

du 15 ~~notes~~ ex.

(5.1)  $Q_H = 2000 \text{ J}$   $Q_C = 1700 \text{ J}$   
 $\epsilon = 1 - \frac{|Q_C|}{|Q_H|} = 1 - \frac{1700}{2000} = 85\%$

$\epsilon = 1 - \frac{1700}{2000} = 15\%$

(5.2)  $\epsilon = 1 - \frac{T_C}{T_H} = 1 - \frac{0 + 273}{100 + 273} = 27\%$

(5.3) a)  $Q_{\text{furnace}} = m C \Delta T + m L_f$   
 $= (2.00 \text{ kg}) (4186 \text{ J/kg} \cdot 20 \text{ K} + 3.335 \times 10^5 \text{ J/kg})$   
 $= 834 \text{ kJ}$

~~W~~  $K = \frac{|Q_C|}{|W|}$   $|W| = \frac{834 \text{ kJ}}{4.00}$   
 $= 209 \text{ kJ}$

$W = -209 \text{ kJ}$  because you do work on the fridge to make it run

b)  $|W| = |Q_H| - |Q_C|$

$|Q_H| = |W| + |Q_C|$   
 $= 209 \text{ kJ} + 834 \text{ kJ}$   
 $= 1.04 \text{ MJ}$

(5.4)  $K = \frac{1}{\frac{T_H}{T_C} - 1} = \frac{1}{\frac{273 + 20}{273 - 20} - 1}$   
 $= 6.33$

(5.5)  $\epsilon_{\text{max}} = \epsilon_{\text{Carnot}} = 1 - \frac{T_C}{T_H}$   
 $= 1 - \frac{273 + 20}{273 + 20} = 49\%$

$K_{\text{max}} = K_{\text{Carnot}} = \frac{1}{\frac{T_H}{T_C} - 1} = \frac{1}{\frac{573}{273} - 1} = 1.05$

(5.6)  $\Delta S = nL = \frac{2.150 \text{ kg} \cdot 3.335 \times 10^5 \text{ J/kg}}{273 \text{ K}}$

$= 1.83 \text{ J/K}$

(5.7) a)  $T_0, V_0, T_f, V_f$ , ideal  
 $\Delta S = \int_0^f \frac{dQ}{T}$

$dQ = dU + dW$   
 $dW = nC_V dT$   $dW = P dV$

$dQ = nC_V dT + P dV$

$\Delta S = \int_1^f \frac{nC_V dT}{T} + \int_1^f \frac{P dV}{T}$

$PV = nRT$   $\frac{P}{T} = \frac{nR}{V}$

$\Delta S = nC_V \int_1^f \frac{dT}{T} + nR \int_1^f \frac{dV}{V}$   
 $= nC_V (\ln T_f - \ln T_0) + nR (\ln V_f - \ln V_0)$   
 $= nC_V \ln \frac{T_f}{T_0} + nR \ln \frac{V_f}{V_0}$

b) isochoric - constant V

$\Delta S = nC_V \ln \frac{T_f}{T_0}$

isothermal - constant T

$\Delta S = nR \ln \frac{V_f}{V_0}$

(5.8)  $Q = \Delta U + W$

$\Delta S = \int_1^f \frac{dQ}{T} = nC_V \ln \frac{T_f}{T_0} + nR \ln \frac{V_f}{V_0}$

$\Delta T = 0$

$\Delta S = nR \ln \frac{V_f}{V_0}$

(5-9)  $\Delta S$  to  $T_c$ :  $\Delta S = \frac{|Q|}{T_c}$   
 $\Delta S$  from  $T_H$ :  $\Delta S = -\frac{|Q|}{T_H}$

$\Delta S_{total} = \frac{|Q|}{T_c} - \frac{|Q|}{T_H}$

(5-10)  $\Delta S$  for heat transfer  
 $\Delta S = m c \ln \frac{T_H}{T_c}$

$\Delta S_1 = m_1 c_1 \ln \frac{T_H}{T_c}$

$\Delta S_2 = m_2 c_2 \ln \frac{T_H}{T_c}$

$\Delta S_{total} = m_1 c_1 \ln \frac{T_H}{T_c} + m_2 c_2 \ln \frac{T_H}{T_c}$

(5-11)  $\Delta S = m_1 c_1 \ln \frac{T_H}{T_c} + m_2 c_2 \ln \frac{T_H}{T_c}$

(5-12)  $\Delta S = m c \ln \frac{T_H}{T_c}$   
 $= (3.00 \text{ kg}) (4186 \text{ J/kg} \cdot \text{K}) \ln \frac{100+273}{273}$   
 $= 3919 \text{ J/K}$

(5-13) a)  $\epsilon = 1 - \frac{T_c}{T_H} = 1 - \frac{300 \text{ K}}{500 \text{ K}} = 40\%$

b)  $|W| = \epsilon |Q_H| = (0.4)(2000 \text{ J})$   
 $= 800 \text{ J}$

c)  $\Delta S = 0$   $\Delta S_{heat} = -\frac{|Q|}{T_H}$   
 $= -\frac{2000 \text{ J}}{500 \text{ K}} = -4 \text{ J/K}$

$\Delta S_{solid} = \frac{|Q|}{T_c}$   
 $= \frac{2000 \text{ J} - 800 \text{ J}}{300 \text{ K}} = 4 \text{ J/K}$

d)  $\Delta S_{total} = 0$

(5-14)  $\Delta S = m c_{ice} \ln \frac{T_H}{T_c} + \frac{m L}{T} + m c_{water} \ln \frac{T_H}{T_c}$

$\Delta S = (2.00 \text{ kg}) \left[ 2050 \frac{\text{J}}{\text{kg} \cdot \text{K}} \ln \frac{273}{253} + \frac{3.335 \times 10^5 \text{ J}}{273 \text{ K}} + 4186 \frac{\text{J}}{\text{kg} \cdot \text{K}} \ln \frac{273}{273} \right]$   
 $= 3489 \text{ J/K}$

$\Delta S_{room} = \text{reservoir, large heat sink}$

$\Delta S = -\frac{|Q|}{T_c}$

$Q = m c_{ice} \Delta T_1 + m L + m c_{water} \Delta T$   
 $= (2.00 \text{ kg}) (2050 \text{ J/kg} \cdot \text{K} \cdot 20 \text{ K} + 3.335 \times 10^5 + 4186 \cdot 25 \text{ K})$   
 $= 958 \text{ kJ}$   
 $\Delta S = -\frac{958 \text{ kJ}}{273 \text{ K}} = -3216 \text{ J/K}$

$3489 - 3216 > 0$ , so it's ok

(5-15)  $\#$  of microstates is  $N+1$

$\#$  of microstates ~~approaches~~ is very large

b)  $\binom{N}{n} = \frac{N!}{n!(N-n)!}$   
 $(N(n))$