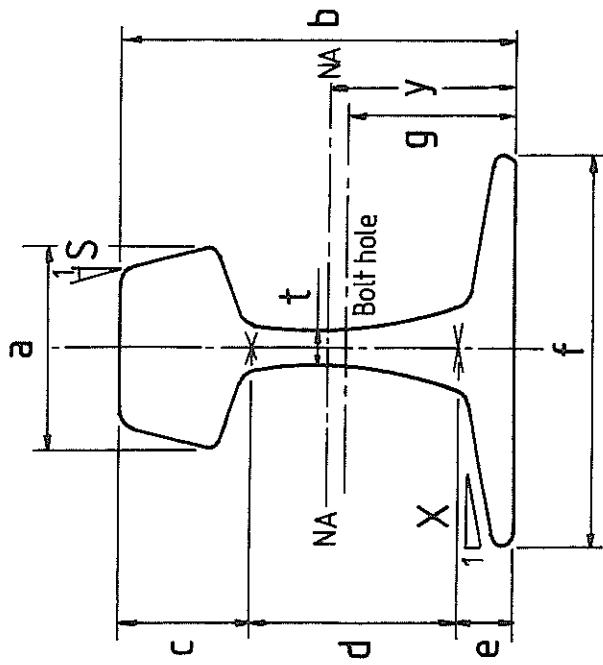


TABLE 12-1  
**RAILS**  
DIMENSIONS AND PROPERTIES

Designation	Mass per m	Dimensions							Total Area			About x-axis		Designation				
		a	b	c	d	e	f	g	s	t	x	y	$A_s$	$I_x$	Head	Foot		
	kg/m	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm <sup>2</sup>	$10^6 \text{ mm}^4$	$10^3 \text{ mm}^3$	$Z_x$	$Z_x$	
RE68	67.6	74.6	185.7	49.2	106.3	30.2	152.4	78.6	40	17.5	4	98.4	8614	39.5	391.7	463.8	RE68	
AS60	61.0	70.0	170.0	49.0	93.0	28.0	146.0	74.5	20	16.5	4	79.1	7770	29.4	323.2	371.4	AS60	
AS50	50.8	70.0	154.0	45.0	84.0	25.0	127.0	67.0	20	15.0	4	74.8	6470	20.1	254.1	269.3	AS50	
AS41	40.7	63.5	136.5	40.5	74.6	21.4	127.0	60.3	—	13.1	5	67.5	5187	13.2	184.4	204.5	AS41	

**PART 13 GANTRY GIRDERS/MONORAIL BEAMS**

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**TABLES**

<b>TABLE 13-1</b>	
Gantry Girders: Composition and Dimensions and Properties.....	<b>13-2</b>

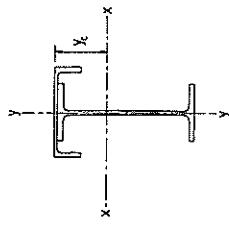
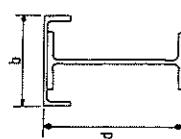


TABLE 13-1  
**GANTRY GIRDERS**  
**COMPOSITION AND DIMENSIONS AND PROPERTIES**



Composed of Beam	Top Flange Channel	Approx. size d x b		Mass per m kg/m	Area $A_g$ mm <sup>2</sup>	$y_c$ mm	$I_k$ mm	About x-axis			About y-axis			Warping Constant $I_w$ $10^8 \text{ mm}^6$				
								Top	Bot	Top F	Top F	Top F	Constant					
		$Z_x$	$Z_y$					$t_y$	$t_y$	$Z_y$	$Z_y$	$J$						
1200WB249	380PFC	1180 x 380	304	38700	492	8240	16800	12000	461	239	78.5	195	1030	4870	38100			
800WB168	380PFC	820 x 380	223	28400	319	3280	10300	6560	340	238	91.7	195	1030	3590	17900			
146	380PFC	810 x 380	201	25600	305	2790	9150	5550	330	221	92.9	186	981	2190	14000			
122	380PFC	802 x 380	178	22600	288	2270	7880	4420	317	193	92.4	173	908	1410	8630			
700WB173	380PFC	726 x 380	228	29000	286	2690	9410	6100	304	249	92.6	200	1050	4720	15400			
150	380PFC	720 x 380	205	26100	274	2300	8380	5160	297	217	91.1	184	970	3300	10700			
130	380PFC	710 x 380	186	23600	261	1950	7470	4340	287	204	92.9	178	936	2020	8330			
115	380PFC	702 x 380	170	21600	249	1670	6710	3690	278	193	94.6	173	908	1370	6540			
<b>UNIVERSAL BEAMS with PARALLEL FLANGE CHANNELS</b>																		
610UB125	380PFC	622 x 380	180	23000	228	1400	6140	3560	247	191	91.2	171	902	2020	4950			
113	380PFC	617 x 380	169	21500	220	1270	5770	3190	243	186	93.1	169	889	1590	4290			
101	380PFC	612 x 380	157	20000	211	1130	5350	2820	288	181	95.2	166	875	1240	3590			
530UB 92.4	380PFC	543 x 380	148	18800	183	833	4540	2320	210	176	96.6	164	861	1230	2370			
82.0	380PFC	538 x 380	137	17500	175	737	4210	2030	205	172	99.1	162	851	985	1970			
530UB 92.4	300PFC	541 x 300	133	16900	200	776	3880	2270	214	96.3	75.5	84.4	562	1050	2070			
82.0	300PFC	536 x 300	122	15600	192	685	3570	1990	210	92.5	77.1	82.4	550	803	1700			
460UB 82.1	300PFC	468 x 300	122	15600	169	528	3120	1760	184	91.1	76.5	81.8	545	982	1240			
74.6	300PFC	465 x 300	115	14600	163	484	2960	1600	182	89.1	78.1	80.8	538	810	1100			
67.1	300PFC	462 x 300	107	13700	157	436	2770	1430	179	86.9	79.8	79.7	531	661	942			
410UB 59.7	300PFC	411 x 300	99.8	12700	137	323	2350	1160	159	84.4	81.5	78.4	523	619	638			
53.7	300PFC	411 x 300	93.8	12000	131	287	2180	1030	155	82.6	83.1	77.5	517	517	534			
360UB 56.7	300PFC	367 x 300	96.8	12300	121	241	2000	983	140	83.5	82.3	78.0	520	622	460			
50.7	300PFC	364 x 300	90.8	11600	116	217	1880	877	137	82.1	84.2	77.2	515	526	397			
44.7	300PFC	360 x 300	84.8	10800	110	191	1740	764	133	80.5	86.3	76.5	510	447	330			

Notes: (1)  $I_y$  Top F =  $I_k$  of channel + ( $I_y$  of Universal or Welded Beam)/2  
 (2)  $Z_y$  Top F =  $(I_y$  Top F)/( $b$ /2)