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Report of the application project at the Faculty of AMP

# Simulation of a medical therapy method with finite elements

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# Contents

<b>1. Introduction to radio frequency ablation</b>	<b>5</b>
<b>2. Computer-aided simulation of radio frequency ablation</b>	<b>5</b>
2.1. About Errors in simulations and numerical approaches . . . . .	5
2.2. The physics behind radio frequency ablation . . . . .	6
<b>3. Mathematical aspects of discrete simulation</b>	<b>6</b>
3.1. Theory of finite elements . . . . .	6
3.1.1. Elliptical problems . . . . .	6
3.1.2. FEM for electrical fields . . . . .	6
3.1.3. FEM for temperature fields . . . . .	6
3.2. Solving systems of ODE over time . . . . .	6
3.3. Axial symmetrie . . . . .	7
3.4. FEM in cylindric Coordinates . . . . .	7
<b>4. Discretization of PDEs</b>	<b>7</b>
4.1. PDE for Electric potential . . . . .	7
4.1.1. Weak formulation of the problem . . . . .	7
4.1.2. Inner Domain . . . . .	8
4.1.3. Electrodes . . . . .	9
4.1.4. Outer boundary . . . . .	9
4.2. PDE for temperature Distribution . . . . .	9
4.2.1. Weak formulation . . . . .	9
<b>5. Applied FEM technologies</b>	<b>10</b>
5.1. Weak solutions . . . . .	10
5.1.1. Electric potential . . . . .	10
5.1.2. Temperature Distribution . . . . .	11
5.2. Discretization / Triangulation . . . . .	13
5.2.1. Grid generation . . . . .	13
5.2.2. Grid refinement . . . . .	13
5.3. Assembling system of equation . . . . .	13
5.3.1. Assemble elementwise . . . . .	13
5.3.2. Add boundary Conditions . . . . .	13
5.4. Error estimations . . . . .	13
5.4.1. H1-Norm . . . . .	13
5.4.2. L2-Norm . . . . .	13
5.4.3. Evtl energy norm . . . . .	13
<b>6. Numerical challenges / Numerical aspects in general</b>	<b>13</b>
6.0.1. Numerical integration . . . . .	13
6.0.2. Numerical gradient on discrete points . . . . .	13
6.0.3. Surface integral . . . . .	13
6.0.4. Solving the system of equations . . . . .	13

<b>7. Applied simulation</b>	<b>13</b>
7.1. Generating TestData / Get reference data . . . . .	13
7.2. Solving the PDEs . . . . .	13
7.3. Combine everything to continous time dependent simulation . . . . .	13
7.4. Interpretation of result numbers . . . . .	13
<b>8. Programming technologies</b>	<b>14</b>
8.1. Performance Optimization . . . . .	14
8.2. MatLab vs C++ . . . . .	14
8.3. Graphical output . . . . .	14
<b>9. Summary and Outlook</b>	<b>14</b>
9.1. Project Summary . . . . .	14
9.1.1. strengths and flaws . . . . .	14
9.1.2. future modifications . . . . .	14
9.2. State of the current Research . . . . .	14
9.3. Other FEM projects and software . . . . .	15
<b>A. Source code Visual C++</b>	<b>17</b>
<b>B. Source code MatLab</b>	<b>17</b>

## List of Figures

## List of Tables

## Listings

1.	Demo . . . . .	17
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# 1. Introduction to radio frequency ablation

Lets talk about:

- Medical Treatment of Tumor
- Radio frequency ablation
- Why RFA Simulation is important
- Motivation
- This project in General

## 2. Computer-aided simulation of radio frequency ablation

### 2.1. About Errors in simulations and numerical approaches

- see TUM dissertation
- There are different sources for errors following the simulation from the line from the real problem down to the discrete solution
- Idealization error: discrepancy between reality and the idealized reality and the idealized constitutive laws and boundary conditions -> Systems are often way more complex in reality, every patient is different
- Modeling errors: discrepancy between mathematical formulation and physical model -> e.g. using dimensionally reduced approaches, like linear dependencies or even constant parameters
- Discretization errors: discrepancy between the continuous description and discrete description of the model
- Solution errors: using iterative approximation methods and rounding errors
- It's basically a butterfly effect
- Optimizing one error source often conflicts with another one -> e.g. handling nonlinearity can cause fatal numerical errors (at least that's what Kroeger said ...)

## 2.2. The physics behind radio frequency ablation

# 3. Mathematical aspects of discrete simulation

## 3.1. Theory of finite elements

### 3.1.1. Elliptical problems

- Elliptical problems in general
- Parabolic / time-dependent problems
- build up system of PDE's to describe problem
- Using the cylindric domain, different domains

### 3.1.2. FEM for electrical fields

- special domain
- boundary conditions

### 3.1.3. FEM for temperature fields

- boundary condition (heat source or sink)

## 3.2. Solving systems of ODE over time

- This is for temperature distribution

### 3.3. Axial symmetrie

- Using axial symmetrie to simplify computations
- reducing one dimension 3D -> 2D
- significant savings calculations time and complexity
- approach: fourier decomposition in angular direction to reduce dependency on the angular  $\varphi$
- using static models, only dependency on space
- maybe Torus elements

### 3.4. FEM in cylindric Coordinates

- Rewrite the equations to cylindric coordinates

Laplace in cartesian coordinates:

$$\nabla^2 := \Delta := \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \quad (1)$$

Laplace in cylindric coordinates:

$$\Delta := \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \phi^2} + \frac{\partial^2}{\partial z^2} \quad (2)$$

Laplace in polar coordinates:

$$\Delta := \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \phi^2} \quad (3)$$

## 4. Discretization of PDEs

### 4.1. PDE for Electric potential

#### 4.1.1. Weak formulation of the problem

Three parts are interesting: - Inner domain

- Fixed Potential of electrodes

- Inner domain
- Outer boundary -> Robin

Constant material parameters:

#### 4.1.2. Inner Domain

- The electric potential of the inner domain is described as :

$$-\nabla \cdot (\sigma(x, y, z, t) \nabla \phi(x, y, z, t)) = 0 \quad (4)$$

- Elliptical boundary problem
- Assuming constant material parameters:  $\nabla \sigma = 0$
- Solution is independent from  $\sigma$  so we can cut it out - Equation becomes Laplace's equation,  $\phi$  becomes time independent

$$-\Delta \phi(x, y, z) = 0 \quad (5)$$

- Using a cylindric domain, we can use cylinder coordinates (see ref Laplace in cylinder)

$$-\Delta \phi(r, \phi, z) = -\frac{1}{r} \frac{\partial \phi}{\partial r} - \frac{\partial^2 \phi}{\partial r^2} - \frac{1}{r^2} \frac{\partial^2 \phi}{\partial \phi^2} - \frac{\partial^2 \phi}{\partial z^2} = 0 \quad (6)$$

- Since the domain has axis symmetry, the solution for  $\phi$  is independent from the angular  $\phi$
- So equation simplifies to

$$-\frac{1}{r} \frac{\partial \phi}{\partial r} - \frac{\partial^2 \phi}{\partial r^2} - \frac{\partial^2 \phi}{\partial z^2} = 0 \quad (7)$$

- PDE is now parabolic and no longer elliptic
- We will care about a more complex formulation later



### 4.1.3. Electrodes

-  $\phi = \pm 1$

### 4.1.4. Outer boundary

- For first try, a simplification with natural boundary conditions

$$n \cdot \nabla \phi = 0 \quad (8)$$

- In cylindrical coordinates

$$TODO \quad (9)$$

## 4.2. PDE for temperature Distribution

### 4.2.1. Weak formulation

Following Kroeger, the temperature distribution is modeled by the heat equation:

$$\partial_t(\rho c T) - \nabla \cdot (\lambda \nabla T) = Q \quad (10)$$

The heat equation is a well known parabolic partial differential equation.

We are assuming  $\rho$  and  $c$  are constant

$\rho$  = density

$c$  = specific heat capacity

$\lambda$  = thermal conductivity, which is depending on T

$T = T(r,z,t)$  = temperature

$Q = Q(r,z,t)$  = heat energy

Cylindrical coordinates: see 'Transient Heat Transfer in a Partially Cooled Cylindrical Rod' from Lawrence Agbezuge

$$\rho c \frac{\partial T}{\partial t} - \frac{d\lambda}{dT} \left[ \left( \frac{\partial T}{\partial r} \right)^2 + \left( \frac{\partial T}{\partial z} \right)^2 \right] - \lambda \left( \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial z^2} \right) = Q \quad (11)$$

For the first run, we assume  $\lambda$  is also constant too, which greatly reduces the complexity of the problem to the form

$$\rho c \frac{\partial T}{\partial t} - \lambda \left( \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial z^2} \right) = Q \quad (12)$$

TODO: explain Q her

$$Q = Q_{(rf)} + Q_{perf}$$

## 5. Applied FEM technologies

### 5.1. Weak solutions

#### 5.1.1. Electric potential

Electric potential / Laplace's equation in cylindrical domain:

$$a_w(u, v) := \int_{\Omega} (\partial_r u \partial_r v + \partial_z u \partial_z v) r dr dz = \int_{\Omega} f v r dr dz \quad (13)$$

$$- u \in H_r^1(\Omega) \cap \{v|_{\Gamma_0} = 0\}$$

$$- v \in H_r^1(\Omega) \cap \{v|_{\Gamma_0} = 0\}$$

Approximate with linear regression functions

Linear regression functions for reference triangles:

$$\phi_1(\xi, \eta) = 1 - \xi - \eta \quad (14)$$

$$\phi_2(\xi, \eta) = \xi \quad (15)$$

$$\phi_3(\xi, \eta) = \eta \quad (16)$$

Specific PDE for electric potential, inner domain:

$$a_w(u, v) := \int_{\Omega} (\partial_r u \partial_r v + \partial_z u \partial_z v) r dr dz = 0 \quad (17)$$

### 5.1.2. Temperature Distribution

This is basically the problem above but as a hyperbolic problem

Using semidiscrete solution and iterate solution over time

We are applying method of the discontinuous galerkein fem

For reference see Jung, Langer : Methode der finiten Elemente für Ingenieure, chapter 7.1

Weak formulation for the problem:

We are looking for  $u(r, z, t) \in V_{g1}$  with  $\dot{u} \in L_2(\Omega)$  for almost every  $t \in (0, T)$ , so

$$(\dot{u}, v)_0 + a(t; u, v) = \langle F(t), v \rangle \text{ for all } v \in V_0 \quad (18)$$

and for almost every  $t \in (0, T)$  is the "Anfangsbedingung -> suche englische Formulierung"

$$(u(r, z, 0), v)_0 = (u_0, v)_0 \text{ for all } v \in V_0 \quad (19)$$

The formal model above is given by

$$\begin{aligned} (\dot{u}, v)_0 &= \int_{\Omega} \dot{u}(r, z, t) v(r, z) r dr dz = \int_{\Omega} \frac{\partial u(r, z, t)}{\partial t} v(r, z) r dr dz, \\ a(t; u, v) &= \int_{\Omega} \left[ \lambda_1(r, z, t) \frac{\partial u}{\partial r} \frac{\partial v}{\partial r} + \lambda_2(r, z, t) \frac{\partial u}{\partial z} \frac{\partial v}{\partial z} \right] \cdot r \cdot dr dz + \int_{\Gamma_3} \alpha(r, z, t) u(r, z, t) v(r, z) ds, \\ \langle F(t), v \rangle &= \int_{\Omega} f(r, z, t) v(r, z) r dr dz + \int_{\Gamma_2} g_2(r, z, t) v(r, z) ds + \int_{\Gamma_3} \alpha(r, z, t) u_A(r, z, t) v(r, z) ds, \\ V_{g1} &= \text{TODO}, \\ V_0 &= \text{TODO} \end{aligned}$$

Adapted for the temperature distribution, assuming  $\lambda$  and all material parameters are constant:

$$a_w(t; u, v) := \int_{\Omega} \rho c (\partial_t u \cdot v) r dr dz + \int_{\Omega} \lambda (\partial_r u \partial_r v + \partial_z u \partial_z v) r dr dz = \int_{\Omega} f v r dr dz \quad (20)$$



## 5.2. Discretization / Triangulation

### 5.2.1. Grid generation

### 5.2.2. Grid refinement

## 5.3. Assembling system of equation

### 5.3.1. Assemble elementwise

### 5.3.2. Add boundary Conditions

## 5.4. Error estimations

### 5.4.1. H1-Norm

### 5.4.2. L2-Norm

### 5.4.3. Evtl energy norm

## 6. Numerical challenges / Numerical aspects in general

### 6.0.1. Numerical integration

### 6.0.2. Numerical gradient on discrete points

### 6.0.3. Surface integral

### 6.0.4. Solving the system of equations

## 7. Applied simulation

### 7.1. Generating TestData / Get reference data

### 7.2. Solving the PDEs

### 7.3. Combine everything to continuous time dependent simulation

### 7.4. Interpretation of result numbers

## 8. Programming technologies

### 8.1. Performance Optimization

### 8.2. MatLab vs C++

- Basically the performance advantages of using C++
- Combine advantages if both languages
- MatLab as documentation of the simulation

### 8.3. Graphical output

## 9. Summary and Outlook

### 9.1. Project Summary

#### 9.1.1. strengths and flaws

- why is it good, why is it bad

#### 9.1.2. future modifications

### 9.2. State of the current Research

- Research in the simulation of medical therapy methods

### 9.3. Other FEM projects and software

- FENICS
- COMSOL
- ANSYS

## References

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## A. Source code Visual C++

Listing 1: For loop to print numbers from 1 to 10

```
1 // Print numbers from 1 to 10
2 #include <stdio.h>
3 int main() {
4     int i;
5     for (i = 1; i < 11; ++i)
6     {
7         printf("%d_", i);
8     }
9     return 0;
10 }
```

---

## B. Source code MatLab

TODO