

# Magnetically Enhanced Microflow Cytometer for Bead- and Cell-based Immunoaffinity Measurements in Whole Blood Samples



Scientific thesis for the attainment of the academic degree Master of Science (M.Sc.) of the Department of Electrical and Computer Engineering at the Technical University of Munich.

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### 1. Theoretical Prequisites

The main measurement principle by a GMR (Giant Magneto Resistance)-Sensor has been already described and characterized exhaustively by Helou [1], Reisbeck [2] and Brenner [3]. Therefore, this theoretical part will focus on (bio-)physical aspects of a cell rolling motion inside a microfluidic channel and surface modification chemistry.

#### 1.1. Microfluidics

The main experiments of this work were carried out in microfluidic environments, which exhibit favorable properties compared to common turbulent systems. From a fluid-mechanical standpoint, shrinking the scales makes interfacial as well as electrokinetic phenomena much more significant, and reduces the importance of pressure and gravity.[4] However, electodynamics, chemistry and fluid dynamics are incetricably intertwined, so that fluid flow can create electric fields (and vice versa), with a degree of coupling driven by the surface chemistry. Many of the resulting phenomena arise or can explained by Cauchy-Momentum equation (eq. 1.3) and the resulting Navier-Stokes equation for incompressible fluids (eq. 1.4).

$$\frac{\partial}{\partial t} \iiint \rho d\mathbf{V} = -\iint \rho \mathbf{u} \cdot \vec{\mathbf{n}} d\mathbf{A}$$
 (1.1)

$$\nabla \cdot \mathbf{u} = 0 \tag{1.2}$$

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \rho \mathbf{u} \cdot \nabla \mathbf{u} = \nabla \cdot \boldsymbol{\tau} + \sum_{i} \mathbf{f}_{i}$$
(1.3)

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \rho \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla p + \eta \nabla^2 \mathbf{u} + \sum_{i} \mathbf{f}_{i}$$
Transient Convection Pressure Viscous Body Forces
$$(1.4)$$

conservation of mass, momentum reynolds number

#### 1.1.1. Flow Field inside Microchannels

The foremost characteristic of a microchannel is the laminar flow behavior, which causes deterministic pathlines. Mathematically this is described by the reynolds number, which compares the intertia to shear forces. If it results below a certain threshold of 2000,

laminar flow can be assumed. This holds true for the utilized microfluidic with the dimensions  $12\,000\,\mu\text{m} \times 700\,\mu\text{m} \times 150\,\mu\text{m}$  (I x w x h) and aequous buffer solutions, where the channel width was used as characteristic length l. Hence, the Navier-Stokes equation can be applied to our system.

$$Re = \frac{2\rho|\overline{u}|l}{\eta} \tag{1.5}$$

The step from the Cauchy momentum equation to the Navier-Stokes equation is complex and harbors several sources of error. First, an incompressible newtonian fluid as well as channel is assumed. The used water suspensions can be approximated with negligible compressibility, which is not true for the real case. Also, for blood or other shear-thinning fluids some deviations are prone for high errors. This happens due to the fact that the  $\tau$  (surface stress tensor) is decomposed into pressure and viscous contributions as shown in the equations 1.6. Then, the divergence relation of the respective viscous stress (eq. 1.7) does not hold for non-uniform viscosity  $\eta$ .

$$\tau = \tau_{viscous} + \tau_{pressure} = 2\eta \epsilon - p\mathbf{I}_{3\times 3}$$
 (1.6)

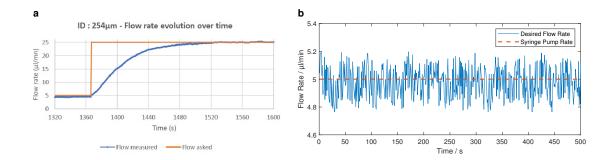
$$\nabla \cdot \boldsymbol{\tau}_{viscous} = \nabla \cdot 2\eta \epsilon = \nabla \cdot \eta \nabla \mathbf{u} \stackrel{only\ if\ \eta}{=} \eta \nabla^2 \mathbf{u}$$
(1.7)

Second, the channel height varies in reality as a result of fabrication inaccuracies. In the model case of a flow through a rectangular channel, no analytical solution of the Navier-Stokes equation exists, but a Fourier Series expansion if channel width is larger than channel height. [5] The equation 1.8 shows that height deviations can have prominent influence on a channel velocity simulation as it is proportional to  $h^2$ . Further, the flow rate (which is the velocity integral over the channel cross section) depends even on  $h^3$ .

$$u_x(y,z) = \frac{4h^2 \Delta p}{\pi^3 \eta l} \sum_{n,odd}^{\infty} \frac{1}{n^3} \left( 1 - \frac{\cosh(n\pi \frac{y}{h})}{\cosh(n\pi \frac{w}{2h})} \right) \sin(n\pi \frac{z}{h})$$
(1.8)

Third, the transient term (eq. 1.4) was neglected in all simulations, but a connected syringe pump possesses a slow rise time (Fig. 1a) and a remaining "pulsation error" in steady state (Fig. 1b). In effect, another error adds to the simulation, which is only valid after several ten seconds of the last flow rate change.

For later studies in a matlab model, the flow velocity and shear stress computations



**Figure 1** Syringe Pump error sources, Set flow rate: \_\_\_\_\_, Real Flow Rate: \_\_\_\_\_ a Transient step answer of a syringe pump through a microtube with 254 μm inner diameter. b Steady state flow rate error around the desired 5 μL min<sup>-1</sup> dispensing rate. A sinusoidal behaviour caused by the microstepping can be observed. [6]

were carried out with the error sources considered.

#### 1.1.2. Particles in Microfluidics

Stokes Drag Force Gravity Electro-static interaction Magnetic Force Friction Interface-Forces

#### 1.1.3.

### 1.2. Surface Chemistry

#### 1.2.1. Silane Chemistry

#### 1.2.2. Carbodiimide Crosslinker Chemistry

EDC-NHS-Activation sulfo-NHS vs. NHS

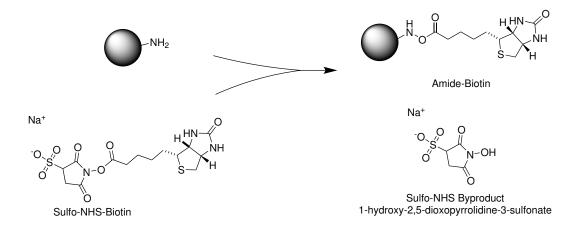


Figure 2 TestSvg

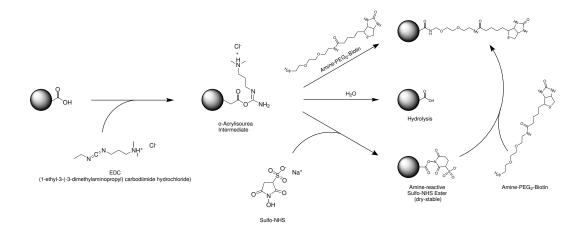


Figure 3 TestSvg

#### 1.2.3. Microscopic Particle Surface Physics

#### 1.2.4. The Biotin-Avidin-System

### 1.3. MRCyte

Short intro over MRCyte Foto of setup with arrows to necessary parts Microscope Stages PEEK holder Helmholtz coils Kepco MFLI DAQ

#### 1.3.1. Focusing Structures

test,test Loss because of reduced velocity and magnetic drag

#### 1.3.2. GMR

Different produced GMR stacks Wheatstone Bridge setup Magnet alignment

#### 1.3.3. Electrical Circuit

Ground PCB Stacked PCBs with spacer

#### 1.3.4. Electronic Readout

test,test

#### **Hysteresis Alignment**

test,test

#### Single GMR

test,test

#### **Dual GMR**

one MFLI supplies both at same freugency. Aux Trigger tested, but no advantage.

# List of Abbreviations

### Symbols

au - surface stress tensor
$\eta$ - dynamic viscosity
$\mu$ F - Microfluidic
ho - density
$\sum_i \mathbf{f}_i$ - body forces
A
AAF - Artificial Anti-Ferromagnet
AcOH - Acetic Acid
AFM - Anti-Ferromagnetism
APTES - (3-aminopropyl)triethoxysilane
D
diH <sub>2</sub> O - deionized water
E
EDC - 1-Ethyl-3-(3-dimethylaminopropyl)carbodiimide
EtOH - Ethanol
F
FM - Ferrimagnetism
FWHM - Full Width at Half Maximum
G
GMR - Giant Magneto Resistance
GUI - Graphical User Interface
Н
H <sub>2</sub> O <sub>2</sub> - Hydrogen Peroxide
H <sub>2</sub> SO <sub>4</sub> - Sulfuric Acid
HCI - Hydrochloric Acid
HF - Hydrofluoric Acid

1
IPA - Isopropanol
M
MACS - MACS running buffer
MeOH - Methanol
MES - 2-(N-morpholino)ethanesulfonic Acid
MNP - Magnetic Nanoparticle
N
N <sub>2</sub> - Nitrogen Gas
NFM - non-ferro-magnetic
NHS - N-hydroxysuccinimide
0
O <sub>2</sub> - Oxygen Gas
P
PAA - Poly(acrylic) Acid
PBS - Phosphate Buffered Saline
PCB - Printed Circuit Board
PDMS - Poly(dimethyl siloxane)
Piranha - H <sub>2</sub> O <sub>2</sub> :H <sub>2</sub> SO <sub>4</sub>
PM - Paramagnetism
S
SiN - Silicon Nitride
SMA - Styrene Maleic Anhydride
SPM - Superparamagnetism
U
u - flow field

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	a Transient step answer of a syringe pump through a microtube with			
	$254\mu m$ inner diameter. b Steady state flow rate error around the de-			
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### Statement

I declare that I have authored this thesis independently, that I have not used other than the declared sources / resources, and that I have explicitly marked all material which has been quoted either literally or by content from the used sources.

Munich, December 4<sup>th</sup>, 2020, Signature