

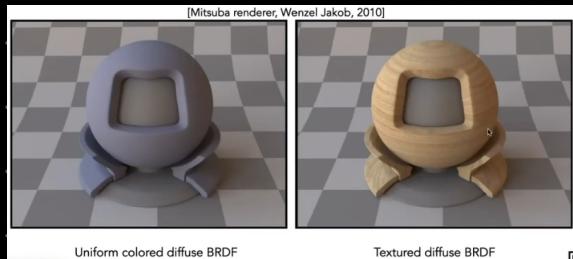


光照与材质密切相关

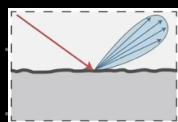
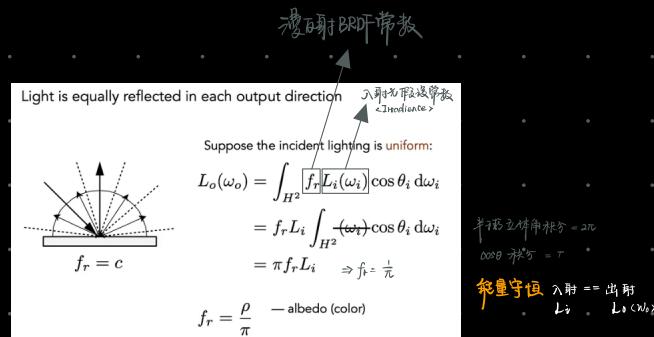
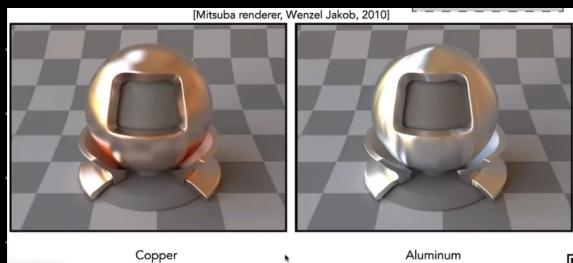
最强渲染器 Monaka 支持多种材质

Material == BRDF

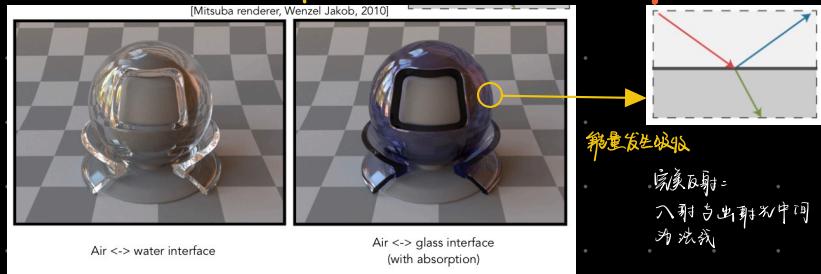
漫反射 Diffuse/Lambertian



亮面反射 Glossy Material BRDF



ideal reflective/refractive material BSDF



镜面反射 perfect specular reflection BRDF

Perfect Specular Reflection

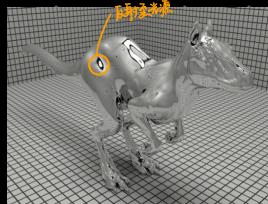
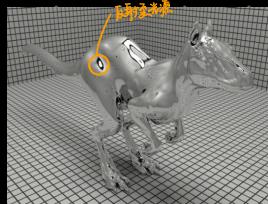
$\theta = \theta_o = \theta_i$

$\omega_o = (\phi_i + \pi) \bmod 2\pi$

$\vec{n} \cdot \vec{\omega}_o = \vec{n} \cdot \vec{\omega}_i$

$$\omega_o = -\omega_i + 2(\omega_i \cdot \vec{n})\vec{n}$$

$\vec{n} \cdot \vec{\omega}_o = 2 \cos \theta \vec{n} = 2(\omega_i \cdot \vec{n})\vec{n}$ 计算出射光



折射 Specular refraction

$$BTDF_{transmit} + BRDF = BSDF_{Scattering}$$

Specular Refraction

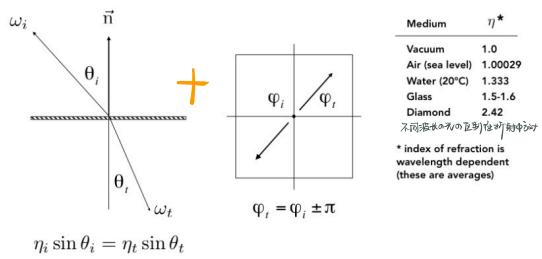
In addition to reflecting off surface, light may be transmitted through surface.

Light refracts when it enters a new medium.



Snell's Law 莫内尔定律 <折射定律>

Transmitted angle depends on
index of refraction (IOR) for incident ray
index of refraction (IOR) for exiting ray



Law of Refraction

$$\begin{aligned} \eta_i \sin \theta_i &= \eta_t \sin \theta_t \\ \cos \theta_t &= \sqrt{1 - \sin^2 \theta_t} \\ &= \sqrt{1 - \left(\frac{\eta_i}{\eta_t}\right)^2 \sin^2 \theta_i} \\ &= \sqrt{1 - \left(\frac{\eta_i}{\eta_t}\right)^2 (1 - \cos^2 \theta_i)} \end{aligned}$$

Total internal reflection:

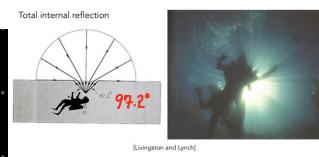
When light is moving from a more optically dense medium to a less optically dense medium: $\frac{\eta_i}{\eta_t} > 1$

Light incident on boundary from large enough angle will not exit medium. 全反射

$$1 - \left(\frac{\eta_i}{\eta_t}\right)^2 (1 - \cos^2 \theta_i) < 0$$

不满足条件

Snell's Window / Circle



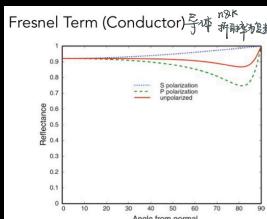
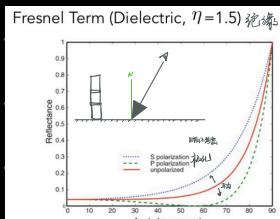
菲涅尔反射 Fresnel Reflection / Term

Reflectance depends on incident angle (and polarization of light)



This example: reflectance increases with grazing angle

[Lafontaine et al. 1997]

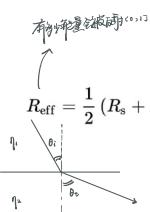


Fresnel Term — Formulae

Accurate: need to consider polarization

$$R_s = \left| \frac{n_1 \cos \theta_i - n_2 \cos \theta_t}{n_1 \cos \theta_i + n_2 \cos \theta_t} \right|^2 = \left| \frac{n_1 \cos \theta_i - n_2 \sqrt{1 - \left(\frac{n_1}{n_2} \sin \theta_i\right)^2}}{n_1 \cos \theta_i + n_2 \sqrt{1 - \left(\frac{n_1}{n_2} \sin \theta_i\right)^2}} \right|^2,$$

$$R_p = \left| \frac{n_1 \cos \theta_i - n_2 \cos \theta_t}{n_1 \cos \theta_i + n_2 \cos \theta_t} \right|^2 = \left| \frac{n_1 \sqrt{1 - \left(\frac{n_1}{n_2} \sin \theta_i\right)^2} - n_2 \cos \theta_t}{n_1 \sqrt{1 - \left(\frac{n_1}{n_2} \sin \theta_i\right)^2} + n_2 \cos \theta_t} \right|^2.$$

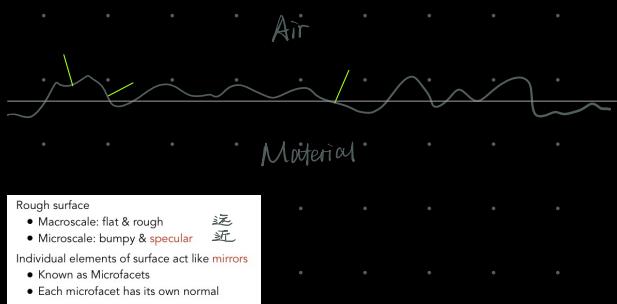
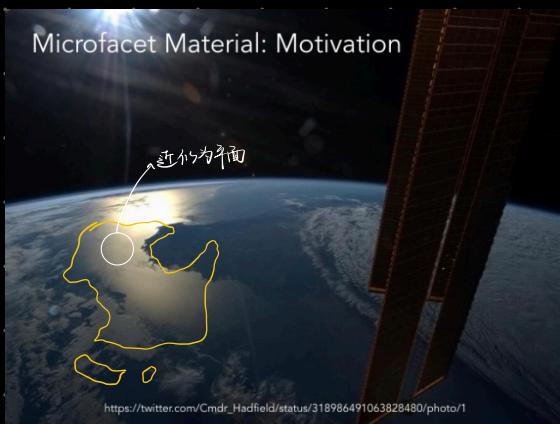


Approximate: Schlick's approximation

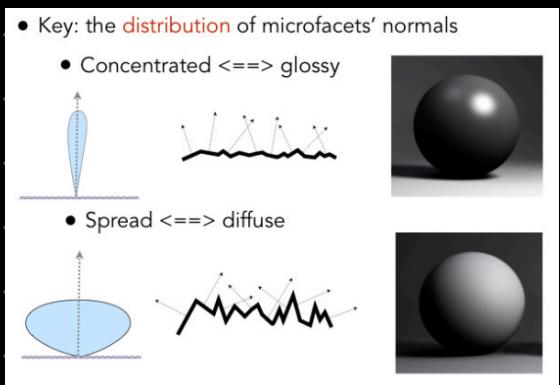
$$R(\theta) = R_0 + (1 - R_0)(1 - \cos \theta)^5 \quad 0^\circ \leq \theta \leq 90^\circ \quad R_0 = 1$$

$$R_0 = \left(\frac{n_1 - n_2}{n_1 + n_2} \right)^2$$

微facet 表面 模型 Microfacet Material

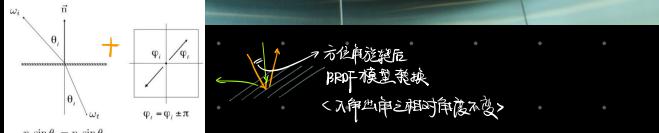


Microfacet BRDF 可用于表现布料材质之表面 [用于 PBR]

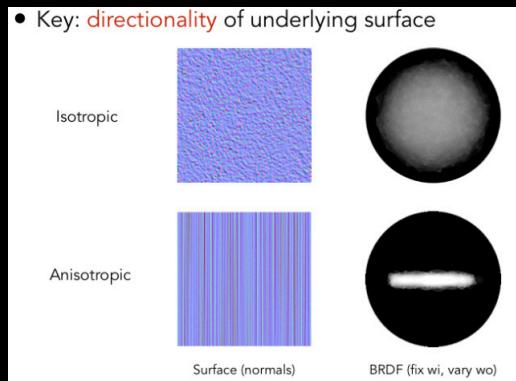
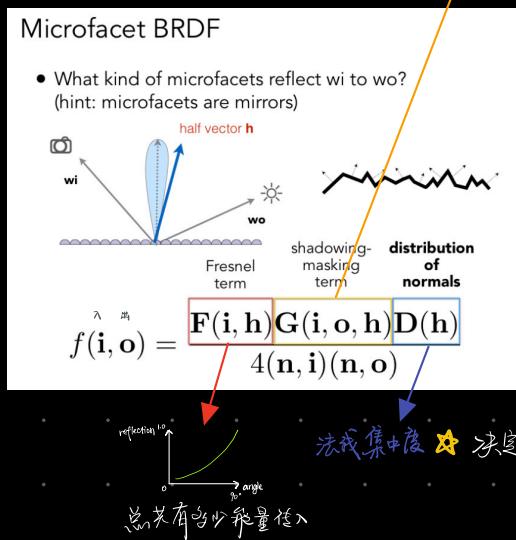
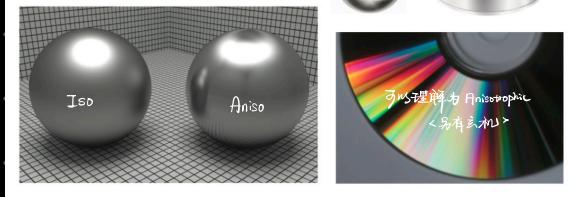


微观表面 vs 宏观表面 通过法线分布表示

Isotropic / Anisotropic Materials BRDFs



Results from oriented microstructure of surface, e.g., brushed metal



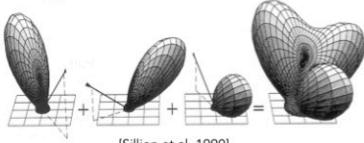
Properties of BRDFs

- Non-negativity

$$f_r(\omega_i \rightarrow \omega_r) \geq 0$$

- Linearity

$$L_r(p, \omega_r) = \int_{H^2} f_r(p, \omega_i \rightarrow \omega_r) L_i(p, \omega_i) \cos \theta_i d\omega_i$$



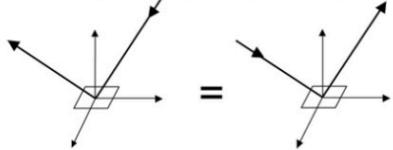
[Sillion et al. 1990]

表示能量分布，非负

将各运算部分先拆开计算，后组合
→ 简单不可

- Reciprocity principle

$$f_r(\omega_r \rightarrow \omega_i) = f_r(\omega_i \rightarrow \omega_r)$$



可逆性

能量守恒

- Energy conservation

$$\forall \omega_r \int_{H^2} f_r(\omega_i \rightarrow \omega_r) \cos \theta_i d\omega_i \leq 1$$

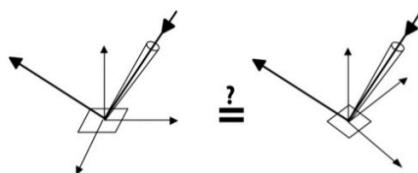
仅与相对方位角差值有关

不必考虑谁大谁小

- Isotropic vs. anisotropic

- If isotropic, $f_r(\theta_i, \phi_i; \theta_r, \phi_r) = f_r(\theta_i, \theta_r, \phi_r - \phi_i)$
- Then, from reciprocity,

$$f_r(\theta_i, \theta_r, \phi_r - \phi_i) = f_r(\theta_r, \theta_i, \phi_i - \phi_r) = f_r(\theta_i, \theta_r, |\phi_r - \phi_i|)$$



Measuring BRDFs

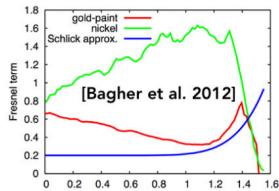
Avoid need to develop / derive models

- Automatically includes all of the scattering effects present

Can accurately render with real-world materials

- Useful for product design, special effects, ...

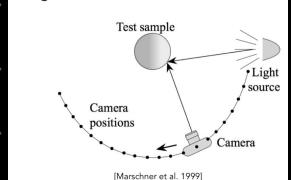
Theory vs. practice:



物理实验之复杂性

⇒ 取近似模型

Image-Based BRDF Measurement



Measuring BRDFs: gonioreflectometer



General approach:

```
foreach outgoing direction wo
    move light to illuminate surface with a thin beam from wo
    for each incoming direction wi
        move sensor to be at direction wi from surface
        measure incident radiance
```

Challenges

- Accurate measurements at grazing angles
 - Important due to Fresnel effects
- Measuring with dense enough sampling to capture high frequency specularities
- Retro-reflection
- Spatially-varying reflectance, ...

Tabular Representation

Store regularly-spaced samples in $(\theta_i, \theta_o, |\phi_i - \phi_o|)$

Better: reparameterize angles to better match specularities

Generally need to resample measured values to table

Very high storage requirements



MERL BRDF Database
[Matusik et al. 2004]

Improving efficiency: Curse of dimensionality

- Isotropic surfaces reduce dimensionality from 4D to 3D
- Reciprocity reduces # of measurements by half 可逆
- Clever optical systems... ↗ 只需对称光路，有利于

Representing / Storing BRDF data

- Desirable qualities
 - Compact representation
 - Accurate representation of measured data
 - Efficient evaluation for arbitrary pairs of directions
 - Good distributions available for importance sampling

MERL BRDF DATABASE